Design Details of Building Archetypes with Dual Steel SMF-SCBF systems

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This document demonstrates the details and key design parameters of the building archetypes used in the study. In summary, the buildings design process is dipected in the flow chart of Fig. 1.

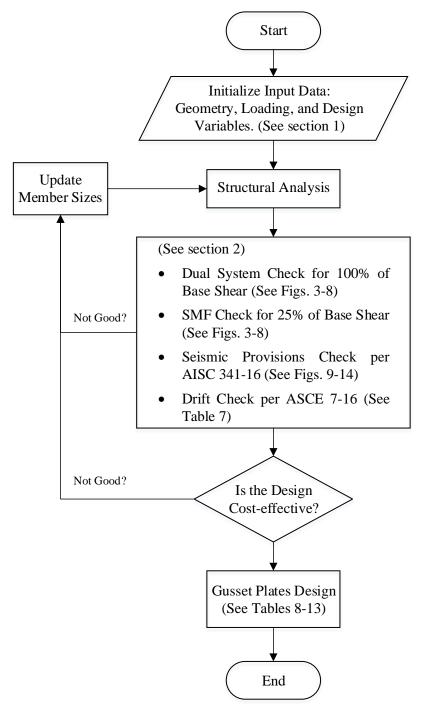


Fig. 1: Flow chart of the design process

General properties of building archetypes

The required general information to design building archetypes are as follows:

• Typical plan and elevation view of building archetypes are shown in Fig. 2. It should be noted that the plan is based on the NIST project [1] in which the bay length of all frames is 20 ft, the height of the first floor is 15 ft, and the other floors are 13 ft. Four braced frames with two-story X bracing configurations are symmetrically considered, and due to the symmetry of the plan and geometric property of using seismic force-resisting system, all building archetypes are modeled as a 2D frame.

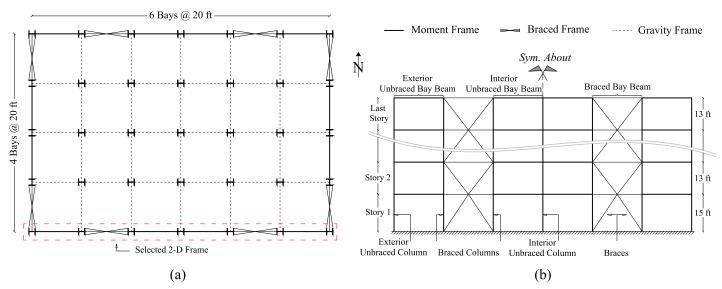


Fig. 2: Typical plan and elevation view of building archetypes; a) plan, b) elevation

- The building archetypes were analyzed and designed in ETABS, ver. 20.0 [2].
- The following codes were used to analyze and design all building archetypes:
 - 1. ASCE 7-16: Minimum Design loads for Buildings and Other Structures [3].
 - 2. AISC 360-16: Specification for Structural Steel Builings [4].
 - 3. AISC 341-16: Seismic Provisions for Structural Steel Buildings [5].
 - 4. AISC 358-16: Prequalified Connections for Special and Intermediate Steel Moment Frames for Seismic Application [6].
- A summary of the design gravity loads are presented in Table 1.

Note: It is assumed in this study that there is no snow load on the building archetypes.

Table 1: Design Gravity Loads

Load	Load Type	Magnitude (psf)	
Dead, D	Dead	90	
Exterior Cladding Wall, D	Dead	25	
Unreduced Design Floor Live, L_o	Floor Live	50	
Unreduced Roof Live, L_o	Roof Live	20	

• Strength and deflection load combinations for strength design and serviceability verifications are provided in Table 2.

Note: It is assumed that the wind load does not control the design.

Table 2: Design Load Combinations

Type of Load Combination	List of Load Combinations*	
	1.4D	
	$1.2D + 1.6L + 0.5L_r$	
Strength	$1.2D + 1.6L_r + 0.5L$	
	$(1.2 + 0.2S_{DS})D + 0.5L \pm 1.0E$	
	$(0.9 - 0.2S_{DS})D \pm 1.0E$	
Deflection	1.0D	
Deficetion	1.0D + 1.0L	

^{*}Load Cases: D: Dead Load, L: Floor Live Load, L: Roof Live Load, E: Earthquake

- Risk category, importance factor, and soil class of the building archetypes were assumed II (office), 1.0, and D respectively.
- Spectral response acceleration parameters are shown in Table 3. It should be noted that the values of S_s and S_I were taken from FEMA P695 [7], and the requirements of ASCE 7-16 § 11.4.8 were not considered for the sake of FEMA P695.

Table 3: Spectral Response Acceleration Parameters

SDC	$S_{s}\left(\mathbf{g}\right)$	$S_1(g)$	F_a	F_v	$S_{MS}(g)$	S_{M1} (g)	$S_{DS}\left(\mathbf{g}\right)$	$S_{D1}\left(\mathbf{g}\right)$	$T_{S}(s)$
D_{max}	1.5	0.599	1.0	1.7	1.5	1.02	1.0	0.68	0.68

• The seismic analysis and design parameters for each building archetype are indicated in Table 4 for the E-W direction.

Table 4: Seismic Analysis and Design Parameters

Building Archetypes	2-Story	4-Story	8-Story	12-Story	16-Story	20-Story
Analysis Procedure	RSA	RSA	RSA	RSA	RSA	RSA
R,Ω_0,C_d	7, 2.5, 5.5	7, 2.5, 5.5	7, 2.5, 5.5	7, 2.5, 5.5	7, 2.5, 5.5	7, 2.5, 5.5
C_uT_a (sec.)	0.341	0.558	0.925	1.248	1.545	1.823
T_1^* (sec.)	0.371	0.614	1.199	1.969	2.672	3.140
C_s	0.143	0.143	0.105	0.078	0.063	0.053
W (kips)	984	1978	3966	5954	7942	9930
V_b ELF (kips)	140.6	282.6	416.5	463.5	499.5	529.0
V_b RSA (kips)	130.4	231.1	243.3	258.3	260.7	278.1
RSA Scaling Factor	1.078	1.223	1.712	1.794	1.916	1.902
V_b Design (kips)	140.6	282.6	416.5	463.5	499.5	529.0
V_b Drift (kips)	130.1	233.4	264.0	273.9	340.3	851.1

^{*}Computed from first-order eigenvalue analysis

- The following material types and corresponding nominal properties were assumed in design:
 - i. Wide-flange sections: A992 Grade 50, $F_y = 50$ ksi, $R_y = 1.1$
 - ii. HSS sections: A500 Grade B, $F_y = 46$ ksi, $R_y = 1.4$
 - iii. Connections: A572 Grade 50, $F_v = 50$ ksi, $R_v = 1.1$
 - iv. E = 29000 ksi, G = 11154 ksi, v = 0.3
- The second order effects were considered through "General 2nd Order" method.
- The "Direct Analysis Method" (DAM) was used to check/design the steel members.
- The P- Δ effects of interior gravity frames were considered through a leaning column with large flexural and axial stiffness, but a pin was introduced at the bottom of the column in each story.
- All nodes in each floor were constrained as a rigid diaphragm.
- The complete quadratic combination (CQC) method was used for combining the value of each parameter of interest for the various modes in modal-response spectrum analysis.

Design outputs and seismic controls

The design outputs and controlled seismic requirements provided by seismic codes are as follows:

- All columns, braces, and beams satisfied the requirements of AISC 341-16 § D1.1 for highly ductile members. Table 5 shows the compactness control of the braces of all building archetypes for the highly ductile requirement of AISC 341-16.
- All brace members had a slenderness ratio less than 200.
- The panel zones were assumed to be elastic and were designed such that their shear strength was higher than the required shear force calculated in AISC 360-16. They also satisfied the seismic requirements per AISC 341-16 § E3.6e.
- Beam to column connections of the SMFs were considered of the type Welded Unreinforced Flange-Welded Web (WUF-W) moment connections, satisfying requirements of AISC 358-16 [6] code.
- The designed cross-sections of all building archetypes are shown in Table 6, and their P-M ratio are depicted in Fig. 3 through Fig. 8.
- All beam-to-column connections of SMFs satisfied the requirements of AISC 341-16 § E3.4 for strong-column/weak-beam criteria.
- The required strength of columns and beams in SCBFs was determined using the capacity-limited seismic load effects. For this purpose, a code in Tcl/Tk language programming was developed according to provisions per AISC 341-16 § F2.3.
- Control of SMFs for strong-column/weak-beam criteria and the P-M ratio of SCBF members for capacity-limited seismic load effects are shown in Fig. 9 through Fig. 14.
- The allowable drift compliance verification of all building archetypes are also illustrated in Table 7.
- Gusset plates are tapered plates, which have been designed using the method presented by Astaneh-Asl et al. [8]. The required strength of gusset plates has been determined using the capacity-limited seismic load effects, and the design process has been done using the developed MATLAB code. Fig. 15 demonstrates the geometric details of gusset plates, and their calculated dimensions using the code mentioned above are shown in Table 8 through Table 13.

