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## WATER TEMPERATURE CASE STUDY

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CE-QUAL-W2 Workshop

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US Army Corps  
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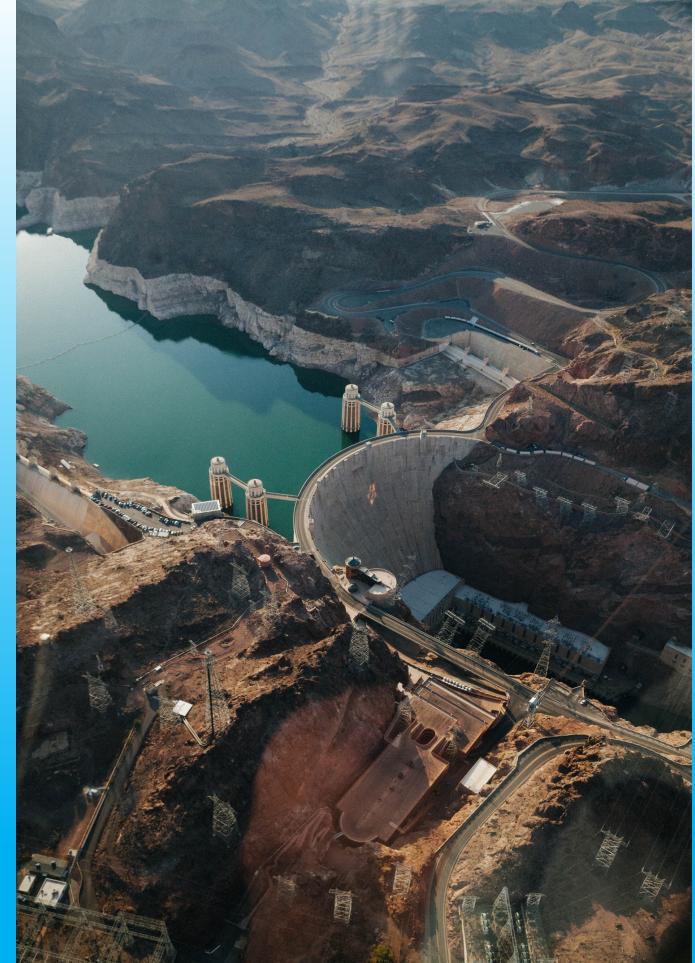
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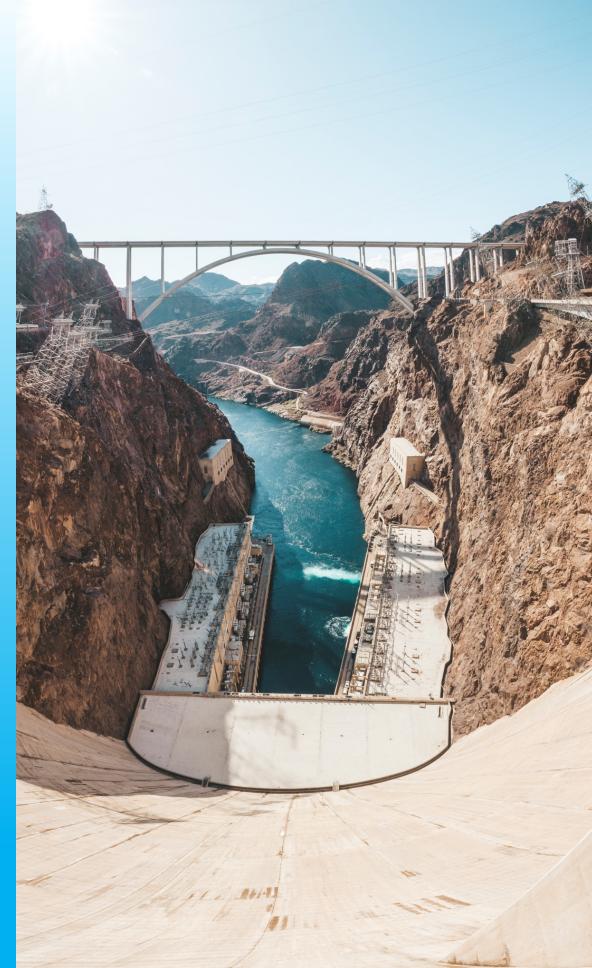
# Case Study Overview

- We will offer a 15-minute case study demonstration, which will walk through the model files
- Participants will become familiar with the location of temperature inputs and outputs in CE-QUAL-W2.
- We will focus on where temperature-related parameters appear in the control file, and the input and output files associated with running a successful temperature model.
- We will tie the theory section of the user-manual to the input/output section of the user-manual.
- This will be followed by a case-study where water quality parameters are changed, and output is analyzed.



