第十一章 耦合电感和理想变压器

作业

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练习

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§ 11-1 11-2 耦合电感概念、VCR、耦合系数

电感元件

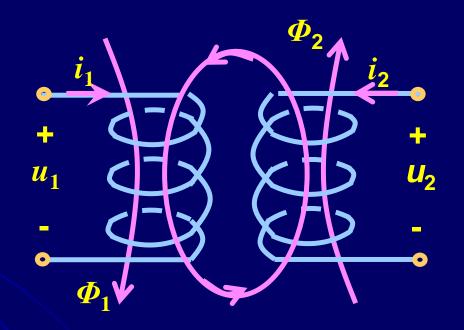
线性电感 Ψ=Li

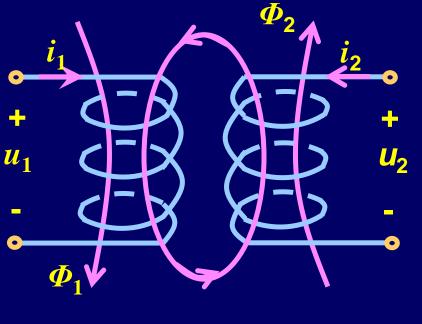
$$i$$
 $+u$

$$u = \frac{d\psi}{dt} = L\frac{di}{dt}$$
 (关联参考方向)

一. 耦合电感的伏安关系

设有两个靠近的线性定常电感线圈





$$\Psi_1 = \Psi_{11} + \Psi_{12} = L_1 i_1 + M_{12} i_2$$

$$\Psi_2 = \Psi_{22} + \Psi_{21} = L_2 i_2 + M_{21} i_1$$

 $M_{12} = M_{21} = M$

$$U_{1}(t) = \frac{d\psi_{1}}{dt} = L_{1}\frac{di_{1}}{dt} + M\frac{di_{2}}{dt}$$

$$U_{2}(t) = \frac{d\psi_{2}}{dt} = L_{2}\frac{di_{2}}{dt} + M\frac{di_{1}}{dt}$$

 i_1 流过第一个线圈产生自感磁链 $\Psi_{11}=L_1i_1$ 且在第二个线圈产生 互感磁链 $\Psi_{21}=M_{21}i_1$

i₂流过第二个线圈产生自感磁链Ψ₂₂=L₂i₂ 且在第一个线圈产生 互感磁链Ψ₁₂=M₁₂i₂

> 当自感磁通与互感磁通 方向不一致时:

$$u_{1}(t) = L_{1}\frac{di_{1}}{dt} - M\frac{di_{2}}{dt}$$

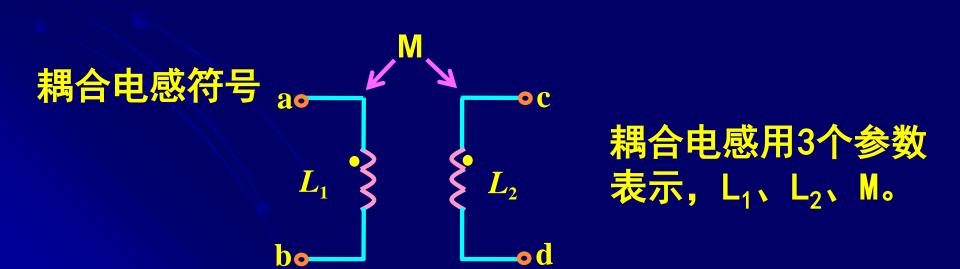
$$u_{2}(t) = L_{2}\frac{di_{2}}{dt} - M\frac{di_{1}}{dt}$$

(1) 自感压降的正负:

当线圈的电压电流关联参考方向时取正,否则取负。

(2) 互感压降的正负:

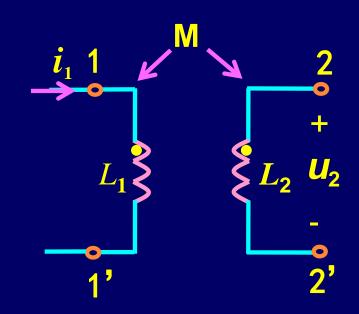
自感磁通与互感磁通一致取正,否则取负,取决于线圈的绕向、电流的参考方向、线圈的相互位置。由于线圈的绕向常常无法知道,需引入同名端(•或*),以标示互感电压的正负。



