#### Sistemas Trifásicos

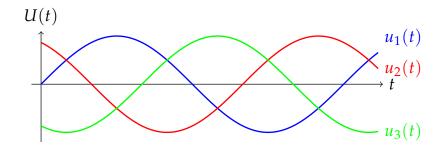
Oscar Perpiñán Lamigueiro

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#### Motivación de los sistemas trifásicos

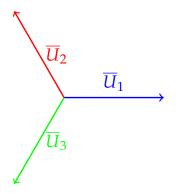
- ► En un sistema trifásico la potencia instantánea es constante, evitando vibraciones y esfuerzos en las máquinas. (*La potencia instantánea de un sistema monofásico es pulsante*.)
- ► La masa de conductor necesaria en un sistema trifásico es un 25% inferior que en un monofásico para transportar la misma potencia.

#### Ondas Trifásicas



$$u_1(t) = U_0 \cos(\omega t)$$
  
 $u_2(t) = U_0 \cos(\omega t + 2\pi/3)$   
 $u_3(t) = U_0 \cos(\omega t - 2\pi/3)$ 

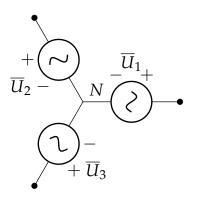
#### Fasores de un sistema trifásico



$$\begin{aligned} \overline{U}_1 &= U \underline{/0} \\ \overline{U}_2 &= U \underline{/2\pi/3} \\ \overline{U}_3 &= U \underline{/-2\pi/3} \end{aligned}$$

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#### Conexión



$$u_1(t) = U_0 \cos(\omega t)$$

$$u_2(t) = U_0 \cos(\omega t + 2\pi/3)$$

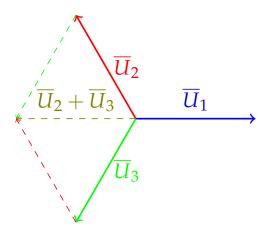
$$\overline{U}_1 = U/0$$

$$\overline{U}_2 = U/2\pi/3$$

$$u_3(t) = U_0 \cos(\omega t - 2\pi/3)$$

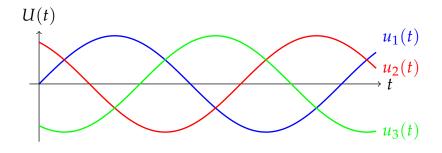
$$\overline{U}_3 = U/-2\pi/3$$

#### Las tensiones suman 0



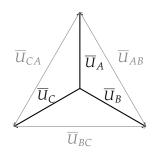
$$\boxed{\overline{U}_1 + \overline{U}_2 + \overline{U}_3 = 0}$$

#### Las tensiones suman 0



$$u_1(t) + u_2(t) + u_3(t) = 0$$

## Tensiones de Fase y Línea



Tensiones de **Fase**:  $U_A$ ,  $U_B$ ,  $U_C$ Tensiones de **Línea**:  $U_{AB}$ ,  $U_{BC}$ ,  $U_{CA}$ 

$$\overline{U}_{AB} = \overline{U}_A - \overline{U}_B$$

$$\overline{U}_{BC} = \overline{U}_B - \overline{U}_C$$

$$\overline{U}_{CA} = \overline{U}_C - \overline{U}_A$$

$$\overline{U}_{AB} + \overline{U}_{BC} + \overline{U}_{CA} = 0$$

## Tensiones de Fase y Línea

$$\overline{U}_A = U_f / \theta_f \overline{U}_B = U_f / \theta_f - 120^\circ$$

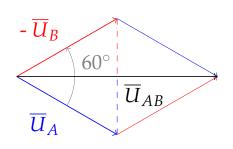
$$\overline{U}_{AB} = \overline{U}_A - \overline{U}_B =$$

$$= U_f / \underline{\theta_f} - U_f / \underline{\theta_f} - 120^\circ =$$

$$= U_f / \underline{\theta_f} + U_f / \underline{\theta_f} + 60^\circ$$

$$= 2 \cdot U_f \cdot \cos(30) / \underline{\theta_f} + 30^\circ =$$

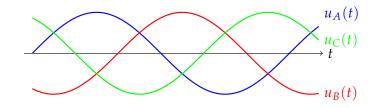
$$= \sqrt{3} U_f / \underline{\theta_f} + 30^\circ$$