Table 5: Controlling the compactness of braces for the highly ductile requirement of AISC 341-16

archetype ID	Story Number	Braces	Diment	ions*		Width to Thickness Ratio	Limit
defictype ID	Story Number	Diaces	W (in)	<i>b</i> (in)	<i>t</i> (in)	b / t	$0.65\sqrt{(E/(R_y.F_y))}$
2-Story	1	HSS 5×5×3/8	5	3.953	0.349	11.33	13.79
2-Story	2	HSS 3.5×3.5×3/8	3.5	2.453	0.349	7.03	13.79
	1	HSS 6×6×1/2	6	4.605	0.465	9.90	
4-Story	2	HSS 5×5×3/8	5	3.953	0.349	11.33	13.79
4 Bioly	3	HSS 5×5×3/8	5	3.953	0.349	11.33	13.77
	4	HSS 4×4×5/16	4	3.127	0.291	10.75	
	1	HSS 6×6×5/8	6	4.257	0.581	7.33	
	2	HSS 6×6×1/2	6	4.605	0.465	9.90	
	3	HSS 6×6×1/2	6	4.605	0.465	9.90	
8-Story	4	HSS 5×5×1/2	5	3.605	0.465	7.75	13.79
,	5	HSS 5×5×1/2	5	3.605	0.465	7.75	
	6	HSS 4.5×4.5×1/2	4.5	3.105	0.465	6.68	
	7	HSS 4.5×4.5×1/2	4.5	3.105	0.465	6.68	
	8	HSS 4×4×3/8	4	2.953	0.349	8.46	
	1	HSS 6×6×5/8	6	4.257	0.581	7.33 9.90	
	2 3	HSS 6×6×1/2 HSS 6×6×1/2	6 6	4.605 4.605	0.465 0.465	9.90 9.90	
	4	HSS 5.5×5.5×3/8	5.5	4.453	0.403	12.76	
	5	HSS 5.5×5.5×3/8	5.5	4.453	0.349	12.76	
	6	HSS 5.5×5.5×3/8	5.5 5.5	4.453	0.349	12.76	
12-Story	7	HSS 5.5×5.5×3/8	5.5	4.453	0.349	12.76	13.79
	8	HSS 5×5×3/8	5.5	3.953	0.349	11.33	
	9	HSS 5×5×3/8	5	3.953	0.349	11.33	
	10	HSS 5×5×3/8	5	3.953	0.349	11.33	
	11	HSS 4.5×4.5×3/8	4.5	3.453	0.349	9.89	
	12	HSS 4×4×5/16	4	3.127	0.291	10.75	
	1	HSS 6×6×5/8	6	4.257	0.581	7.33	
	2	HSS 6×6×1/2	6	4.605	0.465	9.90	
	3	HSS 6×6×1/2	6	4.605	0.465	9.90	
	4	HSS 6×6×1/2	6	4.605	0.465	9.90	
	5	HSS 6×6×1/2	6	4.605	0.465	9.90	
	6	HSS 5.5×5.5×3/8	5.5	4.453	0.349	12.76	
	7	HSS 5.5×5.5×3/8	5.5	4.453	0.349	12.76	
16 Ctomy	8	HSS 5.5×5.5×3/8	5.5	4.453	0.349	12.76	12.70
16-Story	9	HSS 5.5×5.5×3/8	5.5	4.453	0.349	12.76	13.79
	10	HSS 5×5×3/8	5	3.953	0.349	11.33	
	11	HSS 5×5×3/8	5	3.953	0.349	11.33	
	12	HSS 5×5×3/8	5	3.953	0.349	11.33	
	13	HSS 5×5×3/8	5	3.953	0.349	11.33	
	14	HSS 4.5×4.5×5/16	4.5	3.627	0.291	12.46	
	15	HSS 4.5×4.5×5/16	4.5	3.627	0.291	12.46	
	16	HSS 3.5×3.5×5/16	3.5	2.627	0.291	9.03	
	1	HSS 7×7×1/2	7	5.605	0.465	12.05	
	2	HSS $7\times7\times1/2$	7	5.605	0.465	12.05	
	3	HSS 7×7×1/2	7	5.605	0.465	12.05	
	4	HSS 6×6×1/2	6	4.605	0.465	9.90	
	5	HSS 6×6×1/2	6	4.605	0.465	9.90	
	6	HSS 6×6×1/2	6	4.605	0.465	9.90	
	7	HSS 6×6×1/2	6	4.605	0.465	9.90	
	8	HSS 6×6×1/2	6	4.605	0.465	9.90	
	9	HSS 6×6×1/2	6	4.605	0.465	9.90	
20-Story	10	HSS 5×5×1/2	5	3.605	0.465	7.75	13.79
	11	HSS 5×5×1/2	5 5 5	3.605	0.465	7.75	
	12	HSS 5.5×5.5×3/8	5.5	4.453	0.349	12.76	
	13	HSS 5.5×5.5×3/8	5.5	4.453	0.349	12.76	
	14	HSS 5×5×3/8	5	3.953	0.349	11.33	
	15	HSS 5×5×3/8	5	3.953	0.349	11.33	
	16 17	HSS 5×5×3/8	5	3.953	0.349	11.33	
	17	HSS 5×5×3/8	5 4.5	3.953	0.349	11.33	
	18 19	HSS 4.5×4.5×5/16 HSS 4.5×4.5×5/16	4.5 4.5	3.627 3.627	0.291 0.291	12.46 12.46	
		17.3.3 4 3X4 3X3/1D	4.1	1 D / /	U /91	1/40	

 $^{^*}W$: nominal width; t: design wall thickness; b: nominal width minus 3 times the design wall thickness

 Table 6: Designed cross-sections of building archetypes

Archetype ID	Story Number	Braced Column	Unbraced Colu		 Braced Beam 	Unbraced Bea		Braces
Jr			Interior	Exterior		Interior	Exterior	
2-Story	1	W8×58	W8×67	W8×58	W16×57	W10×26	W12×22	HSS 5×5×3/8
	2	W8×58	W8×67	W8×58	W10×45	W12×19	W12×19	HSS 3.5×3.5×3/8
	1	W12×96	W10×100 W10×100	W10×77 W10×77	W16×89	W16×31	W16×31	HSS 6×6×1/2 HSS 5×5×3/8
4-Story	2 3	W12×96 W10×68	W10×100 W10×77	W10×// W10×68	W12×50 W14×53	W16×31 W14×26	W16×31 W14×26	HSS 5×5×3/8
	4	W10×68	W10×77	W10×68	W14×33 W10×45	W14×20 W12×22	W14×20 W12×19	HSS 4×4×5/16
	1	W14×211	W10×77 W12×120	W10×88	W16×89	W12×22 W18×40	W18×40	HSS 6×6×5/8
	2	W14×211 W14×211	W12×120 W12×120	W10×88	W16×89	W18×46	W18×46	HSS 6×6×1/2
	3	W12×136	W12×106	W10×77	W12×50	W18×46	W18×40	HSS 6×6×1/2
	4	W12×136	W12×106	W10×77	W16×89	W18×40	W18×35	HSS 5×5×1/2
8-Story	5	W10×88	W10×100	W10×77	W10×45	W18×35	W18×35	HSS 5×5×1/2
	6	W10×88	W10×100	W10×77	W16×89	W16×31	W16×31	HSS 4.5×4.5×1/2
	7	W8×67	W10×77	W8×67	W16×57	W14×26	W14×26	HSS 4.5×4.5×1/2
	8	W8×67	W10×77	W8×67	W10×45	W12×19	W8×21	HSS 4×4×3/8
	1	W14×311	W12×152	W12×96	W16×89	W18×40	W18×40	HSS 6×6×5/8
	2	W14×311	W12×152	W12×96	W16×89	W18×50	W18×46	HSS 6×6×1/2
	3	W14×211	W12×152	W10×100	W16×89	W18×60	W18×50	HSS 6×6×1/2
	4	W14×211	W12×152	W10×100	W16×89	W18×60	W18×46	HSS 5.5×5.5×3/8
	5	W12×170	W12×136	W10×88	W10×30	W18×55	W18×46	HSS 5.5×5.5×3/8
12-Story	6	W12×170	W12×136	W10×88	W16×89	W18×50	W18×40	HSS 5.5×5.5×3/8
12-Story	7	W12×120	W12×106	W10×77	W10×45	W18×46	W18×40	HSS 5.5×5.5×3/8
	8	W12×120	W12×106	W10×77	W12×50	W18×40	W18×35	HSS 5×5×3/8
	9	W10×77	W10×100	W10×77	W10×30	W18×35	W16×31	HSS 5×5×3/8
	10	W10×77	W10×100	W10×77	W10×45	W16×31	W14×26	HSS 5×5×3/8
	11	W8×67	W10×77	W8×67	W12×50	W14×26	W14×26	HSS 4.5×4.5×3/8
	12	W8×67	W10×77	W8×67	W10×45	W12×19	W12×19	HSS 4×4×5/16
	1	W14×426	W12×170	W12×120	W16×89	W18×40	W18×40	HSS 6×6×5/8
	2	W14×426	W12×170	W12×120	W16×89	W18×60	W18×60	HSS 6×6×1/2
	3	W14×342	W12×170	W12×106	W10×30	W18×65	W18×65	HSS 6×6×1/2
	4	W14×342	W12×170	W12×106	W16×89	W18×65	W18×65	HSS 6×6×1/2
	5	W14×257	W12×170	W12×96	W16×89	W18×65	W18×55	HSS 6×6×1/2
	6	W14×257	W12×170	W12×96	W16×89	W18×65	W18×55	HSS 5.5×5.5×3/8
	7	W14×193	W12×170	W10×100	W10×30	W18×65	W18×50	HSS 5.5×5.5×3/8
16-Story	8	W14×193	W12×170	W10×100	W16×89	W18×65	W18×50	HSS 5.5×5.5×3/8
•	9	W12×152	W12×170	W10×88	W10×45	W18×65	W18×46	HSS 5.5×5.5×3/8
	10	W12×152	W12×170	W10×88	W12×50	W18×55	W18×40	HSS 5×5×3/8
	11	W12×106	W12×120	W10×77	W10×30	W18×46	W18×40	HSS 5×5×3/8
	12	W12×106	W12×120	W10×77	W12×50	W18×40	W18×35	HSS 5×5×3/8
	13	W10×77	W10×100	W10×77	W12×50	W18×35	W16×31	HSS 5×5×3/8
	14	W10×77	W10×100 W10×77	W10×77	W10×45	W16×31	W14×26	HSS 4.5×4.5×5/1
	15	W10×77 W10×77		W8×67	W12×50	W14×26	W12×22	HSS 4.5×4.5×5/1
	16	W10×77 W14×605	W10×77 W14×233	W8×67 W12×190	W10×45 W12×50	W12×19 W18×50	W12×19 W18×40	HSS 3.5×3.5×5/1 HSS 7×7×1/2
	2	W14×605 W14×605	W14×233 W14×233	W12×190 W12×190	W16×89	W18×71	W18×60	HSS 7×7×1/2
	3	W14×445	W14×233 W14×193	W12×190 W12×170	W10×89 W12×50	W21×68	W18×65	HSS 7×7×1/2
	3 4	W14×445 W14×445	W14×193 W14×193	W12×170 W12×170	W16×89	W21×68	W18×65	HSS 6×6×1/2
	-1 -5	W14×398	W14×176	W12×170 W12×152	W10×30	W21×68	W18×65	HSS 6×6×1/2
	6	W14×398	W14×176 W14×176	W12×152 W12×152	W16×89	W21×68	W18×65	HSS 6×6×1/2
	7	W14×311	W14×170 W12×190	W12×132 W12×106	W10×30	W21×68	W18×60	HSS 6×6×1/2
	8	W14×311	W12×190	W12×106	W16×89	W21×68	W18×60	HSS 6×6×1/2
	9	W14×257	W12×190	W12×100	W12×50	W18×71	W18×60	HSS 6×6×1/2
	10	W14×257	W12×190	W12×96	W16×89	W18×71	W18×55	HSS 5×5×1/2
20-Story	11	W12×210	W12×170	W10×88	W14×53	W18×71	W18×55	HSS 5×5×1/2
	12	W12×210	W12×170	W10×88	W16×89	W18×65	W18×46	HSS 5.5×5.5×3/8
	13	W12×152	W12×170	W10×88	W10×45	W18×60	W18×46	HSS 5.5×5.5×3/8
	14	W12×152	W12×152	W10×88	W12×50	W18×55	W18×40	HSS 5×5×3/8
	15	W12×106	W12×136	W10×77	W10×30	W18×55	W18×35	HSS 5×5×3/8
	16	W12×106	W12×136	W10×77	W12×50	W18×40	W18×35	HSS 5×5×3/8
	17	W10×77	W12×150 W12×96	W10×77	W12×50	W18×35	W18×35	HSS 5×5×3/8
	18	W10×77	W12×96	W10×77	W10×45	W18×35	W16×31	HSS 4.5×4.5×5/1
	19	W8×67	W10×77	W8×67	W12×50	W16×31	W14×26	HSS 4.5×4.5×5/1
	20	W8×67					W10×26	

