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## 1.INTRODUCTION

This document constitutes the user manual for Trio-U software. It supersedes the previous document.

TRIO-U is a thermohydraulic calculation modular software package. The two currently available modules include a VDF calculation module “Finite Difference Volume” and a VEF calculation module “Finite Element Volume”.

The VDF and VEF modules are designed to process the 2D or 3D flow of Newtonian, incompressible, weakly expandable fluids the density of which is a function of a local temperature and concentration values (Boussinesq approximation).

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## 2.DATA SET DESCRIPTION

### 2.1BASIC RULES

There is no line concept in Trio-U.

A block may be defined using the braces:

```
{
    a block
}
```

Objects are created in the data set as follows:

*[export] Type identificateur*

**export:** if this keyword is included, *identificateur* (*identifier*) will have a global range, if not its range will apply to the block only (the associated object will be destroyed on exiting the block).

*Type:* every type of object recognised by Trio-U. The list of types recognised is given in the file **hierarchie.dump**.

*identificateur:* the identifier of the object type *Type* created. Trio\_U exits in error if the identifier has already been used.

**Interprete** (interpretor) type objects are then used to handle the created objects with the following syntax:

*Type\_interprete argument*

*Type\_interprete:* any type derived from the **Interprete** (Interpretor) type recognised by Trio\_U. In this manual, they are written in bold.

*argument:* an argument may comprise one or several object identifiers and/or one or several data blocks (refer to Interpretes Généraux (General Interpretors) in 2.3).

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To insert comments in the data set, use # .. # (or /\* .... \*/) the character # must always be enclosed by blanks. Since the 1.6.1 version, comments can be inserted everywhere in the data file not only between interpretors.

### Examples:

- A data set to write Ok on screen:

```

Nom un_nom           # Creation of an object type. Name identifier un_nom #
Read un_nom Ok       # Allocates the string "Ok" to un_nom #
Ecrire un_nom        # Write un_nom on screen #

```

- An incorrect data set:

```

Domaine truc
...
Probleme truc      # Trio_U exits in error #

```

A possible correction:

```

{
Domaine truc
}
# The domain truc is destroyed #
Probleme truc      # this is correct because truc is not used any more #

```

- One data set nesting another:

```

Read _file fichier_inclus ;  # you should use export in
                               the fichier_inclus to export identifiers #

```

example of the fichier\_inclus file:

```

Dimension 2
export Domaine dom
export Probleme_hydraulique pb

```

### Observations:

- The semi-colon is no longer an instruction separator as it was in TRIO-VF.

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- The comma separates items in a list (a comma must be enclosed with spaces or a new line).
- Interpretor keywords are recognised indiscriminately whether they are written in lower and/or upper case. *On the contrary, object names (identifiers) are recognised differently if they are written in upper or lower case.*
- Object names may not exceed 999 characters.
- *In the following description, items (keywords or values) enclosed by [ and ] are facultative.*

## 2.2 OBJECTS

There are several object types.

Physical objects, for example:

- A block object (keyword **Pave**) is defined by its origin and dimensions (keyword **origine** (**origin**) and **longueurs** (**length**)). Discretization is given by the **nombre\_de\_noeuds** (**node number**) in each direction.
- A **Fluide\_incompressible** (**incompressible\_Fluid**) object. This type of object is defined by its physical characteristics (its dynamic viscosity  $\mu$  (keyword **mu**), its density  $\rho$  (keyword **rho**), etc...)
- A **Domaine**.

More abstract object types also exist:

- A **VDF** or **VEF** according to the discretization type.
- **Schema\_euler\_explicite** to indicate the scheme type.
- A **Solveur\_pression** to denote the pressure system solver type.

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- A **Champ\_Uniforme** to define, for example, the gravity field.



## 2.3 INTERPRETORS

Interpretors allow some operations to be carried out on objects. Currently available general interpretors include **Read**, **Read\_file**, **Ecrire (Write)**, **Ecrire\_fichier, (Write\_file)**, **Associate**. Other interpretors shall be described further on.

### 2.3.1 READ

The **Read** interpretor allows an object to be read (defined) in various ways:

```

Read objet
{
  ....
}

```

**Read**: Keyword to read the object *objet* defined between the braces.

```

Read_file nomfic ;

```

**Read\_file**: Keyword to execute a data set given in the *nomfic* file (a space must be entered between the semi-colon and the file name).

```

Read_file objet nomfic

```

**Read \_file**: Keyword to read the object *objet* contained in the file *nomfic*. This is notably used when the calculation domain has already been meshed and the mesh contains the file *nomfic*, simply write ( where *dom* is the name of the meshed domain):

```

Read _file dom nomfic

```

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**Read\_file\_binary** objet nomfic

**Read\_file\_binary**: Keyword to read an object *objet* in the unformatted file type *nomfic*.

**Lire\_Tgrid** domain\_name filename.msh

**Lire\_Tgrid** : Keyword to read Tgrid/Gambit mesh files. 2D (triangles or quadrangles) and 3D (tetra or hexa elements) meshes, may be read by Trio\_U.

**Lire\_Ideas** domain\_name filename.unv

**Lire\_Ideas** : Keyword to read Ideas unv mesh files. 3D tetra mesh elements only may be read by Trio\_U.

**Lire\_MED** [vef] [ family\_names\_from\_group\_names|short\_family\_names ] domain\_name mesh\_name filename.med

**Lire\_MED** : Keyword to read MED mesh files where domain\_name corresponds to the domain name, filename.med corresponds to the file (written in format MED) containing the mesh named mesh\_name. Option **vef** is obsolete and is kept for backward compatibility. The option **family\_names\_from\_group\_names** uses the group names instead of the family names to detect the boundaries into a MED mesh (useful when trying to read a MED mesh file from Gmsh tool which can now read and write MED meshes). The option **short\_family\_names** is useful to suppress FAM\_-\*\_ from the boundary names of the MED meshes.

Note about naming boundaries: When reading filename.med, Trio\_U will detect boundaries between domain (Raccord) when the name of the boundary begins by "type\_raccord\_". For example, a boundary named "type\_raccord\_wall" in filename.med will be considered by Trio\_U as a boundary named wall between two domains.

**NB:** To read several domains from a mesh issued from a MED file, use **Lire\_Med** to read the mesh then use **Create\_domain\_from\_sous\_zone** keyword (see 4.3.12 chapter).

**NB:** If the MED file contains one or several subzone defined as a group of volumes, then **Lire\_MED** will read it and will create two files *ssz.geo* and *ssz\_par.geo* defining the subzones for sequential and/or parallel calculations. These subzones will be read in sequential in the datafile by including (after **Lire\_Med** keyword) something like:

**Lire\_Med** ....

**Read** ssz.geo ;

During the parallel calculation, you will include something:

**Scatter** { ... }

**Read** ssz\_par.geo ;

### 2.3.2WRITE

The **Ecrire (Write)** interpreter allows an object to be written to a file or a standard outlet.

**Ecrire** objet

**Ecrire:** Keyword to write the object objet to a standard outlet.

**Ecrire\_fichier** objet nomfic

**Ecrire\_fichier:** Keyword to write the object objet to a file *nomfic*. Since the v1.6.3, the default format is now binary format file.

A file may be written in binary format with:

**Ecrire\_fichier\_Bin** objet nomfic

It is interesting to write in binary format big meshes for example cause it is very quick to read it compare to formatted format and it needs more than twice less memory on disc.

A file may be written in ASCII format with:

**Ecrire\_fichier\_Formatte** objet nomfic

```

Postraiter_domaine
{
  format name
  [binaire 0|1]
  [fichier name]
  [joints_non_postraites 0|1 ]
  [ecrire_frontiere 0|1]
  domaine name | domaines { name1 name2 ... }
}

```

To write one or more domains in a file with a specified format (MED, LML,LATA). By default, the name of the file will be `datafile_name".format`. The file name can be changed with the **fichier** option. The **ecrire\_frontiere** option will write (if set to 1, the default) or not (if set to 0) the boundaries as fields into the file (it is useful to not add the boundaries when writing a domain extracted from another domain). The **joints\_non\_postraites** (1 by default) will not write the boundaries between the partitioned mesh. Binary (`binaire 1`) or ASCII (`binaire 0`) may be used. By default, it is 0 for LATA and only ASCII is available for LML and only binary is available for MED.

**Ecrire\_MED**: Keyword to write a domain to MED format into a file:

**Ecrire\_MED** domain\_name *filename*

**Ecrire\_Champ\_MED**: Keyword to write a field to MED format into a file. Useful for Homard.

**Ecrire\_Champ\_MED** domain\_name field\_name *filename*

### 2.3.3 ASSOCIATE

The **Associate** interpreter allows one object to be associated with another.

**Associate** objet1 objet2

The order of the two objects in this instruction is not important.

The object *objet2* is associated to *objet1* if this makes sense; if not either *objet1* is associated to *objet2* or the program exits in error because it cannot execute the **Associate** instruction.

For example, to calculate water flow in a pipe, a **Pb\_Hydraulique** type object needs to be defined. But also a **Domaine** type object to represent the pipe, a **Schema\_euler\_explicite** type object for time discretization, a discretization type object (**VDF** or **VEF**) and a **Fluide\_Incompressible** type object which will contain the water properties. These objects must then all be associated with the problem.

### 2.3.4 GEOMETRIC INSTRUCTIONS

**Dimension** dim

This instruction is mandatory.

**Dimension:** Keyword allowing calculation dimensions to be set (2D or 3D). where *dim* is an integer set to 2 or 3.

**Axi**

This instruction is facultative.

**Axi:** This keyword allows a 3D calculation to be executed using cylindrical co-ordinates (R,θ,Z). If this instruction is not included, calculations are carried out using Cartesian co-ordinates.

**Bidim\_Axi**

This instruction is facultative.

**Bidim\_Axi:** Keyword allowing a 2D calculation to be executed using axisymetric co-ordinates (R, Z). If this instruction is not included, calculations are carried out using Cartesian co-ordinates.

**Domaine dom**

Keyword to create a domain where dom is the name.

**Domaine\_ALE**  
dom

Keyword to create a domain where dom is the name with nodes at the interior of the domain are displaced in an arbitrarily prescribed way thanks to ALE description.

### 2.3.5 MESH

```

Mesh dom
{
  [Epsilon  $\epsilon$  ]
  ,
  [objet1]
  ,
  [objet2]
  .....
}

```

The **Mesh** interpreter allows a **Domain** type object *dom* to be meshed with objects *objet1*, *objet2*, etc...

Two points will be confused if the distance between them is less than  $\epsilon$ . By default,  $\epsilon$  is set to  $10^{-12}$ . The keyword **Epsilon** allows an alternative value to be assigned to  $\epsilon$ .

Currently, the two types of objects recognised by TRIO-U to mesh a domain are the **Domain** or the **Pave (block)** object. For example, to mesh a domain *dom* with 3 other domains *domA*, *domB* and *domC* (it is important that boundaries are not defined on the matching edges of the domains ; notice that the interpreter **supprime\_bord** allows to remove a boundary from a domain see §2.3.32):

```

Mailler dom { Domain domA , Domain domB , Domain domC }

```

The object **Pave** is defined as follows:

```

Pave nom_pave
{
  Origine OX OY [OZ]
  Longueurs LX LY [LZ]
  Nombre_de_noeuds NX NY [NZ]
  Facteurs [FX] [FY] [FZ]
  [Symx] [Symy] [Symz]
  [Tanh value]
  [Tanh_dilatation value]
  [Tanh_taille_premiere_maille value]
}
{
  [contact nom_cote X= X0 Y0 <= Y <= Y1 [Z0 <= Z <= Z1]]
  [contact nom_cote Y= Y0 X0 <= X <= X1 [Z0 <= Z <= Z1]]
  [contact nom_cote Z= Z0 X0 <= X <= X1 [Y0 <= Y <= Y1]]
}

```

**Origine:** Keyword to define the pavé (block) origin, that is to say one of the 8 block points (or 4 in a 2D system).

*OX:* X co-ordinates

*OY:* Y co-ordinates

*OZ:* Z co-ordinates

**Longueurs:** Keyword to define the block dimensions, that is to say knowing the origin, length along the axes.

*LX:* Length along X

*LY:* Length along Y

*LZ:* Length along Z

**Facteurs:** Keyword to define stretching factors for mesh discretization in each direction. This is a real number which must be positive (by default 1.0).

*FX:* Stretch factor along X

*FY:* Stretch factor along Y

*FZ:* Stretch factor along Z



### Application to cylindrical co-ordinates:

The same **Pave** (block) object is applied to cylindrical co-ordinates (and the same keywords)

**X = , Y = , Z = )** by means of two restrictions:

X must always correspond to R, and Y to  $\theta$ .

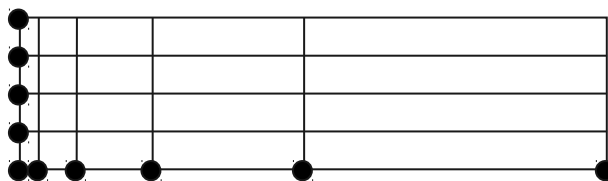
The values entered into the block for lengths in  $\theta$  or co-ordinates in  $\theta$  must correspond to real values given in radians divided by  $2\pi$  ( so in number of turns).

For example:

### **Facteurs 1.2 1.0**

The mesh size in the X direction increases by a factor of 1.2. In Y, the mesh will be regular.

The design hereunder illustrates the example of a block where **NX=6** and **NY=5**:



A stretching factor other than 1 allows refinement on one edge in one direction. To achieve refinement along the two edges of the block in one direction, the following keywords may be used:

**Symx:** Keyword to define a block mesh that is symmetrical with respect to the YZ plane (respectively straight Y in 2D) passing through the block centre.

**Symy:** Keyword to define a block mesh that is symmetrical with respect to the XZ plane (respectively straight X in 2D) passing through the block centre.

**Symz:** Keyword defining a block mesh that is symmetrical with respect to the XY plane passing through the block centre.

**Tanh:** Keyword to generate mesh with tanh (hyperbolic tangent) variation.

**Tanh\_dilatation** New keyword to generate mesh with tanh (hyperbolic tangent) variation.

tanh\_dilatation: The value may be -1,0,1 (0 by default):

0: coarse mesh at the middle of the channel and smaller near the walls

1: coarse mesh at the bottom of the channel and smaller near the top

-1: coarse mesh at the top of the channel and smaller near the bottom

**Tanh\_taille\_premiere\_maille** New keyword to generate mesh with tanh (hyperbolic tangent) variation in the Y direction.

tanh\_taille\_premiere\_maille: size of the first cell of the mesh.

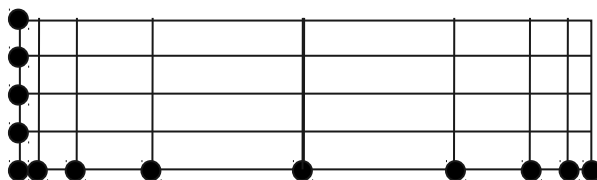
*Example:*

Pave Cavite

```
{
  Origine 0. 0. 0.
  Nombre_de_Noeuds 10 65 10
  Longueurs 6.283185307 2.0 3.141592653
  tanh_dilatation 0
  tanh_taille_premiere_maille 0.01
}
```

Example:

The same block as previously described, where **NX=9** and the keyword **Symx** is selected.



*contact*: Keyword indicating the block side type. This could be **Bord** to indicate that the block side is not in contact with another block and that limitation conditions will be applied to it, **Raccord Local Homogene (Connector)** to indicate (each of theses 3 keywords are separated by a space) that the block side is in contact with the block of another domain (case of two coupled problems), **Internes (Internal)** to indicate that the block has a set of internal faces (these faces will be duplicated automatically by the program and will be processed in a manner

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similar to edge faces). Two boundaries with the same limitation conditions may be given the same name (whether or not they belong to the same block).

The keyword **Internes (Internal)** must be used to execute a calculation with plates, followed by the equation of the surface area covered by the plates.

Block sides that are neither edges nor connectors are not specified. The duplicate nodes of two blocks in contact are automatically recognised and deleted.

*nom\_cote*: name of the block side.

*X0 Y0 Z0 X1 Y1 Z1*: block side co-ordinates. *Note spaces between the coordinate values and the keywords = and <=.*

Example (notice the comma between the description of each block **pave**):

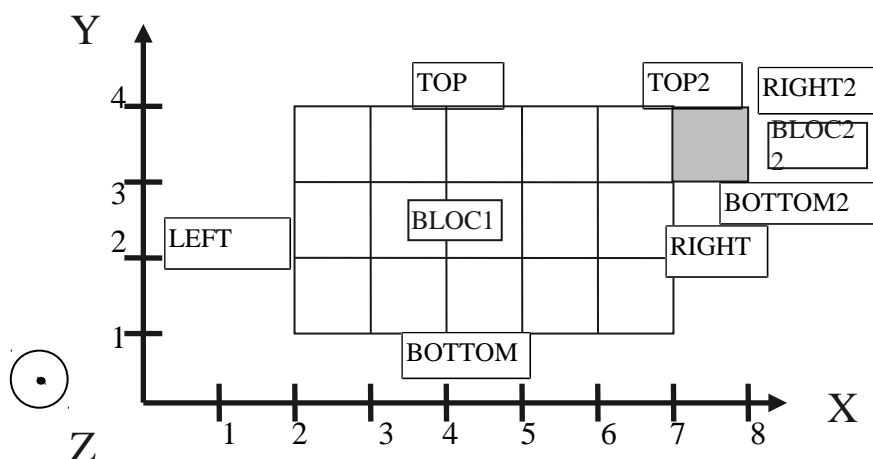
```
pave BLOC1
{
    origine 2 1
    nombre_de_noeuds 6 4
    longueurs 5.0 3.0
}
{
    bord TOP Y = 4 2 <= X <= 7
    bord BOTTOM Y = 1 2 <= X <= 7
    bord LEFT X = 2 1 <= Y <= 4
    bord RIGHT X = 7 1 <= Y <= 3
},
pave BLOC2
{
    origine 7 3
    nombre_de_noeuds 2 2
    longueurs 1.0 1.0
}
{
```

```

bord RIGHT2 X = 8 3 <= Y <= 4
bord TOP2 Y = 4 7 <= X <= 8
bord BOTTOM2 Y = 3 7 <= X <= 8
}

```

2 meshed blocks will be produced with this method (note the XYZ trihedral orientation in TRIO-U):



*Observations:* The side shared by BLOCK1 and BLOCK2 will be detected but will not be specified in the definition of the two blocks.

### 2.3.6 MAILLERPARALLEL(PARALLEL MESH)

**MaillerParallel** creates a parallel distributed hexaedral mesh of a parallelepipedic box. It is equivalent to creating a mesh with a single Pave, splitting it with “partition” and reloading it in parallel with “Scatter”. **MaillerParallel** only works in 3D at this time. It can also be used for a sequential computation (with all NPARTS=1)

```

MaillerParallel {
  domain      domaine_name
  nb_nodes    dimension  nX nY nZ
  splitting    dimension  npartsX npartsY npartsZ
  ghost_thickness  nghost
  [ perio_x ]
  [ perio_y ]
  [ perio_z ]
  [ function_coord_x  funcX | file_coord_x  fileX ]
  [ function_coord_y  funcY | file_coord_y  fileY ]
  [ function_coord_z  funcZ | file_coord_z  fileZ ]
  [ boundary_xmin  name_Xmin ]
  [ boundary_xmax  name_Xmax ]
  [ boundary_ymin  name_Ymin ]
  [ boundary_ymax  name_Ymax ]
  [ boundary_zmin  name_Zmin ]
  [ boundary_zmax  name_Zmax ]
}

```

**domain** : the name of the domain to mesh (it must be an empty domain object).

**nb\_nodes** : dimension defines the spatial dimension (currently only dimension=3 is supported), and nX, nY and nZ defines the total number of nodes in the mesh in each direction.

**splitting** : dimension is the spatial dimension and npartsX, npartsY and npartsZ are the number of parts created. The product of the number of parts must be equal to the number of cpus used for the computation.

**ghost\_thickness** : nghost is the number of ghost cells (equivalent to the epaisseur\_joint parameter of partition).

**perio\_x**, **perio\_y** and **perio\_z** : change the splitting method to provide a valid mesh for periodic boundary conditions.

**function\_coord\_x|y|z** : By default, the meshing algorithm creates nX|nY|nZ coordinates ranging between 0 and 1 (eg a unity size box). If **function\_coord\_x|y|z** is specified, it is used to transform the [0,1] segment to the coordinates of the nodes. funcX must be a function of the x variable only, funcY of y and funcZ of z.

For example:

**function\_coord\_y** (y-1)\*2

will create a box with a uniform mesh over [-1,1] in the y coordinates.

**file\_coord\_x|y|z** : is specified to read in fileX|Y|Z the nX|nY|nZ floating point values used as nodes coordinates.

**boundary\_xmin** : the name of the boundary at the minimum X direction. If it not provided, the default boundary names are xmin, xmax, ymin, ymax, zmin and zmax. If the mesh is periodic in a given direction, only the MIN boundary name is used, for both sides of the box.

### 2.3.7 REMOVE\_ELEM

**Remove\_elem** domain\_name { **liste** integer elem0 elem1 elem2 ... }

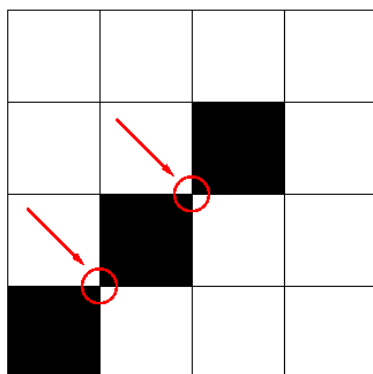
**Remove\_elem** domain\_name { **fonction** condition }

Keyword to remove element from a VDF mesh (named domaine\_name), either from an explicit list of elements or from a geometric condition defined by a condition  $f(x,y)>0$  in 2D and  $f(x,y,z)>0$  in 3D. All the new borders generated are gathered in one boundary called : newBord (to rename it, use **RegroupeBord** keyword. To split it to different boundaries, use **DecoupeBord\_Pour\_Rayonnement** keyword). Example of a removed zone of radius 0.2 centered at  $(x,y)=(0.5,0.5)$ :

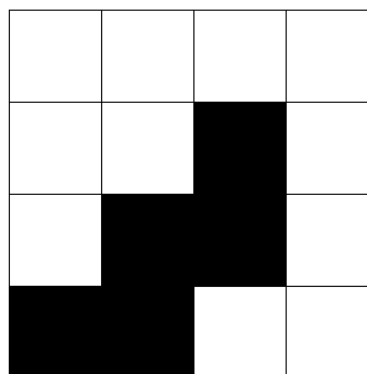
**Remove\_elem** dom { **fonction**  $0.2*0.2-(x-0.5)^2-(y-0.5)^2>0$  }

Warning : the thickness of removed zone has to be large enough to avoid singular nodes as deccribed below :

UNCORRECT – 2 SINGULAR NODES



CORRECT



### 2.3.8 REORDONNER(REORDER)

The **Reordonner** interpreter is required sometimes for a VDF mesh which is not produced by the internal mesher.

Example where this is used:

Read \_file *dom* fichier.geom

Reordonner *dom*

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Observations:

This keyword is redundant when the mesh that is read is correctly sequenced in the Trio\_U sense. This significant mesh operation may take some time...

The message returned by Trio\_U is not explicit when the Reordonner (Resequencing) keyword is required but not included in the data set...

### 2.3.9 CORRIGER\_FRONTIERE\_PERIODIQUE

The **Corriger\_frontiere\_periodique** keyword is mandatory to first define the periodic boundaries, to reorder the faces and eventually fix unaligned nodes of these boundaries. Faces on one side of the periodic domain are put first, then the faces on the opposite side, in the same order. It must be run in sequential before mesh splitting.

```
Corriger_frontiere_periodique {
    domaine domain_name
    bord boundary_name
    [ direction 2|3 dx dy [dz] ]
    [ fichier_post filename ]
}
```

**domaine:** domain\_name is the name of the domain

**bord:** boundary\_name is the name of the boundary (which must contain two opposite sides of the domain)

**direction:** dx dy dz defines the periodicity direction vector (a vector that points from one node on one side to the opposite node on the other side. This vector must be given if the automatic algorithm fails, that is:

- when the node coordinates are not perfectly periodic
- when the periodic direction is not aligned with the normal vector of the boundary faces

**Corriger\_frontiere\_periodique** replaces and improves the **Reordonner\_faces\_periodique** keyword which becomes obsolete and is kept for backward compatibility:

**Reordonner\_faces\_periodiques** DOM BORD

Is a shortcut to:

**Corriger\_frontiere\_periodique** { domaine DOM bord BORD }

### 2.3.10 TRIANGULATE





### 2.3.11 TETRAHEDRALISE

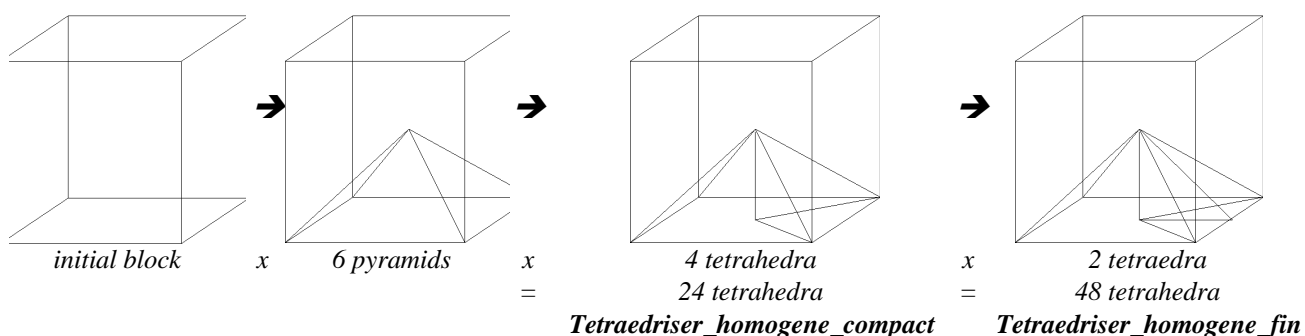
**Tetraedriser\_homogene\_fin** is the recommended option to tetrahedralise blocks.

**Tetraedriser\_homogene\_fin** nom\_domaine

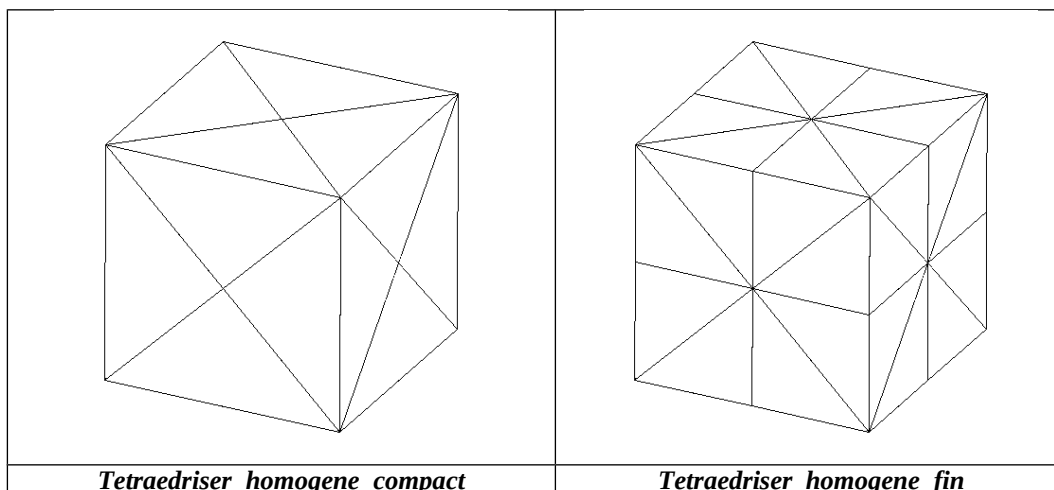
**Tetraedriser\_homogene\_fin** : As an extension (subdivision) of **Tetraedriser\_homogene\_compact** option, this last one cut each initial block in 48 tetrahedra (against 24, previously). This cutting ensures :

- a correct cutting in the corners (in respect to pressure discretization PreP1B).
- a better isotropy of elements than with **Tetraedriser\_homogene\_compact option**.
- a better alignment of summits (this could have a benefit effect on calculation near walls since first elements in contact with it are all contained in the same constant thickness and ii/ by the way, a 3D cartesian grid based on summits can be engendered and used to realise spectral analysis in HIT for instance).

Principle : initial block is divided in 6 pyramids, each of these being cut in 4 (**Tetraedriser\_homogene\_compact**), then 2 tetrahedra (**Tetraedriser\_homogene\_fin**).



Remark : **Tetraedriser\_homogene\_fin** (**Tetraedriser\_homogene\_compact**, respectively) is equivalent in 2D to **Trianguler\_fin** (**Trianguler\_h**).



**Tetraedriser\_homogene\_compact** nom\_domaine

**Tetraedriser\_homogene\_compact** : This keyword generates tetrahedral elements from cartesian or **non-cartesian** hexahedral elements. The process cut each hexahedral in 6 pyramids, each of them being cut then in 4 tetrahedral. So, in comparison with tetra\_homogene, less elements (\*24 instead of \*40) with more homogeneous volumes are generated. Moreover, this process is done in a faster way.

**Tetraedriser\_homogene** nom\_domaine

Use the **Tetraedriser\_homogene** interpreter in VEF discretization to mesh a block in tetrahedra. Each block hexahedral is no longer divided into 5 tetrahedra (keyword **Tetraedriser (Tetrahedralise)**), it is now broken down into 40 tetrahedra. Thus a block defined with 11 nodes in each X, Y, Z direction will contain  $10*10*10*40=40,000$  tetrahedra. This also allows problems in the mesh corners with the P1NC/P1iso/P1bulle or P1/P1 discretization items to be avoided.

**Tetraedriser\_par\_prisme** nom\_domaine

**Tetraedriser\_par\_prisme**: This keyword generates 6 iso-volume tetrahedral element from primary hexahedral one (contrarily to the 5 elements ordinarily generated by tetraedriser). This element is suitable for calculation of gradients at the summit (coincident with the gravity centre of the jointed elements related with) and spectra (due to a better alignment of the points).

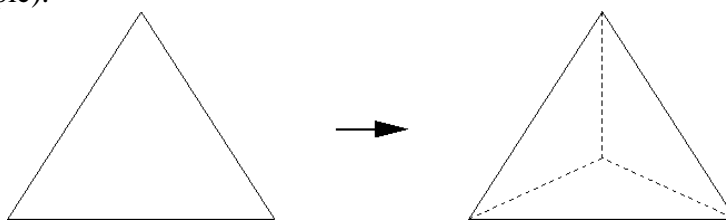
**Tetraedriser** nom\_domaine

To achieve a tetrahedral mesh based on a mesh comprising blocks, the **Tetraedridal** (**Tetrahedralise**) interpreter is used in VEF discretization.

### 2.3.12REFINE

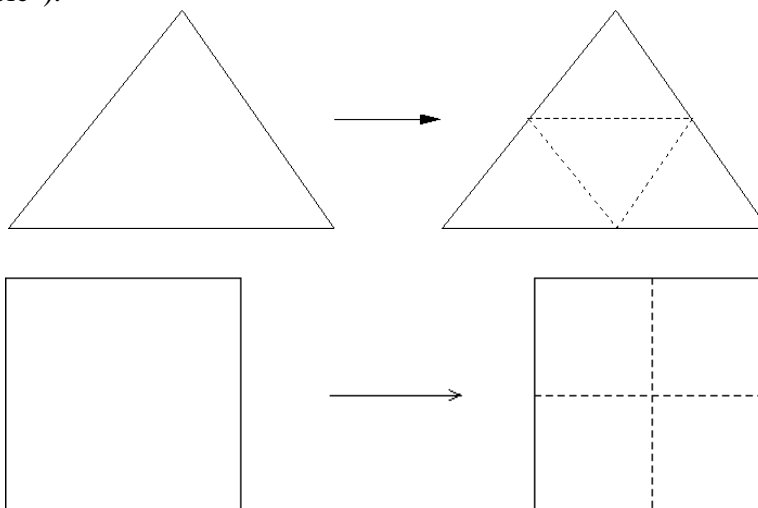
**Raffiner\_anisotrope** domain\_name

Keyword to allows to cut triangle or tetrahedra elements respectively in 3 or 4 new ones by defining a new summit located at the center of the element. Note that such a cut creates flat elements (anisotropic).



**Raffiner\_isotrope** domain\_name

Keyword to allows to cut triangles/quadrangles or tetrahedral/hexaedras elements respectively in 4 or 8 new ones by defining new summits located at the middle of edges (and center of faces and elements for quadrangles and hexaedra). Such a cut preserves the shape of original elements ("isotropic").



### 2.3.13EXTRUDE

```
Extruder { domaine domain_name nb_tranches n direction lx ly lz }
```

**Extruder:** Keyword to create a 3D tetrahedral/hexahedral mesh (a prism is cut in 14) from a 2D triangular/quadrangular mesh named domain\_name with an extrude operation of n points in the direction (lx,ly,lz).

```
Extruder_en3 { domaine N domain_name1 domaine_name2 ... domaine_nameN nb_tranches n
direction lx ly lz [nom_cl_devant boundary_name_1] [nom_cl_derriere boundary_name_2] }
```

**Extruder\_en3:** Keyword to create a 3D tetrahedral/hexahedral mesh (a prism is cut in 3) from a 2D triangular/quadrangular mesh named domain\_name with an extrude operation of n points in the direction (lx,ly,lz). The names of the (by default, “devant” and “derriere”) may be renamed by the keyword **nom\_cl\_devant** and **nom\_cl\_derriere**. If NULL is written for *boundary\_name*, then no boundary condition is generated at this place.

Recommendation : to ensure conformity between meshes (in case of fluid/solid coupling) it is recommended to extrude all the domains at the same time.

```
Extruder_en20 { domaine domain_name nb_tranches n direction lx ly lz }
```

**Extruder\_en20:** It does the same task as **Extruder** except a prism is cut in 20 instead of 3. Options **nom\_cl\_devant** and **nom\_cl\_derriere** are not available so the default name for the boudaries will be “devant” and “derriere”. But you can change this name with the keyword **RegroupeBord**:

```
Extruder_en20 { domaine domaine_name ... }
```

```
RegroupeBord domaine_name new_name_devant { devant }
```

```
RegroupeBord domaine_name new_name_derriere { derriere }
```

```
ExtrudeBord { domaine_init name_domain1 direction x y z
domaine_final name_domain2 nom_bord name_boundary
nb_tranches n [hexa_old] [trois_tetra] }
```

**ExtrudeBord** : Keyword dedicated to generate an extruded mesh from a boundary of a tetrahedral or an hexahedral mesh (Note that ExtrudeBord in VEF generates 3 or 14 tetrahedra from extruded prisms).

**domaine\_init** name\_domain1 : Initial domain with hexaedras or tetrahedras.

**direction** x y z : Directions for the extrusion.

**domaine\_final** name\_domain2 : Extruded domain.

**nom\_bord** name\_boundary : Name of the boundary of the initial domain where extrusion will be applied.

**nb\_tranches** n : Number of elements in the extrusion direction.

**hexa\_old**: Old algorithm for boundary extrusion from a hexahedral mesh

**trois\_tetra** : Optional keyword to generates 3 tetrahedras instead of 14 by default, from extruded prims

As **Extruder** keyword, il will create boundaries named “devant” and “derriere”. If you want to create a periodic boundary named *perio*, use after the **RegroupeBord** keyword:

**RegroupeBord** name\_domain2 *perio* { devant derriere }

This keyword can be used for example to create a periodic box extracted from a boundary of a tetrahedral or a hexahedral mesh. This periodic box may be used then to engender turbulent inlet flow condition for the main domain (see Champ\_front\_calc\_recycl\_fluct\_pbperio)

In the example given below, DFLUI is the main (Hexaedra) domain and BOXPERIO is the periodic box engendered from face ENTCH of DFLUI. Extracted domain is according to the vector (-200,0.,0.) and contains 10 hexaedra in this direction:

**Domaine** DFLUI

**Domaine** BOXPERIO

**Read\_file** DFLUI trio\_DFLUI\_geo.asc

**ExtrudeBord** { **domaine\_init** DFLUI **direction** -200. 0. 0.

**domaine\_final** BOXPERIO **nom\_bord** ENTCH

**nb\_tranches** 10 }

**RegroupeBord** BOXPERIO *perio* { devant derriere }

**Ecrire\_fichier** BOXPERIO BOXPERIO.geom

```
ExtrudeParoi { domaine name_dom nom_bord name_boundary
               [ epaisseur n r1 r2 .... rn ]
               [ critere_absolu 0|1 ]
               [ projection_normale_bord bool ] }
```

**ExtrudeParoi** : Keyword dedicated in 3D (VEF) to create prismatic layer at wall. Each prism is cut in 3 tetraedra.

**domaine** name\_dom : initial domain.

**nom\_bord** name\_boundary : Name of the (no slide) boundary for creation of prismatic layers.

**epaisseur** n r1 r2 .... rn : (relative or absolute) width for each layer.

**critere\_absolu** 0|1 : relative (0, the default) or absolute (1) width for each layer.

**projection\_normale\_bord** bool : keyword to project layers on the same plane that contiguous boundaries.  
default values are : **epaisseur\_relative** 1 **0.5** **projection\_normale\_bord** 1

### 2.3.14 CREATE\_DOMAIN\_FROM\_SOUS\_ZONE

```
Create_domain_from_sous_zone {
    domaine_final domain1
    par_sous_zone name
    domaine_init domain2 }
```

These keyword fills the domain *domain1* with the subzone *name* from the domain *domain2*. It is very useful when meshing several mediums with **Gmsh**. Each medium will be defined as a subzone into **Gmsh**. A MED mesh file will be saved from **Gmsh** and read with **Lire\_Med** keyword by the Trio\_U data file. And with this keyword, a domain will be created for each medium in the Trio\_U data file.

### 2.3.15 EXTRACT\_2D\_FROM\_3D

```
Extract_2D[axi]_from_3D 3D_domaine_name 3D_boundary_name 2D_domaine_name
```

**Extract\_2D\_from\_3D** : Keyword to extract a 2D mesh by selecting a boundary of the 3D mesh. To generate a 2D axisymmetric mesh prefer **Extract\_2Daxi\_from\_3D** keyword

*3D\_domaine\_name* : Domain name of the 3D mesh

*3D\_boundary\_name* : Boundary name. This boundary become the new 2D mesh and all the boundaries, in 3D, attached to the selected boundary, give their name to the new boundaries, in 2D.

*2D\_domaine\_name* : Domain name of the new 2D mesh

### 2.3.16 REORIENTER\_TETRAEDRES

```
Reorienter_tetraedres name_domain
```

This keyword is mandatory for front-tracking computations with the VEF discretisation. For each tetrahedral element of the domain, it checks if it has a positive volume. If the volume (determinant of the three vectors) is negative, it swaps two nodes to reverse the orientation of this tetrahedron.

### 2.3.17 CLEAN MESHES

**NettoiePasNoeuds** *name\_domain*

Keyword **NettoiePasNoeuds** does not delete useless nodes (nodes without elements) from a domain. Keyword **NettoieNoeuds** (suppressed useless nodes) is obsolete since v1.4.6 version cause it is done by default now.

### 2.3.18 ANALYSE\_ANGLE

**Analyse\_angle** *name\_domain* *nb\_histo*

Keyword **Analyse\_angle** prints the histogram of the largest angle of each mesh elements of the domain named *name\_domain*. *nb\_histo* is the histogram number of bins. It is called by default during the domain discretization with *nb\_histo* set to 18. Useful to check the number of elements with angles above 90°.

### 2.3.19 VERIFIERCOIN

**VerifierCoin** *name\_domain* { [**Read\_file** *file.decoupage\_som*] [expert\_only] }

Keyword **VerifierCoin** subdivides inconsistent 2D/3D cells used with VEFPreP1B discretization. Must be used before the mesh is discretized.

The **Read\_file** option can be used only if the *file.decoupage\_som* was previously created by Trio\_U. This option, only in 2D, reverses the common face at two cells (at least one is inconsistent), through the nodes opposed. In 3D, the option has no effect.

The **expert\_only** option deactivates, into the VEFPreP1B divergence operator, the test of inconsistent cells.

### 2.3.20 PRINT MOMENTS ON BOUNDARIES

**Calculer\_moments** nom\_domaine **calcul**  
**Calculer\_moments** nom\_domaine **centre\_de\_gravite** x y [z]

This keyword allows Trio\_U to calculate and print the torque (moment of force) exerted by the fluid on each boundaries in output files (.out) of the domain nom\_domaine. You can either use the keyword **calcul** and the centre of gravity will be calculated or specify a specific centre with **centre\_de\_gravite** keyword.

### 2.3.21 PRINT FLUX PER FACES

**Imprimer\_flux** nom\_domaine { *Bord1 Bord2 ...* }

This keyword allows the flux per face at the boundaries named *Bord1*, *Bord2* of a domain to be printed. The flux are written into the .face files at a frequency defined by **dt\_impr**, the evaluation printing frequency (refer to time scheme keywords). By default, flux are incorporated onto the edges before being displayed.

### 2.3.22 PRINT FLUX PER BOUNDARY

**Imprimer\_flux\_sum** nom\_domaine { *Bord1 Bord2 ...* }

This keyword allows the sum of the flux per face at the boundaries named *Bord1*, *Bord2* of a domain defined by the user in the data set to be printed. The flux are written into the .out files at a frequency defined by **dt\_impr**, the evaluation printing frequency (refer to time scheme keywords).



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### 2.3.23 GATHER BOUNDARIES

```
Regroupebord domaine new_name_bord { Boundary1 Boundary2 Boundary3 ... }
```

Keyword to build one boundary *new\_name\_bord* with several boundaries of the domain named *domaine*.

### 2.3.24 CONVERT BOUNDARIES

```
modif_bord_to_raccord domain_name boundary_name
```

Keyword to convert a boundary of *domain\_name* domain of kind **Bord** to a boundary of kind **Raccord** (named *boundary\_name*). It is useful when using meshes with boundaries of kind **Bord** defined and to run a coupled calculation.

### 2.3.25 SUPPRESS INTERNAL BOUNDARIES

```
Remove_Invalid_Internal_Boundaries domain_name
```

Keyword to suppress an internal boundary of the *domain\_name* domain. Indeed, some mesh tools may define internal boundaries (eg: for post processing task after the calculation) but Trio\_U does not support it yet.

### 2.3.26 DEFINING SUB-AREAS

```

Sous_Zone nom_sous_zone
Associate nom_sous_zone nom_domaine
Read nom_sous_zone {
    bloc_lecture_sous_zone
    [ restriction nom_sous_zone2 ]
    [ union nom_sous_zone3 ]
}

```

**Sous\_Zone (Sub-area)** is an object type describing a domain sub-set.

*nom\_sous\_zone*: **Sous\_Zone (Sub-area)** type object identifier. This is the identifier that must be used to reference the created object type elsewhere in the data set.

A **Sous\_Zone (Sub-area)** type object must be associated with a **Domaine** type object. The **Read** interpreter is used to define the items comprising the sub-area.

**Caution:** The **Domain** type object *nom\_domaine* must have been meshed (and triangulated or tetrahedralised in VEF) prior to carrying out the **Associate** *nom\_sous\_zone nom\_domaine* instruction; this instruction must always be preceded by the read instruction.

**Restriction :** The elements of the sub-area *nom\_sous\_zone* must be included into the other sub-area named *nom\_sous\_zone2*. This keyword should be used first in the **Read** keyword.

**Union :** The elements of the sub-area *nom\_sous\_zone3* will be added to the sub-area *nom\_sous\_zone*. This keyword should be used last in the **Read** keyword.

*bloc\_lecture\_sous\_zone*: one of the following blocks:

**Fonction\_sous\_zone** *function(x,y,z)* : Keyword to build a sub-area with the the elements included into the area defined by *function(x,y,z)>0*. See 2.4.5 how to write a function.

**Rectangle Origine** *x0 y0* **Cotes** *lx ly*

**Boite Origine** *x0 y0 z0* **Cotes** *lx ly lz*

The sub-area will include all the domain elements whose centre of gravity is within the Rectangle in 2D (resp. the Box in 3D).

**Liste** *n n°1 n°i n°n*

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The sub-area will include n domain items, numbers No. 1 No. i No. n.

**fichier** *filename*

The sub-area is read into the file *filename*.

**Intervalle** n1 n2

The sub-area will include domain items whose number is between n1 and n2 (where  $n1 \leq n2$ ).

**Polynomes** { bloc\_lecture\_poly\_1 et bloc\_lecture\_poly\_i et bloc\_lecture\_poly\_n }

Consider the surface area (or volume if referring to a 3D situation) obtained by surface intersection (or volume) defined by  $\text{poly}_1 \Rightarrow 0$  , ,  $\text{poly}_i \Rightarrow 0$  ,  $\text{poly}_n \Rightarrow 0$ . The sub-area will include domain items whose centre of gravity is located within this surface area (or this volume).

*Example:*

Read zone1

```
{
    Polynomes { 2 2 1 2 -0.33 1. et 2 2 1 2 0.66 -1. et 2 1 2 2 0. 1. et 2 1 2 2 1. -1. }
}
```

For:

$x - 0.33 > 0$

$0.66 - x > 0$

$y > 0$

$1 - y > 0$

The syntax to read a polynome is:

Polynome { dimension nx ny nx\*ny c00 c01 c02 ... c0(ny-1)( c10 c11 ... c1(ny-1) ... c(nx-1)0 ... }

For  $c00 + c01y + c02y^2 + \dots + c0(ny-1)y^{(ny-1)} + c10x + c11xy + \dots + c1(ny-1)xy^{(ny-1)} + \dots + c(nx-1)x^{(nx-1)} \dots$

**Couronne Origine** x y [z] **ri** double **re** double

To create a "couronne" in 2D. **Origine**: the center of the circle. **ri, re**: the interior and exterior radius.

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**Tube Origine** x y z **dir** axis **ri** double **re** double **hauteur** double

Keyword to create a tube in 3D where :

**Origine**: the center of the tube.

**dir**: direction of the main axis X, Y or Z

**hauteur**: the height of the tube

**Tube\_hexagonal entreplat** double [IN|OUT]

Keyword to create a hexagonal tube centered at (0,0,0) and with axis along Z.

## 2.3.27 DISCRETIZATION

A discretization object is created with the usual syntax.

```
type_discretization  dis
```

*type\_discretization*: there are several available discretizations:

**VDF** : finite difference volume discretization

**VEFPreP1B** : finite element volume discretization (*PINC/P1-bubble element*). Since the 1.5.5 version, several new discretizations are available thanks to the optional keyword **Read** :

```
VEFPreP1B  dis
Read  dis { [P0] [P1] [Pa]
            [Changement_de_base_P1Bulle 0|1]
            [Cl pression_sommet_faible 0|1]
            [Modif_div_face_dirichlet 0|1]
          }
```

**P0** : Pressure nodes are added on element centres

**P1** : Pressure nodes are added on vertices

**Pa** : Only available in 3D, pressure nodes are added on edges

**Changement\_de\_base\_P1Bulle** value : This option may be used to have the PINC/P0P1 formulation (value set to 0) or the PINC/P1Bulle formulation (value set to 1, the default).

**Cl pression\_sommet\_faible** value : This option is used to specify a strong formulation (value set to 0, the default) or a weak formulation (value set to 1) for an imposed pressure boundary

condition. The first formulation converges quicker and is stable in general cases. The second formulation should be used if there are several outlet boundaries with Neumann condition (see *Ecoulement\_Neumann* test case for example).

**Modif\_div\_face\_dirichlet** value : This option (by default 0) is used to extend control volumes for the momentum equation.

By default, if the **Read** keyword is not used, the VEFPreP1B keyword is equivalent to the former VEFPreP1B formulation (v1.5.4 and sooner). P0P1 (if used with the strong formulation for imposed pressure boundary) is equivalent to VEFPreP1B but the convergence is slower. So:

**VEFPreP1B** *dis*

Is equivalent to :

**VEFPreP1B** *dis*

**Read** *dis* { **P0 P1 Changement\_de\_base\_P1Bulle 1 Cl\_pression\_sommet\_faible 0** }

The discretization used before v1.6.0 version by the old keyword **VEF** is now available with:

**VEFPreP1B** *dis*

**Read** *dis* { **P0** }

Cell shape	Rectangle	Rectangle	Triangle	Qaudrangle	Block	Block	Tetrahedron	Hexahedron
Coordinates	(x,y)	(r,z)	(x,y)	(x,y)	(x,y,z)	(r,θ,z)	(x,y,z)	(x,y,z)
VDF	OK	OK			OK	OK		
VEFPreP1B			OK				OK	

OK<sup>(\*)</sup> means : OK on regular mesh only.

**dis**: the name of the created object.

A **Probleme (Problem)** object may be discretised according to a **VDF** or **VEF** discretization using the **Discretize** interpreter.

**Discretize** pb *dis*

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The problem, *pb*, is discretised according to the *dis* discretization.

**IMPORTANT:** A number of objects must be already associated (a domain, time scheme, central object) prior to invoking the **Discretize** keyword. The physical properties of this central object must also have been read.

**Discretiser\_domaine** dom

This keyword **Discretiser\_domaine** is useful to discretize the domain dom (faces will be created) without defining a problem.

### 2.3.28 ALLOCATE POROSITY

Two types of porosity, volume or surface, may be defined, the first corrects the surface of the passage offered to the fluid following a direction, the second effects the mesh volume in question.

surface porosity = (fluid surface)/(total mesh surface)

volume porosity = (fluid volume)/(total mesh volume)

The porosity can also be defined as a field. The porosity is given at each element and the porosity at each face,  $\Psi(\text{face})$ , is calculated by the average of the porosities of the two neighbour elements  $\Psi(\text{elem1})$ ,  $\Psi(\text{elem2})$  :  $\Psi(\text{face}) = 2 / (1/\Psi(\text{elem1}) + 1/\Psi(\text{elem2}))$ .

**Porosites\_champ** *nom\_pb* *field* *field\_definition*

*nom\_pb*: name of the problem

*domaine*: name of the domain

*field*: field used to define the porosity field (**champ\_fonc\_xyz**, **champ\_uniforme**, **champ\_uniforme\_morceaux**,...)

The volume porosity and surface porosity that are uniform in every direction in space on a sub-area may be defined using the **Porosites** keyword:

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```
Porosites nom_pb nom_sous_zone { [ volumique val_poro_vol ]
[ surfamique 2|3 val_poro_surf_X val_poro_surf_Y [ val_poro_surf_Z ] ] }
```

*nom\_sous\_zone*: name of the sub-area to which porosity are allocated.

*nom\_pb*: name of the problem to which the sub-area is attached.

*val\_poro\_vol*: volume porosity value.

*val\_poro\_surf\_X*: surface porosity value in the X direction.

*val\_poro\_surf\_Y*: surface porosity value in the Y direction.

*val\_poro\_surf\_Z*: surface porosity value in the Z direction.

#### **Observations:**

- Surface porosity values must be given in every direction in space (set this value to 1 if there is no porosity).
- Prior to defining porosity, the problem must have been discretized.
- Can't be used in VEF discretization, use **Porosites\_champ** instead.

### **2.3.29PRECISIONGEOM**

Keyword to change the way floating-point number comparison is done. By default, two numbers are the same if their absolute difference is less than 1e-10. The keyword is useful to change this value:

```
PrecisionGeom new_value
```

Moreover, nodes coordinates will be written in .geom files with this same precision.

### **2.3.30DILATE**

Keyword to multiply the whole coordinates of the geometry.

```
Dilate domain_name value_of_dilatation_coefficient
```

*Example:*

Read\_file dom trio\_DOM\_geo\_33.asc

**Dilate** dom 0.001

### 2.3.31 DECOUPEBORD\_POUR\_RAYONNEMENT

Keyword to subdivide the external boundary of a domain in several parts (may be useful for better accuracy when using radiation model in transparent medium).

```
DecoupeBord_pour_rayonnement {
  domaine fine_domain_name
  bords_a_decouper N boundary_name1 boundary_name2 ... boundary_nameN
  [ domaine_grossier coarse_domain_name
    | nb_parts_naif N n1 n2 ... nN
    | nb_parts_geom N n1*m1 n2*m2 ... nN*mM
    | condition_geometrique N formulae1 formulae2 ... formulaeN ]
  ]
  [nom_fichier_sortie filename [ binaire ]]
}
```

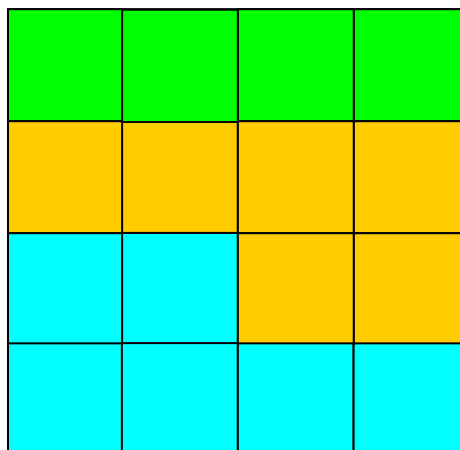
**bords\_a\_decouper** is the keyword to specify the boundaries of the *fine\_domain\_name* domain to be splitted. These boundaries will be cut according the coarse mesh defined by:

-either the keyword **domaine\_grossier** (each boundary face of the coarse mesh *coarse\_domain\_name* will be used to group boundary faces of the fine mesh to define a new boundary). Notice that the *coarse\_domain\_name* domain should have the same boundaries name of the *fine\_domain\_name* domain.

-either by the keyword **nb\_parts\_naif** (each *l*th boundary is splitted into *nI* parts)

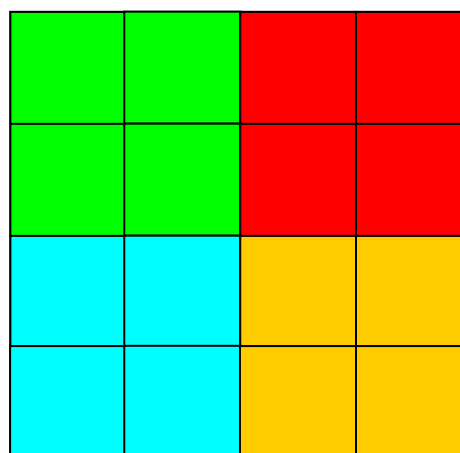
Example: **nb\_parts\_naif** 1 3





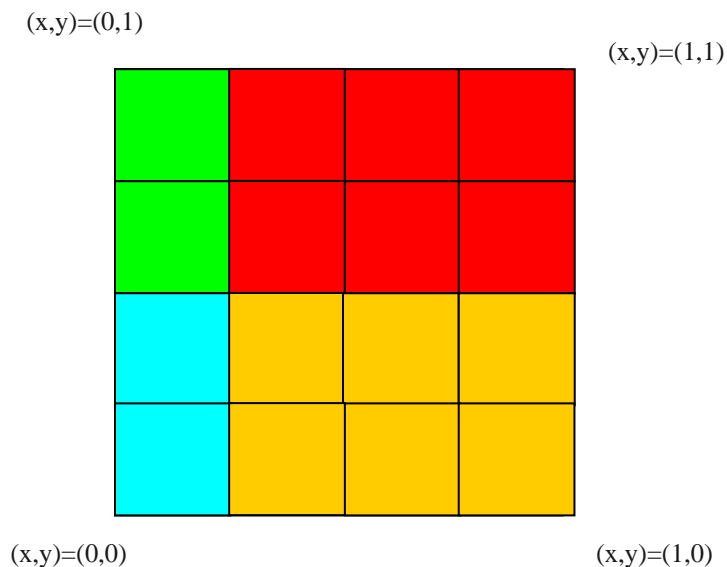
-either by the keyword **nb\_parts\_geom** (each lth boundary is splitted into nI\*mI parts). This keyword is only available for the VDF discretization.

Example: **nb\_parts\_geom** 2 2 2



-either by geometric conditions given by formulaes for each boundary with the keyword **condition\_geometrique**

Example: **condition\_geometrique** 1 (x>0.25)+2\*(y>0.5)



A mesh file (ASCII format, except if **binaire** option is specified) named by default *fine\_domain\_name.newgeom* (or specified by the **nom\_fichier\_sortie** keyword) will be created and will contain the *fine\_domain\_name* domain with the splitted boundaries named *boundary\_name%I* (where I is between from 0 and n-1). Furthermore, several files named *fine\_domain\_name.boundary\_name%I* and *fine\_domain\_name.boundary\_name\_xv* will be created, containing the definition of the subdivided boundaries. *fine\_domain\_name.newgeom* will be used to calculate view factors with **geom2ansys** script whereas only the *fine\_domain\_name.boundary\_name\_xv* files will be necessary for the radiation calculation. The file *fine\_domain\_name.boundary\_list* will contain the list of the boundaries *boundary\_name%I*.

### 2.3.32SUPPRIME\_BORD

```
Supprime_bord domain_name { Boundary_name1 Boundary_name2 ... }
```

Keyword to remove boundaries (named *Boundary\_name1 Boundary\_name2 ...*) of the domain named *domain\_name*.

### 2.3.33ORIENTEFACESBORD

**OrienteFacesBord** *domain\_name*

Keyword to modify the order of the boundary verteces included in a domain, such that the surface normals are outer pointing.

### 2.3.34 TRANSFORMER

Keyword to transform the coordinates of the geometry :

**Transformer** *domain\_name function\_for\_x function\_for\_y [ function\_for\_z ]*

*Example to rotate your mesh by a 90° rotation and to scale the z coordinates by a factor 2:*

Read\_file dom trio\_DOM\_geo\_33.asc

**Transformer** dom -y -x 2\*z

### 2.3.35 ROTATION

Keyword to rotate the geometry of an arbitrary angle around an axis aligned with Ox, Oy or Oz axis :

**Rotation** *domain\_name axis coord0 coord1 angle*

*domain\_name* : name of the domain to wich the transformation is applied

*axis* : X, Y or Z to indicate the direction of the rotation axis

*corrd0, coord1*: coordinates of the center of rotation in the plane orthogonal to the rotation axis.

These coordinates must be specified in the direct triad sense.

*angle* : angle of rotation (in degrees)

### 2.3.36 SOLVE

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**Solve** name\_problem

Interpreter to start calculation with Trio\_U. The problem name\_problem is solved.

### 2.3.37CONVERSION

**Lata\_To\_Other** format *file1 file2*

Interpreter to convert results file named *file1* written with LATA format to a file named *file2* with MED or LML format.

format: MED or LML keyword.

**Warning:** Fields located to faces are not supported yet.

**Lata\_To\_MED** [format] *file1 file2*

Interpreter to convert results file named *file1* to a MED file named *file2*. A data file is also created to reconvert the MED file *file2* to another format specified by the optional given format.

**Warning:** Fields located to faces are not supported yet.

### 2.3.38EXECUTE\_PARALLEL

**Execute\_parallel** { **liste\_cas** N *datafile1 ... datafileN* [ **nb\_procs** N nb1 ... nbN ] }

**Execute\_parallel:** This keyword allows to run several computations in parallel on cpus allocated to Trio\_U. The set of cpus is split in N subsets and each subset will read and execute a different data file. *datafileX* the name of a Trio\_U data file without the .data extension. **nb\_procs** is the number of cpus needed to run each data file. If not given, Trio\_U assumes that computations are sequential. Error messages usually written to stderr and stdout are redirected to .log files (journaling must be activated).

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### 2.3.39 MOYENNE\_VOLUMIQUE

```

Moyenne_volumique { Nom_pb source_problem_name
  Noms_champs N source_field1 source_field2 ... source_fieldN
  Nom_domaine destination_domain_name
  Fonction_filtre {
    type filter_type
    demie-largeur l
    [ omega w ]
    [ expression string ]
  }
  [ Localisation ELEM | SOM ]
  Nom_fichier_post destination_filename ]
  [ Format_post lata | lml ]
}

```

This keyword should be used after **Solve** keyword. It computes the convolution product of one or more fields with a given filtering function.

**Nom\_pb**: name of the problem where the source fields will be searched.

**Noms\_champs**: name of the source fields (these fields must be accessible from the **postraitement**)

**Nom\_domaine**: name of the destination domain (for example, it can be a coarser mesh, but for optimal performance in parallel, the domain should be split with the same algorithm as the computation mesh, eg, same **tranche** parameters for example)

**Fonction\_filter** is the keyword to specify the given filter:

**type** *filter\_type* : This parameter specifies the filtering function. Valid *filter\_type* are :

**Boite** is a box filter,  $f(x,y,z)=(abs(x)<l)*(abs(y)<l)*(abs(z)<l)/(8*l^3)$

**Chapeau** is a hat filter (product of hat filters in each direction) centered on the origin, the half-width of the filter being *l* and its integral being 1.

**Quadra** is a 2<sup>nd</sup> order filter

**Gaussienne** is a normalized gaussian filter of standard deviation *sigma* in each direction (all field elements outside a cubic box defined by *clipping\_half\_width* are ignored, hence, taking *clipping\_half\_width*=2.5\**sigma* yields an integral of 0.99 for a uniform unity field).

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**Parser** allows a user defined function of the x,y,z variables. All elements outside a cubic box defined by `clipping_half_width` are ignored. The parser is much slower than the equivalent c++ coded function...

**demie-largeur l** : This parameter specifies the half width of the filter

[ **omega w** ] : This parameter must be given for the gaussienne filter. It defines the standard deviation of the gaussian filter.

[ **expression** string] : This parameter must be given for the parser filter type. This expression will be interpreted by the math parser with the predefined variables "x", "y" and "z".

**Localisation ELEM | SOM** indicates where the convolution product should be computed: either on the elements or on the nodes of the destination domain.

**Nom\_fichier\_post**: indicates the filename where the result is written

**Format\_post**: gives the fileformat for the result (by default : lata)

Recommandations and details:

- the filter generates also a field called *porosite* which is the result of filtering a unity field.
- the filter handles any kind of source field by evaluating the field at the center of the elements (see `valeur_aux_elems()` function).
- filters with a large half-width are very slow (expect quite long computation time if the filter width is more than 20 mesh cells).
- when filtering cell centered data on a regular grid, the width of the filter will be an odd number of cells with **localisation ELEM** and an even number with **localisation SOM**.
- The filter computes for each given field the following expression: 
$$\hat{f}(x) = \sum_{i \in E} f(y_i) \cdot g(y_i - x) \cdot V(i)$$
 where E is the set of elements for which the center is inside the clipping box,  $y_i$  is the coordinate of the element center (the source field is always interpolated at the center of the elements whatever its native localization) and  $V(i)$  is the volume of the element. The result is computed for each coordinate x of the destination domain (elements or nodes depending on **localisation**).
- For the **boite** filter and with **localisation elem**, the filter width should not be an exact multiple of the size of the source mesh cells (otherwise the filter might produce unpredictable results for some elements).

### 2.3.40EXTRAIRE\_PLAN

```

Extraire_plan {
    Domaine domain_name
    Probleme pb_name
    Epaisseur float
    Origine 2|3 ox oy [oz]

```

```

Point1 2|3 x1 y1 [z1]
Point2 2|3 x2 y2 [z2]
[ Point3 2|3 x3 y3 [z3] | Triangle ]
[ via_extraire_surface
  [ inverse_condition_element ]
  [ avec_certains_bords_pour_extraire_surface n boundary1 ... boundary n ]
]
}

```

This keyword extract a plan mesh named *domain\_name* (this domain should have be declared before) from the mesh of the *pb\_name* problem. The plan can be either a triangle (defined by the keywords **Origine**, **Point1**, **Point2** and **Triangle**), either a regular quadrangle (with keywords **Origine**, **Point1** and **Point2**), or either a generalized quadrangle (with keywords **Origine**, **Point1**, **Point2**, **Point3**). The keyword **Epaisseur** specifies the thickness of volume around the plan which contains the faces of the extracted mesh. The keyword **via\_extraire\_surface** will create a plan and use **Extraire\_surface** algorithm. **Inverse\_condition\_element** keyword then will be used in the case where the plan is a boundary not well oriented, and **avec\_certains\_bords\_pour\_extraire\_surface** is the option related to the **Extraire\_surface** option named **avec\_certains\_bords**.

### 2.3.41EXTRAIRE\_SURFACE

```

Extraire_surface {
  Domaine domain_name
  Probleme pb_name
  Condition_elements  $f(x,y,z)$ 
  Condition_faces  $g(x,y,z)$ 
  [ avec_les_bords ]
  [ avec_certains_bords N name1 name2 ... nameN ]
}

```

This keyword extract a surface mesh named *domain\_name* (this domain should have be declared before) from the mesh of the *pb\_name* problem. The surface mesh is defined by one or two conditions. The first condition is about elements with **Condition\_elements**. For example:

**Condition\_elements**  $x*x+y*y+z*z<1$

Will define a surface mesh with external faces of the mesh elements inside the sphere of radius 1 located at (0,0,0). The second conditions **Condition\_faces** is useful to give a restriction.

By default, the faces from the boundaries are not added to the surface mesh excepted if option **avec\_les\_bords** is given (all the boundaries are added), or if the option **avec\_certains\_bords** is used to add only some boundaries.

### 2.3.42EXTRAIRE\_DOMAINE

```

Extraire_domaine {
    Domaine domain_name
    Probleme pb_name
    Condition_elements f(x,y,z)
}

```

**Extraire\_domaine** : Keyword to create a new new domain built with the domain elements of the *pb\_name* problem verifying the two conditions given by **Condition\_elements**. The problem *pb\_name* should have been discretized.

### 2.3.43INTEGRER\_CHAMP\_MED

```

Integrer_champ_MED {
    Champ_med MED_field
    Methode [ integrale_en_z|debit_total ]
    [zmin float zmax float nb_tranche integer Fichier_sortie output_filename]
}

```

This keyword is used to calculate a flow rate from a velocity MED field read before. The method is either **debit\_total** to calculate the flow rate on the whole surface, either **integrale\_en\_z** to calculate flow rates between  $z=z_{min}$  and  $z=z_{max}$  on **nb\_tranche** surfaces. The output file indicates first the flow rate for the whole surface and then lists for each tranche : the height  $z$ , the surface average value, the surface area and the flow rate. For the **debit\_total** method case, only one tranche is considered.

```

# z      Sum(u.dS)/Sum(dS)  Sum(dS)  Sum(u.dS)
.....

```

### 2.3.44SYSTEM

```

System "unix_commands"

```



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Interpreter to run Unix commands from the data file. Example:

**System** “echo The End | mail [triou@cea.fr](mailto:triou@cea.fr)”

#### 2.3.45 REDRESSER\_HEXAEDES\_VDF

**Redresser\_hexaedres\_VDF** domain\_name

Keyword to convert a domain (named domain\_name) with quadrilaterals/VEF hexaedras which looks like rectangles/VDF hexaedras into a domain with real rectangles/VDF hexaedras.

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## 2.4 OBJECT FIELD DEFINITION

As they are widely used in the data set, descriptions of the various field types recognised by Trio-U is given hereunder.

There are three field families:

- unknown fields; these are not mentioned in the data set
- physical parameter fields and initial condition fields
- boundary fields which are used in limitation conditions or in couplings

Two types of instructions using these fields are found in the data set:

### Field creation:

In accordance with object creation syntax, a field may be created as follows:

*field\_type    identificateur\_champ*

For example: **Champ\_Uniforme** gravity (instruction No. 1)

### Entering values in existing fields:

example No. 1: Values are entered for the **Champ\_Uniforme** (uniform gravity) type gravity object created by instruction No. 1:

**Read** gravite 2 0. -9.81

example No. 2: Imagine that the **Fluide\_Incompressible (Incompressible\_Fluid)** which includes a **Champ\_Don** object type to represent its dynamic viscosity. The read syntax will be as follows:

**mu** *field\_type    bloc\_lecture\_champ*

The **mu** identifier object already exists (it is automatically created when the **Fluide\_Incompressible (Incompressible\_Fluid)** type object that includes it was created). This instruction is used only to enter a value for it.

example No. 3: A fluid inlet with imposed speed type boundary condition is defined as follows:

Gauche      **Frontiere\_ouverte\_vitesse\_imposee**      *boundary\_field\_type*  
*bloc\_lecture\_champ.*

The boundary field is specified without selecting an identifier. A value is entered in the **Champ\_front (Boundary\_field)** type object carried by the **Cond\_lim (limitation\_condition)** type object.

When you write a data set, you are not free to select the syntax, i.e., you are bound by one of the previous cases. You must select a **Champ\_Don** or **Champ\_front** type and correctly fill in its read block. The list of fields that may be used and the associated read blocks will be given here.

## 2.4.1 STATIONARY FIELDS

- **Champ\_Uniforme (Uniform\_field)**: field that is constant in space and stationary.

**Champ\_Uniforme** nb\_comp vrel\_1...[vrel\_i]

*nb\_comp*: number of field components.

*vrel\_1...[vrel\_i]*: values of field components.

- **Field\_uniform\_keps\_from\_ud** : field which allows to impose on a domain K and EPS values derived from U velocity and D hydraulic diameter

**Field\_uniform\_keps\_from\_ud** { U vrel D diam }

*vrel*: this is the value of velocity specified in boundary condition.

*diam*: this is the value of hydraulic diameter specified in boundary condition.

- **Champ\_Uniforme\_Morceaux**: field which is partly constant in space and stationary.