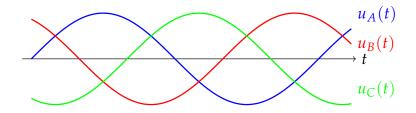
$$U = \sqrt{3} \cdot U_f$$
$$\theta_l = \theta_f + 30^\circ$$

#### Secuencia de Fases

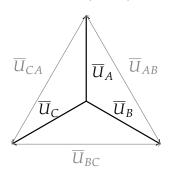
- ► Sentido en el que ocurren los máximos de cada fase.
- ► Secuencia de Fases Directa (SFD): ABC



► Secuencia de Fases Inversa (SFI): ACB



#### Secuencia de Fases Directa (SFD)

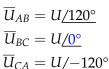


$$\overline{U}_A = \frac{U}{\sqrt{3}} \underline{/90^{\circ}}$$

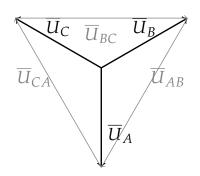
$$\overline{U}_B = \frac{U}{\sqrt{3}} \underline{/-30^{\circ}}$$

$$\overline{U}_C = \frac{U}{\sqrt{3}} \underline{/-150^{\circ}}$$





# Secuencia de Fases Inversa (SFI)

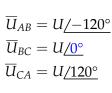


$$\overline{U}_A = \frac{U}{\sqrt{3}} / -90^{\circ}$$

$$\overline{U}_B = \frac{U}{\sqrt{3}} / 30^{\circ}$$

$$\overline{U}_C = \frac{U}{\sqrt{3}} / 150^{\circ}$$





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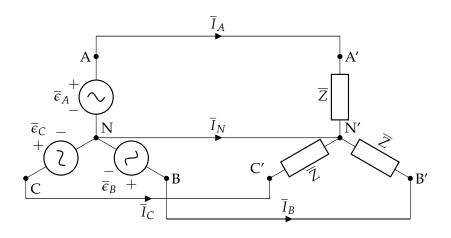
#### Tipos de Receptores

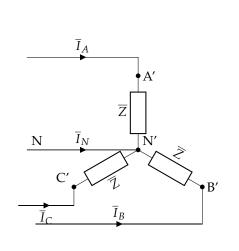
#### Conexión

- **Estrella** (punto común) Y
- ► Triángulo △

#### **Impedancias**

- **Equilibrado** (las tres impedancias son idénticas en módulo y fase).
- **▶** Desequilibrado





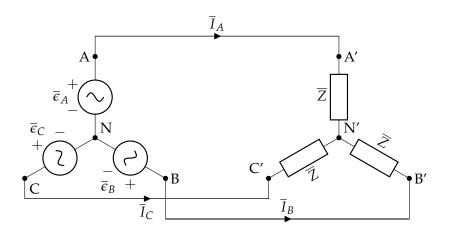
$$\bar{I}_A = \frac{\overline{U}_A}{\overline{Z}} = \frac{U_f}{Z} / \pm 90^\circ - \theta$$

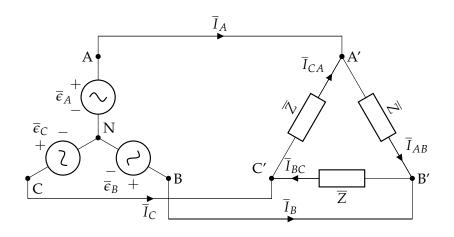
$$\bar{I}_B = \frac{\overline{U}_B}{\overline{Z}} = \frac{U_f}{Z} / \mp 30^\circ - \theta$$

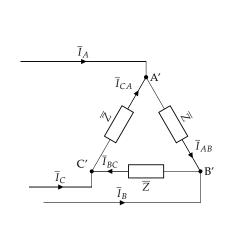
$$\bar{I}_C = \frac{\overline{U}_C}{\overline{Z}} = \frac{U_f}{Z} / \mp 150^\circ - \theta$$

$$|\bar{I}_A| = |\bar{I}_B| = |\bar{I}_C| = \frac{U_f}{Z}$$

$$\bar{I}_A + \bar{I}_B + \bar{I}_C + \bar{I}_N = 0$$
$$\bar{I}_A + \bar{I}_B + \bar{I}_C = 0 \rightarrow \boxed{\bar{I}_N = 0}$$







$$\bar{I}_{AB} = \frac{\overline{U}_{AB}}{\overline{Z}} = \frac{U}{Z} / \pm 120^{\circ} - \theta$$

