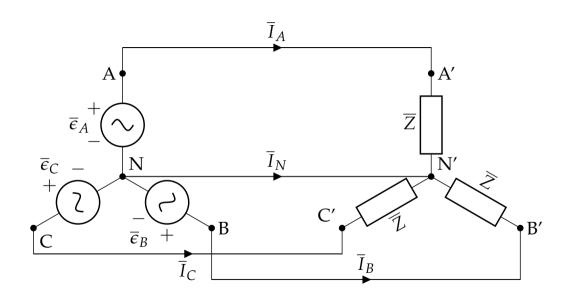
Sistemas Trifásicos

Oscar Perpiñán Lamigueiro

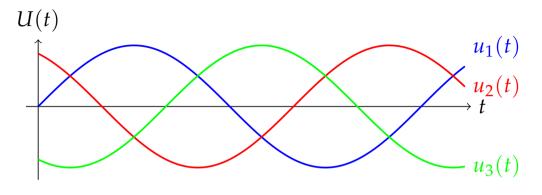
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Motivación de los sistemas trifásicos

- ▶ En un sistema trifásico la potencia instantánea es constante, evitando vibraciones y esfuerzos en las máquinas. (*La potencia instantánea de un sistema monofásico es pulsante*.)
- La masa de conductor necesaria en un sistema trifásico es un 25% inferior que en un monofásico para transportar la misma potencia.

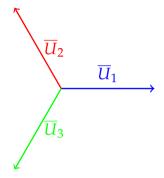
Ondas Trifásicas



$$u_1(t) = U_0 \cos(\omega t)$$

 $u_2(t) = U_0 \cos(\omega t + 2\pi/3)$
 $u_3(t) = U_0 \cos(\omega t - 2\pi/3)$

Fasores de un sistema trifásico



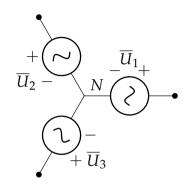
$$\overline{U}_1 = U/\underline{0}$$

$$\overline{U}_2 = U/\underline{2\pi/3}$$

$$\overline{U}_3 = U/\underline{-2\pi/3}$$

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Conexión



$$u_1(t) = U_0 \cos(\omega t)$$

$$\overline{U}_1 = U/0$$

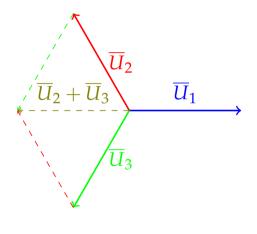
$$u_2(t) = U_0 \cos(\omega t + 2\pi/3)$$

$$\overline{U}_2 = U/2\pi/3$$

$$\overline{U}_3 = U/-2\pi/3$$

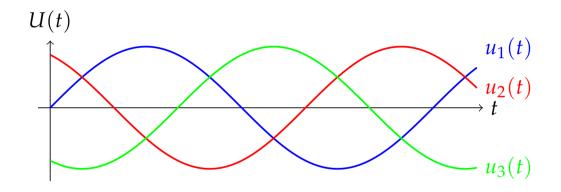
$$\overline{U}_3 = U/-2\pi/3$$

Las tensiones suman 0



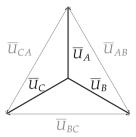
$$\overline{U}_1 + \overline{U}_2 + \overline{U}_3 = 0$$

Las tensiones suman 0



$$u_1(t) + u_2(t) + u_3(t) = 0$$

Tensiones de Fase y Línea



Tensiones de **Fase**: U_A , U_B , U_C Tensiones de **Línea**: U_{AB} , U_{BC} , U_{CA}

$$\overline{U}_{AB} = \overline{U}_A - \overline{U}_B$$

$$\overline{U}_{BC} = \overline{U}_B - \overline{U}_C$$

$$\overline{U}_{CA} = \overline{U}_C - \overline{U}_A$$

$$\overline{U}_{AB} + \overline{U}_{BC} + \overline{U}_{CA} = 0$$

Tensiones de Fase y Línea

$$\overline{U}_A = U_f / \theta_f \overline{U}_B = U_f / \theta_f - 120^\circ$$

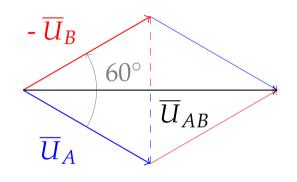
$$\overline{U}_{AB} = \overline{U}_A - \overline{U}_B =$$

$$= U_f / \underline{\theta_f} - U_f / \underline{\theta_f} - 120^\circ =$$

$$= U_f / \underline{\theta_f} + U_f / \underline{\theta_f} + 60^\circ$$

$$= 2 \cdot U_f \cdot \cos(30) / \underline{\theta_f} + 30^\circ =$$

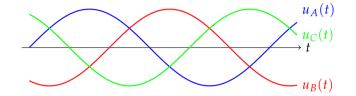
$$= \sqrt{3} U_f / \underline{\theta_f} + 30^\circ$$



