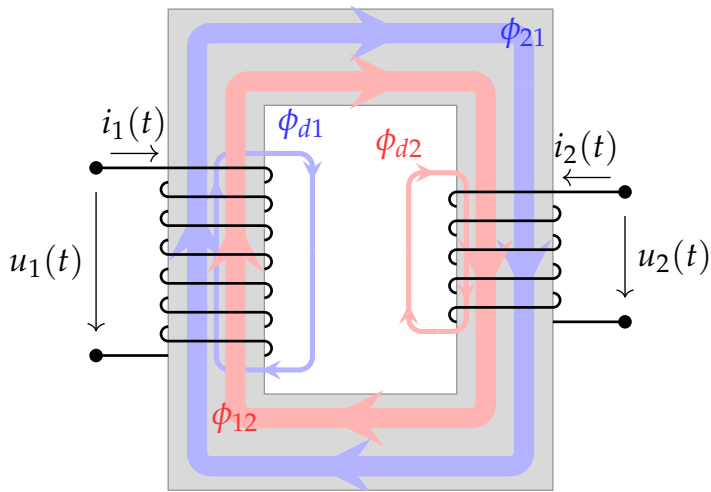


Transformadores

Teoría de Circuitos II

Oscar Perpiñán Lamigueiro

Recordatorio



$$L_1 = N_1 \frac{\phi_{11}}{i_1}$$

$$L_2 = N_2 \frac{\phi_{22}}{i_2}$$

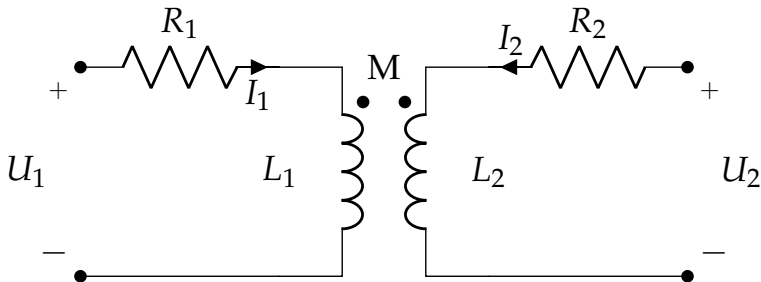
$$M = N_1 \frac{\phi_{12}}{i_2}$$

$$= N_2 \frac{\phi_{21}}{i_1}$$

$$M = k \sqrt{L_1 \cdot L_2}$$

- ① Transformador Real
- ② Transformador Perfecto
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- ⑤ Transformador Perfecto vs. Transformador Ideal
- ⑥ Transformador de Varios Devanados
- ⑦ Autotransformador

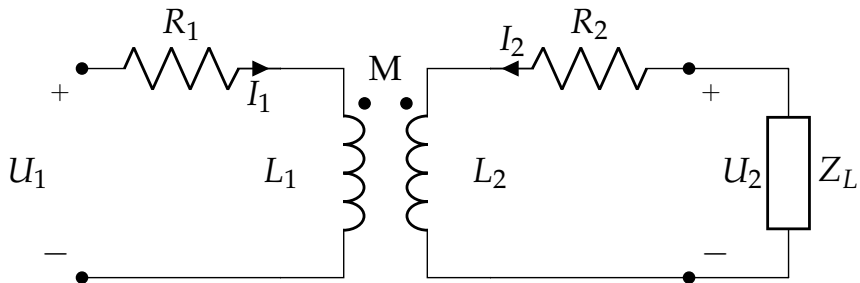
Ecuaciones del Transformador Real



$$\bar{U}_1 = (R_1 + j\omega L_1) \cdot \bar{I}_1 + j\omega M \cdot \bar{I}_2$$

$$\bar{U}_2 = j\omega M \cdot \bar{I}_1 + (R_2 + j\omega L_2) \cdot \bar{I}_2$$

Ejemplo: impedancia de entrada desde primario



Ecuaciones del transformador

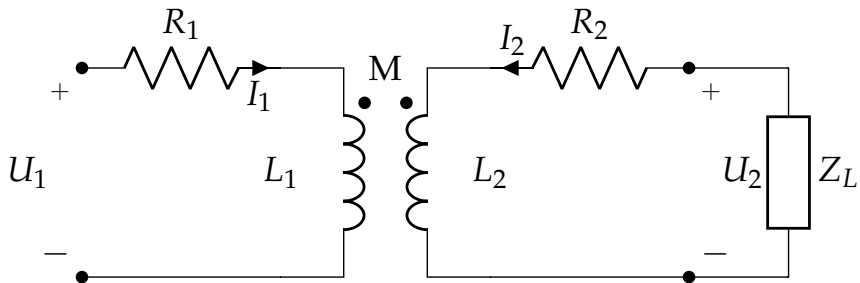
$$\bar{U}_1 = (R_1 + j\omega L_1) \cdot \bar{I}_1 + j\omega M \cdot \bar{I}_2$$

$$\bar{U}_2 = j\omega M \cdot \bar{I}_1 + (R_2 + j\omega L_2) \cdot \bar{I}_2$$

Ecuación de la carga

$$\bar{U}_2 = -\bar{I}_2 \cdot \bar{Z}_L$$

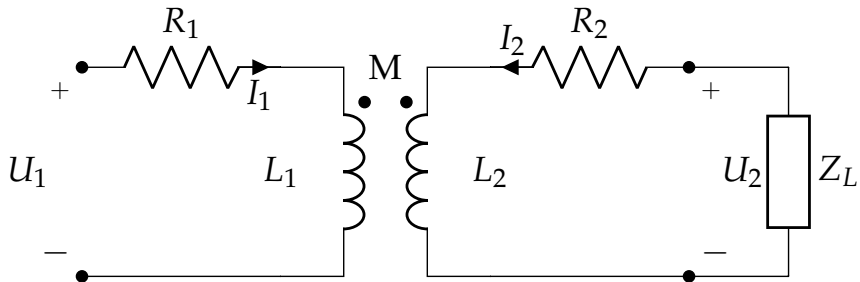
Ejemplo: impedancia de entrada desde primario



Combinando la ecuación del secundario con la ecuación de la carga:

$$\bar{I}_2 = -\frac{j\omega M}{(R_2 + j\omega L_2) + \bar{Z}_L} \cdot \bar{I}_1$$

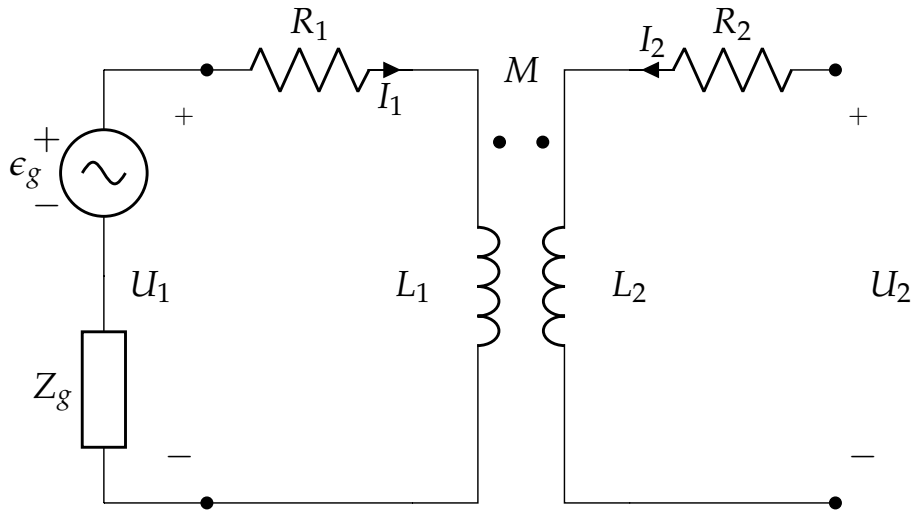
Ejemplo: impedancia de entrada desde primario



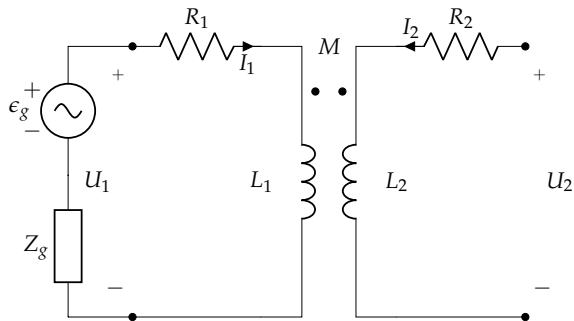
Combinando con la ecuación del primario:

$$\bar{Z}_{in} = \frac{\bar{U}_1}{\bar{I}_1} = (R_1 + j\omega L_1) + \frac{\omega^2 M^2}{(R_2 + j\omega L_2) + \bar{Z}_L} = \boxed{\bar{Z}_1 + \frac{\omega^2 M^2}{\bar{Z}_2 + \bar{Z}_L}}$$

Ejemplo: Equivalente de Thévenin desde secundario



Tensión de Thévenin



Ecuación del generador:

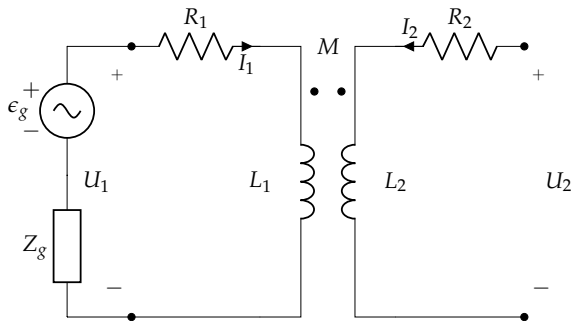
$$\bar{U}_1 = \bar{\epsilon}_g - \bar{I}_1 \cdot \bar{Z}_g$$

Ecuaciones del transformador ($\bar{I}_2 = 0$)

$$\bar{U}_1 = (R_1 + j\omega L_1) \cdot \bar{I}_1$$

$$\bar{U}_2 = j\omega M \cdot \bar{I}_1$$

Tensión de Thévenin



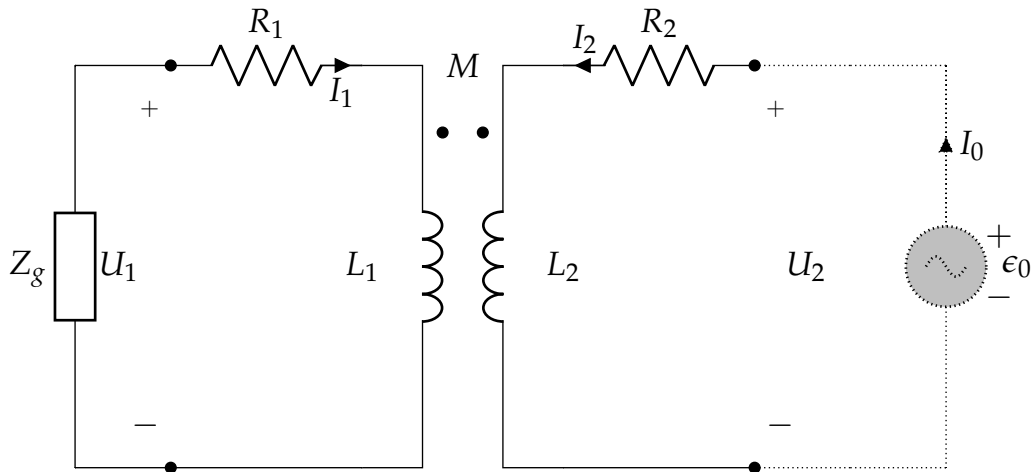
Despejamos I_1 :

$$\bar{I}_1 = \frac{\bar{\epsilon}_g}{\bar{Z}_1 + \bar{Z}_g}$$

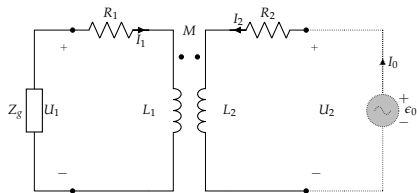
Tensión en abierto:

$$\bar{U}_2 = \bar{\epsilon}_{th} = \frac{j\omega M}{\bar{Z}_1 + \bar{Z}_g} \cdot \bar{\epsilon}_g$$

Impedancia de Thévenin



Impedancia de Thévenin



Ecuaciones del transformador:

$$\bar{U}_1 = (R_1 + j\omega L_1) \cdot \bar{I}_1 + j\omega M \cdot \bar{I}_0$$

$$\bar{\epsilon}_0 = j\omega M \cdot \bar{I}_1 + (R_2 + j\omega L_2) \cdot \bar{I}_0$$

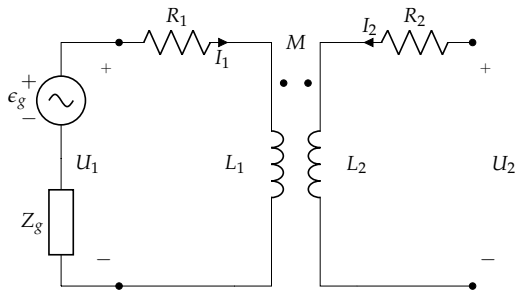
Ecuación de la impedancia:

$$\bar{U}_1 = -\bar{Z}_g \cdot \bar{I}_1$$

Impedancia de Thévenin:

$$\bar{Z}_{th} = \frac{\bar{\epsilon}_0}{\bar{I}_0} = \bar{Z}_2 + \frac{\omega^2 M^2}{\bar{Z}_1 + \bar{Z}_g}$$

Resumen: Equivalente de Thévenin

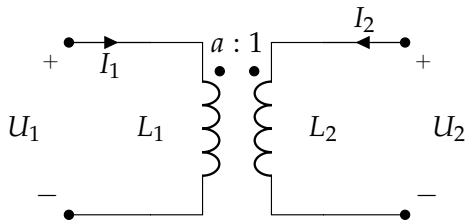


$$\bar{\epsilon}_{th} = \frac{j\omega M}{\bar{Z}_1 + \bar{Z}_g} \cdot \bar{\epsilon}_g$$

$$\bar{Z}_{th} = \frac{\bar{\epsilon}_0}{\bar{I}_0} = \bar{Z}_2 + \frac{\omega^2 M^2}{\bar{Z}_1 + \bar{Z}_g}$$

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- ⑦ Autotransformador

Definición



Las pérdidas resistivas son despreciables.

$$R_1 = R_2 = 0$$

El acoplamiento es perfecto.

$$k = 1 \rightarrow \begin{cases} \phi_{12} &= \phi_{22} \\ \phi_{21} &= \phi_{11} \end{cases}$$

Relación de Transformación

Retomamos las ecuaciones de $M_{12} = M_{21} = M$:

$$N_1 \frac{\phi_{12}}{i_2} = N_2 \frac{\phi_{21}}{i_1}$$

Con la condición $k = 1$ escribimos:

$$N_1 \frac{\phi_{22}}{i_2} = N_2 \frac{\phi_{11}}{i_1}$$

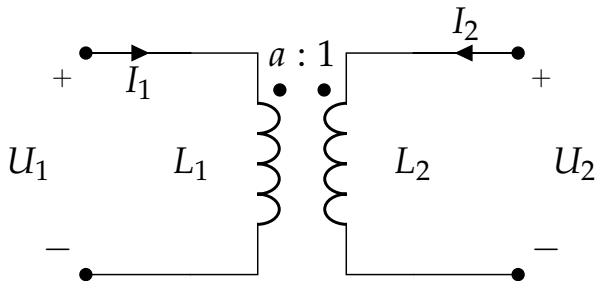
Y con las definiciones de L_1 y L_2 :

$$N_1 \frac{L_2}{N_2} = N_2 \frac{L_1}{N_1}$$

Obtenemos la relación de transformación:

$$\boxed{\frac{L_1}{L_2} = \left(\frac{N_1}{N_2} \right)^2 = a^2}$$

Ecuaciones del Transformador Perfecto



$$\bar{U}_1 = j\omega L_1 \cdot \bar{I}_1 + j\omega M \cdot \bar{I}_2$$

$$\bar{U}_2 = j\omega M \cdot \bar{I}_1 + j\omega L_2 \cdot \bar{I}_2$$

Relación de Tensiones

Dividiendo las ecuaciones:

$$\frac{\bar{U}_1}{\bar{U}_2} = \frac{j\omega L_1 \cdot \bar{I}_1 + j\omega M \cdot \bar{I}_2}{j\omega M \cdot \bar{I}_1 + j\omega L_2 \cdot \bar{I}_2}$$

Empleando la relación de transformación:

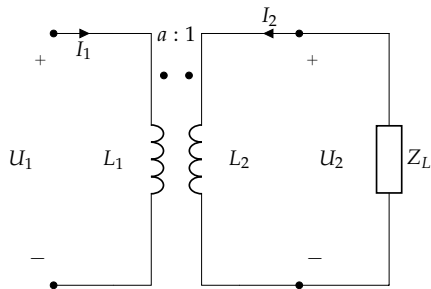
$$\frac{L_1}{L_2} = a^2 \rightarrow \begin{cases} L_1 &= a^2 \cdot L_2 \\ M &= a \cdot L_2 \end{cases}$$

Obtenemos:

$$\frac{\bar{U}_1}{\bar{U}_2} = \frac{a^2 L_2 \cdot \bar{I}_1 + a L_2 \cdot \bar{I}_2}{a L_2 \cdot \bar{I}_1 + L_2 \cdot \bar{I}_2}$$

$$\boxed{\frac{\bar{U}_1}{\bar{U}_2} = a = \frac{N_1}{N_2}}$$

Ejemplo: Impedancia de Entrada



Ecuaciones del transformador:

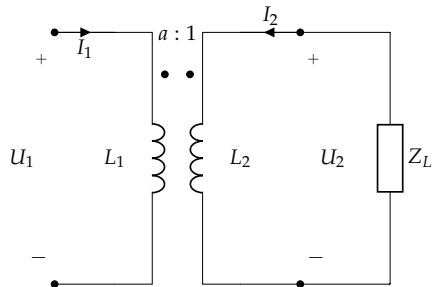
$$\bar{U}_1 = j\omega L_1 \cdot \bar{I}_1 + j\omega M \cdot \bar{I}_2$$

$$\bar{U}_2 = j\omega M \cdot \bar{I}_1 + j\omega L_2 \cdot \bar{I}_2$$

Ecuación de la impedancia:

$$\bar{U}_2 = -\bar{Z}_L \cdot \bar{I}_2$$

Ejemplo: Impedancia de Entrada



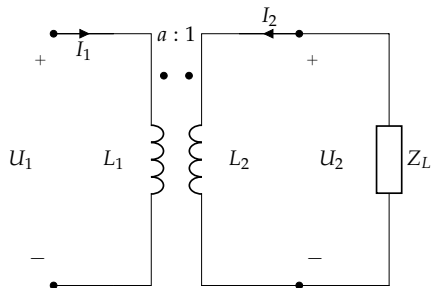
Despejamos I_2 :

$$\bar{I}_2 = -\frac{j\omega M}{j\omega L_2 + \bar{Z}_L} \cdot \bar{I}_1$$

Y sustituimos:

$$\bar{Z}_{in} = \frac{\bar{U}_1}{\bar{I}_1} = j\omega L_1 + \frac{\omega^2 M^2}{j\omega L_2 + \bar{Z}_L}$$

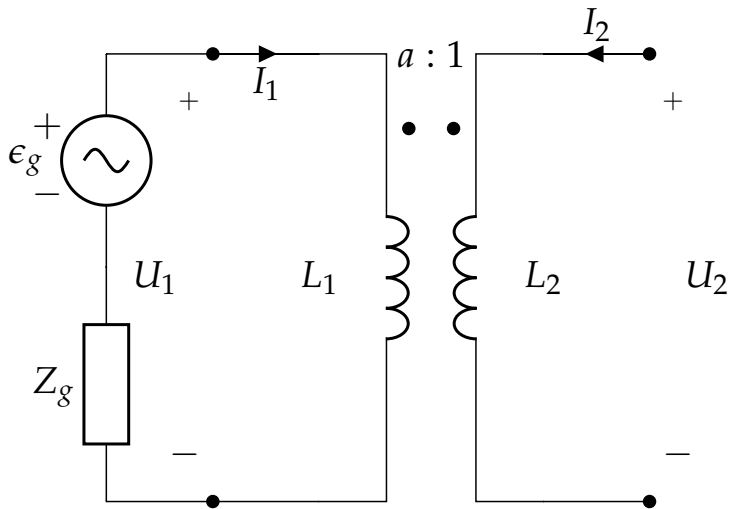
Ejemplo: Impedancia de Entrada



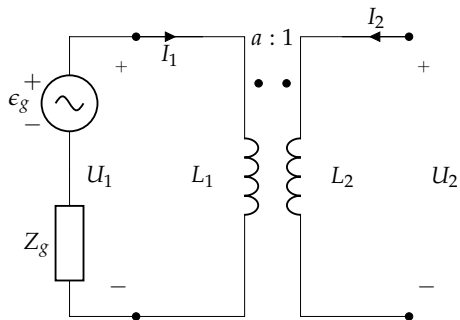
Teniendo en cuenta la relación entre L_1 , L_2 y M :

$$\bar{Z}_{in} = j\omega L_1 + \frac{\omega^2 M^2}{j\omega L_2 + \bar{Z}_L} = \frac{j\omega L_1 \bar{Z}_L}{j\omega L_2 + \bar{Z}_L} \rightarrow \boxed{\bar{Z}_{in} = a^2 \cdot \frac{j\omega L_2 \cdot \bar{Z}_L}{j\omega L_2 + \bar{Z}_L} = \frac{j\omega L_1 \cdot a^2 \cdot \bar{Z}_L}{j\omega L_1 + a^2 \cdot \bar{Z}_L}}$$

Ejemplo: Equivalente de Thévenin desde secundario



Tensión de Thévenin



Ecuación del generador:

$$\bar{U}_1 = \bar{\epsilon}_g - \bar{I}_1 \cdot \bar{Z}_g$$

Ecuaciones del transformador ($\bar{I}_2 = 0$)

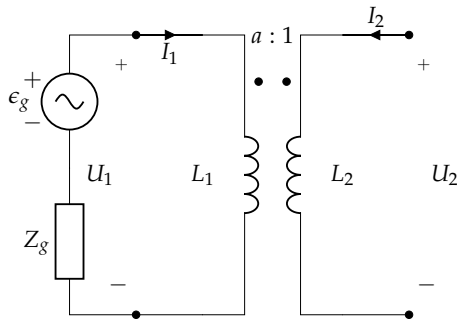
$$\bar{U}_1 = j\omega L_1 \cdot \bar{I}_1$$

$$\bar{U}_2 = j\omega M \cdot \bar{I}_1$$

Despejamos I_1 :

$$\bar{I}_1 = \frac{\bar{\epsilon}_g}{\bar{Z}_g + j\omega L_1}$$

Tensión de Thévenin



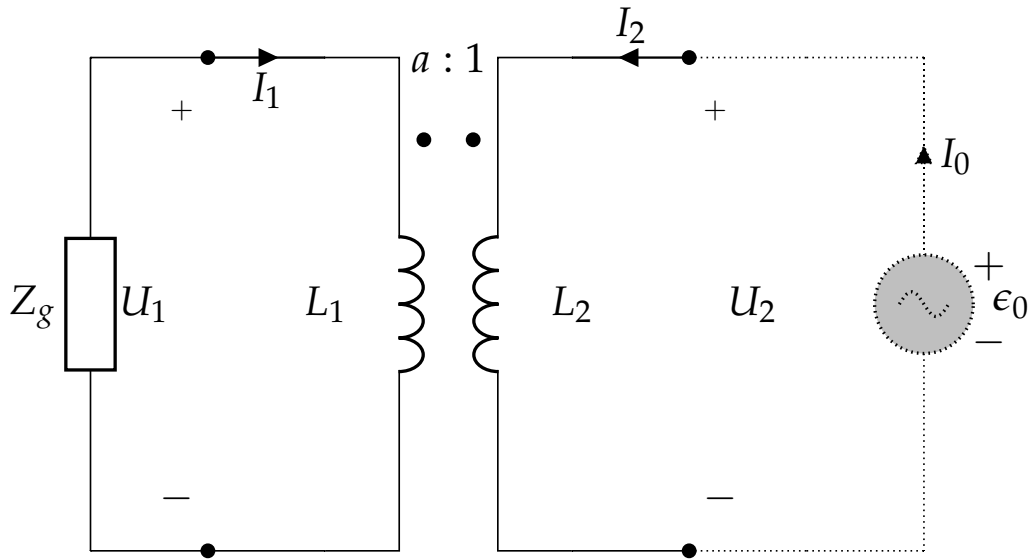
Tensión en abierto:

$$\bar{\epsilon}_{th} = \bar{U}_2 = \frac{j\omega M}{j\omega L_1 + \bar{Z}_g} \cdot \bar{\epsilon}_g$$

Teniendo en cuenta que $M = L_1/a$:

$$\bar{\epsilon}_{th} = \frac{1}{a} \cdot \left(\frac{j\omega L_1}{j\omega L_1 + \bar{Z}_g} \right) \cdot \bar{\epsilon}_g$$

Impedancia de Thévenin



Impedancia de Thévenin

Ecuaciones del transformador:

$$\bar{U}_1 = j\omega L_1 \cdot \bar{I}_1 + j\omega M \cdot \bar{I}_0$$

$$\bar{\epsilon}_0 = j\omega M \cdot \bar{I}_1 + j\omega L_2 \cdot \bar{I}_0$$

Ecuación de la impedancia:

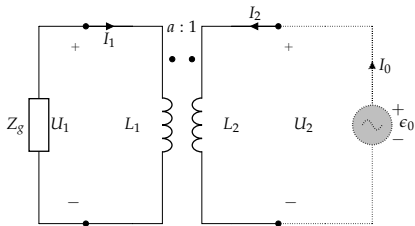
$$\bar{U}_1 = -\bar{Z}_g \cdot \bar{I}_1$$

Impedancia de Thévenin:

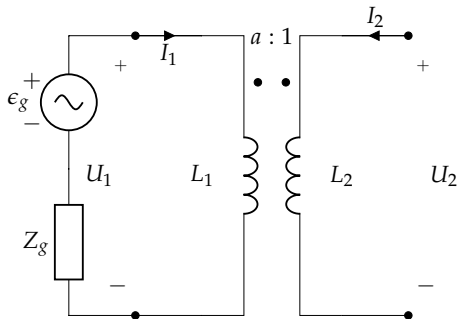
$$\bar{Z}_{th} = \frac{\bar{\epsilon}_0}{\bar{I}_0} = j\omega L_2 + \frac{\omega^2 M^2}{j\omega L_1 + \bar{Z}_g}$$

