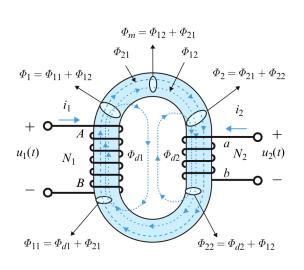
Transformadores Teoría de Circuitos II

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Recordatorio



$$L_1 = N_1 \frac{\phi_{11}}{i_1}$$

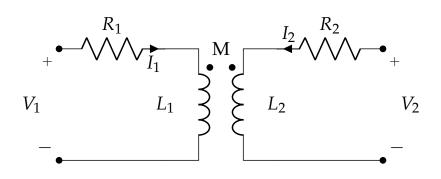
$$L_2 = N_2 \frac{\phi_{22}}{i_2}$$

$$M = N_1 \frac{\phi_{12}}{i_2}$$
$$= N_2 \frac{\phi_{21}}{i_1}$$

$$M = k\sqrt{L_1 \cdot L_2}$$

- Transformador Real
- Transformador Perfecto
- Transformador Idea
- Transferencia de Circuitos
- 5 Transformador Perfecto vs. Transformador Ideal
- Transformador de Varios Devanados
- Autotransformador

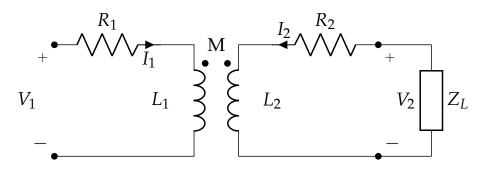
Ecuaciones del Transformador Real



$$\overline{U}_1 = (R_1 + j\omega L_1) \cdot \overline{I}_1 + j\omega M \cdot \overline{I}_2$$

$$\overline{U}_2 = j\omega M \cdot \overline{I}_1 + (R_2 + j\omega L_2) \cdot \overline{I}_2$$

Ejemplo: impedancia de entrada desde primario



Ecuaciones del transformador

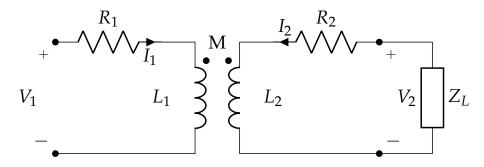
$$\overline{U}_1 = (R_1 + j\omega L_1) \cdot \overline{I}_1 + j\omega M \cdot \overline{I}_2$$

$$\overline{U}_2 = j\omega M \cdot \overline{I}_1 + (R_2 + j\omega L_2) \cdot \overline{I}_2$$

Ecuación de la carga

$$\overline{U}_2 = -\overline{I}_2 \cdot \overline{Z}_L$$

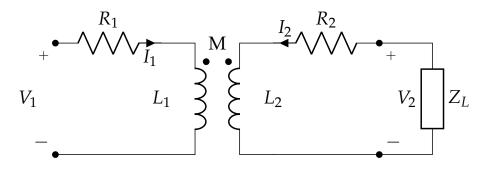
Ejemplo: impedancia de entrada desde primario



Combinando la ecuación del secundario con la ecuación de la carga:

$$\bar{I}_2 = -\frac{j\omega M}{\overline{Z}_L + (R_2 + j\omega L_2)} \cdot \bar{I}_1$$

Ejemplo: impedancia de entrada desde primario

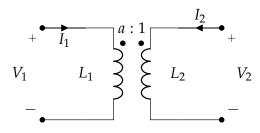


Combinando con la ecuación del primario:

$$\overline{Z}_{in} = \frac{\overline{V}_1}{\overline{I}_1} = (R_1 + j\omega L_1) + \frac{\omega^2 M^2}{\overline{Z}_L + (R_2 + j\omega L_2)}$$

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Definición



Las pérdidas resistivas son despreciables.

$$R_1 = R_2 = 0$$

El acoplamiento es perfecto.

$$k = 1 \rightarrow \left\{ \begin{array}{ll} \phi_{12} &= \phi_{22} \\ \phi_{21} &= \phi_{11} \end{array} \right.$$

