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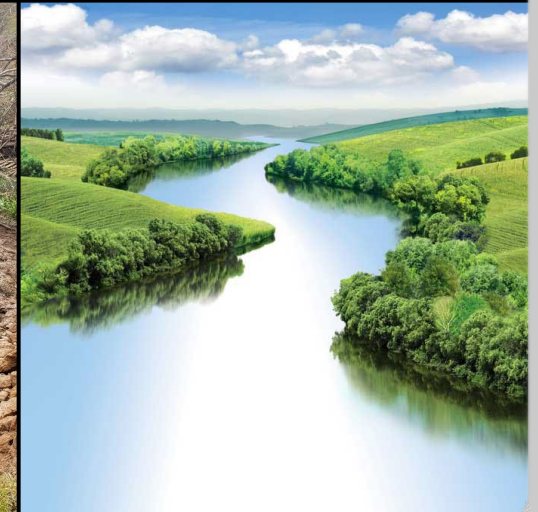
# TOTAL DISSOLVED GAS SIMULATION CASE STUDY

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US Army Corps  
of Engineers



Environmental Systems  
Modeling Team



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# TDG Saturation

- TDG refers to the total amount of dissolved gas present in water.
- High TDG concentrations can cause gas bubble disease and reduce the population of some fish species.
- Spillway operations result in atmospheric gases being forced into the water. The TDG concentrations below the dam are increased by spills, and TDG supersaturation occurs.





# TDG Saturation

Calculating and reporting dissolved gas levels from water quality monitoring

1) Ratio of total dissolved gas pressure (TGP) to atmospheric pressure.

$$TDG(\%) = 100 \frac{P_a + \Delta P}{P_a}$$

*TDG* = percent of total dissolved gas saturation (%),

$P_a$  = local barometric pressure or atmospheric pressure (mmHg),

$\Delta P$  = gauge pressure (mmHg), which can be directly measured by several types of instruments.

2) Gas concentrations measured in mg/L

$$TDG(\%) = \left( 79 \frac{N_2}{N_{2s}} - 21 \frac{DO}{DO_s} \right)$$

$N_2$  = dissolved nitrogen gas (mg L<sup>-1</sup>),

$N_{2s}$  = nitrogen gas saturation (mg L<sup>-1</sup>),

$DO$  = dissolved oxygen [mg-O<sub>2</sub> L<sup>-1</sup>],

$DO_s$  = dissolved oxygen saturation [mg-O<sub>2</sub> L<sup>-1</sup>].

# Overview of TDG Simulation in CE-QUAL-W2

TDG is computed as a derived variable

## 1) N<sub>2</sub> + DO

$$\frac{dN_2}{dt} = -\frac{1}{h} k_{aN_2} (N_2 - N_{2s})$$

$k_{aN_2}$  = nitrogen gas reaeration coefficient, m s<sup>-1</sup>.

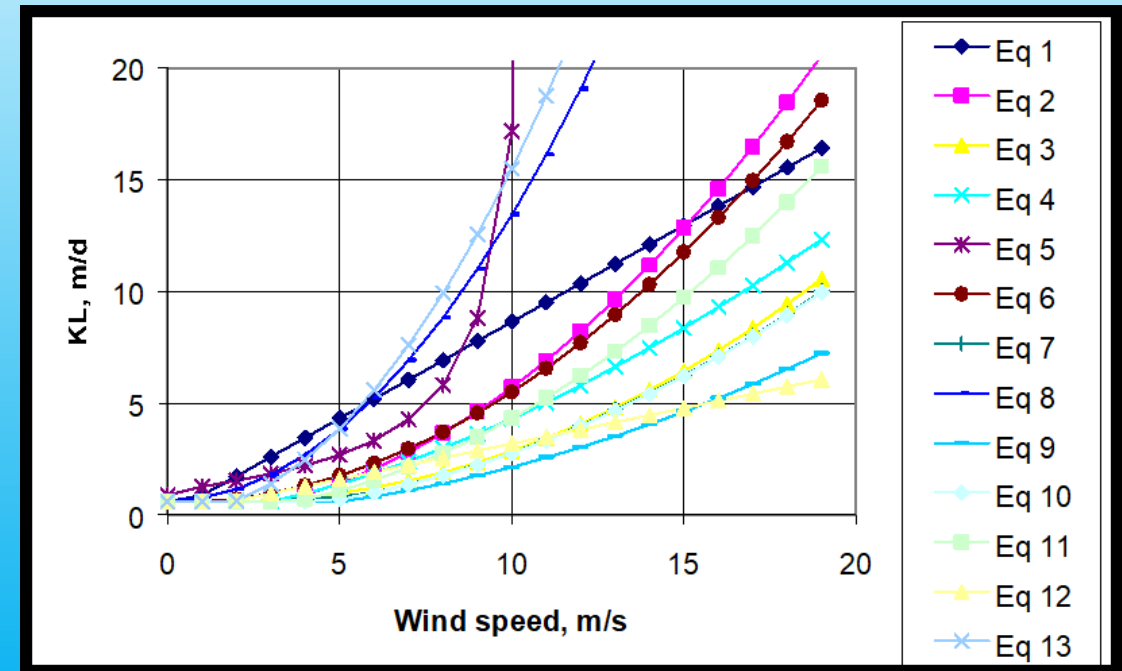
## 2) DGP (Dissolved Gas Pressure)

