

DISS. ETH NO. 15091982

MULTISCALE AND TURBULENT  
INTERACTIONS FOR URBAN MICROCLIMATE  
PREDICTION

A dissertation submitted to  
ETH ZURICH

for the degree of  
DOCTOR OF SCIENCES

presented by  
MARCEL VONLANTHEN  
Master of Science in Mechanical Engineering (EPF Lausanne)  
born 15 September 1982  
citizen of Lausanne, Switzerland

accepted on the recommendation of  
Prof. Dr. Jan Carmeliet, examiner  
Dr. Jonas Allegrini, co-examiner  
Prof. Dr. Johan Meyers, co-examiner  
Prof. Dr. Catherine Gorlé, co-examiner

2015



## ABSTRACT

---

## ZUSAMMENFASSUNG

---

## ACKNOWLEDGMENTS

---



## CONTENTS

---

1	INTRODUCTION	1
1.1	How to cite a paper . . . . .	1
1.2	How to make index . . . . .	1
1.3	How to make tables . . . . .	1
1.4	Add acronyms . . . . .	2
2	BACKGROUND	3
2.1	a long text with equation . . . . .	3
2.2	Large Eddy Simulation . . . . .	5
2.2.1	Filtering operation . . . . .	5
2.2.2	Subgrid stress . . . . .	5
2.3	Turbulence modeling in LES . . . . .	5
3	DISCUSSION	7
3.1	Figures and Images . . . . .	7
3.1.1	Figures and Images in subsection . . . . .	7
	BIBLIOGRAPHY	9
	NOTATION	11
	ACRONYMS	13
	INDEX	15





## INTRODUCTION

---

### 1.1 HOW TO CITE A PAPER

my introduction, I want to cite (Moeng et al., 2007) because he is cool, and also Pope (2000) even cooler. Yeah! The following commands give:

- cite: Moeng et al., 2007
- citep: (Moeng et al., 2007)
- citet: Moeng et al. (2007)
- textcite: Moeng et al. (2007)

See <http://merkel.zoneo.net/Latex/natbib.php> for more styles.

### 1.2 HOW TO MAKE INDEX

Direct Numerical Simulation (DNS) resolves all the turbulent scales. As it is an important topic, I add DNS to the index. Large Eddy Simulation (LES) is also in the index. How to build the index:

1. Build the document with PDFLatex
2. Build the index with makeIndex
3. Build the document again with PDFLatex

Most of the latex editor have a button/shortcut for makeIndex. See <http://en.wikibooks.org/wiki/LaTeX/Indexing> for more information in indexing.

### 1.3 HOW TO MAKE TABLES

A example of a floating table with caption and label (see tab.1.1).

$M$ (size)	60		90		120	
$K$ (# states)	2	5	2	5	2	5
$\sigma = 0.05$						
MPLP	0.71	0.99	0.51	0.96	0	0.95
LPQP-U	0.97	0.99	0.97	1	0.98	1
LPQP-T	1	0.97	1	0.98	1	0.98
TRWS	0	0	0	0	0.39	0
$\sigma = 0.5$						
MPLP	1	1	1	1	1	0.99
LPQP-U	0.99	0.92	0.99	0.91	1	0.94
LPQP-T	0.99	0.95	0.99	0.94	0.99	0.96
TRWS	0	0	0	0	0	0

Table 1.1: Averaged scores achieved by the MPE solvers on the synthetic grid data. The scores

#### 1.4 ADD ACRONYMS

To use linked acronyms, first fill `acronyms.tex` with your entries. The first time an acronym is used with the command `ac{}`, The full name and the acronym in brackets is displayed. At the second use and after, only the acronym without bracket is shown. If you want to display the full name again, use the command `acf{}`. Example:

Three major numerical models exist in Computational Fluid Dynamics ([CFD](#)). The first one, which resolved all the turbulent scales, is known as Direct Numerical Simulation ([DNS](#)). The second one, which resolved only the large scales, is named Large Eddy Simulation ([LES](#)). The third one, which is purely a statistical model, is the Reynolds Average Navier Stokes ([RANS](#)) approach. Nowadays, [DNS](#) is unfeasible for the majority of problems, therefore [RANS](#) models are used. Despite being computational intensive, [LES](#) offers much higher quality results than Reynolds Average Navier Stokes ([RANS](#)) for only a fraction of the computational cost of a [DNS](#).