Relación de Transformación

Retomamos las ecuaciones de $M_{12} = M_{21} = M$:

$$N_1 \frac{\phi_{12}}{i_2} = N_2 \frac{\phi_{21}}{i_1}$$

Con la condición k = 1 escribimos:

$$N_1 \frac{\phi_{22}}{i_2} = N_2 \frac{\phi_{11}}{i_1}$$

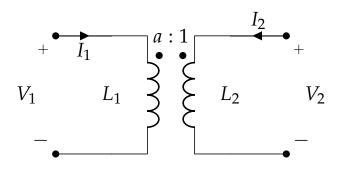
Y con las definiciones de L_1 y L_2 :

$$N_1 \frac{L_2}{N_2} = N_2 \frac{L_1}{N_1}$$

Obtenemos la relación de transformación:

$$\frac{L_1}{L_2} = \left(\frac{N_1}{N_2}\right)^2 = a^2$$

Ecuaciones del Transformador Perfecto



$$\overline{U}_1 = j\omega L_1 \cdot \overline{I}_1 + j\omega M \cdot \overline{I}_2$$

$$\overline{U}_2 = j\omega M \cdot \overline{I}_1 + j\omega L_2 \cdot \overline{I}_2$$

Relación de Tensiones

Dividiendo las ecuaciones:

$$\frac{\overline{U}_1}{\overline{U}_2} = \frac{j\omega L_1 \cdot \overline{I}_1 + j\omega M \cdot \overline{I}_2}{j\omega M \cdot \overline{I}_1 + j\omega L_2 \cdot \overline{I}_2}$$

Empleando la relación de transformación:

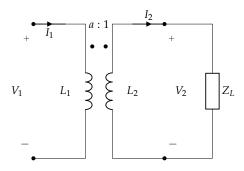
$$\frac{L_1}{L_2} = a^2 \rightarrow \left\{ \begin{array}{ll} L_1 &= a^2 \cdot L_2 \\ M &= a \cdot L_2 \end{array} \right.$$

Obtenemos:

$$\frac{\overline{U}_1}{\overline{U}_2} = \frac{a^2L_2 \cdot \overline{I}_1 + aL_2 \cdot \overline{I}_2}{aL_2 \cdot \overline{I}_1 + L_2 \cdot \overline{I}_2}$$

$$\boxed{\frac{\overline{U}_1}{\overline{U}_2} = a = \frac{N_1}{N_2}}$$

Ejemplo: Impedancia de Entrada



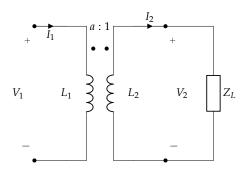
Ecuaciones del transformador:

$$\begin{aligned} \overline{U}_1 &= j\omega L_1 \cdot \overline{I}_1 - j\omega M \cdot \overline{I}_2 \\ \overline{U}_2 &= j\omega M \cdot \overline{I}_1 - j\omega L_2 \cdot \overline{I}_2 \end{aligned}$$

Ecuación de la impedancia:

$$\overline{U}_2 = \overline{Z}_L \cdot \overline{I}_2$$

Ejemplo: Impedancia de Entrada



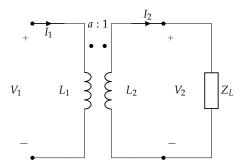
Despejamos I_2 :

$$\bar{I}_2 = \frac{j\omega M}{j\omega L_2 + \overline{Z}_L} \cdot \bar{I}_1$$

Y sustituimos:

$$\overline{Z}_{in} = \frac{\overline{U}_1}{\overline{I}_1} = j\omega L_1 + \frac{j\omega M}{j\omega L_2 + \overline{Z}_L}$$

Ejemplo: Impedancia de Entrada

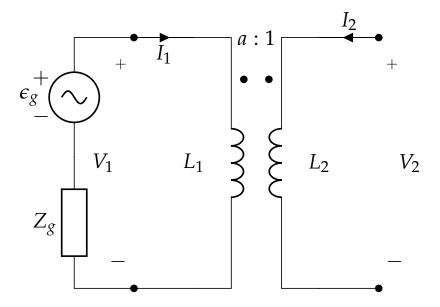


Teniendo en cuenta la relación entre L_1 , L_2 y M:

$$\overline{Z}_{in} = \frac{j\omega L_1 \cdot (a^2 \overline{Z}_L)}{j\omega L_1 + (a^2 \cdot \overline{Z}_L)}$$

$$\overline{Z}_{in} = a^2 \cdot \frac{j\omega L_2 \cdot \overline{Z}_L}{j\omega L_2 + \overline{Z}_L}$$

