

# Week 6 - Applications of Integration

∷ Tags

## Theorem 2.1 Finding the Area between 2 Curves

If  $f(x) \geq g(x)$  and both are continuous

The area between the 2 curves and x=a and x=b is

$$\int_a^b f(x) - g(x) dx$$

## Theorem 2.2 Finding the Area of a Region between Curves that cross

If f(x) and g(x) are continuous

The area between the curves and x=a and x=b

Is still 
$$\int_a^b |f(x)-g(x)| dx = \int_a^c f(x)-g(x) dx + \int_c^b f(x)-g(x) dx$$

## Theorem 2.3 Finding the Area Between 2 Curves, Integrating along the y-axis

If  $u(y) \geq v(y)$  are continuous functions

The area between the curves and y=c and y=d is

$$\int_{c}^{d}|u(y)-v(y)|dy$$

### **Disk Method**

If f(x) is continuous and non-negative

Volume of the solid of revolution formed by f(x) and lines x=a and x=b is  $V=\int_a^b\pi(f(x))^2dx$ 

## Disk Method for Solids of Revolution around y-axis

$$V=\int_{c}^{d}\pi(u(y))^{2}dy$$

### **Washer Method**

Volume of revolution when there are 2 functions and  $f(x) \geq g(x)$ 

$$V = \int_a^b \pi [(f(x))^2 - (g(x))^2] dx$$

**Proof:** 

## Washer Method for Solids of Revolution around y-axis

$$V = \int_{c}^{d} \pi [(u(y))^{2} - (v(y))^{2}] dy$$

## Volume of Revolution with a different axis of revolution

Instead of  $V=\int_a^b\pi(f(x))^2dx$ 

If the axis is x = e

$$V = \int_a^b \pi (f(x) - e)^2 - (-e)^2 dx$$

## **Theorem 2.4 Arc Length**

$$L = \int_a^b \sqrt{1 + (f'(x))^2} dx$$

We start by looking at the distance between 2 points. By Pythagoras' theorem, this is  $\sqrt{(\Delta x)^2 + (\Delta y)^2}$ 

If we make the  $\boldsymbol{x}$  distances constant, then this becomes:

$$egin{aligned} \sqrt{(\Delta x)^2 + (\Delta y_i)^2} \ &= \Delta x \sqrt{1 + (rac{\Delta y_i}{\Delta x})^2} \end{aligned}$$

According to the Mean Value Theorem, there is a point such that  $f'(x_i^*) = \dfrac{\Delta y_i}{\Delta x}$ , so

$$=\Delta x\sqrt{1+(f'(x))^2}$$

If we add up all the lengths of the line segments

$$Lpprox \Sigma_{i=1}^n \sqrt{1+(f'(x))^2}\Delta x$$

This is a Riemann sum

Taking the limit as  $n o \infty$ 

$$L = \lim_{n o \infty} \Sigma_{i=1}^n \sqrt{1 + (f'(x))^2} \Delta x$$

$$L = \int_a^b \sqrt{1 + (f'(x))^2} dx$$

## Theorem 2.5 Arc Length for a y-function

$$L=\int_c^d \sqrt{1+(g'(y))^2}dy$$

#### **Proof:**

Same proof as Theorem 2.4

### **Theorem 2.6 Surface Area of Revolution**

### **Around x-axis**

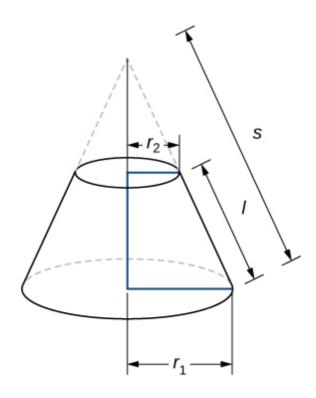
$$A=\int_a^b 2\pi f(x)\sqrt{1+(f'(x))^2}dx$$