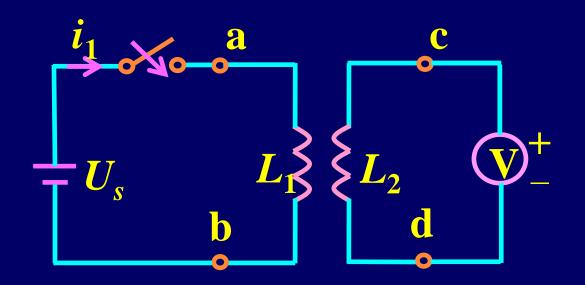
二. 同名端

1 定义

约定在产生互感电压的电流参考方向的流入端、互感电压 参考极性的"+"均用"•"标示,称为同名端。



2 用实验方法确定同名端

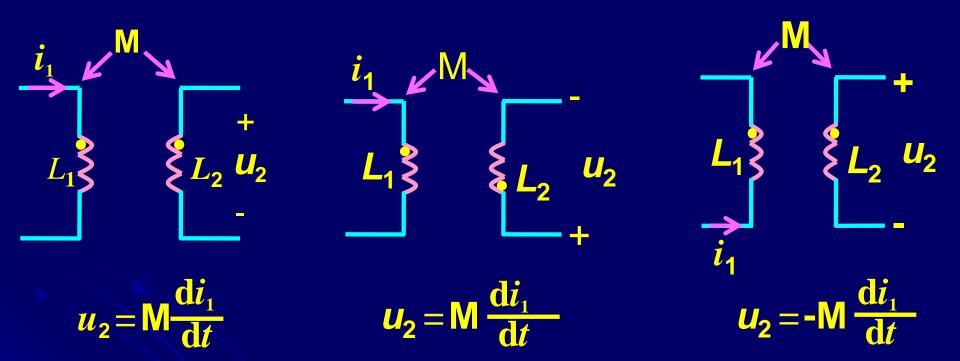


开关闭合后:

若电压表指针正向偏转,则c点电位高, a、c为同名端; 若电压表指针反向偏转,则d点电位高, a、d为同名端.

3. 根据同名端确定互感电压的正负

电流与互感电压的参考方向对同名端一致



4 总结耦合电感的VCR:

(1) 一般情况时:

$$u_{1}(t) = \pm L_{1} \frac{di_{1}}{dt} \pm M \frac{di_{2}}{dt}$$

$$u_{2}(t) = \pm L_{2} \frac{di_{2}}{dt} \pm M \frac{di_{1}}{dt}$$

(2) 正弦稳态时:

$$\dot{U}_1 = \pm j\omega L_1 \dot{I}_1 \pm j\omega M \dot{I}_2$$

$$\dot{U}_2 = \pm j\omega L_2 \dot{I}_2 \pm j\omega M \dot{I}_1$$

三 耦合系数

耦合系数
$$K = \frac{M}{M_{\text{max}}}$$
 用来衡量两线圈耦合程度。

0≤K≤1

Æ1时:全耦合,此时 M=M_{max}

作○时: 无耦合

推导 M_{max}= ?

$$\Psi_{11} = N_1 \Phi_{11} = L_1 i_1$$
 $\Psi_{22} = N_2 \Phi_{22} = L_2 i_2$
 $L_2 = \frac{N_2 \Phi_{22}}{i_2}$
 $L_1 = \frac{N_1 \Phi_{11}}{i_1}$
 $L_2 = \frac{N_2 \Phi_{22}}{i_1}$

$$\Psi_{21} = N_2 \Phi_{21} = Mi_1$$
 $\Psi_{12} = N_1 \Phi_{12} = Mi_2$
 $M^2 = \frac{N_2 \Phi_{21}}{i_1} \frac{N_1 \Phi_{12}}{i_2}$

全耦合时:
$$\Phi_{21} = \Phi_{21 \text{max}} = \Phi_{11}$$

$$\Phi_{12} = \Phi_{12\text{max}} = \Phi_{22}$$

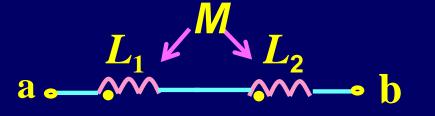
此时
$$\mathbf{M}^2 = \mathbf{M}^2_{\text{max}} = \frac{\mathbf{N}_2 \Phi_{11}}{i_1} \frac{\mathbf{N}_1 \Phi_{22}}{i_2} = L_1 L_2$$

全耦合时:
$$M = M_{\text{max}} = \sqrt{L_1 L_2}$$

四、耦合电感线圈的串联和并联

1. 串联

(1) 串联顺接: 异名端相接



a
$$\stackrel{i}{\longrightarrow} \stackrel{L_1}{\longrightarrow} \stackrel{L_2}{\longrightarrow} \stackrel{b}{\longrightarrow} \stackrel{b}{\longrightarrow$$

$$u_{ab} = L_1 \frac{di}{dt} + M \frac{di}{dt} + L_2 \frac{di}{dt} + M \frac{di}{dt}$$
$$= (L_1 + L_2 + 2M) \frac{di}{dt}$$

等效电感 $L=L_1+L_2+2M$

(2) 反接: 同名端相接

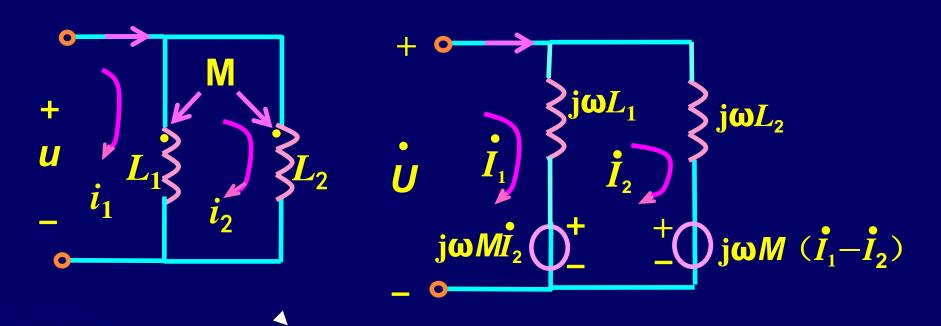
等效电感 $L=L_1+L_2-2M$

正弦稳态时:

顺接等效阻抗 $Z=j\omega L_1+j\omega L_2+2j\omega M$

反接等效阻抗 $Z=j\omega L_1+j\omega L_2-2j\omega M$

2. 正弦稳态时耦合电感的并联(自己推导) (1) 同名端相接时:



列回路方程:

$$\begin{cases} j \omega L_{1} \dot{I}_{1} - j \omega L_{1} \dot{I}_{2} = \dot{U} - j \omega M \dot{I}_{2} \\ -j \omega L_{1} \dot{I}_{1} + (j \omega L_{1} + j \omega L_{2}) \dot{I}_{2} = -j \omega M (\dot{I}_{1} - \dot{I}_{2}) + j \omega M \dot{I}_{2} \end{cases}$$

解出:
$$\dot{I}_1 = \frac{(L_1 + L_2 - 2M)}{j \omega (L_1 L_2 - M^2)} \dot{U}$$

$$Z = \frac{\dot{U}}{\dot{I}_{1}} = \frac{j\omega(L_{1}L_{2} - M^{2})}{L_{1} + L_{2} - 2M}$$

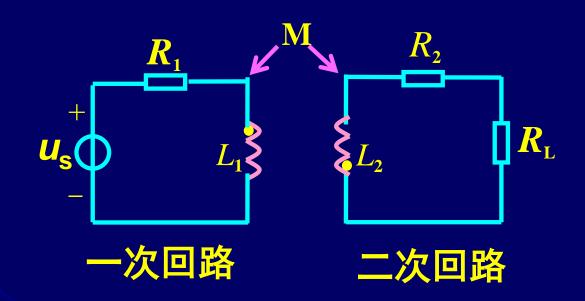
等效电感
$$L = \frac{L_1 L_2 - M^2}{L_1 + L_2 - 2M}$$

(2) 异名端相接时:

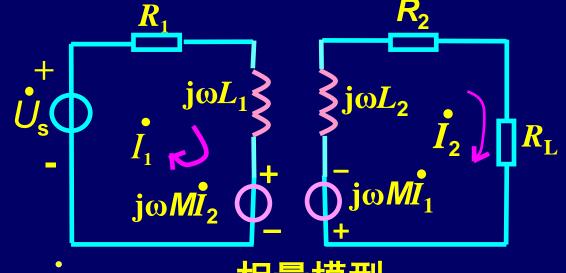
等效电感
$$L = \frac{L_1 L_2 - M^2}{L_1 + L_2 + 2 M}$$

§ 11-3 正弦稳态时空心变压器电路的分析 反映阻抗

• 一. 电路模型



1. 回路法求解电流



$$(R_1 + \mathbf{j}_{\omega}L_1)\dot{I}_1 = -\mathbf{j}_{\omega}M\dot{I}_2 + \dot{U}_S$$

相量模型

$$(R_2 + R_L + j\omega L_2)I_2 = -j\omega MI_1$$

解出:

$$\dot{I}_1 = \frac{Z_{22}U_S}{Z_{11}Z_{22} + \omega^2 M^2}$$

则
$$\dot{I}_2 = \frac{-j \omega M \dot{I}_1}{Z_{22}}$$

分析: (1) 若同名端位置不同, 对1, 无影响,

而 I_2 则改变符号。

(2) 初级看进去的等效阻抗:

$$Z_{i} = \frac{\dot{U}_{S}}{\dot{I}_{1}} = Z_{11} + \frac{\omega^{2} M^{2}}{Z_{22}}$$

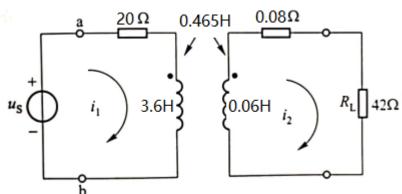
$$\frac{\omega^{2} M^{2}}{Z_{22}} - 反映阻抗Z_{ref}$$

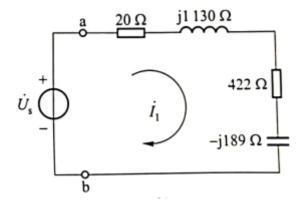
$$\frac{\dot{U}_{S}}{\dot{U}_{S}} - \frac{\omega^{2} M^{2}}{Z_{22}}$$

引入新解法----反映阻抗法

$$\dot{I}_{1} = \frac{\dot{U}_{S}}{Z_{i}} = \frac{\dot{U}_{S}}{Z_{11} + \frac{\omega^{2} M^{2}}{Z_{122}}} \qquad \qquad \dot{I}_{2} = \frac{-j\omega M \dot{I}_{1}}{Z_{22}}$$

例11-5 11-6 求电流 \mathbf{i}_1 、 \mathbf{i}_2 ,已知 \mathbf{u}_S =115 $\sqrt{2}\cos(314t)$ V





解:

$$Z_{11} = R_1 + j\omega L_1 = (20 + j314 \times 3.6) \Omega = (20 + j1130) \Omega$$

$$Z_{22} = R_L + R_2 + j\omega L_2 = (42.08 + j314 \times 0.06) \Omega$$

= 46.1 \(\sum 24.1^\circ \Omega\)