Con $L_2 = L_1/a^2$ y $M = L_1/a$:

$$\bar{Z}_{th} = \frac{1}{a^2} \cdot \frac{j\omega L_1 \cdot \bar{Z}_g}{j\omega L_1 + \bar{Z}_g}$$



Resumen: Equivalente de Thévenin

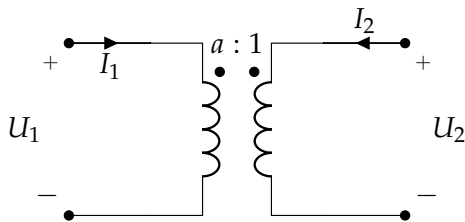


$$\bar{Z}_{th} = \frac{1}{a^2} \cdot \frac{j\omega L_1 \cdot \bar{Z}_g}{j\omega L_1 + \bar{Z}_g}$$

$$\bar{\epsilon}_{th} = \frac{1}{a} \cdot \left(\frac{j\omega L_1}{j\omega L_1 + \bar{Z}_g} \right) \cdot \bar{\epsilon}_g$$

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Definición



Las pérdidas resistivas son despreciables.

$$R_1 = R_2 = 0$$

El acoplamiento es perfecto.

$$k = 1$$

Las bobinas tienen un número muy elevado de espiras.

$$N_1 \rightarrow \infty$$

$$N_2 \rightarrow \infty$$

El flujo en cada bobina es nulo

Para que las tensiones inducidas sean finitas...

$$\bar{U}_1 = N_1 \bar{\phi}_1$$

$$\bar{U}_2 = N_2 \bar{\phi}_2$$

...los flujos (fasoriales) que los atraviesan deben ser nulos.

$$\bar{\phi}_1 \rightarrow 0$$

$$\bar{\phi}_2 \rightarrow 0$$

Siendo:

$$\bar{\phi}_1 = \bar{\phi}_{11} + \bar{\phi}_{12}$$

$$\bar{\phi}_2 = \bar{\phi}_{22} + \bar{\phi}_{21}$$

El flujo mutuo es nulo

Teniendo en cuenta que el acoplamiento es perfecto, $k = 1$:

$$\left. \begin{array}{l} \phi_{12} = \phi_{22} \\ \phi_{21} = \phi_{11} \end{array} \right\} \rightarrow \left\{ \begin{array}{l} 0 = \bar{\phi}_{21} + \bar{\phi}_{12} \\ 0 = \bar{\phi}_{12} + \bar{\phi}_{21} \end{array} \right.$$

O también:

$$\boxed{\bar{\phi}_{11} + \bar{\phi}_{22} = 0}$$

Relación de Transformación

Hemos obtenido:

$$\bar{\phi}_{11} + \bar{\phi}_{22} = 0$$

Con las definiciones de L_1, L_2 :

$$L_1 = N_1 \frac{\phi_{11}}{I_1}; \quad L_2 = N_2 \frac{\phi_{22}}{I_2}$$

Podemos escribir:

$$\frac{L_1 \bar{I}_1}{N_1} + \frac{L_2 \bar{I}_2}{N_2} = 0$$

Y con la relación entre ambas obtenemos*:

$$L_1 = L_2 \cdot \left(\frac{N_1}{N_2} \right)^2 \rightarrow \frac{N_1 L_2 \bar{I}_1}{N_2^2} + \frac{L_2 \bar{I}_2}{N_2} = 0 \rightarrow \boxed{\frac{\bar{I}_1}{\bar{I}_2} = -\frac{1}{a} = -\frac{N_2}{N_1}}$$

*Si las dos corrientes van en el mismo sentido, la ecuación tendrá un signo positivo.

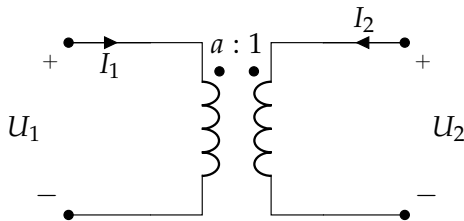
Un transformador ideal no consume potencia

$$\bar{S}_1 = \bar{U}_1 \cdot \bar{I}_1^*$$

$$\bar{S}_2 = \bar{U}_2 \cdot \bar{I}_2^*$$

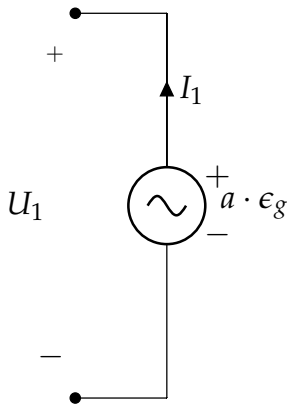
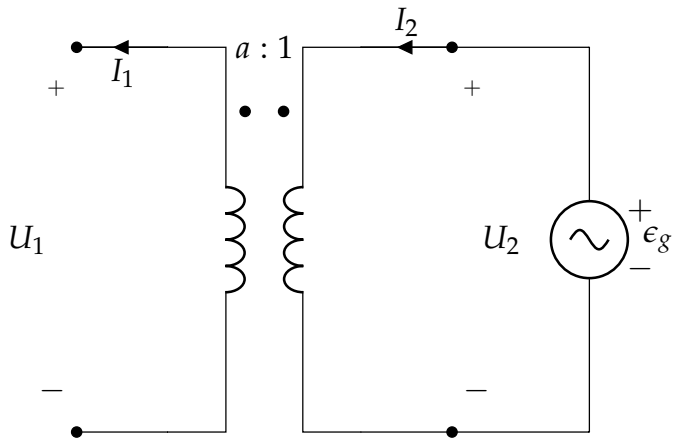
$$\bar{U}_2 \cdot \bar{I}_2^* = \frac{1}{a} \cdot \bar{U}_1 \cdot a \cdot \bar{I}_1^* = \bar{S}_1$$

$$\boxed{\bar{S}_1 = \bar{S}_2} \quad \boxed{P_1 = P_2} \quad \boxed{Q_1 = Q_2}$$



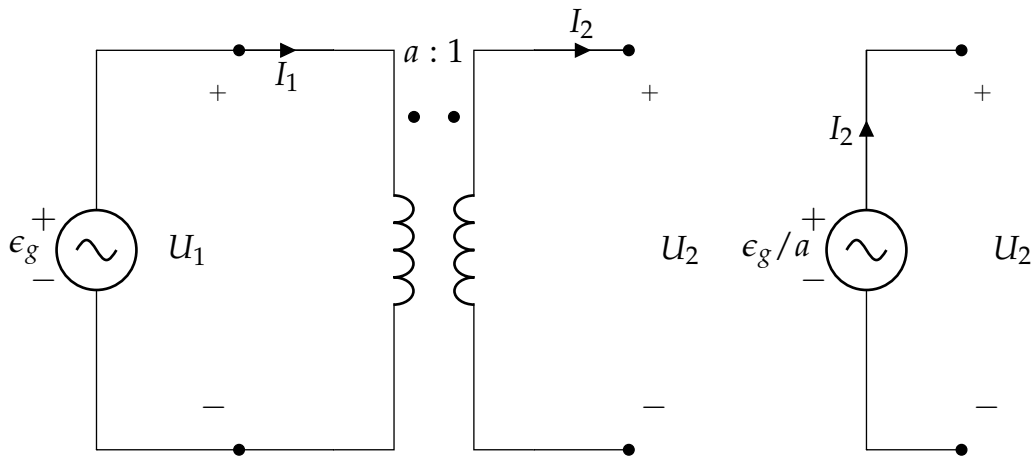
- ① Transformador Real
- ② Transformador Perfecto
- ③ Transformador Ideal
- ④ **Transferencia de Circuitos**
- ⑤ Transformador Perfecto vs. Transformador Ideal
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Fuente de Tensión de Secundario a Primario



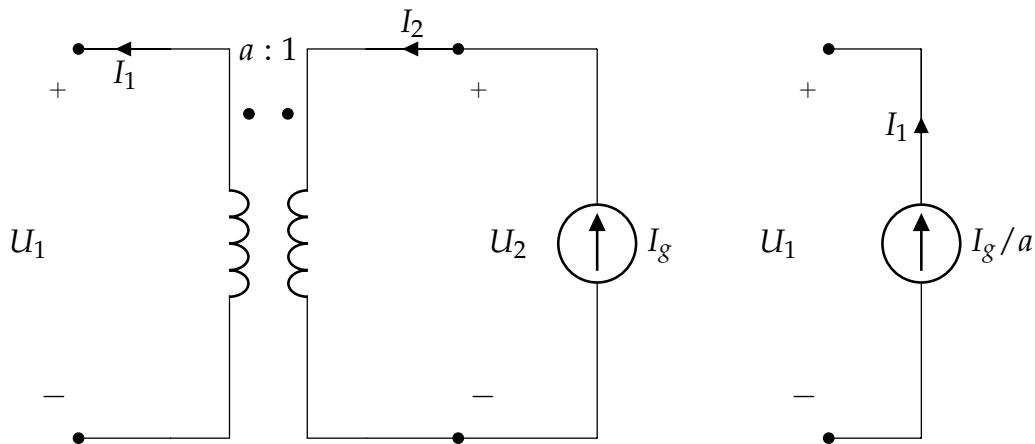
$$\bar{U}_1 = a \cdot \bar{U}_2 \rightarrow \boxed{\bar{\epsilon}_{g1} = a \cdot \bar{\epsilon}_g}$$