```
Champ_Uniforme_Morceaux nom_domaine nb_comp
{ Default val_def sous_zone_1 val_1 ... sous_zone_i val_i }
```

*nom\_domaine*: name of the domain to which the sub-areas belong.

*nb\_comp*: number of field components.

By default, the value *val\_def* is assigned to the field. It takes the *sous\_zone\_i* identifier **Sous\_Zone (sub\_area)** type object value, *val\_i*. **Sous\_Zone (sub\_area)** type objects must have been previously defined if the operator wishes to use a **Champ\_Uniforme\_Morceaux (partly\_uniform\_field)** type object.

- **Valeur\_totale\_sur\_volume**: Similar as **Champ\_Uniforme\_Morceaux** with the same syntax. Used for source terms when we want to specify a source term with a value given for the volume (eg: heat in Watts) and not a value per volume unit (eg: heat in Watts/m3).

```
Valeur_totale_sur_volume nom_domaine nb_comp
{ Default val_def sous_zone_1 val_1 ... sous_zone_i val_i }
```

- **Champ\_Don\_lu**: This field is used to read a data field (values located at the center of the cells) in a file.

```
Champ_Don_lu nom_domain nb_comp filename
```

*name\_domain*: name of the domain

*nb\_comp*: number of field components

*filename*: name of the file. This file has the following format:

```
nb_val_lues          ->Number of values readen in th file
Xi Yi Zi             -> Coordinates readen in the file
Ui Vi Wi             -> Value of the field
```

Example:

Conditions\_initiales { vitesse Champ\_don\_lu dom 2 ftn10 }

- Champ\_som\_lu\_VDF
- Champ\_som\_lu\_VEF

Keywords to read in a file values located at the nodes of a mesh in VDF or VEF discretization :

**Champ\_som\_lu\_VDF** name\_domain nb\_comp tolerance filename  
**Champ\_som\_lu\_VEF** name\_domain nb\_comp tolerance filename

*name\_domain*: the domain name

*nb\_comp*: value of the dimension of the field

*tolerance*: value of the tolerance to check the coordinates of the nodes

*filename*: name of the file. This file has the following format:

```

Xi Yi Zi          -> Coordinates of the node
Ui Vi Wi          -> Value of the field on this node
Xi+1 Yi+1 Zi+1    -> Next point
Ui+1 Vi+1 Zi+1    -> Next value
....

```

- **Champ\_Fonc\_Reprise**: This field is used to read a data field in a save file (.xyz or .sauv) at a specified time. It is very useful, for example, to run a thermohydraulic calculation with velocity initial condition read into a save file from a previous hydraulic calculation.

**Champ\_Fonc\_Reprise** [xyz|formatte|binaire] filename  
 problem\_name field\_name [fonction n f1(val) f2(val) ... fn(val)] time | **last\_time**

*[xyz|formatte|binaire]* : Optional keyword to specify the format of the filename (by default xyz format). If xyz format is activated, the .xyz file from the previous calculation will be given for *filename*, and if formatte or binaire is choosen, the .sauv file of the previous calculation will be specified for *filename*. In the case of a parallel calculation, if the mesh partition does not changed between the previous calculation and the next one, the binaire format should be preferred, because is faster than the xyz format.

*filename*: name of the save file

*problem\_name*: name of the problem

*field\_name*: name of the problem unknown. It may also be the temporal average of a problem unknown (like moyenne\_vitesse, moyenne\_temperature,...)

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*fonction...*: Optional keyword to apply a function on the field being read in the save file (e.g. to read a temperature field in Celsius units and convert it for the calculation on Kelvin units, you will use: **fonction** 1 273.+**val** )

*time*: time of the saved field in the save file. If you give the keyword **last\_time** instead, the last time saved in the save file will be used.

Example:

```
Conditions_initiales { vitesse Champ_Fonc_Reprise pipe.xyz pb vitesse 5.101 }
```

- **Champ\_Fonc\_Med**: This field is used to read a data field in a MED-format file .med at a specified time. It is very useful, for example, to restart a calculation with a new or refined geometry. The field post-processed on the new geometry at med format is used as initial condition for restarting.

**Champ\_Fonc\_Med** [ **last\_time** ] filename.med domain\_name field\_name location time

filename: name of the .med file

domain\_name: name of the domain

field\_name: name of the problem unknown

location: to indicate where the field has been post-processed (**elem** or **som**)

time: time of the field in the .med file

**last\_time**: Optional keyword to use the last time of the MED file instead of the specified time.

Example:

```
Conditions_initiales { temperature Champ_Fonc_Med pipe.med dom temperature elem 0.25 }
```

- **Champ\_init\_canal\_sinal** : For a parabolic profile on U velocity with an unpredictable disturbance on V and W and a sinusoidal disturbance on V velocity :

```

Champ_init_canal_sinal nb_comp { Ucent value h value
    ampli_bruit value [ ampli_sin value ] omega value dir_flow 0
    dir_wall value
    min_dir_flow value
    min_dir_wall value
}
```

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**nb\_comp**: Number of field components.

**Ucent** value : Velocity value at the center of the channel.

**h** value : Half length of the channel.

**ampli\_bruit** value : Amplitude for the disturbance.

**ampli\_sin** value : Amplitude for the sinusoidal disturbance (optional, by default equals to  $u_{cent}/10$ ).

**omega** value : Value of pulsation for the of the sinusoidal disturbance.

In 2D:

$$u = U_{cent} * y(2h-y)/h/h$$

$$v = \text{ampli\_bruit} * \text{rand} + \text{ampli\_sin} * \sin(\omega * x)$$

rand: unpredictable value between -1 and 1.

in 3D:

$$u = U_{cent} * y(2h-y)/h/h$$

$$v = \text{ampli\_bruit} * \text{rand1} + \text{ampli\_sin} * \sin(\omega * x)$$

$$w = \text{ampli\_bruit} * \text{rand2}$$

rand1 and rand2: unpredictable values between -1 and 1.

**min\_dir\_wall** : Keyword to define the value of the minimum coordinate in the wall direction for the initialization of the flow in a channel. Default value for dir\_flow is 0.

**min\_dir\_flow** : Keyword to define the value of the minimum coordinate in the flow direction for the initialization of the flow in a channel. Default value for dir\_flow is 0.

**dir\_wall** : Keyword to define the wall direction for the initialization of the flow in a channel.

-if dir\_wall = 0, the normal to the wall is in direction

-if dir\_wall = 1, the normal to the wall is in Y direction

-if dir\_wall = 2, the normal to the wall is in Z direction

Default value for dir\_flow is 1

**dir\_flow**: Keyword to define the flow direction for the initialization of the flow in a channel.

-if dir\_flow = 0, the flow direction is X

-if dir\_flow = 1, the flow direction is Y

-if dir\_flow = 2, the flow direction is Z

Default value for dir\_flow is 0

## 2.4.2 UNSTATIONNARY FIELDS

- **Champ\_Tabule\_Temps**: this type of field is constant in space and tabulated as a function of time.

```
Champ_Tabule_Temps nb_comp { nval tps_1....tps_nval ... vrel_1 vrel_nval }
```

*nb\_comp*: this refers to the number of field components.

Values are entered into a table based on *nval* couples (*vrel\_i*, *tps\_i*). The value of the field at any time is calculated by linear interpolation from this table.

**Champ\_Uniforme\_Morceaux\_Tabule\_Temps**: this type of field is constant in space on one or several sub\_zones and tabulated as a function of time.

```
Champ_Uniforme_Morceaux_Tabule_Temps domaine_name nb_comp
{
  Default float(1) ... float(nb_comp)
  Sub_zone_name1 { nval tps_1....tps_nval ... vrel_1 vrel_nval }
  Sub_zone_name2 { nval tps_1....tps_nval ... vrel_1 vrel_nval }
  ....
}
```

*domaine\_name*: Name of the domain.

*nb\_comp*: this refers to the number of field components.

**Default** float(1) ... float(nb\_comp) : Constant values for the field on elements not covered by a subzone.

*Sub\_zone\_nameI*: Name of the Ith subzone.

Values are entered into a table based on *nval* couples (*vrel\_i*, *tps\_i*). The value of the field at any time is calculated by linear interpolation from this table.

- **Champ\_Fonc\_t**: this type of field is constant in space and is a function of time.

```
Champ_Fonc_t nb_comp f1(t) ... fnb_comp(t)
```

*nb\_comp*: this refers to the number of field components. *f<sub>i</sub>(t)* is a time dependant function.

- **Champ\_Fonc\_Fonction**: this refers to a field that is a function of another field.



**Champ\_Fonc\_Fonction** nb\_comp field expression

*nb\_comp*: this refers to the number of field components.

*field*: name of the field (for example: temperature)

*expression*: keyword to use a analytical expression like 10.\*EXP(-0.1\*val) where val be the keyword for the field.

Champ\_Fonc\_Fonction\_txyz : this refers to a field that is a function of another field and time and/or space coordinates

**Champ\_Fonc\_Fonction\_txyz** nb\_comp field expression

*nb\_comp*: this refers to the number of field components.

*field*: name of the field (for example: temperature)

*expression*: keyword to use a analytical expression like 10.\*EXP(-0.1\*val)\*x\*y\*z+t where val be the keyword for the field.

- **Champ\_Fonc\_Tabule**: this refers to a field that is tabulated as a function of another field.

**Champ\_Fonc\_Tabule** nb\_comp field  
[ { nval teta\_1 ....teta\_nval..vrel\_1.....vrel\_nval } ]

*nb\_comp*: this refers to the number of field components. Values are entered for a table based on *nval* couples (*vrel\_i*, *teta\_i*). The value of the tabulated field is calculated based on a given field (temperature, concentration,...) by linear interpolation from this table.

- **Champ\_fonc\_xyz**: This keyword represents a new field. It's now possible to write directly in the data file, a string representation of a function  $f(x,y,z)$ .

**Champ\_fonc\_xyz** domain\_name nb\_comp f\_1(x,y,z) ... f\_nbcomp(x,y,z)

$f_i(x,y,z)$  is a string representation of a mathematical expression (see 2.4.5).

- **Champ\_fonc\_txyz** : This keyword defines a new type of field. It makes it possible the definition of a field that depends on the time and the space.

**Champ\_Fonc\_txyz** domain\_name Nb\_comp f\_1(t,x,y,z) ... f\_Nb\_comp(t,x,y,z)

$f_i(x,y,z)$  is a string representation of a mathematical expression (see 2.4.5).

### 2.4.3 STATIONARY BOUNDARY FIELDS

- **Champ\_front\_uniform**: field which is constant in space and stationary

**Champ\_front\_uniforme** nb\_comp vrel\_1...[vrel\_i]

*nb\_comp*: this refers to the number of field components.

*vrel\_1...[vrel\_i]*: these are the values of field components.

- **Boundary\_field\_uniform\_keps\_from\_ud** : field which allows to impose on a boundary K and EPS values derived from U velocity and D hydraulic diameter

**Boundary\_field\_uniform\_keps\_from\_ud** { U vrel D diam }

*vrel*: this is the value of velocity specified in boundary condition.

*diam*: this is the value of hydraulic diameter specified in boundary condition.

- **Champ\_front\_fonc\_XYZ**: boundary field which is not constant in space

**Champ\_front\_fonc\_XYZ** nb\_comp f\_1(x,y,z) ... f\_nbcomp(x,y,z)

$f_i(x,y,z)$  is string representation of mathematical expression (see 2.4.5). For instance, to set the velocity :

Gauche frontiere\_ouverte\_vitesse\_imposee **Champ\_front\_fonc\_xyz** 2 5\*y\*(1-y) 0.

An example with a test :

Gauche frontiere\_ouverte\_vitesse\_imposee **Champ\_front\_fonc\_xyz** 2 (y>1.)\*5\*y\*(1-y) 0.

This example fixes the velocity  $V_x$  with the function  $5*y*(1-y)$  only if  $y > 1$ .

- **Champ\_front\_fonction**: boundary field that is function of another field

**Champ\_front\_fonction** nb\_comp field expression

*nb\_comp*: this refers to the number of field components.

*field*: name of the field (for example: temperature)

*expression*: keyword to use a analytical expression like 10.\*EXP(-0.1\*val) where val be the keyword for the field.

- **Champ\_front\_lu**: boundary field read in a file

**Champ\_front\_lu** domain\_name nb\_comp filename

**Champ\_Front\_lu** : boundary field which is given from data issued from a read file. The format of this file has to be the same that the one generated by **Ecrire\_fichier\_xyz\_valeur** (see 2.6.1).  
nom\_domaine : name of the domain

*nb\_comp* : number of components

*filename* : path for the read file

Example for K and epsilon quantities to be defined for inlet condition in a boundary named "entree":

entree **frontiere\_ouverte\_K\_Eps\_impose Champ\_Front\_lu** dom *2pb\_K\_EPS\_PERIO\_1006.306198.dat*

## 2.4.4 UNSTATIONNARY BOUNDARY FIELDS

- **Champ\_front\_tabule**: a constant field on the boundary, tabulated as a function of time

```
Champ_front_tabule nb_comp {n
t1 t2 t3 ....tn
u1 [v1 w1 ...] u2 [v2 w2 ...] u3 [v3 w3 ...] ... un [vn wn ...] }
```

*nb\_comp*: refers to the number of field components.

Values are entered into a table based on *n* couples (ti, ui) if *nb\_comp* value is 1. The value of a field at a given time is calculated by linear interpolation from this table.

- **Champ\_front\_fonc\_TXYZ**: boundary field which is not constant in space and in time

```
Champ_front_fonc_TXYZ nb_comp f_1(x,y,z,t) ... f_nbcomp(x,y,z,t)
```

*f\_i(x,y,z,t)* is string representation of mathematical expression (see 2.4.5). For instance, to set the velocity :

Gauche frontiere\_ouverte\_vitesse\_imposee **Champ\_front\_fonc\_txyz** 2 y\*sin(t) 0

- **Champ\_front\_bruite**: a field which is variable in time and space in a random manner.

```
Champ_front_bruite nb_comp { [N val L val ] Moyenne m_1.....[m_i ] Amplitude A_1.....[A_i ] }
```

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*nb\_comp*: number of field components

#### Random noise:

If N and L are not defined, the *i*th component of the field varies randomly around an average value  $m_i$  with a maximum amplitude  $A_i$ .

#### White noise:

If N and L are defined, these two additional parameters correspond to L, the domain length and N, the number of nodes in the domain. Noise frequency will be between  $2\pi/L$  and  $2\pi N/(4L)$ :

For example, formula for speed:  $u=U0(t)$   $v=U1(t)$

$Uj(t)=Mj+2\cdot Aj\cdot \text{bruit\_blanc}$  where *bruit\_blanc* (white\_noise) is the formula given in the *mettre\_a\_jour* (update) method of the *Champ\_front\_bruite* (noise\_boundary\_field) (Refer to the *Ch\_fr\_bruite.cpp* file)

- *Champ\_front\_debit* : this field is used to define a flow rate field instead of a velocity field for a Dirichlet boundary condition on Navier Stokes equation.

***Champ\_front\_debit*** *type\_field*

*type\_field* : Kind of field (*champ\_uniforme*, ...) to define the flow rate.

- *Champ\_front\_tangentiel\_VEF* : this field is used to define the tangential speed vector field standard at the boundary in VEF discretization.

***Champ\_front\_tangentiel\_VEF*** *vitesse\_tangentielle* *valeur*

*valeur*: vector field standard [m/s]

- *Boundary\_field\_inward* : this field is used to define the normal vector field standard at the boundary in VDF or VEF discretization.

***Boundary\_field\_inward*** { ***normal\_value*** *value* }

*value*: normal vector value (positive value for a vector oriented outside to inside)

- **Champ\_front\_ALE:** Keyword to define a boundary condition on a moving boundary of a mesh.

**Champ\_front\_ALE** nb\_comp val\_1...[val\_i]

**Example:**

*Boundary\_name* frontiere\_ouverte\_vitesse\_imposee **Champ\_front\_ALE** 2  
20\*0.3\*SIN(6.28\*y)\*COS(20\*t) 0. }

- **Champ\_front\_calc :** This keyword is used on a boundary to get a field from another boundary. The local and remote boundaries should have the same mesh. If not, the **Champ\_front\_recyclage** keyword could be used instead.

**Champ\_front\_calc** FieldProblemName FieldBoundaryName FieldName

FieldProblemName: name of the problem owning the desired field

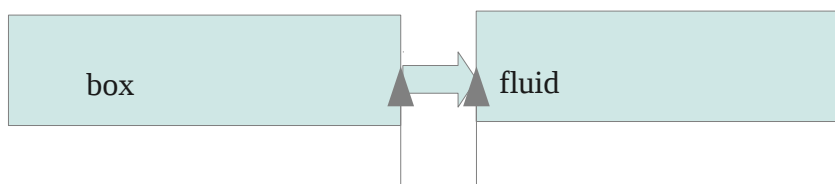
FieldBoundaryName: boundary name of the FieldProblemName problem where the desired field values will be copied from

FieldName: name of the desired field

*Example :*

**Read** fluid

```
{
    ...
    inlet frontiere_ouverte_temperature_imposee
    champ_front_calc box outlet temperature
    ...
}
```



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outlet      inlet

If inlet and outlet are not coincident meshes, but boundaries are coincident, you could use **champ\_front\_recyclage** which can work on this situation :

**Read fluid**

```
{
    ...
    inlet frontiere_ouverte_temperature_imposee
        champ_front_recyclage { pb_champ_evaluateur box temperature 1 }
    ...
}
```

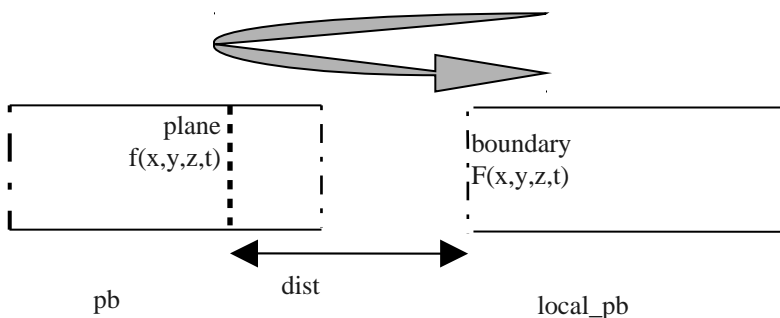
You will notice that outlet boundary is not specified here cause the temperature field is interpolated on the nodes of the inlet boundary so outlet boundary should be located on the inlet boundary (else use **distance\_plan** keyword).

- **Champ\_front\_recyclage** New keyword in 1.6.1 version which replaces and generalizes several obsolete ones:

```
Champ_front_calc_intern
Champ_front_calc_recycl_fluct_pbperio
Champ_front_calc_recycl_champ
Champ_front_calc_intern_2pbs
Champ_front_calc_recycl_fluct
```

```
Champ_front_recyclage {
    pb_champ_evaluateur pb field nb_comp
    [ distance_plan dist0 dist1 [dist2] ]
    [ moyenne_imposee methode_moy [fichier file [second_file] ]
    [ moyenne_recyclee methode_recyc [fichier file [second_file] ]
    [ direction_anisotrope 1|2|3 ]
    [ ampli_moyenne_imposee 2|3 alpha(0) alpha(1) [alpha(2)] ]
    [ ampli_moyenne_recyclee 2|3 beta(0) beta(1) [beta(2)] ]
    [ ampli_fluctuation 2|3 gamma(0) gamma(1) [gamma(2)] ]
}
```

This keyword is to use, in a general way, on a boundary of a local\_pb problem, a field calculated from a linear combination of an imposed field  $g(x,y,z,t)$  with an instantaneous  $f(x,y,z,t)$  and a spatial mean field  $\langle f \rangle(t)$  or a temporal mean field  $\langle f \rangle(x,y,z)$  field extracted from a plane of a problem named pb (pb may be local\_pb itself) :



For each component  $i$ , the field  $F$  applied on the boundary will be:

$$F_i(x,y,z,t) = \alpha_i * g_i(x,y,z,t) + \chi_i * [f_i(x,y,z,t) - \beta_i * \langle f_i \rangle]$$

The different options are :

**pb\_champ\_evaluateur** pb field nb\_comp : To give the name of the pb problem, the name of the field of the problem and its number of components nb\_comp.

**distance\_plan** dist0 dist1 [dist2] : Vector which gives the distance between the boundary and the plane from where the field  $F$  will be extracted. By default, the vector is zero, that should imply the two domains have coincident boundaries.

**ampli\_moyenne\_imposee** 2|3 alpha(0) alpha(1) [alpha(2)] :  $\alpha_i$  coefficients (by default =1)

**ampli\_moyenne\_recyclee** 2|3 beta(0) beta(1) [beta(2)] :  $\beta_i$  coefficients (by default =1)

**ampli\_fluctuation** 2|3 gamma(0) gamma(1) [gamma(2)] :  $\chi_i$  coefficients (by default =1)

**direction\_anisotrope** direction : If an integer is given for direction (X:1, Y:2, Z:3, by default, direction is negative), the imposed field  $g$  will be 0 for the 2 other directions.

**moyenne\_imposee** methode\_moy : Value of the imposed  $g$  field. The methode\_moy option can be :

**profil** [2|3] valx(x,y,z,t) valy(x,y,z,t) [valz(x,y,z,t)] : to specify analytic profile for the imposed  $g$  field.



**interpolation fichier *file*** : to create a imposed field built by interpolation of values read into a *file*. The imposed field is applied on the direction given by the keyword **direction\_anisotrope** (the field is zero for the other directions). The format of the *file* is:

```
pos(1) val(1)
pos(2) val(2)
...
pos(N) val(N)
```

If direction given by **direction\_anisotrope** is 1 (or 2 or 3), then pos will be X (or Y or Z) coordinate and val will be X value (or Y value, or Z value) of the imposed field.

**connexion\_approchee fichier *file*** : to read the imposed field into a *file* where positions and values are given (it is not necessary that the coordinates of the points match the coordinates of the faces of the boundary, indeed, the nearest point of each face of the boundary will be used). The format of the *file* is:

```
N
x(1) y(1) [z(1)] valx(1) valy(1) [valz(1)]
x(2) y(2) [z(2)] valx(2) valy(2) [valz(2)]
...
x(N) y(N) [z(N)] valx(N) valy(N) [valz(N)]
```

**connection\_exacte fichier *file second\_file*** : to read the imposed field into two files. The first *file* contains the points coordinates (which should be the same than the coordinates of each faces of the boundary) and the *second\_file* contains the mean values. The format of the first *file* is:

```
N
1 x(1) y(1) [z(1)]
2 x(2) y(2) [z(2)]
...
N x(N) y(N) [z(N)]
```

The format of the *second\_file* is:

```
N
1 valx(1) valy(1) [valz(1)]
2 valx(2) valy(2) [valz(2)]
...
```

N valx(N) valy(N) [valz(N)]

**logarithmique diametre** double **u\_tau** double **visco\_cin** double **direction** integer : to specify the imposed field (in this case, velocity) by an analytical logarithmic law of the wall :

$$g(x,y,z) = u\_tau * ( \log(0.5*diametre*u\_tau/visco\_cin)/Kappa + 5.1 )$$

With  $g(x,y,z)=u(x,y,z)$  if **direction** is set to 1 ( $g=v(x,y,z)$  if direction is set to 2, and  $g=w(x,y,z)$  if set to 3)

**moyenne\_recylee** methode\_recyc : Method used to do a spatial or a temporal averaging of f field to specify <f>. <f> can be the surface mean of f on the plane (**surface** option, see below) or it can be read from several files (for example generated by the **chmoy\_faceperio** option of the **Traitement\_particulier** keyword to obtain a temporal mean field). The option methode\_recyc can be :

**surfacique** : surface mean for <f> from f values on the plane

Same options of methode\_moy options but applied to read a temporal mean field <f>(x,y,z):

**interpolation**

**connexion\_approchee** fichier *file*

**connexion\_exacte** fichier *file second\_file*

## 2.4.5 SYNTAX TO DEFINE A MATHEMATICAL FUNCTION

In a mathematical function, used for example in field definition, it's possible to use the predefined function (an object parser is used to evaluate the functions) :

**ABS** : absolute value function

**COS** : cosinus function

**SIN** : sinus function

**TAN** : tan function

**ATAN** : arctan function

**EXP** : exponential function

**LN** : neperian logarithm function

**SQRT** : root mean square function

**INT** : integer function

**ERF** : erf function

**RND(x)** : random function (values between 0 and x)

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COSH	: hyperbolic cosinus function
SINH	: hyperbolic sinus function
TANH	: hyperbolic tangent function
ACOS	: inverse cosinus function
ATANH	: inverse hyperbolic tangent function
NOT(x)	: not equal to x
x_AND_y	: and function (returns 1 if x and y true else 0)
x_OR_y	: or function (returns 1 if x or y true else 0)
x_GT_y	: greater to (returns 1 if x>y else 0)
x_GE_y	: greater or equal to (returns 1 if x>=y else 0)
x_LT_y	: lesser to (returns 1 if x<y else 0)
x_LE_y	: lesser or equal to (returns 1 if x<=y else 0)
x_MIN_y	: minimum of x and y
x_MAX_y	: maximum of x and y
x_MOD_y	: modular division of x per y
x_EQ_y	: equal to (returns 1 if x=y else 0)
x_NEQ_y	: not equal to (returns 1 if x!=y else 0)

You can also use the following operations:

+	: addition
-	: subtraction
/	: division
*	: multiplication
%	: modulo
\$	: max
^	: power
<	: lesser than
>	: greater than
[	: less or equal to
]	: greater of equal to

You can also use the following constants:

Pi : pi value (3,1415...)

The variables which can be used are:

x,y,z : coordinates

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t : time

**Examples:**

Champ\_front\_fonc\_txyz 2 cos(y+x^2) t+ln(y)

Champ\_fonc\_xyz dom 2 tanh(4\*y)\*(0.95+0.1\*rnd(1)) 0.

**Possible error:**

Champ\_fonc\_txyz 1 cos(10\*t)\*(1<x<2)\*(1<y<2)

Previous line is wrong. It should be written:

Champ\_fonc\_txyz 1 cos(10\*t)\*(1<x)\*(x<2)\*(1<y)\*(y<2)

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## 2.5 MEDIUM SPECIFICATION

There are several types of medium available. A physical value that is characteristic of a medium is always defined as follows:

name\_of\_the\_physical\_value    field\_type    *field\_description*

### 2.5.1 INCOMPRESSIBLE FLUID

```

Fluide_incompressible fluid
Read fluid
{
  Mu field_type    field_description
  Rho Champ_Uniforme 1 vrel
  [ Cp Champ_Uniforme 1 vrel ]
  [ Lambda field_type    field_description ]
  [ Beta_th field_type    field_description ]
  [ Beta_co field_type    field_description ]
  [ Indice field_type    field_description ]
  [ Kappa field_type    field_description ]
}

```

**Mu:** This is a keyword used to define the dynamic viscosity value ( $\text{kg.m}^{-1}.\text{s}^{-1}$ ).

**Rho:** This is a keyword used to define the fluid density value ( $\text{kg.m}^{-3}$ ).

**Cp:** This is a keyword used to define the specific heat value ( $\text{J.kg}^{-1}.\text{K}^{-1}$ ).

**Lambda:** This is a keyword used to define the conductivity value ( $\text{W.m}^{-1}.\text{K}^{-1}$ ).

**Beta\_th:** This is a keyword used to define a thermal expansion value ( $\text{K}^{-1}$ ).

**Beta\_co:** This is the keyword which defines the volume expansion coefficient values in concentration

**Indice:** This is the keyword which defines the refractivity of fluid.

**Kappa:** This is the keyword which defines the absorptivity of fluid [m<sup>-1</sup>].

## 2.5.2NON NEWTONIAN FLUID

```

Fluide_Ostwald fluid
Read fluid
{
    mu Champ_Ostwald
    K field_type field_description
    n field_type field_description
    rho Champ_Uniforme 1 vrel
    [ Cp Champ_Uniforme 1 vrel ]
    [ lambda field_type field_description ]
    [ Beta_th field_type field_description ]
    [ Beta_co field_type field_description ]
}

```

**Fluide\_Ostwald:** This is the keyword used to describe non-Newtonian fluids, which are governed by Ostwald's law. The law applicable to stress tensor is:

$$\tau = K(T) \cdot (D:D/2)^{((n-1)/2)} \cdot D$$

Where:

D refers to the deformation speed tensor

K refers to fluid consistency (may be a function of the temperature T)

n refers to the fluid structure index

n=1 for a Newtonian fluid,

n<1 for a rheofluidifier fluid

n>1 for a rheothickening fluid

**mu Champ\_Ostwald:** This keyword is used to define the viscosity variation law:

$$\mu(T) = K(T) \cdot (D:D/2)^{((n-1)/2)}$$

**K:** This keyword is used to define fluid consistency

**n:** This keyword is used to define the fluid structure index

**Rho:** This keyword is used to define the fluid density value (kg.m<sup>-3</sup>).

**Cp:** This keyword is used to define the specific heat value (J.kg<sup>-1</sup>.K<sup>-1</sup>).

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**Lambda:** This keyword is used to define the conductivity value ( $\text{W.m}^{-1}.\text{K}^{-1}$ ).

**Beta\_th:** This keyword is used to define the thermal expansion value ( $\text{K}^{-1}$ ).

**Beta\_co:** This keyword is used to define the volume expansion coefficient values in concentration

### 2.5.3 CONSTITUENT

```

Constituant C
Read C
{
  Coefficient_diffusion field_type field_description
}

```

**Coefficient\_diffusion** : This keyword is used to define the diffusion coefficient value (expressed in  $\text{m}^2.\text{s}^{-1}$ ) of the constituent into the fluid. If a multi-constituent problem is being processed, the diffusion coefficients will be a vector field and each components will be the diffusion of the each constituent.

### 2.5.4 SOLID

```

Solide solid
Read solid
{
  Rho Champ_Uniforme 1 vrel
  Cp Champ_Uniforme 1 vrel
  Lambda field_type field_description
}

```

**Rho:** This keyword is used to define the solid density value ( $\text{kg.m}^{-3}$ ).

**Cp:** This keyword is used to define the specific heat value ( $\text{J.kg}^{-1}.\text{K}^{-1}$ ).

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**Lambda:** This keyword is used to define the conductivity value ( $\text{W.m}^{-1}.\text{K}^{-1}$ ).



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*Observations:*

- The user may simply define the properties relative to the problem.
- For the **Fluide\_Incompressible (incompressible\_fluid)** or **Solide (solid)** type, **Cp** and **Rho** must be **Champ\_Uniforme (uniform\_field)** type.
- The defined fields must have a physical value (specifically, they may not be set to zero or a negative value; if the user wishes to carry out the calculation, for example, without taking viscosity into consideration, a negligible diffusion operator should be used, but the user should not assign a value of zero to the viscosity field).
- When a thermohydraulic problem is being processed, gravity must be associated with the **Fluide\_Incompressible (incompressible\_fluid)** object type.

## 2.5.5 COMPRESSIBLE FLUID AT LOW MACH NUMBER

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## Fluide\_Quasi\_Compressible fluide

### Read fluide

```

{
  mu Champ_Uniforme 1 vrel
  [ sutherland mu0 value T0 value [Slambda value] C value ]
  lambda field_type field_description
  pression value
  loi_etat gaz_parfait {
    Prandtl value
    Cp value
    gamma value
    [ loi_etat Melange_gaz_parfait { Prandtl value Sc value } ]
  }
  [loi_etat gaz_reel_rhoT {
    Prandtl value
    Poly_T n+1 m+1
      a00 a01 ... a0m a10 a11... a1m ...an0.....anm
    Poly_rho n+1 m+1
      a00 a01 ... a0m a10 a11... a1m ...an0.....anm
    masse_molaire value
  }]
  [ Traitement_Pth keyword ]
  [ Traitement_rho_gravite keyword ]
  [ temps_debut_prise_en_compte_drho_dt value ]
  [ omega_relaxation_drho_dt value ]
}

```

Keyword to define a gas for a calculation under a small Mach number approximation.  
This gas may be a perfect gas :

**mu** : Dynamic viscosity  $\mu$  [kg/m/s]

**sutherland mu0 T0 [Slamba] C** : Sutherland law for viscosity  $\mu(T)=\mu_0*((T_0+C)/(T+C))*(T/T_0)^{1.5}$  and (optional) for conductivity:  $\lambda(T)=\mu_0*C_p/Prandtl*((T_0+Slambda)/(T+Slambda))*(T/T_0)^{1.5}$

**lambda** : Thermal conductivity  $k$  [W/m/K]

**Pression** : Pressure [Pa]

For a perfect gas (**loi\_etat\_gaz\_parfait**):

**Prandtl** : Prandtl number of the gas  $Pr=\mu*C_p/k$

**Cp** : Specific heat at constant pressure  $C_p$  [J/kg/K]

**gamma** :  $C_p/C_v$  with  $C_v$  specific heat at constant volume

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Or a mixing or perfect gas (**loi\_etat Melange\_gaz\_parfait**)

**Prandtl** : Prandtl number of the gas

**Sc** : Schmidt number of the gas  $Sc = \nu / D$  (D: diffusion coefficient of the mixing)

Or a real gas (**loi\_etat\_gaz\_reel**):

**Poly\_T** : Law for the temperature [K]  $T(P,h) = a00 + a01 * P + a10 * h + a11 * P * h + a02 * P * P + a20 * h * h + \dots$

with P pressure [hPa] and h enthalpy [J/kg]

**Poly\_rho** : Law for the density [kg/m3]

$\rho(P,h) = a00 + a01 * P + a10 * h + a11 * P * h + a02 * P * P + a20 * h * h + \dots$

with P pressure [hPa] and h enthalpy [J/kg]

**Masse\_molaire** : Mass of the gas [kg/mol]

**Traitement\_Pth** keyword : Optional keyword can be used in the description section of a quasi compressible fluid. With this keyword, it's possible to precise a particular treatment for the thermodynamic pressure Pth ; there are three possibilities:

- 1) with the keyword "edo" the code computes Pth solving an O.D.E. ; in this case, the mass is not strictly conserved (it is the default case for quasi compressible computation):
- 2) the keyword "conservation\_masse" forces the conservation of the mass (closed geometry or with periodic boundaries condition).
- 3) the keyword "constant" makes it possible to have a constant Pth ; it's the good choice when the flow is open (e.g. with pressure boundary conditions).

**Traitement\_rho\_gravite** keyword : It may be :

- 1) "standard" : the gravity term is evaluated with  $\rho * g$  (It is the default).
- 2) "moins\_rho\_moyen" : the gravity term is evaluated with  $(\rho - \rho_{\text{moy}}) * g$ .

**temps\_debut\_prise\_en\_compte\_drho\_dt** value : Optional option. While  $\text{time} < \text{value}$ ,  $d\rho/dt$  is set to zero (Rho, volumic mass). Useful for some calculation during the first time steps with big variation of temperature and volumic mass.

**omega\_relaxation\_drho\_dt** value : Optional option to have a relaxed algorithm to solve the mass equation. value is used (1 per default) to specify  $\omega$ :

$$\frac{\partial \rho^{n+1}}{\partial t} = \omega \frac{\rho^{n+1} - \rho^n}{dt} + (1 - \omega) \frac{\partial \rho^n}{\partial t} = \text{Div}(\rho u)$$

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## 2.6 PROBLEMS

A problem is defined by creating an object and assigning the problem type that the user wishes to resolve:

- **Hydraulic problem**

Resolution of the NAVIER STOKES equations:

**Pb\_Hydraulique pb**

- **Turbulent hydraulic problem**

Resolution of NAVIER STOKES equations with turbulence modelling:

**Pb\_Hydraulique\_Turbulent pb**

- **Thermohydraulic problem**

Resolution of coupled NAVIER STOKES/energy equations:

**Pb\_Thermohydraulique pb**

- **Turbulent thermohydraulic problem**

Resolution of NAVIER STOKES/ energy coupled equations, with turbulence modelling.

**Pb\_Thermohydraulique\_Turbulent pb**

- **Hydraulic problem with concentration**

Resolution of NAVIER STOKES/multiple constituent transportation equations:

**Pb\_Hydraulique\_Concentration pb**

- **Turbulent hydraulic problem with concentration:**

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Resolution of NAVIER STOKES/multiple constituent transportation equations

### **Pb\_Hydraulique\_Concentration\_Turbulent pb**

- **Thermohydraulic problem with concentration.**

Resolution of coupled NAVIER STOKES/multiple constituent transportation equations, with turbulence modelling:

### **Pb\_Thermohydraulique\_Concentration pb**

- **Turbulent thermohydraulic problem with concentration.**

Resolution of coupled NAVIER STOKES/multiple constituent transportation equations, with turbulence modelling:

### **Pb\_Thermohydraulique\_Concentration\_Turbulent pb**

- **Conduction problem**

Resolution of the heat equation:

### **Pb\_Conduction pb**

- **Thermohydraulical problem quasi-compressible**

Resolution of thermohydraulical problem under small Mach number:

### **Pb\_Thermohydraulique\_QC pb**

- **Turbulent thermohydraulical problem quasi-compressible**

Resolution of Navier Stokes equations for a turbulent thermohydraulical problem under small Mach number:

### **Pb\_Thermohydraulique\_Turbulent\_QC pb**

A problem is defined by creating an object and assigning the problem type that the user wishes to resolve:

To enter values for the problem objects created, the **Read** interpreter is used with a data block that is always structured as follows:

```

Read nom_pb
{

    bloc_lecture_equations

    [ Postraitement { ..... } ]
    [ Sauvegarde format_sauvegarde nom_fich ]
    [ Sauvegarde_simple format_sauvegarde nom_fich ]
    [ Reprise format_reprise nom_fich ]
}

```

In the following sub-chapters, the data blocks associated with each of the previously mentioned problem types will be presented. The **Postraitement (Post-processing)**, **Sauvegarde (Backup)** and **Reprise (Restart)** options are described in chapters 2.19, 2.17 and 2.18. Following this, this set of options will be assigned using *input\_output\_description* (outlet\_inlet\_block).

## 2.6.1HYDRAULIC PROBLEM

```

Read pb
{
  Navier_Stokes_Standard
  {
    Solveur_pression solveur { ..... }
    [ Dt_projection dt value ]
    [ Projection_initiale boolean ]
    [ methode_calcul_pression_initiale option ]
    [ Seuil_DivU value factor ]
    [ Solveur_bar { } ]
    Diffusion { [dif] }
    [ uzawa value ]
    Convection { [schema] }
    [ Sources { [sou1] , [sou2] , ... } ]
    Boundary_conditions { [cl_hydr1] [cl_hydr2] ..... }
    [ Conditions_initiales { [cl_init] } ]
    [ ecrire_fichier_xyz_valeur nom_champ val_dt_impr bords integer ... ]
    [ equation_non_resolue condition(t) ]
    [ parametre_equation keyword ]
  }

  input_output_description
}

```

**Navier\_Stokes\_Standard:** This keyword is used to define NAVIER STOKES equations.

**Solveur\_pression:** This keyword is used to define the linear pressure system resolution method. Refer to 2.10.

**Dt\_projection dt value:** This keyword checks every period dt the equality of velocity divergence to zero. value is the criteria convergency for the solver used.

**Projection\_initiale boolean:** Keyword to suppress, if boolean equals 0, the initial projection which checks DivU=0. By default, boolean equals 1.

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**methode\_calcul\_pression\_initiale** option : Keyword to select an option for the pressure calculation before the first time step. Options are : **avec\_les\_cl** (default option,  $\Delta P=0$  is solved with Neuman boundary conditions on pressure if any), **avec\_sources** ( $\Delta P=f$  is solved with Neuman boundaries conditions and  $f$  integrating the source terms of the Navier Stokes equation) and **avec\_sources\_et\_operateurs** ( $\Delta P=f$  is solved as with the previous option **avec\_sources** but  $f$  integrating also some operators of the Navier Stokes equation). The two last options are useful and sometime necessary when source terms are implicated when using an implicit time scheme to solve the Navier Stokes equation.

**Seuil\_DivU** value factor : this keyword is intended to minimise the number of iterations during the pressure system resolution. The convergence criteria during this step (“**seuil**” in **solveur\_pression**) is dynamically adapted according to the mass conservation. At  $t^n$ , the linear system  $Ax=B$  is considered as solved if the residual  $\|Ax-B\| < \text{seuil}(t^n)$ . For  $t^{n+1}$ , the threshold value  $\text{seuil}(t^{n+1})$  will be evaluated as:

```

If ( |max(DivU)*dt|<value )
    Seuil(tn+1)= Seuil(tn)*factor
Else
    Seuil(tn+1)= Seuil(tn)*factor
Endif

```

The first parameter (**value**) is the mass evolution the user is ready to accept per timestep, and the second one (**factor**) is the factor of evolution for “**seuil**” (for example, 1.1, so 10% per time step). Investigations has to be lead to know more about the effects of these two last parameters on the behaviour of the simulations

**Solveur\_bar** : This keyword is used to define when filtering operation is called (typically for **EF** convective scheme, **standard** diffusion operator and **Source\_Qdm\_lambdaup** ). A file (**solveur.bar**) is then created and used for inversion procedure. Syntax is the same then for pressure solver (GCP is required for multi-processor calculations and, in a general way, for big meshes).

**Diffusion**: This keyword is used to specify the diffusion operator.

By default, no value is entered into the **Diffusion** { } block. But *dif* may be one of the scheme listed on 2.8.2.

**Convection**: Keyword to alter the convection scheme.

*schema*: This may be one of the scheme listed on 2.8.



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**Sources:** This keyword is used to define the hydraulic equation source terms. Refer to 2.14.

*sou:* Source term definition.

**Boundary\_conditions:** This keyword is used to define hydraulic boundary conditions. Refer to 2.13.1.

*cl\_hydr:* Definition of a hydraulic boundary condition.

**Conditions\_initiales:** This keyword is used to define the initial hydraulic conditions. Refer to 2.12.1.

*cl\_init:* Defines the initial hydraulic conditions.

**Ecrire\_fichier\_xyz\_valeur:** This keyword is used to write the values of a field for some boundaries in a text file with the following format:

n\_valeur

x\_1 y\_1 [z\_1] val\_1

...

x\_n y\_n [z\_n] val\_n

The created files are named : pbname\_fieldname\_[boundaryname]\_time.dat

**Ecrire\_fichier\_xyz\_valeur** name\_field val\_dt\_impr **bords** nb\_bords boundary1...boundaryn

name\_field: the name of the field to write (Champ\_Inc, Champ\_Fonc or a post\_processed field)

val\_dt\_impr: the time period for printing in the file

bords: keyword to post-process only on some boundaries

nb\_bords: number of boundaries

boundary1...boundaryn : name of the boundaries

The name of the files is *pb\_name\_field\_name\_time.dat*

Several **Ecrire\_fichier\_xyz\_valeur** keywords may be written into an equation to write several fields. This kind of files may be read by **Champ\_don\_lu** or **Champ\_front\_lu** for example.

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A binary file will be written if **Ecrire\_fichier\_xyz\_valeur\_bin** is used instead of **Ecrire\_fichier\_xyz\_valeur** keyword.

The equation will not be solved while *condition(t)* is verified if **equation\_non\_resolue** keyword is used. Exemple: The Navier Stokes is not solved between time t0 and t1.

#### Navier\_Sokes\_Standard

```
{
    ...
    equation_non_resolue (t>t0)*(t<t1)
}
```

**Parametre\_equation** keyword : Keywords used to specify additional parameters for the equation. Two keywords are available for the moment: **parametre\_implicite** when using an implicit time schema and **parametre\_diffusion\_implicite** when impliciting diffusion of the equation with the keyword **diffusion\_implicite** used in an explicit time scheme. The options are listed below for each keyword:

#### Parametre\_equation parametre\_implicite

```
{
    [ seuil_convergence_implicite float ]
    [ seuil_generation_solveur float ]
    [ seuil_verification_solveur float ]
    [ seuil_test_preliminaire_solveur float ]
    [ solveur solveur_sys_base ]
    [ resolution_explicite ]
    [ equation_frequence_resolue integer | f (t) ]
}
```

**parametre\_implicite**: Keyword to change for this equation only the parameter of the implicit scheme used to solve the problem

**seuil\_convergence\_implicite**: Keyword to change for this equation only the value of **seuil\_convergence\_implicite** used in the implicit scheme

**seuil\_generation\_solveur**, **seuil\_verification\_solveur**, **seuil\_test\_preliminaire\_solveur**: Keywords to change for this equation only the values of **seuil\_generation\_solveur** or **seuil\_verification\_solveur** or **seuil\_test\_preliminaire\_solveur** used in the implicit scheme

**solveur**: Keyword to change for this equation only the solver used in the implicit scheme

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**resolution\_explicite:** Keyword to solve explicitly the equation whereas the scheme is an implicit scheme.

**equation\_frequence\_resolue** integer | f(t) : Keyword to specify that the equation is solved only every n time steps (n is an integer or given by a time-dependent function f(t)).

#### **Parametre\_equation parametre\_diffusion\_implicite**

```
{
  [ crank 0|1 ]
  [ niter_max_diffusion_implicite integer ]
  [ preconditionnement_diag 0|1 ]
  [ seuil_diffusion_implicite double ]
}
```

**crank 0|1** : Use (1) or not (0, default) a Crank Nicholson method for the diffusion implicitation algorithm. Setting crank to 1 increases the order of the algorithm from 1 to 2.

**niter\_max\_diffusion\_implicite** integer : Change the maximum number of iterations for the CG (Conjugate Gradient) algorithm when solving the diffusion implicitation of the equation.

**preconditionnement\_diag 0|1** : The CG used to solve the implicitation of the equation diffusion operator is not preconditioned by default. If this option is set to 1, a diagonal preconditionning is used.

**seuil\_diffusion\_implicite** double : Change the threshold convergence value used by default for the CG resolution for the diffusion implicitation of this equation.

## **2.6.2TURBULENT HYDRAULIC PROBLEM**

```

Read pb
{
  Navier_Stokes_Turbulent
  {
    .....
    Modele_turbulence modele { ..... }
    [ Traitement_Particulier { kind_of_calculation } ]
  }

  input_output_description
}

```

**Navier\_Stokes\_Turbulent:** This keyword is used to define NAVIER STOKES equations as well as the associated turbulence model equations. The parameters are identical to those of **Navier\_Stokes\_standard** (refer to 5.4.1) with in addition:

**Modele\_turbulence:** This keyword is used to define a turbulence model.

*modele:* Turbulence model selection. Refer to the chapter concerning turbulence models.

**Traitement\_particulier:** Keyword to post-process particular values for two kinds of calculation:

1) **THI:** Keyword for a THI (Homogeneous Isotropic Turbulence) calculation:

```

Traitement_particulier { THI {
  [init_Ec 0|1]
  [calc_spectre 0|1]
  [val_Ec double]
  [facon_init integer]
  [periode_calc_spectre double]
  [conservation_Ec]
  longueur_boite double
  [3D 0|1]
  [1D 0|1]
  [correlations 0|1]
  [champs_scalaires N field1 field2 ... fieldN]
}
}

```

**init\_Ec** 0|1: Keyword to renormalize (1) or not (0) initial velocity so as kinetic energy equals to the value given by keyword **val\_Ec** (default 0)

**calc\_spectre** 0|1 : Keyword to calculate or not the spectrum of kinetic energy

**val\_Ec** double : Keyword (VDF only) to impose a value for kinetic energy by velocity renormalization if **init\_Ec** value is 1.

**facon\_init** integer: Keyword (VDF only) to specify how to renormalize the initial velocity. The kinetic energy will be computed as the:

**0**: spatial kinetic energy

**1**: 1D spectral kinetic energy

**3**: 3D spectral kinetic energy

**periode\_calc\_spectre** double : Period of when to calculate spectrum (VEF option only)

**conservation\_Ec** : If this keyword is used, velocity field will be changed as to have a constant kinetic energy (default 0, VEF option only).

**longueur\_boite** double : Length of the calculation domain (VEF option only).

**3D** 0|1 : Calculate 3D spectrum (default 0, VEF option only).

**1D** 0|1 : Calculate 1D spectrum (default 0, VEF option only).

**correlations** 0|1 : Activate correlation calculation (default 0, VEF option only).

**champs\_scalaires** N field1 field2 ... fieldN: Add N scalar fields to the analysis (e.g. temperature) (Default, N=0, VEF option only)

Several files are created during the calculation.

2) **Canal**: Keyword for statistics on a periodic plane channel.

```

Traitement_particulier { Canal {
    [ dt_impr_moy_spat value ]
    [ dt_impr_moy_temp value ]
    [ debut_stat value ]
    [ fin_stat value ]
    [ pulsation_w value ]
    [ nb_points_par_phase value ]
    [ reprise val_moy_temp_xxxxxx.sauv ]
}
}

```

**dt\_impr\_moy\_spat** value : Period to print the spatial average (default value is 1e6)

**dt\_impr\_moy\_temp** value : Period to print the temporal average (default value is 1e6)

**debut\_stat** value : time to start the temporal averaging (default value is 1e6)

**fin\_stat** value : time to end the temporal averaging (default value is 1e6)

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**pulsation\_w** value : pulsation for phase averaging (in case of pulsating forcing term) (no default value)

**nb\_points\_par\_phase** value : number of samples to represent phase average all along a period (no default value)

**reprise** val\_moy\_temp\_xxxxxx.sauv : keyword to restart a calculation with previous average quantities

Note that for thermal and turbulent problems, averages on temperature and turbulent viscosity are automatically calculated.

To restart a calculation with phase averaging, val\_moy\_temp\_xxxxxx.sauv\_phase file is required on the directory where the job is submitted (this last file will be then automatically loaded by Trio\_U)

**3) THI\_NEW:** Other keyword for a THI (Homogeneous Isotropic Turbulence) calculation

For unstructured approach, Traitement\_particulier have been slightly modified. Averaging process respects better than previously the real location of the quantities (in the y-direction). Moreover, indications like friction velocity and reynolds, and evolution of the time step are calculated and written respectively in the files u\_tau, reynolds\_tau and dt\_evol.

General syntax : Just substitute the previous keyword "nb\_int" and "dir\_echant" to the following ones : Ny and eps. Ny is set to initialise the dimension of tables and eps is the tolerance to check if points belongs to the same y-co-ordinate of the other points.

Note that the present post-treatment is suitable only for plane channel configuration with wall normal direction according to y.

*Example:*

**Traitement\_particulier**

```
{
THI_new{
    init_Ec 1 val_Ec 1.5 facon_init 0
    calc_spectre 1
}
}
```

A new treatment for the temperature field is available for THI computation:

**THI\_thermo**

It offers the possibility to :

- evaluate the probability density function on temperature field,
- gives in a file the temperature field for a future spectral analysis
- monitor the evolution of the max and min temperature on the whole domain

The syntax is the same than for special treatment THI :

```
Traitement_particulier { THI_thermo { init_Ec 1 val_Ec 1.5 facon_init 0
calc_spectre 1 } }
```

**Traitement\_particulier { chmoy\_faceperio { stats val1 val2 } }**

This keyword is used to save in two files :

- the coordinates of the points located at the periodic boundaries (**geom\_face\_perio**)
- the temporal averaged velocity associated to these points (**chmoy\_face\_perio**) between time val1 and val2.

It will be useful then to generate fluctuating inlet conditions.

4) **Ec**: Keyword to print total kinetic energy into the referential linked to the domain (keyword **Ec**). In the case where the domain is moving into a Galilean referential, the keyword **Ec\_dans\_repere\_fixe** will print total kinetic energy in the Galilean referential whereas **Ec** will print the value calculated into the moving referential linked to the domain. **Periode** is the keyword to set the period of printing into the file *datafile\_Ec.son* or *datafile\_Ec\_dans\_repere\_fixe.son*.

**Traitement\_particulier { Ec { Ec|Ec\_dans\_repere\_fixe periode double } }**

### 2.6.3 THERMOHYDRAULIC PROBLEM

```

Read pb
{
  Navier_Stokes_Standard
  {
    .....
    [ Traitement_Particulier { kind_of_calculation } ]
  }
  Convection_diffusion_temperature
  {
    Diffusion { [dif] }
    Convection { [schema] }
    [ Sources { [sou1] [sou2] ..... } ]
    Boundary_conditions { [cl_therm1] [cl_therm2] ..... }
    [ Conditions_initiales { [cl_init] } ]
    [ parametre_equation keyword ]
  }

  input_output_description
}

```

**Navier\_Stokes\_Standard:** This keyword is used to define NAVIER STOKES equations.

**Convection\_diffusion\_temperature:** This keyword is used to define the energy equation (temperature diffusion convection).

**Diffusion:** This keyword is used to specify the diffusion operator.

By default, nothing is put in the **Diffusion** { } block.

*dif:* The value of dif should be **Negligeable** to suppress the temperature diffusion convection equation's diffusion operator.

**Convection:** This keyword is used to change the convection scheme (by default, the UPWIND scheme is selected).

*schema:* May be set to one of the scheme listed on 2.8.

**Sources:** This keyword is used to define the energy equation source terms.

*sou:* Defines the source term.



**Boundary\_conditions:** This keyword is used to define thermal boundary conditions. Refer to 2.13.2.

*cl\_therm:* Defines a thermal boundary condition.

**Conditions\_initiales:** This keyword is used to define initial thermal conditions. Refer to 2.12.2.

*cl\_init:* Defines initial thermal conditions on the domain.

**Traitement\_particulier :** Optional keyword to calculate some interesting values.

**Traitement\_particulier { Temperature { Bord *boundary* Direction integer } }**

Keyword to print mass flow rate and averaged temperature on the boundary. It generates 2 external files : *RhoU\_boundary* and *Tmoyen\_boundary*. The first file gives the product  $\rho \cdot U \cdot S$  at the *boundary* specified above, where U is the velocity in the direction defined by the integer value (0:X, 1:Y, 2:Z). The second one gives at the *boundary* the averaged temperature (according to  $\text{Sum}(\rho \cdot U \cdot S \cdot TdS) / \text{Sum}(\rho \cdot U \cdot SdS)$ ) and Tmin - Tmax for each time step.

**NB :** This calculation available only in VEF framework assumes that all the faces of *boundary* are on the same processor.

**Parametre\_equation :** See 2.6.1

## 2.6.4 TURBULENT THERMOHYDRAULIC PROBLEM

```

Read pb
{
  Navier_Stokes_Turbulent
  {
    .....
  }
  Convection_diffusion_temperature_turbulent
  {
    mêmes instructions que Convection_Diffusion_temperature
    Modele_turbulence modele { }
  }

  input_output_description
}

```

Version 1 does not feature the functionality required to process a turbulence problem in VEF discretization.

**Navier\_Stokes\_Turbulent:** This keyword is used to define NAVIER STOKES equations with turbulence modelling.

**Convection\_diffusion\_temperature\_turbulent:** This keyword is used to define the energy equation (temperature diffusion convection). Parameters are identical to **Convection\_diffusion\_temperature** (refer to 2.6.2) with in addition:

**Modele\_turbulence:** This keyword is used to define a turbulence model.

*modele:* The turbulence model selected for the energy equation. The only currently available model is **Prandtl**.

## 2.6.5 HYDRAULIC PROBLEM WITH CONCENTRATION

```

Read pb
{
  Navier_Stokes_Standard
  {
    .....
    [ Traitement_Particulier { ConcMoy { ConcMoy periode double Tx1 double Tx2 double Tx3
double } } ]
  }
  Convection_diffusion_concentration
  {
    Sources { [Source_Constituant field_type field_description] ... }
    Diffusion { [dif] }
    Convection { [schema] }
    Boundary_conditions { [cl_conc1] [cl_conc2] ..... }
    [ Conditions_initiales { [cl_init] } ]
    [ Nom_inconnue name ]
    [ parametre_equation keyword ]
  }

  input_output_description
}

```

**Navier\_Stokes\_Standard:** this keyword is used to define NAVIER STOKES equations.

**Sources:** This keyword is used to specify the source terms of the equation. **Source\_Constituant** is a keyword to specify source rates, in [[C]/s], for each one of the nb constituents. [C] is the concentration unit.

**Convection\_diffusion\_concentration:** This keyword is used to define the constituent transportation vectorial equation (concentration diffusion convection).

**Diffusion:** This keyword is used to specify the diffusion operator.

*dif:* This is set to **Negligeable** to suppress the constituent transportation equation diffusion operator.

**Convection:** This keyword is used to modify the convection scheme (by default, this is set to the UPWIND scheme).

*schema*: This may be one of the scheme listed on 2.8.

**Boundary\_conditions**: Keyword to define concentration boundary conditions. Refer to 2.13.3.

*cl\_conc*: Definition of a concentration boundary condition.

**Conditions\_initiales**: This keyword is used to define initial concentration conditions. Refer to 2.13.3.

*cl\_init*: Definition of initial concentration conditions.

**Nom\_inconnue** name: Keyword **Nom\_inconnue** will rename the unknown of this equation with the given name. In the postprocessing part, the concentration field will be accessible with this name. This is usefull if you want to track more than one "concentration" (otherwise, only the concentration field in the first concentration equation can be accessed).

**Parametre\_equation** : See 2.6.1

**Traitement\_particulier**: Keyword to post-process particular values for concentration equation:

**ConcMoy periode** double: printing period for values in the *datafile\_ConcMoy.son* file

**Tx1** double: Limit 1 for concentration rate

**Tx2** double: Limit 2 for concentration rate

**Tx3** double: Limit 3 for concentration rate

The format file is :

```
# Time ConcentrationRate1 ConcentrationRate2 ConcentrationRate3
0          0          0          0
0.1        0          0.001      0.002
....
```

Where ConcentrationRateI is evaluated with the concentration field  $C(x,y,z)$  :

$\text{ConcentrationRateI} = \text{Sum}(\text{volume where } Tx(x,y,z) < TxI) / \text{GlobalVolume}$

with  $Tx(x,y,z) = |C(x,y,z) / \text{MeanConcentration} - 1|$

$\text{MeanConcentration} = \text{Sum}(C(x,y,z) * \text{volume}) / \text{GlobalVolume}$

## 2.6.6 TURBULENT HYDRAULIC PROBLEM WITH CONCENTRATION

```

Read pb
{
  Navier_Stokes_Turbulent
  {
    ....
  }
  Convection_diffusion_concentration_turbulent
  {
    ...
    Modele_turbulence modele { }
  }

  input_output_description
}

```

Version 1 does not feature the functionality required to process turbulence problems in VEF discretization.

**Navier\_Stokes\_Turbulent:** This keyword is used to define the NAVIER STOKES equations and the associated turbulence model equations. Refer to 2.6.4.

**Convection\_diffusion\_concentration\_turbulent:** This keyword is used to define the constituent transportation equations (concentration diffusion convection). The parameters are identical to **Convection\_diffusion\_concentration** (refer to 2.6.5) with in addition:

**Modele\_turbulence:** This keyword is used to define a turbulence model.

*modele:* Selection of the turbulence model to be used in the constituent transportation equation. The only model currently available is **Schmidt**.

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## 2.6.7 THERMOHYDRAULIC PROBLEM WITH CONCENTRATION

```

Read pb
{
  Navier_Stokes_Standard
  {
    .....
  }

  Convection_diffusion_temperature
  {
    .....
  }

  Convection_diffusion_concentration
  {
    .....
  }

  input_output_description
}

```

**Navier\_Stokes\_Standard:** This keyword is used to define NAVIER STOKES equations. Refer to 2.6.1.

**Convection\_diffusion\_temperature:** This keyword is used to define the energy equation (temperature diffusion convection). Refer to 2.6.2.

**Convection\_diffusion\_concentration:** This keyword is used to define constituent transportation equations (concentration diffusion convection). Refer to 2.6.5.

## 2.6.8 THERMOHYDRAULIC TURBULENT PROBLEM WITH CONCENTRATION

```

Read pb
{
  Navier_Stokes_Turbulent
  {
    ....
  }

  Convection_diffusion_temperature_turbulent
  {
    ....
  }

  Convection_diffusion_concentration_turbulent
  {
    ....
  }

  input_output_description
}

```

Version 1 does not yet feature the functionality required to process a turbulence problem in VEF discretization.

**Navier\_Stokes\_Turbulent:** This keyword is used to define NAVIER STOKES equations and the associated turbulence model. Refer to 2.6.1.

**Convection\_diffusion\_temperature\_turbulent:** This keyword is used to define the energy equation (temperature diffusion convection). Refer to 2.6.3.

**Convection\_diffusion\_concentration\_turbulent:** This keyword is used to define the constituent transportation equations (concentration diffusion convection). Refer to 2.6.5.

## 2.6.9 CONDUCTION PROBLEM

```

Read pb
{
  Conduction
  {
    Diffusion { [dif] }
    [ Sources { [sou1] [sou2] ..... } ]
    Boundary_conditions { [cl_therm1] [cl_therm2] ..... }
    [ Conditions_initiales { [cl_init] } ]
    [ parametre_equation keyword ]
  }

  input_output_description
}

```

**Conduction:** This keyword is used to define the heat equation.

**Diffusion:** This keyword is used to specify the diffusion operator.

*dif*: Set to **Negligeable** to suppress the constituent transportation equation diffusion operator.

**Sources:** This keyword is used to define the heat equation volume power type source terms. Refer to 2.15.

*sou*: Source term definition.

**Boundary\_conditions:** This keyword is used to define the thermal boundary conditions. Refer to 2.6.4.

*cl\_therm*: Defines the thermal boundary condition.

**Conditions\_initiales:** This keyword is used to define initial thermal conditions. Refer to 2.12.2.

*cl\_init*: Defines the initial thermal conditions.

**Parametre\_equation** : See 2.6.1



## 2.6.10 PROBLEM FOR NAVIER STOKES EQUATIONS UNDER A SMALL MACH NUMBER APPROXIMATION

```

Pb_Thermohydraulique_QC
Read pb
{
  Navier_Stokes_QC { ... }
  Convection_Diffusion_Chaleur_QC
  {
    diffusion { }
    convection { }
    [ mode_calcul_convection ancien
                                | divuT_moins_Tdivu
                                | divrhout_moins_Tdivrhout ]

    sources { }
    Boundary_conditions { }
    conditions_initiales { }
  }
  ...
}

Solve pb

```

The useful keywords for the solved equations are :

**Navier\_Stokes\_QC** : equation for momentum

**Convection\_Diffusion\_Chaleur\_QC** : equation for energy

**Mode\_calcul\_convection** : Option to set the form of the convective operator:

**divrhout\_moins\_Tdivrhout** (the default since 1.6.8):  $\rho \cdot u \cdot \text{grad} T = \text{div}(\rho \cdot u \cdot T) - T \text{div}(\rho \cdot u)$

**divuT\_moins\_Tdivu** :  $u \cdot \text{grad} T = \text{div}(u \cdot T) - T \text{div}(u)$

**ancien** :  $u \cdot \text{grad} T = \text{div}(u \cdot T) - T \cdot \text{div}(u)$

The boundary conditions are described here 2.13.1.

Keywords for the unknowns other than pressure, velocity, temperature are:

**masse\_volumique** : density

**enthalpie** : enthalpy

**pression** : reduced pressure

**pression\_tot** : total pressure

## 2.6.11 TURBULENT THERMOHYDRAULICAL PROBLEM UNDER SMALL MACH NUMBER

```

Pb_Thermohydraulique_Turbulent_QC
Read pb
{
    Navier_Stokes_Turbulent_QC { ... }
    Convection_Diffusion_Chaleur_Turbulent_QC
    {
        diffusion { }
        convection { }
        sources { }
        boundary_conditions
        conditions_initiales { }

        input_output_description
    }

    Solve pb

```

New problem for Navier Stokes equations under a small Mach number approximation and with turbulence model (standard k-eps or k-eps at Low Reynolds)

New keywords for the solved equations are :

**Navier\_Stokes\_Turbulent\_QC** : equation and turbulence model for momentum

**Convection\_Diffusion\_Chaleur\_Turbulent\_QC** : equation and turbulence model for energy

**Prandtl** : To give the value of Prandtl number in the Prandtl model.

**Warning:** Available for VDF and VEF P0/P1NC discretization only.

Low Reynolds k-eps model available in VDF discretisation only.

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## 2.6.12 DISCONTINUOUS FRONT TRACKING PROBLEMS

The generic Front-Tracking problem (**Probleme\_FT\_Disc\_gen**) in the discontinuous version differs from the rest of the Trio\_U code: The problem does not state the number of equations that are enclosed in the problem. Two equations are compulsory: a momentum balance equation (alias Navier-Stokes equation) and an interface tracking equation. The list of equations to be solved is declared in the beginning of the data file.

Another difference with more classical Trio\_U data file, lies in the fluids definition. The two-phase fluid (**Fluide\_Diphasique**) is made with two usual single-phase fluids (**Fluide\_Incompressible**). These two specificities lead to the following general structure of the data file:

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```

dimension 3
Probleme_FT_Disc_gen pb
Domaine DOM
Read_file DOM domain.geom
VEFPrePIB dis
Schema_Euler_explicite sch
Read sch { ../. }
Fluide_Incompressible liquid
Read liquid { ../. }
Fluide_Incompressible gas
Read gas { ../. }
Fluide_Diphasique fluids
Read fluids { ../. }
Constituant constituant
Read constituant { ../. }
Champ_Uniforme gravite
Read gravite 3 0. 0. -9.81
Associate fluide gravite
Navier_Stokes_FT_Disc      eq_hydraulique
Transport_Interfaces_FT_Disc  agit
Transport_Interfaces_FT_Disc  interf
Convection_Diffusion_Concentration eq_diffusion
Associate pb eq_hydraulique
Associate pb agit
Associate pb interf
Associate pb eq_diffusion
Associate pb DOM
Associate pb sch
Associate pb fluids
Associate pb constituant
Discretize pb dis
Read pb
{
  eq_hydraulique { ../. }
  agit          { ../. }
  interf        { ../. }
  eq_diffusion  { ../. }
  liste_postraitements { ../. }
}
Solve pb
Fin

```

In the previous example, the two-phase fluid (**Fluide\_Diphasique**) is named *fluids* and is composed made with two usual single-phase non-compressible fluids (**Fluide\_Incompressible**) named *liquid* and *gas*.

In the previous example, the Front-Tracking problem (**Probleme\_FT\_Disc\_gen**) includes four equations:

- a momentum balance equation (**Navier\_Stokes\_FT\_Disc**) named *eq\_hydraulique*,
- a first interface tracking equation (**Transport\_Interfaces\_FT\_Disc**) named *agit*,
- a second interface tracking equation (**Transport\_Interfaces\_FT\_Disc**) named *interf*,
- a simple convection-diffusion equation (**Convection\_Diffusion\_Concentration**) of a passive scalar (a concentration in chemical specie) named *eq\_diffusion*.