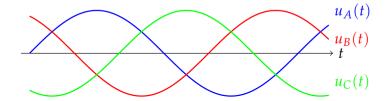
$$U = \sqrt{3} \cdot U_f$$
$$\theta_l = \theta_f + 30^\circ$$

Secuencia de Fases

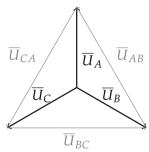
- ▶ Sentido en el que ocurren los máximos de cada fase.
- ► Secuencia de Fases Directa (SFD): ABC



Secuencia de Fases Inversa (SFI): ACB



Secuencia de Fases Directa (SFD)

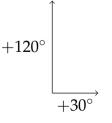


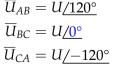
$$\overline{U}_A = \frac{U}{\sqrt{3}} \underline{/90^{\circ}}$$

$$\overline{U}_B = \frac{U}{\sqrt{3}} \underline{/-30^{\circ}}$$

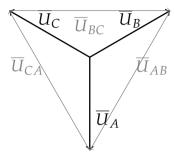
$$\overline{U}_C = \frac{U}{\sqrt{3}} \underline{/-150^{\circ}}$$

$$\frac{I}{\overline{3}}/-150$$





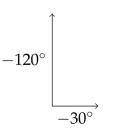
Secuencia de Fases Inversa (SFI)

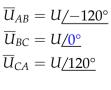


$$\overline{U}_A = \frac{U}{\sqrt{3}} / -90^{\circ}$$

$$\overline{U}_B = \frac{U}{\sqrt{3}} / 30^{\circ}$$

$$\overline{U}_C = \frac{U}{\sqrt{3}} / 150^{\circ}$$





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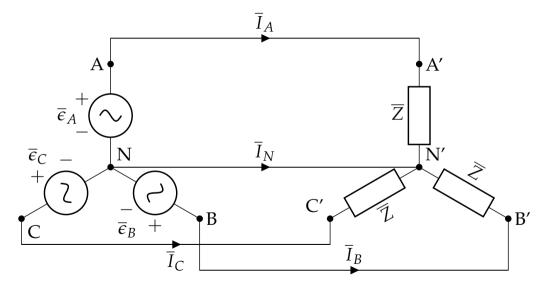
Tipos de Receptores

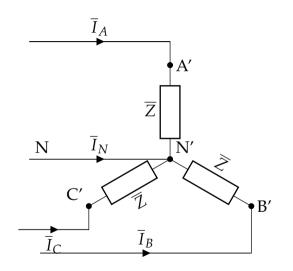
Conexión

- **Estrella** (punto común) Y
- ► Triángulo △

Impedancias

- **Equilibrado** (las tres impedancias son idénticas en módulo y fase).
- Desequilibrado





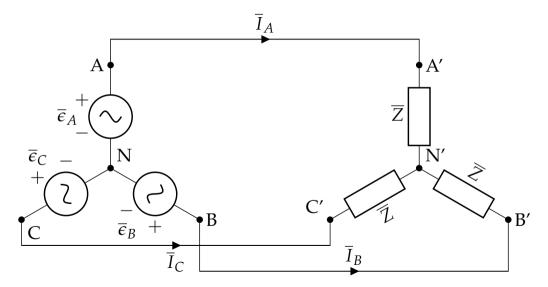
$$\bar{I}_A = \frac{\overline{U}_A}{\overline{Z}} = \frac{U_f}{Z} / \pm 90^\circ - \theta$$

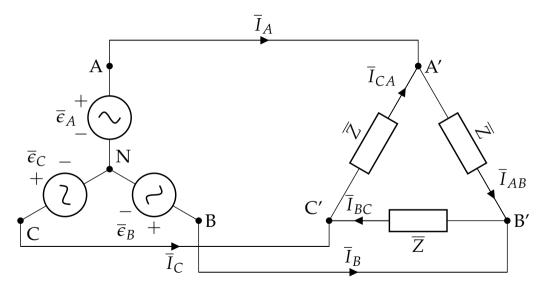
$$\bar{I}_B = \frac{\overline{U}_B}{\overline{Z}} = \frac{U_f}{Z} / \mp 30^\circ - \theta$$