$$\frac{dDGP}{dt} = -k_{DGP} (DGP - PALT_{atm})$$

$$k_{DGP} = \max(k_{DGP}, MINKL)$$

$k_{DGP}$  = air/water gas exchange rate, d<sup>-1</sup>.

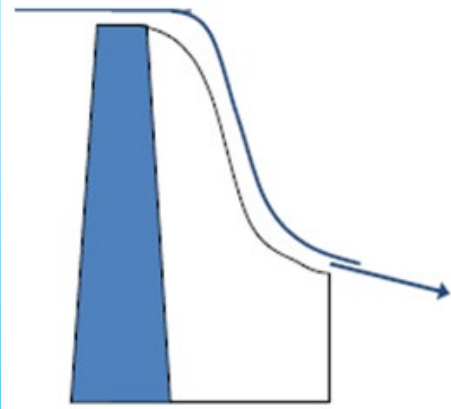
Lake/reservoir Reaeration equations



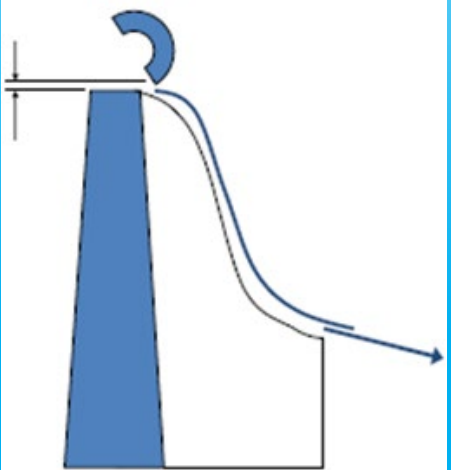
It is assumed that wind is the dominant forcing function for reaeration.

