



Overview/Scope

Cranfield has two aims:

- Develop an internal temperature estimator that can be embedded in the ICP.
- Help 'prove' the benefits of the ICP by quantifying improvements in modelling and state estimation accuracy.

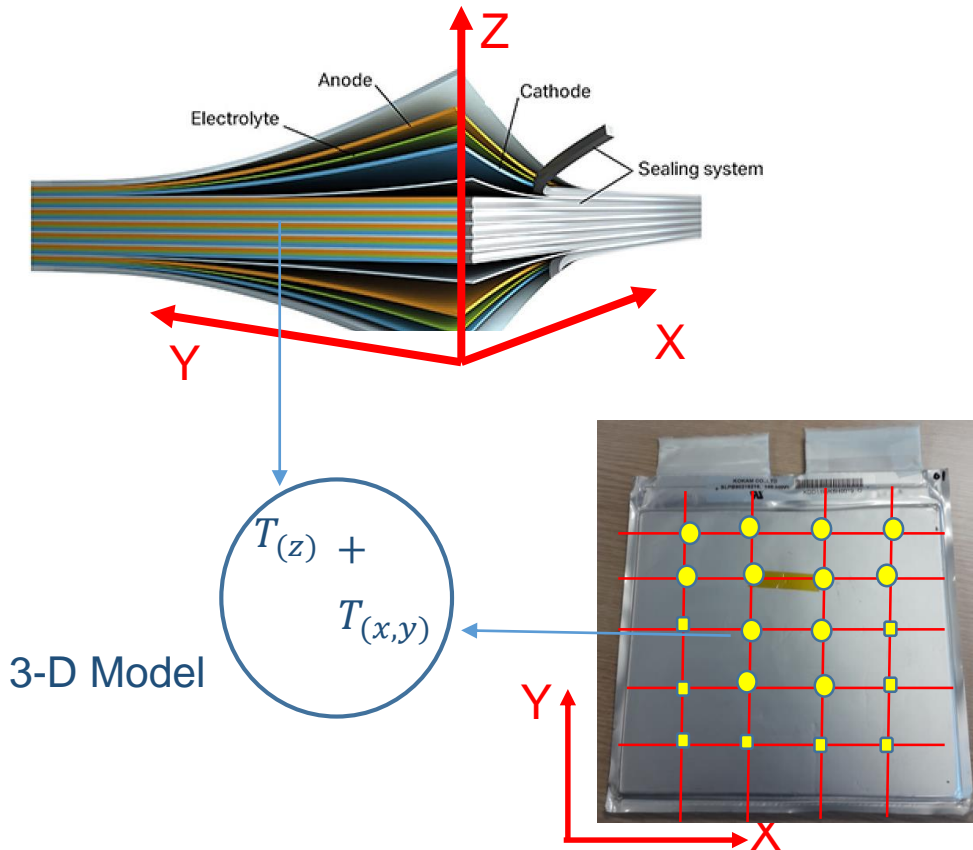


Recap: thermal modelling, temperature prediction and thermal controllability

1-D modelling and the calibration into ICP software and firmware	<ul style="list-style-type: none">• Galerkin Method (<i>GM</i>)• GM using FDM (<i>Open-Loop</i>)• A closed-loop control system using FEM-based GM and state observer	Progress: <ul style="list-style-type: none">• ICP deliverable: 1-D model with state observation and feedback control.• Next step for 1-D model: Model verification and its calibration into software and firmware.
2-D / 3-D modelling, and the innovative methodology	<ul style="list-style-type: none">• GM, FDM, and FEM• Novel FD-FEM for thermal modelling in both horizontal and vertical directions• Consider thermal effects from the perspective of electrochemical reactions, materials and structure reformulation.	Reasons: <p>(1) Different properties in size and thermal conductivities horizontally and vertically; (2) with different level of meshing, FEM and FDM complement with accuracy and calculation speed respectively; (3) thermal nonlinearities introduced by materials, electrochemical reactions, and structure changes.</p>
Thermal Controllability and a strong promotion	<ul style="list-style-type: none">• To replace CFD MSMD module for battery cell with essential prediction and stronger controllability.• Aims on one Nature Scientific Report and one Nature Energy article.	Expected results: <p>Significant application for controllable thermal management for ICP cells; A systematic research on macro and micro thermal modelling.</p>