Fuente de Tensión de Primario a Secundario



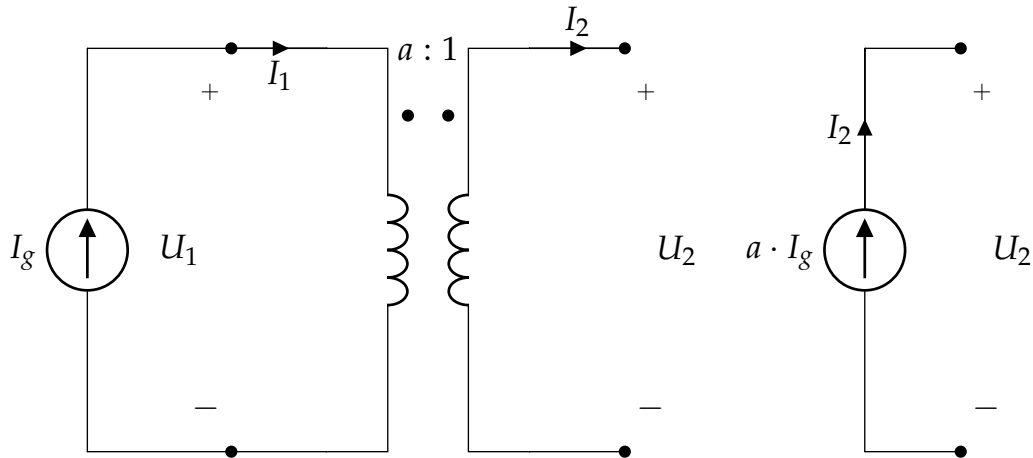
$$\bar{U}_2 = \bar{U}_1/a \rightarrow \boxed{\bar{\epsilon}_{g2} = \bar{\epsilon}_g/a}$$

Fuente de Corriente de Secundario a Primario



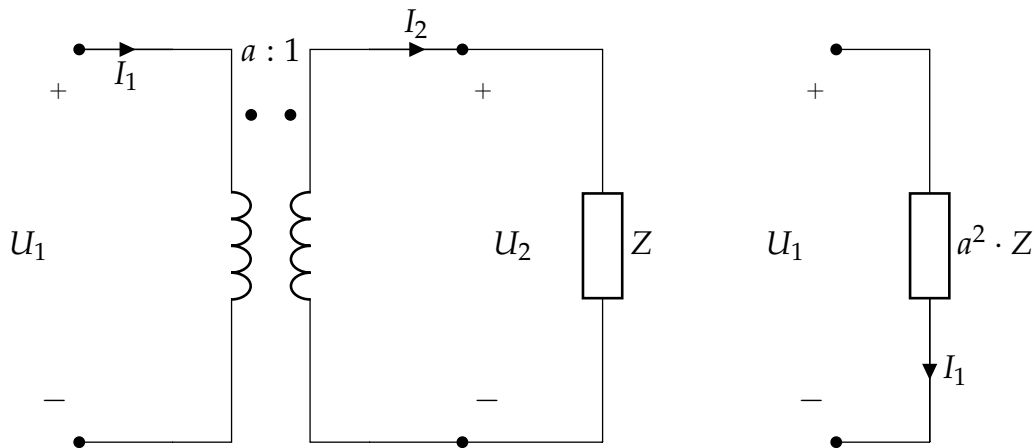
$$\bar{I}_1 = \bar{I}_2/a \rightarrow \boxed{\bar{I}_{g1} = \bar{I}_g/a}$$

Fuente de Corriente de Primario a Secundario



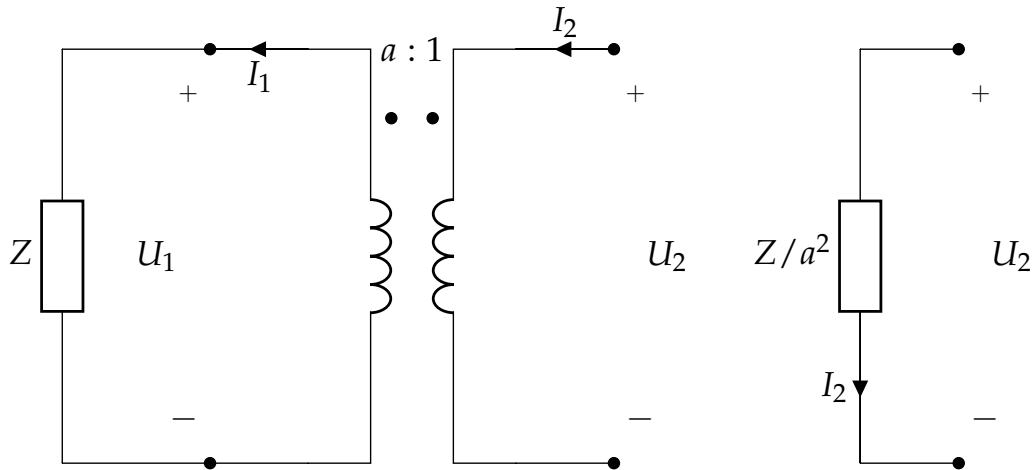
$$\bar{I}_2 = a \cdot \bar{I}_1 \rightarrow \boxed{\bar{I}_{g2} = a \cdot \bar{I}_g}$$

Impedancia de Secundario a Primario



$$\left. \begin{array}{l} \bar{U}_1 = a \cdot \bar{U}_2 \\ \bar{I}_1 = \bar{I}_2 / a \end{array} \right\} \rightarrow \boxed{\bar{Z}_1 = \frac{\bar{U}_1}{\bar{I}_1} = a^2 \cdot \bar{Z}}$$

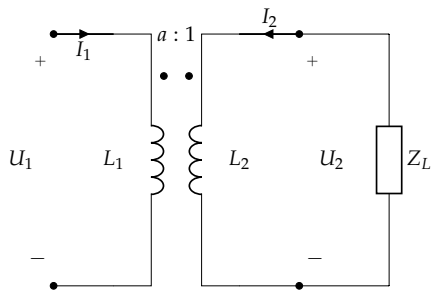
Impedancia de Primario a Secundario



$$\left. \begin{array}{l} \bar{U}_2 = \bar{U}_1 / a \\ \bar{I}_2 = a \cdot \bar{I}_1 \end{array} \right\} \rightarrow \boxed{\bar{Z}_2 = \frac{\bar{U}_2}{\bar{I}_2} = \bar{Z} / a^2}$$

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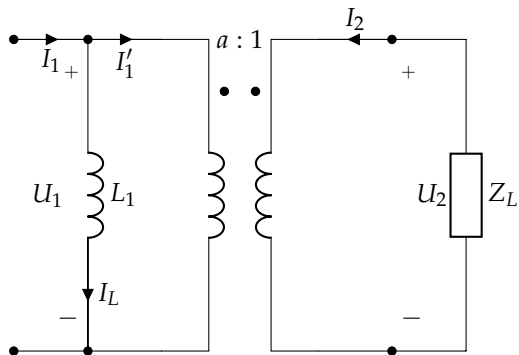
Recordatorio: impedancia de entrada de un T. Perfecto



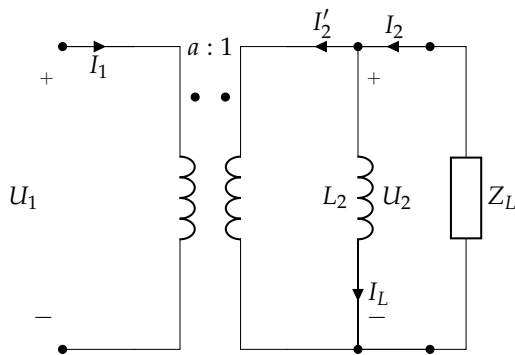
$$\bar{Z}_{in} = \frac{j\omega L_1 \cdot (a^2 \bar{Z}_L)}{j\omega L_1 + (a^2 \cdot \bar{Z}_L)}$$

$$\bar{Z}_{in} = a^2 \cdot \frac{j\omega L_2 \cdot \bar{Z}_L}{j\omega L_2 + \bar{Z}_L}$$

Circuito equivalente con transformador ideal

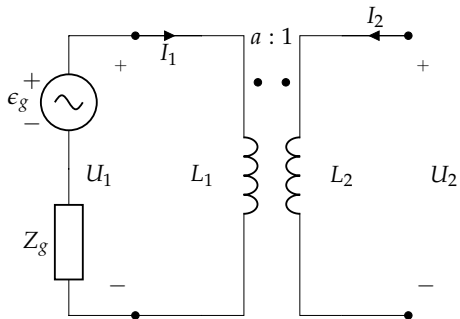


$$\bar{Z}_{in} = \frac{j\omega L_1 \cdot (a^2 \bar{Z}_L)}{j\omega L_1 + (a^2 \cdot \bar{Z}_L)}$$



$$\bar{Z}_{in} = a^2 \cdot \frac{j\omega L_2 \cdot \bar{Z}_L}{j\omega L_2 + \bar{Z}_L}$$