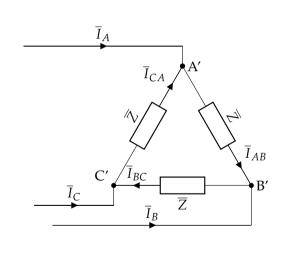
$$\bar{I}_C = \frac{\overline{U}_C}{\overline{Z}} = \frac{U_f}{Z} / \mp 150^\circ - \theta$$

$$|\bar{I}_A| = |\bar{I}_B| = |\bar{I}_C| = \frac{U_f}{Z}$$

$$\bar{I}_A + \bar{I}_B + \bar{I}_C + \bar{I}_N = 0$$
$$\bar{I}_A + \bar{I}_B + \bar{I}_C = 0 \rightarrow \boxed{\bar{I}_N = 0}$$



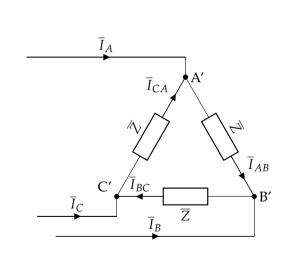




$$ar{I}_{AB} = rac{\overline{U}_{AB}}{\overline{Z}} = rac{U}{Z}/\pm 120^\circ - heta$$
 $ar{I}_{BC} = rac{\overline{U}_{BC}}{\overline{Z}} = rac{U}{Z}/0 - heta$
 $ar{I}_{CA} = rac{\overline{U}_{CA}}{\overline{Z}} = rac{U}{Z}/\mp 120^\circ - heta$
Interde Fase:

Corriente de Fase:

$$\boxed{I_f = |\bar{I}_{AB}| = |\bar{I}_{BC}| = |\bar{I}_{CA}| = \frac{U}{Z}}$$



$$\bar{I}_A = \bar{I}_{AB} - \bar{I}_{CA} = \sqrt{3} \cdot \frac{U}{Z} / \pm 90^\circ - \theta$$

$$\bar{I}_B = \bar{I}_{BC} - \bar{I}_{AB} = \sqrt{3} \cdot \frac{U}{Z} / \mp 30^\circ - \theta$$

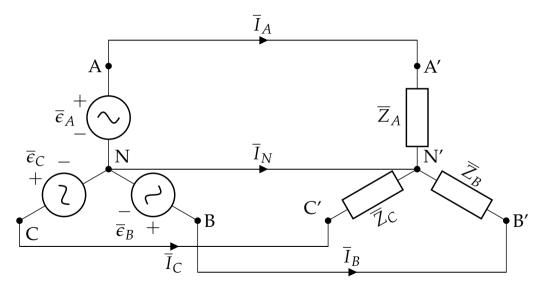
$$\bar{I}_C = \bar{I}_{CA} - \bar{I}_{BC} = \sqrt{3} \cdot \frac{U}{Z} / \mp 150^\circ - \theta$$

Corriente de Línea:

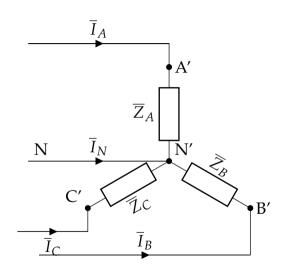
$$\boxed{I = |\bar{I}_A| = |\bar{I}_B| = |\bar{I}_C| = \sqrt{3} \cdot \frac{U}{Z}}$$