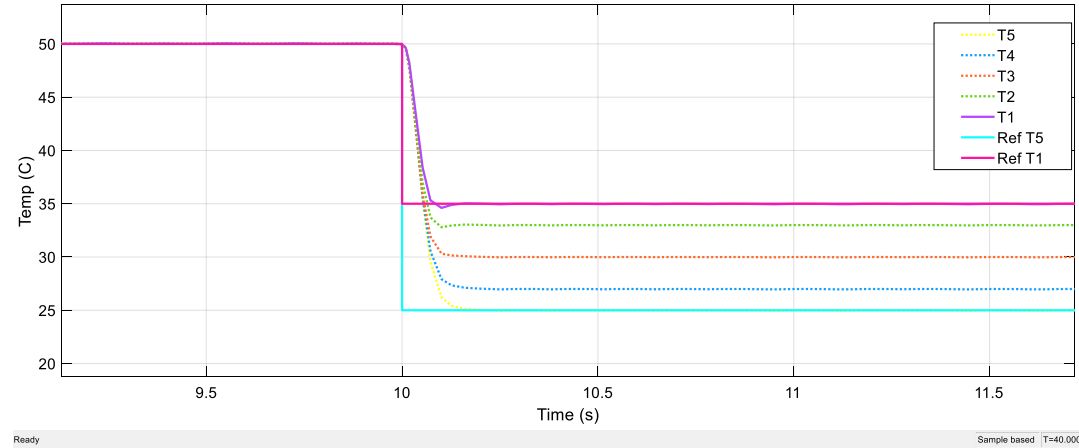
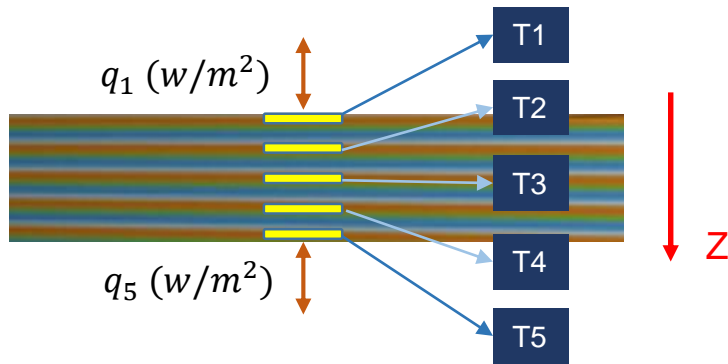
Recap: thermal modelling, temperature prediction and thermal controllability

Help to understand the previous page



- Narrow size along **Z** direction, with varying thermal conductivities between layers and higher requirement of meshing accuracy; **[FEM adopted]**
- Wide size along **X or Y** direction, with lower requirement of meshing accuracy; **[FDM adopted]**
- **Compromise** between FEM and FEM, to reach faster calculation.
- Consider factors like materials, electrochemical reactions, and structure / mechanical changes.