Ejemplo: Equivalente de Thévenin desde secundario



Tensión de Thévenin

Ecuaciones del transformador:

$$\bar{I}_2 = 0 \rightarrow \left\{ \begin{array}{ll} \overline{U}_1 & = j\omega L_1 \cdot \bar{I}_1 \\ \overline{U}_2 & = j\omega M \cdot \bar{I}_1 \end{array} \right.$$

Ecuación del generador:

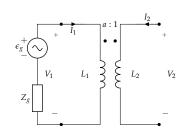
$$\overline{U}_1 = \overline{\epsilon}_g - \overline{I}_1 \cdot \overline{Z}_g$$

Tensión en abierto:

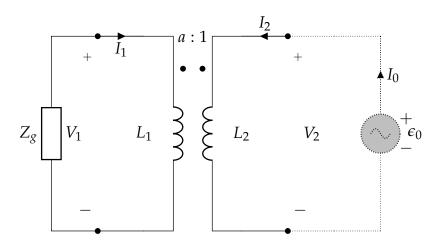
$$\overline{\epsilon}_{th} = \frac{j\omega M}{j\omega L_1 + \overline{Z}_g} \cdot \overline{\epsilon}_g$$

Teniendo en cuenta que $M = L_1/a$:

$$\overline{\epsilon}_{th} = \frac{1}{a} \cdot \left(\frac{j\omega L_1}{j\omega L_1 + \overline{Z}_g} \right) \cdot \overline{\epsilon}_g$$



Impedancia de Thévenin



Impedancia de Thévenin

Ecuaciones del transformador:

$$\overline{U}_1 = j\omega L_1 \cdot \overline{I}_1 + j\omega M \cdot \overline{I}_0$$
$$\overline{\epsilon}_0 = j\omega M \cdot \overline{I}_1 + j\omega L_2 \cdot \overline{I}_0$$

Ecuación de la impedancia:

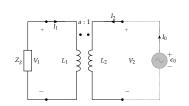
$$\overline{U}_1 = -\overline{Z}_g \cdot \overline{I}_1$$

Impedancia de Thévenin:

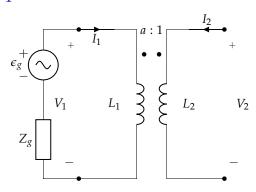
$$\overline{Z}_{th} = \frac{\overline{\epsilon}_0}{\overline{I}_0} = j\omega L_2 + \frac{\omega^2 M^2}{j\omega L_1 + \overline{Z}_g}$$

Con
$$L_2 = L_1/a^2$$
 y $M = L_1/a$:

$$\overline{Z}_{th} = \frac{1}{a^2} \cdot \frac{j\omega L_1 \cdot \overline{Z}_g}{j\omega L_1 + \overline{Z}_g}$$



Resumen: Equivalente de Thévenin

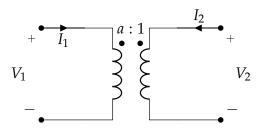


$$\overline{Z}_{th} = \frac{1}{a^2} \cdot \frac{j\omega L_1 \cdot \overline{Z}_g}{j\omega L_1 + \overline{Z}_g}$$

$$\overline{\epsilon}_{th} = \frac{1}{a} \cdot \left(\frac{j\omega L_1}{j\omega L_1 + \overline{Z}_g}\right) \cdot \overline{\epsilon}_g$$

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Definición



Las pérdidas resistivas son despreciables.

$$R_1 = R_2 = 0$$

El acoplamiento es perfecto.

$$k = 1$$

Las bobinas tienen un número muy elevado de espiras.

$$N_1 \to \infty$$

$$N_2 \to \infty$$

El flujo en cada bobina es nulo

Para que las tensiones inducidas sean finitas...

