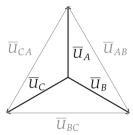
Sistemas Trifásicos Teoría de Circuitos II

Oscar Perpiñán Lamigueiro

- Generadores
- 2 Receptores
- 3 Potencia en Sistemas Trifásicos
- 4 Compensación de Reactiva
- 6 Medida de Potencia en Sistemas Trifásicos
- 6 Conversión de Fuentes Reales
- 7 Estudio generalizado de los sistemas trifásicos

Tensiones de Fase y Línea



Tensiones de **Fase**: U_A , U_B , U_C Tensiones de **Línea**: U_{AB} , U_{BC} , U_{CA}

$$\overline{U}_{AB} = \overline{U}_A - \overline{U}_B$$

$$\overline{U}_{BC} = \overline{U}_B - \overline{U}_C$$

$$\overline{U}_{CA} = \overline{U}_C - \overline{U}_A$$

$$\overline{U}_{AB} + \overline{U}_{BC} + \overline{U}_{CA} = 0$$

Tensiones de Fase y Línea

$$\overline{U}_A = U_f / \theta_f \overline{U}_B = U_f / \theta_f - 120^\circ$$

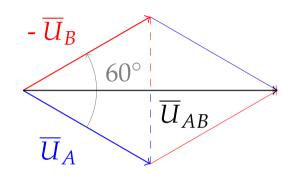
$$\overline{U}_{AB} = \overline{U}_A - \overline{U}_B =$$

$$= U_f / \theta_f - U_f / \theta_f - 120^\circ =$$

$$= U_f / \theta_f + U_f / \theta_f + 60^\circ$$

$$= 2 \cdot U_f \cdot \cos(30) / \theta_f + 30^\circ =$$

$$= \sqrt{3} U_f / \theta_f + 30^\circ$$

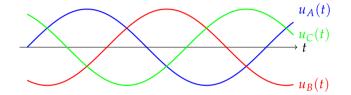


$$U = \sqrt{3} \cdot U_f$$

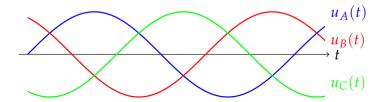
$$\theta_l = \theta_f + 30^\circ$$

Secuencia de Fases

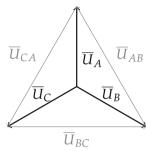
- ▶ Sentido en el que ocurren los máximos de cada fase.
- ► Secuencia de Fases Directa (SFD): ABC



Secuencia de Fases Inversa (SFI): ACB



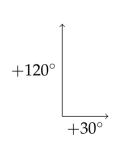
Secuencia de Fases Directa (SFD)

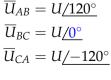


$$\overline{U}_A = \frac{U}{\sqrt{3}} / 90^{\circ}$$

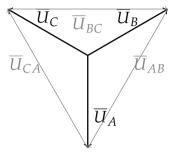
$$\overline{U}_B = \frac{U}{\sqrt{3}} / -30^{\circ}$$

$$\overline{U}_C = \frac{U}{\sqrt{3}} / -150^{\circ}$$





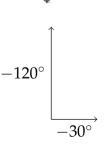
Secuencia de Fases Inversa (SFI)

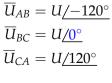


$$\overline{U}_A = \frac{U}{\sqrt{3}} / -90^{\circ}$$

$$\overline{U}_B = \frac{U}{\sqrt{3}} / 30^{\circ}$$

$$\overline{U}_C = \frac{U}{\sqrt{3}} / 150^{\circ}$$





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Tipos de Receptores

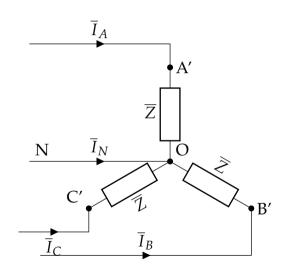
Conexión

- Estrella (punto común) Y
- ► Triángulo △

Impedancias

- **Equilibrado** (las tres impedancias son idénticas en módulo y fase).
- **▶** Desequilibrado

Receptor en Estrella Equilibrado



$$\bar{I}_{A} = \frac{\overline{U}_{A}}{\overline{Z}} = \frac{U_{f}}{Z} / \pm 90^{\circ} - \varphi$$

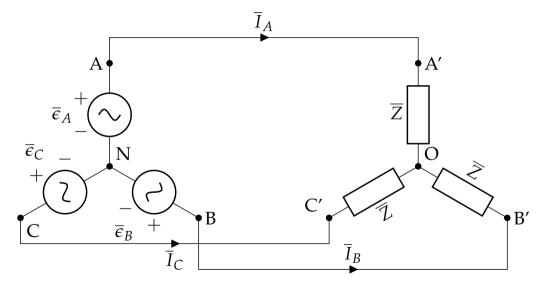
$$\bar{I}_{B} = \frac{\overline{U}_{B}}{\overline{Z}} = \frac{U_{f}}{Z} / \mp 30^{\circ} - \varphi$$

$$\bar{I}_{C} = \frac{\overline{U}_{C}}{\overline{Z}} = \frac{U_{f}}{Z} / \mp 150^{\circ} - \varphi$$