Work finished in January 2020: 1-D modelling with GM & FEM



```
%% Original system
A = [-276.6036 350.8143 -94.4500 26.9857 -6.7464 ;
     175.4071 -323.8286 188.9000 -53.9714 13.4929 ;
     -47.2250 188.9000 -283.3500 188.9000 -47.2250 ;
     13.4929 -53.9714 188.9000 -323.8286 175.4071 ;
     -6.7464 26.9857 -94.4500 350.8143 -276.6036 ];

B = [-0.00001674 0; -0.00001674 -0.00001674; -0.00001674 -0.00001674;
     -0.00001674 -0.00001674; 0 -0.00001674];

C = [1 0 0 0 0; 0 0 0 0 1];
Cforall = [1 0 0 0 0; 0 1 0 0 0; 0 0 1 0 0; 0 0 0 1 0; 0 0 0 0 1];

%% Extended system for tracking control of T1 and T5
Aa = [-276.6036 350.8143 -94.4500 26.9857 -6.7464 0 0;
     175.4071 -323.8286 188.9000 -53.9714 13.4929 0 0;
     -47.2250 188.9000 -283.3500 188.9000 -47.2250 0 0;
     13.4929 -53.9714 188.9000 -323.8286 175.4071 0 0;
     -6.7464 26.9857 -94.4500 350.8143 -276.6036 0 0;
     1 0 0 0 0 0 0;
     0 0 0 0 1 0 0];
```

```
34 %% There are two reference inputs - the reference signals T1 and T5.
35 %% Two control inputs (boundary flux) q1 and q5
36 %%
37 p1 = -40+40i;
38 p2 = -40-40i;
39 p3 = -40;
40 p4 = -50+50i;
41 p5 = -50-50i;
42 p6 = -60;
43 p7 = -100;
44 Ka = place(Aa,Ba,[p1,p2,p3,p4,p5,p6,p7]); % Pole placement (using state feedback) for
45 %extended system with tracking error equations for T1 and T5, computes a
46 %state-feedback matrix.
47 Kc=Ka(:,1:5);
48 Ki=Ka(:,6:7); % Control gain for two control inputs - heat flux q1 and q5.
49 % t = 0:0.01:0.5;
50 sys_ex = ss(Aa-Ba*Ka,Br,Ca,Da);
51 % step(sys_ex,t);
52 opt = stepDataOptions('StepAmplitude',25);
53 step(sys_ex,opt);
54
55 %% State observation based on the above Tracking Control
56 %
57 L = place(A',C',[p1*10, p2*10, p3*10, p4*10, p5*10]);
```

Data generation

Technical paper:

- THT follows the Experimental program proposed by Imperial College on the ICP.

Pulse discharge in progress

Temperature set point to be done next

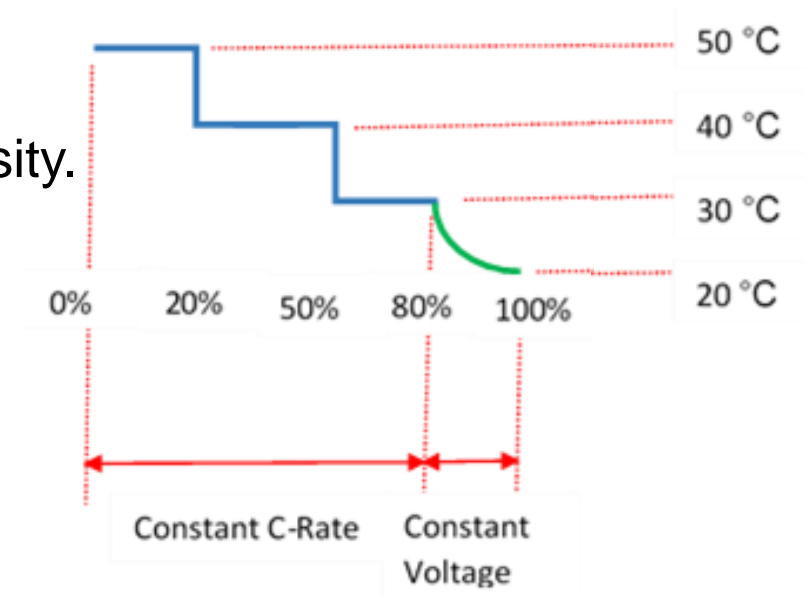
- Experimental program proposed by Cranfield University.