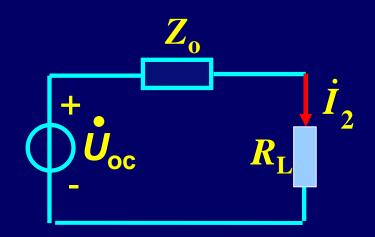
$$Z_{\text{ref}} = \frac{\omega^2 M^2}{Z_{22}} = \frac{314^2 \times 0.465^2}{46.1 / 24.1^{\circ}} \Omega$$
$$= 462.4 / -24.1^{\circ} \Omega = (422 - j189) \Omega$$

$$Z_{ab} = Z_{11} + Z_{ref} = (20 + j1130 + 422 - j189) \Omega = 1040 / 64.8^{\circ} \Omega$$

$$\vec{I}_1 = \frac{115 / 0^{\circ}}{1040 / 64.8^{\circ}} A = 110.6 / -64.8^{\circ} mA$$

$$\vec{I}_2 = \frac{j\omega M \ \vec{I}_1}{Z_{22}} = \frac{314 \times 0.465 \ / 90^{\circ} \times 110.6 \times 10^{-3} \ / -64.8^{\circ}}{46.1 \ / 24.1^{\circ}} = 0.35 \ / 1.1^{\circ} A$$

例11-6: 上题用戴维南定理求
$$\mathbf{I}_2$$
 以 \mathbf{R}_1 以 \mathbf{R}_2 并 $\mathbf{I}_{0c}=\mathbf{j}\omega\mathbf{M}\mathbf{I}_{10}$ 以 $\mathbf{I}_{10}=\frac{\dot{\mathbf{U}}_s}{Z_{11}}=\frac{115\ \angle 0^\circ}{20+\ \mathbf{j}1130}=101.7\angle -89^\circ$ mA $\dot{\mathbf{U}}_{OC}=\mathbf{j}\ \omega\ \mathbf{M}\dot{\mathbf{I}}_{10}$ 以 \mathbf{I}_{10} 以 \mathbf{I}_{10} 以 \mathbf{I}_{10} 以 \mathbf{I}_{20} 的 \mathbf{I}_{20} 以 \mathbf{I}_{20} 的 $\mathbf{I}_{$



(3)
$$\dot{\mathbf{I}}_{2} = \frac{\dot{\mathbf{U}}_{oc}}{Z_{0} + R_{L}} = \frac{14.8 \angle 1^{\circ}}{0.41 - j0.04 + 42} = 0.35 \angle 1.1^{\circ} A$$

例11-7: 求AB端的等效电感。

解:用Zref求解。

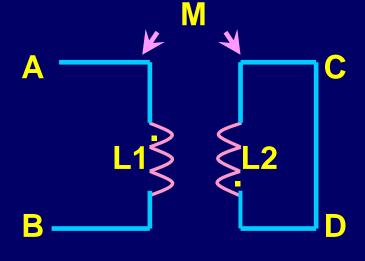
$$Z_{AB} = Z_{11} + \frac{\omega^2 M^2}{Z_{22}}$$

$$Z_{11} = j\omega L_1$$

$$Z_{22} = j\omega L_2$$

$$Z_{AB} = j\omega L_1 + \frac{\omega^2 M^2}{j\omega L_2} = j\omega L_1 - \frac{j\omega M^2}{L_2} = j\omega \left(L_1 - \frac{M^2}{L_2} \right)$$

$$L_{AB} = L_1 - \frac{M^2}{L_2}$$



§11-4 耦合电感的去耦等效变换

对于在一个公共端相连的一对耦合电感,可用三个电感组成的T形网络来等效。

1、同名端在公共端

$$i_{1} \qquad M \qquad i_{2}$$

$$u_{1} \qquad L_{1} \qquad L_{2} \qquad u_{2}$$

$$U_{1}(t) = L_{1} \frac{di_{1}}{dt} + M \frac{di_{2}}{dt}$$

$$u_{2}(t) = L_{2} \frac{di_{2}}{dt} + M \frac{di_{1}}{dt}$$

若两电路对外等效,则对应的 $\frac{dl_1}{dt}$ 及 $\frac{di_2}{dt}$ 系数相等

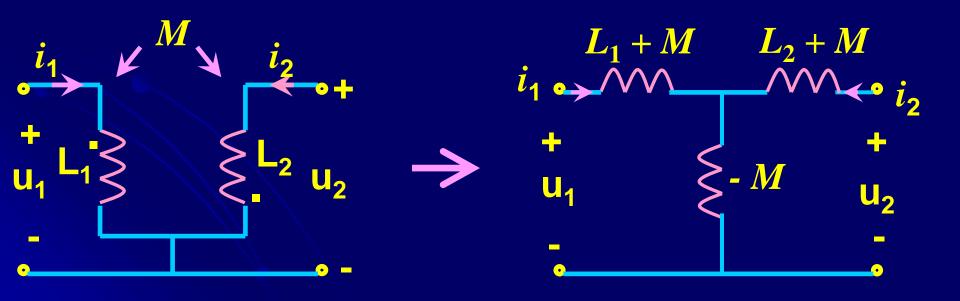
$$\begin{pmatrix} L_1 = L_a + L_b \\ L_2 = L_c + L_b \end{pmatrix} = \begin{pmatrix} L_a = L_1 - M \\ L_b = M \\ L_c = L_2 - M \end{pmatrix}$$