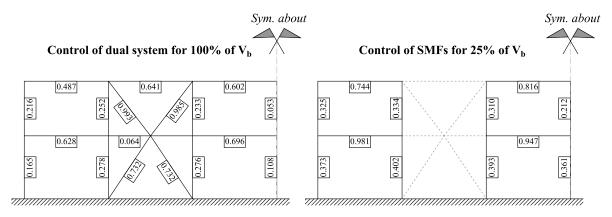


Fig. 3: The P-M ratio of designed cross-sections of 2-Story building archetype

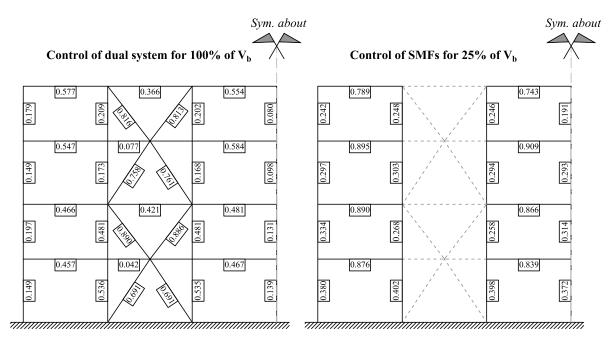


Fig. 4: The P-M ratio of designed cross-sections of 4-Story building archetype

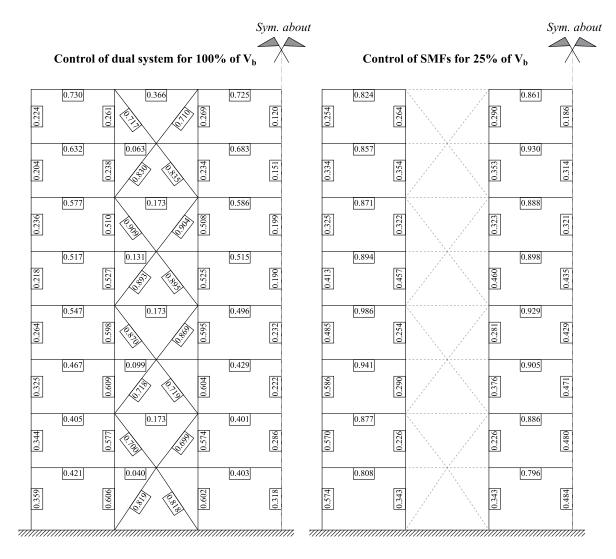


Fig. 5: The P-M ratio of designed cross-sections of 8-Story building archetype

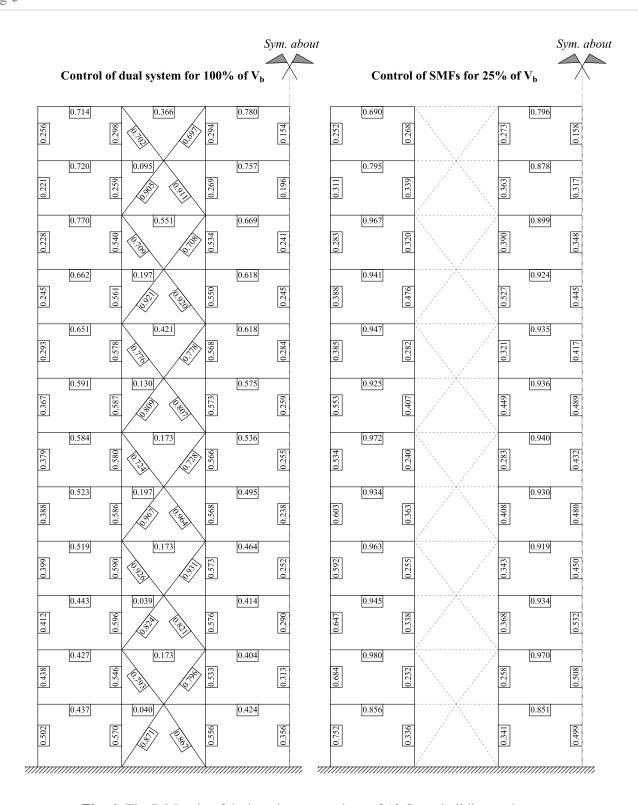


Fig. 6: The P-M ratio of designed cross-sections of 12-Story building archetype

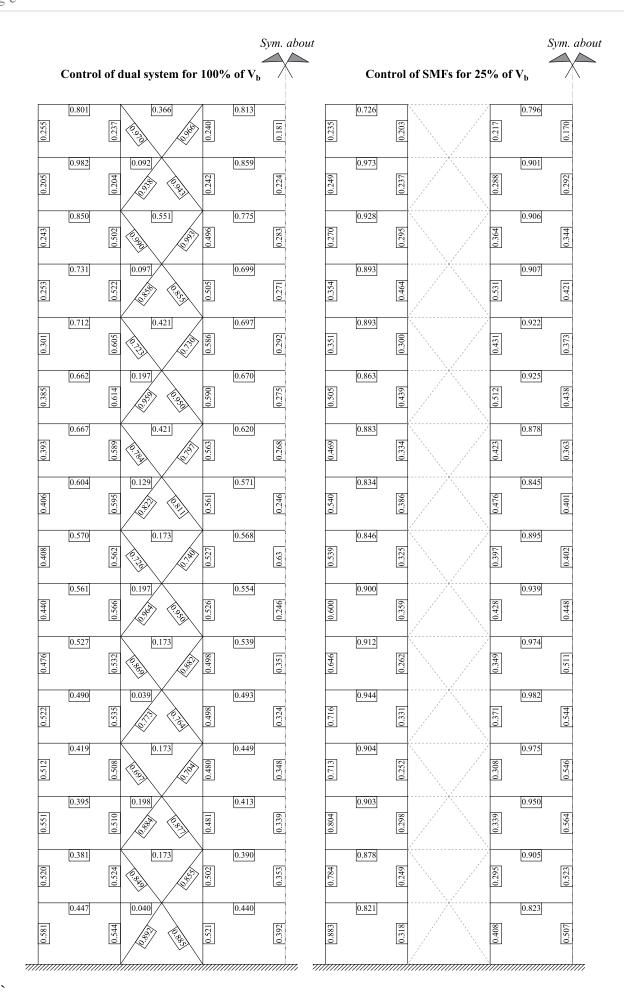


Fig. 7: The P-M ratio of designed cross-sections of 16-Story building archetype

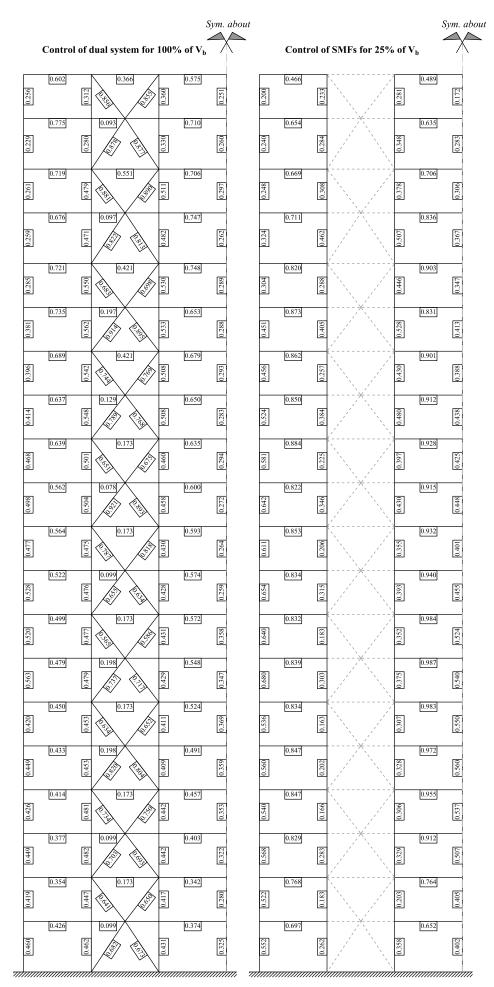


Fig. 8: The P-M ratio of designed cross-sections of 20-Story building archetype

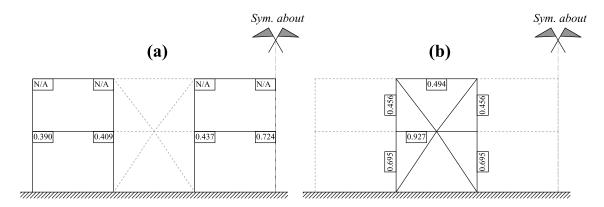


Fig. 9: Seismic provisions check per AISC 341-16 for 2-Story building archetype; a) strong-column/weak-beam criteria, b) capacity-limited seismic load effects

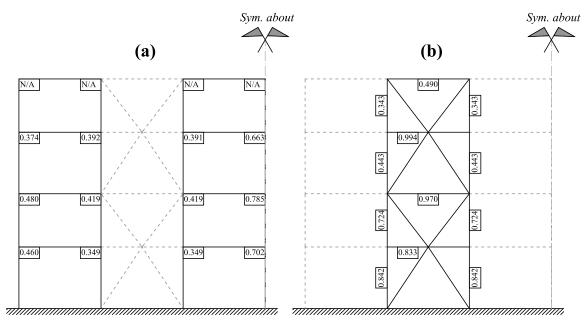


Fig. 10: Seismic provisions check per AISC 341-16 for 4-Story building archetype; a) strong-column/weak-beam criteria, b) capacity-limited seismic load effects

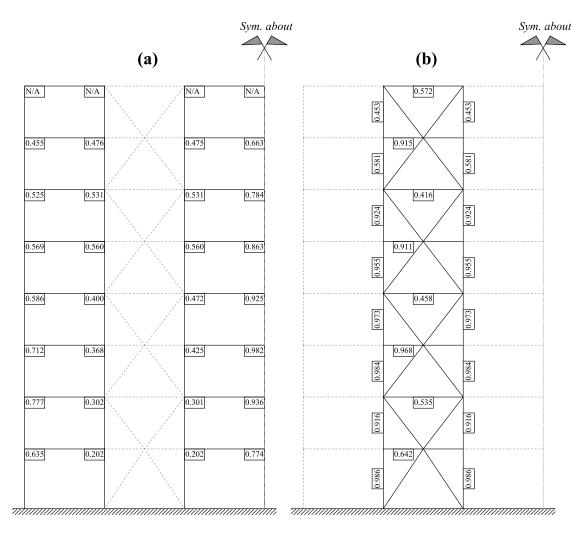


Fig. 11: Seismic provisions check per AISC 341-16 for 8-Story building archetype; a) strong-column/weak-beam criteria, b) capacity-limited seismic load effects

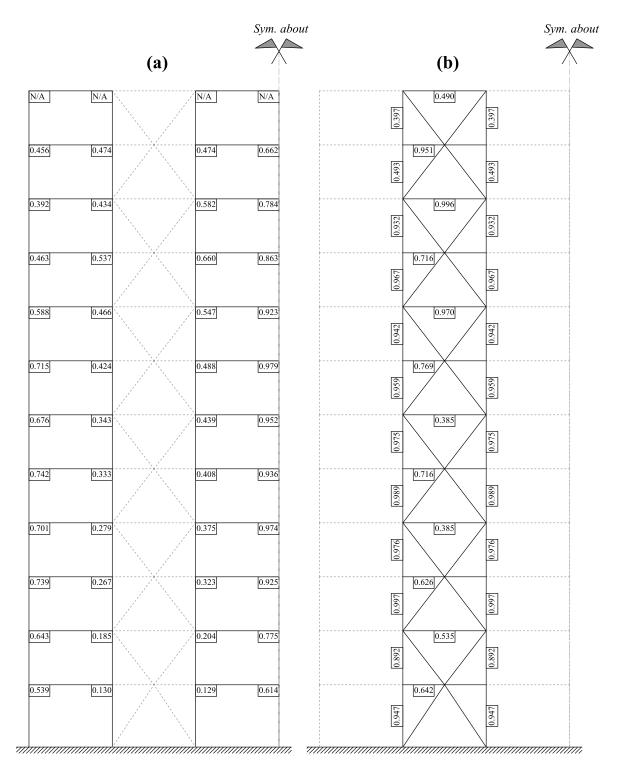


Fig. 12: Seismic provisions check per AISC 341-16 for 12-Story building archetype; a) strong-column/weak-beam criteria, b) capacity-limited seismic load effects

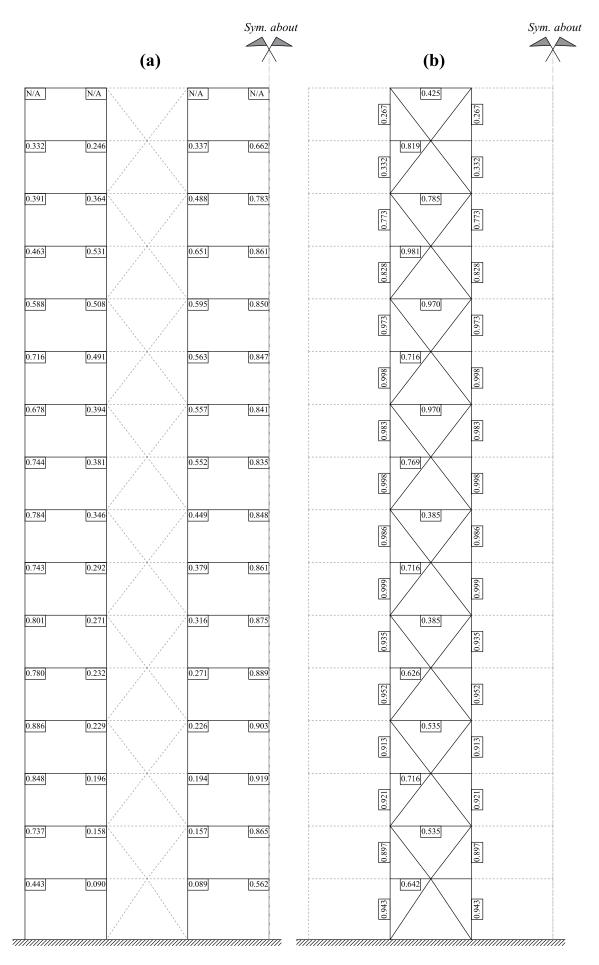


Fig. 13: Seismic provisions check per AISC 341-16 for 16-Story building archetype; a) strong-column/weak-beam criteria, b) capacity-limited seismic load effects

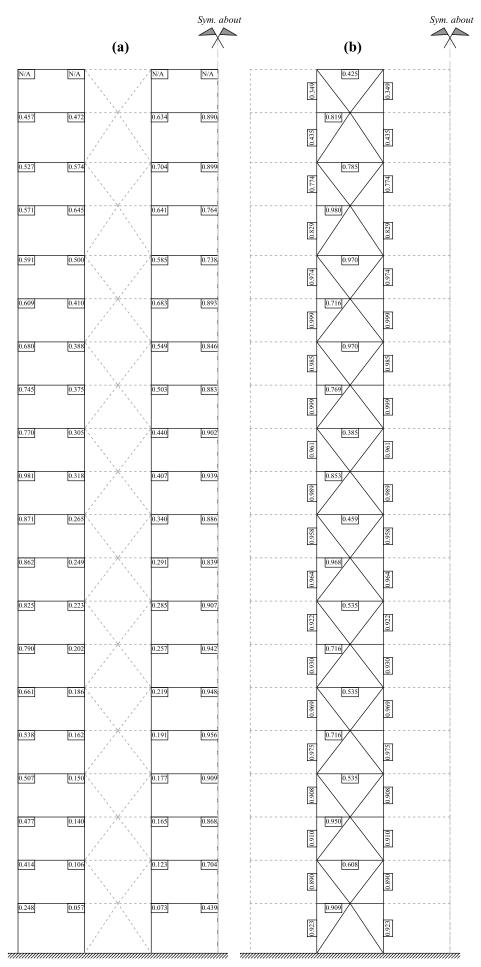


Fig. 14: Seismic provisions check per AISC 341-16 for 20-Story building archetype; a) strong-column/weak-beam criteria, b) capacity-limited seismic load effects