Pulse discharge with back to back cells

Temperature set point with back to back cells

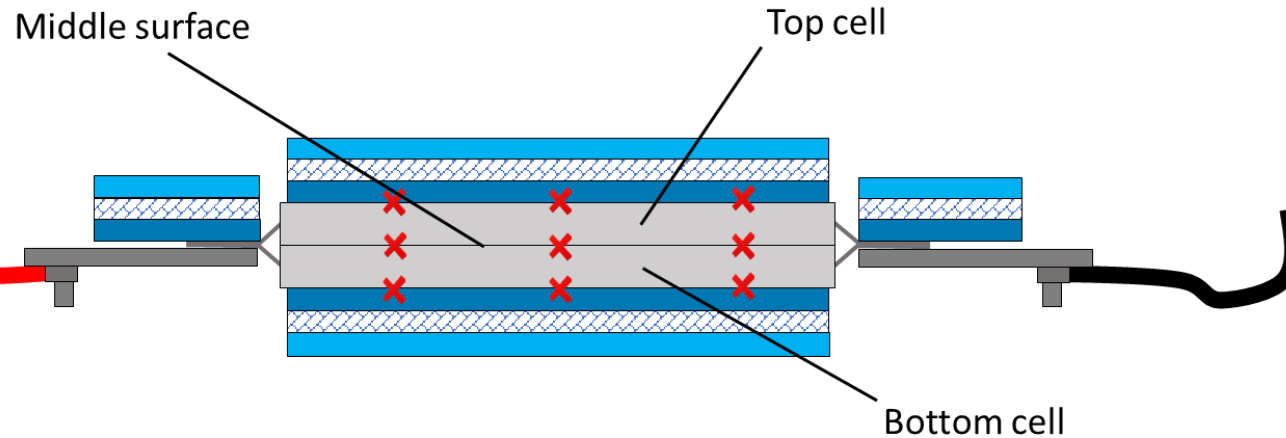
Charge test protocol

Charge test protocol (different C rates)



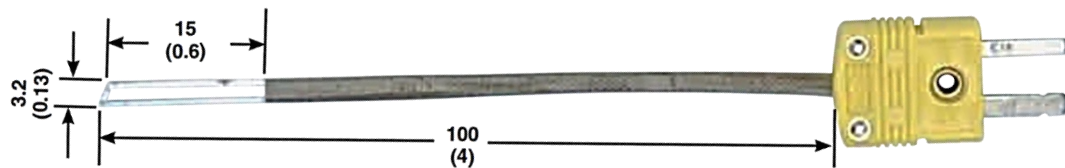
Testing

Cranfield: Model calibration – Experimental setup



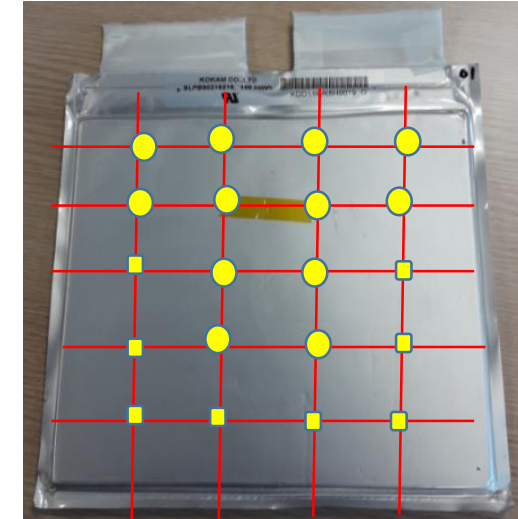
✕ Flat thermocouple position Temperature control module