### **Around y-axis**

$$A=\int_c^d 2\pi g(y)\sqrt{1+(g'(y))^2}dy$$

### Lateral surface area of a cone (excludes base)

 $=\pi rs$  where r is radius and s is slant height



The small cone and large cone are similar triangles so

$$rac{r_2}{r_1} = rac{s-l}{s}$$

Which leads to

$$s=\frac{r_1l}{r_1-r_2}$$

The lateral surface area of frustum

= Lateral surface area of large cone - Lateral surface area of small cone

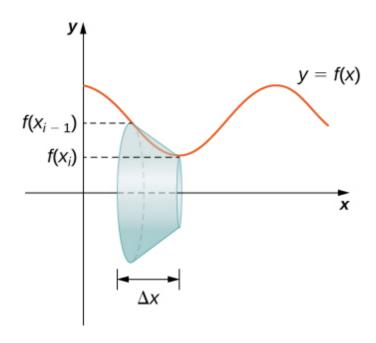
$$=\pi r_1 s - \pi r_2 (s-l)$$

$$=\pi[r_1(rac{r_1l}{r_1-r_2})-r_2(rac{r_1l}{r_1-r_2}-l)]$$

$$=\pi[rac{r_1^2l}{r_1-r_2}-rac{r_1r_2l}{r_1-r_2}+r_2l]$$

$$=\pi [rac{r_1^2 l}{r_1-r_2}-rac{r_1 r_2 l}{r_1-r_2}+rac{r_2 l (r_1-r_2)}{r_1-r_2}]$$

$$egin{align} &=\pi[rac{r_1^2l}{r_1-r_2}-rac{r_1r_2l}{r_1-r_2}+rac{r_1r_2l}{r_1-r_2}-rac{r_2^2l}{r_1-r_2}]\ &=\pi[rac{(r_1^2-r_2^2)l}{r_1-r_2}]\ &=\pi[rac{(r_1-r_2)(r_1+r_2)l}{r_1-r_2}]\ &=\pi(r_1+r_2)l \ \end{pmatrix}$$



Both radii are actually just the y values  $f(x_i)$  and  $f(x_{i-1})$ 

Therefore

$$egin{aligned} s &= \pi(r_1 + r_2) l \ &= \pi(f(x_i) + f(x_i) \sqrt{\Delta x^2 + (\Delta y_i)^2}) \ &= \pi(f(x_i) + f(x_i) \Delta x \sqrt{1 + rac{\Delta y i}{\Delta x}}) \end{aligned}$$

Again, using the Mean Value Theorem

$$=\pi(f(x_{i-1})+f(x_i))\Delta x\sqrt{1+f'(x_i^*)^2}$$

By the Intermediate Value Theorem, there is a point  $x^{**}$  such that  $f(x^{**})=rac{1}{2}[f(x_{i-1})+f(x_i)] = 2\pi f(x^{**})\Delta x\sqrt{1+f'(x_i^*)^2}$ 

Then the area over the whole revolution will be

$$Approx \Sigma_{i=1}^n 2\pi f(x^{**})\Delta x\sqrt{1+f'(x_i^*)^2}$$

We can do a Riemann Sum because as  $n\to\infty$ , both  $x^*$  and  $x^{**}$  will approach x, since they are both in the range  $[x_{i-1},x_i]$ 

Therefore

$$A=\lim_{n}n
ightarrow \Sigma_{i=1}^{n}2\pi f(x^{stst})\Delta x\sqrt{1+f'(x_{i}^{st})^{2}}$$

$$A=\int_a^b (2\pi f(x)\Delta x\sqrt{1+f'(x_i)^2})dx$$

## Theorem 2.7 Mass-Density Formula of a One-Dimensional Object

Let  $\rho(x)$  denote a linear density function, giving the density of the object at point x along the x axis