As the list of equations to be solved in the generic Front-Tracking problem is declared in the data file and not pre-defined in the structure of the problem, each equation has to be distinctively associated with the problem with the **Associate** keyword.

### Some comments on the time scheme

At the time we write this document, the only time scheme for which a proper use has been proven is the explicit Euler scheme (**Schema\_Euler\_explicite**). An example of parameters for this scheme is:

```

Schema_Euler_explicite sch
Read sch
{
    tinit 0.
    tmax 100.
    dt_min 1.e-7
    dt_max 1.e-3
    dt_impr 10.
    dt_sauv 0.2
    facsec 0.8
    seuil_statio -1
}

```

In most situations that have already been experienced, it is advisable not to let the code to select the proper time stepping, but to provide some limits. The usual **facsec** keyword with values lesser than unity can be used along with a maximum time step value defined by **dt\_max**. The threshold value -1 for **seuil\_statio** can be used to prevent the code from stopping during a calm period before another interesting event.

### 2.6.12.1 Two-phase fluid description

It is necessary to first declare the two phases, and second to declare the two-fluid mixture, water and air in the following example:

```

Fluide_Incompressible liquid
Read liquid
{
    mu Champ_Uniforme 1 0.001
    rho Champ_Uniforme 1 1000
}
Fluide_Incompressible gas
Read gas
{
    mu Champ_Uniforme 1 0.00001
    rho Champ_Uniforme 1 1.3
}
Fluide_Diphasique fluids
Read fluids
{
    fluide0 liquid
    fluide1 gas
    sigma Champ_uniforme 1 0.07
    [chaleur_latente Champ_uniforme 1 double ]
}

```

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Obviously, **rho** stands for the fluid density, **mu** for its dynamic viscosity and **sigma** for the surface tension between the two fluids. Another possible attribute of the **Fluide\_Diphasique** object is **chaleur\_latente** for the heat of phase-change (given to the fluid when change from phase 0 to phase 1) in diabatic liquid-vapor problems. It is a signed value for **chaleur\_latente** so negative value is possible if the phase 0 is vapor and phase 1 is liquid.

The classical use of **fluide0/fluide1** is to choose **fluide0** for the liquid (or the denser phase) and **fluide1** for the gas, the vapor or the lighter phase. With this choice, the indicator function used in the code is equivalent to the classical void fraction: the indicator function is equal to 0 in **fluide0** and is equal to 1 in **fluide1**. The other choice of **fluide0/fluide1** is possible, but should be used more carefully.

### The buoyancy forces

The buoyancy forces come out from the gravity acceleration and the difference of density between *fluide0* and *fluide1*. The simplest way of introducing the buoyancy forces is:

```

Champ_Uniforme gravity
Read gravity 3 0 0 -9.81
Associate fluids gravity

```

Another possible way of producing buoyancy forces lies in the forces associated to the change of frame of reference. This term is a source term, included in the momentum balance equation:

```

Read pb
{
  eq_hydraulique
  {
    solveur_pression GCP { ../.. }
    convection      { ../.. }
    diffusion       { ../.. }
    sources { acceleration { acceleration Champ_Fonc_t 3 0. 0. -9.81 } }
    ../..
  }
}

```

### 2.6.12.2 Two-phase momentum balance equation

The two-phase momentum balance equation (**Navier\_Stokes\_FT\_Disc**) has the same attributes as single-phase equations and additional features:

```

eq_hydraulique
{
    solveur_pression GCP { preconditioner { omega 1.5 } seuil 1.e-12 impr }
    modele_turbulence model
    convection { scheme }
    conditions_initiales { ../. }
    boundary_conditions { ../. }
    diffusion { scheme }
    matrice_pression_invariante
    equation_interfaces_proprietes_fluide interf
    [ equation_temperature_mpoint temperature_equation ]
    equations_interfaces_vitesse_imposee 1 agit
    clipping_courbure_interface 10000.
    [ Terme_gravite rho_g | grad_I ]
    [ equations_concentration_source_vortex N EQ_1 ... EQ_N ]
    [ repulsion_aux_bords MINX MAXX SLOPE ]
    [ penalisation_forage { [ pression_reference double ] } ]
}

```

The pressure solvers are common with single-phase Navier-Stokes equations. The most used choice is the **GCP** solver. Alternative choice is for instance solvers from the **Petsc** API package.

The value of **seuil** should be decreased as the mesh size is refined and the number of time steps is increased. For 1000 time steps on a  $10^6$ -nodes domain, indicative maximum values are  $1.e-6$  for a 1-dm<sup>3</sup> domain and  $1.e-9$  for a 1-cm<sup>3</sup> domain.

Up today, two keywords are available for *model*. First, taking the keyword **nul** for *model* means you consider the flow is laminar. Another choice, for a turbulent flow, is the **Wale** model:

```

modele_turbulence sous_maille_wale
{
    Cw 1.e-16
    turbulence_paroi negligeable
}

```

The value of  $1.e-16$  for **Cw** is another way of having a negligible turbulence model. A more physical value (default) is  $0.5$ . However, even with no intention of having of sub-grid turbulence model, the use of **modele\_turbulence** with a keyword different from **nul** allows the strain tensor  $\tau^p$  to be calculated with  $(\nabla \mathbf{V} + {}^t \nabla \mathbf{V})$  and not only with  $(\nabla \mathbf{V})$  alone (this has no physical ground but is specific to the way the strain tensor is calculated in Trio\_U). This second choice is highly recommended.

The **convection** options depend on the discretization choice. With a structured discretization (**VDF**), the most usual choice for *scheme* is **quick** and a with a non-structured discretization (**VEFPreP1B**), it is **muscl**.

The **conditions\_initiales** block is used to define the initial value of the unknown field, the velocity field (**vitesse**) in this momentum balance equation. An example is a computed velocity field (with two zero components):

```

conditions_initiales
{
    vitesse Champ_fonc_xyz dom 3 0. 0. -32*(x-0.025)*(x-0.025)-0.02
}

```

The **boundary\_conditions** block is used to specify boundary conditions.

## boundary\_conditions

```
{
    droite Paroi_fixe
    bas Frontiere_ouverte_vitesse_imposee champ_front_uniforme 3 0. 0. 1.
    haut Sortie_libre_rho_variable champ_front_uniforme 1 0.
    perioy Periodique
}
```

The keyword **Paroi\_fixe** is used to specify zero velocity at the boundary (adherence).

The keyword **Frontiere\_ouverte\_vitesse\_imposee** is used to specify a non-zero velocity at the boundary.

The keyword **Sortie\_libre\_rho\_variable** is used to define an outlet boundary condition at which the pressure is defined through the given field, whereas the density of the two-phase flow may varies (value of  $P/\rho$  given in  $\text{Pa}/\text{kg}\cdot\text{m}^{-3}$ ).

The keyword **Periodique** is used to define periodic boundary condition. The syntax is the same as for single-phase problems. However, this boundary condition has not yet been used successfully with interfaces crossing through the periodic boundary...

Other available boundary condition:

## Frontiere\_ouverte\_vitesse\_vortex

```
{
    sous_zone SOUS_ZONE_NAME
    equation EQ_NAME
    integrale_reference REF_VAL
    signe -1 | 1
    coeff_vitesse DIM vx vy [vz]
}
```

This boundary condition inherits from **Frontiere\_ouverte\_vitesse\_imposee** and might be used to model a "spillway" (e.g. maintain a given altitude of a free surface at some point close to the boundary condition). The velocity of the fluid is a uniform field equal to the vector **coeff\_vitesse** multiplied by a factor  $f$ . The indicator function of equation EQ\_NAME (must be an interface transport equation) is integrated over the region SOUS\_ZONE\_NAME, then REF\_VAL is subtracted. If this value (called "factor") is of the requested sign (signe keyword), then the applied velocity is  $\text{coeff\_vitesse} \times \text{factor}$ , otherwise the velocity is zero. SOUS\_ZONE\_NAME should be a small sub\_zone close to the boundary condition. The amplitude of **coeff\_vitesse** determines the time constant for the liquid level adjustment.

The **diffusion** block has been used for specific model in two-phase cell. However, this model is not available in the current version of Trio\_U: so the keyword **viscosite\_fortement\_variable** is not currently implemented and *scheme* keyword is limited to those available in single-phase problems.

The **matrice\_pression\_invariante** keyword is a shortcut to be used only when the flow is a single-phase one, with interface tracking only used for solid-fluid interfaces. In this peculiar case, the density of the fluid does not evolve during the computation and the pressure matrix does not need to be actuated at each time step.

The **equations\_interfaces\_vitesse\_imposee** keyword is used to specify the velocity field to be used when using an interface that mimics a solid interface moving with a given solid speed of displacement. When this case is selected, the keyword sequence **Methode\_transport\_vitesse\_imposee** in the **Transport\_Interfaces\_FT\_Disc** block will define the velocity field for the displacement of the interface. If two or more solid interfaces are defined, then the keyword **equations\_interfaces\_vitesse\_imposee** should be used as:



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**equations\_interfaces\_vitesse\_imposee** number\_of\_equations equation\_name1 equation\_name2 ...

The **equation\_interfaces\_proprietes\_fluide** block is used for liquid-gas, liquid-vapor and fluid-fluid deformable interface, which transported at the Eulerian velocity. When this case is selected, the keyword sequence **Methode\_transport\_vitesse\_interpolee** is used in the block **Transport\_Interfaces\_FT\_Disc** to define the velocity field for the displacement of the interface.

The **equation\_temperature\_mpoint** should be used in the case of liquid-vapor flow with phase-change (see the \$TRIO\_U\_ROOT/doc/Trio\_U/ft\_chgt\_phase.pdf written in French for more information about the model). The name of the temperature equation, defined with the **convection\_diffusion\_temperature\_ft\_disc** keyword, should be given.

The **clipping\_courbure\_interface** block is used to numerically limit the values of curvature used in the momentum balance equation. Curvature is computed as usual, but values exceeding the clipping value are replaced by this threshold, before using the clipped curvature in the momentum balance. Each time a curvature value is clipped, a counter is increased by one unity and the value of the counter is written in the err file at the end of the time step. This clipping allows not reducing drastically the time stepping when a geometrical singularity occurs in the interface mesh. However, physical phenomena may be concealed with the use of such a clipping!

The **Terme\_gravite** keyword changes the numerical scheme used for the gravity source term. The default is **grad\_i**, which is designed to remove spurious currents around the interface. In this case, the pressure field does not contain the hydrostatic part but only a jump across the interface. This scheme seems not to work very well in vef. The **rho\_g** option uses the more traditional source term, equal to  $\rho \cdot g$  in the volume. In this case, the hydrostatic pressure is visible in the pressure field and the boundary conditions in pressure must be set accordingly. This model produces spurious currents in the vicinity of the fluid-fluid interfaces and with the immersed boundary conditions.

**equations\_concentration\_source\_vortex** N EQ\_1 ... EQ\_N : see **Source\_Constituant\_Vortex** keyword.

**repulsion\_aux\_bords** MINX MAXX SLOPE : This keyword is a hack to prevent bubbles (or droplets) to touch walls. The potential used to take into account gravity is modified to provide a repulsive force located outside the region  $\text{minx} \leq X \leq \text{maxx}$  and  $\text{minx} \leq Y \leq \text{maxx}$  (these coordinates should be at a few mesh cells of the walls inside the domain). SLOPE is the gradient of the potential (2-4 times the gravity should work). Of course, this hack works for rectangular boxes only...

**penalisation\_forcage** { [ **pression\_reference** double ] } : This keyword is useful when a solid-fluid interface is used (see 2.6.12.4). Default is the Direct Forcing method to impose the velocity of the solid-fluid interface. With this keyword **penalisation\_forcage**, user can switch to the Penalized Direct Forcing method. If the optional keyword **pression\_reference** is given, the pressure is L2 penalized to the specified value.

### 2.6.12.3 Fluid-fluid interface tracking equation

To try to be clearer, the two types of interface tracking equations are explained separately. In this section, the case of fluid-fluid interface tracking equations is described. This description stands for all cases of fluid-fluid two-phase flow. The case of solid-fluid interaction will be described in the next section.

In order to perform fluid-fluid two-phase flow (liquid-gas or liquid-liquid), **equation\_interfaces\_proprietes\_fluide** has been declared in the Navier-Stokes equation and the interface tracking equation (**Transport\_Interfaces\_FT\_Disc**) has to specify **vitesse\_interpolee** for the **methode\_transport**. Additional parameters are the remeshing parameters, initial and boundary conditions:

```

interf
{
    methode_transport vitesse_interpolee eq_hydraulique
    methode_interpolation_v method
    conditions_initiales { fichier_geom ... / fonction ... [ , fonction ... | fonction_ignorer_collision ... ] .... }
    boundary_conditions { ../.. }
    [ maillage { ../.. } ]
    remaillage { ... }
    [ collisions { ... } ]
    n_iterations_distance nb
    iterations_correction_volume nb
    volume_impose_phase_1 volume
    [ Parcours_interface { [ correction_parcours_thomas ] } ]
    [ injecteur_interfaces FILENAME ]
    [ suppression_sous_zone SOUS_ZONE_NAME ]
    [ sous_zone_volume_impose SOUS_ZONE_NAME ]
    [ interpolation_repere_local ]
}

```

In the block **methode\_transport**, the keyword **vitesse\_interpolee** is used to specify that the interpolation will use the velocity field of the Navier-Stokes equation named *eq\_hydraulique* to compute the speed of displacement of the nodes of the interfaces.

In the block **methode\_interpolation\_v**, two keywords are possible for *method* to select the way the interpolation is performed. With the choice **valeur\_a\_elem** the speed of displacement of the nodes of the interfaces is the velocity at the center of the Eulerian element in which each node is located at the beginning of the time step. This choice is the default interpolation method. The choice **VDF\_lineaire** is only available with a VDF discretization (**VDF**). In this case, the speed of displacement of the nodes of the interfaces is linearly interpolated on the 4 (in 2D) or the 6 (in 3D) Eulerian velocities closest the location of each node at the beginning of the time step. In peculiar situation, this choice may provide a better interpolated value. Of course, this choice is not available with a VEF discretization (**VEFPreP1B**).

The keyword **conditions\_initiales** is used to define the shape of the initial interfaces through the zero level-set of a **function**, or through a mesh **fichier\_geom** (Refer to 2.6.12.4). Indicator function is set to *0*, that is *fluide0*, where the function is negative; indicator function is set to *1*, that is *fluide1*, where the function is positive; the interfaces are the level-set *0* of that function:

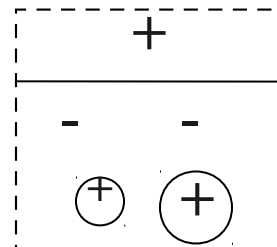
```

conditions_initiales / fonction
(-(x-0.002)^2+(y-0.002)^2+z^2-(0.00125)^2))*((x-0.005)^2+(y-0.007)^2+z^2-(0.00150)^2))*((0.020-z))
}

```

In the above example, there are three interfaces: two bubbles in a liquid with a free surface. One bubble has a radius of *0.00125*, i.e. *1.25 mm*, and its center is *{0.002, 0.002, 0.000}*. The other bubble has a radius of *0.00150*, i.e. *1.5 mm*, and its center is *{0.005, 0.007, 0.000}*. The free surface is above the two bubble, at a level *z=0.02*.

Additional feature in this block concerns the keywords **ajout\_phase0** and **ajout\_phase1**. They can be used to simplify the composition of different interfaces. When using these keywords, the initial function defines the indicator function; **ajout\_phase0** and **ajout\_phase1** are used to modify this initial field. Each time **ajout\_phase0** is used, the field is untouched where the function is positive whereas the indicator field is set to *0* where the function is negative. The keyword **ajout\_phase1** has the symmetrical use, keeping the field value where the function is negative and setting the indicator field to *1* where the function is positive. The previous example can also be written:



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```

conditions_initiales {
    fonction z-0.020 ,
    fonction ajout_phase1 (x-0.002)^2+(y-0.002)^2+z^2-(0.00125)^2 ,
    fonction ajout_phase1 (x-0.005)^2+(y-0.007)^2+z^2-(0.00150)^2
}

```

The **boundary\_conditions** block is used to specify boundary conditions. The keyword adapted to compute the indicator function boundary conditions in the case of two-phase flows is **Paroi\_ft\_disc**. Two kind of boundary condition may be applied : symmetry and contact angle fixed. Symmetry is equivalent to fix an angle of 90 degrees. The angle is measured between the wall and the interface in the phase 0.

```

boundary_conditions {
    cl_1 Paroi_FT_Disc symetrie
    cl_2 Paroi_FT_Disc constant Champ_Front_Uniforme 1 55
    cl_3 Paroi_FT_Disc constant Champ_Front_Fonc_xyz 1 30 +100*x
}

```

The optional **maillage** block is used to specify that we want a Gnuplot drawing of the initial mesh. There is only one keyword, *niveau\_plot*, that is used only to define if a Gnuplot drawing is active (value 1) or not active (value -1). By default, skipping the block will produce non Gnuplot drawing. This option is to be used only in a debug process!

**maillage niveau\_plot -1**

The **remaillage** block is used to specify the operations that are used to keep the solid interfaces in a proper condition. The following example has been successfully used for the free surface of the stirrer simulation:

```

remaillage {
    pas 0.000001
    nb_iter_remaillage 2
    critere_arete 0.35
    critere_remaillage 0.2
    pas_lissage 0.0000001
    nb_iter_barycentrage 5
    lissage_courbure_iterations 5
    lissage_courbure_coeff -0.2
    lissage_courbure_iterations_systematique N1
    lissage_courbure_iterations_si_remaillage N2
    relax_barycentrage 1
    facteur_longueur_ideale 1
    nb_iter_correction_volume 3
    seuil_dvolume_residuel 1e-12
}

```

These parameters are described in the section following the section dedicated to the solid-fluid interface tracking equation (see paragraph 2.6.12.6).

**lissage\_courbure\_iterations\_systematique N1**  
**lissage\_courbure\_iterations\_si\_remaillage N2**

These keywords allow a finer control than the previous `lissage_courbure_iterations` keyword. N1 iterations are applied systematically at each timestep. N2 iterations are applied only if the local or the global remeshing effectively changes the lagrangian mesh connectivity. For proper DNS computation, N1 should be set to 0.

The **collisions** block is used to specify the operations that are used when a collision occurs between two parts of interfaces. When this occurs, it is necessary to build a new mesh that has locally a clear definition of what is inside and what is outside of the mesh.

```
collisions {
  active
  juric_pour_tout
  [ juric_local ] [ phase_continue 0 | 1 ]
  type_remaillage
    Juric / [Source_Isovaleur Indicatrice | Fonction_Distance] / | Thomas / [distance_interface_element_max N
  ] /
}
```

The **collisions** can either be **active** or **inactive**. If the **collisions** are **active** (highly recommended!), the keyword **juric\_pour\_tout** indicates that the Juric level-set reconstruction method will be used to re-create the new mesh after each coalescence or breakup. The next line (**type\_remaillage**) is used to state whose field will be used for the level-set computation. Main option is **Juric**, a remeshing that is compatible with parallel computing. When using **Juric** level-set remeshing, the source field (**source\_isovaleur**) that is used to compute the level-sets is then defined. It can be either the indicator function (**indicatrice**), a choice which is the default one and the most robust, or a geometrical distance computed from the mesh at the beginning of the time step (**fonction\_distance**), a choice that may be more accurate in specific situations. **Type\_remaillage Thomas** is an enhancement of the Juric global remeshing algorithm designed to compensate for mass loss during remeshing. The mesh is always reconstructed with the indicator function (not with the distance function). After having reconstructed the mesh with the Juric algorithm, the difference between the old indicator function (before remeshing) and the new indicator function is computed. The differences occurring at a distance below or equal to  $N$  elements from the interface are summed up and used to move the interface in the normal direction. The displacement of the interface is such that the volume of each phase after displacement is equal to the volume of the phase before remeshing.  $N$  (default value 1) must be smaller than **n\_iterations\_distance** (suggested value: 2).

An alternate choice for the remeshing type (**type\_remaillage**) is **collision\_seq**, which is more complex and tries to sew the two meshes that have collided, once the collision zone has been removed. This algorithm does not work in parallel computation!

**juric\_local**: triggers a new global remeshing algorithm to handle interface collisions: the connex component of interface where collisions occur is extracted and only this part will be remeshed with the global remeshing algorithm.

**phase\_continue**: specifies which phase is the continuous phase that separates connex components (for `suppression_sous_zone` and `juric_local`, and maybe other algorithms that assume a dispersed flow pattern with isolated interfaces).

The **n\_iterations\_distance** keyword is used to specify the number or iterations requested for the smoothing process of computing the field corresponding to the signed distance to the interfaces and located at the center of the Eulerian elements. This smoothing is necessary when there are more Lagrangian nodes than Eulerian two-phase cells. The number of iterations  $nb$  is an integer (typical values 2,3,...).

The **iterations\_correction\_volume** keyword is used to specify the number or iterations requested for the correction process that can be used to keep the volume of the phases constant during the transport process. The number of iterations  $nb$  is an integer (typical value: 1).

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The **volume\_impose\_phase\_1** keyword is used to specify the volume of one phase to keep the volume of the phases constant during the remeshing process. It is an alternate solution to trouble in mass conservation. This option is mainly realistic when only one inclusion of phase 1 is present in the domain. In most other situations, the **iterations\_correction\_volume** keyword seems easier to justify. The volume *volume* to be keep is in  $m^3$  and should agree with initial condition.

**Parcours\_interface** allows you to configure the algorithm that computes the surface mesh to volume mesh intersection. This algorithm has some serious trouble when the surface mesh points coincide with some faces of the volume mesh. Effects are visible on the indicator function, in VDF when a plane interface coincides with a volume mesh surface.

To overcome these problems, the keyword **correction\_parcours\_thomas** keyword can be used: it allows the algorithm to slightly move some mesh points. This algorithm, which is experimental and is NOT activated by default, triggers a correction that avoids some errors in the computation of the indicator function for surface meshes that exactly cross some eulerian mesh edges (strongly suggested !).

**injecteur\_interfaces** FILENAME : Allows to create new interfaces at some given physical times. FILENAME file must contain ascii lines like this: 1.25 1 (x-0.2)<sup>2</sup>+(y-0.52)<sup>2</sup>+(z-0.2)<sup>2</sup>-(0.052)

In this example a sphere of fluid phase 1 will be injected at time=1.25s). If the injected interface collides with an existing interface (eg, indicator function equal to injected phase at some point within the injected interface), injection is cancelled.

**suppression\_sous\_zone** SOUS\_ZONE\_NAME : As soon as an interface overlaps the specified region, the connex component of this interface is searched and destroyed and replaced by "phase\_continue".

**interpolation\_repere\_local** : Triggers a new transport algorithm for the interface: the velocity vector of lagrangian nodes is computed in the moving frame of reference of the center of each connex component, in such a way that relative displacements of nodes within a connex component of the lagrangian mesh are minimized, hence reducing the necessity of barycentering, smooting and local remeshing. Very efficient for bubbly flows.

#### 2.6.12.4 Solid-fluid interface tracking equation

To try to be clearer, the two types of interface tracking equations are explained separately even if it is actually coded in the same object (**Transport\_Interfaces\_FT\_Disc**). In this section, the case of solid-fluid interface tracking equations is described with values that have already been used successfully. However, other set of choices can probably be tried, but the results are still unknown.

When used to mimic a solid-fluid immersed boundary (**equations\_interfaces\_vitesse\_imposee** is declared in the Navier-Stokes equation), the interface tracking equation (**Transport\_Interfaces\_FT\_Disc**) has to specify the speed of displacement of the interface, initial and boundary conditions (IBC, namely Immersed Boundary Condition), remeshing parameters:

```

agit
{
    methode_transport vitesse_imposee ../.
    conditions_initiales { ../. }
    boundary_conditions { ../. }
    remaillage { ../. }
    [ interpolation_champ_face base|lineaire { } ]
    [ nombre_facettes_retenues_par_cellule integer ]
    [ type_vitesse_imposee uniforme|analytique ]
    [ n_iterations_interpolation_ibc integer ]
    [ seuil_convergence_uzawa double ]
    [ nb_iteration_max_uzawa double ]
}

```

In the case of solid-fluid interfaces, the simplest choice in the block **methode\_transport** is to use a value of **vitesse\_imposee** (imposed speed of displacement) with an analytical formula, e.g:

```
methode_transport vitesse_imposee -(z-0.1)*40. 0. (x-0.1)*40.
```

In the above example, the solid interface is rotating around a Y-axis that is centered on  $\{0.1, 0.0, 0.1\}$  and has an angular velocity of  $40 \text{ rad.s}^{-1}$ .

As it is possible to compute the total fluid torque on an interface, an alternative and more physical choice may be to add an equation that will take into account a force coming, e.g., from a magnetic coupling and a feedback force equivalent to the computed total fluid torque. This could lead to a richer description with a possible drift.

It is also possible to define the movement with a time-dependant law for the solid interface with the keywords **Position**, **Vitesse**, **Rotation** and **Derivee\_rotation** (**verification\_derivee** is a keyword to suppress, which is not recommended unless necessary, the check of consistency between  $u_g(t), v_g(t), z_g(t)$  and the time derivative of  $x_g(t), y_g(t), z_g(t)$ ).

```

Loi_horaire law
Read law
{
    Position          2|3    xg(t)  yg(t)  [zg(t)]
    Vitesse           2|3    ug(t)  vg(t)  [wg(t)]
    /Rotation         4|9    R00(t) R01(t) [R02(t)]
                        R10(t) R11(t) [R12(t)]
                        [R20(t) R21(t) R22(t)]
    Derivee_rotation  4|9    dR00(t) dR01(t) [dR02(t)]
                        dR10(t) dR11(t) [dR12(t)]
                        [dR20(t) dR21(t) dR22(t)]

    [verification_derivee 0|1]
}
agit
{
    methode_transport loi_horaire law
    conditions_initiales { ../. }
    boundary_conditions { ../. }
    remaillage { ../. }
}

```

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The keyword **conditions\_initiales** is used to define the shape of the solid interface through a mesh **fichier\_geom.**, or through the zero level-set of a **fonction**, e.g.:

```
conditions_initiales { fonction -(((x-0.1))^2+((y-0.02)/0.3)^2+((z-0.1)/0.3)^2-(0.05^2)) }
```

Positive values of the function define the solid (where the velocity field is forced equal the "vitesse\_imposee"), and negative values of the function define the fluid.

In the above example, the solid interface is an ellipsoid. The center of this ellipsoid is { 0.1, 0.02, 0.1 } and its half-axes are { 0.050, 0.015, 0.015 }.

**Fichier\_geom** uses a line (in 2d calculations) or a surface (in 3d) mesh to create the initial condition for the interfaces. The mesh can be read in a .geom file (keyword **fichier\_geom**) or in a domain previously created (keyword **nom\_domaine**, see example below). The mesh must consist in ORIENTED segments or triangle, the normal vector of the segments or triangles (using the "right hand" rule) must point to "phase 1" (opposite to "phase 0"). Remember that for the **equations\_interfaces\_vitesse\_imposee** keyword (immersed boundary condition), phase 1 is the solid where the velocity vector is forced, and phase 0 is the fluid. There is no check that the orientation is correct ! Incorrect orientation will produce a wrong computation of the indicator function near the interface. It is recommended to check the indicator function with the **lata\_dump** keyword.

The mesh must NOT cross the boundaries of the computational domaine and it must be a CLOSED surface, but not necessarily a connex surface.

You must also tell the code where is "phase 0" and where is "phase 1" initially (phases are automatically updated as the interface moves during the computation). This can be done with the two keywords **point\_phase** and **default\_phase**. The code will search in the computational domain all the connex sets of mesh elements not traversed by the interface. For each set, the user must define to which phase this set must be initialized either with **point\_phase**, or with **default\_phase**.

*This is an experimental feature. Double check the result with the **lata\_dump** keyword !*

```
conditions_initiales {
    Fichier_geom {
        fichier_geom filename.geom | nom_domaine domaine_name
        [ point_phase 0 | 1    Xcoord Ycoord [Zcoord] ]
        ...
        [ default_phase 0 | 1 ]
        [ reverse_normal ]
        [ lata_dump lata_basemane ]
    }
}
```

**fichier\_geom** *filename.geom* : Read the ascii file *filename.geom* (must be in .geom format) and use this mesh to build the interface. Use this method if the computation runs in parallel (since keyword **Read\_file** will not work).

**nom\_domaine** *domain\_name* : *domain\_name* must be a domain previously declared and filled in the .data file, usually with

```
Domaine CYLINDER
Lire_med CYLINDER filename.med
...
Fichier_geom {
    nom_domaine CYLINDER ...
}
```

**point\_phase 0 | 1** *Xcoord Ycoord [ Zcoord ]* : Tells the code that the given point (x,y,z) and the elements nearby is in the given phase (0 or 1). All elements in the same connex set of elements are given this phase number. The point must be located inside the computation domain, but not in a mesh cell crossed by the interface. You can specify several **point\_phase** directives, but only one per connex set of elements.

**default\_phase 0 | 1** : With this keyword, the given phase will be used for all connex sets of elements that do not contain a **point\_phase**. It is recommended to define a **point\_phase** for the biggest connex set of elements and a **default\_phase** for the other phase.

**reverse\_normal** : You can easily build an oriented surface mesh (for example with Salome), but it is not easy to ensure that the normal vector points to "phase 1". If, once you created the mesh, you see that the normal vector points to "phase 0", this keyword will reverse all surface mesh elements to reverse the normal vector. You must check that, after correction, the normal vector is coherent with the **point\_phase** and **default\_phase** that you give.

**lata\_dump** *lata\_basename* : Writes a lata file containing the connex set of elements (each connex set has a different number) and the indicator function. The connex component field is equal to -1 in all cells that are crossed by the surface mesh.

Use this file to

- find coordinates where you should place **point\_phase** directives,
- check that all volumes have the correct phase,
- check that the indicator function is correct in each connex set of elements and near the interface.

The **boundary\_conditions** block is used to specify boundary conditions. In the case of solid interfaces, the indicator function is only important in the vicinity of these interfaces. The keyword adapted to compute the indicator function boundary conditions in that case is **Paroi\_ft\_disc**. Two kind of boundary condition may be applied : symmetry and contact angle fixed. Symmetry is equivalent to fix an angle of 90 degrees. The angle is measured between the wall and the interface in the phase 0.

```
boundary_conditions {
  cl_1 Paroi_FT_Disc symetrie
  cl_2 Paroi_FT_Disc constant Champ_Front_Uniforme 1 55
  cl_3 Paroi_FT_Disc constant Champ_Front_Fonc_xyz 1 30 +100*x
}
```

As for fluid-fluid interfaces (**equation\_interfaces\_proprietes\_fluide**), the block **remaillage** is used to specify the operations that are used to keep the solid interfaces in a proper condition. The following example has been successfully used for the ellipsoid and its speed of displacement previously described.

```
remaillage
{
  pas 1e8
  nb_iter_remaillage 5
  critere_arete 0.5
  critere_remaillage 0.2
  pas_lissage -1
  nb_iter_barycentrage 5
  relax_barycentrage 1
  facteur_longueur_ideale 1
}
```



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**interpolation\_champ\_face base|lineaire { }** : It is possible to compute the imposed velocity for the solid-fluid interface by direct affectation (**interpolation\_scheme** would be set to **base**) or by multi-linear interpolation (**interpolation\_scheme** would be set to **lineaire**). The default value is **base**.

**nombre\_facettes\_retenues\_par\_cellule** integer : Keyword to specify the default number (3) of facets per cell used to describe the geometry of the solid-solid interface. This number should be increased if the geometry of the solid-solid interface is complex in each cell (eulerian mesh too coarse for example).

**type\_vitesse\_imposee uniforme|analytique** : Useful only with **interpolation\_champ\_face** positioned to **lineaire**. Value of the keyword is **uniforme** (for an uniform solid-fluide interface's velocity, i.e. zero for instance) or **analytique** (for an analytic expression of the solid-fluide interface's velocity depending on the spatial coordinates). The default value is **uniforme**.

**n\_iterations\_interpolation\_ibc** integer : Useful only with **interpolation\_champ\_face** positioned to **lineaire**. Set the value concerning the width of the region of the linear interpolation. For the Penalized Direct Forcing model, a value equals to 1 is enough.

**seuil\_convergence\_uzawa** double : Optional option to change the default value ( $10^{-8}$ ) of the threshold convergence for the Uzawa algorithm if used in the Penalized Direct Forcing model. Sometime, the value should be decreased to insure a better convergence to force equality between sequential and parallel results.

**nb\_iteration\_max\_uzawa** double : Optional option to change the default value (30) of the maximal number of iterations for the Uzawa algorithm if used in the Penalized Direct Forcing model. Sometime, the value should be increased to insure a better convergence to force equality between sequential and parallel results.

#### 2.6.12.5 Particle tracking equation

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```

Navier_Stokes_FT_Disc eq_hydraulique
Associate pb eq_hydraulique
Transport_Marqueur_FT particles
Associate pb particles
Read pb
{
  eq_hydraulique { ... }
  particles
  {
    boundary_conditions { }
    conditions_initiales {
      [ ensemble_points { fichier filename / sous_zones N name_zone1 distribution ... name_zoneN
distribution } ]
      [ proprietes_particules { [ fichier filename | distribution { nb_particules nb vitesse u v [w] temperature
value masse_volumique value diametre value } ] } ]
      [ t_debut_integration t_deb_integr ]
    }
    [ sources { ... , ... , ... } ]
    [ injection {
      [ ensemble_points { ... } ]
      [ proprietes_particules { ... } ]
      [ t_debut_injection t_deb_inj ]
      [ dt_injection dt_inj ]
    } ]
    [ transformation_bulles {
      localisation N name_zone1 ... name_zoneN
      diametre_min | beta_transfo diameter_size
      interface interface_name
      [ t_debut_transfo value ]
      [ dt_transfo value ]
    } ]
    [ methode_transport vitesse_interpolee | vitesse_particules ]
    [ methode_couplage suivi | one_way_coupling | two_way_coupling ]
    [ phase_marquee integer ]
    [ nb_iterations integer ]
    [ implicite 0|1 ]
    [ contribution_one_way 0|1 ]
  }
  liste_postraitements
  {
    Postraitement_ft_lata particles
    {
      ...
      champs_elements_sommets { densite_particules volume_particules }
      interfaces_particles { champs_sommets { vitesse volume diametre temperature masse_volumique }
    }
  }
}

```

Particles in a flow can be followed thanks to a **Transport\_Marqueur\_FT** equation.

The **boundary\_conditions** { } block should be left empty cause the boundary conditions for this equation (and used to give the behaviour of the particles velocities at the boudaries) are the same than the boundary conditions of the hydraulic equation.

The initial conditions (**conditions\_initiales** keyword) define the initial state of the particules. The initial locations are defined with the keyword **ensemble\_points**, either thanks to a file (keyword **fichier**) or with sub-zones (keyword **sous\_zones**). In the first case, the format of the file *filename* is:

```

2
nb dimension          where nb is the number of particles and dimension is 2 or 3
nb_values             where nb_values equals to nb*dimension
x1 y1 [z1]           where xi, yi and zi in 3D are the coordinates of ith particle
..
xnb ynb [znb]
```

In the case of a location per sub-zones, the distribution of the particles can be randomized with nb the number of particles:

*name\_zone* **aleatoire** nb

Or uniform with nbX, nbY and nbZ the number of particles in each direction :

*name\_zone* **uniforme** nbX nbY [ nbZ ]

The **proprietes\_particules** gives the particles properties. If the properties are non uniform, they can be read in a file with the keyword **fichier**. The format of the *filename* file is:

```

2
nb dimension          where nb is the number of particles and dimension is 2 or 3
nb_values             where nb_values equals to nb*dimension
u1 v1 [w1]           where ui, vi and wi in 3D are the initial velocity of ith particle
...
unb vnb [wnb]
2
nb 1
nb                   where nb is the number of particles
T1                   where Ti is the initial temperature of ith particle
...
Tnb
2
nb 1
nb                   where nb is the number of particles
Rho1                 where Rhoi is the initial density of ith particle
...
Rhonb
2
nb 1
nb                   where nb is the number of particles
D1                   where Di is the initial diameter of ith particle
...
Dnb
```

In the case of uniform properties for each particles, they can be given by the keyword **distribution** with:

**nb\_particules** nb : the number of particles

**vitesse** u v [w] : the velocity of all the particles

**temperature** value : the value of the temperature for all the particles

**masse\_volumique** value : the value of the density for all the particles

**diametre** value : the value of the diameter for all the particles

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The beginning time for the calculation of the particles trajectories is given by the keyword **t\_debut\_integration**. By default, it is the value given in the time scheme with the keyword **tinit**. Before this time **t\_deb\_integr**, the particles do not move.

The **sources** terms available for this equation are: **trainee** (drag effect), **flottabilite** (buoyancy effect), **masse\_ajoutee** (weight added effect), **portance** (lift effect). The last one is not available yet.

The keyword **injection** can be used to inject periodically during the calculation some other particles. The syntax for **ensemble\_points** and **proprietes\_particles** is the same than the initial conditions for the particles. The keyword **t\_debut\_injection** give the injection initial time (by default, given by **t\_debut\_integration**) and **dt\_injection** gives the injection time period (by default given by **dt\_min**).

The keyword **transformation\_bulles** will activate the transformation of an inclusion (small bubbles) into a particle. **localisation** gives the sub-zones (N number of sub-zones and their names) where the transformation may happen. The diameter size for the inclusion transformation is given by either **diameter\_min** option, in this case the inclusion will be suppressed for a diameter less than *diameter\_size*, either by the **beta\_transfo** option, in this case the inclusion will be suppressed for a diameter less than *diameter\_size*\*cell\_volume (cell\_volume is the volume of the cell containing the inclusion). **interface** specifies the name of the inclusion interface and **t\_debut\_transfo** is the beginning time for the inclusion transformation operation (by default, it is **t\_debut\_integr** value) and **dt\_transfo** is the period transformation (by default, it is **dt\_min** value). In a two phase flow calculation, the particles will be suppressed when entering into the non marked phase (see below):

Other options for the particles:

**methode\_transport** : Kind of transport method for the particles. With **vitesse\_interpolee**, the velocity of the particles is the velocity a fluid interpolation velocity (option by default). With **vitesse\_particules**, the velocity of the particles is governed by the resolution of a momentum equation for the particles.

**methode\_couplage** : Way of coupling between the fluid and the particles. By default, (keyword **suivi**), there is no interaction between both. With **one\_way\_coupling** keyword, the fluid act on the particles. With **two\_way\_coupling** keyword, besides, particles act on the fluid.

**phase\_marquee** integer : Phase number giving the marked phase, where the particles are located (when they leave this phase, they are suppressed). By default, for a the two phase fluide, the particles are supposed to be into the phase 0 (liquid).

**nb\_iterations** integer : Number of sub-timesteps to solve the momentum equation for the particles (1 per default).

**implicite** 0|1 : Impliciting (1) or not (0) the time scheme when weight added source term is used in the momentum equation

**contribution\_one\_way** 0|1: Activate (1, default) or not (0) the fluid forces on the particles when **one\_way\_coupling** or **two\_way\_coupling** coupling method is used.

To post process the location of the particles in the flow, either a volume field for density particles (**densite\_particules**) and volume particles (**volume\_particles**) or point mesh (**interfaces**) visualization can be used but only with the LATA format (and VisIt) for the last one.

## 2.6.12.6 Remeshing

The **remaillage** block only contains parameter's values. These parameters are also described in the document (in French) written by C. Poyet: *Paramètres de transport et de remaillage de l'interface Front-Tracking-Discontinu Version 1.4.7 et patches*, Août 2005.

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```

remaillage {
    pas ../..
    pas_lissage ../..
    nb_iter_remaillage ../..
    nb_iter_barycentrage ../..
    relax_barycentrage ../..
    critere_arete ../..
    critere_remaillage ../..
    impr ../..
    facteur_longueur_ideale ../..
    nb_iter_correction_volume ../..
    seuil_dvolume_residuel ../..
    lissage_courbure_coeff ../..
    lissage_courbure_iterations ../..
    critere_longueur_fixe ../..
}

```

An example of values of these parameters is given in the section "The fluid-fluid interface tracking equation", in the paragraph dedicated to the remeshing keyword (**remaillage**).

The keyword **pas** has default value  $-1$ .; when **pas** is set to a negative value there is no remeshing. It is the time step in second (physical time) between two operations of remeshing.

The keyword **pas\_lissage** has a default value set to  $-1$ .; when **pas\_lissage** is set to a negative value there is no smoothing of mesh. It is the time step in second (physical time) between two operations of smoothing of the mesh.

The keyword **nb\_iter\_remaillage** has a default value set to  $0$ ; when **nb\_iter\_remaillage** is set to the zero value there is no remeshing. It is the number of iterations performed during a remeshing process.

The keyword **nb\_iter\_barycentrage** has a default value set to  $0$ ; when **nb\_iter\_barycentrage** is set to the zero value there is no operation of "barycentrage". The "barycentrage" operation consists in moving each node of the mesh tangentially to the mesh surface and in a direction that let it closer the center of gravity of its neighbors. If **relax\_barycentrage** is set to  $1$ , the node is move to the center of gravity. For values lower than unity, the motion is limited to the corresponding fraction. The parameter **nb\_iter\_barycentrage** is the number of iteration of these node displacements.

The keyword **relax\_barycentrage** has a default value set to  $0$ ; when **relax\_barycentrage** is set to the zero value there is no motion of the nodes. When  $0 < \text{relax\_barycentrage} \leq 1$ , this parameter provides the relaxation ratio to be used in the "barycentrage" operation described for the keyword **nb\_iter\_barycentrage**.

The keyword **critere\_arete** is used to compute two sub-criteria: the minimum and the maximum edge length ratios used in the process of obtaining edges of length close to **critere\_longueur\_fixe**. Their respective values are set to  $(1 - \text{critere\_arete})^2$  and  $(1 + \text{critere\_arete})^2$ . The default values of the minimum and the maximum are set respectively to  $0.5$  and  $1.5$ . When an edge is longer than  $\text{critere\_longueur\_fixe} * (1 + \text{critere\_arete})^2$ , the edge is cut into two pieces; when its length is smaller than  $\text{critere\_longueur\_fixe} * (1 - \text{critere\_arete})^2$ , this edge has to be suppressed.

The keyword **critere\_remaillage** was previously used to compute two sub-criteria: the minimum and the maximum length used in the process of remeshing. Their respective values are set to  $(1 - \text{critere\_remaillage})^2$  and  $(1 + \text{critere\_remaillage})^2$ . The default values of the minimum and the maximum are set respectively to  $0.2$  and  $1.7$ . There are currently not used in data files.

The keyword **impr** is followed by a value that specify the printing time period given. The default value is  $-1$ , which means no printing.

The keyword **facteur\_longueur\_ideale** is used to set a ratio between edge length and the cube root of volume cell for the remeshing process. The default value is *1.0*.

The keyword **nb\_iter\_correction\_volume** give the maximum number of iterations to be performed trying to satisfy the criterion **seuil\_dvolume\_residuel**. The default value is *0*, which means no iteration.

The keyword **seuil\_dvolume\_residuel** give the error volume (in m<sup>3</sup>) that is accepted to stop the iterations performed to keep the volume constant during the remeshing process. The default value is *0.0*.

The keyword **lissage\_courbure\_coeff** is used to specify the diffusion coefficient used in the diffusion process of the curvature in the curvature smoothing process with a time step. The default value is *0.05*. That value usually provides a stable process. Too small values do not stabilize enough the interface, especially with several Lagrangian nodes per Eulerian cell. Too high values induce an additional macroscopic smoothing of the interface that should physically come from the surface tension and not from this numerical smoothing.

The keyword **lissage\_courbure\_iterations** is used to specify the number of iterations to perform the curvature smoothing process. The default value is *1*.

The keyword **critere\_longueur\_fixe** is used to specify the ideal edge length for a remeshing process. The default value is *-1.*, which means that the remeshing does not try to have all edge lengths to tend towards a given value.

## 2.6.12.7 Concentration equation on a two phase-flow with interface tracking

The **Convection\_diffusion\_concentration\_ft\_disc** allows to take into account the interface and prevents the scalar from diffusing through the interface.

```

Probleme_FT_Disc_gen pb
Convection_diffusion_concentration_FT_disc concentration_equation
Associate pb concentration_equation
...
Read pb
{
  ...
  concentration_equation
  {
    ... (parameters for the classic Convection_Diffusion_Concentration, see 2.6.5)
    equation_interface eq_name
    phase 0 | 1
    option RIEN | RAMASSE_MIETTES_SIMPLE
    constante_cinetique VAL
    equations_source_chimie N EQ_NAME_1 ... EQ_NAME_N
    constante_cinetique_nu_t VAL
    equation_nu_t EQ_NAME
  }
}

```

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```

zone_sortie SOUS_ZONE_NAME
[ Sources { Source_Constituant_Vortex { ... } } ]
}

```

**equation\_interface:** this is the name of the interface tracking equation to watch. The scalar will not diffuse through the interface of this equation.

**phase 0|1:** tells whether the scalar must be confined in phase 0 or in phase 1

**option:** Experimental features used to prevent the concentration to leak through the interface between phases due to numerical diffusion.

**RIEN:** do nothing

**RAMASSE\_MIETTES\_SIMPLE:** at each timestep, this algorithm takes all the mass located in the opposite phase and spreads it uniformly in the given phase.

**constante\_cinetique** VAL : experimental, documentation to be written

**equations\_source\_chimie** N EQ\_NAME\_1 ... EQ\_NAME\_N : experimental, documentation to be written

**constante\_cinetique\_nu\_t** VAL : experimental, documentation to be written

**equation\_nu\_t** EQ\_NAME : experimental, documentation to be written

**zone\_sortie** SOUS\_ZONE\_NAME : artificial source term that drops the concentration to zero within the specified sub-zone (see file \_bilan.out below)

Available source term for Convection\_Diffusion\_Concentration\_FT\_Disc :

```

Source_Constituant_Vortex
{
  rayon_spot RADIUS
  integrale INTEGRAL
  debit FLOW
  senseur_interface {
    equation_interface EQ_NAME
    segment_senseur_1 DIM CoordX CoordY [ CoordZ ]
    segment_senseur_2 DIM CoordX CoordY [ CoordZ ]
    nb_points_tests N_POINTS
  }
  delta_spot DIM Dx Dy [ Dz ]

```

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```
}

```

This is a dynamic source term of concentration designed to simulate injection at a free surface: injects a gaussian spot of concentration of given INTEGRAL value (INTEGRAL is a flux, the integral of the source term injected during a timestep is INTEGRAL multiplied by the time step). RADIUS characterizes the radius of the gaussian spot. FLOW is the fluid flow injected in the Navier-Stokes equation (equal to the integral of a source of divergence velocity) in m3/s. **senseur\_interface** describes a sensor to tell where the injection will take place. EQ\_NAME is the name of an interface tracking equation (describes the free surface). **segment\_senseur\_1** and **segment\_senseur\_2** describe a segment that crosses the interface. The position of the free surface will be checked on N\_POINTS points on this segment starting from **segment\_senseur\_1**. If a phase interface is found, the position of the injected spot will be located at this position, plus the **delta\_spot** vector. For proper conservation of the injected species, the **delta\_spot** vector should direct the injection at least at RADIUS distance below the free surface.

Notice: the source term will be taken into account by the **Navier\_Stokes\_FT\_Disc** equation to modify the divergence of the velocity at the injection point only if **equation\_concentration\_source\_vortex** N EQ1 ... EQN keyword is also added to the Navier\_Stokes equation. EQ1..EQN are the names of the concentration equations containing source terms of velocity divergence.

Content of the file *EQ\_NAME\_bilan.out* created when using this equation : every timestep, it writes one line:

column 1: time

column 2: integral of concentration in phase 0

column 3: integral of concentration in phase 1

column 4: integral of zone\_sortie source term during the timestep

column 5: equal to column 4 divided by timestep (eg flux of concentration)

#### 2.6.12.8 Temperature equation on a single phase flow with interface tracking

The **Convection\_diffusion\_temperature** is the keyword to add the temperature equation for a single phase flow with solid-fluid interfaces for example.

```
Probleme_FT_Disc_gen pb
Convection_diffusion_temperature temperature_equation
Associate pb temperature_equation
...
```



```

Read pb {
  ...
  temperature_equation
  {
    ... (parameters for the classic Convection_Diffusion_Temperature)
    [ penalisation_L2_FTD { solid_fluid_interface_name1 1 specified_temperature
                           solid_fluid_interface_name2 1 specified_temperature ... } ]
  }
}

```

The optional keyword **penalisation\_L2\_FTD** is to activate or not (the default is Direct Forcing method) the Penalized Direct Forcing method to impose the specified temperature on the solid-fluid interface.

### 2.6.12.9 Temperature equation on a two-phase flow with interface tracking

The **Convection\_diffusion\_temperature\_ft\_disc** is the keyword (**Convection\_diffusion\_temperature** will return an error) to add the temperature equation for one phase of a front tracking calculation (temperature values for the other phase will not be realistic). A model with two temperature equations (one for each phase will be introduced in future releases). Furthermore, the temperature of the other phase will be set to the saturation temperature, and is a constant (0°C) for the moment.

```

Probleme_FT_Disc_gen pb
Convection_diffusion_temperature_FT_Disc temperature_equation
Associate pb temperature_equation
...
Read pb {
  ...
  temperature_equation
  {
    ... (parameters for the classic Convection_Diffusion_Temperature)
    equation_navier_stokes name
    equation_interface name
    phase 0 | 1
    stencil_width N
    [ maintien_temperature SOUS_ZONE_NAME VALUE ]
  }
}

```

```

}
}

```

**equation\_navier\_stokes** name : The name of the Navier Stokes equation of the problem should be given.

**equation\_interface** name : The name of the interface equation should be given.

**phase** 0 | 1 : Phase in which the temperature equation will be solved. The temperature, which may be postprocessed with the keyword **temperature\_EquationName**, in the orther phase may be negative: the code only computes the temperature field in the specified phase. The other phase is supposed to physically stay at saturation temperature. The code uses a ghost fluid numerical method to work on a smooth temperature field at the interface. In the opposite phase (1-X) the temperature will therefore be extrapolated in the vicinity of the interface and have the opposite sign, saturation temperature is zero by convention).

**stencil\_witdth** N : distance in mesh elements over which the temperature field should be extrapolated in the opposite phase.

**maintien\_temperature** SOUS\_ZONE\_NAME VALUE : experimental, this acts as a dynamic source term that heats or cools the fluid to maintain the average temperature to VALUE within the specified region. At this time, this is done by multiplying the temperature within the SOUS\_ZONE by an appropriate uniform value at each timestep. This feature might be implemented in a separate source term in the future.

#### 2.6.12.10 Post processing

The block **liste\_postraitements** defines the output files to be written during the computation. The output format is **lata** in order to use OpenDX to draw the results. The block **liste\_postraitements** can be divided in one or several sub-blocks that can be written at different frequencies and in different directories. Attention! The directory **lata** used in this example should be created before running the computation or the **lata** files will be lost!

The general structure of the **liste\_postraitements** block is:

```

liste_postraitements
{
    Postraitement_ft_lata post1 { ../.. }
    Postraitement_ft_lata post2 { ../.. }
    ...
}

```

Each **Postraitement\_ft\_lata** has the same general structure:

```

Postraitement_ft_lata post1
{
    dt_post string
    [nom_fichier lata/post]
    [format format]
    [fichiers_multiples]
    champs location { fields_list }
    interfaces interf { champs location { fields_list } }
    skip_header
    print
}

```

The option **dt\_post** is the same than the **Champs** option **dt\_post** defined at the paragraph 2.19.4.

The optional keyword **nom\_fichier** is used to specify the sub-directory and the root of all the post-processing files. The default value is the name of the data file.

In the example, the code will write all files in a subdirectory named *lata* that should be in the directory of the data file. All files will have the prefix *post1*. For instance, the initial interface will be post-processed in the file *post1.lata.INDICATRICE\_INTERF.I.ELEM.DOM.pb.0.000000*, the interface at the first time step could be *post1.lata.INDICATRICE\_INTERF.I.ELEM.DOM.pb.0.010000*, and so on.

The optional keyword **format** can be followed (*format*) by either **binaire** or **ascii**. The first choice is more compact and is actually dedicated to using OpenDX, whereas the second one can be browsed with any textbrowser. The default value is **ascii**.

The optional keyword **fichiers\_multiples** is used in parallel computing to split the post-processing into one file for each processor. When this keyword is not present (default), a single file is constructed by collecting data from all the cpus.

The keyword **champs** can be followed (*location*) by either **sommets**, **elements** or **faces**, and a list of fields (*fields\_list*) to be post-processed in these positions. Of course, this means that the field values are to be post-processed respectively at the summits, the center of the volume elements or the faces of the elements. When the field is not stored in these positions, the post-processed values are interpolated within the closest neighbors. Example, for the pressure and velocity: **champs sommets { pression vitesse }**

A special case concerns the indicator functions. To be able to deal with data files that involve more than one interface, a suffix is used to specify which couple {interface, indicator function} is concerned. The suffix is the name of the interface (**Transport\_Interfaces\_FT\_Disc**) declared in the problem description. The suffix is concatenated with the **indatrice\_**. E.g:

```

champs elements
{
    indatrice_interf
    indatrice_agit
    pression
    concentration
}

```

The keyword **interfaces** is followed by the name of an interface (**Transport\_Interfaces\_FT\_Disc**). In the block under brackets, are defined the fields to be post-processed on the interfaces. E.g:

```

interfaces interf { champs sommets { courbure } }

```

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From the structure of the code, the *location* of the post-processing on interfaces can either be on **sommets** (nodes of the Lagrangian mesh), or on **elements** (center of the triangles of the Lagrangian mesh).

Today, these features are still limited to two physical quantities that can be processed on the **sommets** of the interfaces: **courbure** (curvature) and **vitesse** (speed of displacement). Additional integer parameters may be post-processed, mainly for debugging or to illustrate the parallel computing by domain decomposition: **pe** (index of the processor that is responsible of this part of the interface at the current time step), **pe\_local** (index of the processor that is currently writing the information on this part of the interface at the current time step) and **numero** (index of the part of the interface in the table of the current processor).

The keyword **skip\_header** is used to prevent the post-processing to write header in each file. This can be used in case of restart of a computation or when the post-processing is written in a file created by another post-processing.

The keyword **print** is used to enable the printing of post-processing comments in the *err* file.

The following example has been used to deal with two different interfaces (*interf* and *agit*) in the stirrer and free surface simulation. *interf* corresponds to the free surface whereas *agit* corresponds to the stirrer solid-fluid interface:

```

liste_postraitements
{
    Postraitement_ft_lata post1
    {
        dt_post 0.01
        nom_fichier lata/post1
        format binaire
        print
        champs sommets { vitesse }
        champs elements {
            distance_interface_elem_interf
            distance_interface_elem_agit
            indicatrice_interf
            concentration }
        interfaces interf { champs sommets { courbure } }
    }
    Postraitement_ft_lata post2
    {
        dt_post 0.01
        nom_fichier lata/post2
        format binaire
        print
        interfaces agit { champs sommets { pe } }
    }
}

```

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## 2.6.13 PHASE FIELD PROBLEM

Complete description of the Phase Field model for incompressible and immiscible fluids can be found into this PDF file: \$TRIO\_U\_ROOT/doc/Trio\_U/phase\_field\_non\_miscible\_manuel.pdf

```

Read pb {
  Navier_Stokes_Phase_Field {
    Solveur_Pression ...
    Convection { ... }
    Approximation_de_Boussinesq oui|non
    Viscosite_dynamique_constante oui|non
    Diffusion { ... }
    Sources { Source_Qdm_Phase_Field { Forme_du_terme_source integer }
    Gravite n x y [z]
    Conditions_initiales { ... }
    boundary_conditions { ... }
  }
  Convection_Diffusion_Phase_Field {
    Convection { ... }
    Diffusion { ... }
    Sources { Source_Con_Phase_Field {
      Temps_d_affichage value
      Alpha value Beta value
      Kappa value Kappa_variable oui|non
      Moyenne_de_kappa string
      Multiplicateur_de_kappa value
      Couplage_NS_CH string
      Implicitation_CH oui|non
      Gmres_non_lineaire oui|non
      Seuil_cv_iterations_ptfixe value Seuil_residu_ptfixe value
      Seuil_residu_gmresnl value
      Dimension_espace_de_krylov integer
      Nb_iterations_gmresnl integer
      Residu_min_gmresnl value Residu_max_gmresnl value
    }
  }
  mu_1 value mu_2 value rho_1 value rho_2 value
  Potentiel_chimique_generalise string
  boundary_conditions { ... }
  Conditions_initiales { Concentration ... }
}
Postraitement { Champs dt_post value {
  Concentration
  Potentiel_chimique_generalise ... } }
}

```

**Navier\_Stokes\_Phase\_Field** : Keyword to define the Navier Stokes equation for the Phase Field problem.

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**Approximation\_de\_Boussinesq** oui|non : To use or not the Boussinesq approximation.

**Viscosite\_dynamique\_constante** oui|non : To use or not a viscosity which will depends on "concentration" C (in fact, C is the unknown of Cahn-Hilliard equation).

**Gravite** n x y [z] : Keyword to define gravity in the case Boussinesq approximation is not used.

**Source\_Qdm\_Phase\_Field** { **forme\_du\_terme\_source** integer } : Keyword to define the capillary force into the Navier Stokes equation for the Phase Field problem. The kind of the source term is given by integer (1,2,3 or 4).

**Convection\_Diffusion\_Phase\_Field**: Keyword to define the Cahn-Hilliard equation of the Phase Field problem. The unknown of this equation is the "concentration" C.

**Source\_Con\_Phase\_Field** : Keyword to define the source term of the Cahn-Hilliard equation.

**Temps\_d\_affichage** value : Time during the characteristics of the problem are shown before calculation.

**Alpha** value : To define the internal capillary coefficient  $\alpha$

**Beta** value : To define the parameter  $\beta$  of the model

**Kappa** value : To define the mobility coefficient  $\kappa_0$

**Kappa\_variable** oui|non : To define a mobility which depends on "concentration" C

**Moyenne\_de\_kappa** string : To define how mobility  $\kappa$  is calculated on faces of the mesh according to cell-centered values (string is arithmetique|harmonique|geometrique)

**Multiplicateur\_de\_kappa** value : To define the the parameter a of the mobility expression when mobility depends on C.

**Couplage\_NS\_CH** string : Evaluating time choosen for the term source calculation into the Navier Stokes equation (string is mutilde(n+1/2)|mutilde(n), in order to be conservative, the first choice seems better)

**Implicitation\_CH** oui|non : To define if the Cahn-Hilliard will be solved using a implicit algorithm or not

**Gmres\_non\_lineaire** oui|non : To define the algorithm to solve Cahn-Hilliard equation:(oui: Newton-Krylov method, non: fixed point method)

To define options of the fixed point method:

**Seuil\_cv\_iterations\_ptfixe** value : the convergence threshold

**Seuil\_residu\_ptfixe** value : the threshold for the matrix inversion used in the method

To define options of the Newton-Krylov method:

**Seuil\_residu\_gmresnl** value : the convergence threshold

**Dimension\_espace\_de\_krylov** integer : the vector numbers used in the method

**Nb\_iterations\_gmresnl** integer : the maximal iterations

**Residu\_min\_gmresnl** value : the minimal convergence threshold

**Residu\_max\_gmresnl** value : the maximal convergence threshold

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**mu\_1** value : To define the dynamic viscosity of the first phase

**mu\_2** value : To define the dynamic viscosity of the second phase

**rho\_1** value : To define the density of the first phase

**rho\_2** value : To define the density of the second phase

**Potentiel\_chimique\_generalise** string : To define (string set to avec\_energie\_cinetique) or not (string set to sans\_energie\_cinetique) if the Cahn-Hilliard equation contains the cinetic energy term

**Concentration** : Keyword to postprocess the unknown C of the Cahn-Hilliard equation

**Potentiel\_chimique\_generalise** : Keyword to postprocess the field mutilde

**2.6.14PROBLEM WITH PASSIVE SCALARS**





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*Problem pb*

```
Read pb {
  Navier_Stokes_Standard { ... }
  Convection_Diffusion_Temperature
  {
    Convection { ... }
    Diffusion { ... }
    Sources { ... }
    boundary_conditions { ... }
    Conditions_initiales { temperature ... }
  }
  Equations_Scalaires_Passifs
  {
    Convection_Diffusion_Temperature
    {
      Convection { ... }
      Diffusion { ... }
      Sources { ... }
      boundary_conditions { ... }
      Conditions_initiales { temperature0 ... }
    }
    Convection_Diffusion_Temperature
    {
      Convection { ... }
      Diffusion { ... }
      Sources { ... }
      boundary_conditions { ... }
      Conditions_initiales { temperature1 ... }
    }
    Convection_Diffusion_Temperature
    {
      Convection { ... }
      Diffusion { ... }
      Sources { ... }
      boundary_conditions { ... }
      Conditions_initiales { temperature2 ... }
    }
    ....
  }
  Postraitement {
    Champs dt_post value
    {
      Temperature
      Temperature0
      Temperature1
      Temperature2
      ...
    }
  }
}
```

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*Problem* is a keyword to create a classical problem with a scalar transport equation (e.g: temperature or concentration) and an additional set of passive scalars (e.g: temperature or concentration) equations. The list of keywords available for *Problem* are :

**Pb\_Hydraulique\_Concentration\_Scalaires\_Passifs**

**Pb\_Hydraulique\_Concentration\_Turbulent\_Scalaires\_Passifs**

**Pb\_Thermohydraulique\_Scalaires\_Passifs**

**Pb\_Thermohydraulique\_Turbulent\_Scalaires\_Passifs**

**Pb\_Thermohydraulique\_Concentration\_Scalaires\_Passifs**

**Pb\_Thermohydraulique\_Concentration\_Turbulent\_Scalaires\_Passifs**

**Pb\_Thermohydraulique\_QC\_fraction\_massique\***

**Pb\_Thermohydraulique\_Turbulent\_QC\_fraction\_massique\***

...

\* For these two last problems, hydraulic and energy equations are solved and a list of passive scalar equations may be added.

The unknowns of the passive scalar equation number N are named **temperatureN** or **concentrationN** or **fraction\_massiqueN**. This keyword is used to define initial conditions and the post processing fields. This kind of problem is very useful to test in only one data file (and then only one calculation) different schemes or different boundary conditions for the scalar transport equation.

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## 2.6.15 PROBLEM WITH TRANSPORT OF CHEMICAL SPECIES

```

Probleme_FT_Disc_gen pb
Chimie model
Read model {
  Reactions {
    {
      reactifs formulae
      produits formulae
      constante_taux_reaction double
      [ contre_reaction double ]
      coefficients_activites { Specie1,1 double ... SpecieN1,1 double }
      enthalpie_reaction 0
    },
    ....
    {
      reactifs formulae
      produits formulae
      constante_taux_reaction double
      [ contre_reaction double ]
      coefficients_activites { Specie1,R double ... SpecieNR,R double }
      enthalpie_reaction 0
    }
  }
  [ modele_micro_melange 0|1 ]
  [ constante_modele_micro_melange double ]
  [ espece_en_competition_micro_melange specie ]
}
Associate pb model
Convection_Diffusion_Concentration Specie1
.....
Convection_Diffusion_Concentration SpecieN
Read pb {
  ...
  Specie1
  {
    diffusion { }
    convection { ... }
    nom_inconnue Specie1
    boundary_conditions { ... }
    conditions_initiales { Specie1 ... }
    masse_molaire double
  }
  ...
  SpecieN {
    ....
  }
}

```

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The keyword **Chimie** is used to define the list of reactions thanks to the keyword **Reactions**. In each reaction  $r$  ( $r=1$  to  $R$ ) where  $N_r$  species are used, the following keywords are defined:

- the reactant species (**reactifs** keyword) and their stoichiometric coefficients defined in a formulae, for example  $6*H_p+5*I_m+IO_{3m}$  where  $H_p$ ,  $I_m$  and  $IO_{3m}$  are 3 species
- the product species (**produits** keyword) and their stoichiometric coefficients defined in a formulae, for example  $3*I_2+3*H_2O$  where  $I_2$  and  $H_2O$  are 2 other species
- the forward rate constant for the reaction (**constante\_taux\_reaction** keyword in  $[s^{-1}]$ )  $k_{f,r}$
- the optional equilibrium constant  $K_r=k_{b,r}/k_{f,r}$  (with  $k_{b,r}$  the backward rate constant for the reaction  $[s^{-1}]$ ), defined by the **contre\_reaction** keyword. This should be used for a reversible reaction (by default, it is a non-reversible reaction with  $K_r=0$ )
- the rate exponent  $A_{j,r}$  for each specie  $j$  in the reaction (**coefficients\_activites** keyword)
- the enthalpy generated by the reaction (**enthalpie\_reaction** keyword). For the moment, only 0 for **enthalpie\_reaction** value is possible, that means there is no heat source term into the energy equation caused by the species reaction.

The kinetic of the reaction  $r$  is defined by:  $\omega_r = k_{f,r} \left( \prod_{j=1}^{N_r} [C_{j,r}]^{A_{j,r}} \right) - K_r \left( \prod_{j=1}^{N_r} [C_{j,r}]^{A_{j,r}} \right)$  where  $C_{j,r}$

is the species molar concentration of the reaction.

A turbulent micromixing model can also be activated to change the kinetic, several optional keywords are available :

**modele\_micro\_melange** 1 : activate the model (by default 0)

**constante\_modele\_micro\_melange** double : specify the constant of the model

**espece\_en\_competition\_micro\_melange** specie : keyword to exclude a specie from

To know more on this micromixing model which, one will look at the \$TRIO\_U\_ROOT/ThHyd/Chimie/Chimie.cpp source file.

The transport of the chemical species are then specified by the **Convection\_Diffusion\_Concentration** keyword for the  $N$  species. **Nom\_inconnue** defines the name of the field concentration and **masse\_molaire** the molar mass for the transported specie.

*Example:*

**Read** la\_chimie

{

**modele\_micro\_melange** 1

**constante\_modele\_micro\_melange** 1e-5

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## reactions

```

{
  {
    reactifs H2BO3m+Hp
    produits H3BO3
    constante_taux_reaction 1.e11
    coefficients_activites { H2BO3m 1 Hp 1 }
    enthalpie_reaction 0.
  },
  {
    reactifs 6*Hp+5*Im+IO3m
    produits 3*I2+3*H2O
    constante_taux_reaction 5.8e7
    coefficients_activites { Hp 2 Im 2 IO3m 1 }
    enthalpie_reaction 0.
  },
  {
    reactifs Im+I2
    produits I3m
    constante_taux_reaction 5.6e9
    contre_reaction 786.
    coefficients_activites { Im 1 I2 1 I3m 1 }
    enthalpie_reaction 0.
  }
}

```

## 2.7 COUPLINGS

**Probleme\_Couple** *nom\_pb\_couple*

This instruction causes a **Probleme\_Couple** type object to be created. This type of object has an associated problem list, that is, the coupling of n problems among them may be processed. Coupling between these problems is carried out explicitly via conditions at particular contact limits.

Each problem may be associated either with the **Associate** keyword or with the **Read /groupes** keywords:

**Probleme\_Couple** pbc

**Associate** pbc pb1

**Associate** pbc pb2

**Associate** pbc pb3

**Associate** pbc pb4

Or:

**Probleme\_Couple** pbc

**Read** pbc { **groupes** { { pb1 , pb2 } , { pb3 , pb4 } } }

The difference is that in the first case, the four problems exchange values then calculate their timestep, rather in the second case, the same strategy is used for all the problems listed inside one group, but the second group of problem exchange values with the first group of problems after the first group did its timestep. So, the first case may then also be written like this:

**Probleme\_Couple** pbc

**Read** pbc { **groupes** { { pb1 , pb2 , pb3 , pb4 } } }

There is a physical medium per problem (however, the same physical medium could be common to several problems). Each problem is resolved in a domain.

**Warning :** Presently, coupling requires coincident meshes. In case of non-coincident meshes, boundary condition "**paroi\_contact**" in VEF returns error message (see **paroi\_contact** for correcting procedure).

## 2.7.1 THERMOHYDRAULIC RADIATION COUPLING