5 Ah cell

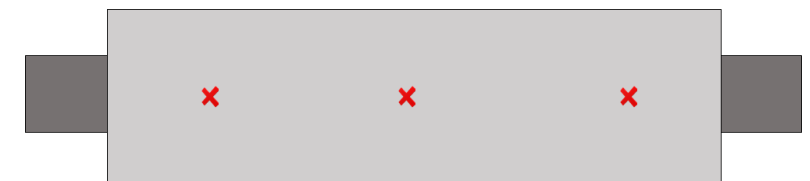


Thickness : 0.05 mm

Ideally :
20 thermocouples per surface



Simplify

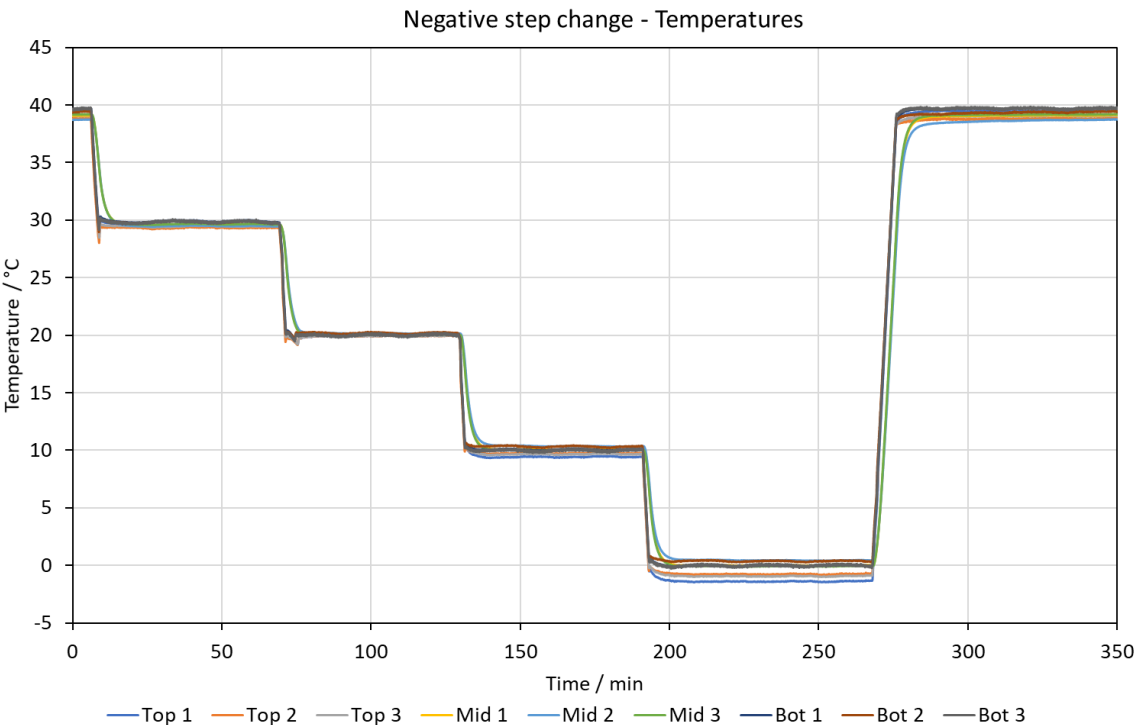
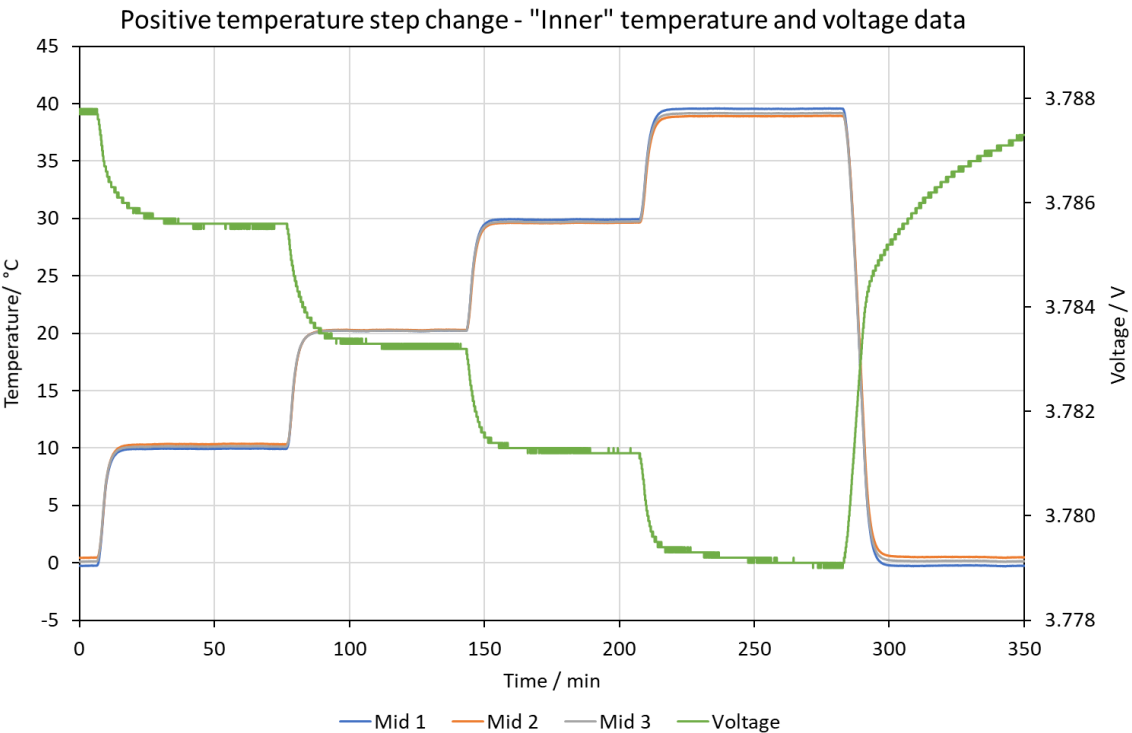