# Reaeration Effects of Spillways, Weirs, and Gates

Spillway/weir



gate



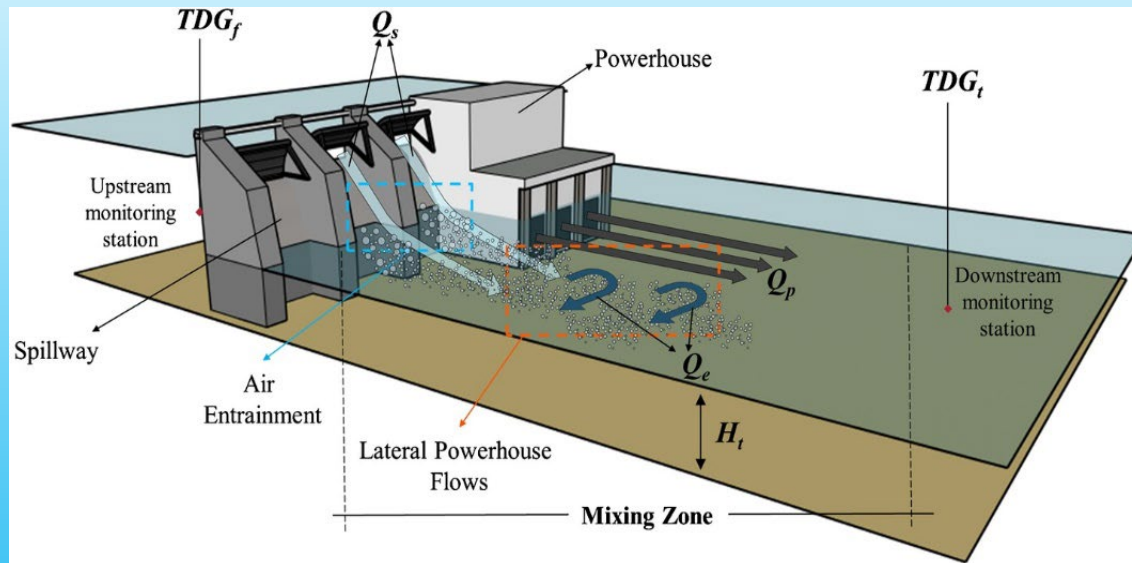
#, EQGT	Equation	Empirical Coefficient Description
1. Linear function of spill on a per spillway basis; 2 empirical coefficients: a and b	$\%TDG = aq_s + b$ $C_{O_2} = \%TDG * C_{sO_2}$	$\%TDG$ = total dissolved gas saturation, % $q_s$ = spill through an individual spillway, kcfs $C_{sO_2}$ = dissolved oxygen saturation, $g\ m^{-3}$
2. Bounded exponential of the spill on a per spillway basis; 3 empirical coefficients: a, b, c	$\%TDG = a + be^{cq_s}$ $C_{O_2} = \%TDG * C_{sO_2}$	$q_s$ = spill through an individual spillway, kcfs $C_{sO_2}$ = dissolved oxygen saturation $g\ m^{-3}$
3. Reaeration effect for a small height weir or dam (<10 m); 3 empirical coefficients: a, b, c (Butts and Evans, 1983)	$\frac{D_a}{D_b} = 1 + 0.38ab(1 - 0.11c)$ $(1 + 0.046T)c$ $C_{O_2} = C_{sO_2} - D_b$	$D_a$ = DO deficit above dam, $g\ m^{-3}$ $D_b$ = DO deficit below dam, $g\ m^{-3}$ $T$ = temperature, $^{\circ}C$ $C_{sO_2}$ = dissolved oxygen saturation, $g\ m^{-3}$

REAERATION	WB1
TYPE: LAKE, RIVER, or ESTUARY	LAKE
EQN#: Equation # (see User Manual)	14
COEF1 User defined parameter	0.3
COEF2 User defined parameter	0.2
COEF3 User defined parameter	0.5
COEF4 User defined parameter	0
DGPO2, fraction of dissolved gas to reaeration coefficient, typical value 1.027	1.027
MINKL (if LAKE, m/d) or MINKA (if RIVER/ESTUARY, day-1)	0.6