```

Pb_Thermohydraulique Pb_fluide
Pb_Conduction Pb_solide
Pb_Couple_Rayonnement Pb_couple
...
Modele_Rayonnement_Milieu_Transparent mod
Read mod {
    nom_pb_rayonnant      problem_name
    fichier_fij           file_name
    fichier_face_rayo      file_name
    [fichier_matrice | fichier_matrice_binaire file_name]
}

Associate pb_couple mod

Read pb_fluide { ... }
Read pb_solide { ... }
...
Solve pb_couple

```

**Pb\_Couple\_Rayonnement:** This keyword is used to define a problem coupling several other problems to which radiation coupling is added.

**Modele\_Rayonnement\_Milieu\_Transparent *mod*:** This refers to the keyword and name of the wall thermal radiation model for a transparent gas and resolving a radiation-conduction-thermohydraulics coupled problem in VDF or VEF.

**Read *mod*:** Keyword to read the *mod* radiation model. The syntax of this radiation model has changed for the 1.5.6 version. Previous syntax is still recognized. Here is the new one:

**nom\_pb\_rayonnant** *problem\_name* : *problem\_name* is the name of the radiating fluid problem

**fichier\_fij** *file\_name* : *file\_name* is the name of the file which contains the shape factor matrix between all the faces.

**fichier\_face\_rayo** *file\_name* : *file\_name* is the name of the file which contains the radiating faces characteristics (area, emission value ...)

**fichier\_matrice|fichier\_matrice\_binaire** *file\_name* : *file\_name* is the name of the ASCII (or binary) file which contains the inverted shape factor matrix. It is an optional keyword, if not defined, the inverted shape factor matrix will be calculated and written in a file.

The two first files can be generated by a preprocessor, they allow the radiating face characteristics to be entered (set of faces considered to be uniform with respect to radiation for emission value, flux, etc.) and the form factors for these various faces. These files have the following format:

File on radiating faces:

N M	-> N nombre de faces rayonnantes (=bords) et (N is the number of radiating faces (=edges) and -> M nombre de faces rayonnantes a emissivité non nulle M equals the number of non-zero emission radiating faces
Nom(i) S(i) E(i)	-> Nom du bord i, surface du bord i, valeur de (Name of the edge i, surface area of the edge i) -> l'émissivité (comprise entre 0 et 1) (emission value (between 0 and 1))

Exemple:

```

13 4
Gauche 50.0 0.0
Droit1 50.0 0.5
Bas 10.0 0.0
Haut 10.0 0.0
Arriere 5.0 0.0
Avant 5.0 0.0
Droit2 30.0 0.5
Bas1 40.0 0.0
Haut1 20.0 0.0
Avant1 20.0 0.0
Arriere1 20.0 0.0
Entree 20.0 0.5
Sortie 20.0 0.5

```

File on form factors:

N	-> Nombre de faces rayonnantes (Number of radiating faces)
Fij	-> Matrice des facteurs de formes avec i,j entre 1 et N (Matrix of form factors where i, j between 1 and N)

Exemple:

```

13
1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.24 0.20 0.10 0.10 0.10 0.10 0.16
0.00 0.00 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.40 0.00 0.00 0.00 0.00 0.00 0.20 0.10 0.10 0.10 0.10 0.00
0.00 0.25 0.00 0.00 0.00 0.00 0.15 0.00 0.15 0.10 0.10 0.15 0.10
0.00 0.25 0.00 0.00 0.00 0.00 0.15 0.30 0.00 0.10 0.10 0.00 0.10
0.00 0.25 0.00 0.00 0.00 0.00 0.15 0.20 0.10 0.00 0.10 0.10 0.10
0.00 0.25 0.00 0.00 0.00 0.00 0.15 0.20 0.10 0.10 0.00 0.10 0.10
0.00 0.25 0.00 0.00 0.00 0.00 0.15 0.30 0.00 0.10 0.10 0.00 0.10

```



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0.00 0.40 0.00 0.00 0.00 0.00 0.00 0.20 0.10 0.10 0.10 0.10 0.00

**Caution:**

- a) The radiation model's precision is decided by the user when he/she names the domain edges. In fact, a radiating face is recognised by the preprocessor as the set of domain edges faces bearing the same name. Thus, if the user subdivides the edge into two edges which are named differently, he/she thus creates two radiating faces instead of one.
- b) The form factors are entered by the user, the preprocessor carries out no calculations other than checking preservation relationships on form factors.
- c) The fluid is considered to be a transparent gas.

**Associate:** This keyword is used to associate the radiation model to the problem.

**Solve:** This keyword is used to resolve the problem coupled to radiation.

## 2.7.2 THERMOHYDRAULIC PROBLEM WITH RADIATION MODEL FOR SEMI TRANSPARENT GAS

```

Fluide_Incompressible fluide
Read fluide { ... }
Pb_Thermohydraulique Pb_fluide
Pb_Couple_Rayo_Semi_Transp Pb_couple
...
Modele_Rayo_Semi_Transp mod
Read mod {
    Eq_rayo_semi_transp {
        solveur solveur
        boundary_conditions
        {
            Name_boundary Boundary_condition_type A value emissivite field_type
            field_description
            .....
        }
    }
    Postraitement { ... }
}
Associate mod fluide
Associate pb_couple fluide
# The model should be associated to the coupling problem BEFORE the time scheme #
Associate pb_couple mod

Read pb_fluide
{
    Navier_Stokes_Standard { .... }
    Convection_Diffusion_Temperature
    {
        diffusion { }
        convection { ... }
        conditions_initiales { ... }
        sources { Source_rayo_semi_transp }
        boundary_conditions { ... }
    }
}
...
Solve pb_couple

```

**Pb\_Couple\_Rayo\_Semi\_Transp** : This keyword is used to define a problem coupling several other problems to which radiation coupling is added.

**Source\_rayo\_semi\_transp** : Radiative term source in energy equation.

**Modele\_Rayo\_Semi\_Transp** : Keyword to define the radiation model for semi transparent gas

**Eq\_rayo\_semi\_transp** : Irradiance G equation. Radiative flux equals  $-\text{grad}(G)/3/\kappa$

**Postraitement** : The model is a problem with the usual definition of the fields being postprocessed, here the **irradiance** field.

**solveur** : Keyword to define the solver of the irradiance equation

*Boundary\_condition\_type* :

**Flux\_radiatif\_VDF** : Boundary condition for radiation equation in VDF.

**Flux\_radiatif\_VEF** : Boundary condition for radiation equation in VEF.

**A** : Constant in boundary condition for irradiance ( $\sqrt{3}$ ) for half-infinite domain or 2 in closed domain)

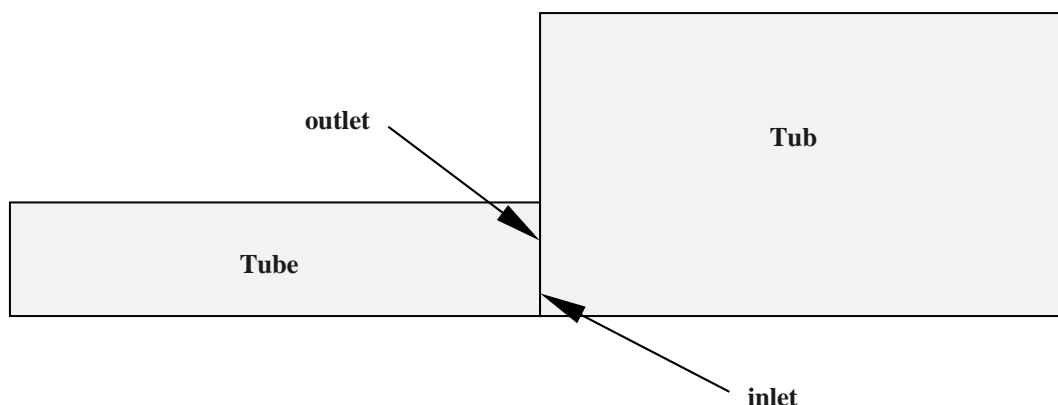
**emissivite** : Wall emissivity, value between 0 and 1.

### Warning:

Calculation with semi transparent gas model may lead to divergence when high temperature differences are used. Indeed, the calculation of the stability time step of the equation does not take in account the source term. In semi transparent gas model, energy equation source term depends strongly of temperature via irradiance and stability is not guaranteed by the calculated time step. Reducing the **facsec** of the time scheme is a good tip to reach convergence when divergence is encountered.

## 2.7.3 OTHER COUPLINGS

Trio-U allows other couplings to be performed. Examples allowed by the structure are given here.



**Dimension 2**

**Domaine tuyau**

**Domaine cuve**

**Read \_file** tuyau geom1.doc

# the tube object is read in the geom1.doc file #

**Read \_file** cuve geom2.doc

# the tub object is read in the geom2.doc file #

**Schema\_Euler\_Explicite** sch

**Read \_file** sch sch\_tps.doc

**VDF** dis

**Fluide\_Incompressible** fluide

**Read \_file** fluide fluide.doc

**Pb\_Hydraulique** pb1

# The Pb\_Hydraulique type object pb1 is created#

**Pb\_Hydraulique** pb2

# The Pb\_Hydraulique type object, pb2 is created#

**Associate** pb1 tuyau

**Associate** pb2 cuve

**Associate** pb1 fluide

**Associate** pb2 fluide

**Probleme\_Couple** pb\_couplage

# Create the pb\_couplage object; problems must be associated to the Probleme\_Couple type object before applying the other instructions #

**Associate** pb\_couplage pb1

# Association of the pb1 object to the pb\_couplage object #

**Associate** pb\_couplage pb2

# Association of the pb2 object to the pb\_couplage object #

**Associate** pb\_couplage sch

**Discretize** pb\_couplage dis

# the tube object contains an edge called outlet

the tub object contains an edge called inlet

The two edges are identical from a geometric point of view and coupling is achieved by means of this edge #

**Read** pb1

{

**Navier\_Stokes\_std**



cea DEN

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```
{
    .....
    boundary_conditions {
        .....
        sortie Frontiere_ouverte_pression_imposee
        Champ_front_recyclage { pb_champ_evaluateur pb2 pression
1 }
    }
}
}

Read pb2
{
    Navier_Stokes_std
    {
        .....
        Conditions_aux_limites {
            .....
            entree Frontiere_ouverte_vitesse_imposee
            Champ_front_recyclage { pb_champ_evaluateur pb1 vitesse
2 }

        }
    }
}

Solve pb_couplage
```

## 2.8 SPATIAL DISCRETIZATION

### 2.8.1 CONVECTIVE SCHEMES

Scheme availability:

<i>Scheme name</i>	<i>Keyword VDF</i>	<i>Keyword VEF</i>
No scheme	Negligeable	Negligeable
Upwind generic formulation		Generic
Upwind	Amont	Amont
Quick-Sharp	Quick	Kquick
Center (order 2)*	Centre	Centre
Center (order 4)*	Centre4	Centre4
Muscl		Muscl
DI_L2		DI_L2
ALE		ALE
EF_stab		EF_stab
EF		EF

(\*): **Warning:** the centered schemes are unstable under some conditions.

The keyword **Negligeable** suppresses the Navier Stokes convection operator.

**EF\_stab** : Keyword for a VEF convective scheme.

```
EF_stab { [TdivU] [alpha factor] [volumes_etendus] [volumes_non_etendus] [old] [test]
          [amont_sous_zone sub_zone_name]
          [alpha_sous_zone N sub_zone_name_1 alpha_1 ... sub_zone_name_N alpha_N]
        }
```

The options of the keyword are :

**TdivU** : To have the convective operator calculated as  $\text{div}(\mathbf{TU}) - \mathbf{TdivU} (= \mathbf{UgradT})$ .

**alpha** double : To weight the scheme centering with the factor double (between 0 (full centered) and 1 (mix between upwind and centered), by default 1).

**volumes\_etendus** : Option for the scheme to use the extended volumes (default, yes).

**volumes\_non\_etendus** : Option for the scheme to not use the extended volumes (default, no).

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**old** : To use old version of EF\_stab scheme (default no).

**test** : Developer option to compare old and new version of EF\_stab

**amont\_sous\_zone** sz\_name : Option to degenerate EF\_stab scheme into Amont (upwind) scheme in the sub zone of name sz\_name. The sub zone may be located arbitrarily in the domain but the more often this option will be activated in a zone where EF\_stab scheme generates instabilities as for free outlet for example.

**alpha\_sous\_zone** N sub\_zone\_name\_1 alpha\_1 .... sub\_zone\_name\_N alpha\_N : Option to change locally the **alpha** value on N sub-zones named sub\_zone\_name\_I. Generally, it is used to prevent from a local divergence by increasing locally the **alpha** parameter.

**Generic** scheme [limiter] [order] : Keyword for generic calling of upwind and muscl convective scheme in VEF discretization. For muscl scheme, limiters and order for fluxes calculations have to be specified. The available limiters are : **minmod** - **vanleer** - **vanalbada** - **chakravarthy** - **superbee**, and the order of accuracy is 1 or 2. Note that **chakravarthy** is a non-symmetric limiter and **superbee** may engender results out of physical limits. By consequence, these two limiters are not recommended.

*Examples:*

```
convection { generic amont }
convection { generic muscl minmod 1 }
convection { generic muscl vanleer 2 }
```

In case of results out of physical limits with muscl scheme (due for instance to strong non-conformal velocity flow field), user can redefine in data file a lower order and a smoother limiter, as :

```
convection { generic muscl minmod 1 }
```

**Amont**: Keyword for upwind scheme in VEF discretization equivalent to **generic** **amont** for Trio\_U version 1.5 or later. The previous upwind scheme can be used with the obsolete in future **amont\_old** keyword.

**Muscl**: Keyword for muscl scheme in VEF discretization equivalent to **generic** **muscl** **vanleer** 2 for Trio\_U version 1.5 or later. The previous muscl scheme can be used with the obsolete in future **muscl\_old** keyword.

**ALE** { scheme } : Keyword to use a convective scheme for ALE method.

*Example:* See the test case ALE\_membrane

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Navier\_Stokes\_standard

```
{
  solveur_pression GCP { ... }
  convection { ALE { amount } }
  diffusion { }
  conditions_initiales { ... }
  boundary_conditions {
    Bord1 frontiere_ouverte_vitesse_imposee
    Champ_front_ALE 2 20*0.3*SIN(6.28*y)*COS(20*t) 0.
  }
}
```

**EF** : For VEF calculations, a centred convective scheme based on Finite Elements formulation can be called through the following data:

Convection { **EF transportant\_bar** val **transporte\_bar** val **antisym** val **filtrer\_resu** val }

This scheme is 2<sup>nd</sup> order accuracy (and get better the property of kinetic energy conservation). Due to possible problems of instabilities phenomena, this scheme has to be coupled with stabilisation process (see **Source\_Qdm\_lambdaup**)

For parameterised studies, following keywords (admitting Boolean values 0 or 1) can be specified.

**transportant\_bar** 1 refers to filtered transporting velocity (P1-conform)

**transporte\_bar** 1 refers to filtered transported velocity (P1-conform)

**antisym** 1 adjoins anti-symmetric part for preserving kinetic energy

**filtrer\_resu** 1 filters all the convective fluxes contribution

In the aim not to specify these keywords, **default\_bar** can be used :

Convection { **EF default\_bar** } , equivalent to :

convection { **EF transportant\_bar** 0 **transporte\_bar** 1 **filtrer\_resu** 1 **antisym** 1 }

*These two last data are equivalent from a theoretical point of view in variationnal writing to :  $\frac{1}{2}[(u, \text{grad } ub, vb) - (u, \text{grad } vb, ub)]$ , where  $vb$  corresponds to the filtered reference test functions.*

*Remark:*

This class requires to define a filtering operator : see **solveur\_bar**



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## 2.8.2 DIFFUSIVE SCHEME

Several possibilities are available to take in count or not the diffusivity:

**Diffusion**: This keyword is used to specify the diffusion operator.

**Diffusion** { [keyword] }

Several possible uses:

**Diffusion** { } : the standard diffusive scheme used is an order 2 scheme.

**Diffusion** { **stab** { [standard integer] [info integer] [new\_jacobian integer]  
[nu integer] [nut integer] [nu\_transp integer] [nut\_transp integer] } }

A keyword allowing consistent and stable calculations even in case of obtuse angle meshes.

Several options are available for general flow:

**standard** integer : to recover the same results as calculations made by standard laminar diffusion operator. However, no stabilization technique is used and calculations may be unstable when working with obtuse angle meshes (by default 0)

**info** integer : developer option to get the stabilizing ratio (by default 0)

**new\_jacobian** integer : when implicit time schemes are used, this option defines a new jacobian that may be more suitable to get stationary solutions (by default 0)

Several options are available for turbulent flow:

**nu** 1 (respectively **nut** 1) takes the molecular viscosity (resp. eddy viscosity) into account in the velocity gradient part of the diffusion expression (by default **nu**=1 and **nut**=1)

**nu\_transp** 1 (respectively **nut\_transp** 1) takes the molecular viscosity (resp. eddy viscosity) into account in the transposed velocity gradient part of the diffusion expression (by default **nu\_transp**=0 and **nut\_transp**=1)

**Diffusion** { **negligeable** } : the diffusivity will not be taken into account exactly as if the equation has no diffusive operator.

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**Diffusion { implicite Solveur kind\_of\_solver { options\_for\_solver } }** : To have diffusive implicitation, it use **Uzawa** algorithm. Very useful when viscosity has large variations.

**Uzawa**: Keyword to set the convergency of the Uzawa algorithm if Implicite Solveur keyword has been set in **Diffusion**.

Example:

Read pb

```
{
  Navier_Stokes_standard
  {
    solveur_pression GCP { ... }
    convection { amount }
    diffusion { implicite solveur cholesky { impr } }
    uzawa 1.e-8
    conditions_initiales { ... }
    boundary_conditions { ... }
  }
  Postraitement { ... }
```

**Diffusion { P1NCP1B { [ alphaE integer] [alphaS integer] [ alphaA integer] [test] [decentrage integer] [epsilon double] } }**

A keyword intended for conduction calculations to improve the default diffusion scheme when used with VEFPre1B discretization.

**alphaE** integer: to add (integer=1) or suppress (integer=0) the P0 part of the operator (by default 1)

**alphaS** integer: to add (integer=1) or suppress (integer=0) the P1 part of the operator (by default 1)

**alphaA** integer: to add (integer=1) or suppress (integer=0) the P2 part of the operator (option not coded yet so by default 0)

**test** : developer option to compare explicit and implicit operators

**decentrage** integer: to ensure the positivity of the operator (by default 1)

**epsilon** double : to weight the P0 part of the operator (between 0, full P1 discretization, and 1, full P0 discretization, default 1e-3)

**Diffusion { standard grad\_Ubar value nu value nut value nu\_transp value nut\_transp value filtrer\_resu value }** : A new keyword, intended for LES calculations, has been developed to optimise and parameterise each term of the diffusion operator.

For parameterised studies, following keywords (admitting Boolean values 0 or 1) can be specified.

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**grad\_Ubar** 1 makes the gradient calculated through the filtered values of velocity (P1-conform).

**nu** 1 (respectively **nut** 1) takes the molecular viscosity (eddy viscosity) into account in the velocity gradient part of the diffusion expression.

**nu\_transp** 1 (respectively **nut\_transp** 1) takes the molecular viscosity (eddy viscosity) into account according in the TRANSPOSED velocity gradient part of the diffusion expression.

**filtrer\_resu** 1 allows to filter the resulting diffusive fluxes contribution.

In the aim not to specify these keywords, **default\_bar** can be used :

diffusion { **standard** default\_bar } , equivalent to :

diffusion { **standard** grad\_Ubar 1 nu 1 nut 1 nu\_transp 1 nut\_transp 1 filtrer\_resu 1 }

Remark:

1. This class requires to define a filtering operator : see **solveur\_bar**
2. The former (original) version: diffusion { } -which omitted some of the term of the diffusion operator- can be recovered by using the following parameters in the new class :  
diffusion { **standard** grad\_Ubar 0 nu 1 nut 1 nu\_transp 0 nut\_transp 1 filtrer\_resu 0 }.

## 2.9 TIME SCHEMES

**type\_schema sch**

*type\_schema*: scheme type in time used.

*sch*: object identifier

The available types are explicit schemes:

**Schema\_Euler\_explicite**  
**Schema\_Adams\_Bashforth\_order\_2**  
**Schema\_Adams\_Bashforth\_order\_3**  
**Runge\_Kutta\_Rationnel\_ordre\_2**  
**Runge\_Kutta\_ordre\_3**  
**Runge\_Kutta\_ordre\_4\_D3P**  
**Schema\_Predictor\_Corrector**  
**Sch\_CN\_iteratif**  
**Sch\_CN\_EX\_iteratif**  
**Schema\_Phase\_Field**  
**RK3\_FT**

And also implicit schemes:

**Schema\_Euler\_implicite**  
**Schema\_Adams\_Moulton\_order\_2**  
**Schema\_Adams\_Moulton\_order\_3**  
**Schema\_Backward\_Differentiation\_order\_2**  
**Schema\_Backward\_Differentiation\_order\_3**

*Example:*

Runge\_Kutta\_ordre\_3 *sch*

The time scheme parameters are then read.

The read block that follows is similar for all scheme types.

```

Read sch
{
  [tinit vrel]

  [tmax vrel]

  [tcpumax vrel]

  [nb_pas_dt_max integer]

  [dt_min vrel]

  [dt_max vrel]

  [dt_start ....]

  [dt_impr vrel]

  [precision_impr integer]

  [dt_sauv vrel]

  [seuil_statio vrel]

  [facsec vrel]

  [facsec_max double]
  [facsec_evol_facteur double]
  [max_iter_implicite int]
  [Solveur solver {
    [seuil_convergence_implicite vrel]
    [no_qdm]
    [solveur solver]
    [seuil_generation_solveur vrel]
    [seuil_test_preliminaire_solveur vrel]
    [seuil_verification_solveur vrel]
    [relax_pression vrel]
    [nb_corrections_max int]
  }
]
  [diffusion_implicite integer ]
  [seuil_diffusion_implicite vrel]
  [impr_diffusion_implicite int]
  [niter_max_diffusion_implicite ivalue]
  [periode_sauvegarde_securite_en_heures ivalue]
  [no_check_disk_space]
}

```

**tinit** vrel: This is a keyword and the value of the initial calculation time (0 by default).

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**tmax** vrel: This is an optional keyword and the time during which the calculation was stopped ( $10^{30}$ s by default).

**tcpumax** vrel : Optional CPU time limit (must be specified in hours) for which the calculation is stopped ( $10^{30}$ s by default).

**nb\_pas\_dt\_max** integer: This is a keyword and the maximum number of calculation time steps.

**dt\_min** vrel: This is a keyword and the minimum calculation time step ( $10^{-16}$ s by default).

**dt\_max** vrel: This keyword gives the maximum calculation time step ( $10^{30}$ s by default).

**dt\_start**: This keyword allows to specify the way to define the time step when (re)starting a calculation.

**dt\_start** dt\_min : the first iteration is based on dt\_min

**dt\_start** dt\_calc : the time step at first iteration is calculated in agreement with CFL condition.

**dt\_start** dt\_fixe value : the first time step is fixed by the user (recommended when restarting calculation with Crank Nicholson temporal scheme to ensure continuity).

By default, the first iteration is based on dt\_calc.

### Schema\_Euler\_Explicite sch

Read sch

```
{
    tinit 0.563
    tmax 1.
    dt_min 0.00001
    dt_max 0.2
    dt_start dt_fixe 0.000154
    dt_impr 0.001
    ...
}
```

**dt\_impr** vrel: This is a keyword and scheme parameter printing time step in time ( $10^{30}$ s by default). The time steps and the flux balances are printed (incorporated onto every side of processed domains) into the **.out** file.

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**precision\_impr** integer: Optional keyword to define the digit number for flux values printed into .out files (by default 3).

**dt\_sauv** vrel: This is a keyword and holds the save time step value ( $10^{30}$ s by default). Every dt\_sauv, fields are saved in the **.sauv** file.

**seuil\_statio** vrel: This is a keyword and holds the value of the convergence threshold ( $10^{-12}$  by default). Problems using this type of time scheme converge when the derivatives  $dG_i/dt$  of all the unknown transported values  $G_i$  have a combined absolute value less than this value. This is the keyword used to set the permanent rating threshold.

**facsec** vrel: This is a keyword and the value assigned to the safety factor for the time step (1. by default). The time step calculated is multiplied by the safety factor. **The first thing to try when a calculation does not converge with an explicit time scheme is to reduce the facsec to 0.5.**

Warning: Some schemes needs a facsec lower than 1 (0.5 is a good start), for example **Schema\_Adams\_Bashforth\_order\_3**

**Solveur** *solver*: This keyword is used to designate the solver selected in the situation where the time scheme is an implicit scheme (see list page 150). *solver* is the name of the solver that allows equation diffusion and convection operators to be set as implicit terms. Keywords corresponding to this functionality are **Simple** (SIMPLE type algorithm), **Simpler** (SIMPLER type algorithm) for incompressible systems, **Piso** (Pressure Implicit with Split Operator), and **Implicite** (similar to PISO, but as it looks like a simplified solver, it will use fewer timesteps. But it may run faster because the pressure matrix is not re-assembled and thus provides CPU gains.

Advice: Since the 1.6.0 version, we recommend to use first the **Implicite** or **Simple**, then **Piso**, and at least **Simpler**. Because the two first give a fastest convergence (several times) than **Piso** and the **Simpler** has not been validated. It seems also than **Implicite** and **Piso** schemes give better results than the **Simple** scheme when the flow is not fully stationary. Thus, if the solution obtained with **Simple** is not stationary, it is recommended to switch to **Piso** or **Implicite** scheme.

**seuil\_convergence\_implicite** : Keyword to set the value of the convergence criteria for the resolution of the implicit system build by solving several times per time step the Navier\_Stokes

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equation and the scalar equations if any. This value **MUST** be used when a coupling between problems is considered (should be set to a value typically of 0.1 or 0.01).

**no\_qdm** : Optional keyword to not solve the impulsion equation (and turbulence models of these equation)

**solveur** solver : **solveur** is an optional keyword to specify a method (different from the default one, **Gmres** with diagonal preconditioning) to solve the linear system for implicitation.

Advice:

A good strategy (best CPU results) for the choice of the solver is to specify a **GMRES** method (and diagonal preconditioning) with a very low convergence threshold but limit to a maximum of 5 iterations (it converges generally quickly in few iterations):

**solveur gmres { diag seuil 1e-30 nb\_it\_max 5 impr }**

And in a first approach, to not use the following thresholds:

**seuil\_generation\_solveur vrel**: Option to create a **GMRES** solver and use *vrel* as the convergence threshold (implicit linear system  $Ax=B$  will be solved if residual error  $\|Ax-B\|$  is lesser than *vrel*)

**seuil\_verification\_solveur vrel** : Option to check if residual error  $\|Ax-B\|$  is lesser than *vrel* after the implicit linear system  $Ax=B$  has been solved.

**seuil\_test\_preliminaire\_solveur vrel** : Option to decide if the implicit linear system  $Ax=B$  should be solved by checking if the residual error  $\|Ax-B\|$  is bigger than *vrel*.

NB:

**seuil\_convergence\_solveur vrel** option becomes obsolete since the 1.6.2 version. In the past, the same value *vrel* was used for the 3 last thresholds.

**facsec\_max** double: Maximum ratio allowed between time step and stability time returned by CFL condition. The initial ratio given by **facsec** keyword is changed during the calculation with the implicit scheme but it couldn't be higher than **facsec\_max** value.



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Warning: Some implicit schemes do not permit high `facsec_max`, example **Schema\_Adams\_Moulton\_order\_3** needs `facsec=facsec_max=1`.

Advice:

The calculation may start with a **facsec** specified by the user and increased by the algorithm up to the **facsec\_max** limit. But the user can also choose to specify a constant `facsec` (**facsec\_max** will be set to **facsec** value then). Faster convergence has been seen and depends on the kind of calculation:

- Hydraulic only or thermal hydraulic with forced convection and low coupling between velocity and temperature (Boussinesq value  $\beta$  low), **facsec** between 20-30
- Thermal hydraulic with forced convection and strong coupling between velocity and temperature (Boussinesq value  $\beta$  high), **facsec** between 90-100
- Thermohydraulic with natural convection, **facsec** around 300
- Conduction only, **facsec** can be set to a very high value ( $10^8$ ) as if the scheme was unconditionally stable

These values can also be used as rule of thumb for initial **facsec** with a **facsec\_max** limit higher.

**max\_iter\_implicite** int: Maximum number of iterations allowed for the implicit algorithm (by default 200).

**relax\_pression** vrel: Value between 0 and 1 (by default 1), this keyword is used only by the SIMPLE algorithm for relaxing the increment of pressure.

**nb\_corrections\_max** int : Maximum number of corrections performed by the **PISO** algorithm to achieve the projection of the velocity field. The algorithm may perform less corrections than `nb_corrections_max` if the accuracy of the projection is sufficient. (By default `nb_corrections_max` is set to 21).

**diffusion\_implicite** integer: This keyword is used to make the diffusion term in the Navier Stokes equation implicit (in this case, *integer* should be set to 1). The stability time step is then only based on the convection time step ( $dt=facsec*dt_{convection}$ ). Thus, in some circumstances, an important gain is achieved with respect to the time step (large diffusion with respect to convection on tightened meshes). Caution: It is however recommended that the user should avoid exceeding the calculation convection time step by selecting a `facsec` that is too large. Start with a `facsec` of 1 and then increase this gradually if you wish to accelerate

calculation. In addition, for a natural convection calculation with a zero initial speed, in the first time step, the convection time is infinite and therefore  $dt = facsec * dt\_max$ .

**seuil\_diffusion\_implicite:** This keyword changes the default value (1e-6) of convergency criteria for the resolution by conjugate gradient used for **implicit diffusion**.

**impr\_diffusion\_implicite** 0|1: Unactivate (default) or not the printing of the convergence during the resolution of the conjugate gradient.

**niter\_max\_diffusion\_implicite:** This keyword changes the default value (number of unknowns) of the maximal iterations number in the conjugate gradient method used for **implicit diffusion**.

**periode\_sauvegarde\_securite\_en\_heures:** This keyword is used to change the default period (10 hours) between the save of the fields in .sauv file.

**no\_check\_disk\_space :** This keyword disables the check of the available amount of disk space during the calculation.

*Note:*

The new scheme **Schema\_Predictor\_Corrector** scheme (2<sup>nd</sup> order) is more accurate and economic than MacCormack scheme. It gives best results with a second ordre convective scheme like quick, centre (VDF).

Example: (See test case Pred\_Cor\_VEF)

**Schema\_Predictor\_Corrector** sch

```
Read sch {
    tinit 0.
    tmax 2.
    dt_min 1.e-5
    dt_max 1.
    dt_impr 1.e-4
    dt_sauv 100
    seuil_statio 1.e-12
}
```

### Sch\_CN\_iteratif

This keyword describes a Crank-Nicholson method of second order accuracy. A mid-point rule formulation is used (Euler-centered scheme).

The basic scheme is:  $u(t+1) = u(t) + du/dt(t+1/2)*dt$ .

The estimation of the time derivative  $du/dt$  at the level  $(t+1/2)$  is obtained either by iterative process. The time derivative  $du/dt$  at the level  $(t+1/2)$  is calculated iteratively with a simple

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under-relaxations method. Since the method is implicit, neither the cfl nor the fourier stability criteria must be respected. The time step is calculated in a way that the iterative procedure converges with the less iterations as possible.

Parameters (*and values taken by default*):

**niter\_min**: minimal number of p-iterations to satisfy convergence criteria (2)

**niter\_max** : number of maximum p-iterations allowed to satisfy convergence criteria (6)

**niter\_avg**: threshold of p-iterations (3). If the number of p-iterations is greater than **niter\_avg**, facsec is reduced, if lesser than **niter\_avg**, facsec is increased (but limited by the **facsec\_max** value).

**facsec\_max** : maximum ratio allowed between dynamical time step returned by iterative process and stability time returned by CFL condition (2).

**seuil**: criteria for ending iterative process ( $\text{Max}(\|u(p) - u(p-1)\| / \text{Max} \|u(p)\|) < \text{seuil}$ ) (0.001)

### Sch\_CN\_EX\_iteratif

This keyword also describes a Crank-Nicholson method of second order accuracy but here, for scalars, because of instabilities encountered when  $dt > dt_{CFL}$ , the Crank Nicholson scheme is not applied to scalar quantities. Scalars are treated according to Euler-Explicite scheme at the end of the CN treatment for velocity flow fields (by doing p Euler explicite under-iterations at  $dt \leq dt_{CFL}$ ).

Parameters are the same (but default values may change) compare to the **Sch\_CN\_iterative** scheme plus a relaxation keyword:

**niter\_min**: (2)

**niter\_max** : (6)

**niter\_avg**: (3)

**facsec\_max** : (20)

**seuil**: (0.05)

**omega**: relaxation factor (0.1)

Remark: for stationary or RANS calculations, no limitation can be given for time step through high value of **facsec\_max** parameter (for instance: **facsec\_max** 1000). In counterpart, for LES calculations, high values of **facsec\_max** may engender numerical instabilities.

### Schema\_Phase\_Field

Keyword for the only available Scheme for time discretization of the Phase Field problem. This keyword has two mandatory options:

**Schema\_CH** scheme { } : Time scheme for the Cahn-Hilliard equation.

**Schema\_NS** scheme { } : Time scheme for the Navier-Stokes equation.

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### **RK3\_FT**

Keyword for Runge Kutta time scheme for Front\_Tracking calculation. Validated en tested only for the two following cases : problem with hydraulic and one interface equation, problem with hydraulic equation, one interface equation and one concentration equation.

## 2.10 PRESSURE SOLVERS

**Solveur\_pression** type\_solveur *solver\_description*

**Solveur\_pression:** This keyword is used to indicate the choice of pressure solver.

Three algorithms are possible for the pressure solver.

### 2.10.1 PRECONDITIONED CONJUGATED GRADIENT

```

Solveur_pression GCP { [ [precond_nul] precond type_precond { [ omega omega ] } ]
  [ seuil seuil ]
  [ impr ]
  [ optimized ]
}
```

Where:

**seuil** *seuil* : corresponds to the conjugated gradient convergence value. The method stops to iterate when the Euclidean residue standard  $\|Ax-B\|$  is less than this value.

**precond\_nul** : Keyword to not use a preconditioning method.

**precond** : is a keyword used to define system preconditioning in order to accelerate resolution by the conjugated gradient. For example, a preconditioning **ssor** with a overrelaxation factor *omega* (between 1 and 2, optimal value around 1.5-1.6). Many parallel preconditioning methods are not equivalent to their sequential counterpart, and you should therefore expect differences, especially when you select a high value of the final residue ("seuil"). The result depends on the number of cpus and on the mesh splitting. It is sometimes useful to run the solver with no preconditioning at all. In particular:

- when the solver does not converge during initial projection,
- when comparing sequential and parallel computations.

With no preconditioning, except in some particular cases (no open boundary), the sequential and the parallel computations should provide exactly the same results within fpu accuracy. If not, there might be a coding error or the system of equations is singular.

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**impr** is the keyword which is used to request display of the Euclidean residue standard each time this iterates through the conjugated gradient (display to the standard outlet).

**optimized** : This keyword triggers a memory and network optimized algorithms useful for strong scaling (when computing less than 100 000 elements per processor). The matrix and the vectors are duplicated, common items removed and only virtual items really used in the matrix are exchanged.

Warning: this is experimental and known to fail in some VEF computations (L2 projection step will not converge). Works well in VDF.

#### Observations:

Use the pressure solver **Arakawa\_P1** with VEF\_P1\_P1 discretization in order to avoid the appearance of parasite pressure.

Example of using the **Arakawa\_P1** solver:

```
solveur_pression Arakawa_P1 { omega 1.5 seuil 1.e-12 impr epsilon 0. }
```

The value of epsilon should be included between 0 and 1. If epsilon = 0, no stabilisation is detected.

## 2.10.2 SOLVERS FROM PETSC API

```
Solveur_pression Petsc Solver { precond Precond
                                [ seuil seuil | nb_it_max integer ]
                                [ impr ]
                                [ save_matrix|read_matrix]
                                }
```

*Solver* : Several solvers through [PETSc API](http://www.mcs.anl.gov/petsc/petsc-current/docs/manualpages/KSP/KSPPIPECG.html) are available :

**GCP** : Conjugate Gradient

**PIPECG** : Pipelined Conjugate Gradient (possible reduced CPU cost during massive parallel calculation due to a single non-blocking reduction per iteration, if Trio\_U is built with a MPI-3 implementation). See: <http://www.mcs.anl.gov/petsc/petsc-current/docs/manualpages/KSP/KSPPIPECG.html>

**GMRES** : Generalized Minimal Residual

**BICGSTAB** : Stabilized Bi-Conjugate Gradient

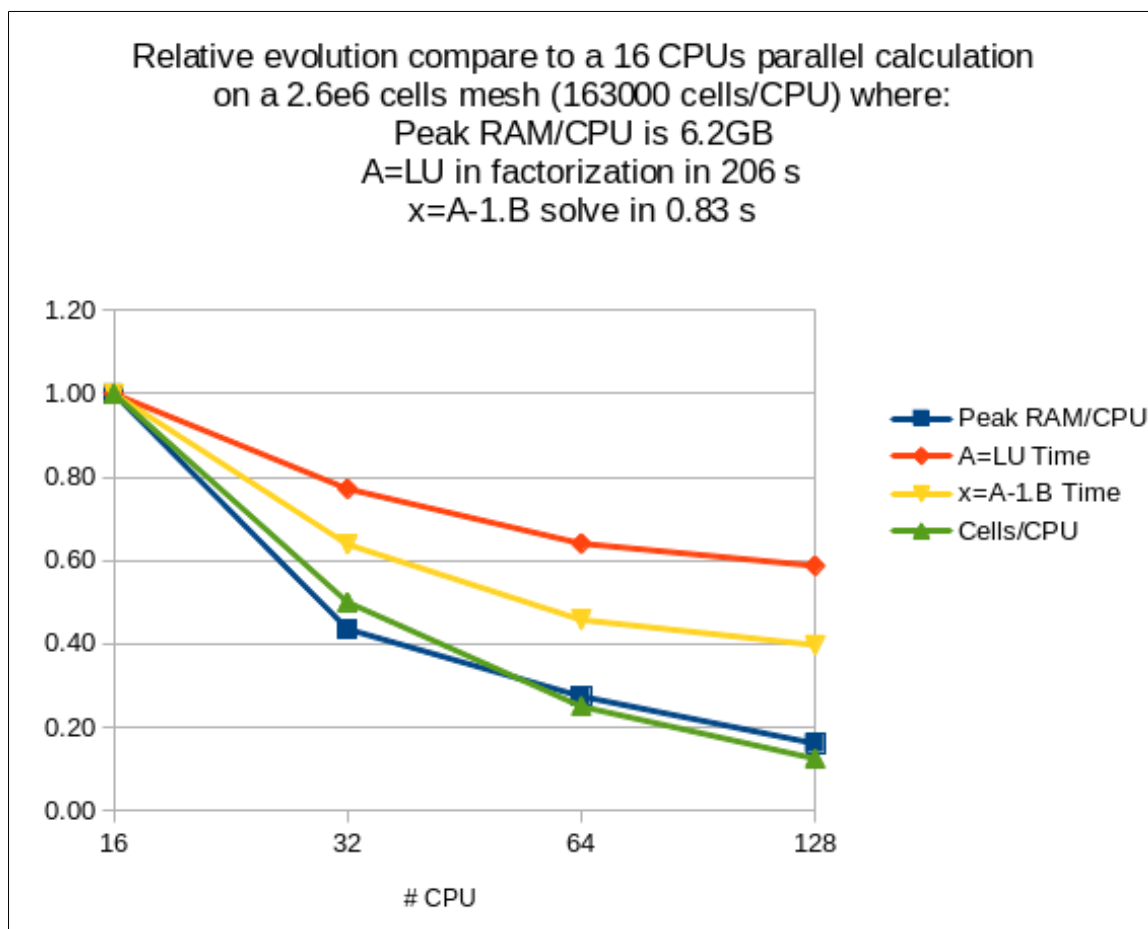
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**IBICGSTAB** : [Improved](#) version of previous one for massive parallel computations (only a single global reduction operation instead of the usual 3 or 4)

**CHOLESKY** : Parallelized version of Cholesky from MUMPS library. This solver accepts since the Trio\_U 1.6.7 version an option to select a different ordering than the automatic selected one by MUMPS (and printed by using the **impr** option). The possible choices are **Metis** | **Scotch** | **PT-Scotch** | **Parmetis**. The two last options can't only be used during a parallel calculation, whereas the two first are available for sequential or parallel calculations. It seems that the CPU cost of A=LU factorization but also of the backward/forward elimination steps may sometimes be reduced by selecting a different ordering than the default one. Notice that this solver requires a huge amount of memory compared to iterative methods. To know how many RAM you will need by core, then use the **impr** option to have detailed informations during the analysis phase and before the factorisation phase (in the following output, you will learn that the largest memory is taken by the 0<sup>th</sup> CPU with 108MB):

```
...
** Rank of proc needing largest memory in IC facto      :      0
** Estimated corresponding MBYTES for IC facto        :    108
...
```

Thanks to the following graph, you read that in order to solve for instance a flow on a mesh with 2.6e6 cells, you will need to run a parallel calculation on 32 CPUs if you have cluster nodes with only 4GB/core (6.2GB\*0.42~2.6GB) :



**CHOLESKY\_OUT\_OF\_CORE** : Same as the previous one but with a written LU decomposition of disc (save RAM memory but add an extra CPU cost during  $Ax=B$  solve)

**CHOLESKY\_SUPERLU** : Parallelized Cholesky from [SUPERLU\\_DIST](#) library (less CPU and RAM efficient than the previous one)

**CHOLESKY\_PASTIX** : Parallelized Cholesky from PASTIX library

**CHOLESKY\_UMFPACK** : Sequential Cholesky from UMFPACK library (seems fast).

**LU**: Same as Cholesky but for a non symmetric matrix.

**CLI** { string } : Command Line Interface. Should be used only by advanced users, to access the whole solver/preconditioners from the PETSC API. To find all the available options, run your calculation with the -ksp\_view -help options:

triou datafile [N] -ksp\_view -help

...

**Preconditioner (PC) Options** -----

-pc\_type Preconditioner:(one of) none jacobi pbjacobi bjacobi sor lu shell mg



eisenstat ilu icc cholesky asm ksp composite redundant nn mat fieldsplit galerkin openmp spai hypre tfs (PCSetType)

HYPRE preconditioner options

-pc\_hypre\_type <pilut> (choose one of) pilut parasails boomeramg euclid

HYPRE ParaSails Options

-pc\_hypre\_parasails\_nlevels <1>: Number of number of levels (None)

-pc\_hypre\_parasails\_thresh <0.1>: Threshold (None)

-pc\_hypre\_parasails\_filter <0.1>: filter (None)

-pc\_hypre\_parasails\_loadbal <0>: Load balance (None)

-pc\_hypre\_parasails\_logging: <FALSE> Print info to screen (None)

-pc\_hypre\_parasails\_reuse: <FALSE> Reuse nonzero pattern in preconditioner (None)

-pc\_hypre\_parasails\_sym <nonsymmetric> (choose one of) nonsymmetric SPD nonsymmetric,SPD

**Krylov Method (KSP) Options** -----

-ksp\_type Krylov method:(one of) cg cgne stcg gltr richardson chebychev gmres tcqmr

bcs bcs1 cgs tfqmr cr lsqr preonly qcg bicg fgmres minres symmlq lgmres lcd (KSPSetType)

-ksp\_max\_it <10000>: Maximum number of iterations (KSPSetTolerances)

-ksp\_rtol <0>: Relative decrease in residual norm (KSPSetTolerances)

-ksp\_atol <1e-12>: Absolute value of residual norm (KSPSetTolerances)

-ksp\_divtol <10000>: Residual norm increase cause divergence (KSPSetTolerances)

-ksp\_converged\_use\_initial\_residual\_norm: Use initial residual residual norm for computing relative convergence

-ksp\_monitor\_singular\_value <stdout>: Monitor singular values (KSPMonitorSet)

-ksp\_monitor\_short <stdout>: Monitor preconditioned residual norm with fewer digits (KSPMonitorSet)

-ksp\_monitor\_draw: Monitor graphically preconditioned residual norm (KSPMonitorSet)

-ksp\_monitor\_draw\_true\_residual: Monitor graphically true residual norm (KSPMonitorSet)

Example to use the multigrid method as a solver, not only as a preconditioner:

**Solveur\_pression Petsc CLI** { -ksp\_type richardson -pc\_type hypre -pc\_hypre\_type boomeramg -ksp\_atol 1.e-7 }

*Precond* : Several preconditioners are available :

**NULL** { } : No preconditioner used

**ILU** { **level** **k** } : Parallel incomplete LU factorization (PILU(k) algorithm from Euclid Hypre library). The integer k is the factorization level (default value, 1). See [here](#) for a more detailed description.

**BLOCK\_JACOBI\_ICC** { **level** **k** **ordering** **natural** | **rcm** } : Incomplete Cholesky factorization for symmetric matrix with the PETSc implementation. The integer k is the

factorization level (default value, 1). In parallel, the factorization is done by block (one per processor by default). The ordering of the local matrix is **natural** by default, but **rcm** ordering, which reduces the bandwidth of the local matrix, may interestingly improves the quality of the decomposition and reduces the number of iterations. This preconditioner converges generally with more iterations than the parallel version ILU from Hypre, but will be much more faster.

**SSOR** { **omega** double } : Symmetric Successive Over Relaxation algorithm. **omega** (default value, 1.5) defines the relaxation factor.

**EISENTAT** { **omega** double } : SSOR version with [Eisenstat trick](#) which reduces the number of computations and thus CPU cost

**SPAI** { **level** nlevels **epsilon** thresh } : Spai Approximate Inverse algorithm from Parasails Hypre library. Two parameters are available, nlevels and thresh. See [here](#) for a more detailed description.

**PILUT** { **level** k **epsilon** thresh } : Dual Threshold Incomplete LU factorization. The integer k is the factorization level and **epsilon** is the drop tolerance. See [here](#) for a more detailed description.

**DIAG** { } : Diagonal (Jacobi) preconditioner.

**BOOMERAMG** { } : Multigrid preconditioner (no option is available yet, look at CLI command and Petsc documentation to try other options).

**seuil** corresponds to the iterative solver convergence value. The iterative solver converges when the Euclidean residue standard  $\|Ax-B\|$  is less than the value *seuil*.

**nb\_it\_max** integer : In order to specify a given number of iterations instead of a condition on the residue with the keyword **seuil**. May be useful when defining a PETSc solver for the implicit time scheme where convergence is very fast: 5 or less iterations seems enough.

**impr** is the keyword which is used to request display of the Euclidean residue standard each time this iterates through the conjugated gradient (display to the standard outlet).

**save\_matrix|read\_matrix** are the keywords to save|read into a file the constant matrix A of the linear system  $Ax=B$  solved (eg: matrix from the pressure linear system for an incompressible flow). It is useful when you want to minimize the MPI communications on massive parallel calculation. Indeed, in VEF discretization, the overlapping width (generaly 2, specified with the **largeur\_joint** option in the partition keyword **partition**) can be reduced to 1, once the matrix has been properly assembled and saved. The cost of the MPI communications in Trio\_U itself (not in PETSc) will be reduced with length messages divided by 2. So the strategy is:

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- I) Partition your VEF mesh with a **largeur\_joint** value of 2
- II) Run your parallel calculation on 0 time step, to build and save the matrix with the **save\_matrix** option. A file named *Matrix\_NBROWS\_rows\_NCPUS\_cpus.petsc* will be saved to the disc (where NBROWS is the number of rows of the matrix and NCPUS the number of CPUs used).
- III) Partition your VEF mesh with a **largeur\_joint** value of 1
- IV) Run your parallel calculation completely now and substitute the **save\_matrix** option by the **read\_matrix** option. Some interesting gains have been noticed when the cost of linear system solve with PETSc is small compared to all the other operations.

### **TIPS:**

- A) Solver for symmetric linear systems (e.g: Pressure system from Navier Stokes equation):
- The **CHOLESKY** parallel solver is from MUMPS library. It offers better performance than all others solvers if you have enough RAM for your calculation. A parallel calculation on a cluster with 4GBytes on each processor, 40000 cells/processor seems the upper limit. Seems to be very slow to initialize above 500 cpus/cores.
  - When running a parallel calculation with a high number of cpus/cores (typically more than 500) where preconditioner scalability is the key for CPU performance, consider **BICGSTAB** with **BLOCK\_JACOBI\_ICC(1)** as preconditioner or if not converges, **GCP** with **BLOCK\_JACOBI\_ICC(1)** as preconditioner.
  - For other situations, the first choice should be **GCP/SSOR**. In order to fine tune the solver choice, each one of the previous list should be considered. Indeed, the CPU speed of a solver depends of a lot of parameters. You may give a try to the **OPTIMAL** solver to help you to find the fastest solver on your study.

- B) Solver for non symmetric linear systems (e.g.: Implicit schemes):
- The **BICGSTAB/DIAG** solver seems to offer the best performances.

Additional information is available into the PETSC documentation available there:  
**\$TRIO\_U\_ROOT/lib/src/LIBPETSC/petsc/\*/docs/manual.pdf**

## **2.10.3CHOLESKY DIRECT METHOD**

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**Solveur\_preSSION Cholesky { [ impr ] }**

Where **impr** is a keyword which may be used to print the resolution time. The Cholesky implementation in Trio\_U is not parallel and will become obsolete. Consider **Petsc Cholesky** keywords for a parallel calculation.

## 2.11. OTHER SOLVERS

We may use also methods for non symmetric linear systems:

### 2.11.1. PETSC API SOLVERS

```
Petsc Solver { ... }
```

Solver may be **GMRES** or **BICGSTAB**. Look at 2.10.2 to see the options.

### 2.11.2. GMRES METHOD

```
Gmres {
  seuil double
  [ diag ]
  [ impr ]
  [ nb_it_max integer ]
  [ controle_residu 0|1 ]
}
```

Where:

**seuil** double: This keyword is used to define the convergence threshold.

**impr** is an optional keyword which may be used to print the convergence

**diag** is an optional keyword to use diagonal preconditioning instead of Pilut one which is not parallel.

**nb\_it\_max** is an optional keyword to set the maximum iterations number for the Gmres.

**controle\_residu** is an optional Boolean (by default 0). If set to 1, the convergence occurs if the residu suddenly increases.

### 2.11.3. GEN METHOD

```

Gen {
  seuil double
  solv_elem bicgstab
  precond precond
  [ impr ]
  [ save_matrice ]
}

```

Where:

**seuil** double: This keyword is used to define the convergence threshold.

**impr** is an optional keyword which may be used to print the convergence

**solv\_elem** is the keyword to specify the solver used with the method (**BICGSTAB** is the solver to use if **Gmres** solver fails to converge with the implicit schemes).

**precond** **precond** : To specify the preconditionner of the solver given with the previous keyword **solv\_elem**. ILU is the recommended one when using **BICGSTAB** solver:

**ILU** { **type** m **filling** n }

With m=1,2,3 (default 2), and n filling of the ILU method (by default 1). For example: **ILU** { **type** 2 **filling** 20 }

**save\_matrice** is an optional keyword to save the matrix in a file.

#### 2.11.4OPTIMAL

```

Optimal {
  seuil val
  [ save_matrice ]
  [ frequence_recalc double ]
  [ nom_fichier_solveur file ]
  [ fichier_solveur_non_recre ]
  [ impr ]
}

```

**Optimal** is a solver which tests several solvers of the previous list to choose the fastest one for the considered linear system. Options:

**seuil** val : Convergence threshold

**save\_matrice** : Keyword to save the linear system (A, x, B) into a file

**frequence\_recalc** double : Keyword to set a time step period (by default, 100) for re-checking the fastest solver

**nom\_fichier\_solveur** file : To specify the file containing the list of the tested solvers

**fichier\_solveur\_non\_recree** : Keyword to avoid the creation of the file containing the list

**impr** : To print the convergency of the fastest solver

Another keyword is available to test solvers:

```

Test_solveur {
  [ fichier_secmem file ]
  [ fichier_matrice file ]
  [ fichier_solution file ]
  [ nb_test int ]
  [ impr ]
  [ solveur string ]
  [ fichier_solveur file ]
  [ genere_fichier_solveur double ]
  [ seuil_verification precision ]
  [ pas_de_solution_initiale ]
  [ ascii ]
}

```

**fichier\_secmem** file : Filename containing the second member B

**fichier\_matrice** file : Filename containing the matrix A

**fichier\_solution** file : Filename containing the solution x

**nb\_test** int : Number of tests to measure the time resolution (one preconditionnement)

**impr** : To print the convergence solver

**solveur** string : To specify a solver

**fichier\_solveur** file : To specify a file containing a list of solvers

**genere\_fichier\_solveur** double : To create a file of the solver with a threshold convergence

**seuil\_verification** precision : Check if the solution satisfy  $\|Ax-B\| < \text{precision}$

**pas\_de\_solution\_initiale** : Resolution isn't initialized with the solution x

**ascii** : Ascii files

## 2.12 INITIAL CONDITIONS

### 2.12.1 SPEEDS

**Vitesse** field\_type bloc\_lecture\_champ

**Vitesse:** This keyword is used to define the initial speed values.

*field\_type* : Type of initial speed field.

### 2.12.2 TEMPERATURE

**Temperature** field\_type bloc\_lecture\_champ

**Temperature:** This keyword is used to define the initial temperature values.

*field\_type* : The initial temperature field type.

The initial temperature is given in °C (or K).

### 2.12.3 TURBULENT VALUES

[ **K\_eps** field\_type bloc\_lecture\_champ ]  
 [ **Flux\_Chaleur\_Turbulente** field\_type bloc\_lecture\_champ ]  
 [ **Fluctu\_Temperature** field\_type bloc\_lecture\_champ ]

**K\_eps:** This keyword is used to define the initial kinetic energy values and the turbulent dissipation rate. The initial turbulent kinetic energy is given in  $\text{m}^2.\text{s}^{-2}$  and the initial turbulent dissipation rate is given in  $\text{m}^2.\text{s}^{-3}$ .

**Flux\_Chaleur\_Turbulente:** This keyword is used to define the initial turbulent heat flux vector values. It is expressed in [mK/s].



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**Fluctu\_Temperature:** This keyword is used to define the initial value vector {temperature fluctuation, fluctuation dissipation rate }. This value is expressed in [K<sup>2</sup>, K<sup>2</sup>].

*field\_type* : Initial value field type.

## 2.13 BOUNDARY CONDITIONS

*It is important to specify here that TRIO-U will not accept any boundary conditions by default.*

### 2.13.1 HYDRAULIC BOUNDARY CONDITIONS

```
[Bord Frontiere_ouverte_vitesse_imposee boundary_field_type bloc_lecture_champ ]
[Bord Frontiere_ouverte_rho_u_impose boundary_field_type bloc_lecture_champ ]
[Bord Frontiere_ouverte_pression_imposee boundary_field_type bloc_lecture_champ ]
[Bord Frontiere_ouverte_gradient_pression_impose boundary_field_type bloc_lecture_champ ]
[Bord Frontiere_ouverte_gradient_pression_libre_VEFPreP1B boundary_field_type bloc_lecture_champ ]
[Bord Frontiere_ouverte_gradient_pression_impose_VEFPreP1B boundary_field_type bloc_lecture_champ ]
[Bord Frontiere_ouverte_pression_imposee_Orlansky ]
[Bord Paroi_fixe]
[Bord Paroi_decalee_Robin { delta value } ]
[Bord Paroi_defilante boundary_field_type bloc_lecture_champ ]
[Bord Symetrie]
[Bord Periodique ]
[Bord Paroi_Knudsen_non_negligeable] field_type_front bloc_lecture_champ
[Bord Paroi_rugueuse { erugu value } ]
```

*Bord*: name of the edge where the boundary condition applies.

*boundary\_field\_type*: boundary field type.

*Direction*: to be selected along X, Y or Z

**Frontiere\_ouverte\_vitesse\_imposee**: This keyword is used to designate a condition of imposed speed at an open boundary called *bord*.

The imposed speed field at the inlet is vectorial and the imposed speed values are expressed in  $m.s^{-1}$ .

**Frontiere\_ouverte\_rho\_u\_impose**: This keyword is used to designate a condition of imposed mass rate at an open boundary called *bord*. The imposed mass rate field at the inlet is vectorial

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and the imposed speed values are expressed in  $\text{kg.s}^{-1}$ . This boundary condition can be used only with the Quasi compressible model (see 2.6.10).

**Frontiere\_ouverte\_pression\_imposee:** This keyword is used to designate an imposed pressure condition at the open boundary called *bord*. The imposed pressure field is expressed in Pa.

**Frontiere\_ouverte\_gradient\_pression\_impose:** Keyword used to designate a normal imposed pressure gradient condition on the open boundary called *bord*.

This boundary condition may be only used in VDF discretization. The imposed  $\partial P/\partial n$  value is expressed in  $\text{Pa.m}^{-1}$ .

**Frontiere\_ouverte\_pression\_imposee\_Orlansky:** This boundary condition may only be used with VDF discretization (\*).

(\*) **Caution:** There is no reference for pressure for these boundary conditions so it is better to add pressure condition (with **Frontiere\_ouverte\_pression\_imposee**) on one or two cells (for symmetry in a channel) of the boundary where Orlansky conditions are imposed.

### **Frontiere\_ouverte\_gradient\_pression\_libre\_VEFPreP1B**

Keyword for an outlet boundary condition in VEF P1B/P1NC like Orlansky.

Example:

Sortie **frontiere\_ouverte\_gradient\_pression\_libre\_VEFPreP1B** Champ\_front\_uniforme 1 0.

### **Frontiere\_ouverte\_gradient\_pression\_impose\_VEFPreP1B**

Keyword for an outlet boundary condition in VEF P1B/P1NC on the gradient of the pressure.

Example:

Sortie **frontiere\_ouverte\_gradient\_pression\_impose\_VEFPreP1B** Champ\_front\_uniforme 1 0.

**Paroi\_fixe:** Keyword used to designate a situation of adherence to the wall called *bord* (normal and tangential speed at the edge is zero).

**Paroi\_decalee\_Robin:** This keyword is used to designate a Robin boundary condition ( $a.u+b.du/dn=c$ ) associated with the Pironneau methodology for the wall laws. The value of given by the **delta** option is the distance between the mesh (where symmetry boundary

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condition is applied) and the fictitious wall. This boundary condition needs the definition of the dedicated source terms (**Source\_Robin** or **Source\_Robin\_Scalaire**) according the equations used. The detailed documentation is there:

[\\$TRIO\\_U\\_ROOT/doc/Trio\\_U/STMF\\_LMSF\\_NT\\_13-011A.pdf](#).

You can also see the four associated validation forms under the \$TRIO\_U\_VALIDATION/./pas\_fini directory:

Fiche\_validation\_Re180\_Pr0.025

Fiche\_validation\_Re180\_Pr0.71

Fiche\_validation\_Re395\_Pr0.71

Fiche\_validation\_Re590

**Paroi\_defilante:** This keyword is used to designate a condition where tangential speed is imposed on the wall called *bord*. If the speed set by the user is not tangential, projection is used.

**Symetrie:** This keyword is used to designate a symmetry condition concerning the speed at the boundary called *bord* (normal speed at the edge equal to zero and tangential speed gradient at the edge equal to zero).

**Periodique:** This keyword is used to indicate the fact that the horizontal speed inlet values are the same as the outlet speed values, at every moment. As regards meshing, the inlet and outlet edges bear the same name.

### **Paroi\_Knudsen\_non\_negligeable**

New boundary condition for number of Knudsen (Kn) above 0.001 where slip-flow condition appears: the velocity near the wall depends on the shear stress :

$Kn = l/L$  with  $l$  is the mean-free-path of the molecules and  $L$  a characteristic length scale.

$$U(y=0) - U_{wall} = k(dU/dY)$$

Where  $k$  is a coefficient given by several laws:

**Mawxell:**  $k = (2-s) \cdot l/s$

**Bestok&Karniadakis:**  $k = (2-s)/s \cdot L \cdot Kn / (1 + Kn)$

**Xue&Fan:**  $k = (2-s)/s \cdot L \cdot \tanh(Kn)$

$s$  is a value between 0 and 2 named accomodation coefficient.  $s=1$  seems a good value.

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*Example:*

```
boundary_conditions {
```

```
.....
```

```
    Bord1 Paroi_Knudsen_non_negligeable vitesse_paroi Champ_front_uniforme 3 0. 0. 0. k
```

```
    Champ_front_uniforme 1 0.1
```

```
}
```

*Warning:*

The keyword is available for VDF calculation only for the moment.

### **Paroi\_rugueuse**

New wall boundary condition for turbulent calculation to change the roughness constant value *Erugu* of a wall (default value 9.11). This keyword change the law for a smooth wall. It adds a constant which depends of a dimensionless roughness height:

$$k_s^+ = \frac{u_* k_s}{\nu} \text{ (where } k_s \text{ is the equivalent sand-grain roughness height)}$$

We have:

$$u^+ = \frac{1}{\kappa} \ln\left(\frac{3.93}{k_s^+} E y^+\right)$$

This law may be compared to the law for a smooth wall :

$$u^+ = \frac{1}{\kappa} \ln(E y^+)$$

With  $K=0.415$  (Von Karman constant),  $E = 9.11$  (*Erugu* value for a smooth law). To deal with this model an atmospheric boundary layer with a velocity profile :

$$U(y) = \frac{u_*}{\kappa} \ln\left(\frac{y}{y_0}\right), \text{ (where } y_0 \text{ is the aerodynamic roughness length)}$$

You may use the law with:

$$Erugu = \frac{\nu}{y_0 \cdot u_*} \text{ (where } k_s = 3.93 E y_0 \text{)}$$

## **2.13.2 THERMAL BOUNDARY CONDITIONS**

Boundary conditions that are not specific to discretization:

```
[Bord Frontiere_ouverte_temperature_imposee boundary_field_type bloc_lecture_champ]
[Bord Frontiere_ouverte_temperature_imposee_rayo_semi_transp boundary_field_type bloc_lecture_champ]

[Bord Frontiere_ouverte T_ext boundary_field_type bloc_lecture_champ]
[Bord Frontiere_ouverte_rayo_semi_transp T_Ext boundary_field_type bloc_lecture_champ]
[Bord Frontiere_ouverte_rayo_transp T_Ext boundary_field_type bloc_lecture_champ]

[Bord Symetrie]
[Bord Periodique ]

[Bord Paroi_adiabatique]
[Bord Paroi_decalee_Robin { delta value } ]
[Bord Paroi_flux_impose boundary_field_type bloc_lecture_champ]
[Bord Paroi_temperature_imposee boundary_field_type bloc_lecture_champ]
[Bord Paroi_echange_externe_impose H_imp boundary_field_type bloc_lecture_champ T_ext
boundary_field_type bloc_lecture_champ]
[Bord Paroi_contact problem_name Bord]
[Bord Paroi_contact_fictif problem_name Bord thermal_conductivity thickness]
```

*Bord*: name of the edge where the boundary condition applies.

*boundary\_field\_type*: boundary field type.

**Frontiere\_ouverte\_temperature\_imposee**: This keyword is used to set an imposed temperature condition at the open boundary called *bord* (in the case of fluid inlet). This condition must be associated with an imposed inlet speed condition. The imposed temperature value is expressed in °C or K.

**Frontiere\_ouverte\_temperature\_imposee\_rayo\_semi\_transp**: Keyword to apply the same condition for a radiation problem with semi transparent gas.

**Frontiere\_ouverte**: This keyword is used to set a boundary outlet temperature condition on the boundary called *bord* (diffusion flux zero). This condition must be associated with a boundary outlet hydraulic condition.

**Frontiere\_ouverte\_rayo\_semi\_transp**: Keyword to apply the same condition for a radiation problem with semi transparent gas.

**Frontiere\_ouverte\_rayo\_transp**: Keyword to apply the same condition for a radiation problem with transparent gas.

**T\_ext:** This keyword is used to define the temperature at the boundary.

**Symetrie:** This keyword is used to set a symmetry condition on temperature on the boundary named *bord*.

**Periodique:** This keyword is used to set a periodic condition on temperature. The two edges dealing with this periodic condition bear the same name.

**Paroi\_adiabatique:** This keyword is used to refer to a normal zero flux condition at the wall called *bord*.

**Paroi\_decalee\_Robin:** This keyword is identical to the one described here: 2.13.1.

**Paroi\_flux\_impose:** This keyword is used to refer to a normal flux condition at the wall called *bord*. The surface area of the flux ( $\text{W.m}^{-2}$ ) is imposed at the boundary according to the following convention: a positive flux is a flux that enters into the domain according to convention.

**Paroi\_temperature\_imposee:** This keyword is used to refer to an imposed temperature condition at the wall called *bord*.

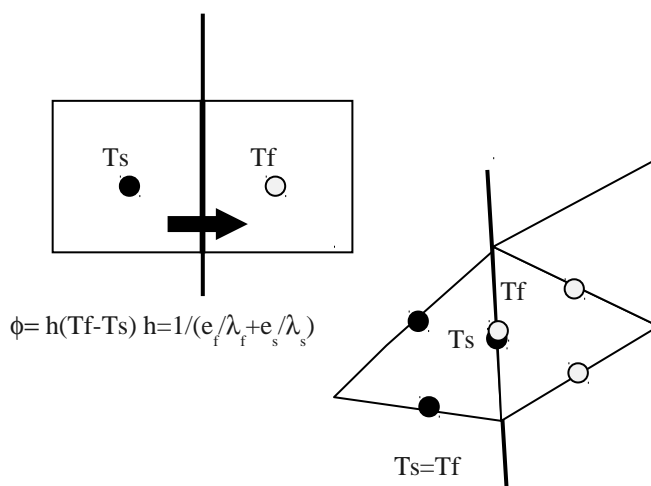
**Paroi\_echange\_externer\_impose:** This keyword is used to set an external type exchange condition with a heat exchange coefficient and an imposed external temperature.



$$\phi = h (T - T_{\text{ext}}) \text{ where } 1/h = 1/h_{\text{imp}} + e/\lambda \text{ in VDF}$$

$$\phi = h_{\text{imp}} (T - T_{\text{ext}}) \text{ in VEF}$$

**Paroi\_contact** : This keyword is used to set a thermal condition between two domains. Important: the name of the boundaries in the two domains should be the same. (Warning: there is also an old limitation not yet fixed on the sequential algorithm in VDF to detect the matching faces on the two boundaries: faces should be ordered in the same way). The kind of condition depends on the discretization. In VDF, it is a heat exchange condition, and in VEF, a temperature condition:



Such a coupling requires coincident meshes for the moment. In case of non-coincident meshes, run is stopped and two external files are automatically generated in VEF (*connectivity\_failed\_boundary\_name* and *connectivity\_failed\_pb\_name.med*). In 2D, the keyword **Decouper\_bord\_coincident** associated to the *connectivity\_failed\_boundary\_name* file allows to generate a new coincident mesh.

