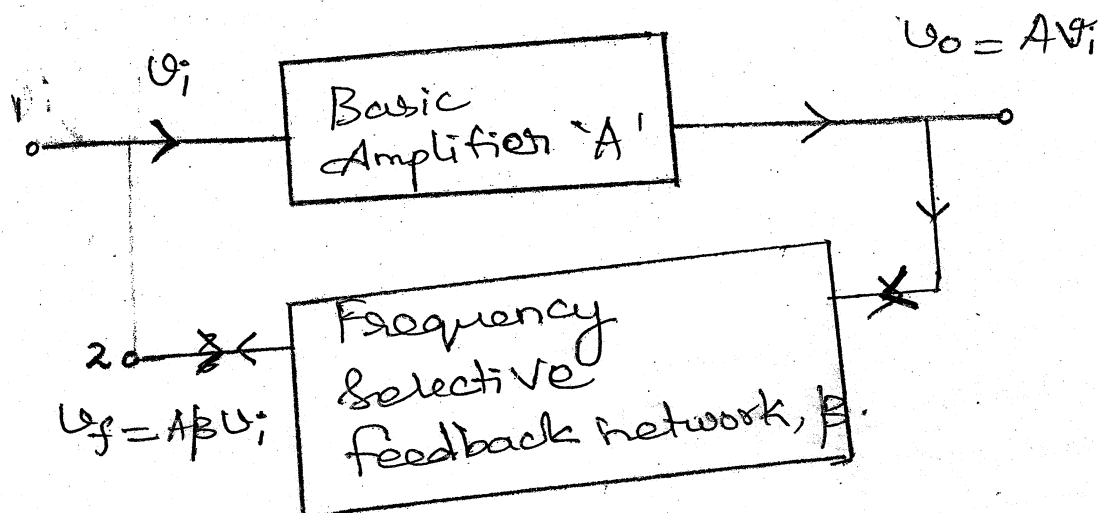


Sine Wave Generators: (Oscillators)

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The feedback oscillator can be used as a sine wave oscillator. It consists of an amplifier with gain A and a frequency selective feedback network with transfer ratio β .

Basic structure of a feedback oscillator:



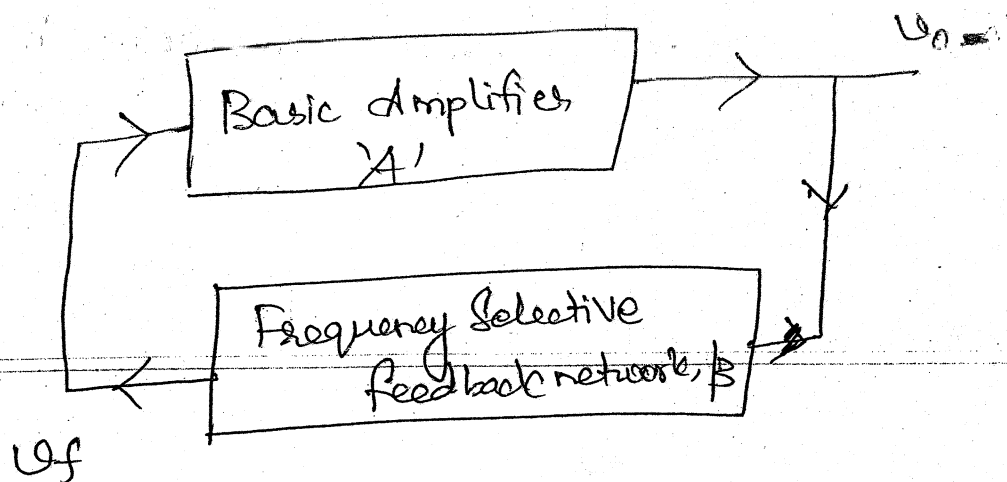
* Output voltage
 $U_o = AU_i$

* feedback voltage: $U_f = \beta U_o$
 $U_f = A\beta U_i \rightarrow \textcircled{1}$

* $A\beta$ = loop gain of the system.

* If $A\beta = 1$, $U_f = U_i$, from eqn $\textcircled{1}$.