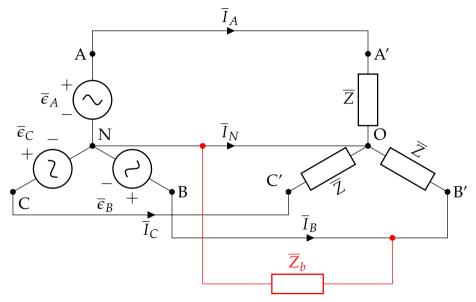
$$|\bar{I}_A| = |\bar{I}_B| = |\bar{I}_C| = \frac{U_f}{Z}$$

$$\bar{I}_A + \bar{I}_B + \bar{I}_C + \bar{I}_N = 0$$
$$\bar{I}_A + \bar{I}_B + \bar{I}_C = 0 \rightarrow \boxed{\bar{I}_N = 0}$$

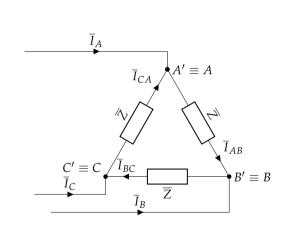
Receptor en Estrella Equilibrado



Receptor en Estrella con Carga Monofásica



Receptor en Triángulo Equilibrado

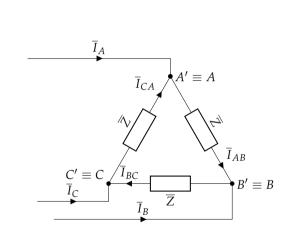


$$ar{I}_{AB} = rac{\overline{U}_{AB}}{\overline{Z}} = rac{U}{Z} / \pm 120^\circ - arphi$$
 $ar{I}_{BC} = rac{\overline{U}_{BC}}{\overline{Z}} = rac{U}{Z} / 0 - arphi$
 $ar{I}_{CA} = rac{\overline{U}_{CA}}{\overline{Z}} = rac{U}{Z} / \mp 120^\circ - arphi$
 $ar{I}_{AB} + ar{I}_{BC} + ar{I}_{CA} = 0$
The de Fase:

Corriente de Fase:

$$\boxed{I_f = |\bar{I}_{AB}| = |\bar{I}_{BC}| = |\bar{I}_{CA}| = \frac{U}{Z}}$$

Receptor en Triángulo Equilibrado



$$\bar{I}_A = \bar{I}_{AB} - \bar{I}_{CA} = \sqrt{3} \cdot \frac{U}{Z} / \pm 90^\circ - \varphi$$

$$\bar{I}_B = \bar{I}_{BC} - \bar{I}_{AB} = \sqrt{3} \cdot \frac{U}{Z} / \mp 30^\circ - \varphi$$

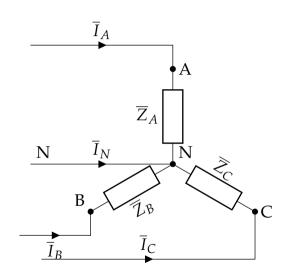
$$\bar{I}_C = \bar{I}_{CA} - \bar{I}_{BC} = \sqrt{3} \cdot \frac{U}{Z} / \mp 150^\circ - \varphi$$

Corriente de Línea:

$$I = |\bar{I}_A| = |\bar{I}_B| = |\bar{I}_C| = \sqrt{3} \cdot \frac{U}{Z}$$

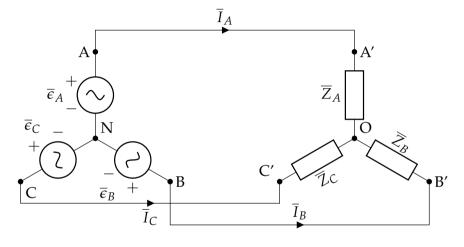
$$I = \sqrt{3} \cdot I_f$$

Receptor en Estrella Desequilibrado con Neutro



$$\bar{I}_A = \frac{\overline{U}_A}{\overline{Z}_A}
\bar{I}_B = \frac{\overline{U}_B}{\overline{Z}_B}
\bar{I}_C = \frac{\overline{U}_C}{\overline{Z}_C}
\bar{I}_A + \bar{I}_B + \bar{I}_C + \bar{I}_N = 0
\bar{I}_A + \bar{I}_B + \bar{I}_C \neq 0 \rightarrow |\bar{I}_N \neq 0|$$