*Example :*

**dimension 2**

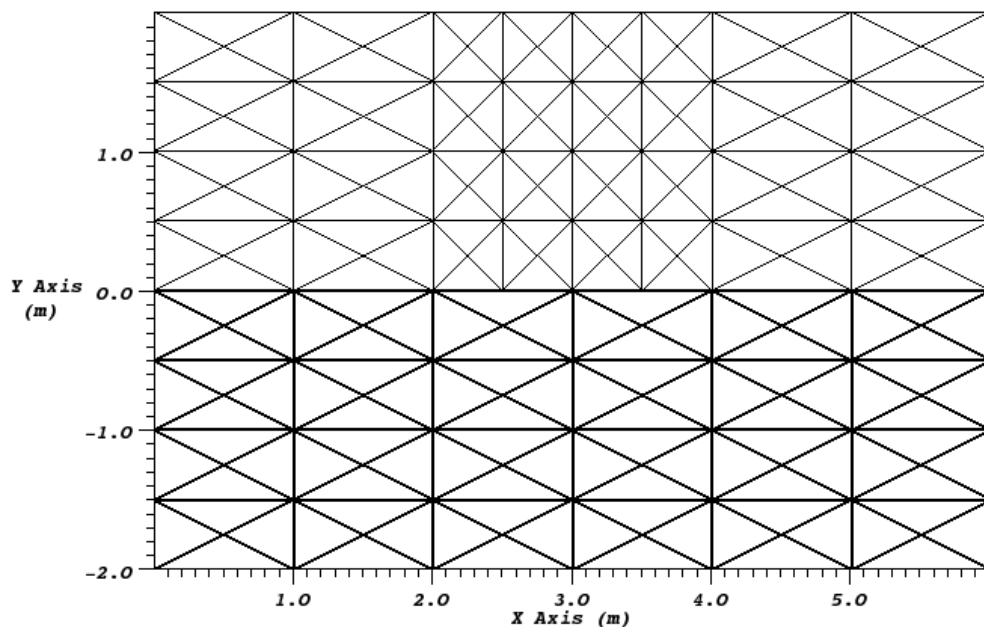
**Domaine solide**

**Read \_file** solide *solide.geom*

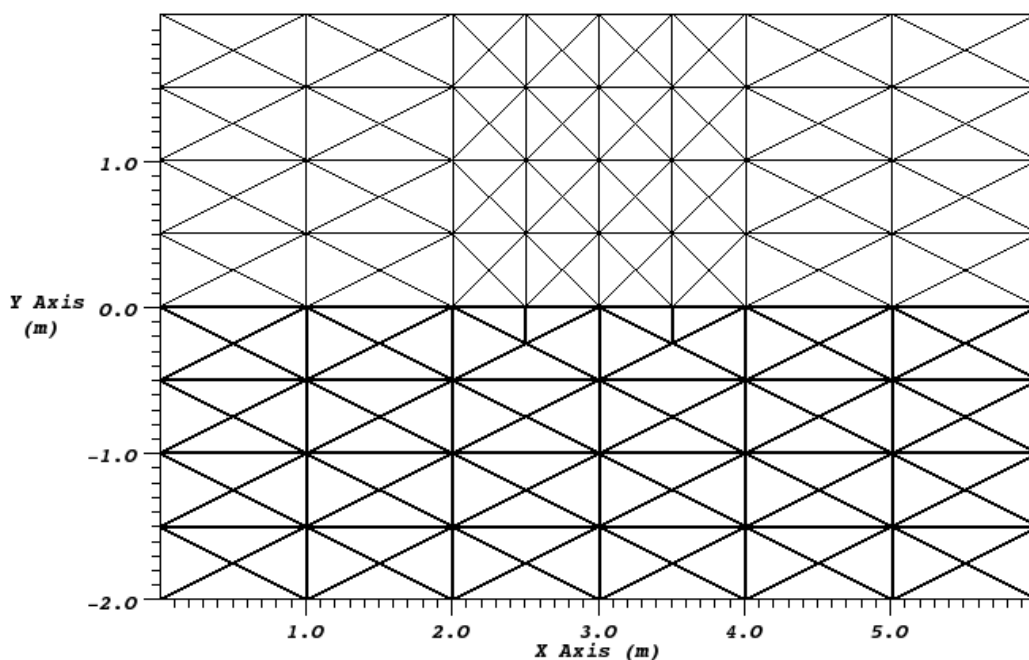
**Decouper\_bord\_coincident** solide *boundary\_name*

**Ecrire\_fichier** solide *new\_solide.geom*





The mesh before (solide in the *solide.geom* file)



The mesh after (solide in the new *solide.geom* file)

In 3D, for a first preliminary cut domain with HOMARD (fluid for instance), the second problem associated to *pb\_name* (solide in a fluid/solid coupling problem) has to be submitted to HOMARD cutting procedure with *connectivity\_failed\_pb\_name.med*.

Such a procedure works as while the primary refined mesh (fluid in our example) impacts the fluid/solid interface with a compact shape as described below (values 2 or 4 indicates the number of division from primary faces obtained in fluid domain at the interface after HOMARD cutting):

2-2-2-2-2-2					
2-4-4-4-4-2				2-2	2-2-2
2-4-4-4-4-2		2-2-2		2-4-2	2-2
2-2-2-2-2		2-4-2		2-2	2-2
		2-2			
OK				NOT OK	

**Paroi\_contact\_fictif** : This keyword is derivated from **paroi\_contact** and is especially dedicated to compute coupled fluid/solid/fluid problem in case of thin material. Thanks to this option, solid is considered as a fictitious media (no mesh, no domain associated), and coupling is performed by considering instantaneous thermal equilibrium in it (for the moment).

problem\_name : name of the problem

Bord : boundary name of the remote problem which should be the same than the local name

thermal\_conductivity : thermal conductivity

thickness : thickness of the fictitious media

## Boundary conditions specific to VDF discretization:

```
[Bord Paroi_echange_global_impose H_imp boundary_field_type bloc_lecture_champ T_ext
boundary_field_type bloc_lecture_champ]

[Bord Paroi_Echange_externe_impose_rayo_semi_transp H_imp boundary_field_type bloc_lecture_champ
T_ext boundary_field_type bloc_lecture_champ]

[Bord Paroi_Echange_contact_VDF pb2 Bord2 temperature val_h_contact ]
[Bord Echange_contact_rayo_transp_VDF pb2 Bord2 temperature temp]
[Bord Paroi_echange_contact_correlation_VDF { dir integer Tinf double Tsup double
lambda function rho function Cp double mu function debit double Dh double dt_impr double
Nu function volume function [ Reprise_correlation ] } ]
```

**Paroi\_echange\_global\_impose:** This keyword is used to set a global type exchange condition (internal) that is to say that diffusion on the first fluid mesh is not taken into consideration.

**H\_imp:** This is a keyword used to define the global exchange coefficient value. The global exchange coefficient value is expressed in  $W.m^{-2}.K^{-1}$ .

**T\_ext:** This is a keyword used to define the external temperature value. The external temperature value is expressed in °C or K.

$$\phi = h_{imp} (T - T_{ext})$$

**Paroi\_Echange\_externe\_impose\_rayo\_semi\_transp:** This keyword is used to set the same condition but for a coupled problem with radiation in semi transparent gas.

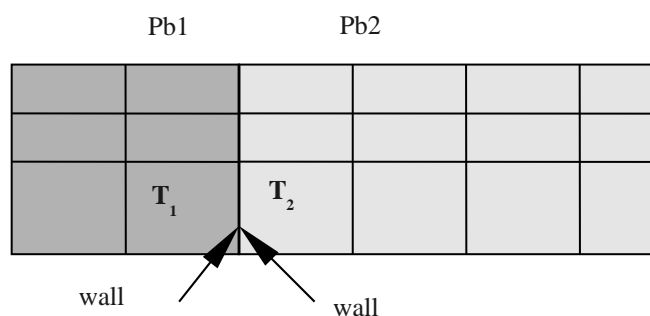
**H\_imp:** This is a keyword used to define the external exchange coefficient value. The external exchange coefficient value is expressed in  $W.m^{-2}.K^{-1}$ .

**T\_ext:** This is a keyword used to define the external temperature value. *vrel2*: external temperature value (°C or K).

In the case of a coupling, one of the following boundary condition types must be used:

**Paroi\_echange\_contact\_VDF** to model the heat flux between two problems. Important: the name of the boundaries in the two problems should be the same.

An example of using this boundary condition:



The following instruction will be found in the pb1 read block:

wall **Paroi\_Echange\_contact\_VDF** pb2 wall **temperature** val\_h\_contact

The following instruction will be found in the pb2 read block

wall **Paroi\_Echange\_contact\_VDF** pb1 wall **temperature** val\_h\_contact

*val\_h\_contact*: this corresponds to the value assigned to a coefficient (expressed in  $W.K^{-1}m^{-2}$ ) that characterises the contact between the two mediums. In order to model perfect contact, *val\_h\_contact* must be taken to be infinite. This value must obviously be the same in both the pb1 and pb2 blocks.

The surface thermal flux exchanged between the two mediums is represented by:

$$\phi = h (T_1 - T_2) \text{ where } 1/h = d_1/\lambda_1 + 1/\text{val\_h\_contact} + d_2/\lambda_2$$

where  $d_i$ : distance between the node where  $T_i$  and the wall is found.

**Echange\_Contact\_Rayo\_Transp\_VDF:** This keyword is used to set an exchange boundary condition in VDF between the fluid and the solid for a problem coupled with radiation. Without radiation, it is the equivalent of the `Paroi_Echange_contact_VDF` exchange condition. Refer to the definition of the latter for identical syntax.

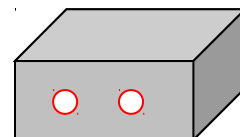
*Bord1, Bord2:* Names of the edges in contact.

*Pb:* Name of the opposed problem of which Bord2 (edge2) is one of the domain boundaries.

**temperature val\_h\_contact:** Keyword used to specify the value of a coefficient (expressed in  $\text{W.K}^{-1}\text{m}^{-2}$ ) which characterises contact between the two mediums. To model perfect contact, *val\_h\_contact* must be taken to be infinite. This value must obviously be the same in both the pb1 and pb2 blocks

**Paroi\_echange\_contact\_correlation\_VDF :** This keyword is used to define a thermal hydraulical 1D model which will apply to a boundary of 2D or 3D domain.

Example: Conduction will be calculated in the 3D gray domain, whereas 1D model will apply in the channel. The boundary condition applying on to the red boundary are defined with the following parameters:



**dir** integer : Direction (0 : axis X, 1 : axis Y, 2 : Axis Z) of the 1D model

**Tinf** double : Inlet fluid temperature of the 1D model ( $^{\circ}\text{C}$  or K)

**Tsup** double : Outlet fluid temperature of the 1D model ( $^{\circ}\text{C}$  or K)

**lambda** function : Thermal conductivity of the fluid ( $\text{W.m}^{-1}\text{K}^{-1}$ )

**rho** function : Mass density of the fluid ( $\text{kg.m}^{-3}$ ) which may be a function of the temperature T

**Cp** double : Calorific capacity value at a constant pressure of the fluid ( $\text{J.kg}^{-1}\text{K}^{-1}$ )

**mu** function : Dynamic viscosity of the fluid ( $\text{kg.m}^{-1}\text{s}^{-1}$ ) which may be a function of the temperature T

**debit** double : Surface flow rate ( $\text{kg.s}^{-1}\text{m}^{-2}$ ) of the fluid into the channel

**Dh** double : Hydraulic diameter (m) of the channel

**dt\_impr** double : Printing period in *name\_of\_data\_file\_time.dat* files of the 1D model results

**Nu** function : Nusselt number which may be a function of the Reynolds number (Re) and the Prandtl number (Pr)

**volume** function : Exact volume of the 1D domain ( $\text{m}^3$ ) which may be a function of the hydraulic diameter (Dh) and the lateral surface (S) of the meshed boundary

**Reprise\_correlation** Optional keyword in the case of a restarting calculation with this correlation

**Warning:** For parallel calculation, the only possible partition will be according the axis of the model with the keyword `Tranche`.

Example:

```

INTERFACE Paroi_Echange_contact_Correlation_VDF
{
    dir 2
    Tinf 1180
    Tsup 751
    lambda 2.774e-3*T^0.701
    rho 90e5/(2077.22*T+90e5*(9.5e-4+9.5e-4/(1-3.4e-2*T)+2.74e-3/(1+9.4e-4*T)))
    Cp 5193
    mu 3.953e-7*T^0.687
    debit -109.5
    Dh 0.016
    dt_impr 0.1
    Nu 0.023*Re^0.8*Pr^(1./3.)
    volume S*Dh*3.1415927/16
}

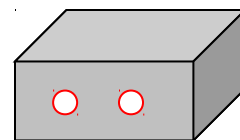
```

Boundary conditions specific to VEF discretization:

[Bord **Paroi\_echange\_contact\_correlation\_VEF** { **dir** integer **Tinf** double **Tsup** double  
**lambda** function **rho** function **Cp** double **mu** function **debit** double **Dh** function **dt\_impr** double  
**Nu** function **surface** function **N** integer **xinf** double **xsup** double [ **Reprise\_correlation** ] } ]

**Paroi\_echange\_contact\_correlation\_VEF** : This keyword is used to define a thermal hydraulic 1D model which will apply to a boundary of 2D or 3D domain.

It has the same options of **Paroi\_echange\_contact\_correlation\_VDF** keyword minus the **volume** option and plus the following options:



**Dh** function : Hydraulic diameter may be a function  $f(x)$  with  $x$  position along the 1D axis ( $xinf \leq x \leq xsup$ )

**surface** function : Section surface of the channel which may be function  $f(Dh, x)$  of the hydraulic diameter ( $Dh$ ) and  $x$  position along the 1D axis ( $xinf \leq x \leq xsup$ )

**N** integer: Number of 1D cells of the 1D mesh

**xinf** double: Position of the inlet of the 1D mesh on the axis direction

**xsup** double: Position of the outlet of the 1D mesh on the axis direction

**Reprise\_correlation** Optional keyword in the case of a restarting calculation with this correlation

**Warning:** For parallel calculation, the only possible partition will be according the axis of the model with the keyword **Tranche\_geom**.

Example:

```

INTERFACE Paroi_Echange_contact_Correlation_VDF

```

```

{
    dir 2
    Tinf 1180
    Tsup 751
    lambda 2.774e-3*T^0.701
    rho 90e5/(2077.22*T+90e5*(9.5e-4+9.5e-4/(1-3.4e-2*T)+2.74e-3/(1+9.4e-4*T)))
    Cp 5193
    mu 3.953e-7*T^0.687
    debit -109.5
    Dh 0.016
    dt_impr 0.1
    Nu 0.023*Re^0.8*Pr^(1./3.)
    Surface 3.1415/4*Dh*Dh
    N 20
    xinf 0.
    xsup 0.8
}

```

### 2.13.3 BOUNDARY CONDITIONS IN CONCENTRATION

```

[Bord Frontiere_ouverte_concentration_imposee boundary_field_type bloc_lecture_champ_front]
[Bord Frontiere_ouverte C_ext boundary_field_type bloc_lecture_champ_front]
[Bord Paroi]
[Bord Paroi_flux_impose boundary_field_type bloc_lecture_champ_front]
[Bord Symetrie]
[Bord Periodique ]

```

*Bord*: name of the edge where the boundary condition is applied.

**Frontiere\_ouverte\_concentration\_imposee**: Keyword used to set an imposed concentration condition at an open boundary called *bord* (situation corresponding to a fluid inlet). This condition must be associated with an imposed inlet speed condition.

**Frontiere\_ouverte**: This keyword is used to refer to a boundary outlet condition on the boundary called *bord* (zero diffusion flux). This condition must be associated with a boundary outlet hydraulic condition.

**C\_ext**: This keyword is used to describe concentration at a boundary.

**Paroi**: This keyword is used to refer to an impermeability condition at a wall called *bord* (standard flux zero). This condition must be associated with a wall type hydraulic condition.

**Paroi\_flux\_impose:** This keyword is used to set a flux boundary condition. If U is the unit of the concentration C, the flux value ( $D \cdot \text{grad}C \cdot n$ ) is given in  $\text{ms}^{-1}U$  and should be a positive quantity if flux is oriented outside to inside the domain.

**Symetrie:** This is a keyword used to refer to a symmetrical condition applied to constituent concentration at the boundary called *bord*.

**Periodique:** This keyword is used to set a periodic condition on temperature. The two edges dealing with this periodic condition bear the same name.

## 2.13.4 BOUNDARY CONDITIONS FOR TURBULENCE

```
[Bord Frontiere_ouverte_K_Eps_impose boundary_field_type bloc_lecture_champ_front]
[Bord Frontiere_ouverte_K_Eps_ext boundary_field_type bloc_lecture_champ_front]
[Bord Paroi]
[Bord Symetrie]
[Bord Periodique]
[Bord Frontiere_ouverte_Fluctu_Temperature_imposee boundary_field_type bloc_lecture_champ_front ]
[Bord Frontiere_ouverte_Fluctu_Temperature_ext boundary_field_type bloc_lecture_champ_front]
[Bord Frontiere_ouverte_Flux_Chaleur_Turbulente_imposee boundary_field_type
bloc_lecture_champ_front ]
[Bord Frontiere_ouverte_Flux_Chaleur_Turb_ext boundary_field_type bloc_lecture_champ_front]
```

*Bord*: name of the edge where the boundary condition applies.

**Frontiere\_ouverte\_K\_eps\_impose:** Keyword used to refer to a turbulence condition imposed on an open boundary called Bord (this situation corresponds to a fluid inlet). This condition must be associated with an imposed inlet speed condition.

**Frontiere\_ouverte:** Keyword used to refer to a boundary outlet condition on the boundary called Bord (zero diffusion flux). This condition must be associated with a boundary outlet hydraulic condition.

**K\_Eps\_ext:** This is a keyword used to define the kinetic energy and turbulent dissipation rate for the boundary.



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The kinetic energy is expressed in  $\text{m}^2.\text{s}^{-2}$ .

The turbulent dissipation rate is expressed in  $\text{m}^2.\text{s}^{-3}$ .

**Paroi:** This is a keyword used to refer to a zero flux condition at the wall called Bord ( $\epsilon$  null and k standard flux). This condition must be associated with a paroi (wall) type hydraulic condition. Caution: this keyword should not be confused with the wall laws which are applicable to static walls when no turbulence condition is applied to them.

**Symetrie:** This keyword is used to refer to a symmetry condition for k and  $\epsilon$  on the boundary called Bord.

**Periodique:** This keyword is used to set a periodic boundary condition for k and  $\epsilon$  on the boundary called Bord.

## 2.14 HYDRAULIC SOURCE TERMS

To introduce a source term into an equation, add the following line into the block defining the equation. The list of source keyword is described below.

```
Sources { source_keyword }
```

To introduce several source terms into the same equation, the blocks corresponding to the various terms need to be separated by a comma:

```
Sources { source_keyword1 , source_keyword2 , ... }
```

### 2.14.1 PRESSURE LOSS TYPE SOURCE TERMS (VDF DISCRETIZATION)

```
Perte_Charge_Reguliere type_perte_charge bloc_definition_pertes_charges
```

**Perte\_Charge\_Reguliere:** source term modelling the presence of a bundle of tubes in a flow.

*type\_perte\_charge:* there are two types of options available: **Longitudinale** or **Transversale**: the first may be used to define pressure loss in the direction of the tube bundle and the second to define the pressure loss in the direction perpendicular to the tube bundle.

The two types of pressure loss definition blocks are as follows:

<b>Perte_Charge_Reguliere</b>	<b>Longitudinale</b>	direction_application
valeur_diametre_hydraulique A val B val nom_sous_zone		

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*direction\_application*: keyword which may be selected from among **X**, **Y** or **Z**.

*valeur\_diamètre\_hydraulique*: tube bundle hydraulic diameter value. This value is expressed in m.

**A** val **B** val: These keywords are used to set law coefficient values for the coefficient of regular pressure losses which are written as follows:

$$\Lambda = A \cdot Re^{-B}$$

*nom\_sous\_zone*: name of the sub area occupied by the tube bundle. A **Sous\_Zone** (Sub-area) type object called *nom\_sous\_zone* (sub\_area\_name) should have been previously created (refer to 2.3.23).

#### **Perte\_Charge\_Reguliere Transversale**

*direction\_application* *valeur\_pas\_faisceau* **d** *valeur\_d* **A** val **B** val *nom\_sous\_zone*

*direction\_application*: keyword which may be selected from among **X**, **Y** or **Z**.

*valeur\_pas\_faisceau*: value of the tube bundle step.

*valeur\_d*: value of the tube external diameter

**A** val **B** val: These keywords are used to set the law coefficient values for the coefficient of regular pressure losses which is written as follows:

$$\Lambda = A \cdot Re^{-B}$$

*nom\_sous\_zone*: name of the sub-area occupied by the tube bundle. A **Sous\_Zone** (Sub-area) type object called *nom\_sous\_zone* (sub\_area\_name) should have been previously created (refer to 0).

## **2.14.2 PRESSURE LOSS TYPE SOURCE TERMS (VEF DISCRETIZATION)**

```

Perte_Charge_Directionnelle { diam_hydr field_type
    lambda function
    direction field_type
    [ sous_zone name ] }

```

**Perte\_Charge\_Directionnelle:** Keyword for directional pressure loss.

**diam\_hydr** field\_type : Hydraulic diameter value.

**lambda** function : Function for loss coefficient which may be Reynolds dependant (Ex: 64/Re)

**direction** field\_type : Field which indicates the direction of the pressure loss.

**sous\_zone** name : Optional sub-zone where pressure loss applies.

```

Perte_Charge_Isotrope { diam_hydr field_type
    lambda function
    [ sous_zone name ] }

```

**Perte\_Charge\_Isotrope** : Keyword for isotropic pressure loss. Same parameters as **Perte\_Charge\_Directionnelle** except **direction** keyword.

```

Perte_Charge_Anisotrope { diam_hydr field_type
    lambda function
    lambda_ortho function
    direction field_type
    [ sous_zone name ] }

```

**Perte\_Charge\_Anisotrope** : Keyword for anisotropic pressure loss. Same parameters as **Perte\_Charge\_Directionnelle** plus:

**lambda\_ortho** function: Function for loss coefficient in transverse direction which may be Reynolds dependant (Ex: 64/Re)

```

Perte_Charge_Circulaire {
    diam_hydr field_type
    diam_hydr_ortho field_type
    lambda function
    lambda_ortho function
    direction field_type
    [ sous_zone name ] }

```

**Perte\_Charge\_Circulaire** : Keyword as anisotropic pressure loss (**Perte\_Charge\_Anisotrope**) but with 3 Reynolds numbers:

$$Re_{tot} = \frac{\|U\|D}{\nu}$$

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$$Re_{long} = \frac{U \cdot nD}{\nu}$$

$$Re_{ortho} = \frac{\|U - U \cdot nn\| Do}{\nu}$$

Defined thanks:

U: Velocity vector

n : Vector direction of the pressure loss given by the **direction** option

D : Hydraulic diameter given the **diam\_hydr** option

Do : Transverse hydraulic diameter given the **diam\_hydr\_ortho** option

$\nu$ : Kinematic viscosity

**lambda** function : Function f(Re\_tot, Re\_long, t, x, y, z) for loss coefficient in the longitudinal direction

**lambda\_ortho** function: Function f(Re\_tot, Re\_ortho, t, x, y, z) for loss coefficient in transverse direction

### 2.14.3 PRESSURE LOSS TYPE SOURCE TERMS (VDF OR VEF DISCRETIZATIONS)

**Perte\_Charge\_Singuliere** **KX** | **KY** | **KZ** coefficient\_value { [ X | Y | Z = location *subzone\_name* ] / Surface *dom* }

**Perte\_Charge\_Singuliere**: source term that is used to model a pressure loss over a surface area (transition through a grid, sudden enlargement).

The surface can be defined:

- either by the faces of elements located on the intersection of a subzone named *subzone\_name* and a X,Y, or Z plane located at X,Y or Z = location.
- or by the faces of the domain 2D named *dom*. This option is only available in 3D and for VEF discretization. The surface *dom* may be an inner surface extracted via *Extraire\_Surface* keyword or may be a domain read in Med file.

**KX**, **KY** or **KZ** keyword specify the directional pressure loss coefficient\_value for respectively a X, Y or Z direction.

Example : **sources** { **Perte\_Charge\_Singuliere** **KX** 0.5 { **X** = 0.35 sous\_zone\_toto } }

## 2.14.4 MOMENTUM SOURCE TERMS

<p><b>Source_Qdm</b>   <i>field_type</i>   <i>field_description</i></p>
---

Momentum source term in the Navier Stokes equation.

<p><b>Canal_perio</b> { <b>bord</b> boundary_name [<b>h</b> value] [ <b>coeff</b> value] [ <b>debit_impose</b> double ] }</p>
---

Momentum source term to maintain flow rate :

**Canal\_perio**: Keyword for the source term.

**bord** boundary\_name : The name of the (periodic) boundary normal to the flow direction.

**h** value: Half height of the channel. Optional.

**coeff** value: Damping coefficient (optional, default value is 10).

**debit\_impose** double : Optional option to specify the aimed flow rate  $Q(0)$ . If not used,  $Q(0)$  is computed by the code after the projection phase, where velocity initial conditions are slightly changed to verify incompressibility.

The expression of the source term is:

$$S(t) = (2*(Q(0) - Q(t)) - (Q(0) - Q(t-dt)))/(coeff*dt*area)$$

Where:

coeff=damping coefficient

area=area of the periodic boundary

$Q(t)$ =flow rate at time  $t$

dt=time step

Three files will be created during calculation on a datafile named DataFile.data. The first file contains the flow rate evolution. The second file is useful for restarting a calculation with the flow rate of the previous stopped calculation, and the last one contains the pressure gradient evolution:

-DataFile\_Channel\_Flow\_Rate\_ProblemName\_BoundaryName

-DataFile\_Channel\_Flow\_Rate\_repr\_ProblemName\_BoundaryName

-DataFile\_Pressure\_Gradient\_ProblemName\_BoundaryName

```

Sources_Qdm_lambdaup { lambda value
    [lambda_min value]
    [lambda_max value]
    [ubar_umprim_cible value] }

```

This source term is a dissipative term which is intended to minimise the energy associated to non-conform scales  $u'$  (responsible for spurious oscillations in some cases). The equation for these scales can be seen as:

$$du'/dt = -\lambda u' + \text{grad } P'$$

where  $-\lambda u'$  represents the dissipative term, with  $\lambda = a/\Delta t$

Optional values **lambda\_main** and **lambda\_max** give the minimal and maximal value for  $\lambda$  whereas **ubar\_umprim\_cible** is a threshold in the  $\lambda$  algorithm calculation (by default 0.1).

For Crank-Nicholson temporal scheme, recommended value for  $a$  is 2.

```

Sources { Source_Qdm_lambdaup { lambda 2. } }

```

Remark:

This method requires to define a filtering operator : see **solveur\_bar**

```

Source_Robin N boundary_name_1 ... boundary_name_N dt_impr

```

This source term should be used when a **Paroi\_decalee\_Robin** boundary condition is set in a hydraulic equation. The source term will be applied on the N specified boundaries. The last value *dt\_impr* is a printing period into the files *reynolds\_tau.dat* and *u\_tau.dat*.

```

Acceleration { [vitesse time_field] acceleration time_field omega time_field domegadt time_field
centre_rotation time_field [ option terme_complet|coriolis_seul|entrainement_seul ] }

```

Momentum source term to take in account the forces due to rotation or translation of a non Galilean referential  $R'$  (centre  $O'$ ) into the Galilean referential  $R$  (centre  $O$ ).

**acceleration** time\_field: Keyword for the acceleration of the referential  $R'$  into the  $R$  referential ( $d^2OO'/dt^2$  term [ $m.s^{-2}$ ]). time\_field is a time dependant field (eg: **Champ\_Fonc\_t**).

**vitesse** time\_field: Optional keyword for the velocity of the referential  $R'$  into the  $R$  referential ( $dOO'/dt$  term [ $m.s^{-1}$ ]). The velocity is mandatory when you want to print the total cinetic energy into the non-mobile Galilean referential  $R$  (see **Ec\_dans\_repere\_fixe** keyword).

**omega** time\_field: Keyword for a rotation of the referential R' into the R referential [rad.s<sup>-1</sup>]. time\_field is a 3D time dependant field specified for example by a **Champ\_Fonc\_t** keyword. The time\_field field should have 3 components even in 2D (In 2D: 0 0 omega).

**domegadt** time\_field: Keyword to define the time derivative of the previous rotation [rad.s<sup>-2</sup>]. Should be zero if the rotation is constant. The time\_field field should have 3 components even in 2D (In 2D: 0 0 domegadt).

**centre\_rotation** time\_field: Keyword to specify the centre of rotation (expressed in R' coordinates) of R' into R (if the domain rotates with the R' referential, the centre of rotation is 0'=(0,0,0)). The time\_field should have 2 or 3 components according the dimension 2 or 3.

**option terme\_complet|coriolis\_seul|entrainement\_seul** : Optional keyword to specify the kind of calculation. **terme\_complet** (default option) will calculate both the Coriolis and centrifugal forces, **coriolis\_seul** will calculate the first one only, **entrainement\_seul** will calculate the second one only.

The source term can be reported in results files with the **Acceleration\_terme\_source** keyword.

## 2.14.5PORIUS MEDIA SOURCE TERMS

Darcy source term with constant permeability :

```
Darcy { modele_K K_constant { valeur value } }
```

Darcy source term with Ergun's law permeability:

```
Darcy { porosite value modele_K ErgunDarcy { diametre value } }
```

This keyword is used for calculation in a porius media with source term of Darcy  $-\nu/K \cdot V$ . This keyword must be used with a **permeability model**. For the moment there are two models :permeability constant or Ergun's law. Darcy source term is **available for quasi compressible** calculation.A new keyword is aded for porosity (**porosite**)

Forcheimer source term with Ergun's law :



**Forchheimer** { **porosite** value **Cf** value **modele\_K** ErgunForchheimer { **diametre** value } }

Forcheimer source term with the constant law :

**Forchheimer** { **Cf** value **modele\_K** **K\_constant** { **valeur** value } }

This keyword makes it possible to add the source term of Forchheimer  $-Cf/\sqrt{K} \cdot V^2$  in the Navier Stokes equations. Like the term of Darcy, we must precise a permeability model : constant or Ergun's law. Moreover we can give the constant Cf : by default its value is 1. Forchheimer source term is **available also for quasi compressible** calculation. A new keyword is added for porosity (**porosite**)

## 2.14.6 BOUSSINESQ TYPE SOURCE TERMS

**Boussinesq\_temperature** { **T0** *vrel* [ **verif\_boussinesq** 0|1 ] }

**Boussinesq\_temperature**: Keyword used to describe a source term that couples the movement quantity equation and energy equation with the Boussinesq hypothesis.

**T0**: Keyword used to describe the reference temperature.

*vrel*: reference temperature value (°C or K). It can also be a time dependant function since the 1.6.6 version.

**verif\_boussinesq**: Optional keyword to check (1) or not (0) the reference temperature in comparison with the mean temperature value in the domain. It is set to 1 by default.

**Boussinesq\_concentration** { **C0** N **C0(1)** .... **C0(N)** [ **verif\_boussinesq** 0|1 ] }

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**Boussinesq\_concentration:** Keyword used to describe a source term that couples the movement quantity equation and constituent transportation equation with the Boussinesq hypothesis

**C0:** Keyword used to describe the reference concentration.

N : Number of constituents

C0(i) : Values for reference concentration for each constituent (may be time dependant since the 1.6.8 version).

**verif\_boussinesq:** Optional keyword to check (1) or not (0) the reference concentration in comparison with the mean concentration value in the domain. It is set to 1 by default.

## 2.14.7CORIOLIS

**Coriolis { omega value }**

Keyword for a Coriolis term in hydraulic equation.

Example: (See also the test case Coriolis)

Sources { **Coriolis { omega 2 0.1 }** }

**Warning:** Only available in VDF.

## 2.15 SCALAR SOURCE TERMS

**Source\_Th\_TdivU**

This term source is dedicated for any scalar (called "T") transportation. Coupled with upwind ("amont") or muscl scheme, this term gives for final expression of convection :  $\text{div}(\mathbf{U}.T) - T.\text{div}(\mathbf{U}) = \mathbf{U}.\text{grad}(T)$

This ensures, in incompressible flow when divergence free is badly resolved, to stay in a better way in the physical boundaries.

**Warning:** Only available in VEF discretization.

### 2.15.1 THERMAL SOURCE TERMS

**Puissance\_thermique** *field\_type bloc\_lecture\_champ*

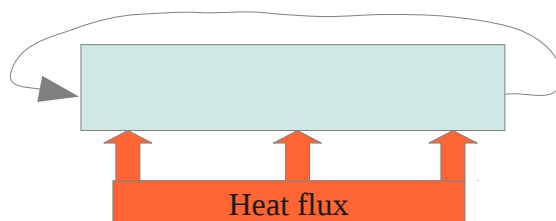
**Puissance\_thermique:** This keyword is used to define a source term corresponding to a volume power release in the energy equation.

*field\_type* : thermal power field type. To impose a volume power on a domain sub-area, the **Champ\_Uniforme\_Morceaux (partly\_uniform\_field)** type must be used.

**Warning:** The volume thermal power is expressed in  $\text{W.m}^{-3}$  in 3D. It is a power per volume unit (in a porous media, it is a power per fluid volume unit).

**Canal\_perio** { **bord** boundary\_name }

Energy source term to add in a periodic channel with heat flux boundary conditions:



**Canal\_perio:** Keyword for the source term.

**bord** boundary\_name : The name of the (periodic) boundary normal to the flow direction.

The expression of the implemented source term is:

$$S(x,y,z,t) = -V(x,y,z,t)*ImposedHeatFlux/(\rho*Cp*Volume*ChannelBulkVelocity)$$

Where:

$V(x,y,z,t)$ =velocity according to the periodic direction

Volume=Volume of the fluid

ImposedHeatFlux=Heat flux imposed on the periodic channel walls

ChannelBulkVelocity= Bulk velocity=Flow rate / area of the periodic boundary

**Warning:** Available in VEF only in the 1.6.8 version.

**Source\_Robin\_Scalaire** N boundary\_name\_1 temp\_wall\_value1 ...  
boundary\_name\_N temp\_wall\_valueN  
dt\_impr

This source term should be used when a **Paroi\_decalee\_Robin** boundary condition is set in a an energy equation. The source term will be applied on the N specified boundaries. The values temp\_wall\_valueI are the temperature specified on the Ith boundary. The last value dt\_impr is a printing period which is mandatory to specify in the data file but has no effect yet.

## 2.15.2GENERIC SOURCE TERM

**Source\_Generique** field\_type bloc\_lecture\_champ

**Source\_Generique** : This keyword is used to define a source term depending on some discrete fields of the problem and (or) analytic expression. It is expressed by the way of a generic field usually used for post-processing.

*field\_type* : generic field type (see §2.19.3).

## 2.16 TURBULENCE MODELS

The turbulence models described hereunder may only be used in discretization. A turbulence model is selected in the hydraulic equation. For scalar convection diffusion equations coupled with the hydraulic equation, a turbulence model is selected as a function of that which was selected for the hydraulic equation.

### 2.16.1 MODELS FOR NAVIER STOKES EQUATIONS

#### 2.16.1.1 SUB-GRID SCALE MODELS

```

Modele_turbulence model
{
  [ Cs valeur ]
  [ longueur_maille Characteristic_length ]
  Turbulence_paroi law...
  [ Correction_visco_turb_pour_controle_pas_de_temps ]
  [ Correction_visco_turb_pour_controle_pas_de_temps_parametre value ]
}

```

**Turbulence\_paro**i: This keyword is used to define the wall turbulence model equations. Refer to 2.16.3.1.

**Cs** value: This is an optional keyword and the value is used to set the constant used in the model. (This is currently only valid for Smagorinsky models and it is set to 0.18 by default.)

**Correction\_visco\_turb\_pour\_controle\_pas\_de\_temps** : Keyword to set a limitation to low time steps due to high values of turbulent viscosity. The limit for turbulent viscosity is calculated so that diffusive time-step is equal or higher than convective time-step. For a stationary flow, the correction for turbulent viscosity should apply only during the first time steps and not when permanent state is reached. To check that, we could post process the **corr\_visco\_turb** field which is the correction of turbulent viscosity: it should be 1. on the whole domain.

**Correction\_visco\_turb\_pour\_controle\_pas\_de\_temps\_parametre** value : Keyword as **Correction\_visco\_turb\_pour\_controle\_pas\_de\_temps** to set a limitation to high values of turbulent viscosity. The specified value is the desired ratio between diffusive time step and convective time step. The value should be greater than 0 and lesser or equal to 1. If set to 1, it is equivalent to the **Correction\_visco\_turb\_pour\_controle\_pas\_de\_temps** keyword.

*Characteristic\_length*: different ways to calculate the characteristic length may be specified :

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**volume** : (by default) characteristic length is based on the cubic square of volume cells. (To avoid discontinuities of this quantity in VEF from a cell to another, a smoothing procedure is applied)

**volume\_sans\_lissage** : for VEF only - the same as previously without smoothing procedure

**Scotti** : **volume** \* Scotti's correction to take into account the stretching of the cell in case of anisotropic meshes.

**arete** : for VEF only - characteristic length relies on the max edge (+ smoothing procedure)

The model keyword may be:

**Sous\_maille**: This keyword is entered to use a structure sub-grid function model.

**Sous\_maille\_selectif**: This keyword is entered to use the selective structure sub-grid function model. This model is derived from the previous model: the only difference is that a filter is applied to the structure function.

The two last keywords for LES models has new options:

**formulation\_a\_nb\_points 4 dir1 dir2** : The structure fonction is calculated on four points and we should add the 2 directions (0:OX, 1:OY, 2:OZ) constituting the homegeneity planes. Example for channel flows, planes parallel to the walls.

**formulation\_a\_nb\_points 6** : By default, the structure fonction is calculated on six points.

**Sous\_maille\_axi**: This keyword is entered to indicate usage of the structure sub-grid function turbulence model available in cylindrical co-ordinates.

**Sous\_maille\_Smago**: This keyword is used to indicate that the Smagorinsky sub-grid turbulence model should be used.

$$\text{Nut} = \text{Cs} * \text{Cs} * \ell * \ell * \sqrt{2 * S * S} \quad (\text{Cs} = 0.18 \text{ by default})$$

**Sous\_maille\_smago\_dyn**: This keyword is used to indicate that the dynamic sub-grid model should be used (available in VDF discretization only). Options are available :

```

Modele_turbulence Sous_maille_smago_dyn
{
  stabilise
  [ 6_points ]
  [ plans_paralleles nb_points integer ]
  [ moy_euler ]
  [ moy_lagrange ]
  Turbulence_paroi law...
  [ Correction_visco_turb_pour_controle_pas_de_temps ]
}

```

**Sous\_maille\_smago\_filtre:** This keyword is used to indicate that the Smagorinsky sub-grid turbulence model should be used with low-filter.

**Sous\_maille\_selectif\_mod:** Keyword with this model (in VDF only).

**Sous\_maille\_1elt\_selectif\_mod:** Keyword for VEF calculation with this model.

**THI** *ki kc*: For homogeneous isotropic turbulence (THI), two integers *ki* and *kc* are needed in VDF (not in VEF).

**Canal** *h dir\_faces\_paro*i: For a channel flow, the half width *h* and the orientation of the wall *dir\_faces\_paro*i are needed.

**formulation\_a\_nb\_points** *4 dir1 dir2*: The structure function is calculated on four points and we should add the 2 directions (0:OX, 1:OY, 2:OZ) constituting the homogeneity planes. Example for channel flows, planes parallel to the walls.

*Example:*

```

Read pb
{
  Navier_Stokes_Turbulent {
    solveur_pression GCP { ... }
    convection { Centre }
    diffusion { }
    conditions_initiales { ... }
    boundary_conditions { ... }
    Sources { ... }
    Modele_turbulence sous_maille_selectif_mod {
      Turbulence_paroi negligeable
      THI 2 4
    }
    Traitement_particulier { ... }
  }
}

```

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## Sous\_maille\_wale

The WALE model is a new sub-grid scale model for eddy-viscosity in LES that has the following properties :

- it goes naturally to 0 at the wall (it doesn't need any information on the wall position or geometry)
- it has the proper wall scaling in  $o(y^3)$  in the vicinity of the wall
- it reproduces correctly the laminar to turbulent transition.

The unique parameter of this sgs model is the value of the constant,  $C_w$ , whose default value 0.5.

*Example:*

Modele\_turbulence **sous\_maille\_wale**

```
{
    turbulence_paroι negligible
    cw 0.5
    Correction_visco_turb_pour_controle_pas_de_temps
}
```



Availability as a function of discretization is as follows:

<i>Model</i>	<i>VDF</i>	<i>VEF</i>
<b>Sous_maille</b>	YES	YES
<b>Sous_maille_selectif</b>	YES	YES
<b>Sous_maille_axi</b>	YES	NO
<b>Sous_maille_DSGS</b>	YES	NO
<b>Sous_maille_Smago</b>	YES	YES
<b>Sous_maille_Smago_filtre</b>	YES	YES
<b>Sous_maille_selectif_mod</b>	YES	NO
<b>Sous_maille_1elt_selectif_mod</b>	NO	YES
<b>Sous_maille_wale</b>	YES	YES

## 2.16.1.2 THE MIXING LENGTH MODEL

```

Modele_turbulence Longueur_Melange
{
  Turbulence_paro law
  [ Fichier ] domainname_Wall_length.xyz
  [ dmax value ]
  [ Canalx height ] [ Tuyaux|Tuyauy|Tuyauz diameter ]
  [ Correction_visco_turb_pour_controle_pas_de_temps ]
  [ Fichier_ecriture_K_Eps filename.med ]
}

```

**Longueur\_Melange** : (following keywords are available in VEF only). This model is based on mixing length modelling. For a non academic configuration (see below), formulation used in the code can be expressed basically as :

$$\nu_t = (\text{Kappa} \cdot y)^2 \cdot dU/dy$$

Till a maximum distance (**dmax**) set by the user in the data file, "y" is set equal to the distance from the wall (dist\_w) calculated previously and saved a file *domainname\_Wall\_length.xyz*. [see Distance\_paro keyword]

Then (from y=dmax), "y" decreases as an exponential function :

$$y = dmax \cdot \exp[-2 \cdot (dist_w - dmax)/dmax]$$

### Example:

Modele\_turbulence Longueur\_Melange

```
{
    turbulence_paroil loi_standard_hydr dt_impr_ustar 0.00001
    dmax 0.3 fichier dom_Wall_length.xyz
}
```

In some cases (academic configurations like pipe, channel, or, experimental ones), it is recommended to use the following data :

**Canalx** [height] : plane channel according to Ox direction (for the moment, formulation in the code relies on fixed heigh : H=2)

**Tuyaux** | **Tuyauz** | **Tuyauz** [diameter] : pipe according to Ox, Oy or Oz direction (for the moment, formulation in the code relies on fixed diameter : D=2)

**Correction\_visco\_turb\_pour\_controle\_pas\_de\_temps** : Keyword to set a limitation to low time steps due to high values of turbulent viscosity. The limit for turbulent viscosity is calculated so that diffusive time-step is equal or higher than convective time-step. For a stationary flow, the correction for turbulent viscosity should apply only during the first time steps and not when permanent state is reached. To check that, we could post process the **corr\_visco\_turb** field which is the correction of turbulent viscosity: it should be 1. on the whole domain.

**Fichier\_ecriture\_K\_eps** : When a restart with k-epsilon model is envisaged, this keyword allows to generate external MED-format file with evaluation of k and epsilon quantities (based on eddy turbulent viscosity and turbulent characteristic length returned by mixing length model). The frequency of the MED file print is set equal to **dt\_impr\_ustar**. Moreover, k-eps MED field is automatically saved at the last time step. MED file is then used for the restarting K-Epsilon calculation with the **Champ\_Fonc\_Med** keyword as explained in the 2.16.1.3 section.

<p><b>Distance_Paroil</b> domain_name nb_boundaries boundary1 boundary2 ... format</p>
--

**Distance\_paroil** : This keyword generates external file "domainname\_Wall\_length.xyz" devoted for instance, for mixing length modelling [see Longueur\_Melange]. In this file, are saved the coordinates of each element (center of gravity) of domain\_name domain and minimum distance between this point and boundaries (specified boundary1,...) that user specifies in data file (typically, those which are associated to walls). Value for format may be binaire (a binary file domainname\_Wall\_length.xyz is written) or formatte (moreover, a formatted file domainname\_Wall\_length\_formatted.xyz is written).

Example :

```
{
```

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```

dimension 3
Pb_Hydraulique_Turbulent pb
Domaine dom
Read _file file.geo ;
Tetraedriser_homogene_compact dom
Distance_paroi dom 3 paroi1 paroi2 paroi3 binaire
Fin
}

```

Where value 3 and names paroi1, paroi2, paroi3 designate respectively the number and the name of the boundaries from which minimum distance is calculated. A field Distance\_paroi is available to post process the distance to the wall:

```

Postraitement {
    Champs dt_post 50. { Distance_paroi elem }
}

```

### 2.16.1.3 THE K-EPSILON MODEL

```

Modele_turbulence K_epsilon
{
    [ Cmu val ]
    Transport_K_Epsilon
    {
        Diffusion { [dif] }
        Convection { [schema] }
        [ Sources
            Sourceansport_Ks C1_epsC2_eps } ]
        | Source_Transport_K_Eps_anisotherme { C1_eps val C2_eps val C3_eps val }
        | Source_Transport_K_Eps_aniso_concen { C1_eps val C2_eps val C3_eps val }
        | Source_Transport_K_Eps_aniso_therm_concen { C1_eps val C2_eps val C3_eps val }
    ]
    boundary_conditions { [cl_turb1] [cl_turb2] ..... }
    [ Conditions_initiales { [cl_init] } ]
    [ parametre_equation keyword ]
}
[ Prandtl_K val ] [ Prandtl_Eps val ]
[ Correction_visco_turb_pour_controle_pas_de_temps ]
Turbulence_paroi ...
}

```

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**Cmu** :Keyword to modify the Cmu constant of k-eps model :  $Nut = Cmu * k^2 / \epsilon$   
Default value is 0.09

**K\_Epsilon**: This keyword is selected to indicate that the turbulence model (k- $\epsilon$ ) should be used.

**Transport\_K\_Epsilon**: This keyword is used to define the (k- $\epsilon$ ) transportation equation.

**Diffusion**: This keyword is used to set the diffusion operator.

*dif*: This should be set to **Negligeable** to suppress the k and  $\epsilon$  transportation equation's diffusion operator.

**Convection**: This keyword is used to alter the convection scheme (by default, the UPWIND scheme is selected).

*schema*: This may be set to **Amont** or **Quick**. Enter the first keyword to select an UPWIND type scheme, the second keyword to select a QUICK-FRAM type scheme.

**Prandtl\_K** : Keyword to change the  $Pr_k$  value (default 1.0).

**Prandtl\_Eps**: Keyword to change the  $Pr_\epsilon$  value (default 1.3).

**Source\_Transport\_K\_Eps**: This keyword is used to alter the source term constants in the standard k-eps model epsilon transportation equation. By default, these constants are set to:

C1\_eps=1.44

C2\_eps=1.92

**Source\_Transport\_K\_Eps\_anisotherme** | **Source\_Transport\_K\_Eps\_aniso\_concen** | **Source\_Transport\_K\_Eps\_aniso\_therm\_concen** : This keywords are used to modify the source term constants in the anisotherm | aniso-concentration | anisotherm and aniso-concentration k-eps model epsilon transportation equation. By default, these constants are set to:

C1\_eps=1.44

C2\_eps=1.92

C3\_eps=1.0

**Boundary\_conditions**: This keyword is used to set the turbulence boundary conditions. Refer to 2.13.4.

*cl\_turb*: Used to set a turbulence boundary conditions.

**Conditions\_initiales:** These keywords are used to set initial turbulence conditions. Refer to 2.12.3.

*cl\_init:* Defines an initial turbulence condition on a boundary. To restart from a previous mixing length calculation, an external MED-format file containing reconstructed K and Epsilon quantities can be read (see 2.16.1.2 section) thanks to the **Champ\_fonc\_MED** keyword (see more details for this keyword in the 2.4.1 section). Example:

```
Conditions_initiales { K_Eps Champ_Fonc_MED [ last_time ] filename.med
domain_name K_Eps_from_nut elem time }
```

Where time is the save time of the MED fields K and Epsilon. For a practical use, last physical time can be simply loaded threw **last\_time** keyword (the specified time is then unused).

**Turbulence\_paro:** This keyword is used to select the wall turbulence model. Refer to 2.16.3.

**Correction\_visco\_turb\_pour\_controle\_pas\_de\_temps :** Keyword to set a limitation to low time steps due to high values of turbulent viscosity. The limit for turbulent viscosity is calculated so that diffusive time-step is equal or higher than convective time-step. For a stationary flow, the correction for turbulent viscosity should apply only during the first time steps and not when permanent state is reached. To check that, we could post process the **corr\_visco\_turb** field which is the correction of turbulent viscosity: it should be 1. on the whole domain.

**Parametre\_equation :** See 2.6.1

**Warning:** When used with the Quasi-compressible model, k and  $\epsilon$  should be viewed as  $\rho k$  and  $\rho \epsilon$  when defining initial and boundary conditions or when visualizing values for k and  $\epsilon$ . This bug will be fixed in a future version.

#### 2.16.1.4 THE K\_EPSILON\_V2 MODEL

```
Modele_turbulence K_epsilon_V2
{
  Transport_K_Epsilon_V2 { ... }
  Transport_V2 { ... }
  EqnF22 { Solveur solver_kind }
  ...
}
```

**K\_Epsilon\_V2** Keyword to refer to a turbulence model available in VDF discretization

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This model is a variant of the K-Epsilon turbulence model called K-Eps-V2. A transport equation for V2 is added to calculate turbulent viscosity ( $\text{Nut} = \text{CmuV2}$ ).

Other new keywords:

**Transport\_K\_Epsilon\_V2** : Transport equation for K-Eps

**Transport\_V2** : Transport equation for V2.

**EqnF22** : Elliptic equation to calculate the V2 transport source term (solver like GMRES is needed)

**V2** : New unknown field.

Example:

```

modele_turbulence K_Epsilon_V2 {
  Transport_K_Epsilon_V2
  {
    convection { amount }
    diffusion { }
    boundary_conditions {
      bas paroi
      haut paroi
      obst paroi
      entree frontiere_ouverte_K_eps_impose Champ_Front_Uniforme 2 1.e-2 1.e-3
      sortie frontiere_ouverte K_EPS_EXT Champ_Front_Uniforme 2 0. 0.
    }
    conditions_initiales { k_eps Champ_Uniforme 2 1.e-3 1.e-3 }
  }
  Transport_V2
  {
    convection { amount }
    diffusion { }
    boundary_conditions {
      bas paroi
      haut paroi
      obst paroi
      entree frontiere_ouverte_K_eps_impose Champ_Front_Uniforme 1 1.e-3
      sortie frontiere_ouverte K_EPS_EXT Champ_Front_Uniforme 1 0.
    }
    conditions_initiales { V2 Champ_Uniforme 1 1.e-6 }
  }
  EqnF22 { Solveur Gmres { } }
}

```

*Warning:*

This model, only available in VDF discretization, is not tested.

## 2.16.1.5 TURBULENCE MODEL K\_EPSILON AT TWO LAYERS

```

Modele_turbulence K_epsilon_2_Couches
{
  Transport_K_KEpsilon {
    ...
    Nb_couches integer
    [impr]
    [Y*_switch integer]
    [Nut_Switch integer]
    [Conv_forcee]
    [Conv_nat]
  }
  Turbulence_paro law_of_the_wall
  ...
}

```

This turbulence model at two layers for the hydraulic equation is a variant of the K-Epsilon turbulence model.

**Transport\_K\_KEpsilon** : Transport equation for K and Epsilon.

**Nb\_couches** : Maximal number of meshes for the first layer.

**Impr** : Optional keyword for output of the mesh number between the two layers.

**Y\*\_switch** : Optional keyword to modify the default value (160) of the y\* switch between the two layers.

**Nut\_Switch** : Optional keyword to modify the default value (30) of the turbulent viscosity between the two layers.

**Conv\_forcee** : Optional keyword to apply the forced convection laws inside the first layer.

**Conv\_nat** : Optional keyword to apply the natural convection laws inside the first layer (default).

Two keywords for the standard law of the wall:

**loi\_paro\_2\_couches** for a hydraulic problem.

**loi\_paro\_2\_couches\_scalaire** for a thermohydraulic problem

The boundary conditions are the same than the K-Epsilon model.

Example: (See also the test case Cavite\_2couches)

```

Navier_Stokes_turbulent
{
  solveur_pression GCP { ... }
  convection { ... }
  diffusion { }
}

```

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```

sources { boussinesq_temperature { T0 20. } }
conditions_initiales { ... }
boundary_conditions { ... }
modele_turbulence K_Epsilon_2_couches {
  Transport_K_KEpsilon
  {
    Nb_couches 10
    Impr
    convection { amount }
    diffusion { }
    boundary_conditions {
      plaq_bas paroi
      plaq_haut paroi
      plaq_gauche paroi
      plaq_droit paroi
    }
    conditions_initiales { k_eps Champ_Uniforme 2 1.e-3 1.e-3 }
  }
  Turbulence_Paroi loi_parois_2_couches
  dt_impr_ustar 10
}

```

*Warning:*

Model only available in VDF discretization.

#### 2.16.1.6 LOW REYNOLDS MODEL

```

Modele_turbulence K_Epsilon_Bas_Reynolds
{
  Transport_K_Epsilon_Bas_Reynolds {
    Diffusion { [dif] }
    Convection { [schema] }
    [ Sources { Source_Transport_K_Eps_Bas_Reynolds { C1_eps val C2_eps val } } ]
    Boundary_conditions { [cl_turb1] [cl_turb2] ..... }
    [ Conditions_initiales { [cl_init] } ]
  }
  Modele_fonc_Bas_Reynolds modele { }
}

```

**K\_Epsilon\_Bas\_Reynolds:** This keyword is selected to indicate that the bas Reynolds k- $\epsilon$  turbulence model should be used. Caution: this model is only available in the VDF module.

**Transport\_K\_Epsilon\_Bas\_Reynolds:** This keyword is used to define the bas Reynolds k- $\epsilon$  transportation equation.



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**Diffusion:** This keyword is used to specify the diffusion operator.

**Convection:** This keyword is used to change the convection scheme.

**Source\_Transport\_K\_Eps\_Bas\_Reynolds C1\_eps C2\_eps:** Keywords used to modify the source term constants in the model's epsilon transportation equation. By default, these constants are set to:  
C1\_eps=1.55  
C2\_eps=2.

**Boundary\_conditions:** This keyword is used to define turbulence boundary conditions. Refer to 2.13.4.

*cl\_turb:* Sets a turbulence boundary condition.

**Conditions\_initiales:** Keyword used to define initial turbulence conditions. Refer to 2.12.3.

*cl\_init:* Sets an initial turbulence condition at a boundary.

**Modele\_fonc\_Bas\_Reynolds:model :** This keyword is used to set the bas Reynolds model used. Currently, two models are available for VDF and VEF discretizations.

*model :* **Launder\_Sharma** for Launder-Sharma model or **Jones\_Launder** for Jones-Launder model.

When Launder Sharma's model is used, one must specify the correct constants C1 and C2 for K\_eps transport equation source termes (C1 = 1.44 and C2 = 1.92) :

```
sources { source_transport_K_Eps_bas_Reynolds { C1_eps 1.44 C2_eps 1.92 } }
```

#### 2.16.1.7LOW REYNOLDS FOR FLOW WITH NATURAL CONVECTION

This turbulence model for the temperature equation may be used at low Reynolds for flow with natural convection. The other keywords are:

**Transport\_Fluctuation\_Temperature\_W\_Bas\_Re :** Transport equation for the temperature fluctuation.

**Modele\_Fonc\_Bas\_Reynolds\_Thermique :** Choice of the coefficient (Jones Lauder).

As the model for hydraulic equation, boundary conditions for the transport equation of the

fluctuations are :

**Frontiere\_ouverte\_Fluctu\_Temperature\_imposee** : inlet boundary condition

**Fluctu\_Temperature\_ext** : outlet boundary condition

Example: (See also the test case Nagano\_WBasRe)

Convection\_Diffusion\_Temperature\_Turbulent

```
{
  diffusion { }
  convection { ... }
  boundary_conditions { ... }
  conditions_initiales { Temperature Champ_Uniforme 1 16. }
  modele_turbulence Fluctuation_Temperature_W_Bas_Re {
    Transport_Fluctuation_Temperature_W_Bas_Re
    {
      diffusion { }
      convection { amount }
      boundary_conditions {
        plaque Paroi_fixe
        loir Frontiere_ouverte_Fluctu_Temperature_imposee Champ_Front_Uniforme 2 0.1 0.1
        planche Frontiere_ouverte_Fluctu_Temperature_ext Champ_Front_Uniforme 2 0. 0.
        plafond Frontiere_ouverte_Fluctu_Temperature_ext Champ_Front_Uniforme 2 0. 0.
      }
      conditions_initiales {
        Fluctu_Temperature Champ_Uniforme 2 1. 1.
      }
    }
  }
  Modele_Fonc_Bas_Reynolds_Thermique_Jones_Launders { }
}
```

*Warning:*

Model only available in VDF discretization.

#### 2.16.1.8 SPECIFIED MODEL

```
Modele_turbulence Combinaison
{
  [nb_var integer var1 var2 ...]
  fonction string
  Turbulence_parois ...
}
```

This keyword specifies a turbulent viscosity model where the turbulent viscosity is user-defined.

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**nb\_var** integer ...: Optional number and names of variables which will be used in the turbulent viscosity definition (by default 0)

**function** string: Fonction for turbulent viscosity. X,Y,Z and variables defined previously can be used.

**Turbulence\_paro...** : This keyword is used to select the wall turbulence model. Refer to 2.16.3.

## 2.16.2 SCALAR EQUATION MODELS

### 2.16.2.1 THE PRANDTL (SCHMIDT) MODEL

For the scalar equations, only the model based on Reynolds analogy is available.

If **K\_Epsilon** was selected in the hydraulic equation, **Prandtl** must be selected for the convection-diffusion temperature equation coupled to the hydraulic equation and **Schmidt** for the concentration equations.

The syntax to use these turbulence models is as follows:

```

Modele_turbulence Prandtl | Schmidt
{
    Turbulence_paro law
    [ dt_impr_nusselt value ]
    [ Prdt | ScTurb double | Prandt_turbulent_fonction_nu_t_alpha string ]
}

```

**Turbulence\_paro** law : A scalar wall law should be specified. Refer to 2.16.3.2.

**Prdt|ScTurb**: Keywords to modify the constant of the model. Default value is 0.9 for turbulent Prandtl number ( $\alpha_t = \nu_t / P_{rt}$ ) and 0.7 for the turbulent Schmidt number ( $D_t = \nu_t / S_{ct}$ ).

**Prandt\_turbulent\_fonction\_nu\_t\_alpha** : Optional keyword to specify turbulent diffusivity (by default,  $\alpha_t = \nu_t / Pr_t$ ) with another formulae, for example:  $\alpha_t = \nu_t^2 / (0.7\alpha + 0.85\nu_t)$  with the string **nu\_t\*nu\_t/(0.7\*alpha+0.85\*nu\_t)** where alpha ( $\alpha$ ) is the thermal diffusivity.

**dt\_impr\_nusselt** : Keyword to print local values of Nusselt number and temperature near a wall during a turbulent calculation. The values will be printed in the "\_Nusselt.face" file each dt\_impr\_nusselt time period.

The local Nusselt expression is as follows :  $Nu = d_{wall}/d_{eq}$  where  $d_{wall}$  is the distance from the first mesh to the wall and  $d_{eq}$  is given by the wall law. This option also gives the value of  $d_{eq}$ ,  $h = \lambda/d_{eq}$  and the fluid temperature of the first mesh near the wall.

For the Neumann boundary conditions (flux\_impose), the "equivalent" wall temperature given by the wall law is also printed (Tparoi equiv.) preceded for VEF calculation by the edge temperature "T face de bord".

#### 2.16.2.2 DYNAMIC SUBGRID SCALE MODEL

```

Modele_turbulence Sous_maille_dyn
{
  [ dynamique_y2 integer ]
  [ stabilise
  [ 6_points ]
  [ plans_paralleles nb_points integer ]
  [ moy_euler ]
  [ moy_lagrange ] ]
  Turbulence_paroi law...
}

```

*Warning:* Available in VDF only. Not coded in VEF yet.

#### 2.16.2.3 THERMAL FLUCTUATION TURBULENCE MODEL

## Modele\_turbulence Fluctuation\_Temperature

```

{
  Transport_Fluctuation_Temperature {
    Diffusion { [dif] }
    Convection { [schema] }
    [ Sources { Source_Transport_Fluctuation_Temperature { Ca val Cb val Cc val Cd val } } ]
    Boundary_conditions { [cl_turb1] [cl_turb2] ..... }
    [ Conditions_initiales { [cl_init] } ]
  }
  Transport_Flux_Chaleur_Turbulente {
    Diffusion { [dif] }
    Convection { [schema] }

    [ Sources { Source_Transport_Flux_Chaleur_Turbulente { C1_teta val C2_teta val C3_teta
val } } ]
    Boundary_conditions { [cl_turb1] [cl_turb2] ..... }
    [ Conditions_initiales { [cl_init] } ]
  }
}

```

**Fluctuation\_Temperature:** This is a keyword used to select a model for thermal fluctuations should a turbulent thermohydraulic problem occur. This model resolves two new equations (keywords **Transport\_Fluctuation\_Temperature** and **Transport\_Flux\_Chaleur\_Turbulente**) and uses specific boundary conditions. The first equation deals with thermal fluctuation ( $T'^2$ ) variance transportation and the thermal fluctuation dissipation rate (new field **Fluctu\_Temperature** of the  $T'^2, Eps\_T'$  components), the second deals with transportation of 3 turbulent heat flux components (new field **Flux\_Chaleur\_Turbulente** belonging to the  $uT', vT', wT'$  components).

**Diffusion:** This keyword is used to specify an equation diffusion operator.

**Convection:** This keyword is used to alter the equation convection scheme.

**Source\_Transport\_Fluctuation\_Temperature Ca Cb Cc Cd:** These keywords are used to modify the source term constants in the temperature fluctuation transportation equation in the thermal fluctuation model. By default, these constants are set to:

Ca=0.8  
Cb=2.0  
Cc=1.96  
Cd=0.8

**Source\_Transport\_Flux\_Chaleur\_Turbulente C1\_teta C2\_teta C3\_teta:** These keywords are used to alter the source term constants in the turbulent heat flux transportation equation in the thermal fluctuation model. By default, these constants are set to:

C1\_teta=5.  
C2\_teta=0.5  
C3\_teta=0.33

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**Boundary\_conditions:** These keywords are used to set the turbulence boundary conditions. Refer to 2.13.4.

*cl\_turb*: Sets a turbulence boundary condition.

**Conditions\_initiales:** This keyword is used to define the initial turbulence conditions. Refer to 2.12.3.

*cl\_init*: Sets an initial turbulence condition at the boundary.

This model features the following keyword that may be used to post-process the fields (refer to 2.12.3):

**Variance\_Temperature:** This keyword is used to post-process the temperature fluctuation variation ( $T'^2$ ) during a k-eps calculation with a turbulence model for thermal fluctuations.

**Taux\_Dissipation\_Temperature:** This keyword is used to post-process the temperature fluctuation dissipation rate during a k-eps calculation with a turbulence model for thermal fluctuations.

**Flux\_Chaleur\_Turbulente:** This keyword is used to post-process turbulence heat flux components ( $uT'$ ,  $vT'$ ,  $wT'$ ) during a k-eps calculation with a turbulence model for thermal fluctuations.

## 2.16.3 WALL LAWS

**Turbulence\_paro**i loi [dt\_impr\_ustar periode ] [nut\_max value] [eps\_min value] [k\_min value]

**Turbulence\_paro**i: This keyword is used to set the wall law model.

**dt\_impr\_ustar**: This keyword is used to print the values ( $U^+$ ,  $d^+$ ,  $u^*$ ) obtained with the wall laws into a file named *datafile\_ProblemName\_Ustar.face* and *periode* refers to the printing period, this value is expressed in seconds.

Keywords to set a limitation to low or high turbulent values for K-Eps models :

**nut\_max** : upper limitation of turbulent viscosity (default value 1.e8).

**eps\_min** : lower limitation of epsilon (default value 1.e-10).

**k\_min**: lower limitation of k (default value 1.e-10).

*loi*: The law selected for wall turbulence. It depends of the equation :

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### 2.16.3.1 MOMENTUM EQUATIONS

**-Loi\_standard\_hydr** (or **Loi\_standard\_hydr\_3couches**) : Keyword for the logarithmic wall law. **Loi\_standard\_hydr** refers to first cell rank eddy-viscosity defined from continuous analytical functions, whereas **Loi\_standard\_hydr\_3couches** from functions separately defined for each sub-layer

**-Loi\_expert\_hydr** { ... } : This keyword is similar to the previous keyword **Loi\_standard\_hydr** but has several additional options into brackets :

**Kappa** value: The value of  $\kappa$  can be changed from the default one (0.415)

**Erugu** value: The value of E can be changed from the default one for a smooth wall (9.11). It is also possible to change the value for one boundary wall only with **paroi\_rugueuse** keyword.

**A\_plus** value: A+ value can be changed from the default one (26.0)

More options for **loi\_expert\_hydr** keyword are available for VEF discretization:

**u\_star\_impose** value : The value of the friction velocity ( $u^*$ ) is not calculated but given by the user.

**methode\_calcul\_face\_keps\_impose** option : The available options select the algorithm to apply K and Eps boundaries condition (the algorithms differ according to the faces).

**toutes\_les\_faces\_accroches** : Default option in 2D (the algorithm is the same than the algorithm used in **Loi\_standard\_hydr**)

**que\_les\_faces\_des\_elts\_dirichlet** : Default option in 3D (another algorithm where less faces are concerned when applying K-Eps boundary condition)

**-Paroi\_TBLE** { N value [ **kappa** value ] [ **facteur** value ] [ **modele\_visco** filename ] [ **stats** value value ] }

Keyword for the Thin Boundary Layer Equation wall-model (a more complete description of the model can be found into [this PDF file](#)). The wall shear stress is evaluated thanks to boundary layer equations applied in a one-dimensional fine grid in the near-wall region. The options are:

**N** value: Number of nodes in the TBLE grid (mandatory option).

**kappa** value : Optional option to change the default 0.415 value for kappa?

**facteur** value: Stretching ratio for the TBLE grid (to refine, the TBLE factor must be greater than 1)

**modele\_visco** filename: File name containing the description of the eddy viscosity model

**stats** values: Statistics of the TBLE velocity and turbulent viscosity profiles. 2 values are required : the starting time and ending time of the statistics computation.

**-Utau\_imp**: Keyword to impose the friction velocity on the wall with a turbulence model for thermohydraulic problems. There are two possibilities to use this keyword :

1- we can impose directly the value of the friction velocity  $u_{star}$ .

Example :                    modele\_turbulence sous\_longueur\_melange

```

{
    Cs 0.01
    turbulence_paro UTAU_IMP { u_tau Champ_uniforme 1 0.1 }
}

```

2- we can also give the friction coefficient **lambda\_c** and hydraulic diameter **diam\_hydr**. **Lambda\_c** can be function of the spatial coordinates x,y,z, the Reynolds number **Re**, and the diameter hydraulic **Dh**. So, Trio\_U determines the friction velocity by :

$$u_{\text{star}} = U \cdot \sqrt{\lambda_c / 8}$$

Example:

```

modele_turbulence longueur_melange
{
    turbulence_paro UTAU_IMP
    {
        diam_hydr Champ_uniforme 1 2
        lambda_c 0.02
    }
}

```

**-Negligeable** : This keyword is used to suppress the calculation of a law of the wall with a turbulence model. The wall stress is directly calculated with the derivative of the velocity, in the direction perpendicular to the wall. ( $\tau_{\text{tan}} / \rho = \nu \, dU/dy$ )

Other available laws:

**-Loi\_Ciofalo\_hydr**

**-Loi\_WW\_hydr**

*Warning:*

Only **Loi\_WW\_hydr** laws have been qualified on channel calculation.