$$\overline{U}_1 = N_1 \overline{\phi}_1$$

$$\overline{U}_2 = N_2 \overline{\phi}_2$$

...los flujos (fasoriales) que los atraviesan deben ser nulos.

$$\frac{\overline{\phi}_1 \to 0}{\overline{\phi}_2 \to 0}$$

Siendo:

$$\overline{\phi}_1 = \overline{\phi}_{11} + \overline{\phi}_{12}$$

$$\overline{\phi}_2 = \overline{\phi}_{22} + \overline{\phi}_{21}$$

El flujo mutuo es nulo

Teniendo en cuenta que el acoplamiento es perfecto, k = 1:

$$\begin{array}{ccc} \phi_{12} & = \phi_{22} \\ \phi_{21} & = \phi_{11} \end{array} \right\} \rightarrow \left\{ \begin{array}{ccc} 0 & = \overline{\phi}_{21} + \overline{\phi}_{12} \\ 0 & = \overline{\phi}_{12} + \overline{\phi}_{21} \end{array} \right.$$

O también:

$$\boxed{\overline{\phi}_{11} + \overline{\phi}_{22} = 0}$$

Relación de Transformación

Hemos obtenido:

$$\overline{\phi}_{11} + \overline{\phi}_{22} = 0$$

Con las definiciones de L_1 , L_2 :

$$L_1 = N_1 \frac{\phi_{11}}{I_1}; \quad L_2 = N_2 \frac{\phi_{22}}{I_2}$$

Podemos escribir:

$$\frac{L_1\bar{I}_1}{N_1} + \frac{L_2\bar{I}_2}{N_2} = 0$$

Y con la relación entre ambas obtenemos

$$L_1 = L_2 \cdot \left(\frac{N_1}{N_2}\right)^2 \to \frac{N_1 L_2 \bar{I}_1}{N_2^2} + \frac{L_2 \bar{I}_2}{N_2} = 0 \to \boxed{\frac{\bar{I}_1}{\bar{I}_2} = \mp \frac{1}{a} = \mp \frac{N_2}{N_1}}$$

Un transformador ideal no consume potencia

$$\overline{S}_1 = \overline{V}_1 \cdot \overline{I}_1^*$$

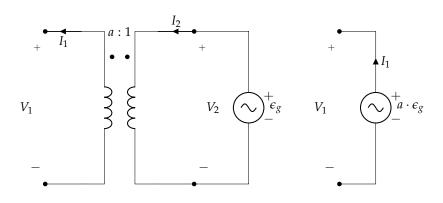
$$\overline{S}_2 = \overline{V}_2 \cdot \overline{I}_2^*$$

$$\overline{V}_2 \cdot \overline{I}_2^* = \frac{1}{a} \cdot \overline{V}_1 \cdot a \cdot \overline{I}_1^* = \overline{S}_1$$

$$\overline{S}_1 = \overline{S}_2 \qquad \boxed{P_1 = P_2} \qquad \boxed{Q_1 = Q_2}$$

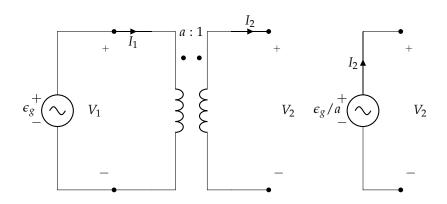
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Fuente de Tensión de Secundario a Primario



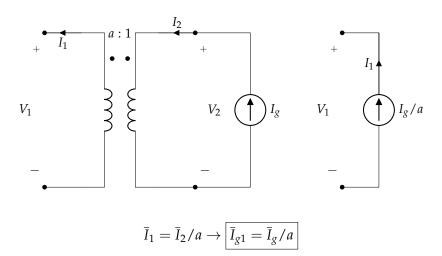
$$\overline{V}_1 = a \cdot \overline{V}_2 \rightarrow \overline{\epsilon}_{g1} = a \cdot \overline{\epsilon}_g$$