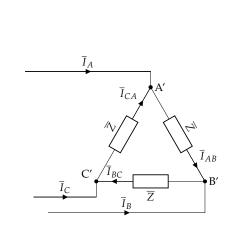
$$\bar{I}_{BC} = \frac{\overline{U}_{BC}}{\overline{Z}} = \frac{U}{Z} / 0 - \theta$$

$$\bar{I}_{CA} = \frac{\overline{U}_{CA}}{\overline{Z}} = \frac{U}{Z} / \mp 120^{\circ} - \theta$$

$$\bar{I}_{AB} + \bar{I}_{BC} + \bar{I}_{CA} = 0$$

Corriente de Fase:

$$\boxed{I_f = |\bar{I}_{AB}| = |\bar{I}_{BC}| = |\bar{I}_{CA}| = \frac{U}{Z}}$$



$$\bar{I}_A = \bar{I}_{AB} - \bar{I}_{CA} = \sqrt{3} \cdot \frac{U}{Z} / \pm 90^\circ - \theta$$

$$\bar{I}_B = \bar{I}_{BC} - \bar{I}_{AB} = \sqrt{3} \cdot \frac{U}{Z} / \mp 30^\circ - \theta$$

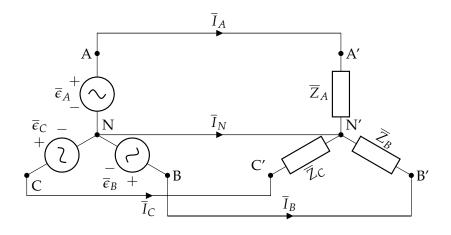
$$\bar{I}_C = \bar{I}_{CA} - \bar{I}_{BC} = \sqrt{3} \cdot \frac{U}{Z} / \mp 150^\circ - \theta$$

Corriente de Línea:

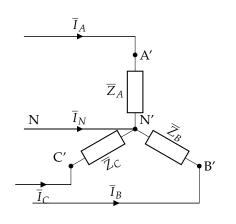
$$\boxed{I = |\bar{I}_A| = |\bar{I}_B| = |\bar{I}_C| = \sqrt{3} \cdot \frac{U}{Z}}$$

$$I = \sqrt{3} \cdot I_f$$

### Receptor en Estrella Desequilibrado con Neutro



## Receptor en Estrella Desequilibrado con Neutro



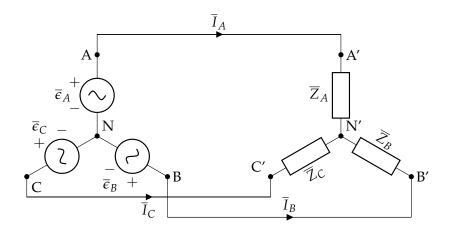
$$\bar{I}_{B} = \frac{\overline{U}_{B}}{\overline{Z}_{B}}$$

$$\bar{I}_{C} = \frac{\overline{U}_{C}}{\overline{Z}_{C}}$$

$$\bar{I}_{A} + \bar{I}_{B} + \bar{I}_{C} + \bar{I}_{N} = 0$$

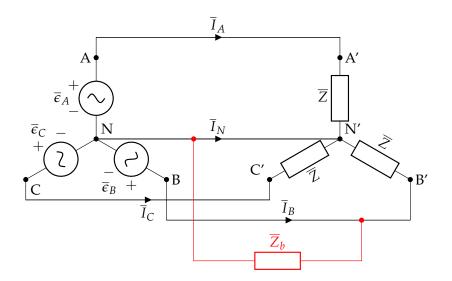
$$\bar{I}_{A} + \bar{I}_{B} + \bar{I}_{C} \neq 0 \rightarrow \boxed{\bar{I}_{N} \neq 0}$$

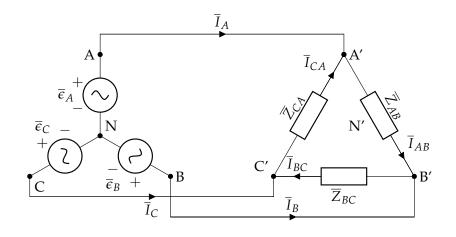
### Receptor en Estrella Desequilibrado sin Neutro