## Start with an existing model

- We will use the DeGray Reservoir model, which is available automatically in the CE-QUAL-W2 download. It is currently set up to model sediment-diagenesis and vertical algae migration.
- We will edit it until it features only the essentials for modeling temperature.
- We are satisfied with the bathymetry and will not change it for this case study. It is simple, with one main waterbody and branch.



## W2 Model Input Files

Organized by File Directory – for me, C:\Users\b2edhijm\Documents\Projects\ERDC Steiss\August 22 Tutorial\Temperature Workshop\Practice\DeGray Reservoir with sediment diagenesis and vertical algae migration2

File type	Label in Control File	File name	
Control File	-	w2_con.csv	Sets many heat-flux control parameters
Wind sheltering	WSC FILE WSCFN	wsc.npt	Wind func impacts both sensible and latent flux
Shading	SHDFN	shade.npt	Local shading – not cloud cover
Bathymetry	BTHFN	bth1.csv	
Meteorological	METFN	met.npt	Sets many heat-flux control parameters
Branch inflow	QINFN branch inflow	qin_br1_equal.npt	
	TINFN branch temp	tin_br1.npt	AD equation – boundary conditions
	CINFN branch conc	cin_br1.csv	
	QDTFN Distributed flow	qin_br1.npt	
Spillway/Gate	QGTFN	qgt.npt	

# Advection Dispersion of Temp

## Advection-Dispersion Equation Balance

$$\frac{\partial B\phi}{\partial t} + \frac{\partial UB\phi}{\partial x} + \frac{\partial WB\phi}{\partial z} - \frac{\partial}{\partial x} [BD_x \frac{\partial \phi}{\partial x}] - \frac{\partial}{\partial z} [BD_z \frac{\partial \phi}{\partial z}] = q_\phi B + S_\phi B \quad (4-12)$$

where:

$\phi$  = laterally averaged constituent concentration,  $g m^{-3}$

$D_x$  = longitudinal temperature and constituent dispersion coefficient,  $m^2 sec^{-1}$

$D_z$  = vertical temperature and constituent dispersion coefficient,  $m^2 sec^{-1}$

$q_\phi$  = lateral inflow or outflow mass flow rate of constituent per unit volume,  $g m^{-3} sec^{-1}$

$S_\phi$  = laterally averaged source/sink term,  $g m^{-3} sec^{-1}$

Substitute H  
into the  
equation for  $\phi$ ,  
which relates to  
temperature as:

$$T = \frac{H}{\rho C_p V}$$

$$H = \rho C_p V T$$

cgs system:	mks system:
$\frac{cal}{cm^3 \cdot ^\circ C}$	$\frac{kg}{m^3 \cdot K}$
$1 cal = 4.168 J$	$1 J = 1 kg \cdot m^2 s^{-2}$

Units:

HYD PRINT - Print in the SNP file	HNAME	FMTH	HMULT	HPRWBC1	HPRWB
NVIOL - Violations of time step	"Timestep violat	(I10)		1	ON
U	"Horizontal velo	(f10.3)		1	ON
W	"Vertical velocity	(f10.3)		1	OFF
T	"Temperature [T]	(f10.3)		1	ON
RHO	"Density [RHO] g	(f10.3)		1	OFF
AZ	"Vertical eddy vi	(f10.3)		1	OFF
SHEAR	"Velocity shear s	(f10.3)		1	OFF
ST	"Internal shear [	(f10.3)		1	OFF
SB	"Bottom shear [t	(f10.3)		1	OFF
ADMX	"Longitudinal m	(f10.3)		1	OFF
DM	"Longitudinal m	(f10.3)		1	OFF
HDG	"Horizontal dent [	(f10.3)		1	OFF
ADMZ	"Vertical momen [	(f10.3)		1	OFF
HPG	"Horizontal pres [	(f10.3)		1	OFF
GRAV	"Gravity term ch	(f10.3)		1	OFF

- Temperature is included in the hydraulic calculations because it affects parameters like density and viscosity, i.e., we don't need to turn this on and off.
- We will need initial and boundary conditions (BC) for this – BCs for temperature in the tin\_br1.npt file

# Kinetics – Equilibrium Model or Term by Term?

Sources/Sinks from manual:

Term-by-term surface heat exchange is computed as:

$$\Phi_n = \Phi_s - \Phi_{sr} + \Phi_a - \Phi_{ar} - \Phi_{br} - \Phi_e - \Phi_c \quad (4-13)$$

where:

- $\phi_n$ : net surface heat flux,  $W m^{-2}$
- $\phi_s$ : incoming short-wave solar radiation,  $W m^{-2}$
- $\phi_{sr}$ : reflected short-wave solar radiation,  $W m^{-2}$
- $\phi_{sn}$ : net short-wave solar radiation,  $\phi_s - \phi_{sr}$ ,  $W m^{-2}$
- $\phi_a$ : incoming long-wave atmospheric radiation,  $W m^{-2}$
- $\phi_{ar}$ : reflected atmospheric long-wave radiation,  $W m^{-2}$
- $\phi_{br}$ : back long-wave radiation,  $W m^{-2}$
- $\phi_e$ : evaporative heat loss,  $W m^{-2}$
- $\phi_c$ : conductive heat loss,  $W m^{-2}$

Heat Exchange Parameters in .xslm interface:

EQ process is described on pages 101-102 of manual part 2.

HEAT EXCHANGE	WB1	WB2	WB3	W
H_SLHTC - Heat computations - Equilibrium (ET) or Term-by-term (TERM)	TERM			
SROC - Read in Short wave solar radiation ON or OFF	OFF			
RHEVAP - Use Ryan-Harleman Evap Model - for cooling ponds ON or OFF	OFF			
METIC - Interpolate meteorological data ON or OFF	ON			
FETCHC - Heinz Stefan Lake fetch correction - there is already an internal fetch	OFF			
AFW - Evaporation coefficient		9.2		
BFW - Evaporation coefficient		0.46		
CFW - Evaporation coefficient		2		
WINDH - Wind height measurement above ground surface, m		10		

# Shortwave Solar Radiation

File input or computed?

HEAT EXCHANGE	WB1	WB2	WB3	W
H SLHTC - Heat computations - Equilibrium (ET) or Term-by-term (TERM)	TERM			
SROC - Read in Short wave solar radiation ON or OFF	OFF			
RHEVAP - Use Ryan-Harleman Evap Model - for cooling ponds ON or OFF	OFF			
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FETCHC - Heinz Stefan Lake fetch correction - there is already an internal fetch	OFF			
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BFW - Evaporation coefficient		0.46		
CFW - Evaporation coefficient		2		
WINDH - Wind height measurement above ground surface, m		10		

It is rare to have a good short-wave solar radiation data source. Therefore, W2 uses an empirical calculation of short-wave solar radiation based on solar altitude and other parameters, as described in the user-manual, page 95-96. Many of these parameters are based on lat/long and time of day.

# Shortwave Solar Radiation – Cloud Cover and Shade

The shortwave solar radiation is dampened by a cloud cover factor that gets defined in the meteorological file.

The shortwave solar radiation is also dampedened by a local shading factor defined in the **shade file**.

1980 DeGray Reservoir meteorology					
JDAY	TAIR	TDEW	WIND	PHI	CLOUD
1.000	2.2	-1.1	1.9	4.72	0.0
1.125	1.7	-1.1	2.3	4.37	0.0
1.250	0.0	-3.3	1.1	5.07	0.0
1.375	3.3	-0.6	2.3	4.37	0.0
1.500	11.1	1.1	2.7	5.07	0.0
1.625	13.9	-1.1	1.1	1.22	0.0
1.750	8.3	-0.6	2.3	2.62	0.0
1.875	6.7	-0.6	1.1	3.85	0.0
2.000	1.7	-1.7	0.0	0.00	0.0
2.125	1.1	-1.7	0.0	0.00	3.0
2.250	2.2	-1.1	1.9	4.02	3.0
2.375	5.0	1.1	2.3	4.37	8.0

W2	Shading	Input File,	Vegetatiand	Topograpcalibratveg	characteand	correctetopography							
Segment	DynSh	TTEleLB	TTEleRB	C1DisLB	C1DiRB	SRFLB1	SRFLB2	SRFRB1	SRFRB2	TOPO1	TOPO2	TOPO3	TOPO4
1	1												
2	1												
3	1												
4	1												
5	1												
6	1												
7	1												
8	1												
9	1												
10	1												
11	1												
12	1												
13	1												
14	1												
15	1												
16	1												

# Shortwave Solar Radiation – Penetration

Theory: Every cell in the model performs this computation.