# Total Dissolved Gas (TDG)

SPILLWAYS	SP1	GATES	GATE1	GATE2	GTE3	GATE4
IUSP- Upstream segment number, spillway segment location		IUGT- Upstream segment number	76	76	76	76
IDSP- Downstream segment number, Downstream segment location		IDGT- Downstream segment number	0	0	0	0
ESP - spillway elevation (crest), m		EGT - Gate elevation m	11.7	7.3	7.3	7.3
A1SP- $\alpha_1$ , empirical coefficient for free-flowing conditions		A1GT $\alpha_1$ coefficient in gate equation for free flowing conditions	10	10	10	10
B1SP- $\beta_1$ , empirical coefficient for free-flowing conditions		B1GT $\beta_1$ coefficient in gate equation for free flowing conditions	1.5	1.5	1.5	1.5
A2SP- $\alpha_2$ , empirical coefficient for submerged conditions		G1GT gamma1 coeff for free flowing conditions	1	1	1	1
B2SP- $\beta_2$ , empirical coefficient for submerged conditions		A2GT $\alpha_2$ coefficient in gate equation for submerged conditions	10	10	10	10
LATSPC-Downstream or lateral withdrawal, DOWN or LAT		B2GT $\beta_2$ coefficient in gate equation for submerged conditions	1.5	1.5	1.5	1.5
PUSPC-How inflows enter into the upstream spillway segment		G2GT gamma2 coeff for submerged conditions	1	1	1	1
ETUSP-Top elevation spillway inflows enter using SPECIFY option		LATGTC downstream or lateral withdrawal LAT or DOWN	DOWN	DOWN	DOWN	DOWN
EBUSP-Bottom elevation spillway inflows enter using SPECIFY option		GTA1 $\alpha_1$ in gate equation for free flowing conditions as a spillway	10	10	10	10
KTUSP-Top layer above which selective withdrawal will not occur		GTB1 $\beta_1$ in gate equation for free flowing conditions as a spillway	1.5	1.5	1.5	1.5
KBUSP-Spillway Up Selective withdrawal bottom layer, Bottom layer below which selective withdrawal will not occur		GTA2 $\alpha_2$ in gate equation for submerged conditions as a spillway	10	10	10	10
PDSPC-How inflows enter into the downstream spillway segment		GTB2 $\beta_2$ in gate equation for submerged conditions as a spillway	1.5	1.5	1.5	1.5
ETUSP-Top elevation spillway inflows enter using SPECIFY option		DYNGTC Either 'B', 'ZGT', or 'FLOW'	FLOW	FLOW	FLOW	FLOW
EBUSP-Bottom elevation spillway inflows enter using SPECIFY option		GTIC EITHER ON or OFF interpolate gate file	ON	ON	ON	ON
KTUSP-Top layer above which selective withdrawal will not occur		PUGTC Specifies how inflows enter the upstream gate segment, DISTR, DENSITY, or SPECIFY	DISTR	DISTR	DISTR	DISTR
KBUSP-Spillway Up Selective withdrawal bottom layer, Bottom layer below which selective withdrawal will not occur		ETUGT Top elevation gate inflows enter using the SPECIFY option, m				
PDSPC-How inflows enter into the downstream spillway segment		EBUGT Bottom elevation gate inflows using the SPECIFY option, m				
ETUSP-Top elevation spillway inflows enter using SPECIFY option		KTUGT Top layer above which selective withdrawal will not occur	2	2	2	2
EBUSP-Bottom elevation spillway inflows enter using SPECIFY option		KBUGT-Selective withdrawal bottom layer, Bottom layer below which selective withdrawal will not occur	55	55	55	55
KTUSP-Top layer above which selective withdrawal will not occur		PDGTC Specifies how inflows enter the downstream gate segment, DISTR, DENSITY, or SPECIFY	DISTR	DISTR	DISTR	DISTR
KBUSP-Spillway Up Selective withdrawal bottom layer, Bottom layer below which selective withdrawal will not occur		ETDGT Top elevation gate inflows enter using the SPECIFY option, m				
PDSPC-How inflows enter into the downstream spillway segment		EBDGT Bottom elevation gate inflows using the SPECIFY option, m				
ETUSP-Top elevation spillway inflows enter using SPECIFY option		KTDGT Top layer above which selective withdrawal will not occur	2	2	2	2
EBUSP-Bottom elevation spillway inflows enter using SPECIFY option		KBDGT-Selective withdrawal bottom layer, Bottom layer below which selective withdrawal will not occur	55	55	55	55
KTUSP-Top layer above which selective withdrawal will not occur		GASGTC Dissolved gas computations ON or OFF	OFF	ON	ON	ON
KBUSP-Spillway Up Selective withdrawal bottom layer, Bottom layer below which selective withdrawal will not occur		EQGT Equation number for computing dissolved gas	2	2	2	2
GASSPC Dissolved gas computations ON or OFF		AGASGT a empirical coefficient	135	135	135	135
EQSP Equation number for computing dissolved gas		BGASGT b empirical coefficient	-35	-35	-35	-35
AGASSP a empirical coefficient		CGASGT c empirical coefficient	-0.1	-0.1	-0.1	-0.1
BGASSP b empirical coefficient						
CGASSP c empirical coefficient						

# Reaeration Effects of Gates - SYSTDG



$$TDG_{rel} = \frac{TDG_{sp}(Q_{sp} + Q_{ent}) + TDG_{ph}(Q_{ph} - Q_{ent})}{Q_{ph} + Q_{sp}}$$