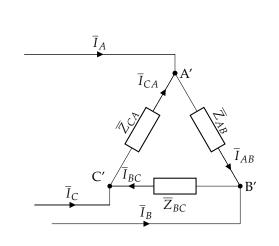


$$\overline{U}_N \neq \overline{U}_{N'}$$

### Receptor en Estrella con Carga Monofásica







$$\bar{I}_{AB} = \frac{\overline{U}_{AB}}{\overline{Z}_{AB}}$$

$$\bar{I}_{BC} = \frac{\overline{U}_{BC}}{\overline{Z}_{BC}}$$

$$\bar{I}_{CA} = \frac{\overline{U}_{CA}}{\overline{Z}_{CA}}$$

$$\begin{split} \bar{I}_A &= \bar{I}_{AB} - \bar{I}_{CA} \\ \bar{I}_B &= \bar{I}_{BC} - \bar{I}_{AB} \\ \bar{I}_C &= \bar{I}_{CA} - \bar{I}_{BC} \end{split}$$

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# Potencia Instantánea en Sistemas Equilibrados

$$u_{A}(t) = \sqrt{2}U_{f}\cos(\omega t + 90^{\circ})$$

$$u_{B}(t) = \sqrt{2}U_{f}\cos(\omega t - 30^{\circ})$$

$$u_{C}(t) = \sqrt{2}U_{f}\cos(\omega t - 150^{\circ})$$

$$p_{A}(t) = u_{A}(t) \cdot i_{A}(t)$$

$$p_{B}(t) = u_{C}(t) \cdot i_{B}(t)$$

$$p_{C}(t) = u_{C}(t) \cdot i_{C}(t)$$

$$i_{A}(t) = \sqrt{2}I_{f}\cos(\omega t + 90^{\circ} - \theta)$$

$$i_{B}(t) = \sqrt{2}I_{f}\cos(\omega t - 30^{\circ} - \theta)$$

$$i_{C}(t) = \sqrt{2}I_{f}\cos(\omega t - 150^{\circ} - \theta)$$

$$p(t) = p_{A}(t) + p_{B}(t) + p_{C}(t)$$

# Potencia Instantánea en Sistemas Equilibrados

$$p(t) = \sqrt{2}U_f \cos(\omega t + 90^\circ) \cdot \sqrt{2}I_f \cos(\omega t + 90^\circ - \theta) +$$

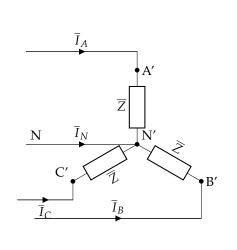
$$+ \sqrt{2}U_f \cos(\omega t - 30^\circ) \cdot \sqrt{2}I_f \cos(\omega t - 30^\circ - \theta) +$$

$$+ \sqrt{2}U_f \cos(\omega t - 150^\circ) \cdot \sqrt{2}I_f \cos(\omega t - 150^\circ - \theta)$$

$$\cos(\alpha) \cdot \cos(\beta) = \frac{1}{2} \cdot (\cos(\alpha + \beta) + \cos(\alpha - \beta))$$

$$p(t) = U_f I_f [\cos(2\omega t + 180^{\circ} - \theta) + \cos(\theta)] + U_f I_f [\cos(2\omega t - 60^{\circ} - \theta) + \cos(\theta)] + U_f I_f [\cos(2\omega t - 300^{\circ} - \theta) + \cos(\theta)]$$

$$p(t) = 3 \cdot U_f \cdot I_f \cdot \cos(\theta) = \sqrt{3} \cdot U \cdot I \cdot \cos(\theta)$$