$$\boxed{I = \sqrt{3} \cdot I_f}$$

Receptor en Estrella Desequilibrado con Neutro

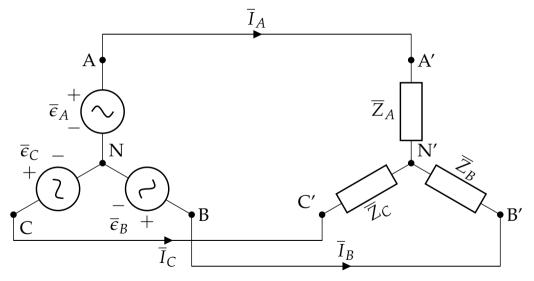


Receptor en Estrella Desequilibrado con Neutro

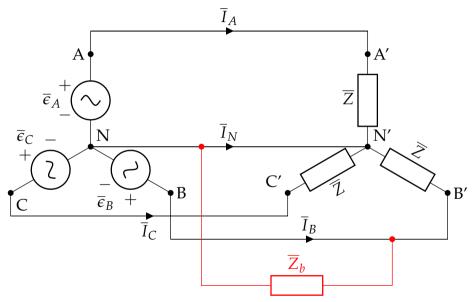


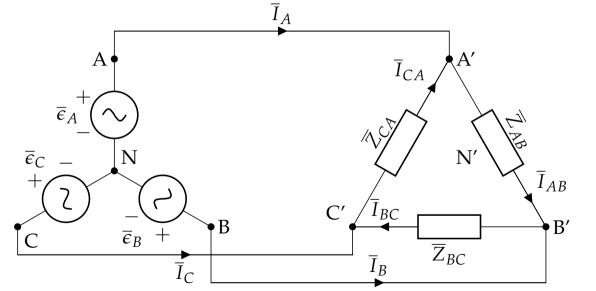
$$\bar{I}_A = \frac{\overline{U}_A}{\overline{Z}_A}
\bar{I}_B = \frac{\overline{U}_B}{\overline{Z}_B}
\bar{I}_C = \frac{\overline{U}_C}{\overline{Z}_C}
\bar{I}_A + \bar{I}_B + \bar{I}_C + \bar{I}_N = 0
\bar{I}_A + \bar{I}_B + \bar{I}_C \neq 0 \rightarrow \overline{I}_N \neq 0$$

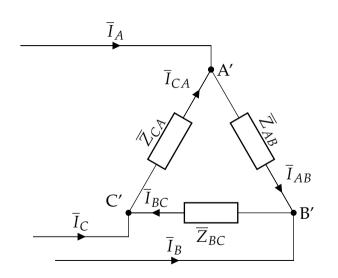
Receptor en Estrella Desequilibrado sin Neutro



Receptor en Estrella con Carga Monofásica







$$\bar{I}_{AB} = \frac{\overline{U}_{AB}}{\overline{Z}_{AB}}$$

$$\bar{I}_{BC} = \frac{\overline{U}_{BC}}{\overline{Z}_{BC}}$$

$$\bar{I}_{CA} = \frac{\overline{U}_{CA}}{\overline{Z}_{CA}}$$

$$\begin{split} \overline{I}_A &= \overline{I}_{AB} - \overline{I}_{CA} \\ \overline{I}_B &= \overline{I}_{BC} - \overline{I}_{AB} \\ \overline{I}_C &= \overline{I}_{CA} - \overline{I}_{BC} \end{split}$$

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Potencia Instantánea en Sistemas Equilibrados

$$\begin{split} u_{A}(t) &= \sqrt{2} U_{f} \cos(\omega t + 90^{\circ}) \\ u_{B}(t) &= \sqrt{2} U_{f} \cos(\omega t - 30^{\circ}) \\ u_{C}(t) &= \sqrt{2} U_{f} \cos(\omega t - 150^{\circ}) \\ i_{A}(t) &= \sqrt{2} I_{f} \cos(\omega t + 90^{\circ} - \theta) \\ i_{B}(t) &= \sqrt{2} I_{f} \cos(\omega t - 30^{\circ} - \theta) \\ i_{C}(t) &= \sqrt{2} I_{f} \cos(\omega t - 150^{\circ} - \theta) \end{split}$$

$$p_{A}(t) &= u_{A}(t) \cdot i_{A}(t) \\ p_{B}(t) &= u_{C}(t) \cdot i_{B}(t) \\ p_{C}(t) &= u_{C}(t) \cdot i_{C}(t) \end{split}$$

$$p(t) &= p_{A}(t) + p_{B}(t) + p_{C}(t)$$

Potencia Instantánea en Sistemas Equilibrados

$$p(t) = \sqrt{2}U_f \cos(\omega t + 90^\circ) \cdot \sqrt{2}I_f \cos(\omega t + 90^\circ - \theta) +$$

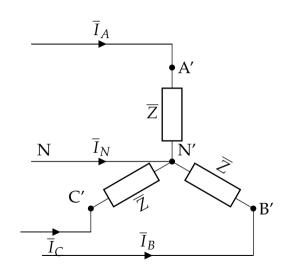
$$+ \sqrt{2}U_f \cos(\omega t - 30^\circ) \cdot \sqrt{2}I_f \cos(\omega t - 30^\circ - \theta) +$$

$$+ \sqrt{2}U_f \cos(\omega t - 150^\circ) \cdot \sqrt{2}I_f \cos(\omega t - 150^\circ - \theta)$$

$$\cos(\alpha) \cdot \cos(\beta) = \frac{1}{2} \cdot (\cos(\alpha + \beta) + \cos(\alpha - \beta))$$

$$p(t) = U_f I_f [\cos(2\omega t + 180^\circ - \theta) + \cos(\theta)] + U_f I_f [\cos(2\omega t - 60^\circ - \theta) + \cos(\theta)] + U_f I_f [\cos(2\omega t - 300^\circ - \theta) + \cos(\theta)]$$