- $Q_{tot}$ ,  $Q_{spill}$ ,  $Q_{ph}$ ,  $Q_{ent}$
- $TDG_{spill}$  is computed from spillway TDG production equation
- $TDG_{rel}$  is computed as the flow weighted average value

*Schneider, M., Hamilton, L., 2015. SYSTDG Developer's Manual. U.S. Army Corps of Engineers, Northwestern Division, Reservoir Control Center.*

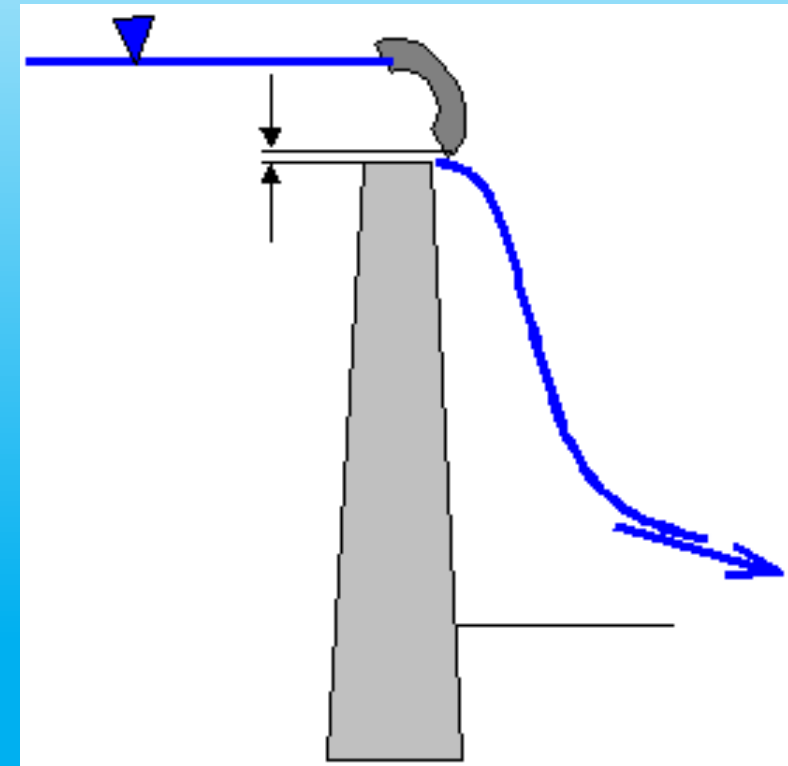


# SYSTDG Algorithms

No	TDG Production Equation
1	$TDG_{sp} = P1 * (1 - e^{P3 * Q_{sp}}) + bp$
2	$TDG_{sp} = P1 * (twe - twce)^{P2} * (1 - e^{P3 * q_s}) + P4 + bp$
3	$TDG_{sp} = P1 * (twe - twce)^{P2} * q_s^{P3} + P4 + bp$
4	$TDG_{sp} = P1 * (twe - twce) + P2 * q_s^{P3} + P4 + bp$
5	$TDG_{sp} = P1 * (1 - e^{P2 * q_s}) + P3 * (Temp_{tw} - P4) + bp$

No	Powerhouse Flow Entrainment Equation
1	$Q_{ent} = E1 * Q_{sp} + E2$
2	$Q_{ent} = \min[(Q_{tot} / 60), 1] * E1 * Q_{sp} + E2$
3	$Q_{ent} = \min[(Q_{sp} / 20), 1] * E1 * Q_{sp} + E2$

SYSTDG is an Excel-based spreadsheet model used to compute TDG saturation levels in reservoir and riverine systems.





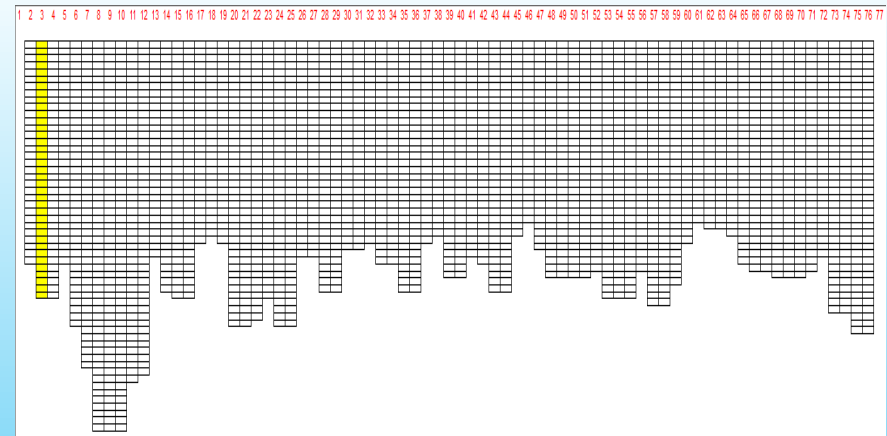
# System Total Dissolved Gas (SYSTDG) Control File