Short wave solar radiation penetrates the surface and decays exponentially with depth according to Bear's Law (see Figure 53):

$$\phi_s(z) = (1 - \beta)\phi_{sn}e^{-\eta z} \quad (4-26)$$

where:

$\phi_s(z)$  =short wave radiation at depth z,  $W m^{-2}$

$\beta$  =fraction absorbed at the water surface

$\eta$  =extinction coefficient,  $m^{-1}$

$\phi_{sn}$  =net short-wave radiation reaching the surface,  $W m^{-2}$

## Model Input:

Extinction coefficient will be a combination of light extinction due to various constituents, such as suspended solids, algae, zooplankton, etc. Extinction will be a function of their concentrations.

EX COEF	WB1	WB2
EXH2O - water light extinction- 1/m	0.45	
EXSS - suspended solids light extinction- 1/m	0.01	
EXOM - extinction organic matter- 1/(m mg/l)	0.2	
BETA - fraction short wave absorbed on surface	0.45	
EXC - Read in light extinction time series ON or OFF	OFF	
EXIC - Interpolation of light extinction time series ON or OFF	OFF	
ALG EXTINCTION	EXA1	EXA2
Algae light extinction- 1/(m mg/l)	0.2	
ZOO EXTINCTION	EXZ1	EXZ2
Zooplankton light extinction- 1/(m mg/l)	0.2	
MACRO EXTINCTION	EXM1	EXM2
Macrophyte light extinction- 1/(m mg/l)	0.01	

# Longwave Radiation

- Longwave radiation from air to water and water back to air use the same formula, based on the temperature of the emitting body, the Stephan-Boltzmann coefficient, and the emissivity of the body.
- Emissivity is a function of vapor pressure, which can be calculated from the measured dew point.

```
ENTRY SURFACE_TERMS (TSUR)

! Partial water vapor pressure of air (mm hg)

! EA = EXP(2.3026*(9.5*TDEW(JW)/(TDEW(JW)+265.5)+0.6609))      ! SW 6/10/2011
! IF (TDEW(JW) > 0.0) EA = EXP(2.3026*(7.5*TDEW(JW)/(TDEW(JW)+237.3)+0.6609))
EA = DEXP(2.3026D0*(7.5D0*TDEW(JW)/(TDEW(JW)+237.3D0)+0.6609D0))

! Partial water vapor pressure at the water surface

IF(TSUR<0.0)THEN
ES = DEXP(2.3026D0*(9.5D0*TSUR/(TSUR+265.5D0)+0.6609D0))
ELSE
ES = DEXP(2.3026D0*(7.5D0*TSUR/(TSUR+237.3D0)+0.6609D0))
ENDIF
```

met - Notepad

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1980 DeGray Reservoir meteorology

JDAY	TAIR	TDEW	WIND	PHI	CLOUD
1.000	2.2	-1.1	1.9	4.72	0.0
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1.375	3.3	-0.6	2.3	4.37	0.0
1.500	11.1	1.1	2.7	5.07	0.0
1.625	13.9	-1.1	1.1	1.22	0.0
1.750	8.3	-0.6	2.3	2.62	0.0
1.875	6.7	-0.6	1.1	3.85	0.0
2.000	1.7	-1.7	0.0	0.00	0.0
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2.250	2.2	-1.1	1.9	4.02	3.0
2.375	5.0	1.1	2.3	4.37	8.0

*Fortran source code showing how vapor pressure is calculated*

# Latent Heat – Evaporation

Parameters that control evaporation are specified in the met data file and the control file.

Evaporative heat loss is computed as:

$$\phi_e = f(W_z)(e_s - e_a) \quad (4-24)$$

where:

$f(W_z)$  = evaporative wind speed function at wind height of z,  $W m^{-2} mm Hg^{-1}$   
 $e_s$  = saturation vapor pressure at the water surface,  $mm Hg$   
 $e_a$  = atmospheric vapor pressure,  $mm Hg$

Evaporative heat loss depends on air temperature and dew point temperature or relative humidity. Surface vapor pressure is computed from the surface temperature for each surface cell on each iteration.