These keywords are only available for a LES calculation.

### 2.16.3.2 SCALAR EQUATIONS

**-Loi\_standard\_hydr\_scalaire** : Keyword for the law of the wall.

**-Loi\_expert\_scalaire** { ... } : Keyword similar to keyword **Loi\_standard\_hydr\_scalaire** but with additional option into brackets :



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**calcul\_ldp\_en\_flux\_impose** value : By default (value set to 0), the law of the wall is not applied for a wall with a Neumann condition. With value set to 1, the law is applied even on a wall with Neumann condition.

**Prdt\_sur\_kappa** value : This option is to change the default value of 2.12 in the scalable wall function.

**-Loi\_Paroi\_Nu\_Impose** : Keyword, it is possible to impose Nusselt numbers on the wall for the thermohydraulic problems. To use this option, it is necessary to give in the data file the value of the hydraulic diameter and the expression of the Nusselt number. This expression can be a function of x, y, z, Re (Reynolds number), Pr (Prandtl number)

Example :

```
Turbulence_paroil Loi_Paroi_Nu_Impose
{
  nusselt 0.023*Re^0.8*Pr^(1./3.)
  diam_hydr champ_uniforme 1 9e-3
}
```

In this example, the Nusselt expression is the Colburn correlation.

**-Loi\_ODVM { N value Gamma value Stats value\_t0 value\_dt Check\_files }**

Thermal wall-function based on the simultaneous 1D resolution of a turbulent thermal boundary-layer and a variance transport equation, adapted to conjugate heat-transfer problems with fluid/solid thermal interaction (where a specific boundary condition should be used : **Paroi\_Echange\_Contact\_ODVM\_VDF**). This law is also available with isothermal walls.

**N** value: number of points per face in the 1D uniform meshes. N should be chosen in order to have the first point situated near  $\Delta y^+ = 1/3$ .

**Gamma** value: Smoothing parameter of the signal between 10e-5 (no smoothing) and 10e-1 (high averaging).

**Stats** value\_t0 value\_dt: Only for plane channel flow, it gives mean and root mean square profiles in the fine meshes, since value\_t0 and every value\_dt seconds. The values are printed into files named *ODVM\_fields\*.dat*.

**Check\_files**: It gives for one boundary face a historical view of local instantaneous and filtered values, as well as the calculated variance profiles from the resolution of the equation. The printed values are into the file *Suivi\_ndeb.dat*.

**-Paroi\_TBLe\_scal { N value [ Prandtl value ] [ facteur value ] [ modele\_visco filename ] [ Nb\_comp value ] [ stats value value ] }**

Keyword for the Thin Boundary Layer Equation thermal wall-model.

**Prandtl** value : Option to change the default value (1.0) of turbulent Prandtl number.

See **Paroi\_TBLe** for the other options.

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**-Negligeable\_scalaire** : Keyword to suppress the calculation of a law of the wall with a turbulence model for thermohydraulic problems. The wall stress is directly calculated with the derivative of the velocity, in the direction perpendicular to the wall.

## 2.17 SAVING A PROBLEM

**Sauvegarde** format\_sauvegarde nom\_fichier

**Sauvegarde\_simple** format\_sauvegarde nom\_fichier

**Sauvegarde**: Keyword used when calculation results are to be backed up.

**Sauvegarde\_simple**: Same keyword than **Sauvegarde** except, the last time step only is saved.

*format\_sauvegarde*: thress keywords may be used: **binaire** (binary format) or **formatte** (ASCII format) or **xyz** (multi-processor/multi-physics format).

The results are saved to the *nom\_fichier* file according to a frequency set by **dt\_sauv** (refer to time schemes 2.9). The file contains all the information saved over time.

If this instruction is not entered, results are saved only upon calculation completion in the file *nom\_du\_cas.sauv*.

When a coupling is performed, the backup-recovery file name must be well specified for each problem. In this case, you must save to different files and correctly specify these files when restarting the calculation.

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## 2.18 RESTARTING A PROBLEM

**Reprise|Resume\_last\_time** format\_reprise nom\_fichier

**Reprise:** This keyword is used to restart a calculation at the **tinit** time with the fields stored into the *nom\_fichier* file. **Resume\_last\_time** does the same thing, but will restart the calculation at the last time found in the file.

*format\_reprise:* there are three keywords available: **binaire** (binary format), **formatte** (formatted format), or **xyz**. The calculation is restarted based on the *nom\_fichier* file. If **xyz** is entered, the *nom\_fichier* file should be the .xyz file created by the previous calculation. With this file, it is possible to restart a parallel calculation on P cpus, whereas the previous calculation has been run on N ( $N < P$ ) cpus. By default, a .xyz file is created at the end of the calculation. To save space disc, you can prevent Trio\_U from writing this **.xyz** file, thanks to a line "**EcritureLectureSpecial** value" (with 0 as value) located in the data file just before the **Solve** keyword.

## 2.19 PROBLEM POST-PROCESSING

Several keywords can be used to create a postprocessing block, into a problem. First, you can create a single postprocessing task (**Postraitement** keyword). Generally, in this block, results will be printed with a specified format at a specified time period.

```
Postraitement {
  Postraitement_definition
}
```

But you can also create a list of postprocessing with **Postraitements** keyword (named with *Post\_name1*, *Post\_name2*, etc...), in order to print results to several formats or with different time periods, or into different results files:

```
Postraitements {
  Post_name1 { Postraitement_definition }
  Post_name2 { Postraitement_definition }
  ...
}
```

The postraitement\_definition has the following syntax :

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```
[Sondes {
  [nom_sonde [type] field_name Periode dts Points
    position_like nom_sonde | n x1 y1 [z1] x2 y2 [z2] .... xn yn [zn]]
  [nom_sonde [type] field_name Periode dts Segment
    position_like nom_sonde | ns x1 y1 [z1] x2 y2 [z2]]
  [nom_sonde [type] field_name Periode dts Segmentpoints
    position_like nom_sonde | ns x1 y1 [z1] x2 y2 [z2] .... xn yn [zn]]
  [nom_sonde [type] field_name Periode dts Plan
    position_like nom_sonde | ns1 ns2 x1 y1 [z1] x2 y2 [z2] x3 y3 [z3]]
  [nom_sonde [type] field_name Periode dts Volume
    position_like nom_sonde | ns1 ns2 ns3 x1 y1 z1 x2 y2 z2 x3 y3 z3 x4 y4 z4]
  [nom_sonde [type] field_name Periode dts Circle
    position_like nom_sonde | n x0 y0 [z0 dir] r teta1 teta2]
  [nom_sonde [type] field_name Periode dts Numero_elem_sur_maitre integer
}]
```

```
[Definition_champs {
  [field_name_post refChamp { ... }]
  [field_name_post Interpolation { ... }]
  [field_name_post Gradient { ... }]
  [field_name_post Divergence { ... }]
  [field_name_post Moyenne { ... }]
  [field_name_post Ecart_Type { ... }]
  [field_name_post Correlation { ... }]
  [field_name_post Transformation { ... }]
  [field_name_post Extraction { ... }]
  [field_name_post Reduction_0D { ... }]
  [field_name_post Morceau_Equation { ... }]
  [field_name_post Predefini { ... }]
  [field_name_post Tparoi_VEF { ... }]
}]
```

```
[Fichier filename] [Format lml|lata|lata_v1|lata_v2|med ] [Domaine domaine_name ]
```

```
[Champs [formatte|binaire] dt_post string | nb_pas_dt_post integer {
  [field_name] [localisation]
  ...
}]
```

```
[Statistiques Dt_post dtst {
  t_deb value t_fin value
  [stat field_name [second_field_name]] [localisation]
  ...
}]
```

```
[Statistiques_en_serie Dt_integr dtst {
  t_deb value t_fin value
  [stat field_name] [localisation]
  ...
}]
```

Where :

**Sondes** is a keyword to define probes postprocessing (1D plots). See 2.19.2

**Definitions\_champs** is a keyword to create new fields for postprocessing. See 2.19.3

**Format, Fichier, Domaine, Champs, Statistiques, Statistiques\_en\_serie** are keywords related to field 2D/3D postprocessing. See 2.19.4 and 2.19.5

*field\_name* is the name of the field being postprocessed and the next paragraph gives details about the different fields.

## 2.19.1 POST-PROCESSING FIELD NAMES

The fields which may currently be post processed are:

<i>Physical values</i>	<i>Keyword for field_name</i>	<i>Unit</i>
Speed	<b>Vitesse</b>	m.s <sup>-1</sup>
Kinetic energy	<b>Energie_cinetique</b>	m <sup>2</sup> .s <sup>-2</sup>
Vorticity	<b>Vorticite</b>	s <sup>-1</sup>
Pressure in incompressible flow (=P/ρ+gz). For Front Tracking probleme (=P+ρgz)	<b>Pression</b> (***)	Pa.m <sup>3</sup> .kg <sup>-1</sup> or Pa
Pressure in incompressible flow (=P+ρgz)	<b>Pression_pa</b>	Pa
Pressure in compressible flow	<b>Pression</b>	Pa
Totale pressure (when quasi compressible model is used)=Pth+P	<b>Pression_tot</b>	Pa
Pressure gradient (=grad(P/ρ+gz))	<b>Gradient_pression</b>	m.s <sup>-2</sup>
Temperature	<b>Temperature</b>	°C or K
Phase temperature of a two phases flow	<b>Temperature_EquationName</b>	°C or K
Mass transfer rate between two phases	<b>Temperature_mpoint</b>	kg.m <sup>-2</sup> .s <sup>-1</sup>
Temperature variance	<b>Variance_Temperature</b>	K <sup>2</sup>
Temperature dissipation rate	<b>Taux_Dissipation_Temperature</b>	K <sup>2</sup> .s <sup>-1</sup>
Temperature gradient	<b>Gradient_temperature</b>	K.m <sup>-1</sup>
Heat exchange coefficient	<b>H_echange_Tref</b> (**)	W.m <sup>-2</sup> .K <sup>-1</sup>
Turbulent heat flux	<b>Flux_Chaleur_Turbulente</b>	m.K.s <sup>-1</sup>
Turbulent viscosity	<b>Viscosite_turbulente</b>	m <sup>2</sup> .s <sup>-1</sup>

Turbulent dynamic viscosity (when quasi compressible model is used)	<b>Viscosite_dynamique_turbulente</b>	kg.m.s <sup>-1</sup>
Turbulent kinetic energy	<b>K</b>	m <sup>2</sup> .s <sup>-2</sup>
Turbulent dissipation rate	<b>Eps</b>	m <sup>3</sup> .s <sup>-1</sup>
Constituent concentration	<b>Concentration</b>	
Component velocity along X	<b>VitesseX</b>	m.s <sup>-1</sup>
Component velocity along Y	<b>VitesseY</b>	m.s <sup>-1</sup>
Component velocity along Z	<b>VitesseZ</b>	m.s <sup>-1</sup>
Mass balance on each cell	<b>Divergence_U</b>	m <sup>3</sup> .s <sup>-1</sup>
Irradiancy	<b>Irradiance</b>	W.m <sup>-2</sup>
Q-criteria	<b>Critere_Q</b>	s <sup>-1</sup>
Distance to the wall $Y^+=yU^*/\nu$	<b>Y_plus</b>	dimensionless
Friction velocity	<b>U_star</b>	m <sup>2</sup> .s <sup>-2</sup>
Cell volumes	<b>Volume_maille</b>	M <sup>3</sup>
Chemical potential	<b>Potentiel_Chimique_Generalise</b>	
Source term in non Galilean referential	<b>Acceleration_terme_source</b>	m.s <sup>-2</sup>
Stability time steps	<b>Pas_de_temps</b>	S
Boundary fluxes	<b>Flux_bords</b>	
Volumetric porosity	<b>Porosite_volumique</b>	dimensionless
Distance to the wall	<b>Distance_Paroi</b> (*)	M
Volumic thermal power	<b>Puissance_volumique</b>	W.m <sup>-3</sup>
Local shear strain rate defined as $\sqrt{(2S_{ij}S_{ij})}$	<b>Taux_cisaillement</b>	s <sup>-1</sup>
Cell Courant number (VDF only)	<b>Courant_maille</b>	dimensionless
Cell Reynolds number (VDF only)	<b>Reynolds_maille</b>	dimensionless

(\*): **distance\_paroi** is a field which can be used only if the mixing length model (see 2.16.1.2) is used in the data file.

(\*\*): **Tref** indicates the value of a reference temperature and must be specified by the user. For example, **H\_echange\_293** is the keyword to use for Tref=293K.

(\*\*\*) : The post-processed pressure is the pressure divided by the fluid's density (P/rho+gz) on incompressible laminar calculation. For turbulent, pressure is P/rho+gz+2/3\*k cause the turbulent kinetic energy is in the pressure gradient.



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**Note 0:** Since the v1.4.8 version, statistical fields can be plotted with probes with the keyword "**operator\_field\_name**" like for example, **Moyenne\_Vitesse** or **Ecart\_Type\_Pression** or **Correlation\_Vitesse\_Vitesse**. For that, it is mandatory to have the statistical calculation of this fields defined with the keyword **Statistiques**.

**Note 1:** Since the 1.5.3 version, physical properties (conductivity, diffusivity,...) can also be interrogated. The name of the fields and components available for post-processing is displayed in the error file after the following message: "Lecture des champs a postraiter". Of course, this list depends of the problem being solved.

For example, the Poiseuille\_VDF test case provides the following fields or components:

...

*Lecture des champs a postraiter*

*Milieu\_base : 1 masse\_volumique*

*Fluide\_Incompressible : 2 viscosite\_cinematique viscosite\_dynamique*

*Equation\_base : 1 volume\_maille*

*Operateur\_base : 0*

*Operateur\_base : 0*

*Navier\_Stokes\_std : 13 divergence\_U gradient\_pressionY gradient\_pressionX*

*gradient\_pression pression\_pa pression vitesseY vitesseX vitesse y\_plus porosite\_volumique*

*critere\_Q vorticite*

...

## 2.19.2 POST-PROCESSING BY PROBE

Probes refer to sensors that allow a value or several points of the domain to be monitored over time. The probes may be a set of points defined one by one (keyword **Points**) or a set of points evenly distributed over a straight segment (keyword **Segment**) or arranged according to a layout (keyword **Plan**) or according to a parallelepiped (keyword **Volume**)

The fields allow all the values of a physical value on the domain to be known at several moments in time.

**Sondes:** This keyword is used to define the probes.

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*nom\_sonde*: This is the name of the file suffix in which the values taken over time will be saved. The complete file name is *nom\_sonde.son*.

*type*: Option to change the positions of the probes. Several options are available:

**grav** : each probe is moved to the nearest cell center of the mesh

**som** : each probe is moved to the nearest vertex of the mesh

**nodes** : each probe is moved to the nearest face center of the mesh

**chsom** : Only available for P1NC sampled field. The values of the probes are calculated according to P1-Conform corresponding field (not recommended for Temperature).

*field\_name*: name of the sampled field.

**Periode**: This keyword is used to set the sampled field measurement frequency. Every *dts* seconds, the field value calculated at the previous time step is written to the *nom\_sonde.son* file.

*dts*: period value(s).

**Points**: This keyword is used to define the number of probe points. The field *field\_name* is sampled at *n* points in the domain.

*n*: number of probe points.

*xi yi zi*: probe measurement point co-ordinates. If the point does not coincide with a calculation node, the measurement is extrapolated linearly according to neighbouring node values.

**Segment**: This keyword is used to define the number of probe segment points. The *field\_name* field is sampled at *ns* points of the segment, evenly distributed.

*ns*: number of probe fields defined on the segment.

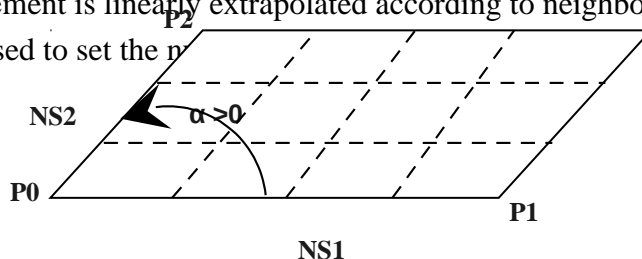
*x1 y1 z1 x2 y2 z2*: co-ordinates of the 2 outer probe segment points. If the point does not coincide with a calculation node, the measurement is linearly extrapolated according to neighbouring node values.

**Segmentpoints**: This keyword is used to define a probe segment from specifics points. The *field\_name* field is sampled at *ns* specifics points.

*ns*: number of specifics points.

*xi yi zi*: co-ordinates of the specifics points. If the point does not coincide with a calculation node, the measurement is linearly extrapolated according to neighbouring node values.

**Plan**: Keyword used to set the *n*



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$x1\ y1\ z1\ x2\ y2\ z2\ x3\ y3\ z3$ : co-ordinates of the 3 points that define the angle. This angle should be positive.

The keyword **Plan** (layout) file format is type .lml, the others (Point and Segment) are arranged in columns.

Observations: the probe co-ordinates should be given in Cartesian co-ordinates (X, Y, Z), including axisymmetric.

**Volume**: This is a keyword used to define the probe volume in a parallelepiped passing through 4 points A, B, C, D, and the number of probes in each direction. For example:

```
Sondes {
Sonde_P pression periode 0.01 volume 5 3 3  0. 0. 0.  5. 0. 0.  2. 2. 0.  0. 0. 2.
}
```

**Circle**: This is a keyword to define several probes located on a circle of radius r and centered at point  $x0,y0,z0$ . dir is an integer which gives the axis normal to the circle plane (0:x axis, 1:y axis, 2:z axis). The n probes are between  $teta1$  and  $teta2$  (angles given in degrees).

**Position\_like** nom\_sonde: Keyword to define a probe at the same position of another probe named nom\_sonde.

**Numero\_elem\_sur\_maitre** integer : Keyword to define a probe on the mesh element integer. Useful when using min/max probes.

### 2.19.3ADVANCED FIELD POST-PROCESSING

```
Definition_champs {
  field_name_post field_type { ... }
  ...
}
```

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**Definition\_champs:** Keyword to create new or more complex field for advanced postprocessing. *field\_name\_post* is the name of the new created field. *field\_type* is one of the following possible type (**refChamp**, **Interpolation**, **Gradient**,...):

```
field_name_post refChamp { Pb_champ nom_pb field_name }
```

*nom\_pb* is the problem name and *field\_name* is the selected field name

```
field_name_post Interpolation { [domaine nom_dom ]
                                localisation type_loc
                                [methode type_method]
                                source field_type { ... }
                                }
```

This keyword creates a field which is an interpolation of the field given by the keyword **source**. *nom\_dom* is the domain name where the interpolation is done (by default, the calculation domain) *type\_loc* indicate where is done the interpolation (« elem » for element or « som » for node). The optional keyword **methode** is limited to **calculer\_champ\_post** for the moment.

```
field_name_post Gradient { source field_type { ... } }
field_name_post Divergence { source field_type { ... } }
```

These keywords enable to calculate gradient or divergency of a given field.

```
field_name_post Moyenne {
    t_deb val1 t_fin val2 source field_type { ... }
    [moyenne_convergee Champ_fonc_reprise file.xyz pb_name Moyenne_field
last_time]
}
field_name_post Ecart_Type {
    t_deb val1 t_fin val2 source field_type { ... }
}
field_name_post Correlation {
    t_deb val1 t_fin val2 sources { field_type { ... } , field_type { ... } }
}
```

These keywords enable to create more statistic fields (see 2.19.5). The option **moyenne\_convergee** allows to read a converged time averaged field in a .xyz file in order to calculate, when restarting the calculation, the statistics fields (rms, correlation) which depend on this average. In that case, the time averaged field is not updated during the restarting calculation. In this case, the time averaged field must be fully converged to avoid errors when calculating high order statistics.

```

field_name_post Transformation {
    methode norme
        | produit_scalaire
        | composante numero integer
        | formule expression 1 f (x,y,z,t,)
        | vecteur expression N f1(x,y,z,t) ... fN(x,y,z,t)
    [localisation loc]
    [source field_type { ... } | sources { field_type { ... } , field_type { ... } , ... }]
}

```

This keyword is used to create a field with a transformation.

**methode norme** : will calculate the norm of a vector given by a **source** field specified by *field\_type*.

**methode produit\_scalaire** : will calculate the dot product of two vectors given by two **sources** fields

**methode composante numero** integer : will create a field by extracting the integer component of a field given by a **source** field

**methode formule expression** 1 : will create a field located to elements using one expression with x,y,z,t parameters and field names given by a **source** field or several **sources** fields. This field will be a scalar or a vector field according to the fields used in the expression.

**methode vecteur expression** N f1(x,y,z,t) ... fN(x,y,z,t) : will create a scalar (N=1) or vector field (N>1) located to elements by defining its N components with N expressions with x,y,z,t parameters and field names given by a **source** field or several **sources** fields.

```

field_name_post Extraction { domaine nom_dom nom_frontiere nom_fr
    [methode [trace | champ_frontiere]]
    source field_type { ... }
}

```

This keyword is used to create a surface field (values at the boundary) of a volume field  
-*nom\_dom* name of a surface domain which should has been created before

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-*nom\_fr* boundary name of the volume domaine where the values of the volume field will be picked

-*type\_methode* name of the extraction method (**trace** by\_default, the field on the surface will be calculated from the volume field or **champ\_frontiere**, the boundary conditions of the volume field will be used)

```

field_name_post Reduction_0D { [methode type_methode]
                                source field_type { ... }
}

```

These keyword is used to calculate the min, max, or mean value of a field.

-*type\_methode* name of the reduction method (**min**, **max**, **somme** for the sum, **somme\_ponderee** for a weighted sum (integral), **norme\_L2** for the L2 norm, **moyenne** for a mean and **moyenne\_ponderee** for a mean ponderated by integration volumes, e.g: cell volumes for temperature or pressure in VDF, volumes around faces for velocity and temperature in VEF)

```

field_name_post Morceau_Equation {
    type piece_type
    [numero 0 | 1]
    option option_type [ compo num_compo ]
    source field_type { ... }
}

```

These keyword is used to calculate a field related to a piece of equation. For the moment, *piece\_type* can only be **opérateur** for equation operators. **numero** will be 0 (diffusive operator), 1 (convective operator), 2 (gradient operator), 3 (divergence operator). **option** (*option\_type*) is limited for the moment to **stability** (for time steps) or **flux\_bords** (for boundary fluxes, in this case **compo** permits to specify the number component of the boundary flux choosen). The keyword **source** will be used to specify the equation. The problem name and the unknown of the equation (temperature, vitesse for example) should be given:

**Source refChamp** { **Pb\_Champ** problem\_name unknown\_field\_of\_equation }

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```

field_name_post Operateur_Eqn {
    numero_source int
    numero_op int
    sans_solveur_masse 0 | 1
    source field_type { ... }
}

```

This keyword is used also to calculate a field related to a piece of equation, either an operator (**numero\_op** option, 0 for diffusive operator, 1 for convective operator) or a source term (**numero\_source** option, the integer will specify the rank of the source term in the equation sources list). The field calculated will be returned either multiplied by the reverse matrix mass (**sans\_solveur\_masse** set to 1) or not (**sans\_solveur\_masse** set to 0, the default). The keyword **source** will be used to specify the equation. The problem name and the unknown of the equation (temperature, vitesse for example) should be given:

**Source** refChamp { **Pb\_Champ** problem\_name unknown\_field\_of\_equation }

```

field_name_post Predefini { Pb_Champ nom_pb field_name } }

```

This keyword is used to post process predefined postprocessing fields. For the moment, only kinetic energy (**energie\_cinetique** keyword to use for *field\_name*) is available.

```

field_name_post Tparoi_VEF {
    Source refChamp { Pb_Champ nom_pb field_name }
}

```

This keyword is used to post process (only for VEF discretization) the temperature field with a slight difference on boundaries with Neumann condition where law of the wall is applied on the temperature field. *nom\_pb* is the problem name and *field\_name* is the selected field name. A keyword (**temperature\_physique**) is available to post process this field without using **Definition\_champs**.

#### Remarks:

1) In the previous examples, if the source field specified with the **source** keyword is already a new post field named *name\_of\_champ\_post\_field*, you should use **source\_reference** *name\_of\_champ\_post\_field* instead of **source** *field\_type* { ... } or **sources\_reference** { name1 name2 ... nameN } if you have N fields.

II) It is possible to create an alias for a source field with the **nom\_source** keyword:

*field\_name field\_type { source field\_type { nom\_source nom } }*

By default, the name of source field is given according to the *field\_type*:

<b>refChamp:</b>	fieldname_natif_domain
<b>Interpolation:</b>	sourcename_localization_domainInterpolation
<b>Moyenne:</b>	Moyenne_sourcename
<b>Ecart_Type:</b>	Ecart_Type_sourcename
<b>Correlation:</b>	Correlation_firstsourcename_secondssourcename
<b>Gradient :</b>	Gradient_sourcename
<b>Divergence :</b>	Divergence_sourcename
<b>Transformation:</b>	Combinaison_sourcename
<b>Extraction:</b>	Extraction_sourcename
<b>Reduction_0D:</b>	Reduction_0D_sourcename
<b>Tparoi_VEF:</b>	Tparoi_VEF_sourcename

III) The components of a field is obtained by adding the number of the component (0 for the first component, 1 for the second one,...). Example:

#### Definition\_champs

```
{
    Pressure_gradient gradient { source refchamp { pb_champ pb pression } }
}
```

#### Champs dt\_post 1.1

```
{
    Gradient_pression0 elem # dp/dx #
    Gradient_pression1 elem # dp/dy #
}
```

IV) The oldier syntax for the field type remains understood. The corresponding types are :

<i>last syntax</i>	<i>old syntax</i>
<b>refChamp</b>	(->Champ_Post_refChamp)
<b>Interpolation</b>	(->Champ_Post_Interpolation)
<b>Moyenne</b>	(->Champ_Post_Statistiques_Moyenne)
<b>Ecart_Type</b>	(->Champ_Post_Statistiques_Ecart_Type)
<b>Correlation</b>	(->Champ_Post_Statistiques_Correlation)
<b>Gradient</b>	(->Champ_Post_Operateur_Gradient)
<b>Divergence</b>	(->Champ_Post_Operateur_Divergence)
<b>Transformation</b>	(->Champ_Post_Transformation)
<b>Extraction</b>	(->Champ_Post_Extraction)
<b>Reduction_0D</b>	(->Champ_Post_Reduction_0D)
<b>Tparoi_VEF</b>	(->Champ_Post_Tparoi_VEF)



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V) It is recommended to build a complex field in a one way process. For example, to define the L2 norm error of velocity compare to an analytical solution, you will define something like:

# Define the L2 error #

**Definition\_champs {**

    Error **reduction\_0D**

    {

**methode norme\_L2 source Transformation**

        {

**methode formule expression 1** velocity-solution

**sources {**

**refChamp { Pb\_champ pb vitesse nom\_source** velocity } ,

**Transformation {**

**methode vecteur expression 2** x\*y x+y **nom\_source** solution

                }

            }

        }

    }

}

# Write the L2 error like a probe in a file #

**Sondes { file\_error** Error **periode** 0.0005 **numero\_elem\_sur\_maitre** 0 }

Another example :

# Calculate circonferential velocity W from velocity components Ux and Uy #

**Definition\_champs**

{

**W Transformation**

    {

**methode formule expression 1** (Ux\*cos(atan(x/y))-Uy\*sin(atan(x/y)))

**sources {**

**Transformation { methode composante numero 0 source refchamp {**  
**Pb\_champ pb vitesse } nom\_source Ux } ,**

**Transformation { methode composante numero 1 source refchamp**  
**{ Pb\_champ pb vitesse } nom\_source Uy }**

        }

    }

}

Another example :

# Calculate X component of the pressure force on a sub-boundary named ring #

**Domaine** ring

**Extraire\_surface {**

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```

Domaine ring Probleme pb
Condition_faces (z+2)*(z+1)*(x^2+y^2-0.51)>0 avec_certains_bords 1 Cylindre
}
...
Read pb {
...
    Definition_champs
    {
        FPx Reduction_0D {
            methode somme source Interpolation {
                domaine ring localisation elem
                source Morceau_equation {
                    type operateur numero 2
                    option flux_bords compo 0
                    source refChamp {
                        Pb_champ pb vitesse
                    }
                }
            }
        }
    }
}
Sondes { filename FPx periode 0.005 numero_elem_sur_maitre 0 }
}

```

#### 2.19.4 GENERAL FIELD POST-PROCESSING

The parameters are:

[ **Fichier** *filename* ]

The name of the result file will be build with *filename* plus the format name choosen. (example: *channel.lata* if *channel.data* is the data file and LATA the results format). By default, *filename* is the name of the data file. In the case, where **Poetraitements** keyword is used (and **Fichier** keyword not specified), *filename* is by default the name of the data file plus the name of the postprocessing block plus the format name choosen (example: *channel\_Post\_name1.lata*)

[ **Format** format ]

This optional parameter specifies the format of the output file. The basename used for the output file is the basename of the data file. For the format parameter, choices are **lml**, **lata**, **lata\_v1**, **lata\_v2**, **med** A short description of each format can be found below. The default value is **lml**. The recommended format is **lata**.

[ **Domaine** domain\_name ]

This optional parameter specifies the domain on which the data should be interpolated before it is written in the output file. The default is to write the data on the domain of the current problem (no interpolation).

**Champs** [ **formatte|binaire** ] **dt\_post** string | **nb\_pas\_dt\_post** integer { ... }

This parameter specifies which fields should be written. The string given after **dt\_post** keyword is the minimum time elapsed in seconds of physical simulation time between two post-processing, it may be a real value or a time expression like  $2*\exp(-t)$  if it we want the a decreasing period. It is also possible to specify this period as a number of time steps, thanks to the **nb\_pas\_dt\_post** keyword. A post-processing is always forced at the end of the computation. The optional keywords **formatte** (ASCII) or **binaire** (Binary) are only applicable for the lml and lata format. Binary format is recommended since it is more compact and much faster to read and to write. The default is ASCII output (for lml format) and binary output (for lata format) and time\_interval=0 (post-process all computed timesteps)

field\_name [ localisation ]

You can specify as many fields as you want. field\_name is the name of a field (example: vitesse), a component of a field (example: vitesse\_x), or a post-processing field previously defined in a definition\_champs block (the valid fields are the same as for probes, see 2.19.2).

The optional localisation keyword can be equal to **elem** (the post-processed field will be interpolated at the center of the elements of the chosen domain, if it is not already a P0 field), **som** (interpolation on the vertices of the domain), or **faces** (works only with the **lata** format and for fields discretized at the faces of the domain: velocity field in VDF and VEF, temperature field in VEF, ... the field is not interpolated and it is written "as is". This option uses a lot more disk space than the other options and it shows the "non conformity" of the velocity field). The default value for localisation is som. You might want to force smooth results or reduce the amount of data being written with the som option (in vef, fields processed with som are much smaller), or you might want to get the most detailed representation of the computed field and use the native localisation of the field (watch for "discretisation" messages in the error file).

**Format:** Optional keyword (set to lml format by default) used to define the file format to which the fields will be written. There are currently four available formats:

**lml:**

Keyword used to select standard result post-processing. This post-processing results in a *nom\_du\_cas.lml* file. If the binary option was not requested for post-processing, an ASCII file is produced (refer also to the example in 5.3).

OBSERVATION: currently all the integers need to be written in FORTRAN format fp.q or Ep.q and not Dp.q

nom_code	character string: name of the code used
version	character string: code version
date	3 integers: dd,mm,yy day month year (2 figures per integer)

nom_problème	character string characterising the problem to be processed (may not include blank characters)
--------------	--

comment	remarks (without blank characters)
---------	------------------------------------

format	keyword, may be FORMAT or BINAIRE
--------	-----------------------------------

GRILLE	keyword
--------	---------

nom_grille	character string: grid name
dim_grille	integer: problem dimension (2D 3D)
nb_noeud	integer: number of grid nodes

xi yi zi (node_nb)	co-ordinates of the nodes where i = 1 to nb_noeud
-----------------------	---

TOPOLOGIE	keyword
-----------	---------

nom_topologie	character string characterising topology
nom_grille	name of the grid to which this topology is related

MAILLE	keyword
--------	---------

nb_maille	integer: mesh number
-----------	----------------------

for each mesh:	
type_maille	element type character string:
	surface elements: POLY4 to POLY8
	volume elements: TETRA4
	PRISM6
	VOXEL8

et

ie1 ie2 .. ien	integers: list of nodes comprising the mesh
----------------	---

FACE keyword

nb\_face integer: number of faces

for each face:

type\_face face type character string:  
linear face : LINE2  
surface area face: POLY3 to POLY8

and

if1 if2 .. ifm list of nodes comprising the face  
je1 je2 list of elements touching the face

TEMPS keyword present at each time step  
val\_temps time value at the time step in question

CHAMPPPOINT keyword

nom\_champ character string characterising the field  
nom\_topologie name of the topology on which the field is defined in points  
temps time value

nom\_var name of the field variable  
nb\_comp number of field component(s)  
unité character string specifying the variable unit  
type\_var character string characterising the type of  
variable discretization (P1, P2 ..)  
nb\_points number of given points

n<sup>3</sup> noeud et valeur du champ list of data i = 1,nb\_points (point\_nb)

CHAMPFACE keyword

nom\_champ character string characterising the field  
nom\_topologie name of the topology on which the field is defined by faces  
temps time value

nom\_var name of the field variable  
nb\_comp number of field component(s)  
unité character string specifying the variable unit  
type\_var character string characterising the variable  
discretization type (P1, P2, ...)  
nb\_faces number of faces on which the field is given

n<sup>3</sup> face et valeur du champ list of data i = 1,nb\_faces (face\_nb)

CHAMPMAILLE keyword

nom\_champ character string characterising the field  
 nom\_topologie name of the topology on which the field is defined by meshes  
 temps time value

nom\_var character string characterising the variable  
 nb\_comp number of field component(s)  
 unité character string specifying the variable unit  
 type\_var character string characterising the variable  
 discretization type (P1, P2, ...)  
 nb\_mailles number of meshes on which the field is given

n<sup>3</sup> maille et valeur du champ list of data i = 1,nb\_mailles (mesh\_nb)

FIN keyword which must complete the graphic file

### **lata, lata v1, lata v2:**

Theses keywords (several versions of the format are available, version 1 with **lata\_v1** keyword or version 2 with **lata\_v2** keyword, the lata keyword is by default setting the version 2 format since the 1.6.4 version) are used to specify a result post-processing format that is broken down into several files. The domain name must also be indicated (see example). This post-processing generates the following files:

- A *nom\_du\_cas.lata* file containing the post-processing file index
- The *nom\_du\_cas.lata.champ.type.domaine.probleme.temps* files containing the fields at a given time for the problem domain where:  
 champ = pressure, speed, temperature, ...  
 type = som, elem  
 domaine = domain name  
 probleme = problem name  
 temps = multiple points in time of dt\_post

## med:

Keyword used to write a Med format file (**M**odélisation **E**change **D**onnées). The binary file generated is *nom\_du\_cas\_000n.med* (n is the number of the writing process) but a file *nom\_du\_cas.med* is also created for the user.

<i>Format</i>	<i>Usable viewing tools</i>	<i>File size for a field backup of over a million meshes</i>	<i>Real number precision in the files</i>
<b>Lml</b>	<b>Data Vizualiser</b> (program not included in the package) <b>Avs Express</b> (program not included in the package) <b>Ensignt</b> (program not included in the package) when the lml2ensight interface located in the ENSIGHT directory of the Trio_U distribution is used	12 Mb	Double
<b>Lata</b>	<b>Avs Express</b> (program not included with the package)	4 Mb	Single

## 2.19.5 FIELD GENERAL POST-PROCESSING FOR STATISTICS

**Statistiques:** This keyword is used to set the statistics.

**Dt\_post:** This keyword is used to set the calculated statistics write period.

*dts:* frequency value.

**t\_deb** value: Start of integration time

**t\_fin** value: End of integration time

*stat:* Set to **Moyenne (average)** to calculate the average of the field *nom\_champ* (field name) over time or **Ecart\_type (std\_deviation)** to calculate the standard deviation (statistic rms) of the field *nom\_champ* (*field\_name*) or **Correlation** to calculate the correlation between the two fields *nom\_champ* and *second\_nom\_champ*.

*nom\_champ:* name of the field on which statistical analysis will be performed. Possible keywords are **Vitesse (speed)**, **Pression (pressure)**, **Temperature**, **Concentration**,...

*localisation:* localisation of post-processed field values (**elem** or **som**).

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Example:

```
Statistiques Dt_post dtst {
    t_deb 0.1 t_fin 0.12
    Moyenne Pression
    Ecart_type Pression
}
```

It will write every **dt\_post** the mean and standard deviation value:

$t \leq t_{deb}$  :

$$\overline{P(t)} = 0$$

$$< P(t) > = 0$$

$t > t_{deb}$  :

$$\overline{P(t)} = \frac{1}{t - t_{deb}} \int_{t_{deb}}^t P(t) dt$$

$$< P(t) > = \sqrt{\frac{1}{t - t_{deb}} \int_{t_{deb}}^t [\overline{P(t)} - P(t)]^2 dt}$$

**Statistiques\_en\_serie**: This keyword is used to set the statistics. Average on **dt\_integr** time interval is post-processed every **dt\_integr** seconds

**dt\_integr** value : Period of integration and write period.

*stat*: Set to **Moyenne (average)** to calculate the average of the field *nom\_champ* (field name) over time or **Ecart\_type (std\_deviation)** to calculate the standard deviation (statistic rms) of the field *nom\_champ* (*field\_name*).

*nom\_champ*: name of the field on which statistical analysis will be performed. Possible keywords are **Vitesse (speed)**, **Pression (pressure)**, **Temperature**, **Concentration**,...

*localisation*: localisation of post-processed field values (**elem** or **som**).

Example:

```
Statistiques_en_serie Dt_integr dtst {
    Moyenne Pression
}
```

Will calculate and write every dtst seconds the mean value:

$$(n+1)dt\_integr > t > n*dt\_integr, \overline{P(t)} = \frac{1}{t - n*dt\_integr} \int_{t - n*dt\_integr}^t P(t) dt$$





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## 2.20 PROBLEM RESOLUTION

The **Solve** interpreter allows a previously defined problem to be resolved.

**Solve** *pb*

**Solve:** Keyword to resolve a problem *pb*

## 2.21 PARALLEL CALCULATION

You need several keywords to run a parallel calculation. First, you will run in sequential mode a data file where you will partition your mesh thanks to the **partition** instruction. Then you will run in parallel mode your complete data file where you will read the partitioned mesh thanks to **Scatter** keyword.

### 2.21.1 PARTITION

The following keyword is used for parallel calculation to cut a domain for each processor. By default, these keyword is commented in the reference test cases.

```

Partition DOMAIN_OBJECT_NAME
{
    [ periodique N BOUNDARY_NAME_1 BOUNDARY_NAME_2 ... ]
    partitionneur ALGORITHM_NAME { OPTIONS }
    [ larg_joint THICKNESS ]
    [ reorder 0|1 ]
    [ nom_zones BASENAME ]
    [ ecrire_decoupage PARTITION_FILENAME ]
    [ ecrire_lata LATAFILE_BASENAME ]
    [ nb_parts_tot N ]
    [ formatte ]
}

```

DOMAIN\_OBJECT\_NAME : the name of the domain object to cut.

**periodique** N BOUNDARY\_NAME\_1 BOUNDARY\_NAME\_2 ... : N is the number of boundary names given. Periodic boundaries must be declared by this method. The partitionning algorithm will ensure that facing nodes and faces in the periodic boundaries are located on the same processor.

**partitionneur** ALGORITHM\_NAME { OPTIONS } : Defines the partitionning algorithm (the effective C++ object used is "Partitionneur\_ALGORITHM\_NAME"). Valid algorithms and options are :

```

partitionneur Metis {
    nb_parts N

```

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```
[ use_weights ]
[ pmetis | kmetis ]
[ nb_essais N ]
}
```

Metis is an external partitionning library. It is a general algorithm that will generate a partition of the domain.

N is the number of non empty parts that must be generated (generally equal to the number of cpus in the parallel run).

If **use\_weights** is specified, weighting of the element-element links in the graph is used to force metis to keep opposite periodic elements on the same processor. This option can slightly improve the partitionning quality but it consumes more memory and takes more time. It is not mandatory since a correction algorithm is always applied afterwards to ensure a correct partitionning for periodic boundaries.

The default values are "**pmetis**", default parameters are automatically chosen by Metis. "**kmetis**" is faster than "**pmetis**" option but the last option produces better partitioning quality. In both cases, the partitioning quality may be slightly improved by increasing the "**nb\_essais**" option (by default N=1). It will compute N partitions and will keep the best one (smallest edge cut number). But this option is CPU expensive, taking N=10 will multiply the CPU cost of partitioning by 10.

Experiments show that only marginal improvements can be obtained with non default parameters.

```
partitionneur Tranche {
    tranches nx ny [nz]
}
```

This algorithm will create a geometrical partitionning by slicing the mesh in the two or three axis directions, based on the geometric center of each mesh element. nz must be given if dimension=3. Each slice contains the same number of elements (slices don't have the same geometrical width, and for VDF meshes, slice boundaries are generally not flat except if the number of mesh elements in each direction is an exact multiple of the number of slices). First, nx slices in the X direction are created, then each slice is split in ny slices in the Y direction, and finally, each part is split in nz slices in the Z direction. The resulting number of parts is nx\*ny\*nz.

If one particular direction has been declared periodic, the default slicing (0, 1, 2, ..., n-1)

is replaced by (0, 1, 2, ... n-1, 0), each of the two "0" slices having twice less elements than the other slices.

```
partitionneur Sous_Zones {
```

```
[ sous_zones N SUBZONE_NAME_1 SUBZONE_NAME_2 ... ]
```

```
}
```

This algorithm will create one part for each specified subzone. All elements contained in the first subzone are put in the first part, all remaining elements contained in the second subzone in the second part, etc...

If all elements of the domain are contained in the specified subzones, then N parts are created, otherwise, a supplemental part is created with the remaining elements.

If no subzone is specified, all subzones defined in the domain are used to split the mesh.

```
partitionneur Partition {
    domaine DOMAINE_NAME
}
```

This algorithm re-use the partition of the domain named DOMAINE\_NAME. It is useful to partition for example a post processing domain. The partition should match with the calculation domain.

```
partitionneur Fichier_Decoupage {
    fichier FILENAME
    [ corriger_partition ]
}
```

This algorithm reads an array of integer values on the disc, one value for each mesh element. Each value is interpreted as the target part number  $n \geq 0$  for this element. The number of parts created is the highest value in the array plus one. Empty parts can be created if some values are not present in the array.

The file format is ASCII, and contains space, tab or carriage-return separated integer values. The first value is the number nb\_elem of elements in the domain, followed by nb\_elem integer values (positive or zero).

Contrary to other partitioning algorithms, no correction is applied by default to the partition (eg. element 0 on processor 0 and corrections for periodic boundaries). If "**corriger\_partition**" is specified, these corrections are applied.

**larg\_joint THICKNESS** : This keyword specifies the thickness of the virtual ghost zone (data known by one processor though not owned by it). The default value is 1 and is generally correct for all algorithms except the QUICK convection scheme that require a thickness of 2. Since the 1.5.5 version, the VEF discretization imply also a thickness of 2 (except VEF P0). Any non-zero positive

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value can be used, but the amount of data to store and exchange between cpus grows quickly with the thickness.

**reorder** 0|1 : If this option is set to 1 (0 by default), the partition is renumbered in order that the processes which communicate the most are nearer on the network. This may slightly improves parallel performance.

**nom\_zones** BASENAME : It is the base name of the .Zone files written on disc. If this keyword is not specified, the geometry is not written on disc (you might just want to generate a "ecrire\_decoupage" or "ecrire\_lata").

**ecrire\_decoupage** FILENAME : After having called the partitionning algorithm, the resulting partition is written on disc in the specified filename. See also partitionneur Fichier\_Decoupage. This keyword is useful to change the partition numbers. First, you write the partition into a file with the option **ecrire\_decoupage**. This file contains the zone number for each element's mesh. Then you can easily permute zone numbers in this file. Then read the new partition to create the .Zones files with the **Fichier\_Decoupage** keyword.

**ecrire\_lata** FILENAME : After having called the partitionning algorithm, a .lata file is written, containing the partitionning for visualization purposes. You can check the generated partition.

**nb\_parts\_tot** N : Keyword to generates N .Zone files, instead of the default number M obtained after the partitionning algorithm. N must be greater or equal to M. This option might be used to perform coupled parallel computations. Supplemental empty zones from M to N-1 are created. This keyword is used when you want to run a parallel calculation on several domains with for example, 2 cpus on a first domain and 10 on the second domain because the first domain is very small compare to second one. You will write **Nb\_parts** 2 and **Nb\_parts\_tot** 10 for the first domain and **Nb\_parts** 10 for the second domain.

**formatte** : These keyword specify ASCII format for the .Zone files. "binaire" is the default and recommended format, but is not actually portable. You must generate the .Zone file on the same computer architecture (big-endian or little endian) than the one used to run the parallel computation. In "ascii" (synonym for "formatte"), some precision might be lost in the node coordinates.

Restrictions for periodic boundary conditions:

Before the 1.4.8 version, periodic boundaries should be on the same processor. So the partitioning should be appropriate. Since the 1.4.8 version, the rule is: periodic faces should be on the same processor. Examples of good partitioning:

<pre> WWWWWWWWW P      0      P P-----P P      1      P WWWWWWWWW         </pre>	<pre> WWWWWWWWW P        P P 0   1   0 P P        P WWWWWWWWW         </pre>
--	--

P: periodic face

W: wall face

The following partitioning will not run. Normally, it will never happen with **Metis** or **Tranche** algorithms if **periodique** keyword is used to define the periodic boundaries.

<pre> WWWWWWWWW P        P P 0     1  P P        P WWWWWWWWW         </pre>	<pre> WWWWWWWWW P          1  P P-----   P P  0   -----P WWWWWWWWW         </pre>
---	---

## 2.21.2SCATTER

Keyword to read a partitioned mesh during a parallel calculation.

**Scatter** name.Zones domain\_name

**Scatter** name.Zones domain\_name: Keyword to read the partitions of the domain domain\_name in the files called name\_0001.Zones to name\_000n.Zones. The files are by default in binary format since the 1.4.8 version. To read formatted .Zones files from an older version, use the **ScatterFormatte** keyword:

**ScatterFormatte** name.Zones domain\_name

**ScatterMED** domain\_name file.med

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This keyword will read the partition of the domain\_name domain into a the MED format files file.med created by Medsplitter.

### 2.21.3MPIRUN

Command line to run a parallel calculation. First the data file (ex: study.data) must contain directive **Partition** to partition the domain and the Trio\_U binary must be ran in sequential mode.

```
$ $exec study 1>out 2>err
```

Then, once the files containing the partitions are generated, change the data file to add the **Scatter** directive to read theses files. Then, we can run Trio\_U in parallel mode thanks to mpirun:

```
$ mpirun -np n $exec study n 1>out 2>err
```

n is the number of cpus which should match the number of partitions.



## 2.22 TOOLS

### 2.22.1 POST PROCESSING

#### 2.22.1.1 Lata2dx

lata2dx is an external tool, which can be used with command lines, to convert LATA or LML files to LATA, OPENDX or PRM files. The source files are located in \$TRIO\_U\_ROOT/Outils/lata2dx/lata2dx. The LATA plugin (\$TRIO\_U\_ROOT/VisIt/plugins/lata) used to import LATA or LML files into VisIt is built with some classes of the lata2dx tool.

The tool lata2dx is compiled during Trio\_U build process. The binary lata2dx is located into \$TRIO\_U\_ROOT/exec

How to use lata2dx is given by running lata2dx:

```
veymont.intra.cea.fr/work/triou > lata2dx
Usage : lata2dx input_file_name
[timestep=n]
[domain=name]
[component=label]
[[binary|ascii]] [bigendian|littleendian]] [[int32|int64]] [[real32|real64]]
  [[binout|asciiout]]  [[bigendianout|littleendianout]]  [[int32out|int64out]]  [[real32out|
real64out]]
[forcegroup]
[regularize=tolerance [invalidate]]
[reconnect=tolerance]
[verbosity=n]
[fortranblocs=no]
...
```

So we will not describe all the options and will just give some few examples. By default, lata2dx converts a LATA file into a OPENDX file on the standard output.

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To convert a binary LATA file to an ASCII LATA file:

**lata2dx** input.lata writelata\_convert=output.lata asciout fortranblocs=no

To convert a LML file to an LATA file:

**lata2dx** input.lml writelata\_convert=output.lata

To select a mesh at several timesteps and several fields:

**lata2dx** input.lata writelata\_convert=output.lata timestep=N1 timestep=N2 ...  
domain=MESH1 component=FIELD1 component=FIELD2

To calculate a time average:

**lata2dx** input.lata writelata=avg.lata timeaverage=rectangles rms\_fluctuations

Each field is replaced by its time average into the input file input.lata. rms\_fluctuations adds new fields rms\_fluct\_XXX for each field XXX.

To build a new LATA file with a reconnect partitioned mesh in a parallel calculation:

**lata2dx** input.lata writelata=output.lata reconnect=epsilon

Where epsilon ( $\sim 1.e-7$  \* biggest size of the mesh) is the biggest length to considerate two points as separated.

...

## 2.22.2 KEYWORD USEFUL FOR DEBUGGING

### 2.22.2.1 Debug

Keyword to debug some differences between two Trio\_U versions on a same data file.

**Debug** problem\_name file\_to\_write\_domain file\_to\_write\_faces error mode\_debug

**problem\_name** : Name of the problem to debug

**file\_to\_write\_domain** : Name of the file where domain will be written in sequential calculation

**file\_to\_write\_faces** : Name of the file where faces will be written in sequential calculation

**error** : Minimal value (by default  $1.e-20$ ) for the differences between the two codes

**mode\_debug** : By default -1 (nothing is written in the different files), you will set 0 for the run with the first code, and 1 for the run with the second code.

If you want to compare the results of the same code in sequential and parallel calculation, first run (mode\_debug=0) in sequential mode (the files file\_to\_write\_domain and file\_to\_write\_faces will be written first) then the second run in parallel calculation (mode\_debug=1).

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During the first run (mode\_debog=0), it prints into the file DEBOG, values at different points of the code thanks to the C++ instruction call.

see for example in Noyau/Resoudre.cpp file the instruction:

```
Debog::verifier(msg,value);
```

Where msg is a string and value may be a double, integer or array.

During the second run (mode\_debog=1), it prints into a file Err\_Debog.dbg the same messages than in the DEBOG file and checks if the differences between results from the two codes are less than error. If not, it prints Ok else show the differences and the lines where it occurred.

*Example:*

dimension 2

Pb\_Thermohydraulique pb

...

Discretize pb dis

**Debog** pb seq faces 1.e-6 0

Read pb { ... }

Solve pb

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## 3.FILES EXAMPLES

### 3.1 MESH FILES

The following is an example of a commented Trio\_U mesh file:

```

ENVEL  <- Nom du domaine (domain name)
2      <- Nombre de valeurs a lire ensuite (number of values to be then read)
60 3   <- Nombre de sommets et dimension (number of peaks and dimension)
180    <- Nombre de valeurs a lire ensuite (number of values to be then read)
.0 .0 .0  <- Liste des coordonnees x y z des sommets (list of peak x y z co-ordinates)
.0 .0 .5
.0 .0 1.0
.0 .0 1.5
.0 .0 2.0
.0 .0 2.5
.0 .0 3.0
.0 .5 .0
.0 .5 .5
.0 .5 1.0
.0 .5 1.5
.0 .5 2.0
.0 .5 2.5
.0 .5 3.0
.0 1.0 .0
.0 1.0 .5
.0 1.0 1.0
.0 1.0 1.5
.0 1.0 2.0
.0 1.0 2.5
.0 1.0 3.0
.5 .0 .0
.5 .0 .5
.5 .0 1.0
.5 .0 1.5
.5 .0 2.0
.5 .0 2.5
.5 .0 3.0
.5 .5 .0
.5 .5 .5
.5 .5 1.0
.5 .5 1.5
.5 .5 2.0
.5 .5 2.5
.5 .5 3.0
.5 1.0 .0
.5 1.0 .5
.5 1.0 1.0
.5 1.0 1.5
.5 1.0 2.0
.5 1.0 2.5
.5 1.0 3.0
1.0 .0 .0
1.0 .0 .5
1.0 .0 1.0
1.0 .0 1.5

```



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1.0.0 2.0  
1.0.0 2.5  
1.0.5 0  
1.0.5 5  
1.0.5 1.0  
1.0.5 1.5  
1.0.5 2.0  
1.0.5 2.5  
1.0 1.0.0  
1.0 1.0.5  
1.0 1.0 1.0  
1.0 1.0 1.5  
1.0 1.0 2.0  
1.0 1.0 2.5

{        <- Debut de la definition des zones du domaine (start of domain area definition)

VOLUME1    <- Nom de la zone (area name)

Hexaetre    <- Type de l'element (HEXAEDRE,TETRAEDRE,RECTANGLE,TRIANGLE) (element type  
(HEXAGON,TETRAHEDRAL,RECTANGLE,TRIANGLE))

2        <- Nombre de valeurs a lire ensuite (number of values to be then read)

22 8        <- Nombre de mailles et nombre de sommets par maille (number of meshes and number of peaks per mesh)

176        <- Nombre de valeurs a lire ensuite (number of values to be then read)

0 1 7 8 21 22 28 29 30 <- Liste des sommets de chaque maille (list of peaks for each mesh)

1 2 8 9 22 23 29 30 <- A noter que la numerotation des sommets demarre de 0 (it should be noted that peak numbering starts at 0)

2 3 9 10 23 24 30 31

3 4 10 11 24 25 31 32

4 5 11 12 25 26 32 33

5 6 12 13 26 27 33 34

7 8 14 15 28 29 35 36

8 9 15 16 29 30 36 37

9 10 16 17 30 31 37 38

10 11 17 18 31 32 38 39

11 12 18 19 32 33 39 40

12 13 19 20 33 34 40 41

21 22 28 29 42 43 48 49

22 23 29 30 43 44 49 50

23 24 30 31 44 45 50 51

24 25 31 32 45 46 51 52

25 26 32 33 46 47 52 53

28 29 35 36 48 49 54 55

29 30 36 37 49 50 55 56

30 31 37 38 50 51 56 57

31 32 38 39 51 52 57 58

32 33 39 40 52 53 58 59

{        <- Debut de la definition des bords de la zone (start of area edge definition)

LAT        <- Nom du bord (edge name)

QUADRANGLE\_3D <- Type des elements de bords (QUADRANGLE\_3D,TRIANGLE\_3D,SEGMENT\_2D) (type of edge elements)  
(QUADRANGLE\_3D,TRIANGLE\_3D,SEGMENT\_2D)

2        <- Nombre de valeurs a lire ensuite (number of valules to be then read)

32 4        <- Nombre de faces de bord et nombre de sommets par face (number of edge faces and number of peaks per face)

128        <- Nombre de valeurs a lire ensuite (number of values to be then read)

0 1 7 8 <- Liste des sommets de chaque face de bord (list of peaks for each face of the edge)

0 7 21 28

1 2 8 9

2 3 9 10

3 4 10 11

[illegible]



cea DEN

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-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1

, <- Virgule pour separer la definition des bords (comma to separate edge definition

NOR  
QUADRANGLE\_3D

2  
11 4  
44  
14 15 35 36  
15 16 36 37  
16 17 37 38  
17 18 38 39  
18 19 39 40  
19 20 40 41  
35 36 54 55  
36 37 55 56  
37 38 56 57  
38 39 57 58  
39 40 58 59

2  
11 2  
22  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1

,  
SUD  
QUADRANGLE\_3D

2  
11 4  
44  
0 1 21 22  
1 2 22 23  
2 3 23 24  
3 4 24 25  
4 5 25 26



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5 6 26 27  
21 22 42 43  
22 23 43 44  
23 24 44 45  
24 25 45 46  
25 26 46 47

2  
11 2  
22  
-1 -1

-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1  
-1 -1

} <- Fin de la definition des bords de la zone (end of area edge definition)  
vide <- Necessary even if it is not yet used by Trio\_U (this is required, even though it is not yet used by Trio\_U)  
vide <- Idem (ditto)  
vide <- Idem (ditto)  
} <- Fin de la definition des zones du domaine (end of domain area definition)  
vide <- Idem (ditto)



### 3.2 DATA SET FILES

For examples of data set files, see under a Trio\_U distribution in either the **Tests\_reference** directory (simple test cases) or **Validation** directory (more complicated test cases).

### 3.3 RESULT FILE

If the binary option was not requested for postprocessing, an ASCII file nom\_du\_cas.lml is obtained, which has the following format:

nom_code	character string: name of the code used
version	character string: code version
date	3 integers: dd,mm,yy day month year with 2 figures per integer
nom_probleme	character string characterising the problem to be processed (without spaces)
comment	remarks (without blank characters)
format	keyword <b>FORMAT</b> or <b>BINAIRE</b>
<b>GRILLE</b>	keyword
nom_grille	character string: grid name
dim_grille	integer: problem dimension (2D, 3D)
nb_noeud	integer: number of nodes in the grid
xi yi zi	node co-ordinates for i = 1 to nb_nœud (node number)
<b>TOPOLOGIE</b>	keyword
nom_topologie	character string characterising the topology
nom_grille	name of the grid related to this topology
<b>MAILLE</b>	keyword
nb_maille	integer: number of meshes
for each mesh:	
type_maille	element type character string:
	surface elements: <b>POLY4</b> a <b>POLY8</b>
	volume elements: <b>TETRA4</b>
	<b>PRISM6</b>
	<b>VOXEL8</b>
and	
ie1 ie2 .. ien	integers: list of nodes comprising the mesh
<b>FACE</b>	keyword
nb_face	integer: number of faces
for each face:	
type_face	type face character string

linear faces: LINE2  
surface area faces: POLY3 a POLY8

and

if1 if2 .. ifm list of nodes comprising the face  
je1 je2 list of elements touching the face

**TEMPS** keyword present at each time step  
val\_temps time value at the time step in question

**CHAMPPPOINT** keyword

nom\_champ character string characterising the field  
nom\_topologie name of the topology on which the field is defined in points  
temps time value

nom\_var name of the field variable  
nb\_comp number of field components  
unite character string specifying the variable unit  
type\_var character string characterising the variable  
discretization type (P1, P2, etc.)  
nb\_points number of given points

n<sup>3</sup> noeud et valeur du champ list of data i = 1,nb\_points (number of points)

**CHAMPFACE** keyword

nom\_champ character string characterising the field  
nom\_topologie name of the topology on which the field is defined in faces  
temps time value

nom\_var name of the field variable  
nb\_comp number of field components  
unite character string specifying the variable unit  
type\_var character string characterising the variable  
discretization type (P1, P2, etc.)  
nb\_faces number of faces on which the field is given

n<sup>3</sup> face et valeur du champ list of data i = 1,nb\_faces (number of faces)

**CHAMPMAILLE** keyword

nom\_champ character string characterising the field  
nom\_topologie name of the topology on which the field is defined in meshes  
temps time value

nom\_var character string characterising variable  
nb\_comp number of field components  
unite character string specifying the variable unit  
type\_var character string characterising the variable  
discretization type (P1, P2, etc.)  
nb\_mailles number of meshes on which the field is given

n<sup>3</sup> maille et valeur du champ list of data i = 1,nb\_mailles (number of meshes)

**FIN** keyword which should end the graph file

An example of a lml file, example.lml:

```

Trio_U Version1 01/09/96
exemple
Trio_U
GRILLE
Grille_dom 3 18
0.00000000e+00 0.00000000e+00 0.00000000e+00
5.00000000e-02 0.00000000e+00 0.00000000e+00
1.00000000e-01 0.00000000e+00 0.00000000e+00
0.00000000e+00 5.00000000e-02 0.00000000e+00
5.00000000e-02 5.00000000e-02 0.00000000e+00
1.00000000e-01 5.00000000e-02 0.00000000e+00
0.00000000e+00 1.00000000e-01 0.00000000e+00
5.00000000e-02 1.00000000e-01 0.00000000e+00
1.00000000e-01 1.00000000e-01 0.00000000e+00
0.00000000e+00 0.00000000e+00 1.00000000e+00
5.00000000e-02 0.00000000e+00 1.00000000e+00
1.00000000e-01 0.00000000e+00 1.00000000e+00
0.00000000e+00 5.00000000e-02 1.00000000e+00
5.00000000e-02 5.00000000e-02 1.00000000e+00
1.00000000e-01 5.00000000e-02 1.00000000e+00
0.00000000e+00 1.00000000e-01 1.00000000e+00
5.00000000e-02 1.00000000e-01 1.00000000e+00
1.00000000e-01 1.00000000e-01 1.00000000e+00
TOPOLOGIE
Topologie_Cavite Grille_dom
MAILLE
4
VOXEL8 1 2 4 5 10 11 13 14
VOXEL8 2 3 5 6 11 12 14 15
VOXEL8 4 5 7 8 13 14 16 17
VOXEL8 5 6 8 9 14 15 17 18
FACE
0
TEMPS 0.00000000e+00
CHAMPPPOINT pression_som_dom Topologie_Cavite 0.00000000e+00
pression_som_dom 1 Pa.m3/kg
type0 18
1 0.00000000e+00
2 0.00000000e+00
3 0.00000000e+00
4 0.00000000e+00
5 0.00000000e+00
6 0.00000000e+00
7 0.00000000e+00
8 0.00000000e+00
9 0.00000000e+00
10 0.00000000e+00
11 0.00000000e+00
12 0.00000000e+00
13 0.00000000e+00
14 0.00000000e+00
15 0.00000000e+00
16 0.00000000e+00
17 0.00000000e+00
18 0.00000000e+00
CHAMPMAILLE vitesseX_elem_dom Topologie_Cavite 0.00000000e+00
vitesseX_elem_dom 1 m/s
type0 4
1 0.00000000e+00
2 0.00000000e+00

```



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```
3 0.00000000e+00
4 0.00000000e+00
CHAMPMAILLE vitesseY_elem_dom Topologie_Cavite 0.00000000e+00
vitesseY_elem_dom 1 m/s
type0 4
1 0.00000000e+00
2 0.00000000e+00
3 0.00000000e+00
4 0.00000000e+00
CHAMPPPOINT vitesse_som_dom Topologie_Cavite 0.00000000e+00
vitesse_som_dom 3 m/s
type1 18
1 0.00000000e+00 0.00000000e+00 0.00000000e+00
2 0.00000000e+00 0.00000000e+00 0.00000000e+00
3 0.00000000e+00 0.00000000e+00 0.00000000e+00
4 0.00000000e+00 0.00000000e+00 0.00000000e+00
5 0.00000000e+00 0.00000000e+00 0.00000000e+00
6 0.00000000e+00 0.00000000e+00 0.00000000e+00
7 0.00000000e+00 0.00000000e+00 0.00000000e+00
8 0.00000000e+00 0.00000000e+00 0.00000000e+00
9 0.00000000e+00 0.00000000e+00 0.00000000e+00
10 0.00000000e+00 0.00000000e+00 0.00000000e+00
11 0.00000000e+00 0.00000000e+00 0.00000000e+00
12 0.00000000e+00 0.00000000e+00 0.00000000e+00
13 0.00000000e+00 0.00000000e+00 0.00000000e+00
14 0.00000000e+00 0.00000000e+00 0.00000000e+00
15 0.00000000e+00 0.00000000e+00 0.00000000e+00
16 0.00000000e+00 0.00000000e+00 0.00000000e+00
17 0.00000000e+00 0.00000000e+00 0.00000000e+00
18 0.00000000e+00 0.00000000e+00 0.00000000e+00
TEMPS 2.00000000e-02
CHAMPPPOINT pression_som_dom Topologie_Cavite 2.00000000e-02
pression_som_dom 1 Pa.m3/kg
type0 18
1 -3.72315262e-07
2 0.00000000e+00
3 3.72315262e-07
4 0.00000000e+00
5 0.00000000e+00
6 0.00000000e+00
7 3.72315262e-07
8 0.00000000e+00
9 -3.72315262e-07
10 -3.72315262e-07
11 0.00000000e+00
12 3.72315262e-07
13 0.00000000e+00
14 0.00000000e+00
15 0.00000000e+00
16 3.72315262e-07
17 0.00000000e+00
18 -3.72315262e-07
CHAMPMAILLE vitesseX_elem_dom Topologie_Cavite 2.00000000e-02
vitesseX_elem_dom 1 m/s
type0 4
1 0.00000000e+00
2 -1.48926105e-07
3 0.00000000e+00
4 1.48926105e-07
CHAMPMAILLE vitesseY_elem_dom Topologie_Cavite 2.00000000e-02
vitesseY_elem_dom 1 m/s
```



cea DEN

# TRIO-U

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```
type0 4
1 0.00000000e+00
2 0.00000000e+00
3 1.48926105e-07
4 -1.48926105e-07
CHAMPPPOINT vitesse_som_dom Topologie_Cavite 2.00000000e-02
vitesse_som_dom 3 m/s
type1 18
1 0.00000000e+00 0.00000000e+00 0.00000000e+00
2 0.00000000e+00 0.00000000e+00 0.00000000e+00
3 0.00000000e+00 0.00000000e+00 0.00000000e+00
4 0.00000000e+00 0.00000000e+00 0.00000000e+00
5 0.00000000e+00 0.00000000e+00 0.00000000e+00
6 0.00000000e+00 0.00000000e+00 0.00000000e+00
7 0.00000000e+00 0.00000000e+00 0.00000000e+00
8 0.00000000e+00 0.00000000e+00 0.00000000e+00
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13 0.00000000e+00 0.00000000e+00 0.00000000e+00
14 0.00000000e+00 0.00000000e+00 0.00000000e+00
15 0.00000000e+00 0.00000000e+00 0.00000000e+00
16 0.00000000e+00 0.00000000e+00 0.00000000e+00
17 0.00000000e+00 0.00000000e+00 0.00000000e+00
18 0.00000000e+00 0.00000000e+00 0.00000000e+00
FIN
```

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## 4.PUBLICATIONS

### **Notes:**

#### **STR/LML/92136**

"Projet TRIO Unitaire – Premières spécifications théoriques" (Unit TRIO project - first theoretical specifications)  
O. CUETO, J.P. MAGNAUD, M.VILLAND

#### **STR/LML/93-183**

"Développement de TRIO-U: planning prévisionnel" (TRIO-U development: forecast scheduling)  
M. FARVACQUE, J.C. MICAELLI

#### **STR/LMTL/96-20**

"TRIO-U: Document de conception TRIO-U Version1" (TRIO U: TRIO-U Version1 design documentation)  
M. FARVACQUE, O. CUETO, Ph. EMONOT

#### **STR/LMTL/96-21**

"TRIO-U: Manuel d'utilisation" (TRIO U: User manual)  
P. LEDAC

#### **STR/LMTL/96-36**

"TRIO-U: Manuel informatique" (TRIO U: Computer manual)  
M. FARVACQUE

#### **STR/LMTL/96-88**

"TRIO-U: User manual"  
O. CUETO, Ph. EMONOT , P. LEDAC

#### **SMTH/LATA/97-001**

F. Barré, D. Laurence  
"Etude d'opportunité – Modélisation des écoulements turbulents" (Opportunity analysis - modelling of turbulent flow)

#### **SMTH/LATA/97-003**

B Bollini, Y. Hascoët  
"Conception et développement d'une IHM pour le code de thermohydraulique TRIO-U" (design and development of an GUI for the TRIO-U thermohydraulic code)  
*Work placement report*

#### **SMTH/LATA/97-006**

ASilveira Neto, Ph. Emonot  
"Simulation numérique fine des écoulements turbulents diphasiques non miscibles" (fine digital simulation of non-miscible disphase turbuent flow)

#### **SMTH/LATA/97-009**

B Piuze, Ph. Emonot  
"Conception et développement d'une IHM pour TRIO-U" (design and development of an GUI for TRIO-U)  
*Work placement report*

#### **SMTH/LATA/97-010**

TRIO-U Work Group

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"Plan de développement de TRIO-U version 2 – Objectifs, contenu du noyau de la version 2, architecture logiciel, co-développement" (TRIO-U version 2 development schedule - goals, content of version 2 core, software architecture, co-development)

**SMTH/LATA/97-012**

Barsamian, O. Cueto, Ph. Emonot

"Application of the dynamic subgrid scale model to TRIO-U"

Technical report

**SMTH/LATA/97-013**

C. Calvin, P. Ledac

"Mesures de performances de TRIO-U sur machines scalaires et parallèles" (measurement of TRIO-U performance on scalar and parallel machines)

**SMTH/LATA/97-014**

TRIO-U Work Group

"Cahier des charges de l'audit de la version 1 de TRIO-U" (TRIO-U version 1 audit specification)

**SMTH/LATA/97-015**

C. Calvin, M. Cordebard

"Intégration d'un découpeur de domaines dans le logiciel de calcul TRIO-U" (incorporation of a domain partitionner into the TRIO-U calculation software)

*Work replacement report*

**SMTH/LATA/97-018**

C. Calvin, Ph. Emonot

"The Parallelism in the TRIO-Unitaire Project"

Communication presented at NURETH'8, Japan, 30/09/97-04/10/97

**SMTH/LATA/97-021**

ASilveira Neto, Ph. Emonot

"The front-tracking method for interface transport"

Communication presented at "European two-phase flow group meeting", Brussels 6-7/06/1997

**SMTH/LATA/97-023**

Barsamian, O. Cueto, Ph. Emonot

"Application of the dynamic subgrid scale model to TRIO-U"

(Further information to note 97-12)

**SMTH/LATA/97-024**

C. Calvin, Ph. Emonot

"The TRIO-Unitaire Project: a parallel CFD 3-dimensional code"

Communication presented at ISCOPE'97, USA, 08-11/12/97

**SMTH/LATA/97-026**

F. Barré, I. Toumi

"Module diphasique tridimensionnel avec approche moyennée de TRIO-U: cahier des charges" (tridimensioned two phase module with the TRIO-U averaging method: specifications)

**SMTH/LATA/97-028**

O. Cueto, C. Calvin, Ph. Emonot

"Principes généraux de la structure logicielle de la version 1 de TRIO-U" (main principles of TRIO-U version 1 software structure)

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#### **SMTH/LATA/98-30**

F. Barré, D. de Crécy, D. Bestion, Ph Emonot, AForestier, J. Gauvain, J.P. Magnaud, I. Toumi, M. Grandotto, N. Thuy

"Organisation du projet TRIO-U" (TRIO-U project organisation)

#### **SMTH/LATA/98-33**

C.Calvin

"Manuel utilisateur de Trio\_U parallèle et environnement d'utilisation sur CRAY T3E" (operation environment on CRAY T3E and parallel Trio\_U user manual)

#### **SMTH/LATA/98-41**

P. Barron, C. Dumas, C.Calvin

"Introduction de méthodes de type multi-grilles dans le code TRIO-U" (Introduction of multi-grid type methods in TRIO-U code)

*Work replacement report*

#### **SMTH/LATA/98-37**

BMenant

"Analyse à l'aide de TRIO-U du fonctionnement thermohydraulique actuel de CASCAD" (analysis of current CASCAD thermohydraulic operation using TRIO-U)

#### **SMTH/LATA/98-42**

BMenant

"Mise en oeuvre de TRIO-U en vue de l'analyse du fonctionnement thermohydraulique actuel de CASCAD" (implementation of TRIO-U with the aim of analysing current CASCAD thermohydraulic operation)

#### **SMTH/LATA/98-45**

BMenant

"Application de TRIO-U à l'étude du transit d'un bouchon d'eau claire dans un circuit primaire de REP" (application of TRIO-U to the study of the transition of a plug of clear water through a primary REP system)

#### **SMTH/LATA/98-46**

KLatour, O. Cueto

"Introduction de la discrétisation P1-P1 dans le logiciel PRICELES" (introduction of P1-P1 discretization in PRICELES software)

*Work replacement report*

#### **SMTH/LATA/98-50**

U. Bieder, Ph. Emonot, D. Laurence

"PRICELES. Summary of the numerical scheme"

#### **SMTH/LATA/99-56**

C. Ackermann

"Modélisation sous-maille dans le logiciel CEA/EDF PRICELES – 1<sup>ère</sup> partie: tests de validation en maillages structurés" (sub-grid modelling in the CEA/EDF PRICELES software - 1<sup>st</sup> section: validation tests in structured meshes)

#### **SMTH/LATA/99-73**

U. Bieder

"PRICELES. Tests of the numerical scheme"

#### **SMTH/LATA/99-64**



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C. Calvin, Ph Emonot

"Etude préliminaire sur l'utilisation de la STL dans TRIO-U V2" (preliminary study concerning the use of STL in TRIO-U V2)

**SMTH/LATA/99-65**

C. Calvin

"Document de conception détaillée du noyau de la version 1 de TRIO-U" (detailed design document concerning the core of TRIO-U version 1)

**SMTH/LATA/99-66**

C. Calvin

"Document de conception détaillée de la version 1 de TRIO-U: introduction" (TRIO-U version 1 detailed design document: introduction)

**SMTH/LATA/99-67**

C. Calvin

"Document de conception détaillée du module géométrie de la version 1 de TRIO-U" (TRIO-U version 1 geometry module detailed design document)

**SMTH/LATA/99-73**

U. Bieder

"PRICELES. Large Eddy Simulation of the very near wake of a circular cylinder"

**SMTH/LATA/99-74**

O. Cueto, G. Fauchet

"Un premier résultat du module diphasique de TRIO-U" (first result for the TRIO-U two phase module)

**Publications:**

**C. Calvin, Ph. Emonot**

"The TRIO-U project: a parallel CFD 3-dimensional code"  
ISCOPE'97, USA, 08-11/12/97

**C. Calvin, Ph. Emonot**

"The Parallelism in the TRIO-Unitaire Project"  
NURETH'8, Japan, 30/09/97-04/10/97

**M. Farvacque, O. Cueto, F. Barré, Ph. Emonot**

"TRIO-U: a new generation of thermalhydraulics computer code"  
NURETH'8, Japan, 30/09/97-04/10/97

**C. Calvin**

"Large thermalhydraulic 3D simulations using TRIO-U code on CRAY T3E"  
3<sup>rd</sup> European SGI/CRAY MPP Workshop, Paris, France, 11-12/09/07

**C. Ackerman**

"Modèles sous-maille pour la thermohydraulique des réacteurs" (sub-grid model for reactor thermohydraulics)  
Séminaire du Centre de physiques des Houches sur les écoulements turbulents complexes, (Houche physics centre symposium on complex turbulent flow), France, 04-07/05/99

**U. Bieder, C. Calvin, Ph Emonot**

"Industrial application of Large Eddy Simulations: validation of a new numerical scheme"  
8<sup>th</sup> International Symposium on CFD, Brême, Germany, 5-10/09/99

	<h1 style="text-align: center;">TRIO-U</h1> <p style="text-align: center;">USER'S MANUAL v1.7.0 08/04/2015</p>	DM2S/STMF/LMSF
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### **O. Cueto**

"Module diphasique de TRIO-U: la méthode ICE" (TRIO-U two phase module: the ICE method)  
Atelier sur les schémas de flux pour la simulation numérique des écoulements diphasiques (workshop concerning flux schemes for digital simulation of two phase flows), Cargèse, France, 22-24/09/99

### **I. Toumi, A Kumbaro, H. Paillère, F. Barré, O. Cueto**

"Numerical methods and physical models for two-phase flow simulations in the TRIO-U code"  
*9<sup>th</sup> International Topical Meeting on Nuclear Reactor Thermal Hydraulics (NURETH'9)*, San Francisco, USA, 3-8/10/99

### **C. Calvin**

"TRIO-U: le code avancé de mécanique des fluides du CEA/DRN" (TRIO-U: CEA/DRN's advanced fluid mechanics code)  
*4<sup>th</sup> Convention of CEA partners, Grenoble, France, 16/11/99*

### **F. Barré, D. Laurence**

"Priceles, une plate-forme avancée pour la simulation de la turbulence" (Priceles, an advanced platform for turbulence simulation)  
*4<sup>th</sup> Convention of CEA partners, Grenoble, France, 16/11/99*

### **C. Calvin**

"TRIO-U: le code avancé de mécanique des fluides du CEA/DRN" (TRIO-U: CEA/DRN's advanced fluid mechanical code)  
*4<sup>th</sup> Convention of CEA partners, Grenoble, France, 16/11/99*

### **U. Bieder, C. Calvin, Ph. Emonot.**

"PRICELES: AParallel CFD 3-Dimensional Code for Industrial Large Eddy Simulations"  
*Parallel CFD 2000, Trondheim-Norway, 2000.*

### **U. Bieder, C. Calvin, Ph. Emonot.**

"PRICELES: An Object Oriented Code for Industrial Large Eddy Simulations"  
CFD2K, Montréal-Canada, 2000.