2、异名端在公共端

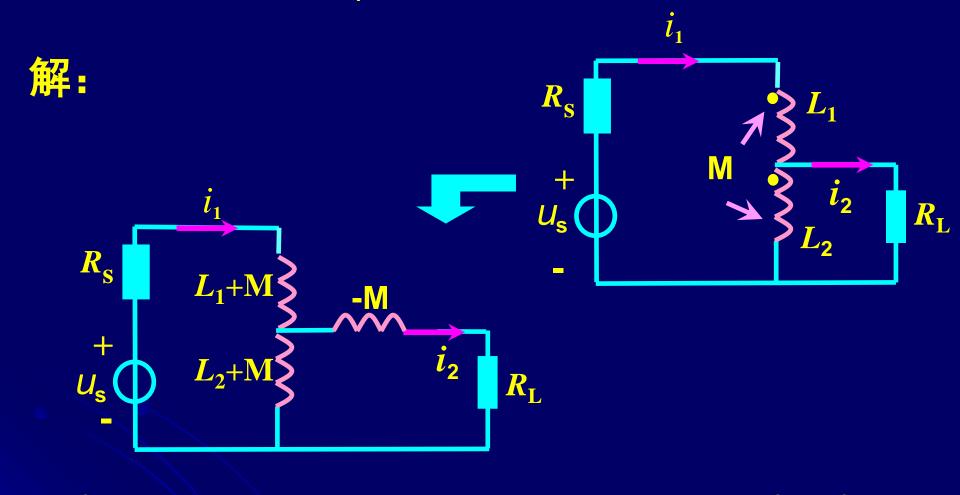
$$L_a = L_1 + M$$

$$L_b = -M$$

$$L_c = L_2 + M$$



例11-9:写出求 i, i, 所需的方程组。

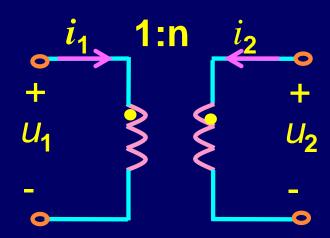


$$I_1[R_s + j\omega(L_1 + L_2 + 2M)] - j\omega(L_2 + M)I_2 = U_s$$

$$-j\omega(L_2 + M)I_1 + (R_L + j\omega L_2)I_2 = 0$$

§ 11-5 理想变压器的 VCR

- 一. 理想变压器的伏安关系
 - 1.电路模型



$$u_2 = nu_1$$

$$i_2 = -\frac{1}{n}i_1$$

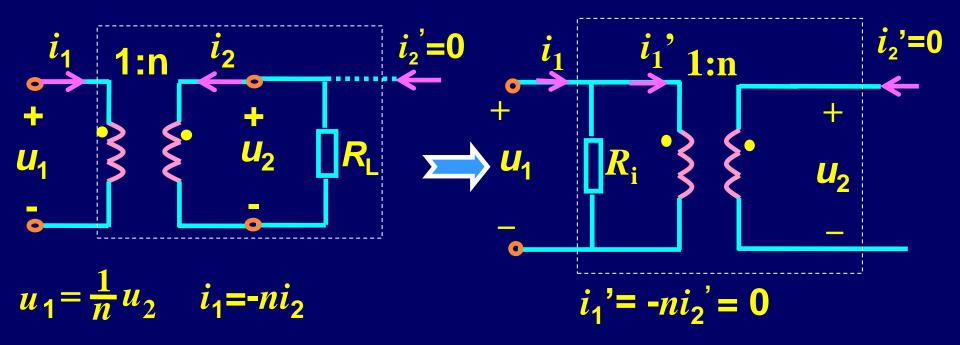
- (1) 两电压高电位端与同名端一致时, 电压比取正, 反之取负。
- (2) 两电流都从同名端流进时, 电流比取负; 反之取正。

匝数比
$$n = \frac{N_2}{N_1}$$

$$p = u_2 i_2 + u_1 i_1 = n u_1 (-\frac{1}{n} i_1) + u_1 i_1 = 0$$

理想变压器既不消耗能量也不储存能量。

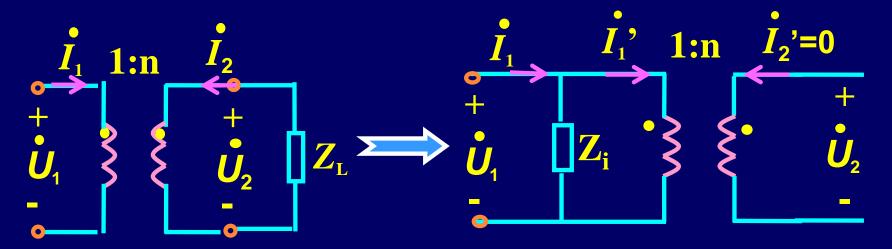
§ 11-6 理想变压器的阻抗变换性质



$$R_i = \frac{u_1}{i_1} = \frac{\frac{1}{n}u_2}{-ni_2} = -\frac{1}{n^2}\frac{u_2}{i_2} = \frac{1}{n^2}R_L$$
 $\therefore R_i = \frac{1}{n^2}R_L$

n>1 电阻折合到初级变小 n<1 电阻折合到初级变大

该结论适于阻抗:

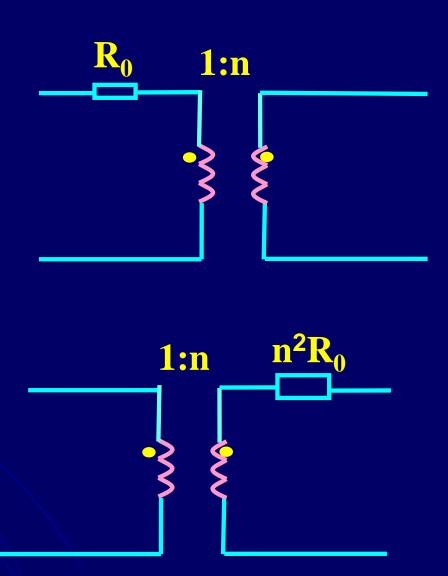


$$Z_{i} = \frac{\dot{U}_{1}}{\dot{I}_{1}} = \frac{\frac{1}{n}\dot{U}_{2}}{-n\dot{I}_{2}} = -\frac{1}{n^{2}}\frac{\dot{U}_{2}}{\dot{I}_{2}} = \frac{1}{n^{2}}Z_{L}$$