Table 7: Verification of design story drifts for building archetypes

T	able 7: Verificat	ion of design	story drifts for build	ling archety	pes
Archetype ID	Story Number	δ_{xe} (in)	$\delta_x = \delta_{xe} . C_d / I_e$ (in)	Δ_i	Δ_i/h_{sx} < 2%
2-Story	1	0.12	0.67	0.67	0.37
	2	0.23	1.27	0.61	0.39
	1	0.14	0.75	0.75	0.42
4-Story	2	0.35	1.90	1.15	0.74
Ž	3	0.53	2.91	1.01	0.65
	4	0.71	3.90	0.99	0.63
	1	0.12	0.67	0.67	0.37
	2	0.29	1.62	0.95	0.61
	3	0.47	2.56	0.94	0.60
8-Story	4	0.69	3.82	1.26	0.80
	5	0.92	5.05	1.23	0.79
	6	1.17	6.43	1.38	0.89
	7 8	1.41	7.74	1.31 1.27	0.84 0.82
	<u>8</u>	1.64 0.12	9.01 0.66	0.66	0.82
	2	0.12	1.57	0.66	0.58
	3	0.28	2.47	0.91	0.58
	4	0.43	3.71	1.24	0.79
	5	0.07	4.95	1.24	0.80
	6	1.15	6.30	1.35	0.86
12-Story	7	1.13	7.65	1.35	0.86
	8	1.66	9.12	1.48	0.95
	9	1.93	10.62	1.50	0.96
	10	2.22	12.19	1.56	1.00
	11	2.50	13.75	1.56	1.00
	12	2.77	15.24	1.49	0.96
	1	0.14	0.78	0.78	0.43
	2	0.34	1.85	1.07	0.68
	3	0.53	2.91	1.06	0.68
	4	0.75	4.11	1.20	0.77
	5	0.97	5.34	1.23	0.79
	6	1.25	6.86	1.52	0.97
	7	1.53	8.40	1.54	0.99
	8	1.82	10.03	1.63	1.04
16-Story	9	2.12	11.66	1.64	1.05
	10	2.44	13.43	1.77	1.13
	11	2.77	15.25	1.82	1.16
	12	3.12	17.16	1.90	1.22
	13	3.47	19.11	1.95	1.25
	14	3.85	21.19	2.08	1.34
	15	4.23	23.25	2.06	1.32
	16	4.58	25.22	1.97	1.26
	1	0.16	0.86	0.86	0.48
	2	0.36	1.97	1.11	0.71
	3	0.56	3.10	1.13	0.72
	4	0.81	4.48	1.38	0.88
	5	1.07	5.90	1.42	0.91
	6	1.35	7.43	1.54	0.98
	7	1.63	8.99	1.56	1.00
	8	1.94	10.67	1.68	1.07
	9	2.25	12.37	1.71	1.09
20. %	10	2.59	14.27	1.90	1.22
20-Story	11	2.95	16.21	1.94	1.25
	12	3.33	18.29	2.08	1.33
	13	3.71	20.41	2.12	1.36
	14	4.12	22.64	2.23	1.43
	15	4.53	24.91	2.27	1.46
	16	4.95	27.24	2.33	1.49
	17	5.39	29.62	2.38	1.52
	18	5.83	32.04	2.42	1.55
	19	6.27	34.47	2.42	1.55
				2.29	1.47

 δ_{xe} : elastic absolute displacement; δ_x : inelastic absolute displacement; Δ_i : inelastic drift; Δ_i/h_{sx} : inelastic drift ratio

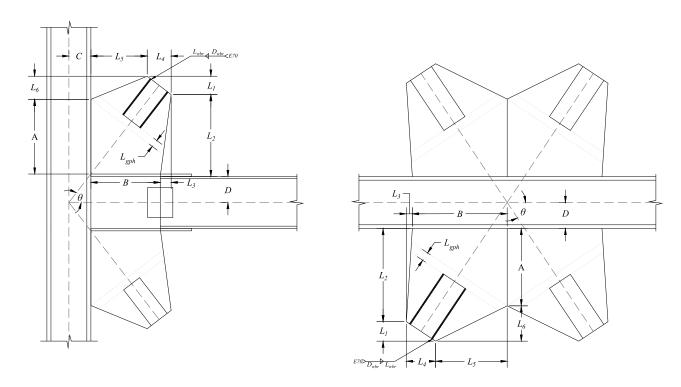


Fig. 15: Geometric parameters of gusset plates

Table 8: Gusset plates details of 2-Story building archetype

Level		Dimen	tions A , A	B, and L	$_{1}$ to L_{6} fo	r gusset j	plates (a	ll dimens	ions are	in inche	s)	Weld properties	
Level		L_1	L_2	L_3	L_4	L_5	L_6	A	В	t_g	L_{gph}	L_{wbr}	D_{wbr}
3	Lower	3.35	19.14	2.54	4.36	13.34	5.51	16.98	15.16	0.5	1.5	10	0.31
2	Upper	3.35	14.31	1.9	4.36	16.44	6.78	10.88	18.89	0.5	1.5	10	0.31
2	Lower	3.88	17.5	1.13	5.82	15.53	7.68	13.71	20.22	0.75	2	12	0.38
1	Upper	3.88	32.28	2.08	5.82	15.53	7.68	28.48	19.27	0.75	2	12	0.38

tg: gusset plate thickness

 Table 9: Gusset plates details of 4-Story building archetype

Laval		Dimen	tions A ,	B, and L	l_1 to L_6 fo	r gusset j	olates (a	ll dimens	ions are	in inche	s)	Weld properties	
Level		L_1	L_2	L_3	L_4	L_5	L_6	A	В	t_g	L_{gph}	L_{wbr}	D_{wbr}
5	Lower	3.66	17.54	2.33	4.76	11.21	4.63	16.57	13.63	0.5	1.5	8	0.38
4	Upper	3.66	12.02	1.60	4.76	13.63	5.63	10.05	16.79	0.5	1.5	8	0.38
4	Lower	4.27	17.17	2.28	5.55	17.43	7.19	14.24	20.70	0.75	2	12	0.38
3	Upper	4.27	24.45	3.25	5.55	16.01	6.61	22.11	18.31	0.75	2	12	0.38
3	Lower	4.27	24.45	3.25	5.55	16.01	6.61	22.11	18.31	0.75	2	12	0.38
2	Upper	4.27	17.17	2.28	5.55	18.52	7.64	13.79	21.78	0.75	2	12	0.38
2	Lower	4.44	19.24	1.24	6.66	16.56	8.19	15.49	21.98	0.75	2	13	0.56
1	Upper	4.44	37.15	2.40	6.66	16.56	8.19	33.40	20.82	0.75	2	13	0.56

Table 10: Gusset plates details of 8-Story building archetype

Level		Dimen	tions A ,	B, and L	to L_6 fo	r gusset j	olates (a	ll dimens	ions are	in inche	s)	Weld	properties
Level		L_{I}	L_2	L_3	L_4	L_5	L_6	A	В	t_g	L_{gph}	L_{wbr}	D_{wbr}
9	Lower	3.66	19.41	2.58	4.76	13.34	5.51	17.56	15.52	0.5	1.5	10	0.38
8	Upper	3.66	14.31	1.9	4.76	16.35	6.75	11.21	19.21	0.5	1.5	10	0.38
8	Lower	3.96	17.17	2.28	5.15	18.47	7.63	13.51	21.35	0.75	2	12	0.44
7	Upper	3.96	20.85	2.77	5.15	16.01	6.61	18.21	18.39	0.75	2	12	0.44
7	Lower	3.96	20.85	2.77	5.15	16.01	6.61	18.21	18.39	0.75	2	12	0.44
6	Upper	3.96	17.17	2.28	5.15	16.04	6.62	14.51	18.91	0.75	2	12	0.44
6	Lower	4.27	17.24	2.29	5.55	16.01	6.61	14.89	19.27	0.75	2	12	0.5
5	Upper	4.27	22.63	3.01	5.55	16.01	6.61	20.29	18.55	0.75	2	12	0.5
5	Lower	4.27	22.63	3.01	5.55	16.01	6.61	20.29	18.55	0.75	2	12	0.5
4	Upper	4.27	17.17	2.28	5.55	16.76	6.92	14.52	20.03	0.75	2	12	0.5
4	Lower	4.88	18.31	2.43	6.34	17.48	7.22	15.98	21.39	0.75	2	13	0.56
3	Upper	4.88	25.73	3.42	6.34	17.08	7.05	23.55	20	0.75	2	13	0.56
3	Lower	4.88	25.73	3.42	6.34	17.08	7.05	23.55	20	0.75	2	13	0.56
2	Upper	4.88	18.31	2.43	6.34	19.24	7.94	15.25	23.14	0.75	2	13	0.56
2	Lower	4.44	21.57	1.39	6.66	18.11	8.96	17.05	23.38	1	2.5	14	0.63
1	Upper	4.44	41.73	2.69	6.66	18.11	8.96	37.22	22.08	1	2.5	14	0.63