Recordatorio: Equivalente de Thévenin



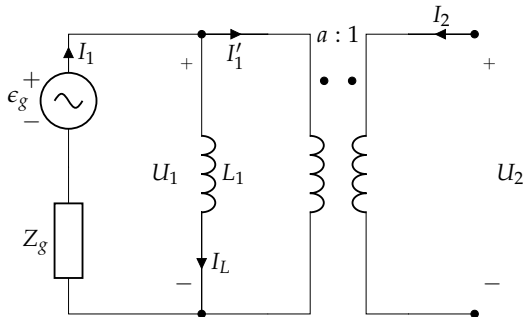
$$\bar{Z}_{th} = \frac{1}{a^2} \cdot \frac{j\omega L_1 \cdot \bar{Z}_g}{j\omega L_1 + \bar{Z}_g}$$

$$\bar{\epsilon}_{th} = \frac{1}{a} \cdot \left(\frac{j\omega L_1}{j\omega L_1 + \bar{Z}_g} \right) \cdot \bar{\epsilon}_g$$

Equivalente en primario con transformador ideal

$$\bar{Z}_{th} = \frac{1}{a^2} \cdot \frac{j\omega L_1 \cdot \bar{Z}_g}{j\omega L_1 + \bar{Z}_g}$$

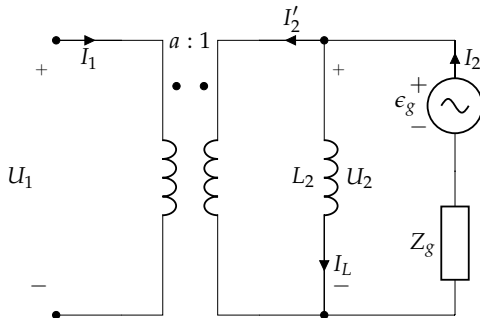
$$\bar{\epsilon}_{th} = \frac{1}{a} \cdot \left(\frac{j\omega L_1}{j\omega L_1 + \bar{Z}_g} \right) \cdot \bar{\epsilon}_g$$



Equivalente en secundario con transformador ideal

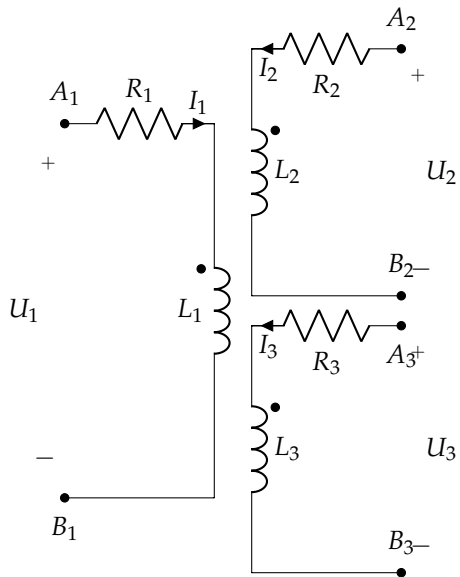
$$\bar{Z}_{th} = a^2 \cdot \frac{j\omega L_2 \cdot \bar{Z}_g}{j\omega L_2 + \bar{Z}_g}$$

$$\bar{e}_{th} = a \cdot \left(\frac{j\omega L_2}{j\omega L_2 + \bar{Z}_g} \right) \cdot \bar{e}_g$$

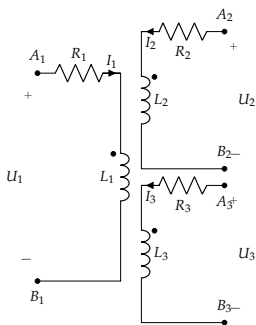


- ① Transformador Real
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Transformador Real de Varios Devanados



Ecuaciones del Transformador Real

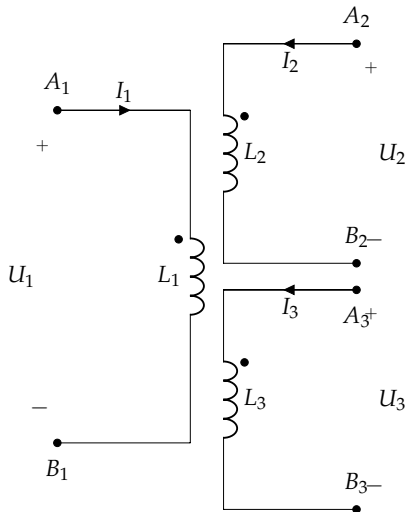


$$\bar{U}_1 = (R_1 + j\omega L_1) \cdot \bar{I}_1 + j\omega M_{12} \cdot \bar{I}_2 + j\omega M_{13} \cdot \bar{I}_3$$

$$\bar{U}_2 = j\omega M_{12} \cdot \bar{I}_1 + (R_2 + j\omega L_2) \cdot \bar{I}_2 + j\omega M_{23} \cdot \bar{I}_3$$

$$\bar{U}_3 = j\omega M_{13} \cdot \bar{I}_1 + j\omega M_{12} \cdot \bar{I}_2 + (R_3 + j\omega L_3) \cdot \bar{I}_3$$

Transformador Perfecto



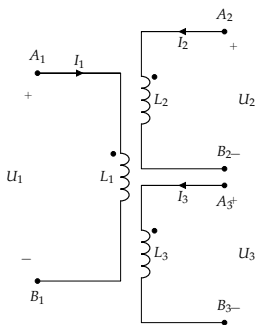
Las pérdidas resistivas son despreciables.

$$R_1 = R_2 = R_3 = 0$$

El acoplamiento es perfecto.

$$k_{12} = k_{13} = k_{23} = 1$$

Ecuaciones del Transformador Perfecto

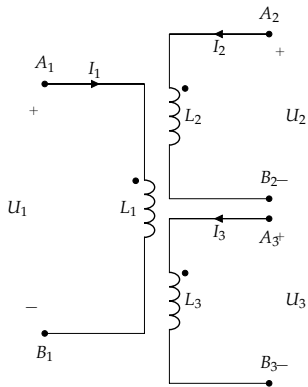


$$\bar{U}_1 = j\omega L_1 \cdot \bar{I}_1 + j\omega M_{12} \cdot \bar{I}_2 + j\omega M_{13} \cdot \bar{I}_3$$

$$\bar{U}_2 = j\omega M_{12} \cdot \bar{I}_1 + j\omega L_2 \cdot \bar{I}_2 + j\omega M_{23} \cdot \bar{I}_3$$

$$\bar{U}_3 = j\omega M_{13} \cdot \bar{I}_1 + j\omega M_{12} \cdot \bar{I}_2 + j\omega L_3 \cdot \bar{I}_3$$

Relaciones de Transformación



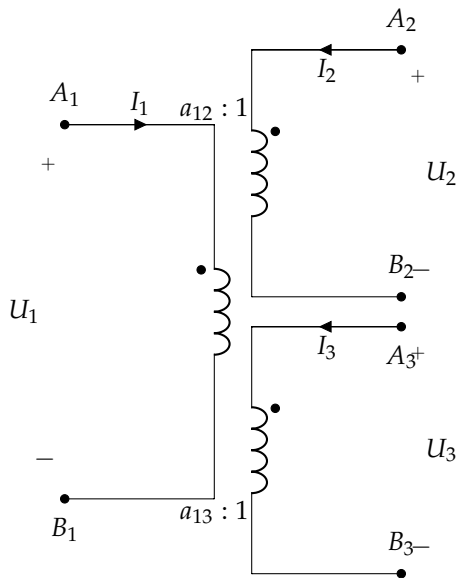
$$\frac{L_1}{L_2} = \left(\frac{N_1}{N_2} \right)^2 = a_{12}^2$$

$$\frac{L_1}{L_3} = \left(\frac{N_1}{N_3} \right)^2 = a_{13}^2$$

$$\frac{\bar{U}_1}{\bar{U}_2} = a_{12}$$

$$\frac{\bar{U}_1}{\bar{U}_3} = a_{13}$$

Transformador Ideal



Relación de Transformación del Transformador Ideal

Debido a las condiciones de idealidad:

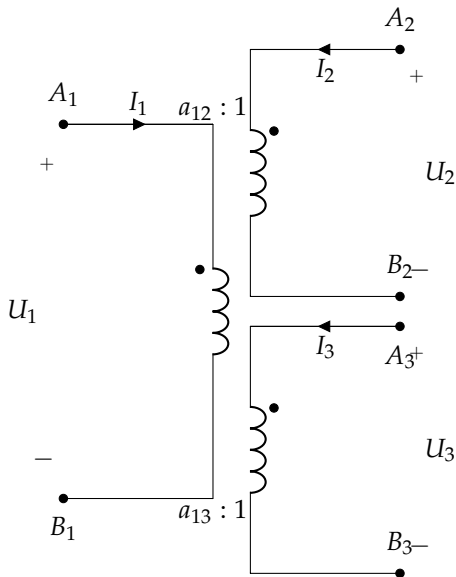
$$\bar{\phi}_{11} + \bar{\phi}_{22} + \bar{\phi}_{33} = 0$$

$$N_1 \bar{I}_1 + N_2 \bar{I}_2 + N_3 \bar{I}_3 = 0$$

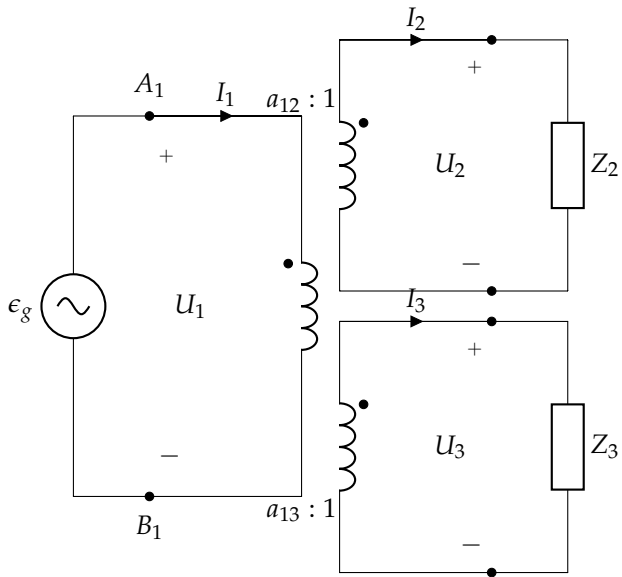
En términos de corriente:

$$\boxed{\bar{I}_1 = -1/a_{12} \cdot \bar{I}_2 - 1/a_{13} \cdot \bar{I}_3}$$

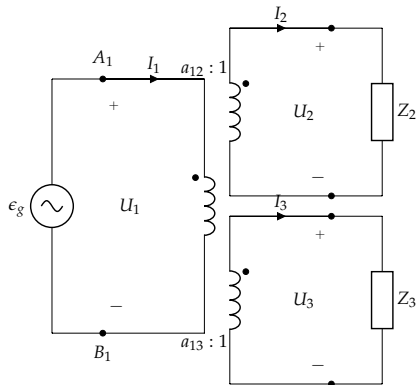
Si las corrientes I_2 e I_3 son salientes, en la ecuación anterior los signos serán positivos.



Impedancia de Entrada



Impedancia de Entrada*



Ecuaciones del transformador:

$$\bar{U}_1 = \bar{U}_2 \cdot a_{12}$$

$$\bar{U}_1 = \bar{U}_3 \cdot a_{13}$$

$$\bar{I}_1 = 1/a_{12} \cdot \bar{I}_2 + 1/a_{13} \cdot \bar{I}_3$$

Ecuaciones Terminales

$$\bar{U}_2 = \bar{Z}_2 \cdot \bar{I}_2$$

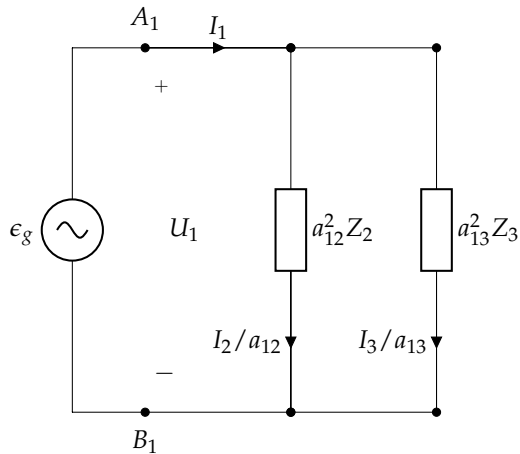
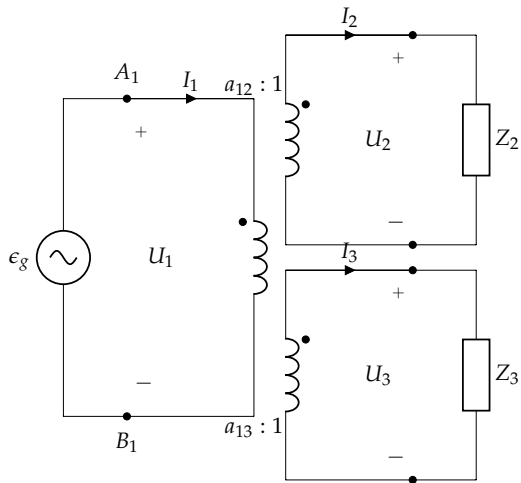
$$\bar{U}_3 = \bar{Z}_3 \cdot \bar{I}_3$$

Resultado:

$$\frac{\bar{I}_1}{\bar{U}_1} = \bar{Y}_{in} = \frac{1}{a_{12}^2 \bar{Z}_2} + \frac{1}{a_{13}^2 \bar{Z}_3}$$

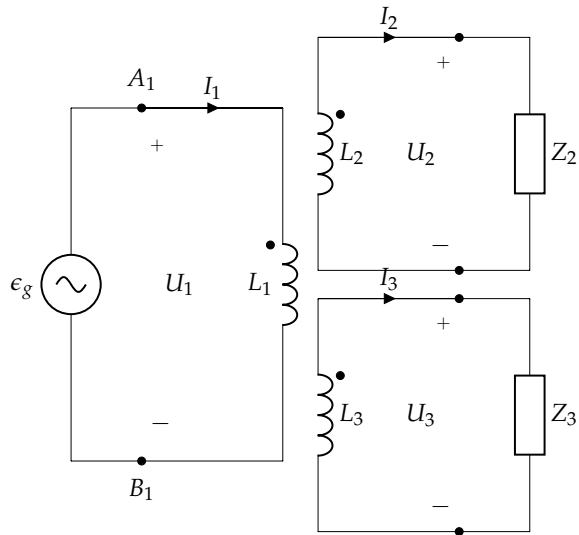
*Las corrientes en 2 y 3 son salientes, y por tanto, en la ecuación de corrientes usamos el signo positivo.

