06_Robust Performance

1. Sensitivity Functions

Sensitivity Function and Complementary Sensitivity Function

Gang of Four

Why Sensitivity Function

2. Youla Parametrization

Stable P Case

Unstable P Case

3. Modeling Uncertainty

Comparison Between Open-Loop and Closed-Loop Behavior

Forms of Uncertainty

Unmodeled Dynamics Uncertainty

4. Stability in the Presence of Uncertainty

Stability Margins

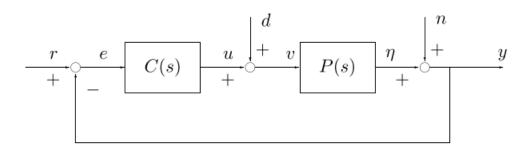
Robust Stability Condition for Additive Uncertainty

Robust Stability Condition for Multiplicative Uncertainty

Youla Parametrization and Robust Stability when ${\cal P}$ is stable

Summary

1. Sensitivity Functions



$$\begin{bmatrix} y \\ \eta \\ v \\ u \\ e \end{bmatrix} = \begin{bmatrix} \frac{PC}{1+PC} & \frac{P}{1+PC} & \frac{1}{1+PC} \\ \frac{PC}{1+PC} & \frac{P}{1+PC} & \frac{-PC}{1+PC} \\ \frac{C}{1+PC} & \frac{1}{1+PC} & \frac{-C}{1+PC} \\ \frac{-PC}{1+PC} & \frac{-PC}{1+PC} & \frac{-C}{1+PC} \\ \frac{1}{1+PC} & \frac{-PC}{1+P} & \frac{-1}{1+PC} \end{bmatrix} \begin{bmatrix} r \\ d \\ n \end{bmatrix}$$

Sensitivity Function and Complementary Sensitivity Function

• Sensitivity Function: $S = \frac{1}{1+PC}$

• Complementary Sensitivity Function: $T = \frac{PC}{1+PC}$

• Property: S+T=1

Gang of Four

• Sensitivity Function: $\frac{1}{1+PC}$

• Load Sensitivity Function: $\frac{P}{1+PC}$

• Complementary Sensitivity Function: $\frac{PC}{1+PC}$

• Noise Sensitivity Function: $\frac{C}{1+PC}$

Why Sensitivity Function

$$e = S(s)(r - P(s)d - n)$$

• minimizing sensitivity ⇒ minimizing tracking error.

 Sensitivity improvements in one frequency range must be paid for with sensitivity deteriorations in another frequency range

2. Youla Parametrization

In control theory the <u>Youla–Kučera parametrization</u> (also simply known as <u>Youla parametrization</u>) is a formula that describes all **possible stabilizing feedback controllers** for a given plant P, as **function of a single parameter** Q.

Stable P Case

Stability Theorem with Gang of Four

Assume P is stable. The closed loop is stable if

$$\frac{1}{1+PC}$$
 , $\frac{P}{1+PC}$, $\frac{C}{1+PC}$ and $\frac{PC}{1+PC}$

are stable.

Controller Design

Now choose $C = \frac{Q}{1 - PQ}$ for some function Q.

Then the closed loop system is **stable if and only if** Q is stable.

Illustration

$$\begin{split} \frac{C}{1+PC} &= Q & \frac{PC}{1+PC} &= PQ \\ \frac{1}{1+PC} &= 1-PQ & \frac{P}{1+PC} &= P(1-PQ) \end{split}$$

"Gang of four" is **stable if and only if** Q is stable.

Unstable P Case

Controller Design

Consider unstable system P and a stabilizing controller C_0 . Let A,B,F_0 and G_0 be stable transfer functions such that

$$P=rac{B}{A} \quad , \quad C_0=rac{G_0}{F_0}$$

and

$$AF_0 + BG_0 = I$$

(This is called a **doubly coprime factorization**)

Now define controller

$$C = \frac{G_0 + QA}{F_0 - QB}$$

The system is then **stable** if Q is stable

Illustration

$$egin{aligned} rac{C}{1+PC} &= A\left(G_0+QA
ight) & rac{PC}{1+PC} &= B\left(G_0+QA
ight) \ rac{1}{1+PC} &= A\left(F_0-QB
ight) & rac{P}{1+PC} &= B\left(F_0-QB
ight) \end{aligned}$$

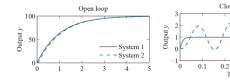
3. Modeling Uncertainty

Comparison Between Open-Loop and Closed-Loop Behavior

- Small difference in open-loop ⇒Small difference in closed-loop
- Large difference in open-loop \Rightarrow Large difference in closed-loop

Similar in open loop but large differences in closed loop

$$P_1(s) = \frac{100}{s+1}$$
 $P_2(s) = \frac{100}{(s+1)(0.025 s + 1)}$



Large differences in open loop but similar in closed loop:

Forms of Uncertainty

There are mainly two forms of model uncertainty

• Parameter Uncertainty

$$P(s) = \frac{1}{s+3}$$
 , $P_{true}(s) = \frac{1}{s+3.1}$

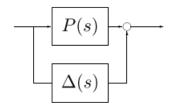
• Unmodeled Dynamics

$$P(s) = \frac{1}{s+3}$$
 , $P_{true}(s) = \frac{1}{(s+3)(0.01s+1)}$

Unmodeled Dynamics Uncertainty

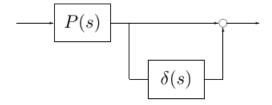
Additive Uncertainty

$$egin{aligned} P_{ ext{true}}\left(s
ight) &= P(s) + \Delta(s) \ \Delta(s) &= P_{ ext{true}}\left(s
ight) - P(s) \end{aligned}$$