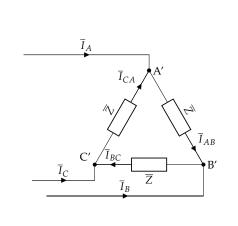
$$P = 3 \cdot P_Z = 3 \cdot U_Z I_Z \cos(\theta)$$
$$Q = 3 \cdot Q_Z = 3 \cdot U_Z I_Z \sin(\theta)$$

$$I_Z = I$$
$$U_Z = U_F$$

$$P = 3U_F I \cos(\theta) = \sqrt{3}UI \cos(\theta)$$

$$Q = 3U_F I \sin(\theta) = \sqrt{3}UI \sin(\theta)$$

$$S = \sqrt{P^2 + O^2} = \sqrt{3}UI$$



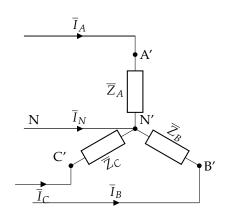
$$P = 3 \cdot P_Z = 3 \cdot U_Z I_Z \cos(\theta)$$
$$Q = 3 \cdot Q_Z = 3 \cdot U_Z I_Z \sin(\theta)$$

$$I_Z = I_F$$
$$U_Z = U$$

$$P = 3UI_F \cos(\theta) = \sqrt{3}UI \cos(\theta)$$

$$Q = 3UI_F \sin(\theta) = \sqrt{3}UI \sin(\theta)$$

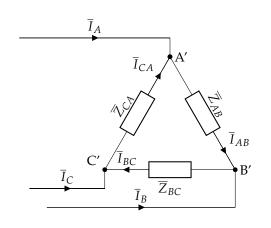
$$S = \sqrt{P^2 + Q^2} = \sqrt{3}UI$$



$$P = P_A + P_B + P_C$$

$$Q = Q_A + Q_B + Q_C$$

$$\overline{S} = P + jQ$$



$$P = P_{AB} + P_{BC} + P_{CA}$$

$$Q = Q_{AB} + Q_{BC} + Q_{CA}$$

$$\overline{S} = P + jQ$$

#### Comparativa Monofásica-Trifásica

Comparemos un sistema monofásico y un sistema trifásico (3H) que transmiten la misma potencia activa y funcionan a la misma tensión entre líneas.

$$UI_1\cos\theta = P_1 = P_3 = \sqrt{3}UI_3\cos\theta \rightarrow \boxed{I_1 = \sqrt{3}I_3}$$

Las **pérdidas en la línea** deben ser **iguales** para salvar la **misma distancia**:

$$2R_1I_1^2 = P_{1l} = P_{3l} = 3R_3I_3^2$$

Sustituyendo la relación de corrientes y teniendo en cuenta la relación entre resistencia y sección:

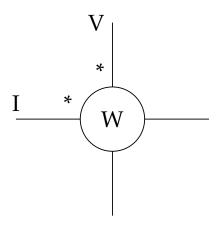
$$2 \cdot R_1 \cdot 3I_3^2 = 3 \cdot R_3I_3^2 \to R_1 = \frac{1}{2}R_3 \to \boxed{S_1 = 2 \cdot S_3}$$

Finalmente, la relación entre masas de conductor es:

$$\frac{m_3}{m_1} = \frac{3 \cdot S_3}{2 \cdot S_1} = \boxed{\frac{3}{4}}$$

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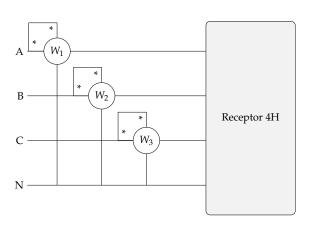
#### Recordatorio: vatímetro



**Vatímetro**: equipo de medida de 4 terminales (1 par para tensión, 1 par para corriente)

$$W = \Re(\overline{U} \cdot \overline{I}^*)$$

#### Sistema de 4 Hilos

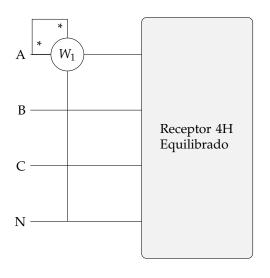


$$W_1 = \Re(\overline{U}_A \cdot \overline{I}_A^*) = P_A$$

$$W_2 = \Re(\overline{U}_B \cdot \overline{I}_B^*) = P_B$$

$$W_3 = \Re(\overline{U}_C \cdot \overline{I}_C^*) = P_C$$

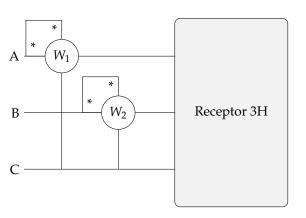
$$P = W_1 + W_2 + W_3$$



$$P_A = P_B = P_C$$

$$P = 3 \cdot W_1$$

#### Sistema de 3 Hilos



#### Montaje de Aron

$$W_1 = \Re(\overline{U}_{AC} \cdot \overline{I}_A^*)$$

$$W_2 = \Re(\overline{U}_{BC} \cdot \overline{I}_B^*)$$

$$W_1 + W_2 = ?$$

#### Sistema de 3 Hilos

Desarrollamos las dos expresiones usando corrientes de fase y obviando el operador  $\Re$ :