Fuente de Tensión de Primario a Secundario

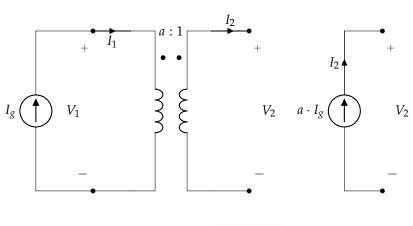


$$\overline{V}_2 = \overline{V}_1/a \rightarrow \boxed{\overline{\epsilon}_{g2} = \overline{\epsilon}_g/a}$$

Fuente de Corriente de Secundario a Primario

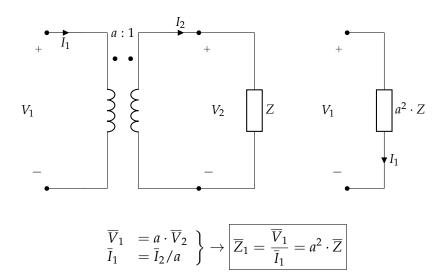


Fuente de Corriente de Primario a Secundario

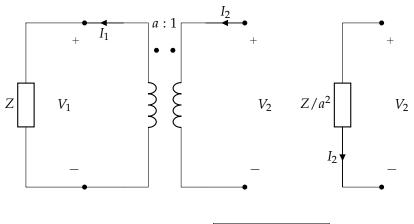


$$\bar{I}_2 = a \cdot \bar{I}_1 \rightarrow \boxed{\bar{I}_{g2} = a \cdot \bar{I}_g}$$

Impedancia de Secundario a Primario



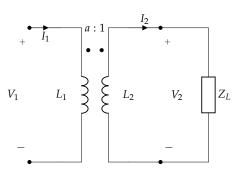
Impedancia de Primario a Secundario



$$\begin{vmatrix} \overline{V}_2 & = \overline{V}_1/a \\ \overline{I}_2 & = a \cdot \overline{I}_1 \end{vmatrix} \rightarrow \overline{Z}_2 = \frac{\overline{V}_2}{\overline{I}_2} = \overline{Z}/a^2$$

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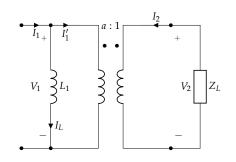
Recordatorio: impedancia de entrada de un T. Perfecto



$$\overline{Z}_{in} = \frac{j\omega L_1 \cdot (a^2 \overline{Z}_L)}{j\omega L_1 + (a^2 \cdot \overline{Z}_L)}$$

$$\overline{Z}_{in} = a^2 \cdot \frac{j\omega L_2 \cdot \overline{Z}_L}{j\omega L_2 + \overline{Z}_L}$$

Circuito equivalente con transformador ideal

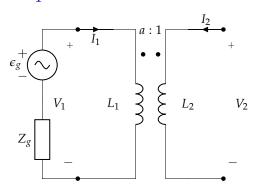


$$V_1$$
 V_2
 V_2
 V_2
 V_2
 V_2
 V_2
 V_2
 V_3
 V_4
 V_4
 V_4
 V_5
 V_5
 V_6
 V_7
 V_8
 V_8
 V_9
 V_9

$$\overline{Z}_{in} = \frac{j\omega L_1 \cdot (a^2 \overline{Z}_L)}{j\omega L_1 + (a^2 \cdot \overline{Z}_L)}$$

$$\overline{Z}_{in} = a^2 \cdot \frac{j\omega L_2 \cdot \overline{Z}_L}{j\omega L_2 + \overline{Z}_L}$$

Recordatorio: Equivalente de Thévenin



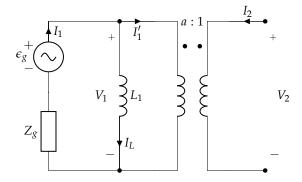
$$\overline{Z}_{th} = \frac{1}{a^2} \cdot \frac{j\omega L_1 \cdot \overline{Z}_g}{j\omega L_1 + \overline{Z}_g}$$

$$\overline{\epsilon}_{th} = \frac{1}{a} \cdot \left(\frac{j\omega L_1}{j\omega L_1 + \overline{Z}_g}\right) \cdot \overline{\epsilon}_g$$