$$p(t) = 3 \cdot U_f \cdot I_f \cdot \cos(\theta) = \sqrt{3} \cdot U \cdot I \cdot \cos(\theta)$$



$$P = 3 \cdot P_Z = 3 \cdot U_Z I_Z \cos(\theta)$$

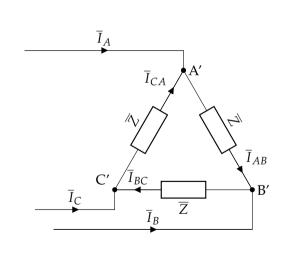
$$Q = 3 \cdot Q_Z = 3 \cdot U_Z I_Z \sin(\theta)$$

$$I_Z = I$$
$$U_Z = U_F$$

$$P = 3U_F I \cos(\theta) = \sqrt{3}UI \cos(\theta)$$

$$Q = 3U_F I \sin(\theta) = \sqrt{3}UI \sin(\theta)$$

$$S = \sqrt{P^2 + Q^2} = \sqrt{3}UI$$



$$P = 3 \cdot P_Z = 3 \cdot U_Z I_Z \cos(\theta)$$

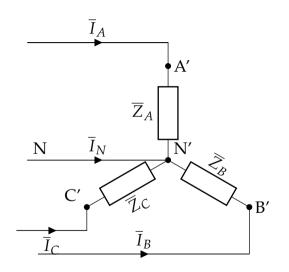
$$Q = 3 \cdot Q_Z = 3 \cdot U_Z I_Z \sin(\theta)$$

$$I_Z = I_F$$
$$U_Z = U$$

$$P = 3UI_F \cos(\theta) = \sqrt{3}UI \cos(\theta)$$

$$Q = 3UI_F \sin(\theta) = \sqrt{3}UI \sin(\theta)$$

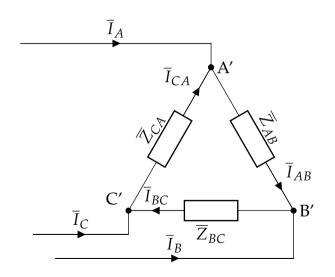
$$S = \sqrt{P^2 + Q^2} = \sqrt{3}UI$$



$$P = P_A + P_B + P_C$$

$$Q = Q_A + Q_B + Q_C$$

$$\overline{S} = P + jQ$$



$$P = P_{AB} + P_{BC} + P_{CA}$$

$$Q = Q_{AB} + Q_{BC} + Q_{CA}$$

$$\overline{S} = P + jQ$$

Comparativa Monofásica-Trifásica

Comparemos un sistema monofásico y un sistema trifásico (3H) que transmiten la **misma potencia activa** y funcionan a la **misma tensión entre líneas**.

$$UI_1\cos\theta = P_1 = P_3 = \sqrt{3}UI_3\cos\theta \rightarrow I_1 = \sqrt{3}I_3$$

Las pérdidas en la línea deben ser iguales para salvar la misma distancia:

$$2R_1I_1^2 = P_{1l} = P_{3l} = 3R_3I_3^2$$

Sustituyendo la relación de corrientes y teniendo en cuenta la relación entre resistencia y sección:

$$2 \cdot R_1 \cdot 3I_3^2 = 3 \cdot R_3I_3^2 \to R_1 = \frac{1}{2}R_3 \to \boxed{S_1 = 2 \cdot S_3}$$

Finalmente, la relación entre masas de conductor es:

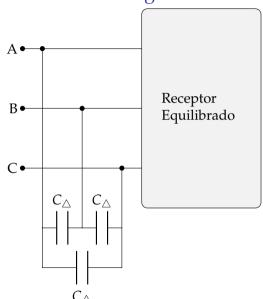
$$\frac{m_3}{m_1} = \frac{3 \cdot S_3}{2 \cdot S_1} = \boxed{\frac{3}{4}}$$

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Objetivo

- Sea un receptor **equilibrado inductivo** del que conocemos P, Q y, por tanto, su factor de potencia $\cos \theta$.
- Para reducir la potencia reactiva del sistema debemos instalar un **banco de condensadores** que suministrarán una potencia reactiva Q_c .
- Como **resultado**, la potencia reactiva y el factor de potencia del sistema serán $Q' = Q Q_c$ y $\cos \theta' > \cos \theta$.
- En trifásica existen dos posibilidades:
 - ► Conexión en triángulo: C_{\triangle}
 - ightharpoonup Conexión en estrella: C_Y .