\therefore If we join terminals $\textcircled{1}$ & $\textcircled{2}$ and remove external signal, $A\beta = 1$



$$A = \frac{V_o}{V_f}, \quad B = \frac{V_f}{V_o}$$

Barkhausen Criterion for oscillation:

An output signal can be continuously obtained without any input signal, if the loop gain of the system satisfies the following condition.

$$AB = 1$$

Note:

The condition ~~of~~ $AB = 1$ can be satisfied only at one specific frequency f_0 for the given component values.

∴ The condition for oscillation can be rewritten as

$$A(j\omega_0) B(j\omega_0) = 1 \angle 0^\circ$$

i.e.

$$|AB| = 1$$

$$\angle AB = 0^\circ \text{ (or) multiples of } 2\pi$$

Note:

Practically the oscillators are designed for $|A\beta| > 1$ so that oscillations grow.

Types of sine wave oscillators:

The sine wave oscillators are classified according to range of frequency.

(a) Audio frequency oscillators:
(few hertz to several 100 kHz)

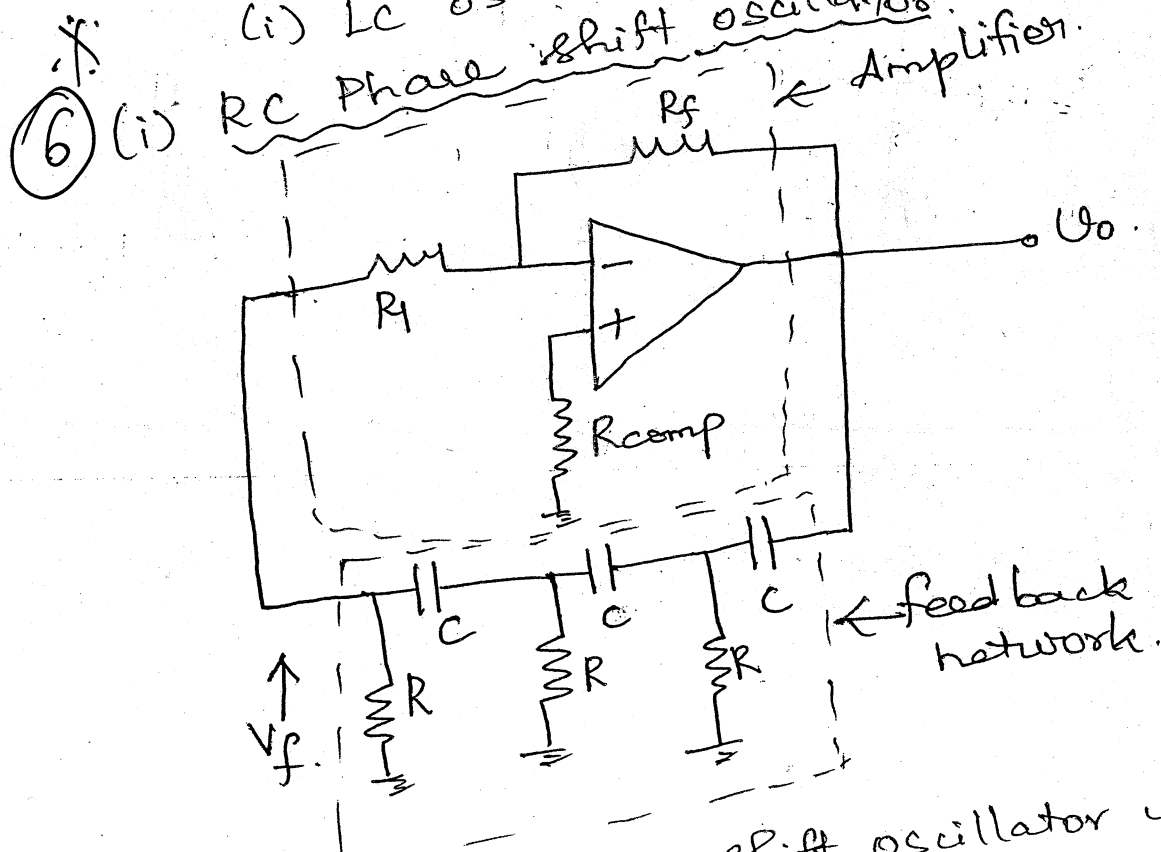
(i) RC phase shift oscillator.