Equivalente en primario con transformador ideal

$$\overline{Z}_{th} = \frac{1}{a^2} \cdot \frac{j\omega L_1 \cdot \overline{Z}_g}{j\omega L_1 + \overline{Z}_g}$$

$$\overline{\epsilon}_{th} = \frac{1}{a} \cdot \left(\frac{j\omega L_1}{j\omega L_1 + \overline{Z}_g}\right) \cdot \overline{\epsilon}_g$$



Equivalente en secundario con transformador ideal

$$\overline{Z}_{th} = a^2 \cdot \frac{j\omega L_2 \cdot \overline{Z}_g}{j\omega L_2 + \overline{Z}_g}$$

$$\overline{\epsilon}_{th} = a \cdot \left(\frac{j\omega L_2}{j\omega L_2 + \overline{Z}_g}\right) \cdot \overline{\epsilon}_g$$

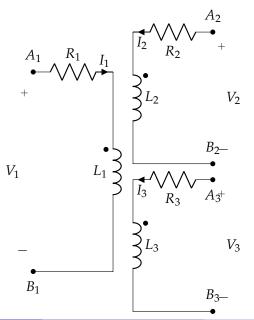
$$a : 1$$

$$\epsilon_{g}$$

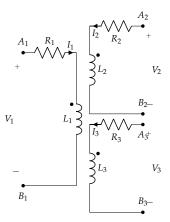
$$L_2 > V_2$$

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Transformador Real de Varios Devanados

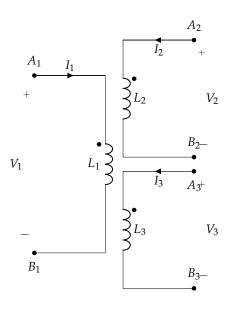


Ecuaciones del Transformador Real



$$\overline{U}_{1} = (R_{1} + j\omega L_{1}) \cdot \overline{I}_{1} + j\omega M_{12} \cdot \overline{I}_{2} + j\omega M_{13} \cdot \overline{I}_{3}
\overline{U}_{2} = j\omega M_{12} \cdot \overline{I}_{1} + (R_{2} + j\omega L_{2}) \cdot \overline{I}_{2} + j\omega M_{23} \cdot \overline{I}_{3}
\overline{U}_{3} = j\omega M_{13} \cdot \overline{I}_{1} + j\omega M_{12} \cdot \overline{I}_{2} + (R_{3} + j\omega L_{3}) \cdot \overline{I}_{3}$$

Transformador Perfecto



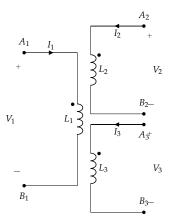
Las pérdidas resistivas son despreciables.

$$R_1 = R_2 = R_3 = 0$$

El acoplamiento es perfecto.

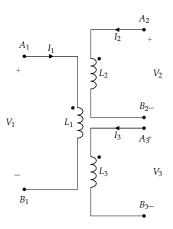
$$k_{12} = k_{13} = k_{23} = 1$$

Ecuaciones del Transformador Perfecto



$$\begin{split} \overline{U}_1 &= j\omega L_1 \cdot \overline{I}_1 + j\omega M_{12} \cdot \overline{I}_2 + j\omega M_{13} \cdot \overline{I}_3 \\ \overline{U}_2 &= j\omega M_{12} \cdot \overline{I}_1 + j\omega L_2 \cdot \overline{I}_2 + j\omega M_{23} \cdot \overline{I}_3 \\ \overline{U}_3 &= j\omega M_{13} \cdot \overline{I}_1 + j\omega M_{12} \cdot \overline{I}_2 + j\omega L_3 \cdot \overline{I}_3 \end{split}$$

Relaciones de Transformación



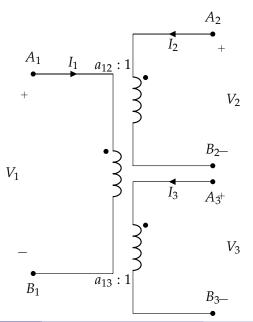
$$\frac{L_1}{L_2} = \left(\frac{N_1}{N_2}\right)^2 = a_{12}^2$$

$$\frac{L_1}{L_3} = \left(\frac{N_1}{N_3}\right)^2 = a_{13}^2$$

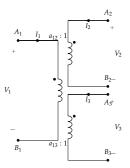
$$\frac{\overline{U}_1}{\overline{U}_2} = a_{12}$$

$$\frac{\overline{U}_1}{\overline{U}_1} = a_{13}$$

Transformador Ideal



Relación de Transformación del Transformador Ideal



Debido a las condiciones de idealidad:

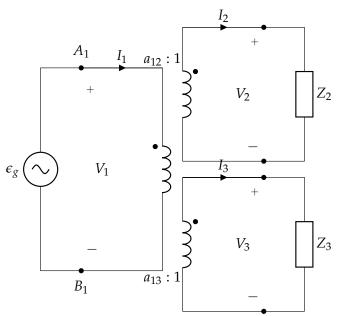
$$\overline{\phi}_{11} \pm \overline{\phi}_{22} \pm \overline{\phi}_{33} = 0$$

$$N_1 \bar{I}_1 \pm N_2 \bar{I}_2 \pm N_3 \bar{I}_3 = 0$$

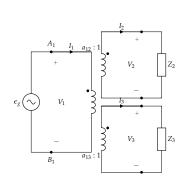
En términos de corriente:

$$\bar{I}_1 = \mp 1/a_{12} \cdot \bar{I}_2 \mp 1/a_{13} \cdot \bar{I}_3$$

Impedancia de Entrada



Impedancia de Entrada



Ecuaciones del transformador:

$$\overline{U}_1 = \overline{U}_2 \cdot a_{12}$$

$$\overline{U}_1 = \overline{U}_3 \cdot a_{13}$$

$$\overline{I}_1 = 1/a_{12} \cdot \overline{I}_2 + 1/a_{13} \cdot \overline{I}_3$$

Ecuaciones Terminales

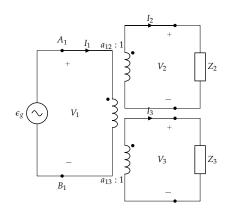
$$\overline{U}_2 = \overline{Z}_2 \cdot \overline{I}_2$$

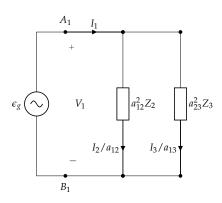
$$\overline{U}_3 = \overline{Z}_3 \cdot \overline{I}_3$$

Resultado:

$$\frac{\overline{I}_1}{\overline{U}_1} = \overline{\overline{Y}_{in}} = \frac{1}{a_{12}^2 \overline{Z}_2} + \frac{1}{a_{13}^2 \overline{Z}_3}$$

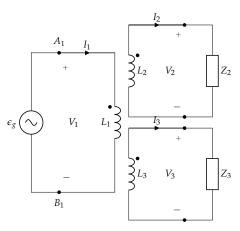
Circuito Equivalente



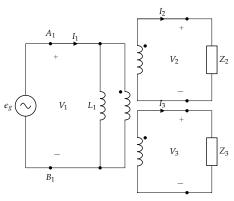


Circuito Equivalente de un Transformador Perfecto

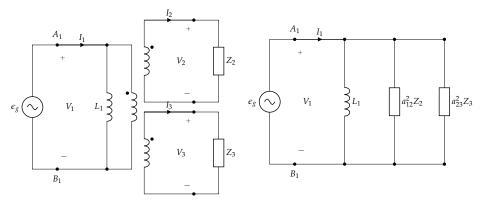
Transformador Perfecto



Equivalente Ideal

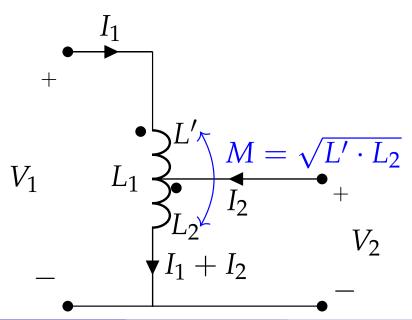


Circuito Equivalente de un Transformador Perfecto

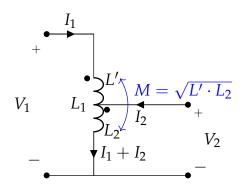


- Transformador Rea
- Transformador Perfecto
- Transformador Idea
- Transferencia de Circuitos
- 5 Transformador Perfecto vs. Transformador Ideal
- Transformador de Varios Devanados
- Autotransformador