tg: gusset plate thickness

Table 11: Gusset plates details of 12-Story building archetype

Level		Dimen	tions A ,	B, and L	to L_6 fo	r gusset j	olates (a	ll dimens	ions are	in inche	s)	Weld properties	
Level		L_1	L_2	L_3	L_4	L_5	L_6	A	В	t_g	L_{gph}	L_{wbr}	D_{wbr}
13	Lower	3.66	19.41	2.58	4.76	13.34	5.51	17.56	15.52	0.5	1.5	10	0.31
12	Upper	3.66	14.31	1.9	4.76	14.72	6.08	11.89	17.58	0.5	1.5	10	0.31
12	Lower	3.96	15.45	2.05	5.15	15.52	6.41	13.01	18.62	0.5	1.5	11	0.38
11	Upper	3.96	21.94	2.92	5.15	14.41	5.95	19.95	16.65	0.5	1.5	11	0.38
11	Lower	4.27	24.13	3.21	5.55	16.01	6.61	21.78	18.35	0.75	2	12	0.38
10	Upper	4.27	17.17	2.28	5.55	16.1	6.65	14.79	19.37	0.75	2	12	0.38
10	Lower	4.27	17.17	2.28	5.55	16.1	6.65	14.79	19.37	0.75	2	12	0.38
9	Upper	4.27	24.72	3.28	5.55	16.01	6.61	22.38	18.27	0.75	2	12	0.38
9	Lower	4.27	24.72	3.28	5.55	16.01	6.61	22.38	18.27	0.75	2	12	0.38
8	Upper	4.27	17.24	2.29	5.55	16.01	6.61	14.89	19.27	0.75	2	12	0.38
8	Lower	4.57	19.42	2.58	5.94	17.61	7.27	16.72	20.98	0.5	1.5	14	0.38
7	Upper	4.57	25.22	3.35	5.94	17.61	7.27	22.52	20.21	0.5	1.5	14	0.38
7	Lower	4.57	25.22	3.35	5.94	17.61	7.27	22.52	20.21	0.5	1.5	14	0.38
6	Upper	4.57	19.24	2.56	5.94	17.61	7.27	16.54	21	0.5	1.5	14	0.38
6	Lower	4.57	19.24	2.56	5.94	17.61	7.27	16.54	21	0.5	1.5	14	0.38
5	Upper	4.57	26.31	3.5	5.94	17.61	7.27	23.62	20.06	0.5	1.5	14	0.38
5	Lower	4.57	26.31	3.5	5.94	17.61	7.27	23.62	20.06	0.5	1.5	14	0.38
4	Upper	4.57	18.89	2.51	5.94	19.76	8.16	15.3	23.19	0.5	1.5	14	0.38
4	Lower	4.88	20.6	2.74	6.34	21	8.67	16.81	24.6	0.75	2	15	0.5
3	Upper	4.88	29.41	3.91	6.34	19.21	7.93	26.36	21.65	0.75	2	15	0.5
3	Lower	4.88	29.41	3.91	6.34	19.21	7.93	26.36	21.65	0.75	2	15	0.5
2	Upper	4.88	20.6	2.74	6.34	21	8.67	16.81	24.6	0.75	2	15	0.5
2	Lower	4.44	23.9	1.54	6.66	19.67	9.72	18.61	24.78	0.75	2	16	0.56
1	Upper	4.44	45.11	2.91	6.66	19.67	9.72	39.83	23.41	0.75	2	16	0.56

tg: gusset plate thickness

Table 12: Gusset plates details of 16-Story building archetype

T1		Dimen						ll dimens				Weld	properties
Level		L_1	L_2	L_3	L_4	L_5	L_6	A	В	t_g	L_{gph}	L_{wbr}	D_{wbr}
17	Lower	3.35	18.95	2.52	4.36	12.27	5.07	17.24	14.12	0.5	1.5	9	0.31
16	Upper	3.35	13.16	1.75	4.36	13.92	5.75	10.77	16.53	0.5	1.5	9	0.31
16	Lower	3.96	14.31	1.9	5.15	14.64	6.04	12.23	17.89	0.5	1.5	10	0.38
15	Upper	3.96	20.55	2.73	5.15	13.34	5.51	19.01	15.76	0.5	1.5	10	0.38
15	Lower	3.96	20.55	2.73	5.15	13.34	5.51	19.01	15.76	0.5	1.5	10	0.38
14	Upper	3.96	14.31	1.9	5.15	14.64	6.04	12.23	17.89	0.5	1.5	10	0.38
14	Lower	4.27	17.17	2.28	5.55	16.76	6.92	14.52	20.03	0.75	2	12	0.38
13	Upper	4.27	24.57	3.26	5.55	16.01	6.61	22.23	18.29	0.75	2	12	0.38
13	Lower	4.27	24.57	3.26	5.55	16.01	6.61	22.23	18.29	0.75	2	12	0.38
12	Upper	4.27	17.17	2.28	5.55	16.1	6.65	14.79	19.37	0.75	2	12	0.38
12	Lower	4.27	17.17	2.28	5.55	16.1	6.65	14.79	19.37	0.75	2	12	0.38
11	Upper	4.27	25.1	3.34	5.55	16.01	6.61	22.76	18.22	0.75	2	12	0.38
11	Lower	4.27	25.1	3.34	5.55	16.01	6.61	22.76	18.22	0.75	2	12	0.38
10	Upper	4.27	17.24	2.29	5.55	16.01	6.61	14.89	19.27	0.75	2	12	0.38
10	Lower	4.57	17.34	2.3	5.94	16.01	6.61	15.3	19.65	0.75	2	12	0.44
9	Upper	4.57	24.08	3.2	5.94	16.01	6.61	22.04	18.76	0.75	2	12	0.44
9	Lower	4.57	24.08	3.2	5.94	16.01	6.61	22.04	18.76	0.75	2	12	0.44
8	Upper	4.57	17.17	2.28	5.94	16.02	6.61	15.13	19.68	0.75	2	12	0.44
8	Lower	4.57	17.17	2.28	5.94	16.02	6.61	15.13	19.68	0.75	2	12	0.44
7	Upper	4.57	24.66	3.28	5.94	16.01	6.61	22.63	18.68	0.75	2	12	0.44
7	Lower	4.57	24.66	3.28	5.94	16.01	6.61	22.63	18.68	0.75	2	12	0.44
6	Upper	4.57	17.17	2.28	5.94	18.44	7.61	14.13	22.1	0.75	2	12	0.44
6	Lower	4.88	18.31	2.43	6.34	19.24	7.94	15.25	23.14	0.75	2	13	0.56
5	Upper	4.88	26.91	3.58	6.34	17.08	7.05	24.74	19.84	0.75	2	13	0.56
5	Lower	4.88	26.91	3.58	6.34	17.08	7.05	24.74	19.84	0.75	2	13	0.56
4	Upper	4.88	18.65	2.48	6.34	17.08	7.05	16.48	20.94	0.75	2	13	0.56
4	Lower	4.88	18.65	2.48	6.34	17.08	7.05	16.48	20.94	0.75	2	13	0.56
3	Upper	4.88	27.64	3.67	6.34	17.08	7.05	25.47	19.75	0.75	2	13	0.56
3	Lower	4.88	27.64	3.67	6.34	17.08	7.05	25.47	19.75	0.75	2	13	0.56
2	Upper	4.88	18.31	2.43	6.34	19.24	7.94	15.25	23.14	0.75	2	13	0.56
2	Lower	4.44	21.57	1.39	6.66	18.11	8.96	17.05	23.38	1	2.5	14	0.63
1	Upper	4.44	43.95	2.83	6.66	18.11	8.96	39.43	21.94	1	2.5	14	0.63
ta: 011886	et plate thicl	rness											