$$\overline{U}_{AC} \cdot \overline{I}_{A}^{*} = \overline{U}_{AC} \cdot (\overline{I}_{AB}^{*} - \overline{I}_{CA}^{*})$$

$$\overline{U}_{BC} \cdot \overline{I}_{B}^{*} = \overline{U}_{BC} \cdot (\overline{I}_{BC}^{*} - \overline{I}_{AB}^{*})$$

Sumamos las dos expresiones:

$$\overline{U}_{AC} \cdot \overline{I}_{A}^{*} + \overline{U}_{BC} \cdot \overline{I}_{B}^{*} = \overline{U}_{AC} \cdot \overline{I}_{AB}^{*} - \overline{U}_{AC} \cdot \overline{I}_{CA}^{*} + \overline{U}_{BC} \cdot \overline{I}_{BC}^{*} - \overline{U}_{BC} \cdot \overline{I}_{AB}^{*}$$

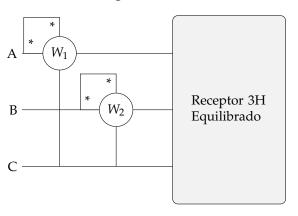
Y agrupamos, teniendo en cuenta que  $\overline{U}_{AB} + \overline{U}_{BC} + U_{CA} = 0$ :

$$\overline{U}_{CA} \cdot \overline{I}_{CA}^* + \overline{U}_{BC} \cdot \overline{I}_{BC}^* + (\overline{U}_{AC} \cdot \overline{I}_{AB}^* - \overline{U}_{BC} \cdot \overline{I}_{AB}^*) = \overline{S}_{CA} + \overline{S}_{BC} + \overline{S}_{AB}$$

Extrayendo la parte real de este resultado obtenemos:

$$\Re(\overline{S}_{AB} + \overline{S}_{BC} + \overline{S}_{CA}) = P \to \boxed{W_1 + W_2 = P}$$

Cuando el sistema es equilibrado, las lecturas individuales de los vatímetros tienen significado.



$$W_1 = \Re(\overline{U}_{AC} \cdot \overline{I}_A^*) = ?$$

$$W_2 = \Re(\overline{U}_{BC} \cdot \overline{I}_B^*) = ?$$

Supongamos SFD:

$$\overline{U}_{AC} = -\overline{U}_{CA} = U/-120^{\circ} + 180^{\circ} = U/60^{\circ}$$

$$\overline{I}_{A} = I/90^{\circ} - \theta$$

$$\overline{U}_{AC} \cdot \overline{I}_{A}^{*} = UI/\theta - 30^{\circ} \rightarrow \boxed{W_{1} = UI\cos(\theta - 30^{\circ})}$$

$$\overline{U}_{BC} = U/\underline{0}$$

$$\overline{I}_B = I/\underline{-30^\circ - \theta}$$

$$\overline{U}_{BC} \cdot \overline{I}_B^* = UI/\underline{\theta + 30^\circ} \rightarrow \boxed{W_2 = UI\cos(\theta + 30^\circ)}$$

Desarrollamos los dos cosenos:

$$\cos(30^{\circ} - \theta) = \cos 30^{\circ} \cos \theta + \sin 30^{\circ} \sin \theta$$
$$\cos(30^{\circ} + \theta) = \cos 30^{\circ} \cos \theta - \sin 30^{\circ} \sin \theta$$

Si sumamos obtenemos la potencia activa:

$$W_1 + W_2 = \sqrt{3}UI\cos\theta = P$$

Si restamos obtenemos la potencia reactiva (salvo un factor):

$$W_1 - W_2 = UI \sin \theta = \frac{Q}{\sqrt{3}}$$

Por tanto, también podemos calcular el ángulo del receptor:

$$\tan\theta = \sqrt{3} \frac{W_1 - W_2}{W_1 + W_2}$$

Repetimos el desarrollo con SFI:

$$\overline{U}_{AC} = -\overline{U}_{CA} = U/120^{\circ} + 180^{\circ} = U/-60^{\circ}$$

$$\overline{I}_{A} = I/-90^{\circ} - \theta$$

$$\overline{U}_{AC} \cdot \overline{I}_{A}^{*} = UI/\theta + 30^{\circ} \rightarrow W_{1} = UI\cos(\theta + 30^{\circ})$$