(ii) Wein bridge oscillator.

(b) High frequency oscillators:

(i) LC oscillator.

(ii) RC phase shift oscillator.



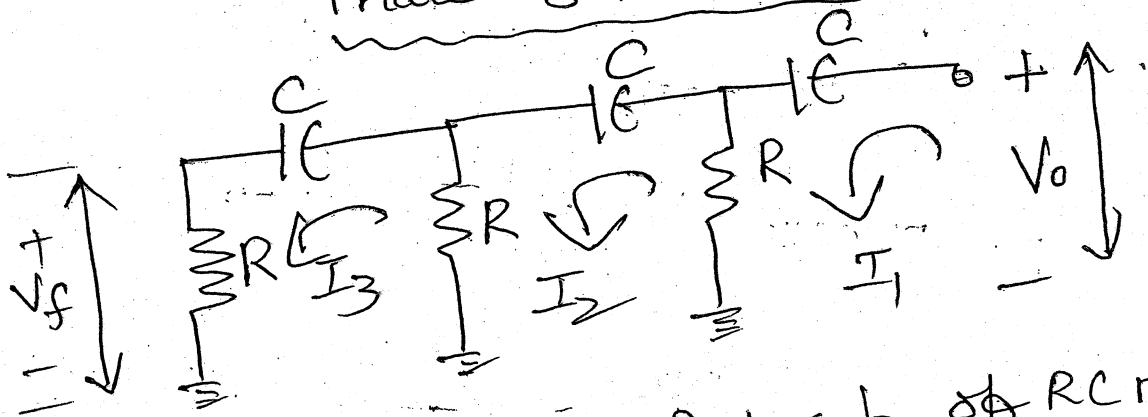
The RC phase shift oscillator uses op-amp in ~~an~~ inverting mode. Therefore

it provides a 180° phase shift. To introduce additional 180° phase shift so that total phase shift is 360° , we use RC feedback network.

The RC feedback network consists of 3 identical RC stages where each stage provides a phase shift of 60° .

Analysis:

Phase shift network:



Calculating feedback factor β of RC n/w:

Applying KVL for loop 1.

$$\frac{I_1}{j\omega C} + (I_1 - I_2)R = V_o$$

Substitute $j\omega = s$.

$$\frac{I_1}{sC} + (I_1 - I_2)R = V_o$$

$$\boxed{\frac{I_1}{sC} + (I_1 - I_2)R = V_o} \quad \text{--- (1)}$$

Applying KVL for Loop2:

(27) (28)
V-9

$$I_2 \cdot \frac{1}{j\omega C} + (I_2 - I_3)R + (I_2 - I_1)R = 0.$$

Sub $j\omega = s$

$$\frac{I_2}{sC} + I_2 R - I_3 R + I_2 R - I_1 R = 0.$$

$$\boxed{-I_1 R + I_2 (2R + \frac{1}{sC}) - I_3 R = 0} \rightarrow \textcircled{2}$$

Applying KVL for Loop3:

$$\frac{I_3}{j\omega C} + I_3 R + (I_3 - I_2)R = 0.$$

Sub $j\omega = s$

$$\frac{I_3}{sC} + I_3 R + R I_3 - I_2 R = 0.$$

$$\boxed{0 - I_2 R + I_3 (2R + \frac{1}{sC}) = 0} \rightarrow \textcircled{3}$$

$$\boxed{V_f = I_3 R} \rightarrow \textcircled{4}$$

$$\begin{bmatrix} R + \frac{1}{sC} & -R & 0 \\ -R & (2R + \frac{1}{sC}) & -R \\ 0 & -R & (2R + \frac{1}{sC}) \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ I_3 \end{bmatrix} = \begin{bmatrix} V_0 \\ 0 \\ 0 \end{bmatrix}$$

$$\Delta = \left(R + \frac{1}{sC}\right) \left[\left(2R + \frac{1}{sC}\right) \left(2R + \frac{1}{sC}\right) - (-R)(-R) \right]$$