15	SYSTDGC	SYSTDG	N2BND	DOBND	DGPBN	TDGTA				
16		OFF	OFF	OFF	OFF	OFF				
17										
18	GATE GAS	GTTYPE	SPBC							
19	POWR1	POW	1							
20	SB1	SPB	2.03							
21	SB2	SPB	2.03							
22	SB3	SPB	2.03							
23	SB4	SPB	2.03							
24	SB5	SPB	2.03							
25	SB6	SPB	2.03							
26	SB7	SPB	2.03							
27	SB8	SPB	2.03							
28	SB9	SPB	2.03							
29	SB10	SPB	2.03							
30	SB11	SPB	2.03							
31	SB12	SPB	2.03							
32	SB13	SPB	2.03							
33	SB14	SPB	2.03							
34	SB15	SPB	2.03							
35	SB16	SPB	2.03							
36	SB17	SPB	2.03							
37	SB18	SPB	2.03							
38	OTHER	FLD	1							
39										
40	GATE	FBE	TWCE	TWEMO	TWE	TWETS	TDGLOC	QSPILL	TDGSPMN	
41	SPB1	-1	0	0	18.92	ON	SPB	0	110	
42										
43	GATE TDG	TDGEQ	P1	P2	P3	P4	P1	P2	P3	P4
44	SPB1	4	1.84	18.64	0.73	29.47				

# Bonneville Dam

- Bonneville Dam is located on Columbia River Mile (RM) 146.1 and is a run-of-river dam.
- The reservoir is 48 miles long, from Bonneville Dam to the foot of Dalles Dam upstream, with a surface area of 29.5 square miles, and a capacity of 537,000 acre-feet.
- The full forebay elevation is 77 feet, and the maximum forebay elevation is 82.5 feet.
- The Dam is 171 feet high and 2,477 feet long.
- The spillway is 1,070 feet long and contains 18 spill bays each with a 50 feet by 60 feet lift gate.
- Bonneville Dam is equipped with 2 powerhouse units, 18 spillbays, and 1 fish ladder.
- Columbia River System Operations Final Environmental Impact Statement:
  - <https://www.nwd.usace.army.mil/CRSO/Final-EIS/>

# Bonneville Dam W2 Model



File type		File name
Wind sheltering	WSC FILE WSCFN	BON_WSC.npt
Shading	SHDFN	BON_SHD_1.npt
Bathymetry	BTHFN	BON_NAVD88_BTH_2011.csv
Meteorological	METFN	BON_2011_2015_MET.csv
Branch inflow	QINFN branch inflow	DALLES_OUTFLOW.csv
	TINFN branch temp	two_41_TDA.opt
	CINFN branch conc	cwo_41_TDA.opt
	QDTFN Distributed flow	BON_DistributedTribInflow.npt
	TDTFN Distributed temp	two_41_TDA.opt
	CDTFN Distributed conc	cwo_41_TDA.opt
Spillway/Gate	QGTFN	QGT_BON_2011_2015.csv