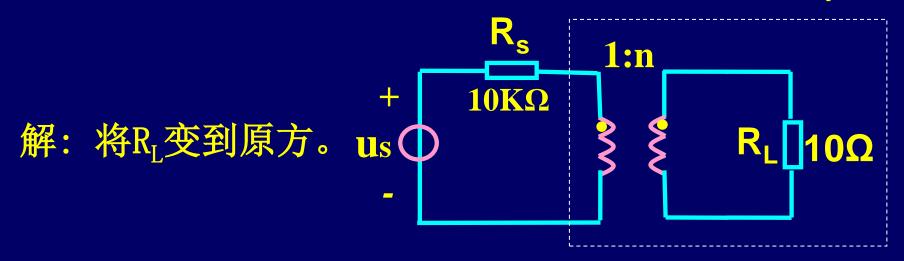
$$Z_{i} = \frac{1}{n^{2}}Z_{L}$$

理想变压器有变换阻抗的性质,可以实现最大功率匹配。

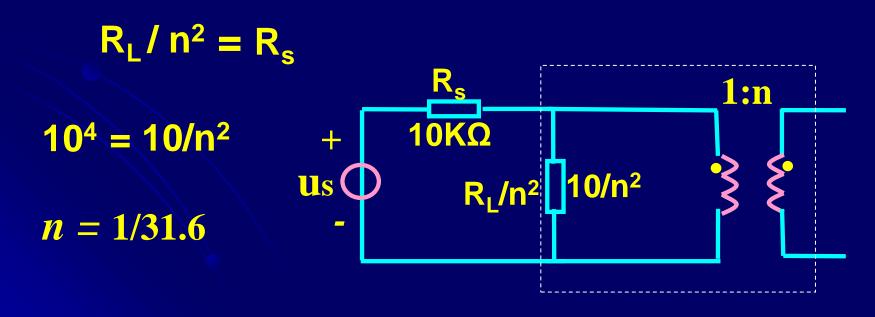
阻抗由原方 ⇒付方:



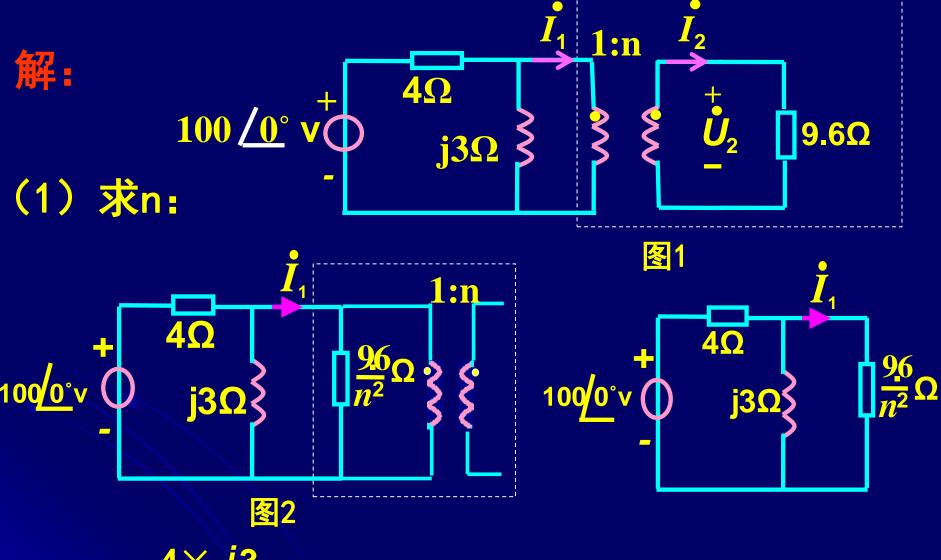
例11-10: 求使负载获得最大功率时的匝比n。



 R_L 在付方获最大功率相当于 R_L/n^2 在原方获最大功率。



补充例1: 求负载获得最大功率时的匝比n,求功率 P_{Lmax} 。



$$Z_0 = \frac{4 \times j3}{4 + j3} = 2.4 \angle 53.1^{\circ}\Omega$$
 $\frac{9.6}{n^2} = 2.4$ $n = 2$

(2) 求 P_{L max}

法1: 图2中,求 $\frac{9.6}{n^2}\Omega$ 的功率,为最大功率

100/0° v j3
$$\Omega$$
 $\frac{1}{9.6} = 2.4\Omega$

$$\vec{I}_1 = \frac{100 \angle 0^{\circ}}{4 + j3 / / 2.4} \times \frac{j3}{j3 + 2.4} = 13.986 \angle 26.54^{\circ} A$$