Receptor en Estrella Desequilibrado sin Neutro



$$\overline{U}_N \neq \overline{U}_O$$

Método del desplazamiento del neutro

Ecuaciones del receptor:

$$\overline{U}_{A'O} = \overline{I}_A \cdot \overline{Z}_A$$

$$\overline{U}_{B'O} = \overline{I}_B \cdot \overline{Z}_B$$

$$\overline{U}_{C'O} = \overline{I}_C \cdot \overline{Z}_C$$

Ecuación del nudo O:

$$\bar{I}_A + \bar{I}_B + \bar{I}_C = 0$$

Método del desplazamiento del neutro

Relacionamos las tensiones en el receptor con las tensiones del generador:

$$\begin{aligned} \overline{U}_{A'O} &= \overline{U}_{AN} - \overline{U}_{ON} \\ \overline{U}_{B'O} &= \overline{U}_{BN} - \overline{U}_{ON} \\ \overline{U}_{C'O} &= \overline{U}_{CN} - \overline{U}_{ON} \end{aligned}$$

Despejamos las corrientes teniendo en cuenta estas relaciones:

$$ar{I}_A = rac{\overline{U}_{AN} - \overline{U}_{ON}}{\overline{Z}_A}$$
 $ar{I}_B = rac{\overline{U}_{BN} - \overline{U}_{ON}}{\overline{Z}_B}$
 $ar{I}_C = rac{\overline{U}_{CN} - \overline{U}_{ON}}{\overline{Z}_C}$

Método del desplazamiento del neutro

Finalmente, usando la ecuación del nudo O despejamos la tensión U_{ON} (tensión de desplazamiento del neutro)*:

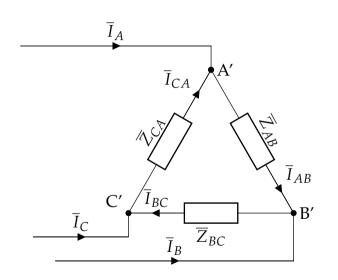
$$\overline{U}_{ON} = \frac{\overline{U}_{AN} \cdot \overline{Y}_A + \overline{U}_{BN} \cdot \overline{Y}_B + \overline{U}_{CN} \cdot \overline{Y}_C}{\overline{Y}_A + \overline{Y}_B + \overline{Y}_C}$$

Una vez calculada esta tensión \overline{U}_{ON} se pueden calcular las corrientes de línea:

$$\begin{split} \overline{I}_A &= (\overline{U}_{AN} - \overline{U}_{ON}) \cdot \overline{Y}_A \\ \overline{I}_B &= (\overline{U}_{BN} - \overline{U}_{ON}) \cdot \overline{Y}_B \\ \overline{I}_C &= (\overline{U}_{CN} - \overline{U}_{ON}) \cdot \overline{Y}_C \end{split}$$

^{*}Se puede llegar a este mismo resultado aplicando el teorema de Millman.

Receptor en Triángulo Desequilibrado

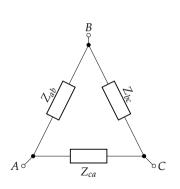


$$ar{I}_{AB} = rac{U_{AB}}{\overline{Z}_{AB}}$$
 $ar{I}_{BC} = rac{\overline{U}_{BC}}{\overline{Z}_{BC}}$
 $ar{I}_{CA} = rac{\overline{U}_{CA}}{\overline{Z}_{CA}}$

$$\begin{split} \bar{I}_A &= \bar{I}_{AB} - \bar{I}_{CA} \\ \bar{I}_B &= \bar{I}_{BC} - \bar{I}_{AB} \\ \bar{I}_C &= \bar{I}_{CA} - \bar{I}_{BC} \end{split}$$

Transformación de receptores

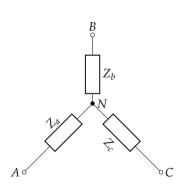
Triángulo a Estrella



$$\overline{Z}_a = \frac{\overline{Z}_{ab} \cdot \overline{Z}_{ca}}{\overline{Z}_{ab} + \overline{Z}_{bc} + \overline{Z}_{ca}}$$

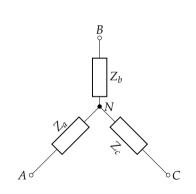
$$\overline{Z}_b = \frac{\overline{Z}_{bc} \cdot \overline{Z}_{ab}}{\overline{Z}_{ab} + \overline{Z}_{bc} + \overline{Z}_{ca}}$$

$$\overline{Z}_c = \frac{\overline{Z}_{ca} \cdot \overline{Z}_{bc}}{\overline{Z}_{ab} + \overline{Z}_{bc} + \overline{Z}_{ca}}$$



Transformación de receptores

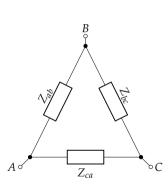
Estrella a Triángulo



$$\overline{Y}_{ab} = \frac{\overline{Y}_a \overline{Y}_b}{\overline{Y}_a + \overline{Y}_b + \overline{Y}_c}$$

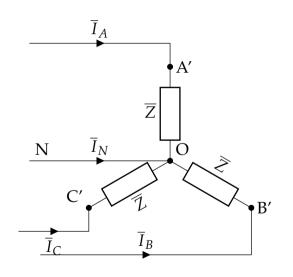
$$\overline{Y}_{bc} = \frac{\overline{Y}_b \overline{Y}_c}{\overline{Y}_a + \overline{Y}_b + \overline{Y}_c}$$

$$\overline{Y}_{ca} = \frac{\overline{Y}_c \overline{Y}_a}{\overline{Y}_a + \overline{Y}_b + \overline{Y}_c}$$