The model user can include different evaporation formulations using an evaporation wind speed formula of the form

$$f(W_z) = a + bW_z^c \quad (4-27)$$

where:

$f(W_z)$  = wind speed function with wind measured at height z,  $W m^{-2} mm Hg^{-1}$   
 $a$  = empirical coefficient, 9.2 default  
 $b$  = empirical coefficient, 0.46 default  
 $c$  = empirical coefficient, 2 default  
 $W_z$  = wind speed measured at 2 m above the ground,  $m s^{-1}$

## ENTRY SURFACE\_TERMS (TSUR)

```
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EA = DEXP(2.3026D0*(7.5D0*TDEW(JW)/(TDEW(JW)+237.3D0)+0.6609D0))

! Partial water vapor pressure at the water surface

IF(TSUR<0.0)THEN
ES = DEXP(2.3026D0*(9.5D0*TSUR/(TSUR+265.5D0)+0.6609D0))
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ES = DEXP(2.3026D0*(7.5D0*TSUR/(TSUR+237.3D0)+0.6609D0))
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met - Notepad  
File Edit Format View Help  
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2.125	1.1	-1.7	0.0	0.00	3.0
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RHEVAP - Use Ryan-Harleman Evap Model - for cooling ponds ON or OFF	OFF			
METIC - Interpolate meteorological data ON or OFF	ON			
FETCHC - Heinz Stefan Lake fetch correction - there is already an internal fetch	OFF			
AFW - Evaporation coefficient		9.2		
BFW - Evaporation coefficient		0.46		
CFW - Evaporation coefficient		2		
WINDH - Wind height measurement above ground surface, m		10		

# Sensible Heat – Conduction and Convection

Surface heat conduction is computed as:

$$\phi_c = C_c f(W_z)(T_s - T_a) \quad (4-25)$$

where:

$C_c$  = Bowen's coefficient,  $0.47 \text{ mm Hg } ^\circ\text{C}^{-1}$  ← Constant

$T_a$  = air temperature,  $^\circ\text{C}$  ← Met file

# Temperature Output Comparison

Model run with (1) default DeGray settings and with (2) all accessory modules and water quality calculations turned off.

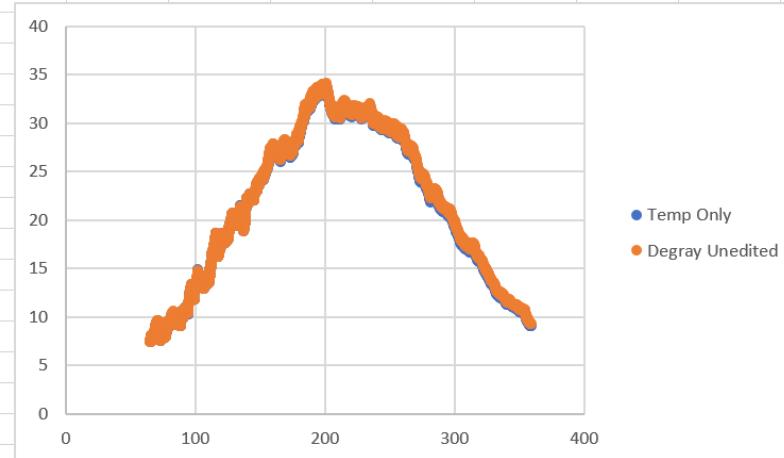
MISCELLANEOUS	NDAY	SELECTC	HABTATC	ENVIRPC	AERATEC	INITUWL	ORGCC	SED_DIAG
	100	OFF	OFF	OFF	OFF	OFF	OFF	OFF

CST COMP - Water quality computations	CCC	LIMC	CUF	CO2PPM	CO2YRLY	
CCC: Turn ON or OFF water quality calculations, LIMC: Limiting nutrient comp	OFF	ON	1	400	ON	

# Comparison at Layer 2

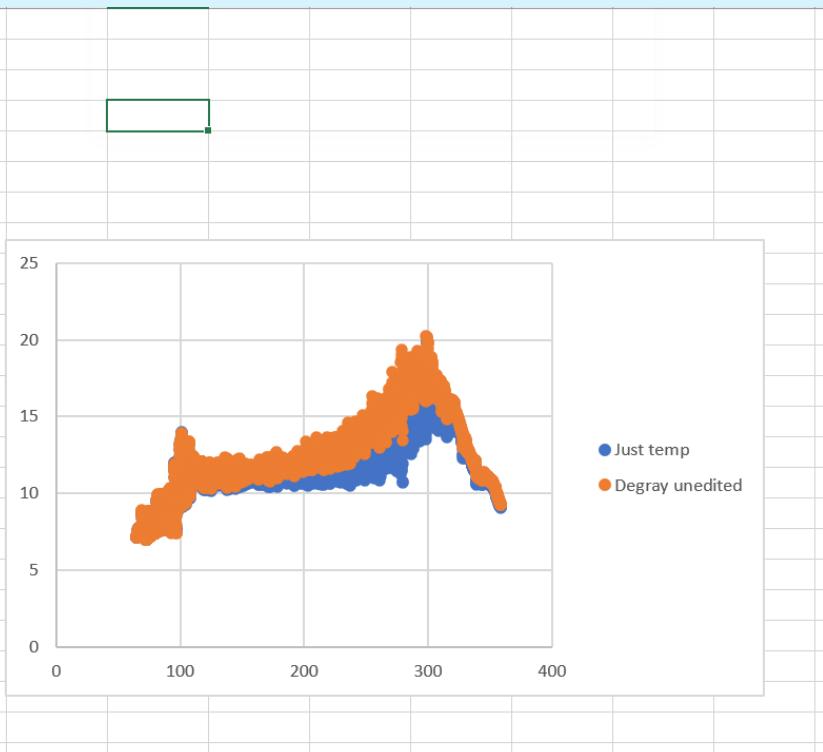