## BACKGROUND

---

### 2.1 A LONG TEXT WITH EQUATION

The microclimate over urban areas involves a wide range of flow scales. On the one hand, obstacles such as buildings, civil engineering structures or small terrain features, affect the atmospheric boundary layer. The topology of such obstacles results into small flow structures with a typical size of  $\mathcal{O} = 10^0 m$ . On the other hand, large scale effects, such as regional winds and convective cells, generate large scale eddies with a size of  $\mathcal{O} = 10^2 m$ . Resolving this wide range of scales in a single fine-grained Large Eddy Simulation (LES) model would still be unfeasible due to its computational cost in terms of cell count and time stepping. Even the use of local mesh refinement to tackle the cell count problem would still require a very small time step to keep the Courant number below unity. Therefore, a nesting procedure is proposed to solve the both issues. An LES-within-LES nesting is composed of a Small-domain fine-grained LES (referred as S-LES from now), which is embedded in a Large-domain coarse-grained LES (referred as L-LES). The fields of the L-LES are interpolated on the boundaries of the S-LES to achieve the nesting. A blending zone, also named relaxation zone, is sometime added in the S-LES domain to ensure a smooth transition between the flow fields of the two simulations.

Reynolds Averaged Navier-Stokes (RANS) nesting procedures are already common practice for operational Numerical Weather Prediction (NWP). For example, most of the European meteorological offices use the a global planetary model to get macroscale climate prediction and transfer the relevant data to a nested NWP model for the mesoscale weather prediction.

The reference LES and coarse LES solve the standard filtered Navier-stokes equation for mass and momentum (Smagorinsky, 1963), which can be written in conservative form as:

$$\frac{\partial \bar{u}_i}{\partial x_i} = 0 \quad (2.1a)$$

$$\frac{\partial \bar{u}_i}{\partial t} + \frac{\partial \bar{u}_i \bar{u}_j}{\partial x_j} = -\frac{\partial \bar{p}}{\partial x_i} + \nu \frac{\partial^2 \bar{u}_i}{\partial x_j \partial x_j} - \frac{\partial \tau_{ij}}{\partial x_j} \quad (2.1b)$$

with  $\bar{p}$  and  $\bar{u}_i$  the filtered (resolved) pressure and velocity fields, defined as

$$\bar{p} = p - p' \quad (2.2a)$$

$$\bar{u}_i = u_i - u'_i \quad (2.2b)$$

with  $p'$  and  $u'_i$  the residual pressure and velocity fields. On each filtered field, an averaging operation can be applied:

$$\langle \bar{p} \rangle = \bar{p} - p'' \quad (2.3a)$$

$$\langle \bar{u}_i \rangle = \bar{u}_i - u''_i \quad (2.3b)$$

with  $\langle \cdot \rangle$  the averaging operation on  $\bar{p}$  and  $\bar{u}_i$  fields, and  $p''$ ,  $u''_i$  the pressure and velocity fluctuation respectively.

The residual stress tensor  $\tau_{ij}^{sgs}$ , also know as the sub-grid stress (sgs) tensor is defined as

$$\tau_{ij}^{sgs} = \overline{u_i u_j} - \bar{u}_i \bar{u}_j. \quad (2.4)$$

In this study the dynamic Smagorinsky-Lilly model proposed by Lilly, 1992 is used to modeled the sgs stress tensor. It is approximated by

$$\tau_{ij} = \frac{1}{3} \delta_{ij} \tau_{kk} + 2(C_D \Delta)^2 |\bar{S}| \bar{S}_{ij} \quad (2.5)$$

where  $\delta_{ij} = 1$  if  $i = j$  and zero otherwise,  $C_D$  the Smagorinsky coefficient,  $\Delta$  the filter size, and  $|\bar{S}| = (2\bar{S}_{ij}\bar{S}_{ij})^2$  the magnitude of the stain-rate tensor  $\bar{S}_{ij} = (\partial \bar{u}_i / \partial x_j + \partial \bar{u}_j / \partial x_i) / 2$ . In the original model,  $C_D$  is set as constant, which is not true near the wall and in the flow regions with high shear stresses. Therefore Lilly proposed a dynamic version of the  $C_D$  coefficient

$$C_D = \frac{1}{2} \frac{L_{ij} M_{ij}}{M_{ij}^2} \quad (2.6)$$

with

$$L_{ij} - \frac{1}{3}\delta_{ij}L_{kk} = 2C_D M_{ij} \quad (2.7a)$$

$$M_{ij} = \Delta^2 |\bar{S}| \bar{S}_{ij} - \Delta^2 \overline{|\bar{S}| \bar{S}_{ij}} \quad (2.7b)$$

which allows realistic values of  $C_D$  for wall bounded flow.