Conexión en Triángulo



$$Q = P \tan \theta$$

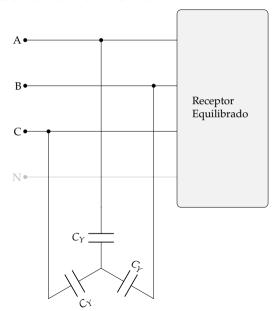
$$Q' = P \tan \theta' =$$

$$= Q - Q_c$$

$$Q_c = 3 \cdot \omega C_{\triangle} \cdot U^2$$

$$C_{\triangle} = \frac{P(\tan\theta - \tan\theta')}{3\omega U^2}$$

Conexión en Estrella



$$Q = P \tan \theta$$

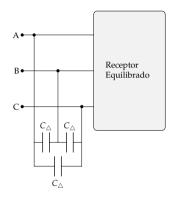
$$Q' = P \tan \theta' =$$

$$= Q - Q_c$$

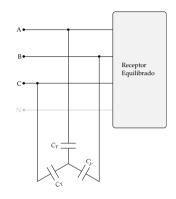
$$Q_c = 3 \cdot \omega C_Y \cdot U_f^2$$

$$C_Y = \frac{P(\tan\theta - \tan\theta')}{\omega U^2}$$

Comparación Estrella-Triángulo



$$C_{\triangle} = \frac{P(\tan\theta - \tan\theta')}{3\omega U^2}$$

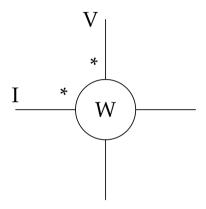


$$C_Y = \frac{P(\tan\theta - \tan\theta')}{\omega U^2}$$

Dado que $C_Y = 3 \cdot C_{\triangle}$ la configuración recomendada es triángulo.

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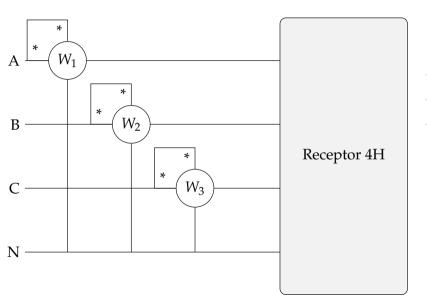
Recordatorio: vatímetro



Vatímetro: equipo de medida de 4 terminales (1 par para tensión, 1 par para corriente)

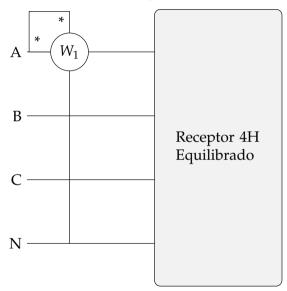
$$W = \Re(\overline{U} \cdot \overline{I}^*)$$

Sistema de 4 Hilos



 $W_1 = \Re(\overline{U}_A \cdot \overline{I}_A^*) = P_A$ $W_2 = \Re(\overline{U}_B \cdot \overline{I}_B^*) = P_B$ $W_3 = \Re(\overline{U}_C \cdot \overline{I}_C^*) = P_C$

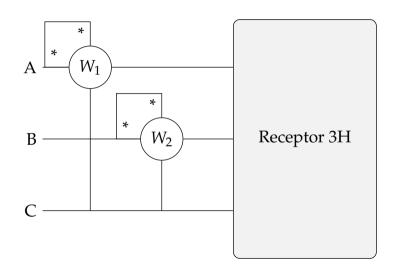
 $P = W_1 + W_2 + W_3$



$$P_A = P_B = P_C$$

$$P = 3 \cdot W_1$$

Sistema de 3 Hilos



Montaje de Aron

$$W_1 = \Re(\overline{U}_{AC} \cdot \overline{I}_A^*)$$

$$W_2 = \Re(\overline{U}_{BC} \cdot \overline{I}_B^*)$$

$$W_1 + W_2 = ?$$

Sistema de 3 Hilos

Desarrollamos las dos expresiones usando corrientes de fase y obviando el operador \Re :

$$\overline{U}_{AC} \cdot \overline{I}_{A}^{*} = \overline{U}_{AC} \cdot (\overline{I}_{AB}^{*} - \overline{I}_{CA}^{*})$$

$$\overline{U}_{BC} \cdot \overline{I}_{B}^{*} = \overline{U}_{BC} \cdot (\overline{I}_{BC}^{*} - \overline{I}_{AB}^{*})$$

Sumamos las dos expresiones:

$$\overline{U}_{AC} \cdot \overline{I}_{A}^{*} + \overline{U}_{BC} \cdot \overline{I}_{B}^{*} = \overline{U}_{AC} \cdot \overline{I}_{AB}^{*} - \overline{U}_{AC} \cdot \overline{I}_{CA}^{*} + \overline{U}_{BC} \cdot \overline{I}_{BC}^{*} - \overline{U}_{BC} \cdot \overline{I}_{AB}^{*}$$