 t_g : gusset plate thickness

Table 13: Gusset plates details of 20-Story building archetype

Lower 3.35 17.91 2.38 4.36 12.27 5.07 16.20 14.25 0.50 1.5 9 0.5	Laval		Dimentions A , B , and L_1 to L_6 for gusset plates (all dimensions are in inches)										Weld properties	
20 Upper 3.35 13.16 1.75 4.36 13.92 5.75 10.77 16.53 0.50 1.5 9 0.2 20 Lower 3.96 15.45 2.05 5.15 15.52 6.41 13.01 18.62 0.50 1.5 11 0.2 19 Lower 3.96 21.94 2.92 5.15 14.41 5.95 19.95 16.65 0.50 1.5 11 0.0 18 Upper 3.96 15.45 2.05 5.15 15.52 6.41 13.01 18.62 0.50 1.5 11 0.0 18 Lower 4.27 17.17 2.28 5.55 16.01 6.61 22.23 18.29 0.75 2 12 0.0 16 Upper 4.27 17.17 2.28 5.55 16.01 6.65 14.79 19.37 0.75 2 12 0.2 16 Upper 4.27 25.10 </th <th>Level</th> <th></th> <th>L_1</th> <th>L_2</th> <th>L_3</th> <th>L_4</th> <th>L_5</th> <th>L_6</th> <th>A</th> <th>В</th> <th>t_g</th> <th>L_{gph}</th> <th>L_{wbr}</th> <th>D_{wbr}</th>	Level		L_1	L_2	L_3	L_4	L_5	L_6	A	В	t_g	L_{gph}	L_{wbr}	D_{wbr}
Lower 3.96 15.45 2.05 5.15 15.52 6.41 13.01 18.62 0.50 1.5 11 0.00	21	Lower	3.35	17.91	2.38	4.36	12.27	5.07	16.20	14.25	0.50	1.5	9	0.31
19	20	Upper	3.35	13.16	1.75	4.36	13.92	5.75	10.77	16.53	0.50	1.5	9	0.31
19	20	Lower	3.96	15.45	2.05	5.15	15.52	6.41	13.01	18.62	0.50	1.5	11	0.31
18 Upper 3.96 15.45 2.05 5.15 15.52 6.41 13.01 18.62 0.50 1.5 11 0.0 18 Lower 4.27 17.17 2.28 5.55 16.06 6.92 14.52 20.03 0.75 2 12 0.0 17 Upper 4.27 24.57 3.26 5.55 16.01 6.61 22.23 18.29 0.75 2 12 0.0 16 Upper 4.27 17.17 2.28 5.55 16.10 6.65 14.79 19.37 0.75 2 12 0.0 16 Lower 4.27 17.17 2.28 5.55 16.01 6.61 14.79 19.37 0.75 2 12 0.0 15 Upper 4.27 17.17 2.28 5.55 16.01 6.61 22.76 18.22 0.75 2 12 0.0 15 Lower 4.27 17.34	19	Upper	3.96	21.94	2.92	5.15	14.41	5.95	19.95	16.65	0.50	1.5	11	0.31
18	19	Lower	3.96	21.94	2.92	5.15	14.41	5.95	19.95	16.65	0.50	1.5	11	0.31
17	18	Upper	3.96	15.45	2.05	5.15	15.52	6.41	13.01	18.62	0.50	1.5	11	0.31
17	18	Lower	4.27	17.17	2.28	5.55	16.76	6.92	14.52	20.03	0.75	2	12	0.38
16 Upper 4.27 17.17 2.28 5.55 16.10 6.65 14.79 19.37 0.75 2 12 0.0 16 Lower 4.27 17.17 2.28 5.55 16.10 6.65 14.79 19.37 0.75 2 12 0.0 15 Upper 4.27 25.10 3.34 5.55 16.01 6.61 22.76 18.22 0.75 2 12 0.0 14 Upper 4.27 17.24 2.29 5.55 16.01 6.61 14.89 19.27 0.75 2 12 0.0 14 Lower 4.57 17.34 2.30 5.94 16.01 6.61 15.30 19.65 0.75 2 12 0.2 13 Upper 4.57 23.58 3.13 5.94 16.01 6.61 21.54 18.82 0.75 2 12 0.2 12 Upper 4.57 17.17	17	Upper	4.27	24.57	3.26	5.55	16.01	6.61	22.23	18.29	0.75	2	12	0.38
16 Lower 4.27 17.17 2.28 5.55 16.10 6.65 14.79 19.37 0.75 2 12 0.0 15 Upper 4.27 25.10 3.34 5.55 16.01 6.61 22.76 18.22 0.75 2 12 0.0 15 Lower 4.27 25.10 3.34 5.55 16.01 6.61 22.76 18.22 0.75 2 12 0.0 14 Upper 4.27 17.24 2.29 5.55 16.01 6.61 14.89 19.27 0.75 2 12 0.0 13 Upper 4.57 17.34 2.30 5.94 16.01 6.61 21.54 18.82 0.75 2 12 0.0 13 Lower 4.57 17.17 2.28 5.94 17.35 7.16 14.58 20.01 0.75 2 12 0.2 12 Upper 4.27 17.17	17	Lower	4.27	24.57	3.26	5.55	16.01	6.61	22.23	18.29	0.75	2	12	0.38
15 Upper 4.27 25.10 3.34 5.55 16.01 6.61 22.76 18.22 0.75 2 12 0.0 15 Lower 4.27 25.10 3.34 5.55 16.01 6.61 22.76 18.22 0.75 2 12 0.0 14 Upper 4.27 17.24 2.29 5.55 16.01 6.61 14.89 19.27 0.75 2 12 0.0 14 Lower 4.57 17.34 2.30 5.94 16.01 6.61 15.30 19.65 0.75 2 12 0.2 13 Upper 4.57 23.58 3.13 5.94 16.01 6.61 21.54 18.82 0.75 2 12 0.2 12 Upper 4.57 17.17 2.28 5.94 17.35 7.16 14.58 21.01 0.75 2 12 0.2 12 Lower 4.27 17.17	16	Upper	4.27	17.17	2.28	5.55	16.10	6.65	14.79	19.37	0.75	2	12	0.38
15 Lower 4.27 25.10 3.34 5.55 16.01 6.61 22.76 18.22 0.75 2 12 0.01 14 Upper 4.27 17.24 2.29 5.55 16.01 6.61 14.89 19.27 0.75 2 12 0.01 14 Lower 4.57 17.34 2.30 5.94 16.01 6.61 15.30 19.65 0.75 2 12 0.01 13 Upper 4.57 23.58 3.13 5.94 16.01 6.61 21.54 18.82 0.75 2 12 0.01 13 Lower 4.57 23.58 3.13 5.94 16.01 6.61 21.54 18.82 0.75 2 12 0.01 13 Lower 4.57 23.58 3.13 5.94 16.01 6.61 21.54 18.82 0.75 2 12 0.01 12 Upper 4.57 17.17 2.28 5.94 17.35 7.16 14.58 21.01 0.75 2 12 0.01 12 Lower 4.27 17.17 2.28 5.55 17.43 7.19 14.24 20.70 0.75 2 12 0.01 11 Upper 4.27 24.56 3.26 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.01 11 Lower 4.27 24.56 3.26 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.01 10 Upper 4.27 17.17 2.28 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.01 10 Upper 4.28 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.01 10 Lower 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.01 10 Lower 4.88 18.65 2.48 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.01 18 Lower 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.01 19 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.01 10 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.01 10 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.01 10 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.01 10 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.01 10 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.01 10 Upper 4.88 27.40 3.64 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.01 10 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.01 10 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.01 10 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.01 10 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.01 10 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.01 10 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.01 10 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.01 10 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.01 10 Upp	16	Lower	4.27	17.17	2.28	5.55	16.10	6.65	14.79	19.37	0.75	2	12	0.38
14 Upper 4.27 17.24 2.29 5.55 16.01 6.61 14.89 19.27 0.75 2 12 0.01 14 Lower 4.57 17.34 2.30 5.94 16.01 6.61 15.30 19.65 0.75 2 12 0.02 13 Upper 4.57 23.58 3.13 5.94 16.01 6.61 21.54 18.82 0.75 2 12 0.02 12 Upper 4.57 17.17 2.28 5.94 17.35 7.16 14.58 21.01 0.75 2 12 0.02 12 Upper 4.27 17.17 2.28 5.55 17.43 7.19 14.24 20.70 0.75 2 12 0.02 11 Upper 4.27 24.56 3.26 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.03 10 Upper 4.27 17.17 <td>15</td> <td>Upper</td> <td>4.27</td> <td>25.10</td> <td>3.34</td> <td>5.55</td> <td>16.01</td> <td>6.61</td> <td>22.76</td> <td>18.22</td> <td>0.75</td> <td>2</td> <td>12</td> <td>0.38</td>	15	Upper	4.27	25.10	3.34	5.55	16.01	6.61	22.76	18.22	0.75	2	12	0.38
14 Lower 4.57 17.34 2.30 5.94 16.01 6.61 15.30 19.65 0.75 2 12 0.4 13 Upper 4.57 23.58 3.13 5.94 16.01 6.61 21.54 18.82 0.75 2 12 0.4 13 Lower 4.57 23.58 3.13 5.94 16.01 6.61 21.54 18.82 0.75 2 12 0.4 12 Upper 4.57 17.17 2.28 5.94 17.35 7.16 14.58 21.01 0.75 2 12 0.2 12 Lower 4.27 17.17 2.28 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.2 11 Lower 4.27 24.56 3.26 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.2 10 Upper 4.27 17.17	15	Lower	4.27	25.10	3.34	5.55	16.01	6.61	22.76	18.22	0.75	2	12	0.38
13 Upper 4.57 23.58 3.13 5.94 16.01 6.61 21.54 18.82 0.75 2 12 0.0 13 Lower 4.57 23.58 3.13 5.94 16.01 6.61 21.54 18.82 0.75 2 12 0.0 12 Upper 4.57 17.17 2.28 5.94 17.35 7.16 14.58 21.01 0.75 2 12 0.0 12 Lower 4.27 17.17 2.28 5.55 17.43 7.19 14.24 20.70 0.75 2 12 0.0 11 Upper 4.27 24.56 3.26 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.0 11 Lower 4.27 17.17 2.28 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.0 10 Upper 4.88 18.31	14	Upper	4.27	17.24	2.29	5.55	16.01	6.61	14.89	19.27	0.75	2	12	0.38
13 Lower 4.57 23.58 3.13 5.94 16.01 6.61 21.54 18.82 0.75 2 12 0.4 12 Upper 4.57 17.17 2.28 5.94 17.35 7.16 14.58 21.01 0.75 2 12 0.4 12 Lower 4.27 17.17 2.28 5.55 17.43 7.19 14.24 20.70 0.75 2 12 0.4 11 Upper 4.27 24.56 3.26 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.4 11 Lower 4.27 24.56 3.26 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.4 11 Lower 4.27 17.17 2.28 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.4 10 Upper 4.27 17.17 2.28 5.55 16.76 6.92 14.52 20.03 0.75 2 12 0.4 10 Lower 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.4 9 Upper 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.4 9 Lower 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.4 8 Upper 4.88 18.65 2.48 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.4 8 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.4 7 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.4 7 Lower 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.4 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.4 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.4 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.4 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.4 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.4 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.4 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.4 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.4 6 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.4 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.4 6 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.4 6 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.4 6 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.4 6 Upper 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.4	14	Lower	4.57	17.34	2.30	5.94	16.01	6.61	15.30	19.65	0.75	2	12	0.44
12 Upper 4.57 17.17 2.28 5.94 17.35 7.16 14.58 21.01 0.75 2 12 0.4 12 Lower 4.27 17.17 2.28 5.55 17.43 7.19 14.24 20.70 0.75 2 12 0.3 11 Upper 4.27 24.56 3.26 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.3 10 Upper 4.27 17.17 2.28 5.55 16.76 6.92 14.52 20.03 0.75 2 12 0.3 10 Lower 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.3 9 Upper 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.3 8 Upper 4.88 18.65	13	Upper	4.57	23.58	3.13	5.94	16.01	6.61	21.54	18.82	0.75	2	12	0.44