In the rest of this paper, the superscript  $\cdot^R$  is used to describe any fields of the REF-LES. In a similar fashion, the superscripts  $\cdot^L$  and  $\cdot^S$  are used for L-LES and S-LES fields respectively.

The S-LES solves a modified set of filtered Navier-Stokes equations, which includes the implicit blending between the coarse-grained  $\bar{u}_i^L$  and the fine-grained  $\bar{u}_i^S$  velocity field. The mass and momentum conservation equations become

$$\frac{\partial \bar{u}_i^S}{\partial x_i} = 0 \quad (2.8a)$$

$$\frac{\partial \bar{u}_i^S}{\partial t} + \frac{\partial \bar{u}_i^S \bar{u}_j^S}{\partial x_j} = -\frac{\partial \bar{p}^S}{\partial x_i} + \nu \frac{\partial^2 \bar{u}_i^S}{\partial x_j \partial x_j} - \frac{\partial \tau_{ij}^S}{\partial x_j} + \frac{w}{\tau_r} (\bar{u}_i^L - \bar{u}_i^S) \quad (2.8b)$$

with  $w \in [0,1]$  the blending factor and  $\tau_r$  the relaxation time. The fourth rhs term acts as a source term and enforces the blending. It acts by correcting the error between the calculated field  $\bar{u}_i^S$  and the target field  $\bar{u}_i^L$ . Higher is the error, stronger is the correction.

## 2.2 LARGE EDDY SIMULATION

### 2.2.1 Filtering operation

#### 2.2.1.1 filtering the physical space

#### 2.2.1.2 filtering the wavenumber space

#### 2.2.1.3 filter width

### 2.2.2 Subgrid stress

## 2.3 TURBULENCE MODELING IN LES



## DISCUSSION

---

### 3.1 FIGURES AND IMAGES

The pillars of the creation taken by the Hubble Space Telescope on [fig.3.1](#).



Figure 3.1: The pillars of the creation.

#### 3.1.1 *Figures and Images in subsection*

On [fig.3.2](#), a view of Buzz Aldrin on the moon.

## DISCUSSION

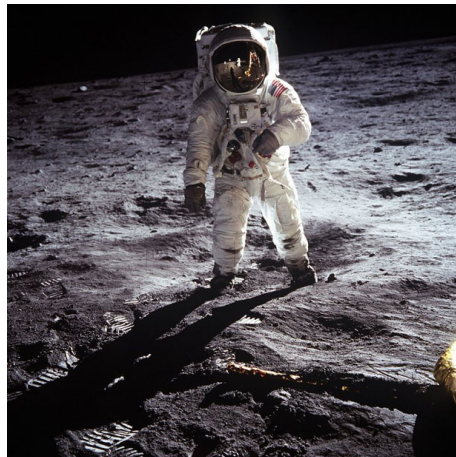


Figure 3.2: Buzz Aldrin on the moon.



## BIBLIOGRAPHY

---

- Lilly, D. K. (1992). "A proposed modification of the Germano subgrid-scale closure method." In: *Physics of Fluids A: Fluid Dynamics* 4.3, p. 633. ISSN: 08998213. DOI: [10.1063/1.858280](https://doi.org/10.1063/1.858280). URL: <http://scitation.aip.org/content/aip/journal/pofa/4/3/10.1063/1.858280>.
- Moeng, C-H. et al. (2007). "Examining Two-Way Grid Nesting for Large Eddy Simulation of the PBL Using the WRF Model." In: *Monthly Weather Review* 135.6, pp. 2295–2311. ISSN: 0027-0644. DOI: [10.1175/MWR3406.1](https://doi.org/10.1175/MWR3406.1). URL: <http://journals.ametsoc.org/doi/abs/10.1175/MWR3406.1>.
- Pope, Stephen (2000). *Turbulent Flows*. Cambridge University Press, p. 773. ISBN: 978-0-521-59886-6. URL: [www.cambridge.org/9780521598866](http://www.cambridge.org/9780521598866).
- Smagorinsky, J. (1963). "General circulation experiments wiht the primitive equations I. The basic experiment." In: *Monthly Weather Review* 91.3, pp. 99–164. ISSN: 0036-8075. DOI: [10.1126/science.27.693.594](https://doi.org/10.1126/science.27.693.594).