3 thermocouples per surface

Testing

Cranfield: Model calibration – Temperature step change

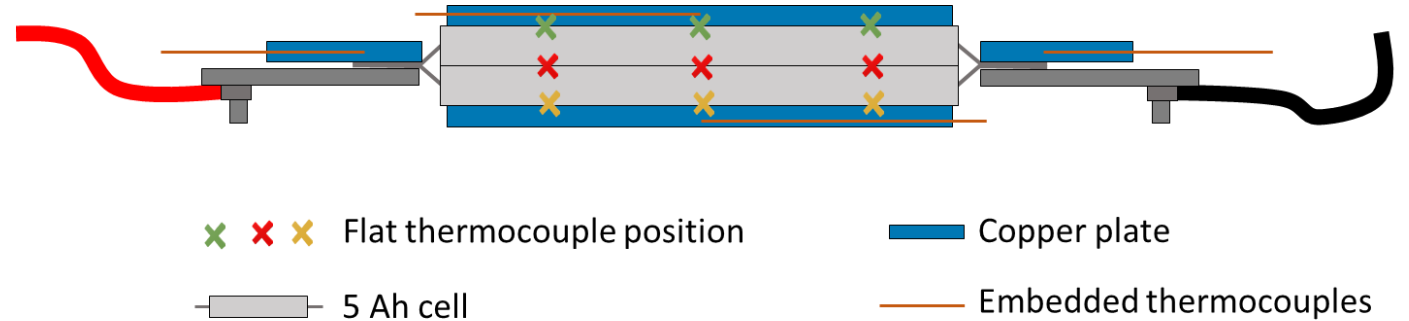
Positive step change		Negative step change	
Start temp. (°C)	End temp. (°C)	Start temp. (°C)	End temp. (°C)
0	10	40	30
10	20	30	20
20	30	20	10
30	40	10	0
40	0	0	40



Testing

Cranfield: Model calibration – Flat thermocouples offset

- Temperature offset between TCs
- Offset dependent of the temperature
- Larger at 0 °C and 40 °C (up to



Pulse discharge 20 °C 100 – 50 %