$$+ R \left[-R \left(2R + \frac{1}{sC}\right) - 0 \right]$$

$$= \left(R + \frac{1}{sC}\right) \left(\left(2R + \frac{1}{sC}\right)^2 - R^2 \right) + R \left[-2R^2 - \frac{R}{sC} \right]$$

$$= \left(R + \frac{1}{sC}\right) \left(4R^2 + \frac{1}{s^2 C^2} + \frac{4R}{sC} - R^2 \right) - 2R^3 - \frac{R^2}{sC}$$

$$= \left(R + \frac{1}{sC}\right) \left(3R^2 + \frac{1}{s^2 C^2} + \frac{4R}{sC} \right) - 2R^3 - \frac{R^2}{sC}$$

$$= 3R^3 + \frac{R}{s^2 C^2} + \frac{4R^2}{sC} + \frac{3R^2}{sC} + \frac{1}{s^3 C^3} + \frac{4R}{s^2 C^2} - 2R^3 - \frac{R^2}{sC}$$

$$\Delta = R^3 + 6 \frac{R^2}{sC} + \frac{5R}{s^2 C^2} + \frac{1}{s^3 C^3}$$

$$\Delta I_3 = \begin{bmatrix} \left(R + \frac{1}{sC}\right) & -R & V_0 \\ -R & \left(2R + \frac{1}{sC}\right) & 0 \\ 0 & -R & 0 \end{bmatrix} = \left(R + \frac{1}{sC}\right)(0-0) + R[0-0] + V_0[R^2-0]$$

$$= \boxed{V_0 R^2}$$

$$\therefore I_3 = \frac{\Delta I_3}{\Delta} = \frac{V_0 R^2}{R^3 + 6 \frac{R^2}{sC} + \frac{5R}{s^2 C^2} + \frac{1}{s^3 C^3}}$$

⑤ ⑥ ⑦
V-10

$$I_3 = \frac{V_0 R^2 s^3 C^3}{1 + 5RSC + 6R^2 S^2 C^2 + R^3 S^3 C^3}$$

⑤

From eqn ④ $\Rightarrow V_f = I_3 R$

Sub eqn ⑤

$$V_f = \frac{V_0 R^3 S^3 C^3}{1 + 5SRC + 6S^2 R^2 C^2 + R^3 C^3 S^3}$$

⑥

$$\beta = \frac{V_f}{V_0}$$

From eqn ⑥, $\beta = \frac{V_f}{V_0} = \frac{R^3 S^3 C^3}{1 + 5SRC + 6S^2 R^2 C^2 + R^3 C^3 S^3}$

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ator

\div by $S^3 C^3 R^3$

$$\beta = \frac{1}{\frac{1}{S^3 C^3 R^3} + \frac{5}{S^2 R^2 C^2} + \frac{6}{SRC} + 1}$$

Sub $s = j\omega$. $\therefore s^2 = -\omega^2$, $s^3 = -j\omega^3$.

$$\beta = \frac{1}{1 + \frac{6}{j\omega RC} - \frac{5}{\omega^2 R^2 C^2} - \frac{1}{j\omega^3 C^3 R^3}}$$

⑦

Let cut off parameter $\alpha = \frac{1}{\omega RC}$

Sub ' α ' in eqn ⑦.

$$\beta = \frac{1}{1 + \frac{6\alpha}{j} - \frac{5\alpha^2 - \alpha^3}{j}}$$

$$\beta = \frac{1}{1 - j6\alpha - 5\alpha^2 + j\alpha^3}$$

$$\beta = \frac{1}{(1 - 5\alpha^2) + j\alpha(\alpha^2 - 6)} \rightarrow \textcircled{8}$$

For $A\beta = 1$, β should be real.

i.e. imaginary term should be zero.

$$\alpha(\alpha^2 - 6) = 0$$

$$\alpha^3 - 6 = 0$$

$$\alpha^3 = 6$$

$$\alpha = \sqrt[3]{6}$$

$$\therefore \frac{1}{\omega RC} = \sqrt[3]{6}$$

$$\Rightarrow \frac{1}{2\pi f RC} = \sqrt[3]{6} \Rightarrow f = \frac{1}{2\pi RC \sqrt[3]{6}}$$