Circuito Equivalente

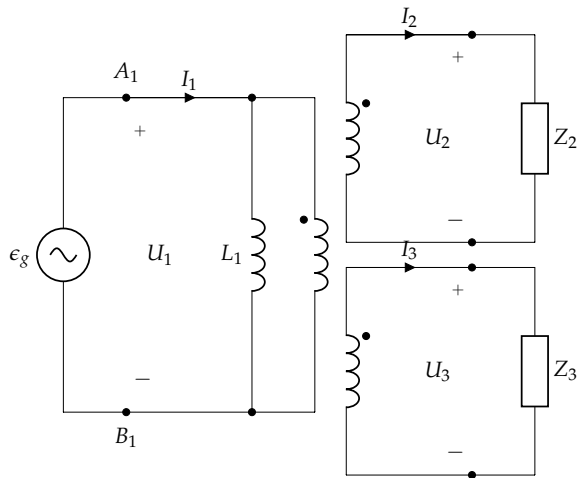


Circuito Equivalente de un Transformador Perfecto

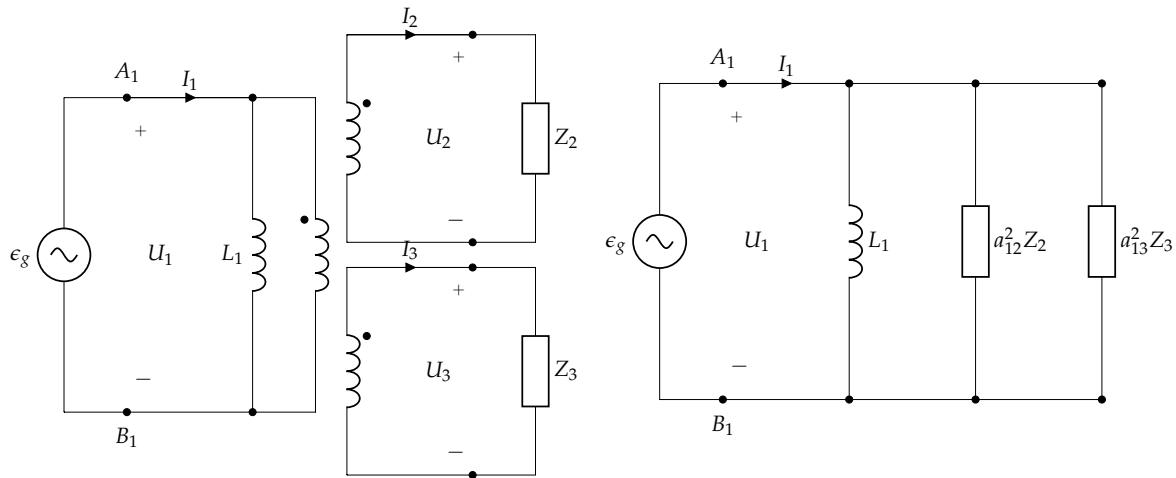
Transformador Perfecto



Equivalente Ideal

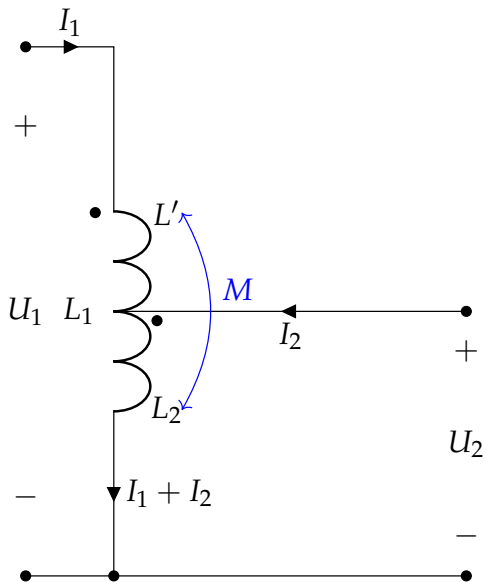


Circuito Equivalente de un Transformador Perfecto

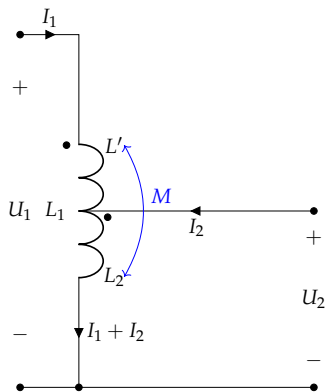


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Autotransformador Perfecto



Ecuaciones del Autotransformador Perfecto

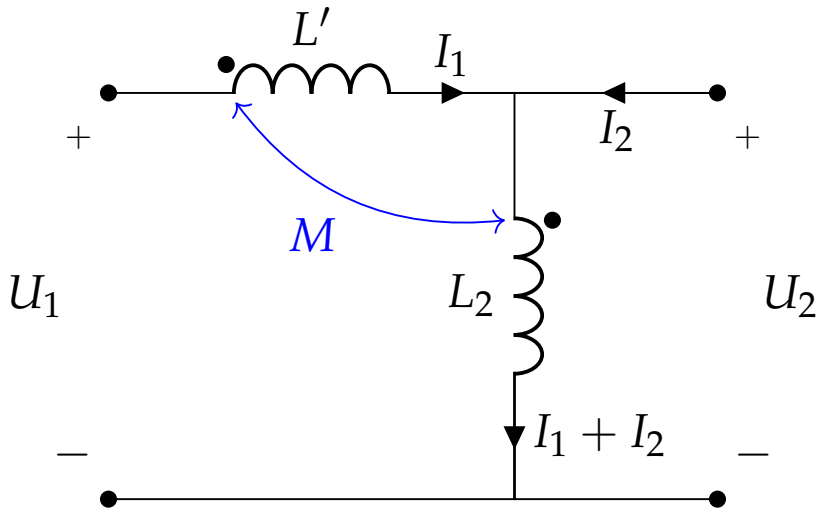


$$\bar{U}_1 = j\omega L_1 \cdot \bar{I}_1 + j\omega(M + L_2) \cdot \bar{I}_2$$

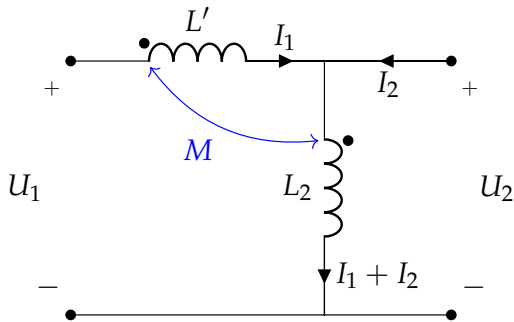
$$\bar{U}_2 = j\omega(M + L_2) \cdot \bar{I}_1 + j\omega L_2 \cdot \bar{I}_2$$

$$M = \sqrt{L' \cdot L_2}$$

Circuito Alternativo del Autotransformador Perfecto



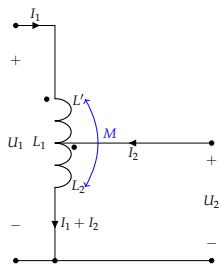
Ecuaciones del Circuito Alternativo



$$\bar{U}_1 = j\omega(L' + L_2 + 2M) \cdot \bar{I}_1 + j\omega(L_2 + M) \cdot \bar{I}_2$$

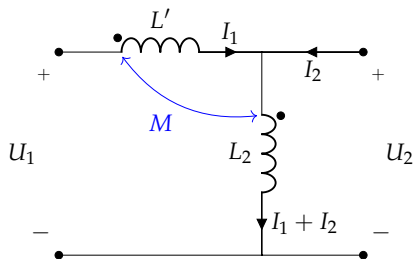
$$\bar{U}_2 = j\omega(L_2 + M) \cdot \bar{I}_1 + j\omega L_2 \cdot \bar{I}_2$$

Ecuaciones Comparadas



$$\bar{U}_1 = j\omega L_1 \cdot \bar{I}_1 + j\omega (M + L_2) \cdot \bar{I}_2$$

$$\bar{U}_2 = j\omega (L_2 + M) \cdot \bar{I}_1 + j\omega L_2 \cdot \bar{I}_2$$



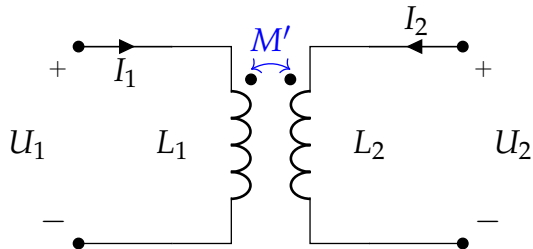
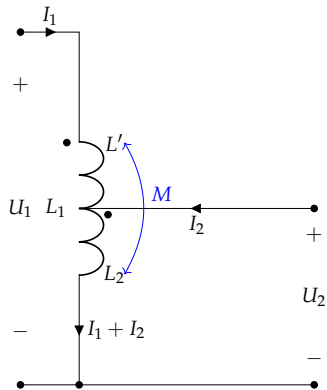
$$\bar{U}_1 = j\omega (L' + L_2 + 2M) \cdot \bar{I}_1 + j\omega (M + L_2) \cdot \bar{I}_2$$

$$\bar{U}_2 = j\omega (L_2 + M) \cdot \bar{I}_1 + j\omega L_2 \cdot \bar{I}_2$$

$$L_1 = L' + L_2 + 2M$$

$$M = \sqrt{L' \cdot L_2}$$

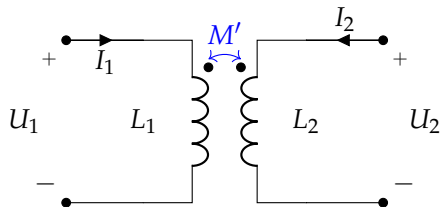
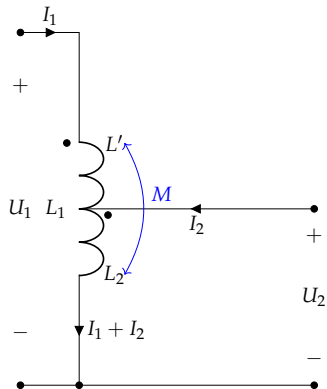
Transformador Perfecto Equivalente



$$L_1 = L' + L_2 + 2M$$

$$M' = M + L_2$$

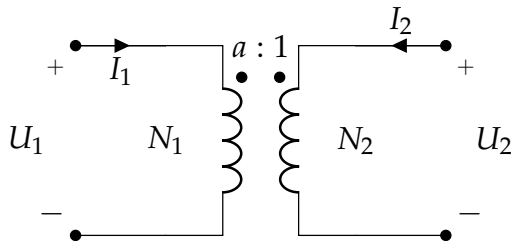
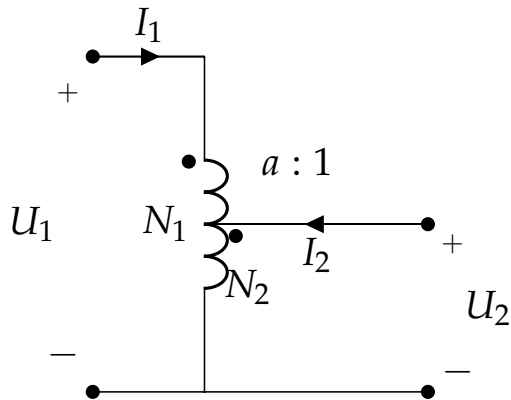
Transformador Perfecto Equivalente



Comprobamos:

$$\begin{aligned}
 M' &= \sqrt{L_1 \cdot L_2} = \\
 &= \sqrt{(L' + L_2 + 2M)L_2} = \\
 &= \sqrt{L'L_2 + L_2^2 + 2ML_2} = \\
 &= \sqrt{M^2 + L_2^2 + 2ML_2} = \\
 &= M + L_2
 \end{aligned}$$

Equivalente del Autotransformador Ideal



$$\frac{U_1}{U_2} = \frac{N_1}{N_2} = a$$

$$\frac{I_1}{I_2} = -\frac{N_2}{N_1} = -\frac{1}{a}$$