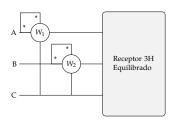
$$\overline{U}_{BC} = U/0$$

$$\overline{I}_{B} = I/30^{\circ} - \theta$$

$$\overline{U}_{BC} \cdot \overline{I}_{B}^{*} = UI/\theta - 30^{\circ} \rightarrow W_{2} = UI\cos(\theta - 30^{\circ})$$

$$W_{1} + W_{2} = \sqrt{3}UI\cos\theta = P$$

$$W_{1} - W_{2} = -UI\sin\theta = -\frac{Q}{\sqrt{3}}$$



SFD

$$W_1 = UI\cos(\theta - 30^\circ)$$

$$W_2 = UI\cos(\theta + 30^\circ)$$

$$Q = \sqrt{3}(W_1 - W_2)$$

$$\tan \theta = \sqrt{3} \frac{W_1 - W_2}{W_1 + W_2}$$

 $P = W_1 + W_2$ 

SFI

$$W_1 = UI\cos(\theta + 30^\circ)$$
$$W_2 = UI\cos(\theta - 30^\circ)$$

 $P = W_1 + W_2$ 

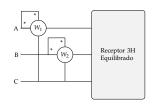
$$Q = \sqrt{3}(\frac{W_2 - W_1}{W_1})$$

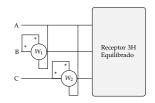
$$\tan \theta = \sqrt{3} \frac{W_2 - W_1}{W_1 + W_2}$$

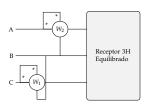
#### Otras conexiones: 3H SFD

$$(ABC) :: A \triangleright B \triangleright C \Longrightarrow \{AB, BC, CA\}$$

$$W_1 = UI\cos(\theta - 30^\circ)$$
  $P = W_1 + W_2$   
 $W_2 = UI\cos(\theta + 30^\circ)$   $Q = \sqrt{3}(W_1 - W_2)$ 







 $W_1 : AC \notin SFD$  $W_2 : BC \in SFD$   $W_1: BA \notin SFD$ 

 $W_2: CA \in SFD$ 

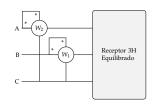
 $W_1: CB \notin SFD$ 

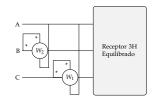
 $W_2: AB \in SFD$ 

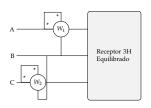
#### Otras conexiones: 3H SFI

$$(ACB) :: A \triangleright C \triangleright B \Longrightarrow \{AC, CB, BA\}$$

$$W_1 = UI\cos(\theta - 30^\circ)$$
  $P = W_1 + W_2$   
 $W_2 = UI\cos(\theta + 30^\circ)$   $Q = \sqrt{3}(W_1 - W_2)$ 







 $W_1: BC \notin SFI$  $W_2: AC \in SFI$   $W_1: CA \notin SFI$ 

 $W_2: BA \in SFI$ 

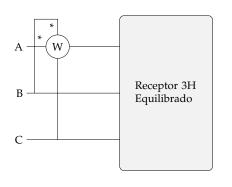
 $W_1: AB \notin SFI$ 

 $W_2: CB \in SFI$ 

#### Medida de Reactiva con un Vatímetro

Cuando el sistema está equilibrado, es posible medir la potencia reactiva con un único vatímetro.