在图2中求 $\frac{9.6}{n^2}$ Ω 的功率,得最大功率:

$$P_{1 \text{ max}} = 13.986^2 \times 2.4 = 496.46 \text{ W}$$

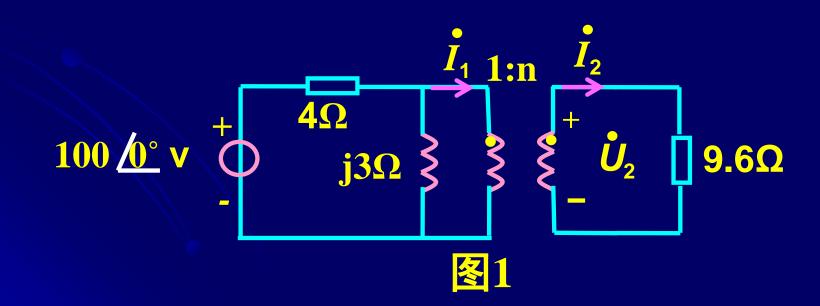
法2:

在图1中求9.6 Ω 的功率,为最大功率:

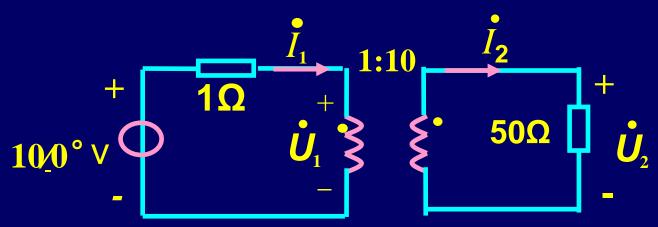
已求出
$$I_1 = 13.986 \angle 26.54$$
 A

$$\dot{I}_2 = \frac{1}{2}\dot{I}_1 = 6.993\angle 26.54^{\circ}A$$

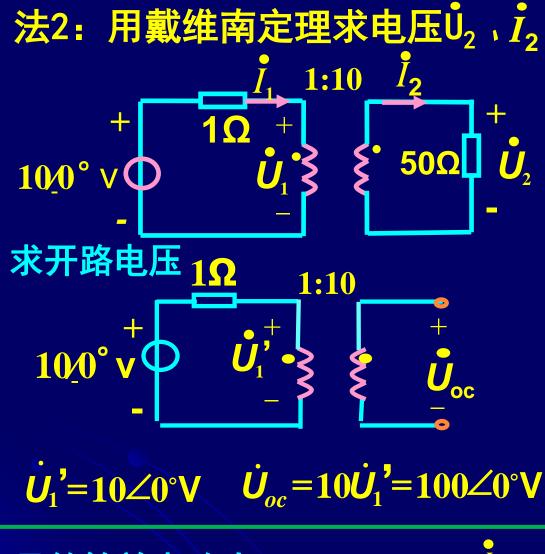
$$P_{L \text{max}} = 6.993^2 \times 9.6 = 496.46 \text{W}$$



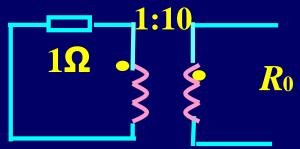
例11-11 求图示电路中 $\dot{\mathbf{U}}_1$ 、 $\dot{\mathbf{U}}_2$ 、 $\dot{\mathbf{I}}_1$ 、 $\dot{\mathbf{I}}_2$