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Receptor en Estrella Equilibrado



$$P = 3 \cdot P_Z = 3 \cdot U_Z I_Z \cos(\varphi)$$
$$Q = 3 \cdot Q_Z = 3 \cdot U_Z I_Z \sin(\varphi)$$

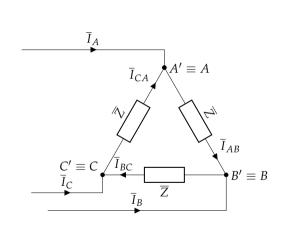
$$I_Z = I$$
$$U_Z = U_F$$

$$P = 3U_F I \cos(\varphi) = \sqrt{3}UI \cos(\varphi)$$

$$Q = 3U_F I \sin(\varphi) = \sqrt{3}UI \sin(\varphi)$$

$$S = \sqrt{P^2 + Q^2} = \sqrt{3}UI$$

Receptor en Triángulo Equilibrado



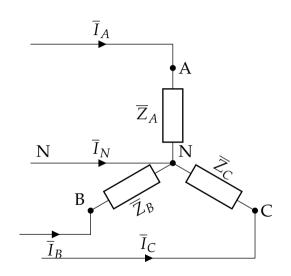
$$P = 3 \cdot P_Z = 3 \cdot U_Z I_Z \cos(\varphi)$$
$$Q = 3 \cdot Q_Z = 3 \cdot U_Z I_Z \sin(\varphi)$$

$$I_Z = I_F$$
$$U_Z = U$$

$$P = 3UI_F \cos(\varphi) = \sqrt{3}UI \cos(\varphi)$$

 $Q = 3UI_F \sin(\varphi) = \sqrt{3}UI \sin(\varphi)$
 $S = \sqrt{P^2 + Q^2} = \sqrt{3}UI$

Receptor en Estrella Desequilibrado

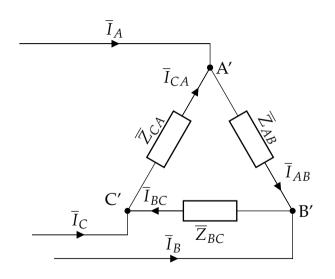


$$P = P_A + P_B + P_C$$

$$Q = Q_A + Q_B + Q_C$$

$$\overline{S} = P + jQ$$

Receptor en Triángulo Desequilibrado



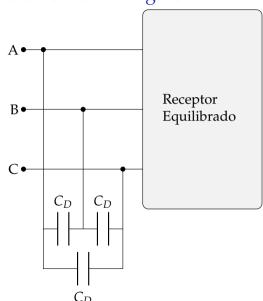
$$P = P_{AB} + P_{BC} + P_{CA}$$

$$Q = Q_{AB} + Q_{BC} + Q_{CA}$$

$$\overline{S} = P + jQ$$

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Conexión en Triángulo



$$Q = P \tan \varphi$$

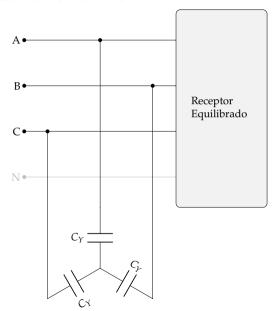
$$Q' = P \tan \varphi' =$$

$$= Q - Q_c$$

$$Q_c = 3 \cdot \omega C_{\triangle} \cdot U^2$$

$$C_{\triangle} = \frac{P(\tan \varphi - \tan \varphi')}{3\omega U^2}$$

Conexión en Estrella



$$Q = P \tan \varphi$$

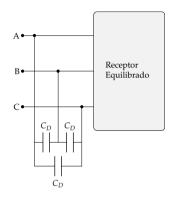
$$Q' = P \tan \varphi' =$$

$$= Q - Q_c$$

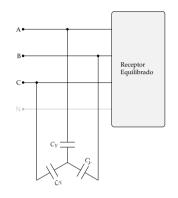
$$Q_c = 3 \cdot \omega C_Y \cdot U_f^2$$

$$C_Y = \frac{P(\tan \varphi - \tan \varphi')}{\omega U^2}$$

Comparación Estrella-Triángulo



$$C_{\triangle} = \frac{P(\tan \varphi - \tan \varphi')}{3\omega U^2}$$

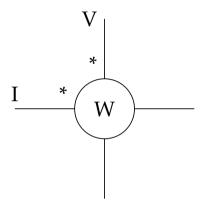


$$C_{Y} = \frac{P(\tan \varphi - \tan \varphi')}{\omega U^{2}}$$

Dado que $C_Y = 3 \cdot C_{\triangle}$ la configuración recomendada es triángulo.