12 Lower 4.27 17.17 2.28 5.55 17.43 7.19 14.24 20.70 0.75 2 12 0.1 11 Upper 4.27 24.56 3.26 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.1 11 Lower 4.27 24.56 3.26 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.1 10 Upper 4.27 17.17 2.28 5.55 16.76 6.92 14.52 20.03 0.75 2 12 0.1 10 Lower 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.1 9 Upper 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.1 8 Upper 4.88 18.65 2.48 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.1 8 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.1 7 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.1 7 Lower 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.1 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.1 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.1 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.1 6 Upper 4.88 27.40 3.64 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.1 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.1 6 Upper 4.88 27.40 3.64 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.1 6 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.1 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.1 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.1 6 Lower 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.1 7 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.1 7 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.1 7 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.1 8 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.1 8 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.1 9 Upper 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.1	13	Lower	4.57	23.58	3.13	5.94	16.01	6.61	21.54	18.82	0.75	2	12	0.44
11 Upper 4.27 24.56 3.26 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.3 11 Lower 4.27 24.56 3.26 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.3 10 Upper 4.27 17.17 2.28 5.55 16.76 6.92 14.52 20.03 0.75 2 12 0.3 10 Lower 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.3 9 Upper 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.3 8 Upper 4.88 18.65 2.48 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.3 8 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13	12	Upper	4.57	17.17	2.28	5.94	17.35	7.16	14.58	21.01	0.75	2	12	0.44
11 Lower 4.27 24.56 3.26 5.55 16.01 6.61 22.22 18.30 0.75 2 12 0.3 10 Upper 4.27 17.17 2.28 5.55 16.76 6.92 14.52 20.03 0.75 2 12 0.3 10 Lower 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.3 9 Upper 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.3 9 Lower 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.3 8 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 8 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 7 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 7 Lower 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3	12	Lower	4.27	17.17	2.28	5.55	17.43	7.19	14.24	20.70	0.75	2	12	0.5
10 Upper 4.27 17.17 2.28 5.55 16.76 6.92 14.52 20.03 0.75 2 12 0.5 10 Lower 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.5 9 Upper 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.5 8 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.5 8 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.5 7 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.5 7 Lower 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 </td <td>11</td> <td>Upper</td> <td>4.27</td> <td>24.56</td> <td>3.26</td> <td>5.55</td> <td>16.01</td> <td>6.61</td> <td>22.22</td> <td>18.30</td> <td>0.75</td> <td>2</td> <td>12</td> <td>0.5</td>	11	Upper	4.27	24.56	3.26	5.55	16.01	6.61	22.22	18.30	0.75	2	12	0.5
10 Lower 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.3 9 Upper 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.3 9 Lower 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.3 8 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 8 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 7 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 <td>11</td> <td>Lower</td> <td>4.27</td> <td>24.56</td> <td>3.26</td> <td>5.55</td> <td>16.01</td> <td>6.61</td> <td>22.22</td> <td>18.30</td> <td>0.75</td> <td>2</td> <td>12</td> <td>0.5</td>	11	Lower	4.27	24.56	3.26	5.55	16.01	6.61	22.22	18.30	0.75	2	12	0.5
9 Upper 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.3 9 Lower 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.3 8 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 8 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 7 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 <td>10</td> <td>Upper</td> <td>4.27</td> <td>17.17</td> <td>2.28</td> <td>5.55</td> <td>16.76</td> <td>6.92</td> <td>14.52</td> <td>20.03</td> <td>0.75</td> <td>2</td> <td>12</td> <td>0.5</td>	10	Upper	4.27	17.17	2.28	5.55	16.76	6.92	14.52	20.03	0.75	2	12	0.5
9 Lower 4.88 26.64 3.54 6.34 17.08 7.05 24.46 19.88 0.75 2 13 0.3 8 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 8 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 7 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 5 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 <td>10</td> <td>Lower</td> <td>4.88</td> <td>18.31</td> <td>2.43</td> <td>6.34</td> <td>17.48</td> <td>7.22</td> <td>15.98</td> <td>21.39</td> <td>0.75</td> <td>2</td> <td>13</td> <td>0.56</td>	10	Lower	4.88	18.31	2.43	6.34	17.48	7.22	15.98	21.39	0.75	2	13	0.56
8 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 8 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 7 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 5 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 5 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.3 4 Upper 4.88 18.31	9	Upper	4.88	26.64	3.54	6.34	17.08	7.05	24.46	19.88	0.75	2	13	0.56
8 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 7 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 5 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.3 5 Lower 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.3 4 Upper 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 <td>9</td> <td>Lower</td> <td>4.88</td> <td>26.64</td> <td>3.54</td> <td>6.34</td> <td>17.08</td> <td>7.05</td> <td>24.46</td> <td>19.88</td> <td>0.75</td> <td>2</td> <td>13</td> <td>0.56</td>	9	Lower	4.88	26.64	3.54	6.34	17.08	7.05	24.46	19.88	0.75	2	13	0.56
7 Upper 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 7 Lower 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 5 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 5 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.3 4 Upper 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.3	8	Upper	4.88	18.65	2.48	6.34	17.08	7.05	16.48	20.94	0.75	2	13	0.56
7 Lower 4.88 27.40 3.64 6.34 17.08 7.05 25.22 19.78 0.75 2 13 0.3 6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 6 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 5 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.3 5 Lower 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.3 4 Upper 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.3	8	Lower	4.88	18.65	2.48	6.34	17.08	7.05	16.48	20.94	0.75	2	13	0.56
6 Upper 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.5 6 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.5 5 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.5 5 Lower 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.5 4 Upper 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.5	7	Upper	4.88	27.40	3.64	6.34	17.08	7.05	25.22	19.78	0.75	2	13	0.56
6 Lower 4.88 18.65 2.48 6.34 17.08 7.05 16.48 20.94 0.75 2 13 0.3 5 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.3 5 Lower 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.3 6 Upper 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.3	7	Lower	4.88	27.40	3.64	6.34	17.08	7.05	25.22	19.78	0.75	2	13	0.56
5 Upper 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.5 5 Lower 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.5 4 Upper 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.5	6	Upper	4.88	18.65	2.48	6.34	17.08	7.05	16.48	20.94	0.75	2	13	0.56
5 Lower 4.88 27.87 3.70 6.34 17.08 7.05 25.70 19.72 0.75 2 13 0.34 Upper 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.35	6	Lower	4.88	18.65	2.48	6.34	17.08	7.05	16.48	20.94	0.75	2	13	0.56
4 Upper 4.88 18.31 2.43 6.34 17.48 7.22 15.98 21.39 0.75 2 13 0.5	5	Upper	4.88	27.87	3.70	6.34	17.08	7.05	25.70	19.72	0.75	2	13	0.56
**	5	Lower	4.88	27.87	3.70	6.34	17.08	7.05	25.70	19.72	0.75	2	13	0.56
4 Lower 5.49 20.08 2.67 7.13 18.68 7.71 17.89 23.14 1.00 2.5 14 0.0	4	Upper	4.88	18.31	2.43	6.34	17.48	7.22	15.98	21.39	0.75	2	13	0.56
	4	Lower	5.49	20.08	2.67	7.13	18.68	7.71	17.89	23.14	1.00	2.5	14	0.63
3 Upper 5.49 31.40 4.17 7.13 18.68 7.71 29.17 21.64 1.00 2.5 14 0.0	3	Upper	5.49	31.40	4.17	7.13	18.68	7.71	29.17	21.64	1.00	2.5	14	0.63
3 Lower 5.49 31.40 4.17 7.13 18.68 7.71 29.17 21.64 1.00 2.5 14 0.0	3	Lower	5.49	31.40	4.17	7.13	18.68	7.71	29.17	21.64	1.00	2.5	14	0.63
2 Upper 5.49 20.08 2.67 7.13 18.68 7.71 17.86 23.14 1.00 2.5 14 0.0	2	Upper	5.49	20.08	2.67	7.13	18.68	7.71	17.86	23.14	1.00	2.5	14	0.63
2 Lower 4.99 24.20 1.56 7.49 18.11 8.96 20.23 24.04 1.00 2.5 14 0.0	2	Lower	4.99	24.20	1.56	7.49	18.11	8.96	20.23	24.04	1.00	2.5	14	0.63
1 Upper 4.99 45.98 2.97 7.49 18.11 8.96 42.02 22.64 1.00 2.5 14 0.0	1	Upper	4.99	45.98	2.97	7.49	18.11	8.96	42.02	22.64	1.00	2.5	14	0.63