Autotransformador Perfecto



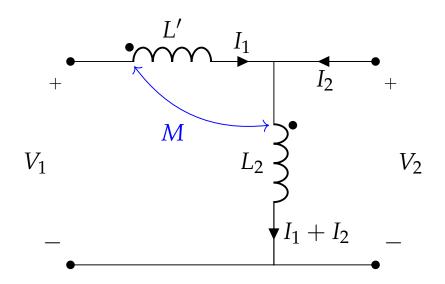
Ecuaciones del Autotransformador Perfecto



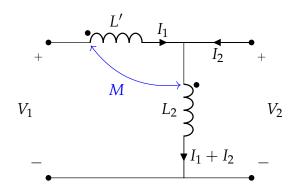
$$\overline{U}_1 = j\omega L_1 \cdot \overline{I}_1 + j\omega (M + L_2) \cdot \overline{I}_2$$

$$\overline{U}_2 = j\omega (M + L_2) \cdot \overline{I}_1 + j\omega L_2 \cdot \overline{I}_2$$

Circuito Alternativo del Autotransformador Perfecto

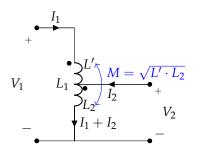


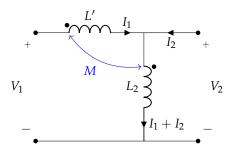
Ecuaciones del Circuito Alternativo



$$\begin{aligned} \overline{U}_1 &= j\omega(L' + L_2 + 2M) \cdot \overline{I}_1 + j\omega(L_2 + M) \cdot \overline{I}_2 \\ \overline{U}_2 &= j\omega(L_2 + M) \cdot \overline{I}_1 + j\omega L_2 \cdot \overline{I}_2 \end{aligned}$$

Ecuaciones Comparadas

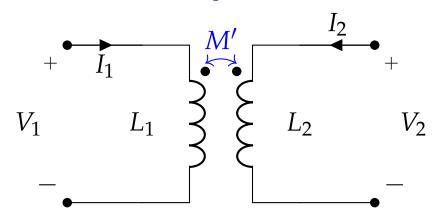




$$\begin{split} \overline{U}_1 &= j\omega L_1 \cdot \overline{I}_1 + j\omega (\mathbf{M} + \mathbf{L_2}) \cdot \overline{I}_2 = j\omega (\mathbf{L}' + \mathbf{L_2} + 2\mathbf{M}) \cdot \overline{I}_1 + j\omega (\mathbf{M} + \mathbf{L_2}) \cdot \overline{I}_2 \\ \overline{U}_2 &= j\omega (\mathbf{L_2} + \mathbf{M}) \cdot \overline{I}_1 + j\omega L_2 \cdot \overline{I}_2 = j\omega (\mathbf{L_2} + \mathbf{M}) \cdot \overline{I}_1 + j\omega L_2 \cdot \overline{I}_2 \end{split}$$

$$L_1 = L' + L_2 + 2M$$
$$M' = M + L_2$$

Transformador Perfecto Equivalente

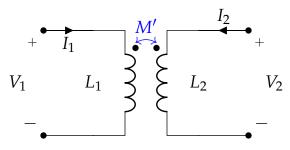


$$L_1 = L' + L_2 + 2M$$

$$M = \sqrt{L' \cdot L_2}$$

$$M' = M + L_2$$

Transformador Perfecto Equivalente



Comprobamos:

$$M' = \sqrt{L_1 \cdot L_2} =$$

$$= \sqrt{(L' + L_2 + 2M)L_2} =$$

$$= \sqrt{L'L_2 + L_2^2 + 2ML_2} =$$

$$= \sqrt{M^2 + L_2^2 + 2ML_2} =$$

$$= M + L_2$$

Autotransformador Ideal