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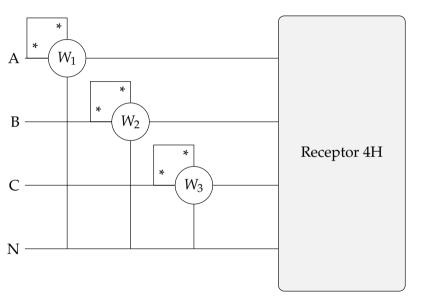
Recordatorio: vatímetro



Vatímetro: equipo de medida de 4 terminales (1 par para tensión, 1 par para corriente)

$$W = \Re(\overline{U} \cdot \overline{I}^*)$$

Sistema de 4 Hilos



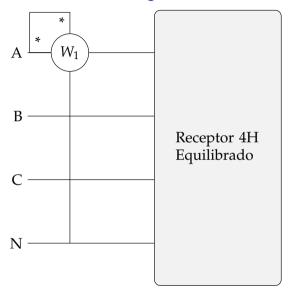
$$W_1 = \Re(\overline{U}_A \cdot \overline{I}_A^*) = P_A$$

$$W_2 = \Re(\overline{U}_B \cdot \overline{I}_B^*) = P_B$$

$$W_3 = \Re(\overline{U}_C \cdot \overline{I}_C^*) = P_C$$

 $P = W_1 + W_2 + W_3$

Sistema de 4 Hilos Equilibrado



$$P_A = P_B = P_C$$

$$P=3\cdot W_1$$

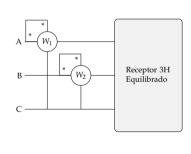
Sistema de 3 Hilos Equilibrado (SFD)

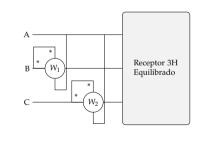
 $(ABC) :: A \triangleright B \triangleright C \Longrightarrow \{AB, BC, CA\}$

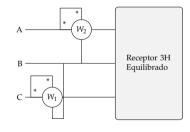
$$W_1 = UI\cos(\varphi - 30^\circ)$$

$$W_2 = UI\cos(\varphi + 30^\circ)$$

$$P = W_1 + W_2$$
$$O = \sqrt{3}(W_1 - W_2)$$







 $W_1 : AC \notin SFD$ $W_2 : BC \in SFD$

 $W_1: BA \notin SFD$ $W_2: CA \in SFD$ $W_1: CB \notin SFD$ $W_2: AB \in SFD$

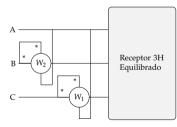
Sistema de 3 Hilos Equilibrado (SFI)

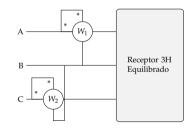
 $(ACB) :: A \triangleright C \triangleright B \Longrightarrow \{AC, CB, BA\}$

$$W_1 = UI\cos(\varphi - 30^\circ)$$
$$W_2 = UI\cos(\varphi + 30^\circ)$$

$$P = W_1 + W_2$$
$$O = \sqrt{3}(W_1 - W_2)$$





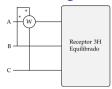


 $W_1 : BC \notin SFI$ $W_2 : AC \in SFI$

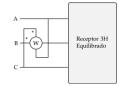
 $W_1 : CA \notin SFI$ $W_2 : BA \in SFI$

 $W_1: AB \notin SFI$ $W_2: CB \in SFI$

Conexiones para medida de reactiva



$$W=\Re(\overline{U}_{BC}\cdot\overline{I}_A^*)$$

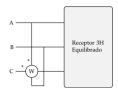


$$W=\Re(\overline{U}_{CA}\cdot\overline{I}_B^*)$$

$$CA \in SFD$$

 $CA \notin SFI$

$$SFD \to W = \frac{Q}{\sqrt{3}}$$
$$SFI \to W = -\frac{Q}{\sqrt{3}}$$

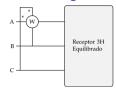


$$W=\Re(\overline{U}_{AB}\cdot\overline{I}_C^*)$$

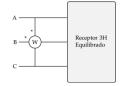
$$AB \in SFD$$

 $AB \notin SFI$

Conexiones para medida de reactiva



$$W=\Re(\overline{U}_{CB}\cdot\overline{I}_A^*)$$



$$W=\Re(\overline{U}_{AC}\cdot\overline{I}_B^*)$$

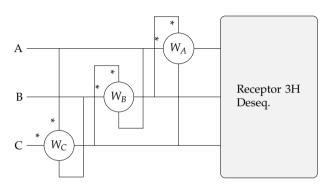
$$SFD \to W = -\frac{Q}{\sqrt{3}}$$
$$SFI \to W = \frac{Q}{\sqrt{3}}$$