JUST TEMP		DEGRAY UNEDITED							
JDAY	Temp	JDAY	Temp	Difference	% Diff	Max % diff			
64.5	7.4	64.5	7.4	0	0	0.0250392			
64.604	7.515	64.604	7.517	0.002	0.000266				
64.701	7.557	64.701	7.56	0.003	0.000397				
64.806	7.561	64.806	7.562	0.001	0.000132				
64.903	7.575	64.903	7.576	0.001	0.000132				
65	7.599	65	7.6	0.001	0.000132				
65.104	7.594	65.104	7.592	-0.002	-0.00026				
65.201	7.538	65.201	7.536	-0.002	-0.00027				
65.306	7.491	65.306	7.489	-0.002	-0.00027				
65.403	7.52	65.403	7.519	-0.001	-0.00013				
65.5	7.718	65.5	7.724	0.006	0.000777				
65.604	7.962	65.604	7.992	0.03	0.003754				
65.701	8.078	65.701	8.114	0.036	0.004437				
65.806	8.026	65.806	8.064	0.038	0.004712				
65.903	7.973	65.903	8.011	0.038	0.004743				
66	7.93	66	7.969	0.039	0.004894				
66.104	7.889	66.104	7.928	0.039	0.004919				
66.201	7.85	66.201	7.887	0.037	0.004691				

The graph displays two data series: 'Temp Only' (blue circles) and 'Degray Unedited' (orange squares). Both series follow a similar trend, starting at approximately 8 on the y-axis at x=75, rising to a peak of about 34 at x=200, and then gradually declining to approximately 10 at x=375.



# Comparison at Layer 16

JUST TEMP		DEGRAY UNEDITED		Difference	% Diff	Max % diff
JDAY	Temp	JDAY	Temp			
64.5	7.2	64.5	7.2	0	0	0.256413148
64.604	7.186	64.604	7.186	0	0	
64.701	7.164	64.701	7.164	0	0	
64.806	7.129	64.806	7.129	0	0	
64.903	7.114	64.903	7.114	0	0	
65	7.131	65	7.132	0.001	0.00014	
65.104	7.195	65.104	7.195	0	0	
65.201	7.301	65.201	7.3	-0.001	-0.00014	
65.306	7.385	65.306	7.384	-0.001	-0.00014	
65.403	7.482	65.403	7.481	-0.001	-0.00013	
65.5	7.483	65.5	7.479	-0.004	-0.00053	
65.604	7.494	65.604	7.49	-0.004	-0.00053	
65.701	7.533	65.701	7.538	0.005	0.000663	
65.806	7.607	65.806	7.628	0.021	0.002753	
65.903	7.675	65.903	7.707	0.032	0.004152	
66	7.716	66	7.747	0.031	0.004002	
66.104	7.726	66.104	7.743	0.017	0.002196	
66.201	7.709	66.201	7.706	-0.003	-0.00039	
66.306	7.669	66.306	7.652	-0.017	-0.00222	
66.403	7.619	66.403	7.601	-0.018	-0.00237	
66.5	7.569	66.5	7.56	-0.009	-0.00119	
66.604	7.532	66.604	7.53	-0.002	-0.00027	
66.701	7.511	66.701	7.51	0.001	0.00012	



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# Questions?



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