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## 5.FRENCH-ENGLISH DICTIONNARY FOR TRIO\_U KEYWORDS

Although most keywords in Trio\_U have English counterparts with a similar spelling, there are some exceptions and users not so familiar with English would anyway not find straightforward to guess the English translation thus the meaning of a Trio keyword.

These pages are intended to help non French speaking Trio\_U users to get familiar with the keywords used throughout the input data file of Trio\_U.

### Easy ones:

Fortunately the most numerous, just a couple of letters at the end change between English and French

- Probleme, Domaine, Origine, Limite, Frontiere, Initiale, Molaire, Uniforme = problem, domain, origin, limit, frontier, initial, molar, uniform
- Objet = object
- Schema = scheme
- Pave = pave (to pave the floor with stones, tiles, cobbles...)
- Homogene = homogeneous
- Thermohydraulique, Volumique, Surfaceutique, Hyperbolique, periodique, adiabatique = thermal-hydraulic, volumic, surfacic, hyperbolic, periodic, adiabatic
- Tabule = tabulated
- Tangentiel = tangential
- Solide, fluid = solid, fluid
- Porosite, diffusivite, viscosite = porosity, diffusivity, viscosity

### A bit harder to guess... ?

- Calculer (abbreviated as "calc")= to calculate, to compute
- Solveur = solver
- Nombre = number
- Facteur = factor
- Sous-zone = sub-zone
- Champ = field (of a variable)
- Morceau = a piece, a chunk
- Echange = exchange

### Names:

- Temps = time
- Vitesse = velocity
- Pression = pressure
- Chaleur = heat
- Paroi = wall
- Fichier = file
- Sonde = probe
- Amont = upwind
- Moyenne = average
- Ecart\_type = root mean square
- Longueur = length
- Noeud = node (of a grid)
- Bord = edge
- Chapeau = hat (cosine shaped)
- Tourbillon = vortex

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- Bruit = noise
- Perte de charge = pressure loss, head loss

### Verbs:

- Ecrire = to write
- Trianguler = to mesh a 2D surface with triangles
- Tetraedriser = to mesh a 3D volume with tetrahedrons
- Imprimer = to print
- Sauvegarde = the action of saving the job results
- Reprise = the action of restarting a job from previously saved results

### Adjectives:

- Parfait = perfect( for a gas)
- Imposer(e) = imposed
- Ouvert(e) = open
- Defilante = moving
- Bas = low

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## 6.TEST CASES INDEX

Test cases can be found in the \$TRIO\_U\_ROOT/tests directory.

Keywords	Test case 1	Test case 2	Test case 3
1d	<a href="#">Traitement Particulier THI_VEF</a>		
3d	<a href="#">Extract 2D from 3D_VEF</a>	<a href="#">Traitement Particulier THI_VEF</a>	
abs	<a href="#">test_op_conv_vef_jdd1</a>	<a href="#">test_op_conv_vef_jdd2</a>	<a href="#">test_op_conv_vef_jdd3</a>
acceleration	<a href="#">Cylindre_tournant</a>	<a href="#">Champ_tabule_temps</a>	<a href="#">Repere_Translation</a>
XXXsource_term_acceleration			
acceleration_terme_source	<a href="#">Cylindre_tournant</a>	<a href="#">Champ_tabule_temps</a>	<a href="#">Repere_Translation</a>
active	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_Chute_Goutte_2D</a>	<a href="#">FTD_VDF_parallel_ok</a>
XXXadiabatic			
adiabatique			
acos			
XXXadd_phase0			
ajout_phase0	<a href="#">FTD_VDF_parallel_ok</a>	<a href="#">FTD_reprise_xyz_vdf_3d</a>	
XXXadd_phase1			
ajout_phase1	<a href="#">FTD_VEF_parallel_ok</a>	<a href="#">FTD_Transfo_bulles_VDF_3D</a>	<a href="#">FTD_Transfo_bulles_VEF_3D</a>
XXXrandom			
aleatoire	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VEF_2D</a>	<a href="#">Quasi_Comp_IBC_VDF_2D</a>
alpha	<a href="#">2Tri</a>	<a href="#">2Cubes</a>	<a href="#">4Cubes</a>
XXXsubzone_alpha			
alpha_sous_zone	<a href="#">EF_stab_alpha_sous_zone</a>		
XXXupwind			
amont	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">sans</a>
XXXold_upwind			
amont_old	<a href="#">test_op_conv_vef_jdd4</a>		
XXXsubzone_upwind			
amont_sous_zone	<a href="#">EF_stab_ss_zone_Amont</a>	<a href="#">EF_stab_alpha_sous_zone</a>	
XXX			
ampli_bruit	<a href="#">LP_WW_VDF</a>	<a href="#">LP_WW_VEF</a>	<a href="#">Init_canal</a>
XXX			
ampli_fluctuation	<a href="#">Chmoy_faceperio</a>	<a href="#">Test_recycl_fluct</a>	
XXX			
ampli_moyenne_imposee	<a href="#">OBI_diffuser_VEF_k_eps_jdd1</a>	<a href="#">OBI_diffuser_VEF_k_eps_jdd2</a>	<a href="#">ChannelKEps_CLboitePerio_entree_jdd1</a>
XXX			
ampli_moyenne_recyclee	<a href="#">OBI_diffuser_VEF_k_eps_jdd1</a>	<a href="#">OBI_diffuser_VEF_k_eps_jdd2</a>	<a href="#">ChannelKEps_CLboitePerio_entree_jdd1</a>
XXX			
ampli_sin	<a href="#">Init_canal</a>	<a href="#">TBLE_VDF_3D</a>	<a href="#">DYN_6_points</a>
XXX			
amplitude	<a href="#">CL_var</a>	<a href="#">centre4_VDF</a>	
XXXangle_analyse			
analyse_angle	<a href="#">Kernel_MED_2D_gmsh</a>	<a href="#">Kernel_Raffiner_simplex_jdd5</a>	<a href="#">Kernel_Raffiner_simplex_jdd6</a>
XXXanalytic			
analytique	<a href="#">pena_ellipsoide_jdd1</a>	<a href="#">pena_ellipsoide_jdd2</a>	
XXXold			
ancien	<a href="#">test_conservation_energie_QC_jdd1</a>	<a href="#">test_conservation_energie_QC_jdd4</a>	
XXXboussinesq_approximation			

<b>approximation_de_boussinesq</b>	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
<b>XXXedge</b>			
<b>arete</b>			
<b>associate</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
<b>associer</b>	<a href="#">Collecteur</a>	<a href="#">PETSC_OPENMP</a>	<a href="#">resume_last_time</a>
<b>XXXwith_some_boundaries</b>			
<b>avec_certains_bords</b>	<a href="#">Cx</a>	<a href="#">Collecteur</a>	<a href="#">VAHL_DAVIS</a>
<b>XXXwith_some_boundaries_for_extract_surface</b>			
<b>avec_certains_bords_pour_extraire_surface</b>			
<b>atanh</b>			
<b>XXXwith_kinetic_energy</b>			
<b>avec_energie_cinetique</b>	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
<b>XXXwith_boundaries</b>			
<b>avec_les_bords</b>	<a href="#">Extrait_plan</a>	<a href="#">Extraire_domaine_2D</a>	
<b>XXXwith_boundary_conditions</b>			
<b>avec_les_cl</b>			
<b>XXXwith_source_terms</b>			
<b>avec_sources</b>	<a href="#">debit_impose_jdd1</a>	<a href="#">debit_impose_jdd2</a>	<a href="#">debit_impose_jdd3</a>
<b>XXXwith_source_terms_and_operators</b>			
<b>avec_sources_et_operateurs</b>			
<b>axi</b>	<a href="#">Th_Axi</a>	<a href="#">Hyd_Axi</a>	<a href="#">ThHyd_Axi_3D</a>
<b>XXX</b>			
<b>base</b>	<a href="#">centre4_VDF</a>	<a href="#">Cell_numbers_VDF</a>	<a href="#">ibc_refroidi_jdd1</a>
<b>beta</b>	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
<b>beta_co</b>	<a href="#">Hyd_C_RK3</a>	<a href="#">diagonale</a>	<a href="#">Boussinesq</a>
<b>beta_th</b>	<a href="#">Cx</a>	<a href="#">Debog</a>	<a href="#">EF_2D</a>
<b>beta_transfo</b>			
<b>bicgstab</b>	<a href="#">Collecteur</a>	<a href="#">Def_VEF_impl</a>	<a href="#">QC_VDF_diff_impl</a>
<b>bidim_axi</b>	<a href="#">Th_Axi_RZ</a>	<a href="#">Hyd_Axi_RZ</a>	<a href="#">Radiation_jdd9</a>
<b>XXXbinary</b>			
<b>binaire</b>	<a href="#">Cx</a>	<a href="#">sreprise</a>	<a href="#">stat_VEF</a>
<b>block_jacobi_icc</b>			
<b>XXXbox</b>			
<b>boite</b>	<a href="#">Tuyau</a>	<a href="#">Kernel</a>	<a href="#">keps_3D_VEF</a>
<b>boomeramg</b>	<a href="#">PETSC_cpu_3D_MG</a>		
<b>XXXboundary</b>			
<b>bord</b>	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">RK2</a>
<b>XXXboundaries</b>			
<b>bords</b>	<a href="#">ThHyd_keps_VEF</a>	<a href="#">ChFrontLu_gen_file</a>	<a href="#">ThHyd_keps_VEF_perio</a>
<b>XXXboundaries_to_cut</b>			
<b>bords_a_decouper</b>	<a href="#">geom2ansys</a>	<a href="#">Test_Radiation_dec</a>	
<b>boundary_xmin</b>	<a href="#">MaillerParallel</a>		
<b>boundary_xmax</b>	<a href="#">MaillerParallel</a>		
<b>boundary_ymin</b>	<a href="#">MaillerParallel</a>		
<b>boundary_ymax</b>	<a href="#">MaillerParallel</a>		

boundary_zmin	<a href="#">MaillerParallel</a>		
boundary_zmax			
boussinesq_concentration	<a href="#">Boussinesq</a>	<a href="#">Champ_fonc_fonction</a>	<a href="#">ThHyd_C_K_Eps_P0P1Pa</a>
boussinesq_temperature	<a href="#">Debog</a>	<a href="#">EF_2D</a>	<a href="#">Cl_var</a>
c0	<a href="#">Boussinesq</a>	<a href="#">CoefDiffNul</a>	<a href="#">Champ_fonc_fonction</a>
c1_eps	<a href="#">Marche</a>	<a href="#">docond_BasRe</a>	<a href="#">Marche_incline</a>
c1_teta			
c2_eps	<a href="#">Marche</a>	<a href="#">docond_BasRe</a>	<a href="#">Marche_incline</a>
c2_teta			
c3_eps	<a href="#">ThHyd_KEPS_VEF</a>	<a href="#">ThHyd_Cond_K_Eps</a>	<a href="#">Hyd_C_KEPS_2D_VEF</a>
c3_teta			
ca			
XXX			
calc_spectre	<a href="#">TP_THI_VDF</a>	<a href="#">SGE_Fst_VDF</a>	<a href="#">SGE_Fst_sel_VDF</a>
XXX			
calcul	<a href="#">VAHL_DAVIS_VEF</a>		
XXX			
calcul_ldp_en_flux_impose	<a href="#">Test_tparoi_jdd3</a>	<a href="#">Test_2D_VEF_Radiation_K_Eps</a>	
XXX			
calculer_moments	<a href="#">M3DLAM</a>	<a href="#">upwind</a>	<a href="#">VAHL_DAVIS_VEF</a>
XXXperiodic_channel			
canal_perio	<a href="#">Tuyau</a>	<a href="#">LP_WW_VDF</a>	<a href="#">LP_WW_VEF</a>
XXX			
canalx	<a href="#">Paroi_rugueuse</a>	<a href="#">ThHyd_Coupl_LM_2D_VEF</a>	<a href="#">ThHyd_Coupl_LM_3D_VEF</a>
cb			
cc			
cd			
XXX			
centre4	<a href="#">centre4_VDF</a>	<a href="#">centre4_VEF</a>	<a href="#">QC_centre4_VDF</a>
XXX			
centre	<a href="#">THI</a>	<a href="#">LP_WW_VDF</a>	<a href="#">Import_MED</a>
XXX			
centre_de_gravite	<a href="#">M3DLAM</a>	<a href="#">upwind</a>	<a href="#">Cylindre_tournant</a>
XXX			
centre_rotation	<a href="#">Cylindre_tournant</a>	<a href="#">Repere_Rotation_VEF</a>	<a href="#">Repere_Rotation_Variable</a>
c_ext	<a href="#">Hyd_C_RK3</a>	<a href="#">diagonale</a>	<a href="#">tubeY_jdd1</a>
chakravorthy	<a href="#">EFstab_Muscl_and_Limiters_VEF_jdd5</a>	<a href="#">EFstab_Muscl_and_Limiters_VEF_jdd12</a>	
XXX			
chaleur_latente	<a href="#">FTD_2D_Axi</a>	<a href="#">FTD_Boiling_bubble</a>	<a href="#">FTD_Couplage_champ_cl_VDF</a>
XXXfield_readXXX			
champ_don_lu	<a href="#">periodique</a>		
XXXfield_function			
champ_fonc_fonction	<a href="#">diagonale</a>	<a href="#">Wale_Prdt_Dyn</a>	<a href="#">QC_centre4_VDF</a>
XXXfield_function_txyz			
champ_fonc_fonction_txyz	<a href="#">Champ_fonc_fonction_txyz_VDF</a>	<a href="#">Champ_fonc_fonction_txyz_VEF</a>	
XXXfield_function_med			



champ_fonc_med	<a href="#">Import_MED</a>	<a href="#">Extrait_plan</a>	<a href="#">Champ_fonc_MED</a>
XXXfield_readXXX			
champ_fonc_reprise	<a href="#">P1toP0P1Pa</a>	<a href="#">P1toP1Bulle</a>	<a href="#">K_eps_init_par_LM</a>
XXXfield_function_tabulated			
champ_fonc_tabule	<a href="#">Phys_var</a>	<a href="#">Nu_var_VEF</a>	<a href="#">Pred_Cor_VEF</a>
XXXfield_function_t			
champ_fonc_t	<a href="#">Cylindre_tournant</a>	<a href="#">Repere_Translation</a>	<a href="#">Repere_Rotation_VEF</a>
XXXfield_function_txyz			
champ_fonc_txyz	<a href="#">Parallele</a>	<a href="#">Champ_fonc_xyz</a>	<a href="#">Champ_Fonc_txyz</a>
XXXfield_function_xyz			
champ_fonc_xyz	<a href="#">2D_P0</a>	<a href="#">2D_P1</a>	<a href="#">3D_P0</a>
XXXboundary_field_analytic			
champ_front_analytique			
XXXboundary_field_noise			
champ_front_bruite	<a href="#">Cl_var</a>	<a href="#">centre4_VDF</a>	
XXXboundary_field_calculated			
champ_front_calc	<a href="#">Collecteur</a>	<a href="#">Champ_front_calc</a>	
XXXboundary_field_flowrate			
champ_front_debit	<a href="#">debit_impose_jdd1</a>	<a href="#">debit_impose_jdd2</a>	<a href="#">debit_impose_jdd3</a>
XXXboundary_field_function			
champ_front_fonction	<a href="#">Himp_var</a>	<a href="#">FTD_VDF_mono_var</a>	
XXXboundary_field_function_txyz			
champ_front_fonc_txyz	<a href="#">Parallele</a>	<a href="#">ChFront(TXYZ)</a>	<a href="#">U_in_var_impl</a>
XXXboundary_field_function_xyz			
champ_front_fonc_xyz	<a href="#">Sondes</a>	<a href="#">ChDonXYZ</a>	<a href="#">PETSC_VEF</a>
XXXboundary_field_read			
champ_front_lu	<a href="#">Impinging_jet</a>	<a href="#">ChFrontLu_read_file</a>	<a href="#">Backward_Facing_Step_3D_jdd1</a>
XXXchamp_front_normal_vef			
champ_front_normal_vef			
XXXboundary_field_recycled			
champ_front_recyclage	<a href="#">smago_VDF</a>	<a href="#">smago_VEF</a>	<a href="#">Chmoy_faceperio</a>
XXXboundary_field_tabulated			
champ_front_tabule	<a href="#">Cl_var</a>	<a href="#">Cl_var_VEF</a>	<a href="#">Hyd_C_VDF_Smago</a>
boundary_field_inward	<a href="#">2D_P1</a>	<a href="#">Inward_field_jdd1</a>	<a href="#">Inward_field_jdd2</a>
XXXboundary_field_tangential_vef			
champ_front_tangentiel_vef	<a href="#">Debog_VEF</a>	<a href="#">Reprise_xyz2</a>	<a href="#">Reprise_xyz3</a>
XXXboundary_field_uniform			
champ_front_uniforme	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
boundary_field_uniform_keps_from_ud	<a href="#">Uniform_keps_front_field_from_u_d_jdd1</a>	<a href="#">Uniform_keps_front_field_from_u_d_jdd2</a>	<a href="#">Uniform_keps_front_field_from_u_d_jdd3</a>
XXXboundary_field			
champ_frontiere	<a href="#">ThHyd_3D_VEFPreP1B</a>	<a href="#">Uniform_keps_front_field_from_u_d_jdd1</a>	<a href="#">Uniform_keps_front_field_from_u_d_jdd2</a>
XXXfield_channel_XXX			
champ_init_canal_sinal	<a href="#">LP_WW_VDF</a>	<a href="#">LP_WW_VEF</a>	<a href="#">Init_canal</a>
XXXfield_med			
champ_med	<a href="#">Extrait_plan</a>		
XXXfield_ostwald			

champ_ostwald	<a href="#">ThHyd_2D_VDF_Ostwald</a>	<a href="#">PETSC_ThHyd_2D_VEF_Ostwald</a>	
XXXfields			
champs	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
XXXfield_nodes_read_vefXXX			
champ_som_lu_vef	<a href="#">TP_THI_VEF</a>	<a href="#">SGE_Fst_VEF</a>	<a href="#">centre_VEF_old</a>
XXXfield_time_tabulated			
champ_tabule_temps	<a href="#">Champ_tabule_temps</a>		
XXXfield_uniform			
champ_uniforme	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
XXXfield_piecewise_uniform			
champ_uniforme_morceaux	<a href="#">Chp_Morc</a>	<a href="#">Polynomes</a>	<a href="#">docond_3D</a>
XXXfield_time_tabulated_piecewise_uniform			
champ_uniforme_morceaux_tabule_temps	<a href="#">ThHyd_Coupl_LM_3D_VEF</a>		
field_uniform_keps_from_ud	<a href="#">Uniform_keps_front_field_from_ud_jdd5</a>	<a href="#">Uniform_keps_front_field_from_ud_jdd6</a>	<a href="#">Uniform_keps_front_field_from_ud_jdd7</a>
XXX			
changement_de_base_p1bulle	<a href="#">THI_VEF</a>	<a href="#">Blocage_Post</a>	<a href="#">VAHL_DAVIS_VEF</a>
XXX			
chapeau	<a href="#">Moyenne_volumique_3d</a>		
XXXchemistry			
chimie	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>	
XXX			
chmoy_faceperio	<a href="#">Chmoy_faceperio</a>		
XXX			
chsom	<a href="#">Sondes</a>	<a href="#">Sondes_chsom</a>	
cholesky	<a href="#">Cx</a>	<a href="#">2D_P0</a>	<a href="#">2D_P1</a>
cholesky_superlu			
cholesky_out_of_core			
cholesky_umfpak			
cholesky_pastix			
circle	<a href="#">Cx</a>	<a href="#">P1toP0PIPa</a>	<a href="#">PETSC_CUDA</a>
XXX			
cl_pression_sommet_faible	<a href="#">Blocage_Post</a>	<a href="#">VAHL_DAVIS_VEF</a>	
cli	<a href="#">PETSC_cpu_3D_CGSPAI</a>		
XXX			
clipping_courbure_interface	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_Chute_Goutte_2D</a>	
cmu	<a href="#">Extraire_domaine_2D</a>		
XXX			
collisions	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_Chute_Goutte_2D</a>	<a href="#">FTD_VDF_parallel_ok</a>
XXXcombination			
combinaison	<a href="#">Flux_CL_periodique</a>	<a href="#">Combinaison_Canal_ThHyd</a>	
XXXcomponent			
compo	<a href="#">Cx</a>	<a href="#">VAHL_DAVIS</a>	<a href="#">VAHL_DAVIS_VEF</a>
coefficient_diffusion	<a href="#">Hyd_C_RK3</a>	<a href="#">diagonale</a>	<a href="#">Boussinesq</a>
XXXactivities_coefficients			
coefficients_activites	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>	
XXXvelocity_coefficient			

coeff_vitesse			
XXXcomponent			
composante	<a href="#">upwind</a>	<a href="#">CoeDiffNul</a>	<a href="#">docond_VEF_3D</a>
concentration	<a href="#">Hyd_C_RK3</a>	<a href="#">diagonale</a>	<a href="#">Boussinesq</a>
XXXmean_concentration			
concmoy			
XXX			
coeff	<a href="#">Canal_perio_VEF_2D</a>		
XXX			
condition_elements	<a href="#">Extrait_plan</a>	<a href="#">Extraire_domaine</a>	<a href="#">Extraire_domaine_2D</a>
XXX			
condition_faces	<a href="#">Cx</a>	<a href="#">Extrait_plan</a>	<a href="#">Extraire_domaine</a>
XXX			
condition_geometrique	<a href="#">DecoupBord_pour_rayonnement</a>		
XXXinitial_conditions			
conditions_initiales	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
boundary_conditions	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
conditions_limites	<a href="#">Collecteur</a>	<a href="#">PETSC_OPENMP</a>	<a href="#">resume_last_time</a>
conduction	<a href="#">RK2</a>	<a href="#">RK3</a>	<a href="#">RK4</a>
XXXconductivity			
conductivite	<a href="#">Phys_var</a>	<a href="#">Boussinesq</a>	<a href="#">ETD_VDF_mono_var</a>
XXX			
connexion_approchee	<a href="#">Test_recycl_lecture</a>	<a href="#">OBI_diffuser_VEF_k_eps_jdd1</a>	<a href="#">OBI_diffuser_VEF_k_eps_jdd2</a>
XXX			
connexion_exacte	<a href="#">Chmoy_faceperio</a>		
XXXkinetic_energy_conservation			
conservation_ec	<a href="#">Traitement_Particulier_THI_VEF</a>		
XXXmass_conservation			
conservation_masse	<a href="#">Wale_Prdt_Dyn</a>	<a href="#">QC_centre4_VDF</a>	<a href="#">QC_verifP_jdd1</a>
constant	<a href="#">Paroi_VEF_3D</a>	<a href="#">Bilans_VEF_QC</a>	<a href="#">Quasi_Comp_3D</a>
XXX			
constante_cinetique			
XXX			
constante_cinetique_nu_t			
XXX			
constante_taux_reaction	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>	
XXXconstituent			
constituant	<a href="#">Hyd_C_RK3</a>	<a href="#">diagonale</a>	<a href="#">Boussinesq</a>
XXX			
contre_reaction	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>	
XXX			
controle_residu	<a href="#">Impinging_jet</a>	<a href="#">Quasi_Comp_Coupl_keps_VEF_impl</a>	<a href="#">Quasi_Comp_Coupl_Sous_Maille_VEF_impl</a>
XXX			
contribution_one_way	<a href="#">ETD_Colonne_VDF_3D_Couplage</a>	<a href="#">ETD_Colonne_VEF_3D_Couplage</a>	<a href="#">ETD_particles_coupling_jdd5</a>
convection	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
XXXconvection_diffusion_heat_qc			

convection_diffusion_chaleur_qc	<a href="#">DarcyFlow_jdd2</a>	<a href="#">DarcyFlow_jdd4</a>	<a href="#">QC_verifP_jdd1</a>
XXXconvection_diffusion_heat_turbulent_qc			
convection_diffusion_chaleur_turbulent_qc	<a href="#">Paroi_VEF_3D</a>	<a href="#">Bilans_VEF_QC</a>	<a href="#">Quasi_Comp_3D</a>
convection_diffusion_concentration	<a href="#">Hyd_C_RK3</a>	<a href="#">diagonale</a>	<a href="#">Boussinesq</a>
convection_diffusion_concentration_ft_disc	<a href="#">FTD_vef_3d_ibc_interf</a>		
convection_diffusion_concentration_turbulent	<a href="#">CoefDiffNul</a>	<a href="#">Hyd_C_keps_2D</a>	<a href="#">ThHyd_C_K_Eps</a>
XXXconvection_diffusion_mass_fraction_qc			
convection_diffusion_fraction_massique_qc	<a href="#">Quasi_Comp_Cond_GP_VDF_FM</a>	<a href="#">Quasi_Comp_Obst_GP_VDF_FM</a>	
XXXconvection_diffusion_mass_fraction_turbulent_qc			
convection_diffusion_fraction_massique_turbulent_qc	<a href="#">Quasi_Comp_Cond_GP_VDF_Turb_FM</a>		
convection_diffusion_phase_field	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
convection_diffusion_temperature	<a href="#">Cx</a>	<a href="#">Debog</a>	<a href="#">EF_2D</a>
convection_diffusion_temperature_ft_disc	<a href="#">FTD_Boiling_bubble</a>	<a href="#">FTD_Couplage_champ_cl_VDF</a>	
convection_diffusion_temperature_turbulent	<a href="#">cpu_3D</a>	<a href="#">EF_stab</a>	<a href="#">Bilans_VEF</a>
XXX			
contribution_one_way	<a href="#">FTD_Colonne_VDF_3D_Couplage</a>	<a href="#">FTD_Colonne_VEF_3D_Couplage</a>	<a href="#">FTD_particles_coupling_jdd5</a>
XXXcoriolis_only			
coriolis_seul			
XXX			
correction_parcours_thomas	<a href="#">FTD_remail_thomas_vdf</a>		
XXX			
correction_visco_turb_pour_controle_pas_de_temps	<a href="#">ThHyd_C_K_Eps_VEF</a>	<a href="#">ThHyd_C_SsMaille_Smago_VEF</a>	
XXX			
correction_visco_turb_pour_controle_pas_de_temps_parametre	<a href="#">ThHyd_C_K_Eps</a>	<a href="#">ThHyd_C_SsMaille_Smago_VDF</a>	
correlation	<a href="#">VAHL_DAVIS</a>	<a href="#">docond_VEF</a>	<a href="#">stat_reprise</a>
XXXtemperature_velocity_correlation			
correlation_temperature_vitesse	<a href="#">les_Re395Pr071_T0Q_jdd5</a>	<a href="#">les_Re395Pr0025_T0Q_jdd5</a>	
XXXvelocity_velocity_correlation			
correlation_vitesse_vitesse			
XXXfix_periodic_boundary			
corriger_frontiere_periodique	<a href="#">3D_P0</a>	<a href="#">3D_P1</a>	<a href="#">Tuyau</a>
XXXfix_partition			
corriger_partition			
XXX			
corr_visco_turb	<a href="#">ThHyd_C_K_Eps</a>	<a href="#">ThHyd_C_SsMaille_Smago_VDF</a>	<a href="#">ThHyd_C_SsMaille_Smago_VEF</a>
XXX			
cotes	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">Tuyau</a>
XXX			
couplage_ns_ch	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
XXX			
courant_maille	<a href="#">Cell_numbers_VDF</a>		
XXX			
courbure	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">Cell_numbers_VDF</a>	<a href="#">ftd_gravite_jdd1</a>

XXX			
couronne	<a href="#">Kernel Sous_zone</a>	<a href="#">Symetrie Implicite</a>	
XXX			
cp	<a href="#">Cx</a>	<a href="#">RK2</a>	<a href="#">RK3</a>
crank	<a href="#">Adams Bashforth</a>	<a href="#">ibc_refroidi_jdd1</a>	<a href="#">ibc_refroidi_jdd2</a>
XXXcreate_domain_from_subzone			
create_domain_from_sous_zone	<a href="#">Kernel Create domain from sous_zone</a>		
XXXedge_criteria			
critere_arete	<a href="#">FTD Tgrid</a>	<a href="#">Bulle oscillante</a>	<a href="#">Cell numbers_VDF</a>
XXX			
critere_longueur_fixe	<a href="#">FTD Chute Goutte 2D</a>	<a href="#">FTD VEF_parallel_ok</a>	<a href="#">Quasi_Comp_IBC_VEF_2D</a>
XXX			
critere_q	<a href="#">Marche_incline</a>	<a href="#">Champ_Front_Vortex</a>	<a href="#">Marche_incline_jdd1</a>
XXXremeshing_criteria			
critere_remaillage	<a href="#">FTD Tgrid</a>	<a href="#">Bulle oscillante</a>	<a href="#">Cell numbers_VDF</a>
XXX			
cs	<a href="#">smago_VDF</a>	<a href="#">Test_tparoi_jdd1</a>	<a href="#">Test_tparoi_jdd2</a>
XXXflow_rate			
debit	<a href="#">VAHL_DAVIS</a>	<a href="#">VAHL_DAVIS_VEF</a>	<a href="#">debit_impose_jdd2</a>
XXXimposed_flow_rate			
debit_impose	<a href="#">Source_canal_perio_jdd2</a>	<a href="#">Source_canal_perio_jdd3</a>	<a href="#">Source_canal_perio_jdd4</a>
XXXtotal_flow_rate			
debit_total	<a href="#">Extrait_plan</a>		
XXXdebug			
debog	<a href="#">2D_P1</a>	<a href="#">Debog</a>	<a href="#">2Cubes</a>
XXX			
decouper_bord_coincident	<a href="#">Decouper_bord_coincident</a>		
XXXpartition_boundary_for_radiation			
decoupebord_pour_rayonnement	<a href="#">geom2ansys</a>	<a href="#">Test_Radiation_dec</a>	
partition	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
decouper	<a href="#">Collecteur</a>	<a href="#">PETSC_OPENMP</a>	<a href="#">resume_last_time</a>
XXXdefault_bar			
default_bar	<a href="#">Tuyau</a>	<a href="#">THI_VEF</a>	<a href="#">Pb_couples</a>
default_phase	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>	<a href="#">Forces_IBC_3D_VDF</a>
XXXdefault			
defaut	<a href="#">Poreps</a>	<a href="#">Chp_Morc</a>	<a href="#">Polynomes</a>
XXXfields_definition			
definition_champs	<a href="#">Cx</a>	<a href="#">muscl</a>	<a href="#">Sondes</a>
delta	<a href="#">Turbul_LES_Robin_wall_law</a>	<a href="#">Turbul_RANS_Robin_wall_law</a>	<a href="#">Fiche_validation_Re590_jdd3</a>
XXX			
delta_spot			
XXX			
demie-largeur	<a href="#">Moyenne_volumique_2d</a>	<a href="#">Moyenne_volumique_3d</a>	<a href="#">Moyenne_vol_quadra_3d</a>
XXX			
densite_particules	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VDF_3D</a>	<a href="#">FTD_Colonne_VEF_2D</a>
XXX			

<b>derivee_rotation</b>	<a href="#">Forces_IBC_2D_VEF</a>		
<b>XXX</b>			
<b>dh</b>	<a href="#">CanalColburnVEFRayo</a>		
<b>diag</b>	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>	<a href="#">Def_VEF_impl</a>
<b>XXX</b>			
<b>diam_hydr</b>	<a href="#">Perte_Charge_VEF</a>	<a href="#">Abort_timestep_jdd1</a>	<a href="#">Abort_timestep_jdd2</a>
<b>XXX</b>			
<b>diam_hydr_ortho</b>	<a href="#">Perte_Charge_Circulaire_QC_VEF</a>	<a href="#">Perte_Charge_Circulaire_VEF_jdd1</a>	<a href="#">Perte_Charge_Circulaire_VEF_jdd2</a>
<b>XXXdiameter</b>			
<b>diametre</b>	<a href="#">DarcyFlow_jdd1</a>	<a href="#">DarcyFlow_jdd2</a>	<a href="#">DarcyFlow_jdd3</a>
<b>XXXminimal_diameter</b>			
<b>diametre_min</b>	<a href="#">FTD_Transfo_bulles_VDF_3D</a>	<a href="#">FTD_Transfo_bulles_VEF_3D</a>	
<b>diffusion</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
<b>XXXimplicit_diffusion</b>			
<b>diffusion_implicite</b>	<a href="#">DI_L2</a>	<a href="#">Parallele</a>	<a href="#">poise_VEF</a>
<b>XXXthermal_diffusivity</b>			
<b>diffusivite_thermique</b>	<a href="#">Phys_var</a>	<a href="#">Champ_fonc_fonction</a>	
<b>XXXdilatability</b>			
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<b>dimension</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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<b>direction</b>	<a href="#">ExtrudeParoi</a>	<a href="#">Perte_Charge_VEF</a>	<a href="#">Canal_perio_incline_VEF</a>
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<b>XXX</b>			
<b>direction_ecoulement</b>	<a href="#">Loi_paro2D_VEF_jdd1</a>	<a href="#">Loi_paro2D_VEF_jdd2</a>	<a href="#">Loi_paro2D_VEF_jdd3</a>
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<b>discretize</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
<b>discretiser</b>	<a href="#">Collecteur</a>	<a href="#">PETSC_OPENMP</a>	<a href="#">resume_last_time</a>
<b>XXXdiscretize_domain</b>			
<b>discretiser_domaine</b>	<a href="#">Kernel_Sous_zone</a>	<a href="#">Kernel_remove_invalid_internal_boundary</a>	
<b>XXX</b>			
<b>distance_interface_element_max</b>	<a href="#">FTD_sloshing_jdd1</a>	<a href="#">FTD_remaillage_vdf</a>	<a href="#">FTD_remaillage_vef</a>
<b>XXX</b>			
<b>distance_paro</b>	<a href="#">Distance_paro</a>	<a href="#">Canal_VEF_2D_LongMelange_Va</a> <a href="#">nDriest</a>	
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<b>distance_plan</b>	<a href="#">Test_recycl_fluct</a>	<a href="#">jones_laundry_VDF</a>	<a href="#">laundry_sharma_VDF</a>

distribution	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VDF_3D</a>	<a href="#">FTD_Colonne_VEF_2D</a>
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divergence	<a href="#">ChFront(TXYZ_VEFPrePIB</a>		
XXX			
divergence_u	<a href="#">2DPimp0X</a>	<a href="#">3DPimp0X</a>	<a href="#">2D_P1NCP1P0Pa</a>
XXX			
divrhout_moins_tdivrhout	<a href="#">test_conservation_energie_QC_jdd3</a>	<a href="#">test_conservation_energie_QC_jdd6</a>	
XXX			
divut_moins_tdivu	<a href="#">test_conservation_energie_QC_jdd2</a>	<a href="#">test_conservation_energie_QC_jdd5</a>	
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dmax	<a href="#">Distance_paro</a>	<a href="#">Canal_VEF_2D_LongMelange_Va</a> <a href="#">nDriest</a>	
domain	<a href="#">Tuyau</a>	<a href="#">Build_1_domains_from_3</a>	<a href="#">CouplageFluide_Pb1Pb2_VEF_C</a> <a href="#">N</a>
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domaine	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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domaine_final	<a href="#">Canal_perio_incline_VEF</a>		
XXX			
domaine_grossier	<a href="#">geom2ansys</a>		
XXX			
domaine_init	<a href="#">Canal_perio_incline_VEF</a>		
XXX			
domegadt	<a href="#">Cylindre_tournant</a>	<a href="#">Repere_Rotation_VEF</a>	<a href="#">Repere_Rotation_Variable</a>
dt_calc	<a href="#">2D_P0</a>	<a href="#">2D_P1</a>	<a href="#">3D_P0</a>
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dt_fixe	<a href="#">Collecteur</a>	<a href="#">Blocage_Post</a>	<a href="#">Cell_numbers_VDF</a>
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dt_impr	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
XXX			
dt_impr_nusselt	<a href="#">Impinging_jet</a>	<a href="#">ThHyd_C_K_Eps</a>	<a href="#">ThHyd_C_K_Eps_VEF</a>
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dt_impr_ustar	<a href="#">Tuyau</a>	<a href="#">Marche</a>	<a href="#">SGE_3D_VDF</a>
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dt_injection	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VEF_2D</a>	
XXX			
dt_max	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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dt_min	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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dt_post	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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dt_sauv	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>

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dt_start	<a href="#">2D_P0</a>	<a href="#">2D_P1</a>	<a href="#">3D_P0</a>
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dt_transfo	<a href="#">FTD_Transfo_bulles_VDF_3D</a>		
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ec	<a href="#">THI</a>	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>
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ec_dans_repere_fixe	<a href="#">Cylindre_tournant</a>	<a href="#">Repere_Rotation_VEF</a>	
XXXstandard_deviation			
ecart_type	<a href="#">Sondes</a>	<a href="#">Sondes_chsom</a>	<a href="#">stat_reprise</a>
XXXpressure_standard_deviation			
ecart_type_pression	<a href="#">Obstacle</a>	<a href="#">Obstacle_reprise</a>	
XXXtemperature_standard_deviation			
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XXX			
echange_contact_rayo_transp_vdf			
XXXwrite			
ecrire	<a href="#">RK2</a>	<a href="#">gradp</a>	<a href="#">Kernel</a>
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ecrire_champ_med	<a href="#">Kernel_ecrire_champ_med</a>		
XXXwrite_partition			
ecrire_decoupage	<a href="#">Cx</a>	<a href="#">THI</a>	<a href="#">Post_Eclate</a>
XXXwrite_file			
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XXXwrite_binary_file			
ecrire_fichier_bin	<a href="#">Moyenne_convergee</a>	<a href="#">ThHyd_Coupl_Laminaire</a>	
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ecrire_fichier_formatte	<a href="#">ThHyd_Coupl_Laminaire</a>	<a href="#">Canal_perio_incline_VEF</a>	
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ecrire_fichier_xyz_valeur	<a href="#">ThHyd_keps_VEF</a>	<a href="#">ChFrontLu_gen_file</a>	<a href="#">ThHyd_keps_VEF_perio</a>
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ecrire_fichier_xyz_valeur_bin			
XXXwrite_boundary			
ecrire_frontiere	<a href="#">Kernel_remove_invalid_internal_boundary</a>		
XXXwrite_lata			
ecrire_lata			
XXXwrite_med			
ecrire_med	<a href="#">MED_docond</a>		
XXXwrite_file_xyz			
ecriturelecturespecial	<a href="#">cpu_3D</a>	<a href="#">keps_3D_VEF</a>	<a href="#">Paroi_rugueuse</a>
ef	<a href="#">EF_2D</a>	<a href="#">Tuyau</a>	<a href="#">THI_VEF</a>
ef_stab	<a href="#">2Tri</a>	<a href="#">2Cubes</a>	<a href="#">4Cubes</a>
eisenstat			
XXX			



<b>elem</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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<b>emissivite</b>	<a href="#">Quasi_Comp_VD_GP_VDF_P1</a>	<a href="#">Quasi_Comp_VD_GP_VEF_P1</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_P1</a>
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<b>epsilon</b>	<a href="#">Tuyau</a>	<a href="#">PETSC_GCP_SPAL_P0P1Pa</a>	<a href="#">CouplageFluide_Pb1Pb2_VEF_CN</a>
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<b>equations_concentration_source_vortex</b>			
<b>equation_interface</b>	<a href="#">FTD_vef_3d_ibc_interf</a>		
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<b>equation_interfaces_proprietes_fluide</b>	<a href="#">FTD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">ftd_gravite_jdd1</a>
<b>XXXequation_interfaces_imposed_velocity</b>			
<b>equation_interfaces_vitesse_imposee</b>	<a href="#">IBC_penalisation_poiseuille_jdd1</a>	<a href="#">IBC_penalisation_poiseuille_jdd2</a>	
<b>XXXequations_interfaces_imposed_velocity</b>			
<b>equations_interfaces_vitesse_imposee</b>	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>	<a href="#">Cell_numbers_VDF</a>
<b>equation_navier_stokes</b>	<a href="#">FTD_Boiling_bubble</a>	<a href="#">FTD_Couplage_champ_cl_VDF</a>	
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<b>XXX</b>			
<b>equation_frequence_resolue</b>	<a href="#">VAHL_DAVIS_impl</a>		
<b>XXXequations_passive_scalars</b>			
<b>equations_scalaires_passifs</b>	<a href="#">Scalaires_passifs</a>	<a href="#">Quasi_Comp_IBC_VDF_2D</a>	<a href="#">Quasi_Comp_IBC_VEF_2D</a>
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<b>equations_source_chimie</b>			
<b>XXXrugosity</b>			
<b>erugu</b>	<a href="#">Marche</a>	<a href="#">Paroi_rugueuse</a>	<a href="#">ThHyd_keps_VEF</a>
<b>XXXspecie</b>			
<b>espece</b>	<a href="#">Quasi_Comp_Cond_GP_VDF_FM</a>	<a href="#">Quasi_Comp_Obst_GP_VDF_FM</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_Turb_FM</a>
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<b>execute_parallel</b>	<a href="#">Execute_parallel</a>	<a href="#">Execute_parallel_without_Petse</a>	
<b>export</b>	<a href="#">SGE_3D_VDF</a>	<a href="#">SGE_3D_VEF</a>	<a href="#">croix_3D_VDF</a>
<b>expression</b>	<a href="#">upwind</a>	<a href="#">VAHL_DAVIS</a>	<a href="#">CoefDiffNul</a>
<b>extraction</b>	<a href="#">Cx</a>	<a href="#">Inward_field_jdd1</a>	<a href="#">Inward_field_jdd2</a>
<b>extract_2d_from_3d</b>	<a href="#">Extract_2D_from_3D</a>	<a href="#">Extract_2D_from_3D_VEF</a>	<a href="#">Heated_floor_k_eps_jdd1</a>
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<b>XXXextract_plane</b>			
<b>extraire_plan</b>	<a href="#">Extrait_plan</a>	<a href="#">ThHyd_3D_VEFPrePIB</a>	
<b>XXXextract_surface</b>			
<b>extraire_surface</b>	<a href="#">Cx</a>	<a href="#">Collecteur</a>	<a href="#">VAHL_DAVIS</a>
<b>XXXextrude_boundary</b>			
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<b>XXXextrude_wall</b>			
<b>extrudeparoi</b>	<a href="#">ExtrudeParoi</a>		
<b>XXXextrude_in3</b>			
<b>extruder_en3</b>	<a href="#">Extruder_en3</a>	<a href="#">Extract_2D_from_3D</a>	<a href="#">Kernel_Extrusion_en3</a>
<b>XXXextrude_in20</b>			
<b>extruder_en20</b>	<a href="#">Kernel_Extrusion_en20</a>		
<b>XXXextrude</b>			
<b>extruder</b>	<a href="#">Kernel_Extrusion</a>	<a href="#">Kernel_ExtrudeBord</a>	
<b>XXX</b>			
<b>facsec</b>	<a href="#">RK2</a>	<a href="#">RK3</a>	<a href="#">RK4</a>
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<b>XXX</b>			
<b>faces</b>	<a href="#">2D_P1</a>	<a href="#">Debog</a>	<a href="#">2Cubes</a>
<b>XXXideal_length_factor</b>			
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<b>XXXfile</b>			
<b>fichier</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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<b>fichier_decoupage</b>	<a href="#">THI</a>		
<b>XXXfile_write_k_eps</b>			
<b>fichier_ecriture_k_eps</b>			
<b>XXXfile_radiation_faces</b>			
<b>fichier_face_rayo</b>	<a href="#">Radiation_jdd2</a>	<a href="#">Radiation_jdd4</a>	<a href="#">Radiation_jdd5</a>
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<b>fichier_geom</b>	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>	<a href="#">Forces_IBC_3D_VDF</a>
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<b>fichier_post</b>			
<b>XXXfile_solver</b>			
<b>fichier_solveur</b>	<a href="#">Test_solveur_non_sym</a>		
<b>XXXfile_output</b>			
<b>fichier_sortie</b>	<a href="#">Extrait_plan</a>		
<b>XXXfiles</b>			
<b>fichiers_multiples</b>			
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<b>file_coord_y</b>			
<b>file_coord_z</b>			
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<b>fin</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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<b>fluctu_temperature_ext</b>	<a href="#">Nagano_WBasRe</a>		
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<b>fluide_diphastique</b>	<a href="#">FTD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">ftd_gravite_jdd1</a>
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<b>fluide_quasi_compressible</b>	<a href="#">Paroi_VEF_3D</a>	<a href="#">Bilans_VEF_OC</a>	<a href="#">Quasi_Comp_3D</a>
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<b>flux_bords</b>	<a href="#">Cx</a>	<a href="#">smago_VDF</a>	<a href="#">smago_VEF</a>
<b>XXXexternal_turbulent_heat_flux</b>			
<b>flux_chaleur_turb_ext</b>			
<b>XXXturbulent_heat_flux</b>			
<b>flux_chaleur_turbulente</b>			
<b>XXXradiation_flux_vdf</b>			
<b>flux_radiatif_vdf</b>	<a href="#">Quasi_Comp_VD_GP_VDF_P1</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_P1</a>	<a href="#">Quasi_Comp_Obst_GP_VDF_P1</a>

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f_m_ext			
XXX			
fonction_distance	<a href="#">FTD_VDF_RK3</a>		
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fonction_filtre	<a href="#">Moyenne_volumique_2d</a>	<a href="#">Moyenne_volumique_3d</a>	<a href="#">Moyenne_vol_quadra_3d</a>
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fonction_sous_zone	<a href="#">Kernel_Sous_zone</a>	<a href="#">PorousWithPloss_VEF_jdd4</a>	
XXX			
fonction	<a href="#">FTD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">Cell_numbers_VDF</a>
XXX			
formule	<a href="#">VAHL_DAVIS</a>	<a href="#">CoefDiffNul</a>	<a href="#">Poiseuille_VEF</a>
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format_post	<a href="#">Moyenne_volumique_2d</a>	<a href="#">Moyenne_volumique_3d</a>	<a href="#">Moyenne_vol_quadra_3d</a>
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formatte	<a href="#">Debog</a>	<a href="#">Sonde</a>	<a href="#">docond</a>
XXXmass_fraction0			
fraction_massique0	<a href="#">Quasi_Comp_Cond_GP_VDF_FM</a>	<a href="#">Quasi_Comp_Obst_GP_VDF_FM</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_Turb_FM</a>
XXXmass_fraction1			
fraction_massique1	<a href="#">Quasi_Comp_Obst_GP_VDF_FM</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_Turb_FM</a>	
XXXmass_fraction			
fraction_massique			
XXXopen_boundary_imposed_concentration			
frontiere_ouverte_concentration_imposee	<a href="#">Hyd_C_RK3</a>	<a href="#">diagonale</a>	<a href="#">Boussinesq</a>
XXXopen_boundary_imposed_thermal_fluctuation			
frontiere_ouverte_fluctu_temperature_imposee	<a href="#">Nagano_WBasRe</a>		
XXXopen_boundary_imposed_turbulent_heat_flux			
frontiere_ouverte_flux_chaleur_turbulente_imposee			
XXXopen_boundary_imposed_mass_fraction			
frontiere_ouverte_fraction_massique_imposee	<a href="#">Quasi_Comp_Cond_GP_VDF_FM</a>	<a href="#">Quasi_Comp_Obst_GP_VDF_FM</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_Turb_FM</a>
XXXopen_boundary			
frontiere_ouverte	<a href="#">Cl_var</a>	<a href="#">Marche</a>	<a href="#">Sondes</a>
XXXopen_boundary_imposed_pressure_gradient			
frontiere_ouverte_gradient_pression_imposee	<a href="#">gradp</a>	<a href="#">docond_3D</a>	<a href="#">Nagano_WBasRe</a>
XXXopen_boundary_imposed_k_eps			
frontiere_ouverte_k_eps_imposee	<a href="#">Marche</a>	<a href="#">Pb_couples</a>	<a href="#">keps_1D_VEF</a>
XXXopen_boundary_imposed_pressure			
frontiere_ouverte_pression_imposee	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
XXXopen_boundary_XXX			
frontiere_ouverte_rayo_transp	<a href="#">Rayonnement_VDF</a>	<a href="#">Rayonnement_VEF</a>	<a href="#">Rayonnement_VDF_croix</a>

XXXopen_boundary_imposed_momentum			
frontiere_ouverte_rho_u_impose	<a href="#">QC_d_rho_dt_jdd3</a>	<a href="#">QC_d_rho_dt_jdd4</a>	<a href="#">Abort_timestep_jdd1</a>
XXXopen_boundary_imposed_temperature			
frontiere_ouverte_temperature_imposee	<a href="#">Cx</a>	<a href="#">Debog</a>	<a href="#">Cl_var</a>
XXXopen_boundary_imposed_velocity			
frontiere_ouverte_vitesse_imposee	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
XXXopen_boundary_imposed_vortex_velocity			
frontiere_ouverte_vitesse_vortex			
function_coord_x			
function_coord_y	<a href="#">MaillerParallel</a>		
function_coord_z	<a href="#">MaillerParallel</a>		
gamma	<a href="#">Paroi_VEF_3D</a>	<a href="#">Bilans_VEF_QC</a>	<a href="#">Quasi_Comp_3D</a>
XXX			
gaussienne			
XXXperfect_gas			
gaz_parfait	<a href="#">Paroi_VEF_3D</a>	<a href="#">Bilans_VEF_QC</a>	<a href="#">Quasi_Comp_3D</a>
XXXreal_gas			
gaz_reel			
XXXpreconditioned_conjugate_gradient			
gcp	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">THI</a>
gen	<a href="#">Collecteur</a>	<a href="#">QC_VDF_diff_impl</a>	<a href="#">QC_VEF_diff_impl</a>
generic	<a href="#">muscl</a>	<a href="#">VAHL_DAVIS_VEF</a>	<a href="#">ChDonFoncxyzVEF</a>
ghost_thickness	<a href="#">MaillerParallel</a>		
gmres	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>	<a href="#">Impinging_jet</a>
XXXnon_linear_gmres			
gmres_non_lineaire	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
grad_i	<a href="#">FTD_hanging_drop_jdd1</a>	<a href="#">FTD_hanging_drop_jdd2</a>	
gradient	<a href="#">muscl</a>	<a href="#">coude_irreg</a>	<a href="#">docond_VEF_3D</a>
XXXpressure_gradient			
gradient_pression	<a href="#">upwind</a>	<a href="#">2DPimp0X</a>	<a href="#">3DPimp0X</a>
XXXtemperature_gradient			
gradient_temperature	<a href="#">VAHL_DAVIS_VEF</a>	<a href="#">gradient_temperature</a>	
XXX			
grad_ubar	<a href="#">PETSC_Canal_VEF_2D_LongMelange</a>		
XXX			
grav	<a href="#">Sondes</a>	<a href="#">coude_irreg</a>	<a href="#">DarcyFlow_jdd1</a>
XXXgravity			
gravite	<a href="#">Coup</a>	<a href="#">Debog</a>	<a href="#">EF_2D</a>
XXXgroups			
groupes	<a href="#">CouplageFluide_Pb1Pb2_VEF_CN_perio</a>		
XXXheight			
hauteur	<a href="#">Sous_zone_VDF</a>	<a href="#">FTD_VDF_mono_var</a>	
XXX			
h_echange_tref			
XXXimposed_heat_exchange			
h_imp	<a href="#">conduc</a>	<a href="#">Himp_var</a>	<a href="#">Collecteur</a>

XXX			
homogene	<a href="#">Coup</a>	<a href="#">Debog</a>	<a href="#">docond</a>
ibicgstab			
ilu	<a href="#">Collecteur</a>	<a href="#">QC_VDF_diff_impl</a>	<a href="#">QC_VEF_diff_impl</a>
XXX			
implicitation_ch	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
XXX			
implicite	<a href="#">Collecteur</a>	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>
XXXprint_fluxes			
imprimer_flux	<a href="#">Cx</a>	<a href="#">Debog</a>	<a href="#">docond</a>
XXXprint_fluxes_sum			
imprimer_flux_sum	<a href="#">M3DLAM</a>	<a href="#">VAHL_DAVIS_VEF</a>	
XXX			
impr	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
XXX			
impr_diffusion_implicite	<a href="#">DiffusionImpliciteQdm</a>	<a href="#">diffusion_implicite_jdd9</a>	<a href="#">diffusion_implicite_jdd10</a>
XXX			
indicatrice	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_Chute_Goutte_2D</a>	<a href="#">FTD_VDF_parallel_ok</a>
XXX			
indice	<a href="#">Quasi_Comp_VD_GP_VDF_P1</a>	<a href="#">Quasi_Comp_VD_GP_VEF_P1</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_P1</a>
info			
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init_ec	<a href="#">THI</a>	<a href="#">TP_THI_VDF</a>	<a href="#">SGE_Fst_VDF</a>
initial_partition_type			
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injecteur_interfaces	<a href="#">Injecteur_interfaces</a>	<a href="#">Bullage_Huile_Creuset_Froid_jdd1</a>	<a href="#">Bullage_Huile_Creuset_Froid_jdd2</a>
XXXinjectorXXX			
injection	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VEF_2D</a>	
XXXsum_on_zXXX			
integrale_en_z	<a href="#">Extrait_plan</a>		
integrale_reference			
XXXsum_med_field			
integrer_champ_med	<a href="#">Extrait_plan</a>		
interface	<a href="#">PCS</a>	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>
interfaces	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>
XXXinternamls			
internes	<a href="#">Ellipsoid_vdf_therm</a>	<a href="#">ellipsoid_vdf_therm_jdd1</a>	<a href="#">ellipsoid_vdf_therm_jdd2</a>
interpolation	<a href="#">Cx</a>	<a href="#">muscl</a>	<a href="#">Sondes</a>
XXXface_field_interpolation			
interpolation_champ_face	<a href="#">Cell_numbers_VDF</a>	<a href="#">ibc_refroidi_jdd1</a>	<a href="#">ibc_refroidi_jdd2</a>
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interpolation_repere_local	<a href="#">FTD_instab2D</a>	<a href="#">FTD_Boiling_bubble</a>	<a href="#">Injecteur_interfaces</a>
XXXinterval			
intervalle			
XXX			
inverse_condition_element			

