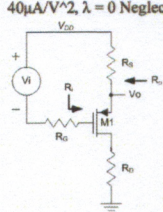


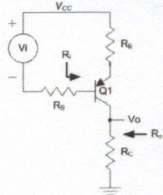
30. What is the low frequency output resistance, R_o , in Ω for the amplifier shown at 27°C with $R_d = 35.2\text{k}\Omega$, $R_s = 0.6\text{k}\Omega$ and $R_g = 9.5\text{k}\Omega$. Use: $W/L = 67$, $I_d = 156\mu\text{A}$, $V_{TP} = -0.5\text{V}$, $k'_p = 40\mu\text{A/V}^2$, $\lambda = 0$ Neglect body effect.



$$g_m = \sqrt{2 \cdot k'_p \cdot (W/L) \cdot I_d} = \sqrt{2 \cdot (40 \times 10^{-6}) \cdot (67) \cdot (156 \times 10^{-6})} = 0.0009144$$

$$R_o = R_s \parallel 1/g_m = \frac{1}{\frac{1}{600} + 0.0009144} = \frac{1}{0.002581085} = 387.4\Omega$$

29. What is the low frequency output resistance, R_o , in $\text{k}\Omega$ for the amplifier shown at 27°C with $R_c = 62.3\text{k}\Omega$, $R_e = 0.9\text{k}\Omega$ and $R_b = 0.9\text{k}\Omega$? Use: $I_c = 28\mu\text{A}$, $\beta = 22$, $V_A = 10\text{V}$, and $V_t = kT/q = 26\text{mV}$. Use the "short-cut approach" discussed in class.



$$g_m = \frac{I_c}{V_t} = \frac{(28 \times 10^{-6})}{(26 \times 10^{-3})} = 0.001077$$

$$r_{\pi} = \frac{\beta}{g_m} = 20428.57$$

$$r_o = \frac{V_A}{I_c} = \frac{10}{(28 \times 10^{-6})} = 357142.86$$

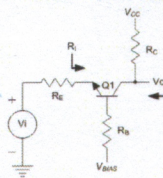
$$R_{o1} = r_o \left[1 + \frac{\beta R_E}{R_b + R_E + r_{\pi}} \right] + \frac{R_E}{1 + \left(\frac{R_E}{r_{\pi} + R_b} \right)}$$

$$= 357142.86 \left[1 + \frac{22 \cdot 900}{900 + 900 + 20428.57} \right] + \frac{900}{1 + \left(\frac{900}{20428.57 + 900} \right)} = 675266.28 + 863.56 = 676129.84$$

$$R_o = R_c \parallel R_{o1} = \frac{1}{\frac{1}{62300} + \frac{1}{676129.84}} = \frac{1}{0.00001753} = 57043.86\Omega = 57.04\text{k}\Omega$$

57.2 k Ω (moodle)

26. What is the low frequency voltage gain for the amplifier shown at 27°C with $R_c = 40.6\text{k}\Omega$, $R_e = 0.1\text{k}\Omega$ and $R_b = 0.5\text{k}\Omega$? Use: $I_c = 48\mu\text{A}$, $\beta = 197$, and $V_t = kT/q = 26\text{mV}$. Neglect the effect of base-width modulation.



$$g_m = \frac{I_c}{V_t} = \frac{(48 \times 10^{-6})}{(26 \times 10^{-3})} = 0.001846$$

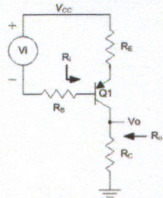
$$V_{BE} = -V_i \cdot \frac{1}{1 + g_m \left(\frac{R_b}{\beta + 1} + R_E \right)}$$

$$V_o = -g_m V_{BE} R_c \rightarrow \frac{V_o}{V_i} = g_m R_c \left(\frac{1}{1 + g_m \left(\frac{R_b}{\beta + 1} + R_E \right)} \right) \Rightarrow \frac{V_o}{V_i} = \frac{g_m R_c}{1 + \frac{g_m R_b}{\beta + 1} + g_m R_E}$$

$$\frac{0.001846 \cdot 40600}{1 + \left(\frac{0.001846 \cdot 500}{197 + 1} \right) + (0.001846 \cdot 100)} =$$

63.02 (calculated)
62.97 (moodle answer)

25. What is the low frequency voltage gain for the amplifier shown at 27°C with $R_c = 36.6\text{k}\Omega$, $R_e = 0.1\text{k}\Omega$ and $R_b = 1.0\text{k}\Omega$? Use: $I_c = 971\mu\text{A}$, $\beta = 44$, and $V_t = kT/q = 26\text{mV}$. Neglect the effect of base-width modulation.

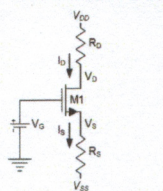


$$g_m = \frac{I_c}{V_t} = \frac{(971 \times 10^{-6})}{(26 \times 10^{-3})} = 0.037346$$

$$r_{\pi} = \frac{\beta}{g_m} = \frac{44}{0.037346} = 1178.167$$

$$A_v = \frac{-\beta R_c}{R_b + r_{\pi} + (\beta + 1) R_E} = \frac{(-44)(36600)}{1000 + 1178.167 + (45 \cdot 100)} = -241.14$$

24. For the MOSFET bias circuit shown, what value of R_d in kilohms is needed to allow the maximum possible peak-to-peak signal swing on the drain without clipping? Use: $V_{DD} = 8\text{V}$, $V_{SS} = -7\text{V}$, $V_g = -0.6\text{V}$, $R_s = 4.8\text{k}\Omega$, $V_t = 0.5\text{V}$, and $V_{on} = 0.15$. (Remember that $V_{on} = V_{ov} = V_{gs} - V_t$) Neglect the effect of channel-length modulation and body effect. (Hint: Be sure to keep the MOSFET in saturation!)

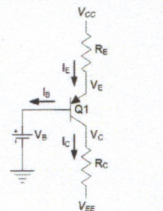


$$V_{GS} = V_{GN} + V_t = 0.15 + 0.5 = 0.65$$

$$-V_G + V_{GS} + I_S R_s + V_{SS} = 0 \rightarrow -(-0.6) + 0.65 + I_S (4800) + 7\text{V} = 0 \rightarrow I_S = \frac{-8.25}{4800} = -0.00172 \quad I_S = I_D$$

$$V_G = V_{GS} - V_t = 0.65 - 0.5 = 0.15\text{V}$$

23. For the BJT bias circuit shown, what is the base current, I_b , in microamps? Use $V_{CC} = 7\text{V}$, $V_{EE} = -8\text{V}$, $V_b = 2.9\text{V}$, $R_c = 1.8\text{k}\Omega$, and $R_e = 6.8\text{k}\Omega$. Assume that the transistor is in the forward-active region, with $\beta = 46$ and $|V_{be(on)}| = 0.7\text{V}$. Neglect the effects of base-width modulation.



$$V_E = V_{be} + V_b = 0.7 + 2.9 = 3.4$$

$$I_E = \frac{V_{CC} - V_E}{R_E} = \frac{7 - 3.4}{6800} = 0.0005$$

$$I_B = \frac{I_E}{(1 + \beta)} = \frac{0.0005}{(1 + 46)} = 0.000010638\text{A} = 10.6\mu\text{A}$$