\therefore Frequency of oscillation,

$$f_0 = \frac{1}{2\pi RC \sqrt[3]{6}}$$

when $\alpha^2 = 6$

$$\beta = \frac{1}{(1-5\alpha^2)} = \frac{1}{(1-5 \times 6)} = \frac{1}{(1-30)} = -\frac{1}{29}$$

$$\boxed{\beta = -\frac{1}{29}}$$

The negative sign indicates RC feedback
w/o produces a phase shift of 180° .

$$|\beta| = \frac{1}{29}$$

For sustained oscillation $|A\beta| \geq 1$

$$\therefore \left| \frac{A}{29} \right| \geq 1$$

$$\therefore \boxed{|A| \geq 29}$$

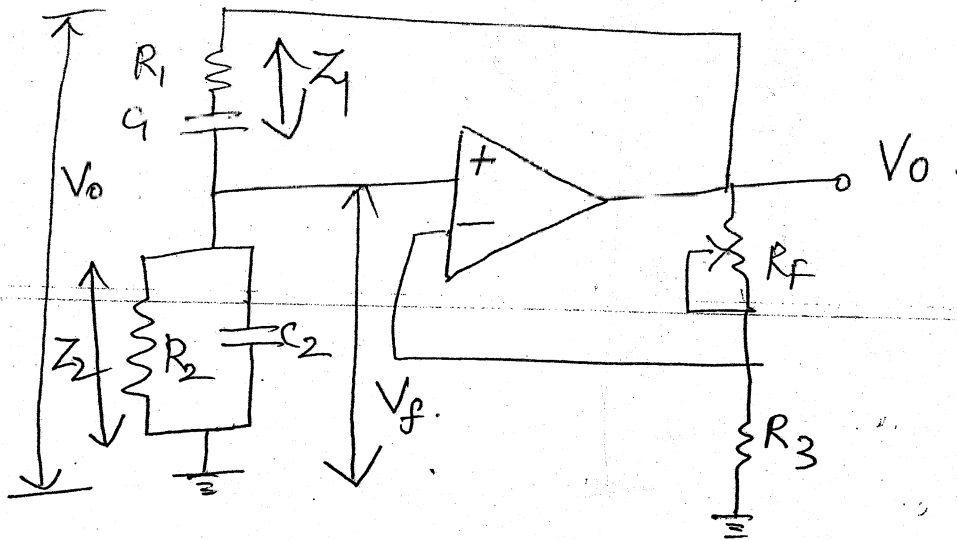
\therefore The gain of inverting op-amp
should be at least 29.

Gain of inverting op-amp $A = -\frac{R_f}{R_i}$

$$|A| = \left| \frac{R_f}{R_i} \right| = 29$$

$$\therefore \boxed{R_f = 29R_i}$$

Wien bridge Oscillator:

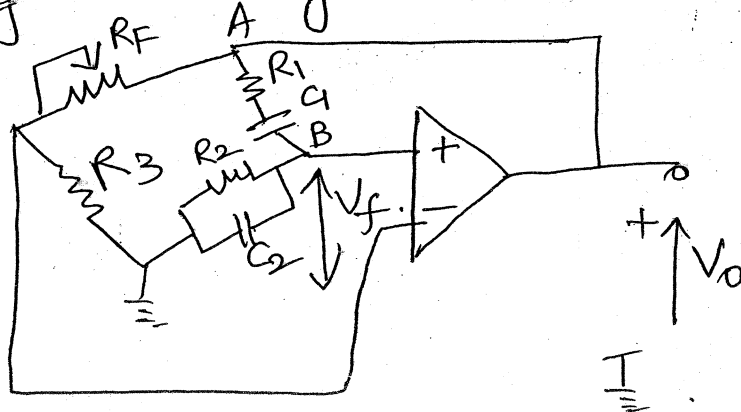


* It is a audio frequency oscillator.

* The feedback signal is connected to the non-inverting terminal of the op-amp. \therefore The feedback network does not provide any phase shift.