# W2 Modeled TDG Results with N2+DO

## SYSTDG = ON

**Eq 4:**  $TDG_{sp} = P1 * (twe - twce) + P2 * q_s^{P3} + P4 + bp$

$P1 = 1.84, P2 = 18.64, P3 = 0.73, P4 = 29.47$

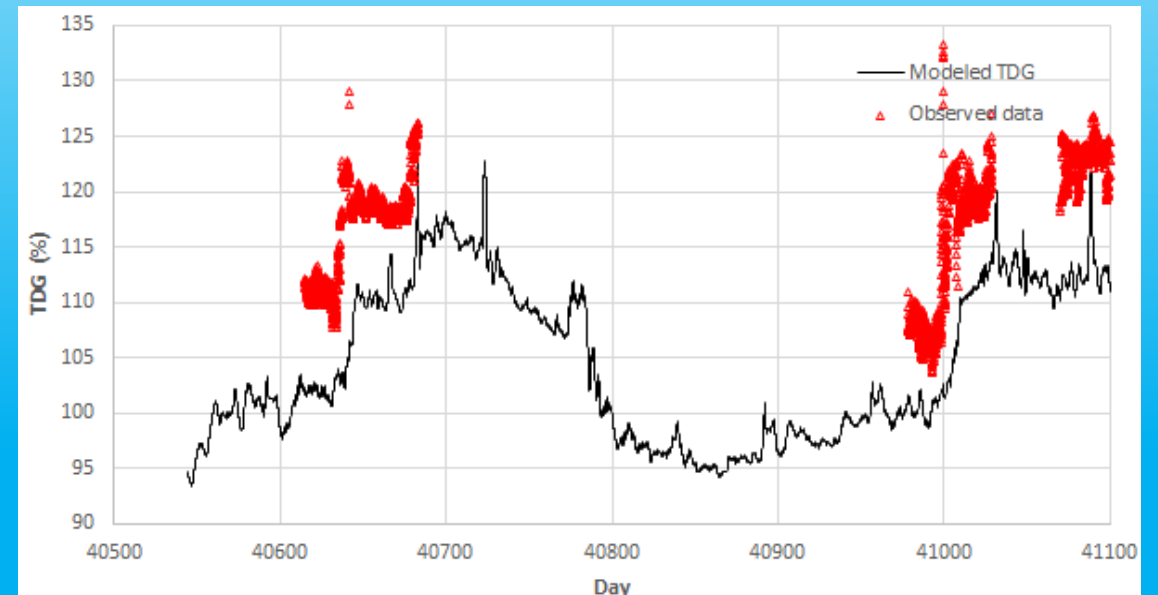
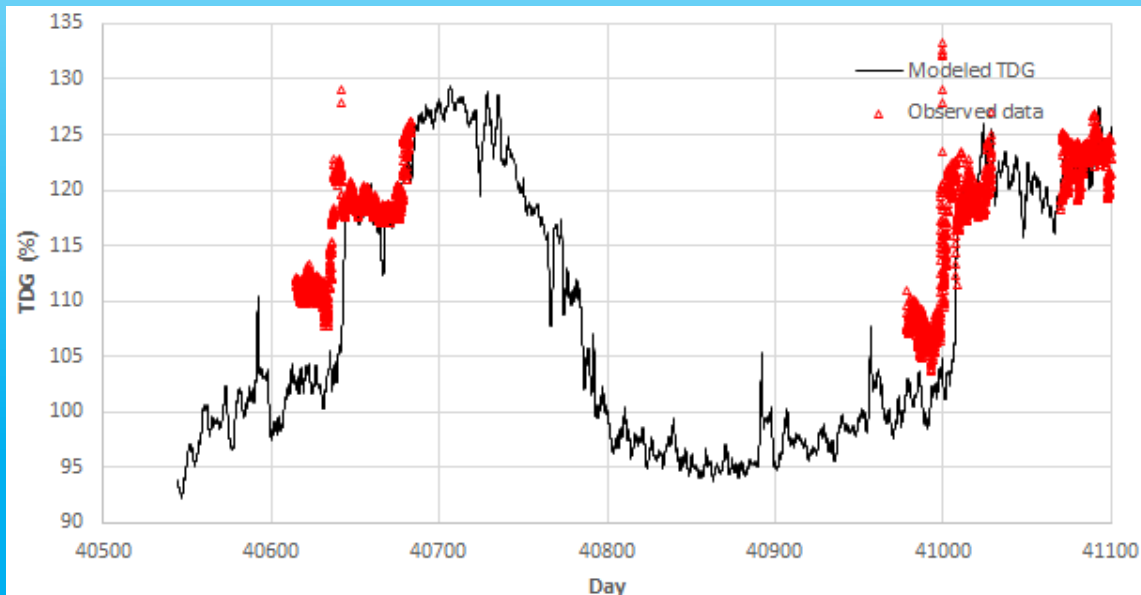
$Q_{ent} = E1 * Q_{sp} + E2$