## NOTATION

---

### PROBABILITY

---

SYMBOL	MEANING
$P(\cdot)$	probability mass function
$Z$	partition sum; normalization constant of a distribution
$A$	logarithm of the partition sum
$A^*$	conjugate dual of the log partition sum
$\mathbb{E}_P[X]$	expected value of $X$ , w.r.t. distribution $P$
$\text{Cov}_P[X]$	covariance of $X$ , w.r.t. distribution $P$
$D_{KL}(q\ p)$	Kullback-Leibler divergence of distributions $q$ and $p$
$I(p, q)$	mutual information of $p$ and $q$
$H(P)$	entropy of the distribution $P$
$\beta$	inverse temperature in a Gibbs distribution
$\mathbb{I}_{\text{expr}}(x)$	indicator function returning 1 if the Boolean expression $\text{expr}$ involving variable $x$ is true and 0 otherwise.

## Bibliography

### STRUCTURED OUTPUT

SYMBOL	MEANING
$\mathcal{Y}_i$	domain of the $i$ -th output variable
$y_i$	individual output variable, $y_i \in \mathcal{Y}_i$
$\mathcal{Y}$	product space of all the individual output domains
$\mathbf{y}$	all the output variables of an example
$\mathcal{X}$	domain of the input variables
$\mathbf{x}$	all the input variables of an example
$\mathcal{Z}_i$	domain of the $i$ -th hidden output variable
$z_i$	individual hidden output variable, $z_i \in \mathcal{Z}_i$
$\mathcal{Z}$	product space of all individual hidden output domains
$\mathbf{z}$	all the hidden output variables of an example
$\phi(\mathbf{x}, \mathbf{y})$	feature map of an example $(\mathbf{x}, \mathbf{y})$
$\psi(\mathbf{y}'   \mathbf{x}, \mathbf{y})$	feature map difference: $\phi(\mathbf{x}, \mathbf{y}') - \phi(\mathbf{x}, \mathbf{y})$
$\Delta_{\mathbf{y}^*}(\mathbf{y})$	loss when predicting $\mathbf{y}$ instead of $\mathbf{y}^*$
$\mathbf{w}$	(linear) parameters of a structured model
$\ell(\mathbf{w}, \mathbf{x}, \mathbf{y})$	surrogate loss of parameter $\mathbf{w}$ for example $(\mathbf{x}, \mathbf{y})$

### FACTOR GRAPHS AND GRAPHICAL MODELS

SYMBOL	MEANING
$E(\mathbf{y})$	energy of output configuration $\mathbf{y}$
$\theta_c(\mathbf{y}_c)$	potential of factor $c$ and assignment $\mathbf{y}_c$
$\bar{\theta}_c(\mathbf{y}_c)$	negative potential (score) of factor $c$ and assignment $\mathbf{y}_c$
$\mathcal{G}$	graph
$\mathcal{V}$	vertices of a graph
$\mathcal{E}$	edges of a graph
$\mathcal{N}(i)$	neighboring vertices of vertex $i$
$d_i$	degree of the $i$ -th vertex
$\mathcal{FG}$	factor graph
$\mu$	marginal variables
$\mathcal{M}$	marginal polytope
$\mathcal{L}_{\mathcal{G}}$	local marginal polytope for graph $\mathcal{G}$

## ACRONYMS

---

DNS	Direct Numerical Simulation
LES	Large Eddy Simulation
DES	Detached Eddy Simulation
RANS	Reynolds Average Navier Stokes
CFD	Computational Fluid Dynamics



## INDEX

---

Direct Numerical Simulation, [1](#),  
[2](#)

Large Eddy Simulation, [1](#)

Reynolds Average Navier Stokes,  
[2](#)





## CURRICULUM VITAE

---

## COLOPHON

This document was typeset in  $\text{\LaTeX}$  using the typographical look-and-feel `classicthesis`. The bibliography is typeset using `biblatex` with `natbib`.