* The circuit can be viewed as a wien bridge with series RC n/w in one arm and parallel RC n/w in adjoining arm. Resistor R_3 and R_f in other two arms.

* We achieve zero phase shift condition, by balancing the bridge.



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chithra

(30)

V-12

Analysis:

* The gain of the op-amp amplifier

$$A = 1 + \frac{R_f}{R_3} \rightarrow \textcircled{1}$$

$$* V_f = \frac{V_o Z_2}{Z_1 + Z_2}$$

$$\therefore \frac{V_f}{V_o} = \frac{Z_2}{Z_1 + Z_2}$$

$$\beta = \frac{V_f}{V_o} = \frac{Z_2}{Z_1 + Z_2} \rightarrow \textcircled{2}$$

Chaplace transform)

$$Z_1 = R_1 + \frac{1}{sC_1} = \frac{sC_1 R_1 + 1}{sC_1} \rightarrow \textcircled{3}$$

$$Z_2 = \frac{R_2 \cdot \frac{1}{sC_2}}{R_2 + \frac{1}{sC_2}} = \frac{R_2}{1 + sC_2 R_2} \rightarrow \textcircled{4}$$

Sub $\textcircled{3}$ & $\textcircled{4}$ in $\textcircled{2}$

$$\begin{aligned} \beta &= \frac{R_2 / (1 + sC_2 R_2)}{\frac{sC_1 R_1 + 1}{sC_1} + \frac{R_2}{1 + sC_2 R_2}} \\ &= \frac{R_2 / (1 + sC_2 R_2)}{(1 + sC_1 R_1)(1 + sC_2 R_2) + R_2 sC_1} \end{aligned}$$

$$= \frac{R_2 s C_1}{(1 + s C_1 R_1)(1 + s C_2 R_2) + R_2 s C_1}$$

$$= \frac{s R_2 C_1}{1 + s C_1 R_1 + s C_2 R_2 + s^2 R_1 R_2 C_1 C_2 + s R_2 C_1}$$

$$\beta = \frac{s R_2 C_1}{1 + s(R_1 C_1 + R_2 C_2 + R_2 C_1) + s^2 R_1 R_2 C_1 C_2} \quad (1)$$

Let $s = j\omega$.

$$\beta = \frac{j\omega R_2 C_1}{1 + j\omega(R_1 C_1 + R_2 C_2 + R_2 C_1) - \omega^2 R_1 R_2 C_1 C_2}$$

∴ The condition for oscillation is β should be real.

$$\therefore 1 - \omega^2 R_1 R_2 C_1 C_2 = 0$$

$$\omega^2 R_1 R_2 C_1 C_2 = 1$$

$$\omega^2 = \frac{1}{R_1 R_2 C_1 C_2}$$

$$\omega = \frac{1}{\sqrt{R_1 R_2 C_1 C_2}} = 2\pi f_0$$

∴ Frequency of oscillation

$$f_0 = \frac{1}{2\pi \sqrt{R_1 R_2 C_1 C_2}} \quad (6)$$

* when oscillation condition is satisfied, (31) (32)

$$\beta = \frac{j\omega R_2 C}{j\omega (R_1 C + R_2 C + R_2 C)}$$

V-13

$$\beta = \frac{R_2 C}{(R_1 C + R_2 C + R_2 C)} \rightarrow \text{A}$$

* If $R_1 = R_2 = R$ & $C = C_2 = C$

$$(6) \Rightarrow f_0 = \frac{1}{2\pi\sqrt{R^2 C^2}} = \frac{1}{2\pi RC}$$

$$(7) \Rightarrow \beta = \frac{RC}{(RC + RC + RC)} = \frac{RC}{3RC} = \frac{1}{3}$$

* Note:
For sustained oscillation

$$|A\beta| \geq 1$$

$$|A/\beta| \geq 1$$

$$|A| \geq 3$$

$$A = 1 + \frac{R_F}{R_3}$$

$$1 + \frac{R_F}{R_3} = 3 \Rightarrow \frac{R_F}{R_3} = 2 \Rightarrow R_F = 2R_3$$

Disadvantages:

It cannot be used for generating high frequency signals as it does not provide phase shift.