$E1 = 0, E2 = 0$

## SYSTDG = OFF

**Eq 1:**  $TDG(\%) = a * Q_s + b$

$a = 0.12, b = 105.61$





# W2 Modeled TDG Results With DGP

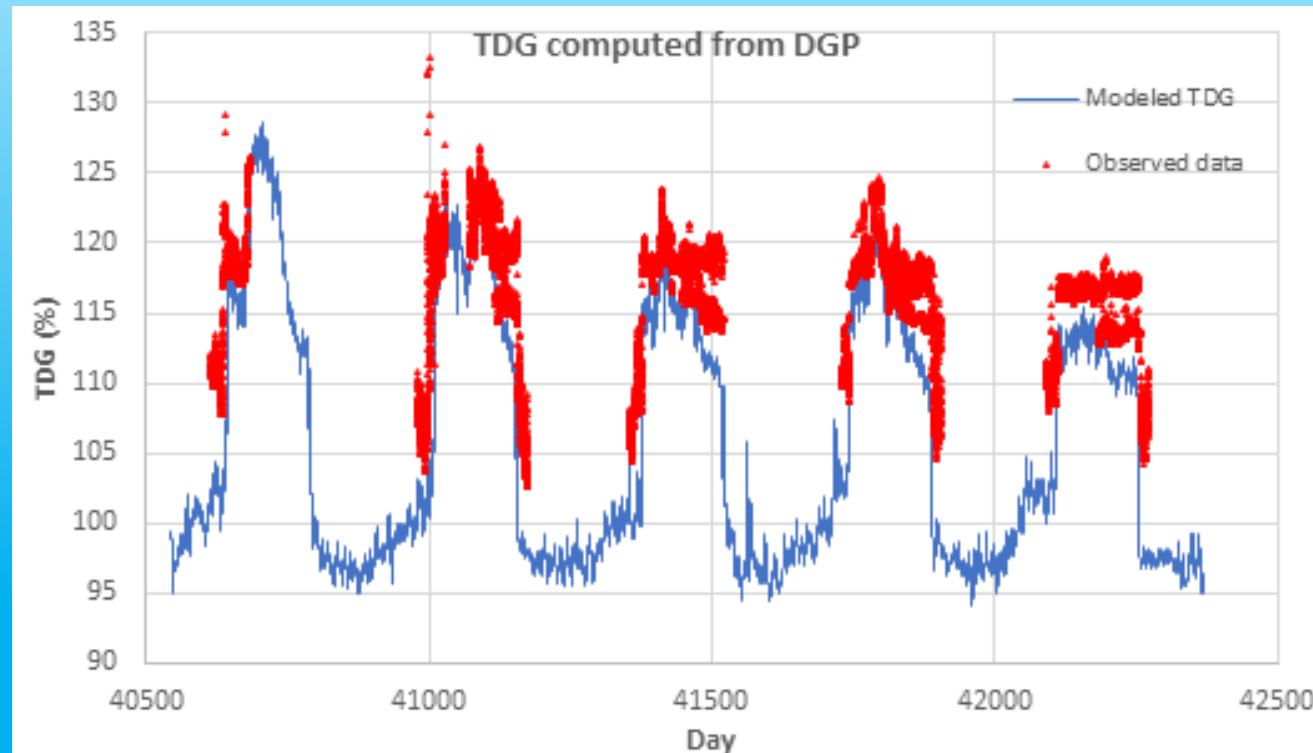
SYSTDG = ON

Eq 4:  $TDG_{sp} = P1 * (twe - twce) + P2 * q_s^{P3} + P4 + bp$

$$Q_{ent} = E1 * Q_{sp} + E2$$

$$P1 = 1.84, P2 = 18.64, P3 = 0.73, P4 = 29.47$$

$$E1 = 0, E2 = 0$$



# Hands-On Exercises

- Review model input files from “Bonneville W2 Project”
- Run the W2 model and review the model outputs of withdrawal TDG in [dwo\\_76.csv](#)
- Change SYSTDG parameters and rerun the model and see the difference of TDG in [dwo\\_76.csv](#)
  - P1, P2, P3, P4
  - E1, E2

# Questions?



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