$$W=\Re(\overline{U}_{BA}\cdot\overline{I}_C^*)$$

$$BA \notin SFD$$

 $BA \in SFI$

Medida de la reactiva con receptor desequilibrado



$$W_A = \Re(\overline{U}_{BC} \cdot \overline{I}_A^*)$$

$$W_B = \Re(\overline{U}_{CA} \cdot \overline{I}_B^*)$$

$$W_C = \Re(\overline{U}_{AB} \cdot \overline{I}_C^*)$$

$$\overline{U}_{AB} = \pm \sqrt{3} \cdot \overline{U}_C \cdot e^{j\pi/2}$$

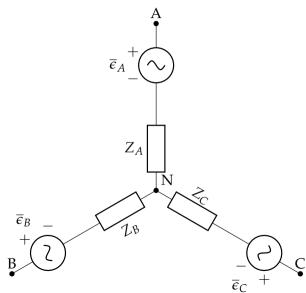
$$\overline{U}_{BC} = \pm \sqrt{3} \cdot \overline{U}_A \cdot e^{j\pi/2}$$

$$\overline{U}_{CA} = \pm \sqrt{3} \cdot \overline{U}_B \cdot e^{j\pi/2}$$

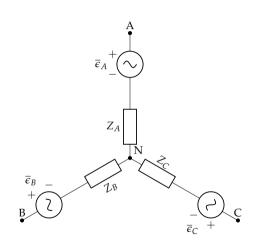
$$W_A + W_B + W_C = \pm Q/\sqrt{3}$$

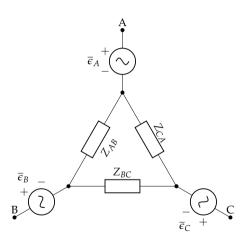
- Generadores
- 2 Receptores
- 3 Potencia en Sistemas Trifásicos
- 4 Compensación de Reactiva
- 6 Medida de Potencia en Sistemas Trifásicos
- 6 Conversión de Fuentes Reales
- ② Estudio generalizado de los sistemas trifásicos