Multiplicative Uncertainty

$$egin{aligned} P_{ ext{true}}\left(s
ight) &= P(s)(1+\delta(s)) \ \delta(s) &= rac{P_{ ext{true}}\left(s
ight) - P(s)}{P(s)} \end{aligned}$$



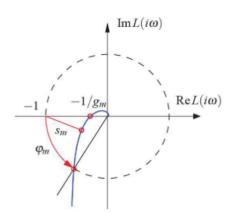
Properties

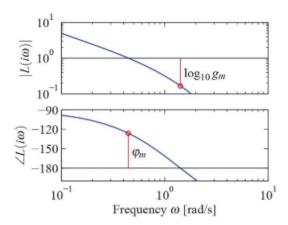
$$\Delta(s) = \delta(s)P(s)$$

4. Stability in the Presence of Uncertainty

Stability Margins

In classical theories, we have <u>Phase Margin</u> and <u>Gain Margin</u>. But for uncertainty modelling, it is not enough. We need to introduce <u>Stability Margin(Vector Stability Margin)</u>





Robust Stability Condition for Additive Uncertainty

Theorem

The system is **robust stable**, if

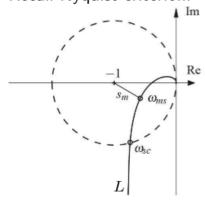
$$egin{aligned} |C(i\omega)\Delta(i\omega)| &< |1+L(i\omega)| \quad, \quad orall \omega \geq 0 \ |\Delta(i\omega)| &< \left|rac{1+L(i\omega)}{C(i\omega)}
ight| \quad, \quad orall \omega \geq 0 \end{aligned}$$

We can write it in the Infinity Norm: $\|H\|_{\infty}=\sup_{\omega}|H(i\omega)|$, then it will become:

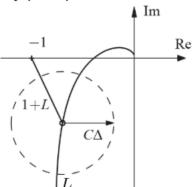
$$|\Delta(i\omega)| < \left|rac{1 + L(i\omega)}{C(i\omega)}
ight| \quad , \quad orall \omega \geq 0 \Rightarrow \|\Delta CS\|_{\infty} < 1$$

Illustration

Recall Nyquist criterion:



Nyquist plot for uncertain system:



$$1+L_{
m true}\,=1+P_{
m true}\,C=1+(P+\Delta)C=1+L+C\Delta$$

- ullet 1+L is the distance between point on the phase trait and the (-1,0) point
- $C\Delta$ is the circle bound of uncertainty

Robust Stability Condition for Multiplicative Uncertainty

Theorem

The system is robust stable, if

$$|\delta(i\omega)| = \left|rac{\Delta(i\omega)}{P(i\omega)}
ight| < \left|rac{1+L(i\omega)}{P(i\omega)C(i\omega)}
ight| = \left|rac{1}{T(i\omega)}
ight| \quad , \quad orall \omega \geq 0$$

We can present it in the Infinity Norm form:

$$|\delta(i\omega)| < \left|rac{1}{T(i\omega)}
ight| \quad , \quad orall \omega \geq 0, orall \omega \geq 0 \Longrightarrow \|\delta T\|_{\infty} < 1$$

Youla Parametrization and Robust Stability when P is stable

Now let $C=rac{Q}{1-PQ}$ and Q is stable.

Then closed loop is stable for $\Delta=0$.

• In the case of **additive uncertainty**, the condition for robust stability is

$$\|\Delta(i\omega)C(i\omega)S(i\omega)\|_{\infty} < 1 \text{ so } \|\Delta Q\|_{\infty} < 1$$

or
$$Q$$
 is stable and $|Q(i\omega)|<\left|rac{1}{\Delta(i\omega)}
ight|\quad,\quadorall\omega\geq0$

• In the case of **multiplicative uncertainty**, the condition for robust stability is

$$\|\delta(i\omega)T(i\omega)\|_{\infty} < 1 \text{ so } \|\delta PQ\|_{\infty} < 1$$

or
$$Q$$
 is stable and $|Q(i\omega)|<\left|rac{1}{P(i\omega)\Delta(i\omega)}
ight|, orall\omega\geq 0$

Summary

- Sensitivity Function:
 - **◦** Smaller Sensitivity **→** Smaller Track Error
 - But we cannot make it small in a frequency, there will be "sacrifice"
- Youla Parametrization
 - \circ Find Q and make it stable
- Modelling Uncertainty
 - o Parameter Uncertainty

- Unmodeled Uncertainty
 - Additive Uncertainty
 - Multiplicative Uncertainty
- Stability in the Presence of Uncertainty
 - Stability Margins: the smallest distance
 - $\circ \ \ Robust \ Stability \ Condition \ for \ Additive \ Uncertainty$
 - Robust Stability Condition for Multiplicative Uncertainty
 - \circ Youla Parametrization and Robust Stability when P is stable

06_Robust Performance 7