tg: gusset plate thickness

References

- [1] C. Kircher, G. Deierlein, J. Hooper, H. Krawinkler, S. Mahin, B. Shing, J. Wallace, Evaluation of the FEMA P-695 Methodology for Quantification of Building Seismic Performance Factors, (2010).
- [2] CSI, Integrated building design software, ETABS Version 20, Computers and Structures Inc., Berkeley, California, USA, (2022).
- [3] ASCE/SEI 7-16, Minimum design loads and associated criteria for buildings and other structures, American Society of Civil Engineers, Reston, Virginia, 2017.
- [4] ANSI/AISC 360-16, Specification for Structural Steel Buildings, American Institute of Steel Construction, Chicago, Illinois, 2016.
- [5] ANSI/AISC 341-16, Seismic Provisions for Structural Steel Buildings, American Institute of Steel Construction, Chicago, Illinois, 2016.
- [6] ANSI/AISC 358-16, Prequalified Connections for Special and Intermediate Steel Moment Frames for Seismic Application, American Institute of Steel Construction, Chicago, Illinois, 2016.
- [7] FEMA, Quantification of building seismic performance factors, Washington, D.C, 2009.
- [8] A. Astaneh-Asl, M. Cochran, R. Sabelli, Seismic detailing of gusset plates for special concentrically braced frames, 2006.