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irradiance	<a href="#">Quasi_Comp_VD_GP_VDF_P1</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_P1</a>	<a href="#">Quasi_Comp_Obst_GP_VDF_P1</a>
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iterations_correction_volume	<a href="#">FTD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">fid_gravite_jdd1</a>
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joints_non_postraites			
jones_launder	<a href="#">docond_BasRe</a>	<a href="#">Nagano_WBasRe</a>	<a href="#">jones_launder_VDF</a>
juric	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_Chute_Goutte_2D</a>	<a href="#">FTD_VDF_parallel_ok</a>
XXX			
juric_local	<a href="#">FTD_instab2D</a>	<a href="#">FTD_Boiling_bubble</a>	<a href="#">Bullage_Huile_Creuset_Froid_jdd1</a>
XXX			
juric_pour_tout	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_Chute_Goutte_2D</a>	<a href="#">FTD_VDF_parallel_ok</a>
kappa	<a href="#">Marche</a>	<a href="#">ThHyd_keps_VEF</a>	<a href="#">PF_RT_boussi_p1</a>
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kappa_variable	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
kmetis	<a href="#">VAHL_DAVIS_VEFPreP1B</a>	<a href="#">Test_2D_VDF_Radiation</a>	
k	<a href="#">Marche</a>	<a href="#">smago_VDF</a>	<a href="#">smago_VEF</a>
k_eps_ext	<a href="#">Marche</a>	<a href="#">Pb_couples</a>	<a href="#">keps_1D_VEF</a>
XXXk_epsilon_low_reynolds			
k_epsilon_bas_reynolds	<a href="#">docond_BasRe</a>	<a href="#">Nagano_WBasRe</a>	<a href="#">jones_launder_VDF</a>
k_epsilon	<a href="#">Marche</a>	<a href="#">Pb_couples</a>	<a href="#">keps_1D_VEF</a>
k_eps	<a href="#">Marche</a>	<a href="#">Pb_couples</a>	<a href="#">keps_1D_VEF</a>
k_min			
kx	<a href="#">PCS</a>	<a href="#">Perte_Charge_Singuliere_VDF</a>	<a href="#">Perte_Charge_Singuliere_VEF</a>
ky			
kz	<a href="#">PCS_med_VEF</a>	<a href="#">Perte_Charge_QC_VEF</a>	
lambda	<a href="#">Cx</a>	<a href="#">RK2</a>	<a href="#">RK3</a>
lambda_min	<a href="#">2D_P0P1_GCP_SSOR_BLOC</a>		
lambda_max	<a href="#">2D_P0P1_GCP_SSOR_BLOC</a>		
lambda_c	<a href="#">LoiParoi_UTAU_Imp_VDF</a>		
lambda_ortho	<a href="#">Perte_Charge_Directionnelle</a>	<a href="#">Perte_Charge_Anisotrope_QC_VE</a>	<a href="#">Perte_Charge_Circulaire_QC_VEF</a>
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larg_joint	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
last_time	<a href="#">Import_MED</a>	<a href="#">P1toP0P1Pa</a>	<a href="#">P1toP1Bulle</a>
lata_dump	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>	<a href="#">Forces_IBC_3D_VDF</a>
lata	<a href="#">Cx</a>	<a href="#">2D_P0</a>	<a href="#">2D_P1</a>
lata_v1	<a href="#">Post_Stat</a>		
lata_v2	<a href="#">Extraire_domaine_2D</a>		
lata_to_med	<a href="#">Extrait_plan</a>		
lata_to_other	<a href="#">Lata_To_other</a>	<a href="#">champ_synonyme</a>	
level	<a href="#">PETSC_cpu_3D_CGILU</a>	<a href="#">ThHyd_keps_VEF_impl</a>	<a href="#">PETSC_GCP_SPAI_P0P1Pa</a>
XXXlinear			
lineaire	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
read	<a href="#">upwind</a>	<a href="#">gradp_VEF</a>	<a href="#">muscl_old</a>
lire	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
read_file_binary	<a href="#">Drag_jdd1</a>	<a href="#">Drag_jdd2</a>	<a href="#">Drag_jdd3</a>

lire_fichier_bin	<a href="#">ftd_gravite_jdd1</a>	<a href="#">Moyenne_convergee</a>	<a href="#">FTD_vef_3d_ibc_interf</a>
read_file	<a href="#">Cx</a>	<a href="#">Sonde</a>	<a href="#">Tuyau</a>
lire_fichier	<a href="#">Collecteur</a>	<a href="#">PETSC_OPENMP</a>	<a href="#">Uniform_keps_front_field_from_u d_jdd1</a>
XXXread_ideas			
lire_ideas	<a href="#">Lire_unv</a>		
XXXread_med			
lire_med	<a href="#">Import_MED</a>	<a href="#">MED_docond</a>	<a href="#">Pb_couples</a>
XXXread_tgrid			
lire_tgrid	<a href="#">FTD_Tgrid</a>	<a href="#">geom2ansys</a>	<a href="#">Impinging_jet</a>
XXX			
lissage_courbure_coeff	<a href="#">FTD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">FTD_Chute_Goutte_2D</a>
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lissage_courbure_iterations	<a href="#">FTD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">FTD_Chute_Goutte_2D</a>
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lissage_courbure_iterations_systematique	<a href="#">FTD_Couplage_champ_cl_VDF</a>		
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lissage_courbure_iterations_si_remaillage	<a href="#">FTD_Couplage_champ_cl_VDF</a>		
XXXlist			
liste	<a href="#">Kernel_Remove_elem</a>		
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liste_cas	<a href="#">Execute_parallel</a>	<a href="#">Execute_parallel_without_Petsc</a>	
XXX			
liste_postraitements	<a href="#">FTD_Tgrid</a>	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>
lml	<a href="#">Cx</a>	<a href="#">2D_P0</a>	<a href="#">2D_P1</a>
local	<a href="#">Coup</a>	<a href="#">Debog</a>	<a href="#">docond</a>
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localisation	<a href="#">Cx</a>	<a href="#">muscl</a>	<a href="#">Sondes</a>
XXXlogarithmic			
logarithmique			
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loi_etat	<a href="#">Paroi_VEF_3D</a>	<a href="#">Bilans_VEF_QC</a>	<a href="#">Quasi_Comp_3D</a>
XXX			
loi_expert_hydr	<a href="#">Marche</a>	<a href="#">ThHyd_keps_VEF</a>	
XXX			
loi_expert_scalaire	<a href="#">ThHyd_keps_VEF</a>	<a href="#">Test_tparoi_jdd3</a>	<a href="#">ThHyd_C_SsMaille_Smago_VDF</a>
XXX			
loi_horaire	<a href="#">Forces_IBC_2D_VEF</a>	<a href="#">Rotation_IBC_2D_VDF</a>	<a href="#">Rotation_IBC_2D_VEF</a>
XXX			
loi_paroι_nu_impose	<a href="#">Paroi_fictif_turbulent_vef</a>	<a href="#">Compare_VDF_Flux_Turb_Nu_I mpose</a>	<a href="#">Compare_VEF_Flux_Turb_Nu_Im pose</a>
XXX			
loi_standard_hydr	<a href="#">THI</a>	<a href="#">Tuyau</a>	<a href="#">cpu_3D</a>
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loi_standard_hydr_3couches			
XXX			
loi_standard_hydr_scalaire	<a href="#">cpu_3D</a>	<a href="#">Bilans_VEF</a>	<a href="#">Nu_var_VEF</a>
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longitudinale	<a href="#">PCR</a>	<a href="#">keps_3D_VEF</a>	<a href="#">Pertes_d_charges_CF_VDF</a>
XXXlength			
longueur	<a href="#">CanalColburnVEFRayo</a>		
XXXbox_length			
longueur_boite	<a href="#">Traitement_Particulier_THI_VEF</a>		
XXX			
longueur_maille	<a href="#">Canal_VEF_3D_SCOTTI</a>	<a href="#">Quasi_Comp_Coupl_Incomp</a>	<a href="#">ThHyd_C_Wale_Scalaires_Passifs_VEFPrePIB</a>
XXXmixing_length			
longueur_melange	<a href="#">Distance_paro</a>	<a href="#">Paroi_rugueuse</a>	<a href="#">TBLE_VDF_3D_scal</a>
XXXlengths			
longueurs	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">RK2</a>
XXXmesh			
maillage	<a href="#">Cas_RZ_Symetrie_Fluide</a>		
mesh	<a href="#">Sonde</a>	<a href="#">upwind</a>	<a href="#">MED_docond</a>
mailler	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">RK2</a>
XXXparallel_meshXXX			
maillerparallel	<a href="#">MaillerParallel</a>		
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maintien_temperature			
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masse_ajoutee	<a href="#">FTD_Flottabilite_VDF_2D</a>	<a href="#">FTD_Flottabilite_VEF_2D</a>	<a href="#">FTD_Inst_Masse_Ajout_VDF_2D</a>
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masse_molaire	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_FM</a>
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masse_volumique	<a href="#">upwind</a>	<a href="#">Bilans_VEF_QC</a>	<a href="#">Quasi_Comp_3D</a>
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match_type			
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matrice_pression_invariante	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>	
max	<a href="#">centre4_VEF</a>	<a href="#">VAHL_DAVIS_VEF</a>	<a href="#">Cell_numbers_VDF</a>
med	<a href="#">Import_MED</a>	<a href="#">MED_docond</a>	<a href="#">Pb_couples</a>
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melange_gaz_parfait	<a href="#">Quasi_Comp_Cond_GP_VDF_FM</a>	<a href="#">Quasi_Comp_Obst_GP_VDF_FM</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_Turb_FM</a>
metis	<a href="#">Cx</a>	<a href="#">RK3</a>	<a href="#">RK4</a>
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methode_couplage	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VDF_3D</a>	<a href="#">FTD_Colonne_VEF_2D</a>
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methode_interpolation_v	<a href="#">FTD_2D_Axi</a>	<a href="#">FTD_VDF_RK3</a>	<a href="#">FTD_Couplage_champ_cl_VDF</a>
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methode_transport	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>
min	<a href="#">centre4_VEF</a>	<a href="#">VAHL_DAVIS_VEF</a>	<a href="#">Cell_numbers_VDF</a>
minmod	<a href="#">Diagonale_Cube_jdd3</a>		
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mode_calcul_convection	<a href="#">test_conservation_energie_QC_jdd</a>	<a href="#">test_conservation_energie_QC_jdd</a>	<a href="#">test_conservation_energie_QC_jdd</a>

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modele_fonc_bas_reynolds	<a href="#">docond_BasRe</a>	<a href="#">Nagano_WBasRe</a>	<a href="#">jones_launder_VDF</a>
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modele_rayonnement_milieu_transparent	<a href="#">geom2ansys</a>	<a href="#">Radiation_jdd1</a>	<a href="#">Radiation_jdd2</a>
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modele_rayo_semi_transp	<a href="#">Quasi_Comp_VD_GP_VDF_P1</a>	<a href="#">Quasi_Comp_VD_GP_VEF_P1</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_P1</a>
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k_epsilon_2_couches	<a href="#">ThHyd_2couches</a>	<a href="#">Cavite_2couches</a>	<a href="#">ThHyd_Coupl_2Couches</a>
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k_epsilon_v2	<a href="#">CanalV2</a>	<a href="#">ObstacleV2</a>	
XXXturbulence_model			
modele_turbulence	<a href="#">THI</a>	<a href="#">Tuyau</a>	<a href="#">Marche</a>
XXXchange_boundary_to_XXX			
modif_bord_to_raccord	<a href="#">Collecteur</a>		
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modif_div_face_dirichlet	<a href="#">VAHL_DAVIS_VEF</a>		
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moins_rho_moyen	<a href="#">Wale_Prdt_Dyn</a>	<a href="#">DarcyFlow_jdd2</a>	<a href="#">DarcyFlow_jdd4</a>
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morceau_equation	<a href="#">Cx</a>	<a href="#">VAHL_DAVIS</a>	<a href="#">VAHL_DAVIS_VEF</a>
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moy_euler	<a href="#">DYN_Moy_Euler</a>		
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moy_lagrange			
XXX			
moyenne_de_kappa	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
XXX			
moyenne	<a href="#">Cx</a>	<a href="#">Cl_var</a>	<a href="#">Sondes</a>
XXX			
moyenne_convergee	<a href="#">Moyenne_convergee</a>		
XXX			
moyenne_imposee	<a href="#">Chmoy_faceperio</a>	<a href="#">Test_recycl_fluct</a>	<a href="#">Couplage_champ_cl_VDF</a>
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moyenne_ponderee	<a href="#">VAHL_DAVIS</a>	<a href="#">Cell_numbers_VDF</a>	<a href="#">Canal_perio_thermique</a>
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moyenne_pression	<a href="#">Obstacle</a>	<a href="#">Obstacle_reprise</a>	
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moyenne_recyclee	<a href="#">Test_recycl_fluct</a>	<a href="#">Couplage_champ_cl_VDF</a>	<a href="#">Couplage_champ_cl_VEF</a>
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moyenne_temperature	<a href="#">VAHL_DAVIS_VEF</a>	<a href="#">Moyenne_convergee</a>	<a href="#">Quasi_Comp_Coupl_Incomp</a>
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moyenne_vitesse	<a href="#">Moyenne_mobile</a>	<a href="#">Cylindre_chauffant</a>	<a href="#">Turbul_LES_Robin_wall_law</a>
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moyenne_volumique	<a href="#">Moyenne_volumique_2d</a>	<a href="#">Moyenne_volumique_3d</a>	<a href="#">Moyenne_vol_quadra_3d</a>
mu0	<a href="#">Paroi_VEF_3D</a>	<a href="#">Quasi_Comp_3D</a>	<a href="#">QC_verifP_jdd10</a>

XXX			
<b>multiplicateur_de_kappa</b>	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
XXXdynamic_viscosity			
<b>mu</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
<b>muscl</b>	<a href="#">Cx</a>	<a href="#">2D_P0</a>	<a href="#">2D_P1</a>
<b>muscl_old</b>	<a href="#">muscl_old</a>		
<b>n</b>	<a href="#">TBLE_VDF_3D</a>	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>
<b>navier_stokes_ft_disc</b>	<a href="#">FTD_Tgrid</a>	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>
<b>navier_stokes_phase_field</b>	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
<b>navier_stokes_qc</b>	<a href="#">DarcyFlow_jdd2</a>	<a href="#">DarcyFlow_jdd4</a>	<a href="#">QC_verifP_jdd1</a>
<b>navier_stokes_standard</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
<b>navier_stokes_turbulent</b>	<a href="#">THI</a>	<a href="#">Tuyau</a>	<a href="#">Marche</a>
<b>navier_stokes_turbulent_qc</b>	<a href="#">Paroi_VEF_3D</a>	<a href="#">Bilans_VEF_QC</a>	<a href="#">Quasi_Comp_3D</a>
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<b>n_iterations_interpolation_ibc</b>	<a href="#">Cell_numbers_VDF</a>	<a href="#">ibc_refroidi_jdd1</a>	<a href="#">ibc_refroidi_jdd2</a>
XXX			
<b>nb_corrections_max</b>	<a href="#">VAHL_DAVIS_impl_jdd11</a>	<a href="#">VAHL_DAVIS_impl_jdd22</a>	
XXX			
<b>nb_iteration_max_uzawa</b>	<a href="#">pena_ellipsoide_jdd1</a>	<a href="#">pena_ellipsoide_jdd2</a>	
XXX			
<b>nb_iterations</b>	<a href="#">FTD_Colonne_VDF_2D</a>		
XXX			
<b>nb_iterations_gmresnl</b>	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
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<b>nb_iter_barycentrage</b>	<a href="#">FTD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">Cell_numbers_VDF</a>
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<b>nb_iter_correction_volume</b>	<a href="#">FTD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">FTD_Chute_Goutte_2D</a>
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<b>nb_iter_remaillage</b>	<a href="#">FTD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">Cell_numbers_VDF</a>
<b>nb_it_max</b>	<a href="#">Impinging_jet</a>	<a href="#">Poreux_VEF_jdd6</a>	<a href="#">ThHyd_C_K_Eps_P0P1Pa</a>
<b>nb_nodes</b>	<a href="#">MaillerParallel</a>		
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<b>nb_particules</b>	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VDF_3D</a>	<a href="#">FTD_Colonne_VEF_2D</a>
<b>nb_parts</b>	<a href="#">Cx</a>	<a href="#">RK3</a>	<a href="#">RK4</a>
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<b>nb_parts_geom</b>	<a href="#">DecoupBord_pour_rayonnement</a>		
XXX			
<b>nb_parts_naif</b>	<a href="#">Test_Radiation_dec</a>		
<b>nb_parts_tot</b>	<a href="#">Pb_couples</a>	<a href="#">docond_anisoproc</a>	<a href="#">Cylindre_chauffant</a>
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<b>nb_pas_dt_max</b>	<a href="#">Cx</a>	<a href="#">THI</a>	<a href="#">2Tri</a>
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<b>nb_pas_dt_post</b>	<a href="#">VAHL_DAVIS</a>	<a href="#">VAHL_DAVIS_VEFPreP1B_impl</a>	
<b>nb_points</b>	<a href="#">DYN_6_points</a>	<a href="#">DYN_Moy_Euler</a>	<a href="#">DYN_plans_parallelles</a>
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<b>nb_points_tests</b>			

XXX			
nb_procs	<a href="#">Execute_parallel</a>	<a href="#">Execute_parallel_without_Petsc</a>	
XXX			
nb_tranches	<a href="#">Canal_perio_incline_VEF</a>		
XXX			
nb_var	<a href="#">Flux_CL_periodique</a>	<a href="#">Combinaison_Canal_ThHyd</a>	
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negligeable	<a href="#">muscl</a>	<a href="#">2DSymX</a>	<a href="#">3DPerio</a>
negligeable_scalaire	<a href="#">EF_stab</a>	<a href="#">CoefDiffNul</a>	<a href="#">DYN_6_points</a>
nettoiepasnoeuds			
new_jacobian			
nodes	<a href="#">Sondes</a>	<a href="#">EF_stab</a>	<a href="#">Impinging_jet</a>
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nom	<a href="#">RK2</a>	<a href="#">Kernel</a>	<a href="#">debit_impose_jdd2</a>
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nom_frontiere	<a href="#">Cx</a>	<a href="#">Inward_field_jdd1</a>	<a href="#">Inward_field_jdd2</a>
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n_iterations_distance	<a href="#">ETD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">ftd_gravite_jdd1</a>
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niter_max_diffusion_implicite	<a href="#">keps_3D_VEF</a>	<a href="#">docond_diff_impl</a>	<a href="#">diffusion_implicite_jdd1</a>
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nom_bord	<a href="#">ExtrudeParoi</a>	<a href="#">Canal_perio_incline_VEF</a>	
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nombre_de_noeuds	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">RK2</a>
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nom_cl_devant	<a href="#">Extruder_en3</a>		
XXX			
nom_cl_derriere	<a href="#">Extruder_en3</a>		
XXXfilename			
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nom_pb_rayonnant	<a href="#">Rayonnement_Cuve_2D</a>		

XXXsource_name			
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noms_champs	<a href="#">Moyenne_volumique_2d</a>	<a href="#">Moyenne_volumique_3d</a>	<a href="#">Moyenne_vol_quadra_3d</a>
XXXnorm			
norme	<a href="#">upwind</a>	<a href="#">docond_VEF_3D</a>	<a href="#">Inward_field_jdd1</a>
XXXl2_norm			
norme_l2	<a href="#">pena_couette_jdd1</a>	<a href="#">pena_couette_jdd2</a>	
not	<a href="#">Th_Axi</a>	<a href="#">CanalV2</a>	<a href="#">Cx_impl</a>
no_check_disk_space	<a href="#">cpu_3D</a>	<a href="#">Collecteur</a>	<a href="#">Turbul_LES_Robin_wall_law</a>
XXXno_momentum			
no_qdm	<a href="#">Radiation_jdd2</a>	<a href="#">Radiation_jdd4</a>	<a href="#">Radiation_jdd5</a>
XXX			
nu	<a href="#">Taux_cisaillement</a>	<a href="#">CanalColburnVEFRayo</a>	<a href="#">PETSC_Canal_VEF_2D_LongMelange</a>
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nu_transp	<a href="#">PETSC_Canal_VEF_2D_LongMelange</a>	<a href="#">VEF_diffusion_P0_turbulent_stab</a>	
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numero	<a href="#">Cx</a>	<a href="#">upwind</a>	<a href="#">VAHL_DAVIS</a>
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numero_elem_sur_maitre	<a href="#">Cx</a>	<a href="#">VAHL_DAVIS</a>	<a href="#">VAHL_DAVIS_VEF</a>
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nut	<a href="#">Taux_cisaillement</a>	<a href="#">PETSC_Canal_VEF_2D_LongMelange</a>	<a href="#">VEF_diffusion_P0_turbulent_stab</a>
XXX			
nu_t	<a href="#">Conduite_lm_prdt_var</a>	<a href="#">Conv_Pipe_InOut_jdd1</a>	<a href="#">Conv_Pipe_InOut_jdd2</a>
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nut_transp	<a href="#">PETSC_Canal_VEF_2D_LongMelange</a>	<a href="#">VEF_diffusion_P0_turbulent_stab</a>	
null			
nusselt	<a href="#">Paroi_fictif_turbulent_vef</a>	<a href="#">Compare_VDF_Flux_Turb_Nu_Impose</a>	<a href="#">Compare_VEF_Flux_Turb_Nu_Impose</a>
nut_max	<a href="#">keps_3D_VEF</a>	<a href="#">ChFrontLu_gen_file</a>	<a href="#">ChFrontLu_read_file</a>
odvm			
omega	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">THI</a>
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omega_relaxation_drho_dt	<a href="#">Quasi_Comp_Obst_GP_VEF</a>		
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one_way_coupling	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VDF_3D</a>	<a href="#">FTD_Colonne_VEF_2D</a>
optimized	<a href="#">QC_centre4_VDF</a>		
option	<a href="#">Cx</a>	<a href="#">VAHL_DAVIS</a>	<a href="#">VAHL_DAVIS_VEF</a>
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XXXoperator_number			
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XXXorigin			
origine	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">RK2</a>

ordering			
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orientefacesbord	<a href="#">Cx</a>	<a href="#">Read_matrix</a>	
p0	<a href="#">2Tri</a>	<a href="#">2D_P0</a>	<a href="#">3D_P0</a>
p1	<a href="#">2Tri</a>	<a href="#">2D_P1</a>	<a href="#">3D_P1</a>
p1ncp1b	<a href="#">OpDiffP1B_mixte_scalaire_explicite_2D</a>	<a href="#">OpDiffP1B_mixte_scalaire_implicite_2D</a>	
pa	<a href="#">2Cubes</a>	<a href="#">4Cubes</a>	<a href="#">3DPerio</a>
XXXequation_parameter			
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parcours_interface	<a href="#">FTD_remail_thomas_vdf</a>		
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parmetis			
XXXwall			
paroi	<a href="#">2Tri</a>	<a href="#">2D_P0</a>	<a href="#">2D_P1</a>
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paroi_adiabatique	<a href="#">RK2</a>	<a href="#">RK3</a>	<a href="#">RK4</a>
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paroi_contact	<a href="#">Debog</a>	<a href="#">docond</a>	<a href="#">sdocond</a>
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paroi_contact_fictif	<a href="#">conduction_couple_jdd1</a>	<a href="#">conduction_couple_jdd2</a>	<a href="#">cond_coup_fictif_vdf_impl</a>
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paroi_decalee_robin	<a href="#">Turbul_LES_Robin_wall_law</a>	<a href="#">Turbul_RANS_Robin_wall_law</a>	<a href="#">Fiche_validation_Re590_jdd3</a>
XXXmoving_wall			
paroi_defilante	<a href="#">defilante</a>	<a href="#">Def_VEF_impl</a>	<a href="#">Reprise_impl</a>
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paroi_echange_contact_correlation_vdf	<a href="#">CanalColburnVDF</a>		
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paroi_echange_contact_correlation_vef	<a href="#">CanalColburnVEFRayo</a>		
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paroi_echange_contact_vdf	<a href="#">Coup</a>	<a href="#">docond_3D</a>	<a href="#">Debog_3D_Pb_couple</a>
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paroi_echange_externe_impose	<a href="#">Collecteur</a>	<a href="#">Tparoi_VDF</a>	<a href="#">Paroi_VEF_3D</a>
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paroi_echange_global_impose	<a href="#">conduc</a>	<a href="#">Himp_var</a>	<a href="#">Tparoi_VDF</a>
XXXwall			
paroi_fixe	<a href="#">Cx</a>	<a href="#">2Tri</a>	<a href="#">sans</a>
XXXimposed_flux_wall			
paroi_flux_impose	<a href="#">conduc</a>	<a href="#">Th_Axi_RZ</a>	<a href="#">Bilans_VEF</a>
XXXwallXXX			
paroi_ft_disc	<a href="#">ETD_Tgrid</a>	<a href="#">ETD_IBC_3D_VEF</a>	<a href="#">ETD_vef_3d_ibc</a>
XXX			

paroi_rugueuse	<a href="#">Paroi_rugueuse</a>		
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paroi_tble	<a href="#">TBLE_VDF_3D</a>	<a href="#">TBLE_VDF_3D_scal</a>	<a href="#">TBLE_VDF_WALE_3D</a>
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paroi_tble_scal	<a href="#">TBLE_VDF_3D_scal</a>	<a href="#">CanalPlan_LM_Th_TBLE_VEF</a>	<a href="#">Channel_ML_Thydr_TBLE_VEF_ReT7200_jdd3</a>
XXXimposed_temperature_wall			
paroi_temperature_imposee	<a href="#">Cx</a>	<a href="#">RK2</a>	<a href="#">RK3</a>
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parser			
partition	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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partitionneur	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
XXXtime_step			
pas_de_temps	<a href="#">conduc_VEF</a>	<a href="#">VAHL_DAVIS_VEF</a>	<a href="#">ThHyd_C_Wale_Scalaires_Passifs_VEFPrePIB</a>
XXXsmoothing_time_step			
pas_lissage	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>
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pas	<a href="#">THI</a>	<a href="#">FTD_Tgrid</a>	<a href="#">docond_VEF_3D</a>
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pave	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">RK2</a>
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pb_champ	<a href="#">Cx</a>	<a href="#">muscl</a>	<a href="#">Sondes</a>
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pb_champ_evaluateur	<a href="#">smago_VDF</a>	<a href="#">smago_VEF</a>	<a href="#">Chmoy_faceperio</a>
pb_conduction	<a href="#">RK2</a>	<a href="#">RK3</a>	<a href="#">RK4</a>
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pb_couple_rayonnement	<a href="#">geom2ansys</a>	<a href="#">Radiation_jdd1</a>	<a href="#">Radiation_jdd2</a>
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pb_couple_rayo_semi_transp	<a href="#">Quasi_Comp_VD_GP_VDF_P1</a>	<a href="#">Quasi_Comp_VD_GP_VEF_P1</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_P1</a>
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pb_hydraulique_concentration	<a href="#">Hyd_C_RK3</a>	<a href="#">diagonale</a>	<a href="#">Constituants</a>
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pb_hydraulique_concentration_scalaires_passifs	<a href="#">Scalaires_passifs</a>	<a href="#">Scalaires_passifs_VEF</a>	
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pb_hydraulique_concentration_turbulent	<a href="#">CoefDiffNul</a>	<a href="#">Hyd_C_keps_2D</a>	<a href="#">Hyd_C_VDF_Smago</a>
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pb_hydraulique_concentration_turbulent_scalaires_passifs			
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pb_hydraulique	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">2Tri</a>
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pb_hydraulique_turbulent	<a href="#">THI</a>	<a href="#">Tuyau</a>	<a href="#">Marche</a>
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pb_phase_field	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
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<b>pb_thermohydraulique_concentration</b>	<a href="#">Boussinesq</a>	<a href="#">Sondes_chsom</a>	<a href="#">Champ_fonc_fonction</a>
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<b>pb_thermohydraulique_concentration_scalaires_passifs</b>			
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<b>pb_thermohydraulique_concentration_turbulent</b>	<a href="#">ThHyd_C_K_Eps</a>	<a href="#">ThHyd_C_K_Eps_VEF</a>	<a href="#">ThHyd_C_SsMaille_Smago_VDF</a>
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<b>pb_thermohydraulique_concentration_turbulent_scalaires_passifs</b>	<a href="#">ThHyd_C_Wale_Scalaires_Passifs_VEFPreP1B</a>		
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<b>pb_thermohydraulique</b>	<a href="#">Cx</a>	<a href="#">Debog</a>	<a href="#">EF_2D</a>
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<b>pb_thermohydraulique_qc_fraction_massique</b>	<a href="#">Quasi_Comp_IBC_VDF_2D</a>	<a href="#">Quasi_Comp_IBC_VEF_2D</a>	<a href="#">Quasi_Comp_IBC_VEF_3D</a>
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<b>pb_thermohydraulique_qc</b>	<a href="#">DarcyFlow_jdd2</a>	<a href="#">DarcyFlow_jdd4</a>	<a href="#">QC_verifP_jdd1</a>
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<b>pb_thermohydraulique_scalaires_passifs</b>			
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<b>pb_thermohydraulique_turbulent</b>	<a href="#">cpu_3D</a>	<a href="#">EF_stab</a>	<a href="#">Bilans_VEF</a>
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<b>pb_thermohydraulique_turbulent_qc_fraction_massique</b>	<a href="#">Quasi_Comp_Cond_GP_VDF_Turb_FM</a>		
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<b>pb_thermohydraulique_turbulent_qc</b>	<a href="#">Paroi_VEF_3D</a>	<a href="#">Bilans_VEF_QC</a>	<a href="#">Quasi_Comp_3D</a>
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<b>pb_thermohydraulique_turbulent_scalaires_passifs</b>			
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<b>penalisation_forcage</b>	<a href="#">Cell_numbers_VDF</a>	<a href="#">ibc_refroidi_jdd1</a>	<a href="#">ibc_refroidi_jdd2</a>
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<b>penalisation_l2_ftd</b>			
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<b>perio_y</b>			
<b>perio_z</b>	<a href="#">MaillerParallel</a>		
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<b>periode</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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XXX			
<b>periode_sauvegarde_securite_en_heures</b>	<a href="#">Cx</a>	<a href="#">ThHyd_C_K_Eps_P0P1Pa</a>	<a href="#">Turbul_LES_Robin_wall_law</a>
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<b>perte_charge_anisotrope</b>	<a href="#">Perte_Charge_Directionnelle</a>	<a href="#">Perte_Charge_Anisotrope_QC_VEF</a>	<a href="#">Perte_Charge_Circulaire_VEF_jdd1</a>
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<b>perte_charge_circulaire</b>	<a href="#">Perte_Charge_Circulaire_QC_VEF</a>	<a href="#">Perte_Charge_Circulaire_VEF_jdd1</a>	<a href="#">Perte_Charge_Circulaire_VEF_jdd2</a>



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perte_charge_directionnelle	<a href="#">Perte_Charge_VEF</a>	<a href="#">PorousWithPLOSS_VEF_jdd1</a>	<a href="#">PorousWithPLOSS_VEF_jdd2</a>
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perte_charge_isotrope	<a href="#">Abort_timestep_jdd1</a>	<a href="#">Abort_timestep_jdd2</a>	<a href="#">Perte_Charge_Directionnelle</a>
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perte_charge_reguliere	<a href="#">PCR</a>	<a href="#">keps_3D_VEF</a>	<a href="#">Pertes_d_charges_CF_VDF</a>
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perte_charge_singuliere	<a href="#">PCS</a>	<a href="#">Perte_Charge_Singuliere_VDF</a>	<a href="#">Perte_Charge_Singuliere_VEF</a>
petsc	<a href="#">Cx</a>	<a href="#">muscl</a>	<a href="#">EF_stab</a>
petsc_gpu			
phase	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
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phase_continue	<a href="#">FTD_instab2D</a>	<a href="#">FTD_Boiling_bubble</a>	<a href="#">FTD_Marqueur_VEF_3D</a>
XXX			
phase_marquee	<a href="#">FTD_Marqueur_VDF_2D</a>	<a href="#">FTD_Transfo_bulles_VDF_3D</a>	<a href="#">FTD_Transfo_bulles_VEF_3D</a>
pilut			
pisso	<a href="#">P_out_var_impl</a>	<a href="#">Radiation_jdd2</a>	<a href="#">Radiation_jdd4</a>
plan	<a href="#">muscl</a>	<a href="#">muscl_old</a>	<a href="#">smago_VDF</a>
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plans_paralleles	<a href="#">DYN_plans_paralleles</a>		
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plaque_thermique_vdf			
pmetis			
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point_phase	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>	<a href="#">Forces_IBC_3D_VDF</a>
point	<a href="#">Cx</a>	<a href="#">muscl</a>	<a href="#">THI_VEF</a>
point1	<a href="#">Extrait_plan</a>	<a href="#">ThHyd_3D_VEFPrePIB</a>	
point2	<a href="#">Extrait_plan</a>	<a href="#">ThHyd_3D_VEFPrePIB</a>	
point3	<a href="#">Extrait_plan</a>		
points	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">RK2</a>
poly_rho	<a href="#">Quasi_Comp_VD_GR_VDF</a>	<a href="#">Quasi_Comp_Cond_GR_VDF</a>	<a href="#">Quasi_Comp_Obst_GR_VDF</a>
poly_T	<a href="#">Quasi_Comp_VD_GR_VDF</a>	<a href="#">Quasi_Comp_Cond_GR_VDF</a>	<a href="#">Quasi_Comp_Obst_GR_VDF</a>
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polynomes	<a href="#">Polynomes</a>		
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porosites	<a href="#">Poreps</a>	<a href="#">Porosites</a>	
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porosites_champ	<a href="#">Poreux_VEF_2D</a>	<a href="#">Poreux_VEF_3D</a>	<a href="#">Poreux_VEF_jdd1</a>
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porosite_volumique	<a href="#">Poreux_VEF_2D</a>	<a href="#">Poreux_VEF_3D</a>	<a href="#">Poreux_VEF_jdd1</a>
XXXlift			
portance			
position	<a href="#">Forces_IBC_2D_VEF</a>		
position_like	<a href="#">upwind</a>	<a href="#">champ_synonyme</a>	
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postraitement	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">RK2</a>

XXXpost_processing_ft_lata			
postraitement_ft_lata	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>
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postraitements	<a href="#">Cx</a>	<a href="#">2D_P0</a>	<a href="#">2D_P1</a>
XXXpost_process_domain			
postraiter_domaine	<a href="#">Sonde</a>	<a href="#">Kernel</a>	<a href="#">docond</a>
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potentiel_chimique_generalise	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
prandtl_eps	<a href="#">Marche</a>	<a href="#">Reprise_xyz_VDF</a>	<a href="#">Reprise_grossier_fin</a>
prandtl_k	<a href="#">Marche</a>	<a href="#">Reprise_xyz_VDF</a>	<a href="#">Reprise_grossier_fin</a>
prandtl	<a href="#">cpu_3D</a>	<a href="#">EF_stab</a>	<a href="#">Bilans_VEF</a>
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prandt_turbulent_fonction_nu_t_alpha	<a href="#">Conduite_lm_prdt_var</a>	<a href="#">Conv_Pipe_InOut_jdd1</a>	<a href="#">Conv_Pipe_InOut_jdd2</a>
prandtl_eps	<a href="#">Marche</a>	<a href="#">Reprise_xyz_VDF</a>	<a href="#">Reprise_grossier_fin</a>
prandtl_k	<a href="#">Marche</a>	<a href="#">Reprise_xyz_VDF</a>	<a href="#">Reprise_grossier_fin</a>
prdt	<a href="#">ThHyd_C_K_Eps</a>	<a href="#">ThHyd_C_SsMaille_Smago_VDF</a>	<a href="#">ThHyd_C_SsMaille_Smago_VEF</a>
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prdt_sur_kappa	<a href="#">ThHyd_keps_VEF</a>	<a href="#">ThHyd_C_SsMaille_Smago_VDF</a>	
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precisiongeom	<a href="#">Impinging_jet</a>	<a href="#">ChFrontLu_read_file</a>	<a href="#">IBC_penalisation_poiseuille_jdd1</a>
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precision_impr	<a href="#">VDF_2x3</a>	<a href="#">Bilans_VEF</a>	<a href="#">VAHL_DAVIS</a>
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precond_nul	<a href="#">Transformer</a>	<a href="#">ChFrontExtXYZ</a>	<a href="#">ChDonFoncxyzVDF</a>
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precond	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">THI</a>
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preconditionnement_diag	<a href="#">Adams_Bashforth</a>	<a href="#">ibc_refroidi_jdd1</a>	<a href="#">ibc_refroidi_jdd2</a>
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predefini	<a href="#">P1toP0P1Pa</a>	<a href="#">P1toP1Bulle</a>	<a href="#">TP_Canal_VDF</a>
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pression	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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pression_pa	<a href="#">Cx</a>	<a href="#">2D_P0</a>	<a href="#">Bilans_VEF</a>
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pression_reference	<a href="#">Cell_numbers_VDF</a>	<a href="#">ibc_refroidi_jdd1</a>	<a href="#">ibc_refroidi_jdd2</a>
XXXtotal_pressure			
pression_tot	<a href="#">QC_verifP_jdd1</a>	<a href="#">QC_verifP_jdd2</a>	<a href="#">QC_verifP_jdd3</a>
print	<a href="#">FTD_Tgrid</a>	<a href="#">Cell_numbers_VDF</a>	<a href="#">FTD_VDF_mono_var</a>
XXXproblem			
probleme	<a href="#">Cx</a>	<a href="#">Collecteur</a>	<a href="#">VAHL_DAVIS</a>
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probleme_couple	<a href="#">Coup</a>	<a href="#">Debog</a>	<a href="#">docond</a>
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probleme_ft_disc_gen	<a href="#">FTD_Tgrid</a>	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>
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produits	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>	
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profil	<a href="#">Couplage_champ_cl_VDF</a>	<a href="#">Couplage_champ_cl_VEF</a>	<a href="#">Reordonner_faces_periodiques</a>
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projection_initiale	<a href="#">Reprise_xyz2</a>	<a href="#">Reprise_xyz3</a>	<a href="#">Champ_fonc_xyz</a>
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projection_normale_bord			
XXX			
proprietes_particules	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VDF_3D</a>	<a href="#">FTD_Colonne_VEF_2D</a>
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pr	<a href="#">Paroi_fictif_turbulent_vef</a>	<a href="#">Compare_VDF_Flux_Turb_Nu_Impose</a>	<a href="#">Compare_VEF_Flux_Turb_Nu_Impose</a>
pt-scotch			
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puissance_volumique	<a href="#">Champ_Fonc_txyz</a>	<a href="#">FTD_VDF_mono_var</a>	<a href="#">ThHyd_Coupl_Keps_Re7500_VEF</a>
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quadra	<a href="#">Moyenne_vol_quadra_3d</a>		
quick	<a href="#">Cl_var</a>	<a href="#">cpu_3D</a>	<a href="#">VDF_2x3</a>
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raccord	<a href="#">Coup</a>	<a href="#">Debog</a>	<a href="#">docond</a>
rectangle	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">Poreps</a>
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redresser_hexaedres_vdf	<a href="#">Kernel_Redresser_hexaedres_vdf</a>		
XXXanisotropic_refine			
raffiner_anisotrope	<a href="#">Boussinesq</a>		
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raffiner_isotrope	<a href="#">Champ_fonc_MED</a>	<a href="#">VAHL_DAVIS_VEF</a>	<a href="#">ChDonFoncxyzVEF</a>
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rayon_spot			
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reactifs	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>	
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reduction_0d	<a href="#">Cx</a>	<a href="#">VAHL_DAVIS</a>	<a href="#">centre4_VEF</a>
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refchamp	<a href="#">Cx</a>	<a href="#">muscl</a>	<a href="#">Sondes</a>
refinement_type			
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relax_barycentrage	<a href="#">FTD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">Cell_numbers_VDF</a>
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relax_pression	<a href="#">Hyd_Cx_segsol</a>	<a href="#">docond_segsol</a>	<a href="#">VAHL_DAVIS_segsol</a>
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remaillage	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>
remove_elem	<a href="#">Kernel_Remove_elem</a>		

<b>remove_invalid_internal_boundaries</b>	<a href="#">Kernel_remove_invalid_internal_boundary</a>		
<b>XXXjoin_boundary</b>			
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<b>re_long</b>	<a href="#">Perte_Charge_Circulaire_QC_VEF</a>	<a href="#">Perte_Charge_Circulaire_VEF_jdd1</a>	<a href="#">Perte_Charge_Circulaire_VEF_jdd2</a>
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<b>re_tot</b>	<a href="#">Perte_Charge_Circulaire_QC_VEF</a>	<a href="#">Perte_Charge_Circulaire_VEF_jdd1</a>	<a href="#">Perte_Charge_Circulaire_VEF_jdd2</a>
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<b>reordonner_faces_periodiques</b>	<a href="#">P1toP0P1Pa</a>	<a href="#">P1toP1Bulle</a>	<a href="#">QC_VEF_diff_impl</a>
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<b>reprise_correlation</b>			
<b>XXXrestart</b>			
<b>reprise</b>	<a href="#">sdocond</a>	<a href="#">sreprise</a>	<a href="#">Extension</a>
<b>XXX</b>			
<b>repulsion_aux_bords</b>			
<b>XXX</b>			
<b>residu_max_gmresnl</b>	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
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<b>resolution_explicite</b>	<a href="#">Impinging_jet</a>	<a href="#">ChFrontLu_gen_file</a>	<a href="#">Reprise_grossier_fin</a>
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<b>resoudre</b>	<a href="#">PETSC_OPENMP</a>	<a href="#">resume_last_time</a>	<a href="#">ThHyd_C_K_Eps_P0P1Pa</a>
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<b>resume_last_time</b>	<a href="#">resume_last_time</a>	<a href="#">ThHyd_C_K_Eps_VEF</a>	<a href="#">resume_last_time_xyz</a>
<b>XXX</b>			
<b>restriction</b>	<a href="#">Kernel_Sous_Zone_Fonction</a>		
<b>XXX</b>			
<b>reverse_normal</b>	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>	
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<b>reynolds_maille</b>	<a href="#">Cell_numbers_VDF</a>		
<b>XXXdensity</b>			
<b>rho</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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<b>ri</b>	<a href="#">Sous_zone_VDF</a>	<a href="#">FTD_VDF_mono_var</a>	<a href="#">Kernel_Sous_zone</a>
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rotation	<a href="#">Forces_IBC_2D_VEF</a>	<a href="#">Inward_field_jdd1</a>	<a href="#">Inward_field_jdd2</a>
XXXrunge_kutta_order_2			
runge_kutta_rationnel_ordre_2	<a href="#">RK2</a>	<a href="#">QC_centre4_VDF</a>	<a href="#">Obstacle_Turb_quadra</a>
XXXrunge_kutta_order_3			
runge_kutta_ordre_3	<a href="#">RK3</a>	<a href="#">THI</a>	<a href="#">EF_stab</a>
XXXrunge_kutta_order_4			
runge_kutta_ordre_4_d3p	<a href="#">RK4</a>	<a href="#">Cell_numbers_VDF</a>	<a href="#">FTD_VDF_mono_var</a>
XXXwithout_kinetic_energy			
sans_energie_cinetique	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
XXXsave			
sauvegarde	<a href="#">Debog</a>	<a href="#">Sonde</a>	<a href="#">docond</a>
XXXdelete_and_saveXXX			
sauvegarde_simple	<a href="#">Cx</a>	<a href="#">PETSC_GCP</a>	<a href="#">VAHL_DAVIS</a>
save_matrix			
save_matrice	<a href="#">Def_VEF_impl</a>	<a href="#">PETSC_cpu_3D_CGILU</a>	<a href="#">PETSC_ThHyd_2D_VEF_Ostwald</a>
XXXscatter_ascii			
scatterformatte	<a href="#">periodique</a>	<a href="#">Build_1_domains_from_3</a>	
XXXscatter_med			
scattermed	<a href="#">Kernel_splitter_med</a>		
scatter	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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sch_cn_ex_iteratif	<a href="#">Tuyau</a>	<a href="#">Sondes</a>	<a href="#">THI_VEF</a>
XXX			
sch_cn_iteratif	<a href="#">CN_iteratif_VDF</a>	<a href="#">CN_iteratif_VEF</a>	<a href="#">CN_iteratif_VDF_fluide</a>
XXXscheme_ch			
schema_ch	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
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schema_euler_explicite	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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schema_euler_implicite	<a href="#">sans_impl</a>	<a href="#">Collecteur</a>	<a href="#">tubeY_jdd1</a>
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XXXscheme_phase_field			
schema_phase_field	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
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schema_predictor_corrector	<a href="#">Debog_VEF</a>	<a href="#">Pred_Cor_P1B</a>	<a href="#">Pred_Cor_VEF</a>
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schema_adams_bashforth_order_2	<a href="#">Adams_Bashforth</a>	<a href="#">Multistep_Methods_jdd2</a>	<a href="#">Multistep_Methods_jdd4</a>
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schema_adams_bashforth_order_3	<a href="#">Multistep_Methods_jdd3</a>	<a href="#">Multistep_Methods_jdd5</a>	<a href="#">Schema_Adams_Bashforth_order_3</a>
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schema_adams_moulton_order_2	<a href="#">Multistep_Methods_jdd6</a>		
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schema_adams_moulton_order_3	<a href="#">Multistep_Methods_jdd7</a>	<a href="#">Schema_Adams_Moulton_order_3</a>	
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schema_backward_differentiation_order_2	<a href="#">ThHyd_C_K_Eps_P0P1Pa</a>	<a href="#">Multistep_Methods_jdd8</a>	

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schema_backward_differentiation_order_3	<a href="#">Multistep_Methods_jdd9</a>		
schmidt	<a href="#">CoefDiffNul</a>	<a href="#">Hyd_C_keps_2D</a>	<a href="#">ThHyd_C_K_Eps</a>
scotch			
scotti	<a href="#">Canal_VEF_3D_SCOTTI</a>		
sc	<a href="#">Quasi_Comp_Cond_GP_VDF_FM</a>	<a href="#">Quasi_Comp_Obst_GP_VDF_FM</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_Turb_FM</a>
scturb	<a href="#">ThHyd_C_K_Eps</a>	<a href="#">ThHyd_C_K_Eps_P0P1Pa</a>	<a href="#">ThHyd_C_SsMaille_Smago_VDF</a>
segment	<a href="#">THI</a>	<a href="#">Coup</a>	<a href="#">2D_P0</a>
segmentpoints	<a href="#">VAHL_DAVIS</a>		
XXX			
segment_senseur_1			
XXX			
segment_senseur_2			
XXX			
senseur_interface			
XXX			
seuil_convergence_implicite	<a href="#">sans_impl</a>	<a href="#">docond_impl</a>	<a href="#">Def_VEF_impl</a>
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seuil_convergence_variable			
XXX			
seuil_convergence_uzawa	<a href="#">pena_ellipsoide_jdd1</a>	<a href="#">pena_ellipsoide_jdd2</a>	
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seuil_cv_iterations_ptfixe	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
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seuil_diffusion_implicite	<a href="#">poise_VEF</a>	<a href="#">Pred_Cor_P1B</a>	<a href="#">Yahl_Davis_hexa</a>
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seuil_divu	<a href="#">2D_P0</a>		
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seuil_dvolume_residuel	<a href="#">FTD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">FTD_Chute_Goutte_2D</a>
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seuil_generation_solveur			
XXX			
seuil_verification_solveur			
XXX			
seuil_test_preliminaire_solveur			
XXX			
seuil_residu_gmresnl	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
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seuil	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">THI</a>
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seuil_statio	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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short_family_names	<a href="#">PCS_med_VEF</a>	<a href="#">Kernel_med_shorty</a>	<a href="#">Kernel_ecrire_champ_med</a>
sigma	<a href="#">FTD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">ftd_gravite_jdd1</a>

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signe			
simpler	<a href="#">sans_impl</a>	<a href="#">docond_impl</a>	<a href="#">Reprise_impl</a>
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slambda	<a href="#">Paroi_VEF_3D</a>	<a href="#">Quasi_Comp_3D</a>	<a href="#">QC_verifP_jdd10</a>
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solv_elem	<a href="#">Collecteur</a>	<a href="#">QC_VDF_diff_impl</a>	<a href="#">QC_VEF_diff_impl</a>
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solveur	<a href="#">sans_impl</a>	<a href="#">Collecteur</a>	<a href="#">tubeY_jdd1</a>
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solv_optimal			
XXXsum			
somme	<a href="#">Cx</a>	<a href="#">VAHL_DAVIS</a>	<a href="#">VAHL_DAVIS_VEF</a>
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somme_ponderee	<a href="#">FTD_all_VDF</a>	<a href="#">FTD_all_VEF</a>	<a href="#">Mixing_Bidim_Axi_jdd1</a>
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sommets	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">Cell_numbers_VDF</a>	<a href="#">ftd_gravite_jdd1</a>
XXX			
som	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
XXXprobes			
sondes	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
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sortie_libre_rho_variable	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>	<a href="#">FTD_IBC_3D_VEF</a>
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source_con_phase_field	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
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source_constituant	<a href="#">diagonale</a>	<a href="#">Constituants</a>	<a href="#">Constituant_VEF</a>
XXX			
source_constituant_vortex			
XXX			
source_generique	<a href="#">CoefDiffNul</a>	<a href="#">SourcesTranformation</a>	<a href="#">VAHL_DAVIS_source_gen</a>
XXX			
source_isovaleur	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_Chute_Goutte_2D</a>	<a href="#">FTD_VDF_parallel_ok</a>
XXX			
source_qdm	<a href="#">2D_P0</a>	<a href="#">2D_P1</a>	<a href="#">3D_P0</a>
XXX			
source_qdm_lambdaup	<a href="#">Tuyau</a>	<a href="#">THI_VEF</a>	<a href="#">Canal_VEF_3D_SCOTTI</a>
XXX			
source_qdm_phase_field	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>

XXX			
source_rayo_semi_transp	<a href="#">Quasi_Comp_VD_GP_VDF_P1</a>	<a href="#">Quasi_Comp_VD_GP_VEF_P1</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_P1</a>
XXXsource_robin			
source_robin	<a href="#">Turbul_LES_Robin_wall_law</a>	<a href="#">Turbul_RANS_Robin_wall_law</a>	<a href="#">Fiche_validation_Re590_jdd3</a>
XXXsource_robin_scalar			
source_robin_scalaire	<a href="#">Turbul_LES_Robin_wall_law</a>	<a href="#">Turbul_RANS_Robin_wall_law</a>	<a href="#">Fiche_validation_Re180_Pr0.71_jdd3</a>
source	<a href="#">Cx</a>	<a href="#">muscl</a>	<a href="#">Sondes</a>
sources	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">2D_P0</a>
XXX			
source_reference	<a href="#">VAHL_DAVIS_VEF</a>	<a href="#">Inward_field_jdd1</a>	<a href="#">Inward_field_jdd2</a>
XXX			
sources_reference	<a href="#">upwind</a>	<a href="#">VAHL_DAVIS</a>	<a href="#">docond_VEF_3D</a>
XXX			
source_th_tdivu	<a href="#">Sondes</a>	<a href="#">Sondes_chsom</a>	<a href="#">Source_TdivU_amont</a>
XXX			
source_transport_fluctuation_temperature			
XXX			
source_transport_flux_chaleur_turbulente			
XXX			
source_transport_k_eps_anisotherme	<a href="#">ThHyd_keps_VEF</a>	<a href="#">ThHyd_Cond_K_Eps</a>	<a href="#">Extraire_domaine_2D</a>
XXX			
source_transport_k_eps_bas_reynolds	<a href="#">docond_BasRe</a>	<a href="#">jones_launder_VDF</a>	<a href="#">launder_sharma_VDF</a>
XXX			
source_transport_k_eps	<a href="#">Marche</a>	<a href="#">Marche_incline</a>	<a href="#">Reprise_xyz_VDF</a>
XXX			
sous_maille_1elt_selectif_mod	<a href="#">SGE_Fst_sel_mod_VEF</a>		
XXX			
sous_maille_dsgrs			
XXX			
sous_maille_dyn	<a href="#">DYN_6_points</a>	<a href="#">DYN_Moy_Euler</a>	<a href="#">Wale_Prdt_Dyn</a>
XXX			
sous_maille_selectif_mod	<a href="#">SGE_Fst_sel_mod_VDF</a>		
XXX			
sous_maille_selectif	<a href="#">TBLE_VDF_3D</a>	<a href="#">SGE_Fst_sel_VDF</a>	<a href="#">LP_ODVM_Timp_VDF</a>
XXX			
sous_maille_smago_dyn	<a href="#">DYN_6_points</a>	<a href="#">DYN_Moy_Euler</a>	<a href="#">DYN_plans_paralleles</a>
XXX			
sous_maille_smago_filtre			
XXXsmagorinsky_model			
sous_maille_smago	<a href="#">smago_VDF</a>	<a href="#">smago_VEF</a>	<a href="#">Hyd_C_VDF_Smago</a>
XXX			
sous_maille	<a href="#">THI</a>	<a href="#">cpu_3D</a>	<a href="#">stat_VEF</a>
XXXwale_model			
sous_maille_wale	<a href="#">Tuyau</a>	<a href="#">EF_stab</a>	<a href="#">THI_VEF</a>
XXXsubzoneXXXsub_zone			
sous_zone	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">Tuyau</a>



XXXsubzones			
sous_zones	<a href="#">LP_Ciofalo_VDF</a>	<a href="#">Maill_Pave_tanh</a>	<a href="#">Decoup_period_2D</a>
spai	<a href="#">PETSC_GCP_SPAL_P0P1Pa</a>		
splitting	<a href="#">MaillerParallel</a>	<a href="#">Kernel_splitter_med</a>	
ssor	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">THI</a>
stab	<a href="#">ThHyd_C_K_Eps_P0P1Pa</a>	<a href="#">VEF_diffusion_P0_stab</a>	<a href="#">VEF_diffusion_P0_stab_TVD</a>
XXX			
stabilise	<a href="#">DYN_6_points</a>	<a href="#">DYN_Moy_Euler</a>	<a href="#">Wale_Prdt_Dyn</a>
standard	<a href="#">Tuyau</a>	<a href="#">THI_VEF</a>	<a href="#">Pb_couples</a>
XXX			
statistiques_en_serie	<a href="#">Post_Eclate</a>	<a href="#">Post_Meshtv</a>	<a href="#">Moyenne_mobile</a>
XXX			
statistiques	<a href="#">Cx</a>	<a href="#">stat_VEF</a>	<a href="#">docond_VEF</a>
stencil_width			
XXX			
suivi			
superbee	<a href="#">EFstab_Muscl_and_Limiters_VEF_jdd7</a>	<a href="#">EFstab_Muscl_and_Limiters_VEF_jdd14</a>	
XXX			
suppression_sous_zone			
XXXremove_boundary			
supprime_bord	<a href="#">ChFrontLu</a>	<a href="#">Extract_2D_from_3D</a>	<a href="#">Kernel_supprime_bord</a>
surface	<a href="#">Extrait_plan</a>	<a href="#">Extraire_domaine</a>	<a href="#">CanalColburnVEFRayo</a>
XXX			
surfacique	<a href="#">Poreps</a>	<a href="#">Porosites</a>	<a href="#">Cylindre_chauffant</a>
sutherland	<a href="#">Paroi_VEF_3D</a>	<a href="#">Quasi_Comp_3D</a>	<a href="#">QC_verifP_jdd10</a>
XXXsymmetry			
symetrie	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
symx	<a href="#">RK2</a>	<a href="#">RK3</a>	<a href="#">RK4</a>
symy	<a href="#">Kernel</a>	<a href="#">Sondes</a>	<a href="#">PETSC_VEF</a>
symz	<a href="#">Kernel</a>	<a href="#">PETSC_VEF</a>	
system	<a href="#">geom2ansys</a>	<a href="#">Bulle_oscillante</a>	<a href="#">Cell_numbers_VDF</a>
t0	<a href="#">Debog</a>	<a href="#">EF_2D</a>	<a href="#">Cl_var</a>
XXX			
tanh	<a href="#">Parallele</a>	<a href="#">DYN_6_points</a>	<a href="#">DYN_Moy_Euler</a>
XXX			
tanh_dilatation	<a href="#">Maill_Pave_tanh</a>		
XXX			
tanh_taille_premiere_maille	<a href="#">Wale_Prdt_Dyn</a>	<a href="#">Maill_Pave_tanh</a>	<a href="#">QC_VDF_diff_impl</a>
XXX			
taux_cisaillement	<a href="#">M3DLAM</a>	<a href="#">Taux_cisaillement</a>	<a href="#">Couette_cylindrique</a>
XXX			
taux_dissipation_temperature			
XXXt_begin			
t_deb	<a href="#">Cx</a>	<a href="#">Sondes</a>	<a href="#">stat_VEF</a>
XXX			
t_debut_injection	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VEF_2D</a>	

XXX			
t_debut_integration	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VDF_3D</a>	<a href="#">FTD_Colonne_VEF_2D</a>
XXX			
t_debut_transfo	<a href="#">FTD_particles_transfo_jdd1</a>	<a href="#">FTD_particles_transfo_jdd2</a>	
XXX			
tcpumax	<a href="#">ThHyd_C_K_Eps_P0P1Pa</a>		
XXX			
tdivu	<a href="#">test_op_conv_vef_jdd3</a>		
temperature	<a href="#">Cx</a>	<a href="#">RK2</a>	<a href="#">RK3</a>
temperature_mpoint	<a href="#">FTD_Boiling_bubble</a>	<a href="#">FTD_Couplage_champ_cl_VDF</a>	
XXXwall_temperature			
temperature_paro			
XXX			
temperature_physique	<a href="#">Test_tparoi_jdd1</a>	<a href="#">Test_tparoi_jdd2</a>	<a href="#">Test_tparoi_jdd3</a>
XXX			
temperature_thermique	<a href="#">FTD_Boiling_bubble</a>		
XXX			
temps_d_affichage	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
XXX			
temps_debut_prise_en_compte_drho_dt			
XXX			
terme_complet	<a href="#">Cylindre_tournant</a>	<a href="#">Repere_Rotation_VEF</a>	<a href="#">Repere_Rotation_Variable</a>
XXX			
terme_gravite	<a href="#">Bulle_oscillante</a>	<a href="#">ftd_gravite_jdd1</a>	<a href="#">FTD_Colonne_VDF_2D</a>
XXX			
test_solveur	<a href="#">Test_solveur_sym</a>	<a href="#">Test_solveur_non_sym</a>	
XXX			
tetraedriser_homogene_compact	<a href="#">docond_VEF_3D</a>	<a href="#">Distance_paro</a>	<a href="#">Paroi_rugueuse</a>
XXX			
tetraedriser_homogene_fin	<a href="#">THI_VEF</a>	<a href="#">keys_3D_VEF</a>	<a href="#">Periodique_Metis</a>
XXX			
tetraedriser_homogene	<a href="#">3D_P0</a>	<a href="#">3D_P1</a>	<a href="#">DI_L2</a>
XXX			
tetraedriser_par_prisme	<a href="#">3DParoix</a>	<a href="#">ThHyd_keys_VEF_perio</a>	
XXX			
tetraedriser	<a href="#">LP_WW_VEF</a>	<a href="#">Newton_3D</a>	<a href="#">TP_THI_VEF</a>
XXX			
thi	<a href="#">THI</a>	<a href="#">TP_THI_VDF</a>	<a href="#">SGE_Fst_VDF</a>
XXX			
thomas	<a href="#">FTD_sloshing_jdd1</a>	<a href="#">FTD_remaillage_vdf</a>	<a href="#">FTD_remaillage_vef</a>
XXX			
t_debut_integration	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VDF_3D</a>	<a href="#">FTD_Colonne_VEF_2D</a>
XXX			
t_ext	<a href="#">Cl_var</a>	<a href="#">Sondes</a>	<a href="#">conduc</a>
XXXt_end			
t_fin	<a href="#">Cx</a>	<a href="#">Sondes</a>	<a href="#">stat_VEF</a>

XXX			
tinf	<a href="#">CanalColburnVEFRayo</a>		
tinit	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
tmax	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
XXX			
trace	<a href="#">Inward_field_jdd1</a>	<a href="#">Inward_field_jdd2</a>	<a href="#">Inward_field_jdd3</a>
XXXdrag			
trainee	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VDF_3D</a>	<a href="#">FTD_Colonne_VEF_2D</a>
XXX			
traitement_particulier	<a href="#">THI</a>	<a href="#">TP_THI_VDF</a>	<a href="#">tubeY_jdd1</a>
XXX			
traitement_pth	<a href="#">Paroi_VEF_3D</a>	<a href="#">Bilans_VEF_QC</a>	<a href="#">Quasi_Comp_3D</a>
XXX			
traitement_rho_gravite	<a href="#">Wale_Prdt_Dyn</a>	<a href="#">DarcyFlow_jdd2</a>	<a href="#">DarcyFlow_jdd4</a>
XXX			
tranche	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">RK2</a>
XXX			
tranches	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">RK2</a>
XXX			
transformation	<a href="#">upwind</a>	<a href="#">VAHL_DAVIS</a>	<a href="#">CoefDiffNul</a>
XXX			
transformation_bulles	<a href="#">FTD_Marqueur_VDF_2D</a>	<a href="#">FTD_Transfo_bulles_VDF_3D</a>	<a href="#">FTD_Transfo_bulles_VEF_3D</a>
XXXtransform			
transformer	<a href="#">2D_P0</a>	<a href="#">2D_P1</a>	<a href="#">3D_P0</a>
XXXtransport_thermal_fluctuation			
transport_fluctuation_temperature			
XXXtransport_turbulent_heat_flux			
transport_flux_chaleur_turbulente			
transport_interfaces_ft_disc	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>
XXXtransport_k_epsilon_low_reynolds			
transport_k_epsilon_bas_reynolds	<a href="#">docond_BasRe</a>	<a href="#">Nagano_WBasRe</a>	<a href="#">jones_launder_VDF</a>
transport_k_epsilon	<a href="#">Marche</a>	<a href="#">Pb_couples</a>	<a href="#">keys_1D_VEF</a>
XXX			
transport_marqueur_ft	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VDF_3D</a>	<a href="#">FTD_Colonne_VEF_2D</a>
XXX			
transversale	<a href="#">PCR</a>	<a href="#">Pertes_d_charges_CF_VDF</a>	
XXXtriangle			
triangle	<a href="#">Extrait_plan</a>		
XXXtriangulate_in2			
triangler	<a href="#">EF_stab</a>	<a href="#">gradp_VEF</a>	<a href="#">Post_multi</a>
XXXtriangulate_in4			
triangler_h	<a href="#">2Tri</a>	<a href="#">2D_P0</a>	<a href="#">2D_P1</a>
XXXtriangulate_in8			
triangler_fin	<a href="#">Canal_incline_VEF</a>	<a href="#">K_eps_init_par_LM</a>	<a href="#">Canal_perio_VEF_2D</a>
XXX3_tetra			
trois_tetra	<a href="#">Kernel_ExtrudeBord_3tetra</a>	<a href="#">ThermalCoupling_TurbulentFlow_VEF_jdd2</a>	

XXX			
tsup	<a href="#">CanalColburnVEFRayo</a>		
XXX			
tube	<a href="#">DI_L2</a>	<a href="#">tubeY_jdd1</a>	<a href="#">tubeY_jdd2</a>
XXX			
tube_hexagonal			
XXXlaw_of_the_wall			
turbulence_paroi	<a href="#">THI</a>	<a href="#">Tuyau</a>	<a href="#">Marche</a>
tx1			
tx2			
tx3			
type	<a href="#">Cx</a>	<a href="#">Collecteur</a>	<a href="#">VAHL_DAVIS</a>
XXXremeshing_type			
type_remaillage	<a href="#">FTD_Tgrid</a>	<a href="#">FTD_Chute_Goutte_2D</a>	<a href="#">FTD_VDF_parallel_ok</a>
XXXimposed_velocity_type			
type_vitesse_imposee	<a href="#">Cell_numbers_VDF</a>	<a href="#">ibc_refroidi_jdd1</a>	<a href="#">ibc_refroidi_jdd2</a>
two_way_coupling	<a href="#">FTD_Colonne_VDF_3D_Couplage</a>	<a href="#">FTD_Colonne_VEF_3D_Couplage</a>	<a href="#">FTD_particles_coupling_jdd5</a>
XXX			
ubar_umprim_cible	<a href="#">2D_P0P1_GCP_SSOR_BLOC</a>		
XXX			
ucent	<a href="#">LP_WW_VDF</a>	<a href="#">LP_WW_VEF</a>	<a href="#">Init_canal</a>
XXXuniform			
uniforme	<a href="#">Cell_numbers_VDF</a>	<a href="#">ibc_refroidi_jdd1</a>	<a href="#">ibc_refroidi_jdd2</a>
XXX			
union	<a href="#">Kernel_Sous_Zone_Fonction</a>		
use_weights	<a href="#">THI_VEF</a>	<a href="#">Canal_perio_VDF_3D_Keps</a>	
u_tau	<a href="#">Test_tparoi_jdd1</a>	<a href="#">Test_tparoi_jdd2</a>	<a href="#">Test_tparoi_jdd3</a>
u_star	<a href="#">QC_centre4_VDF</a>	<a href="#">ThHyd_keps_VEF</a>	<a href="#">Cylindre_chauffant</a>
utau_imp	<a href="#">Test_tparoi_jdd1</a>	<a href="#">Test_tparoi_jdd2</a>	<a href="#">Test_tparoi_jdd3</a>
uzawa			
XXXkinetic_energy_value			
val_ec	<a href="#">THI</a>	<a href="#">TP_THI_VDF</a>	<a href="#">SGE_Fst_VDF</a>
XXX			
valeur_a_elem			
normal_value	<a href="#">2D_P1</a>	<a href="#">Inward_field_jdd1</a>	<a href="#">Inward_field_jdd2</a>
XXX			
valeur_totale_sur_volume	<a href="#">Poreps</a>	<a href="#">Chp_Morc_2D</a>	<a href="#">puissance_tot_VDF</a>
vanalbada	<a href="#">EFstab_Muscl_and_Limiters_VEF_jdd4</a>	<a href="#">EFstab_Muscl_and_Limiters_VEF_jdd11</a>	
vanleer	<a href="#">muscl</a>	<a href="#">Diagonale_Cube_jdd4</a>	<a href="#">Diagonale_Cube_jdd5</a>
XXX			
variance_temperature			
vdf	<a href="#">PCR</a>	<a href="#">PCS</a>	<a href="#">RK2</a>
XXXvdf_linear			
vdf_lineaire	<a href="#">FTD_2D_Axi</a>	<a href="#">FTD_VDF_RK3</a>	<a href="#">FTD_Couplage_champ_cl_VDF</a>
vefprep1b	<a href="#">Cx</a>	<a href="#">2Tri</a>	<a href="#">2D_P0</a>
XXXvector			

<b>vecteur</b>	<a href="#">upwind</a>	<a href="#">docond_VEF_3D</a>	<a href="#">PF_RT_boussi_p1</a>
<b>XXXcheck_boussinesq</b>			
<b>verif_boussinesq</b>	<a href="#">FTD_VDF_mono_var</a>	<a href="#">ThHyd_Cond_K_Eps</a>	
<b>XXXcheck_derivative</b>			
<b>verification_derivee</b>			
<b>XXXcheck_XXX</b>			
<b>verifiercoin</b>	<a href="#">Cx</a>	<a href="#">muscl</a>	<a href="#">2Cubes</a>
<b>XXXwith_extract_surface</b>			
<b>via_extraire_surface</b>	<a href="#">Extrait_plan</a>	<a href="#">ThHyd_3D_VEFPrePIB</a>	
<b>XXXcinematic_viscosity</b>			
<b>viscosite_cinematique</b>	<a href="#">Nu_var_VEF</a>	<a href="#">ThHyd_Cond_K_Eps</a>	<a href="#">Taux_cisaillement</a>
<b>XXXdynamic_viscosity</b>			
<b>viscosite_dynamique</b>	<a href="#">Parallele</a>	<a href="#">FTD_VDF_mono_var</a>	<a href="#">ThHyd_Cond_K_Eps</a>
<b>XXXconstant_dynamic_viscosity</b>			
<b>viscosite_dynamique_constante</b>	<a href="#">PF_RT_boussi_p1</a>	<a href="#">PF_RT_boussi_p2</a>	<a href="#">PF_RT_boussi_p3</a>
<b>XXXturbulent_dynamic_viscosity</b>			
<b>viscosite_dynamique_turbulente</b>	<a href="#">Quasi_Comp_3D</a>	<a href="#">Quasi_Comp_Cond_GP_VDF_Turb</a>	
<b>XXXturbulent_viscosity</b>			
<b>viscosite_turbulente</b>	<a href="#">THI</a>	<a href="#">Marche</a>	<a href="#">THI_VEF</a>
<b>XXXimposed_velocity</b>			
<b>vitesse_imposee</b>	<a href="#">FTD_IBC_3D_VEF</a>	<a href="#">FTD_vef_3d_ibc</a>	<a href="#">Cell_numbers_VDF</a>
<b>XXXinterpolated_velocity</b>			
<b>vitesse_interpolee</b>	<a href="#">FTD_Tgrid</a>	<a href="#">Bulle_oscillante</a>	<a href="#">ftd_gravite_jdd1</a>
<b>XXX</b>			
<b>vitesse_particules</b>	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VDF_3D</a>	<a href="#">FTD_Colonne_VEF_2D</a>
<b>XXXtangential_velocity</b>			
<b>vitesse_tangentielle</b>	<a href="#">Debog_VEF</a>	<a href="#">Reprise_xyz2</a>	<a href="#">Reprise_xyz3</a>
<b>XXXvelocity</b>			
<b>vitesse</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
<b>XXXvelocity_x</b>			
<b>vitesse_x</b>	<a href="#">Post_Eclate</a>	<a href="#">Sondes_chsom</a>	<a href="#">champ_synonyme</a>
<b>XXXvelocity_y</b>			
<b>vitesse_y</b>	<a href="#">Post_Eclate</a>	<a href="#">Poiseuille_VDF_uzawa</a>	
<b>XXXvelocity_z</b>			
<b>vitesse_z</b>	<a href="#">Turbulent_Simple_water_jet_jdd1</a>	<a href="#">Turbulent_Simple_water_jet_jdd2</a>	<a href="#">Turbulent_Simple_water_jet_jdd3</a>
<b>volume</b>	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VDF_3D</a>	<a href="#">FTD_Colonne_VEF_2D</a>
<b>XXXimposed_volume_phase_1</b>			
<b>volume_impose_phase_1</b>	<a href="#">FTD_VDF_RK3</a>		
<b>XXX</b>			
<b>volume_maille</b>	<a href="#">muscl</a>	<a href="#">muscl_old</a>	<a href="#">coude_irreg</a>
<b>XXX</b>			
<b>volume_particules</b>	<a href="#">FTD_Colonne_VDF_2D</a>	<a href="#">FTD_Colonne_VDF_3D</a>	<a href="#">FTD_Colonne_VEF_2D</a>
<b>XXX</b>			
<b>volume_sans_lissage</b>	<a href="#">Quasi_Comp_Coupl_Incomp</a>	<a href="#">ThHyd_C_Wale_Scalaires_Passifs_VEFPrePIB</a>	
<b>XXXextended_volumes</b>			
<b>volumes_etendus</b>	<a href="#">EF_stab_paroie_old</a>	<a href="#">EF_stab_alpha_sous_zone</a>	<a href="#">Test_recycl_2pbs_turb_VEF</a>

<b>XXXnot_extended_volumes</b>			
<b>volumes_non_etendus</b>			
<b>XXXvorticity</b>			
<b>vorticite</b>	<a href="#">THI</a>	<a href="#">Marche</a>	<a href="#">THI_VEF</a>
<b>x</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
<b>xinf</b>	<a href="#">CanalColburnVEFRayo</a>		
<b>xsup</b>	<a href="#">CanalColburnVEFRayo</a>		
<b>xyz</b>	<a href="#">P1toP0P1Pa</a>	<a href="#">P1toP1Bulle</a>	<a href="#">Reprise_impl</a>
<b>y</b>	<a href="#">Cx</a>	<a href="#">PCR</a>	<a href="#">PCS</a>
<b>y_plus</b>	<a href="#">Marche</a>	<a href="#">Newton_3D</a>	<a href="#">smago_VDF</a>
<b>z</b>	<a href="#">Cx</a>	<a href="#">THI</a>	<a href="#">3D_P0</a>
<b>XXXoutlet_zone</b>			
<b>zone_sortie</b>			
<b>6_points</b>	<a href="#">DYN_6_points</a>	<a href="#">Wale_Prdt_Dyn</a>	
<b>_gt_</b>			
<b>_ge_</b>			
<b>_lt_</b>			
<b>_le_</b>			

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