Estrella a Triángulo

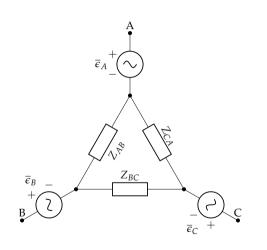


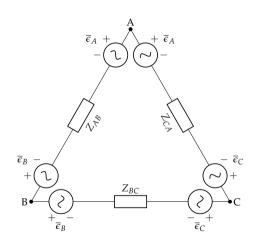
Transformamos impedancia



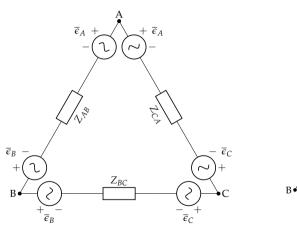


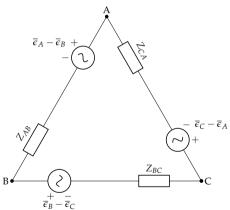
Aplicamos movilidad de fuentes



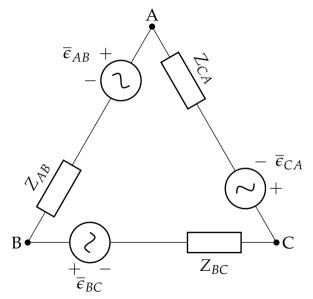


Asociamos fuentes

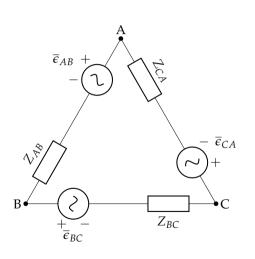


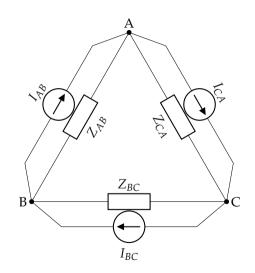


Triángulo a Estrella

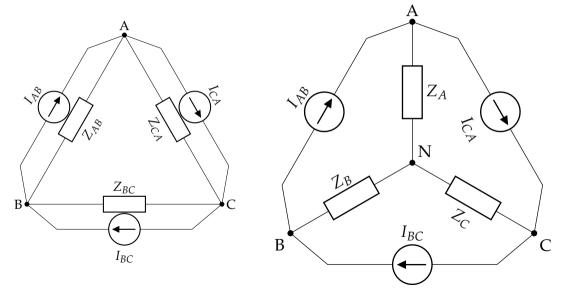


Transformamos fuentes

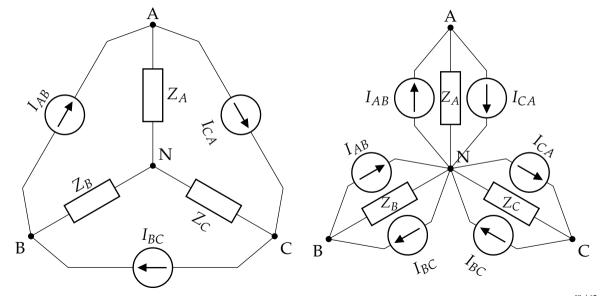




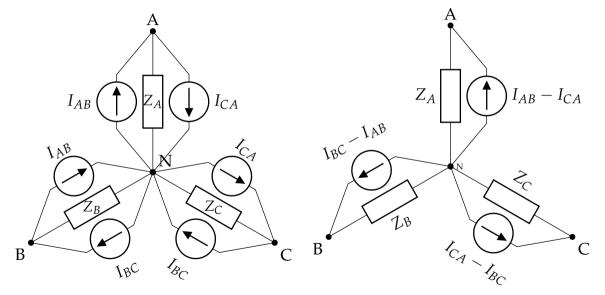
Transformamos impedancias



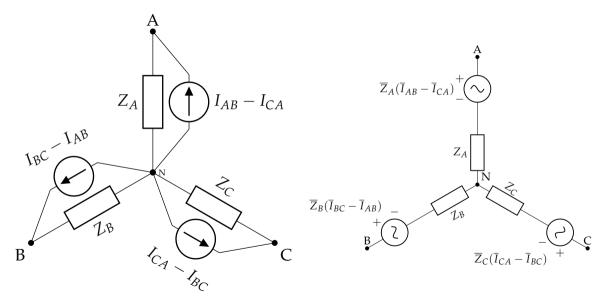
Aplicamos movilidad de fuentes



Asociamos fuentes

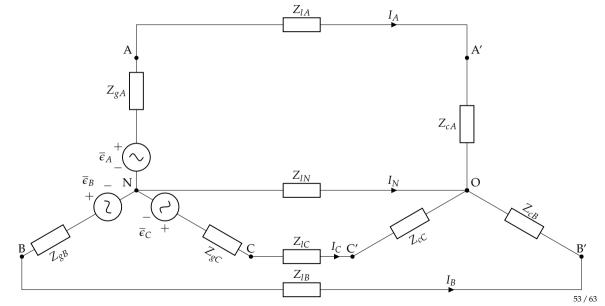


Transformamos fuentes

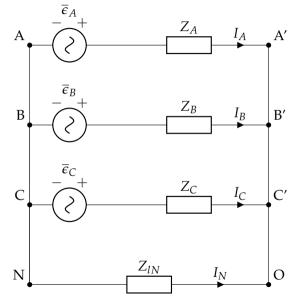


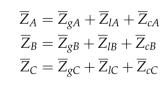
- Generadores
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Planteamiento del sistema

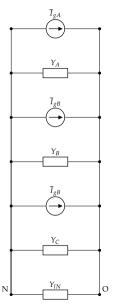


Agrupamos impedancias de generador, línea y receptor





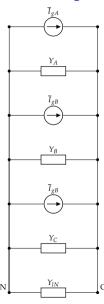
Conversión de fuentes

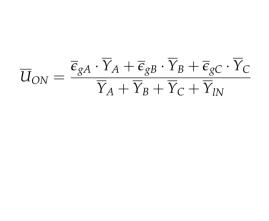


$$\begin{split} \bar{I}_{gA} &= \overline{\epsilon}_A \cdot \overline{Y}_A \\ \bar{I}_{gB} &= \overline{\epsilon}_B \cdot \overline{Y}_B \\ \bar{I}_{gC} &= \overline{\epsilon}_C \cdot \overline{Y}_C \end{split}$$

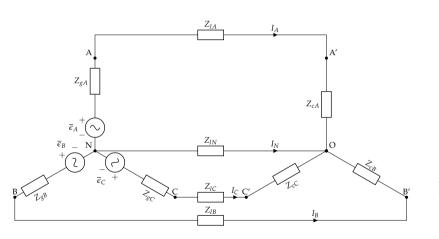
$$\overline{U}_{ON} = \frac{\overline{I}_{gA} + \overline{I}_{gB} + \overline{I}_{gC}}{\overline{Y}_A + \overline{Y}_B + \overline{Y}_C + \overline{Y}_{lN}}$$

Tensión de desplazamiento del neutro





Cálculo de corrientes



$$\bar{I}_{A} = \frac{\overline{\epsilon}_{A} - \overline{U}_{ON}}{\overline{Z}_{gA} + \overline{Z}_{lA} + \overline{Z}_{cA}}$$

$$\bar{I}_{B} = \frac{\overline{\epsilon}_{B} - \overline{U}_{ON}}{\overline{Z}_{gB} + \overline{Z}_{lB} + \overline{Z}_{cB}}$$

$$\bar{I}_{C} = \frac{\overline{\epsilon}_{C} - \overline{U}_{ON}}{\overline{Z}_{gC} + \overline{Z}_{lC} + \overline{Z}_{cC}}$$

$$\bar{I}_{N} = -\overline{I}_{A} - \overline{I}_{B} - \overline{I}_{C}$$

Aplicación a sistemas equilibrados

La suma de las fuerzas electromotrices es 0

$$\overline{\epsilon}_{gA} + \overline{\epsilon}_{gB} + \overline{\epsilon}_{gC} = 0$$

Las tres impedancias son iguales

$$\overline{Y}_A = \overline{Y}_B = \overline{Y}_C$$

Por tanto,

$$\overline{U}_{ON} = \frac{3 \cdot \overline{Y} \cdot \left(\overline{\epsilon}_{gA} + \overline{\epsilon}_{gB} + \overline{\epsilon}_{gC}\right)}{3 \cdot \overline{Y} + \overline{Y}_{lN}} = 0$$

Este resultado es independiente de la existencia del neutro y de su impedancia.