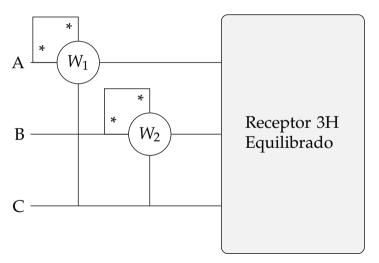
Y agrupamos, teniendo en cuenta que $\overline{U}_{AB} + \overline{U}_{BC} + \overline{U}_{CA} = 0$:

$$\overline{U}_{CA} \cdot \overline{I}_{CA}^* + \overline{U}_{BC} \cdot \overline{I}_{BC}^* + (\overline{U}_{AC} \cdot \overline{I}_{AB}^* - \overline{U}_{BC} \cdot \overline{I}_{AB}^*) = \overline{S}_{CA} + \overline{S}_{BC} + \overline{S}_{AB}$$

Extrayendo la parte real de este resultado obtenemos:

$$\Re(\overline{S}_{AB} + \overline{S}_{BC} + \overline{S}_{CA}) = P \to W_1 + W_2 = P$$

Cuando el sistema es equilibrado, las lecturas individuales de los vatímetros tienen significado.



$$W_1 = \Re(\overline{U}_{AC} \cdot \overline{I}_A^*) = ?$$

$$W_2 = \Re(\overline{U}_{BC} \cdot \overline{I}_B^*) = ?$$

Supongamos SFD:

$$\overline{U}_{AC} = -\overline{U}_{CA} = U/-120^{\circ} + 180^{\circ} = U/60^{\circ}$$

$$\overline{I}_{A} = I/90^{\circ} - \theta$$

$$\overline{U}_{AC} \cdot \overline{I}_{A}^{*} = UI/\theta - 30^{\circ} \rightarrow W_{1} = UI\cos(\theta - 30^{\circ})$$

$$\overline{U}_{BC} = U/\underline{0}$$

$$\overline{I}_B = I/\underline{-30^\circ - \theta}$$

$$\overline{U}_{BC} \cdot \overline{I}_B^* = UI/\underline{\theta + 30^\circ} \rightarrow \boxed{W_2 = UI\cos(\theta + 30^\circ)}$$

Desarrollamos los dos cosenos:

$$\cos(30^{\circ} - \theta) = \cos 30^{\circ} \cos \theta + \sin 30^{\circ} \sin \theta$$
$$\cos(30^{\circ} + \theta) = \cos 30^{\circ} \cos \theta - \sin 30^{\circ} \sin \theta$$

Si sumamos obtenemos la potencia activa:

$$W_1 + W_2 = \sqrt{3}UI\cos\theta = P$$

Si restamos obtenemos la potencia reactiva (salvo un factor):

$$W_1 - W_2 = UI \sin \theta = \frac{Q}{\sqrt{3}}$$

Por tanto, también podemos calcular el ángulo del receptor:

$$\tan \theta = \sqrt{3} \frac{W_1 - W_2}{W_1 + W_2}$$

Repetimos el desarrollo con SFI:

$$\overline{U}_{AC} = -\overline{U}_{CA} = U/120^{\circ} + 180^{\circ} = U/-60^{\circ}$$

$$\overline{I}_{A} = I/-90^{\circ} - \theta$$

$$\overline{U}_{AC} \cdot \overline{I}_{A}^{*} = UI/\theta + 30^{\circ} \rightarrow W_{1} = UI\cos(\theta + 30^{\circ})$$

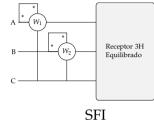
$$\overline{U}_{BC} = U/0$$

$$\overline{I}_{B} = I/30^{\circ} - \theta$$

$$\overline{U}_{BC} \cdot \overline{I}_{B}^{*} = UI/\theta - 30^{\circ} \rightarrow W_{2} = UI\cos(\theta - 30^{\circ})$$

$$W_{1} + W_{2} = \sqrt{3}UI\cos\theta = P$$

$$W_{1} - W_{2} = -UI\sin\theta = -\frac{Q}{\sqrt{3}}$$



$$W_1 = UI\cos(\theta - 30^\circ)$$
$$W_2 = UI\cos(\theta + 30^\circ)$$

$$W_2 = UI\cos(\theta - 30^\circ)$$

 $W_1 = UI\cos(\theta + 30^\circ)$

$$P = W_1 + W_2$$
$$Q = \sqrt{3}(W_1 - W_2)$$

$$P = W_1 + W_2$$

$$Q = \sqrt{3}(W_2 - W_1)$$

$$Q = \sqrt{3}(W_1 - W_2)$$

$$\tan \theta = \sqrt{3}\frac{W_1 - W_2}{W_1 + W_2}$$

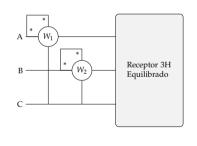
$$\tan \theta = \sqrt{3} \frac{W_2 - W_1}{W_1 + W_2}$$