#### Supongamos SFD:



$$W = \Re(\overline{U}_{BC} \cdot \overline{I}_{A}^{*})$$

$$\overline{U}_{BC} = U/\underline{0}$$

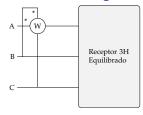
$$\overline{I}_{A} = I/\underline{90^{\circ} - \theta}$$

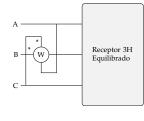
$$W = \Re(UI/\underline{\theta - 90^{\circ}}) =$$

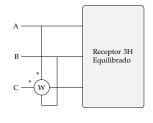
$$= UI \sin(\theta)$$

$$W = \frac{Q}{\sqrt{2}}$$

# Conexiones para medida de reactiva







$$W=\Re(\overline{U}_{BC}\cdot\overline{I}_A^*)$$

 $W = \Re(\overline{U}_{CA} \cdot \overline{I}_{R}^{*})$ 

$$AB \in SFD$$
  
 $AB \notin SFI$ 

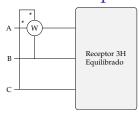
 $W = \Re(\overline{U}_{AB} \cdot \overline{I}_{C}^{*})$ 

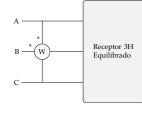
$$BC \in SFD$$
  
 $BC \notin SFI$ 

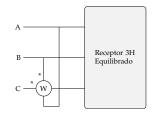
$$SFD \rightarrow \boxed{W = \frac{Q}{\sqrt{3}}}$$

$$SFI \to W = -\frac{Q}{\sqrt{3}}$$

# Conexiones para medida de reactiva







$$W=\Re(\overline{U}_{CB}\cdot\overline{I}_A^*)$$

 $AC \in SFI$ 

 $W = \Re(\overline{U}_{AC} \cdot \overline{I}_{R}^{*})$ 

 $W = \Re(\overline{U}_{BA} \cdot \overline{I}_C^*)$ 

$$CB \notin SFD$$
  
 $CB \in SFI$ 

$$\rightarrow W = -\frac{Q}{\sqrt{3}}$$

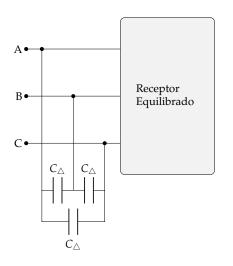
$$=\frac{\sqrt{3}}{\sqrt{3}}$$

- 1 Introducción
- 2 Generadores
- Receptores
- 4 Potencia en Sistemas Trifásicos
- 6 Medida de Potencia en Sistemas Trifásicos
- 6 Compensación de Reactiva

### Objetivo

- Sea un receptor **equilibrado inductivo** del que conocemos P, Q y, por tanto, su factor de potencia  $\cos \theta$ .
- ▶ Para reducir la potencia reactiva del sistema debemos instalar un banco de condensadores que suministrarán una potencia reactiva Q<sub>c</sub>.
- ► Como **resultado**, la potencia reactiva y el factor de potencia del sistema serán  $Q' = Q Q_c$  y  $\cos \theta' > \cos \theta$ .
- ► En trifásica existen dos posibilidades:
  - ightharpoonup Conexión en triángulo:  $C_{\triangle}$
  - ightharpoonup Conexión en estrella:  $C_{\gamma}$ .

### Conexión en Triángulo



$$Q = P \tan \theta$$

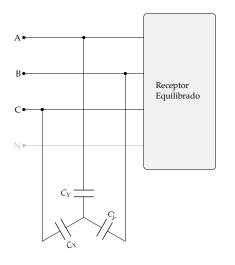
$$Q' = P \tan \theta' =$$

$$= Q - Q_c$$

$$Q_c = 3 \cdot \omega C_{\triangle} \cdot U^2$$

$$C_{\triangle} = \frac{P(\tan\theta - \tan\theta')}{3\omega U^2}$$

#### Conexión en Estrella



$$Q = P \tan \theta$$

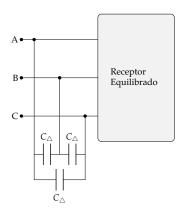
$$Q' = P \tan \theta' =$$

$$= Q - Q_c$$

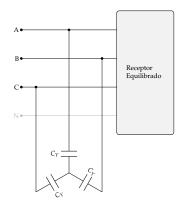
$$Q_c = 3 \cdot \omega C_Y \cdot U_f^2$$

$$C_Y = \frac{P(\tan \theta - \tan \theta')}{\omega U^2}$$

# Comparación Estrella-Triángulo



$$C_{\triangle} = \frac{P(\tan\theta - \tan\theta')}{3\omega U^2}$$



$$C_Y = \frac{P(\tan \theta - \tan \theta')}{\omega U^2}$$

Dado que  $C_Y = 3 \cdot C_{\triangle}$  la **configuración recomendada** es **triángulo**.