Aplicación a sistemas desequilibrados

Sistemas con neutro de impedancia no nula

$$\overline{U}_{ON} = \frac{\overline{\epsilon}_{gA} \cdot \overline{Y}_A + \overline{\epsilon}_{gB} \cdot \overline{Y}_B + \overline{\epsilon}_{gC} \cdot \overline{Y}_C}{\overline{Y}_A + \overline{Y}_B + \overline{Y}_C + \overline{Y}_{IN}}$$

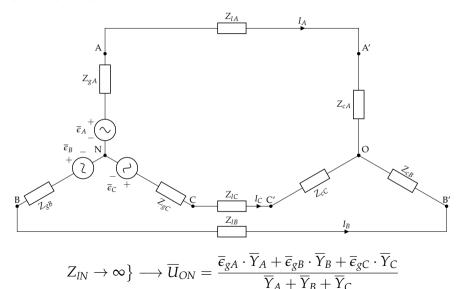
▶ Sistemas con neutro de impedancia nula ($\overline{Z}_{lN} = 0$, $\overline{Y}_{lN} \to \infty$)

$$\overline{U}_{ON} = \frac{\overline{\epsilon}_{gA} \cdot \overline{Y}_A + \overline{\epsilon}_{gB} \cdot \overline{Y}_B + \overline{\epsilon}_{gC} \cdot \overline{Y}_C}{\overline{Y}_A + \overline{Y}_B + \overline{Y}_C + \overline{Y}_{lN}} = 0$$

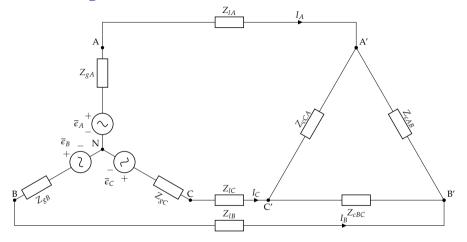
Sistemas sin neutro ($\overline{Z}_{lN} \to \infty$, $\overline{Y}_{lN} = 0$)

$$\overline{U}_{ON} = \frac{\overline{\epsilon}_{gA} \cdot \overline{Y}_A + \overline{\epsilon}_{gB} \cdot \overline{Y}_B + \overline{\epsilon}_{gC} \cdot \overline{Y}_C}{\overline{Y}_A + \overline{Y}_B + \overline{Y}_C}$$

Sistema sin neutro

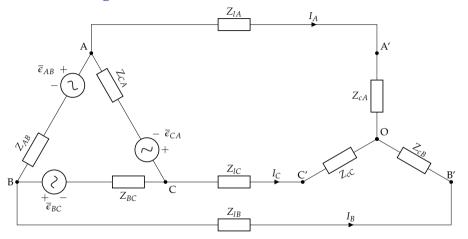


Receptor en triángulo



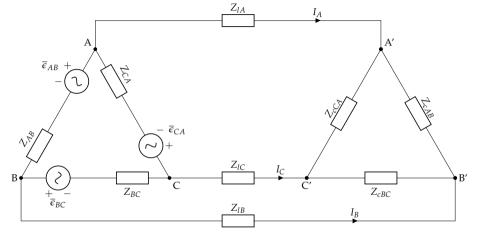
$$\left. \begin{array}{l} \text{Transformación de Receptor} \\ Z_{lN} \rightarrow \infty \end{array} \right\} \longrightarrow \overline{U}_{ON} = \frac{\overline{\epsilon}_{gA} \cdot \overline{Y}_A + \overline{\epsilon}_{gB} \cdot \overline{Y}_B + \overline{\epsilon}_{gC} \cdot \overline{Y}_C}{\overline{Y}_A + \overline{Y}_B + \overline{Y}_C} \end{array}$$

Generador en triángulo



$$\left. \begin{array}{l} \text{Transformación de Generador} \\ Z_{IN} \rightarrow \infty \end{array} \right\} \longrightarrow \overline{U}_{ON} = \frac{\overline{\epsilon}_{gA} \cdot \overline{Y}_A + \overline{\epsilon}_{gB} \cdot \overline{Y}_B + \overline{\epsilon}_{gC} \cdot \overline{Y}_C}{\overline{Y}_A + \overline{Y}_B + \overline{Y}_C} \end{array}$$

Generador y Receptor en triángulo



Transformación de Generador Transformación de Receptor $Z_{IN} \rightarrow \infty$

$$\left. \begin{array}{l} \text{eptor} \\ \end{array} \right\} \longrightarrow \overline{U}_{ON} = \frac{\overline{\epsilon}_{gA} \cdot \overline{Y}_A + \overline{\epsilon}_{gB} \cdot \overline{Y}_B + \overline{\epsilon}_{gC} \cdot \overline{Y}_C}{\overline{Y}_A + \overline{Y}_B + \overline{Y}_C} \right.$$