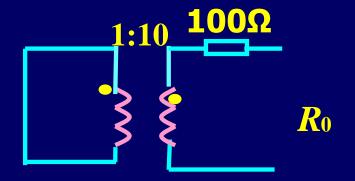


法1: 用阻抗折合的方法,把负载阻抗折合到初级



求等效阻抗R₀

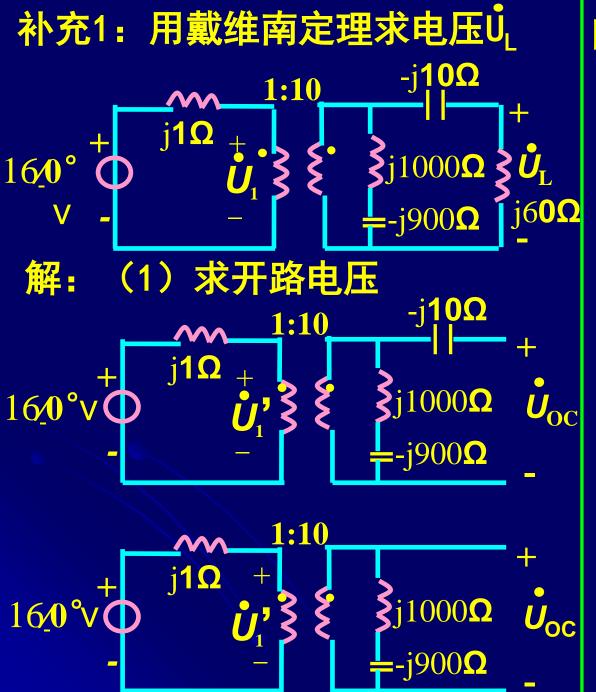




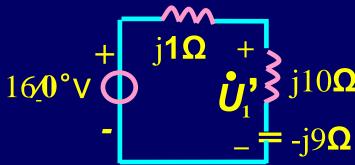
$$R_0 = 100 \Omega$$

$$\dot{U}_2 = \frac{100}{3} \angle 0^{\circ} V$$

$$\dot{I}_2 = \frac{2}{3} \angle 0^{\circ} A$$



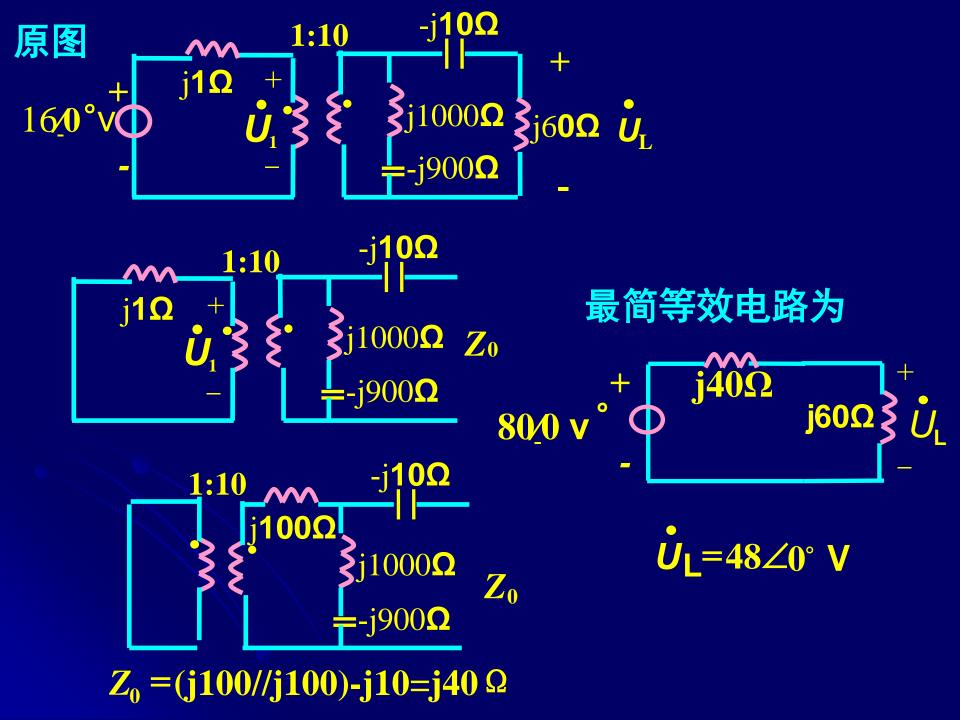
阻抗折合法求开路电压

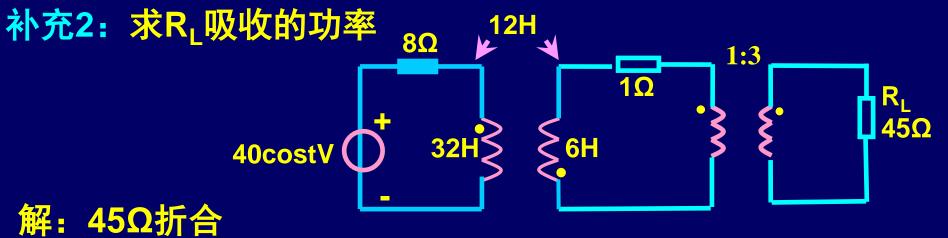


$$\dot{U}_{1}'=8 \angle 0^{\circ} \text{ V}$$

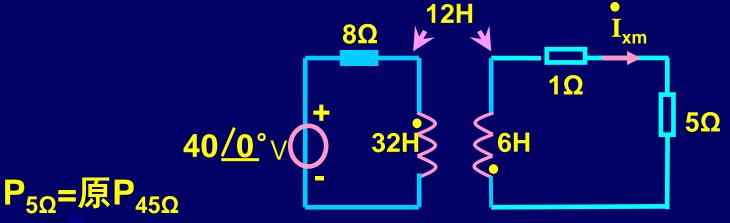
$$\dot{U}_{OC}=10\dot{U}_{1}=80\angle 0^{\circ} \text{ V}$$

(2) 求等效阻抗Z₀









$$P_{5\Omega}=5I_x^2$$

现求Ix

用戴维南定理求 İx

(1) 求
$$\dot{\mathbf{U}}_{\text{ocm}} = -j\omega \mathbf{M} \dot{\mathbf{I}}_{10m}$$

$$40/0^{\circ} \mathbf{V}$$

$$\mathbf{\dot{I}}_{10m} = \frac{\dot{\mathbf{U}}_{\text{sm}}}{\mathbf{Z}_{11}} = \frac{40 \angle 0^{\circ}}{8+ j32} \mathbf{A}$$

$$\dot{\mathbf{U}}_{\text{ocm}} = -j12 \times \frac{40 \angle 0^{\circ}}{8+ j32} \mathbf{V}$$

$$\mathbf{\dot{U}}_{\text{ocm}} = -j12 \times \frac{40 \angle 0^{\circ}}{8+ j32} \mathbf{V}$$

$$\mathbf{\dot{Z}}_{0} = \mathbf{\dot{Z}}_{22} + \frac{\mathbf{\dot{M}}^{2} \omega^{2}}{\mathbf{\dot{Z}}_{11}} = 1+j6 + \frac{144}{8+j32} \Omega$$

$$\mathbf{\dot{U}}_{\text{ocm}} = -j12 \times \frac{40 \angle 0^{\circ}}{8+ j32} \mathbf{\dot{U}}_{\text{ocm}}$$

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(3)
$$\dot{\mathbf{I}}_{xm} = \frac{\dot{\mathbf{U}}_{ocm}}{Z_0 + R_L} = -2 = 2 / 180^\circ \text{ A}$$
 $P_{RL} = (2^2 \div 2) \times 5 = 10 \text{W}$