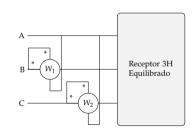
Otras conexiones: 3H SFD

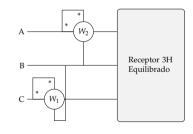
$$(ABC) :: A \triangleright B \triangleright C \Longrightarrow \{AB, BC, CA\}$$

$$W_1 = UI\cos(\theta - 30^\circ)$$
$$W_2 = UI\cos(\theta + 30^\circ)$$

$$P = W_1 + W_2$$
$$Q = \sqrt{3}(W_1 - W_2)$$







 $W_1 : AC \notin SFD$ $W_2 : BC \in SFD$

$$W_1: BA \notin SFD$$

 $W_2: CA \in SFD$

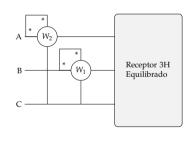
 $W_1: CB \notin SFD$ $W_2: AB \in SFD$

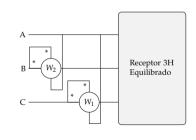
Otras conexiones: 3H SFI

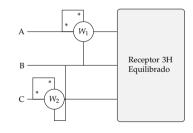
$$(ACB) :: A \triangleright C \triangleright B \Longrightarrow \{AC, CB, BA\}$$

$$W_1 = UI\cos(\theta - 30^\circ)$$
$$W_2 = UI\cos(\theta + 30^\circ)$$

$$P = W_1 + W_2$$
$$Q = \sqrt{3}(W_1 - W_2)$$





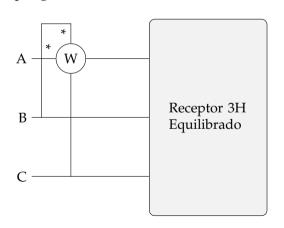


 $W_1 : BC \notin SFI$ $W_2 : AC \in SFI$ $W_1 : CA \notin SFI$ $W_2 : BA \in SFI$ $W_1: AB \notin SFI$ $W_2: CB \in SFI$

Medida de Reactiva con un Vatímetro

Cuando el sistema está equilibrado, es posible medir la potencia reactiva con un único vatímetro.

Supongamos SFD:



$$W = \Re(\overline{U}_{BC} \cdot \overline{I}_{A}^{*})$$

$$\overline{U}_{BC} = U/\underline{0}$$

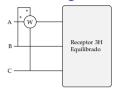
$$\overline{I}_{A} = I/\underline{90^{\circ} - \theta}$$

$$W = \Re(UI/\underline{\theta - 90^{\circ}}) =$$

$$= UI \sin(\theta)$$

$$W = \frac{Q}{W} = \frac{Q}{W}$$

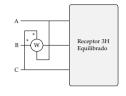
Conexiones para medida de reactiva



$$W=\Re(\overline{U}_{BC}\cdot\overline{I}_A^*)$$

$$BC \in SFD$$

 $BC \notin SFI$

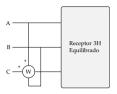


$$W=\Re(\overline{U}_{CA}\cdot\overline{I}_B^*)$$

$$CA \in SFD$$

 $CA \notin SFI$

$$SFD \to W = \frac{Q}{\sqrt{3}}$$
$$SFI \to W = -\frac{Q}{\sqrt{3}}$$

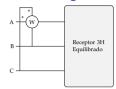


$$W=\Re(\overline{U}_{AB}\cdot\overline{I}_C^*)$$

$$AB \in SFD$$

 $AB \notin SFI$

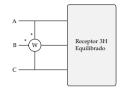
Conexiones para medida de reactiva



$$W=\Re(\overline{U}_{CB}\cdot\overline{I}_A^*)$$

$$CB \notin SFD$$

 $CB \in SFI$



$$W=\Re(\overline{U}_{AC}\cdot\overline{I}_B^*)$$

$$SFD \rightarrow W = -\frac{Q}{\sqrt{3}}$$

$$SFI \rightarrow W = \frac{Q}{\sqrt{2}}$$

$$W=\Re(\overline{U}_{BA}\cdot\overline{I}_C^*)$$

$$BA \notin SFD$$

 $BA \in SFI$