Mass 
$$m=\int_a^b 
ho(x)dx$$

#### **Proof:**

We treat a rod as if it had no thickness

$$m_ipprox
ho(x_i^*)(x_i-x_{i-1})$$

$$m_ipprox
ho(x_i^*)\Delta x$$

$$m = \Sigma_{i=1}^n m_i pprox 
ho(x_i^*) \Delta x$$

This is a Riemann sum, taking the limit as  $n o \infty$ 

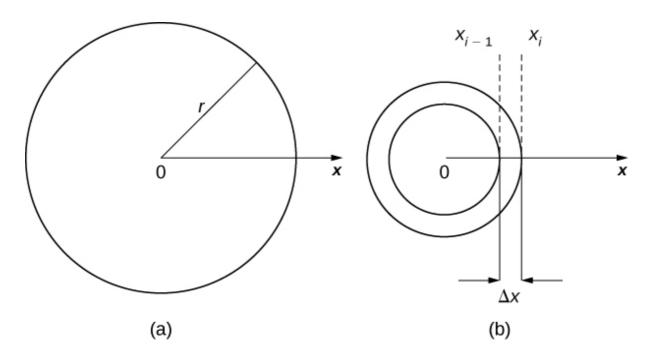
$$m = \lim_{n o \infty} \Sigma_{i=1}^n 
ho(x_i^*) \Delta x$$

$$m = \int_a^b 
ho(x) dx$$

## Theorem 2.8 Mass–Density Formula of a Circular Object

Let ho(x) be an integrable function representing radial density of a disk r

Mass 
$$m=\int_0^r 2\pi x 
ho(x) dx$$



Area 
$$A=\pi(x_i^2)-\pi(x_{i-1})^2$$
  $=\pi[x_i^2-x_{i-1}^2]$   $=\pi(x_i+x_{i-1})(x_i-x_{i-1})$   $=\pi(x_i+x_{i+1})\Delta x$   $x_i^*pprox rac{(x_i+x_{i-1})}{2}$ , so  $pprox 2\pi x_i^*\Delta x$ 

Using  $ho(x^*)$  to approximate the density of the washer

$$mpprox \Sigma_{i=1}^n m_ipprox 2\pi x_i^*
ho(x_i^*)\Delta x$$

This is a Riemann sum, hence as  $n o \infty$ 

$$m = \lim_{n o \infty} \Sigma_{i=1}^n 2\pi x_i^* 
ho(x_i^*) \Delta x$$

$$m=\int_0^r 2\pi x 
ho(x) dx$$

## Work

Work done by a force F(x) from point a to b is

$$\int_a^b F(x)dx$$

$$W_ipprox F(x_i^*)(x_i{-}x_{i-1})$$

$$W_i pprox F(x*i)\Delta x$$

$$W = \Sigma_{i=1}^n W_i pprox \Sigma_{i=1}^n F(x_i^*) \Delta x$$

Which is a Riemann sum, hence as  $n o \infty$ 

$$W = \lim_{n o \infty} \Sigma_{i=1}^n F(x_i^*) \Delta x$$

$$W = \int_a^b F(x) dx$$

## **Pumping Problems**

Work for pumping water from the initial distance of  $h_0$  to the bottom h is:

$$W=\int_{h_0}^h \pi 
ho r^2 x dx$$

#### **Proof:**

**Density equation** 

$$ho = rac{m}{V} \! 
ightarrow m = 
ho V$$
 1.

Force equation

$$F = mq$$

Plugging in 1.:

$$F=
ho Vg$$
 2.

Work equation

$$W = Fd$$

Plugging in 2.:

$$W = 
ho V g d$$

$$W_i = 
ho \pi r^2 x_i^* \Delta x$$

$$\Sigma_{i=1}^n W_i = \Sigma_{i=1}^n 
ho \pi r^2 x_i^* \Delta x$$

This is a Riemann sum, hence as  $n o \infty$ 

$$W = \lim_{n o \infty} \Sigma_{i=1}^n 
ho \pi r^2 x_i^* \Delta x$$

$$W=\int_{h_0}^h \pi 
ho r^2 x dx$$

## **Hydrostatic Force**

Force = Pressure\*Area\*Distance below water

$$F_i = \rho As$$

Assuming the thickness is thin enough, we can assume a constant force on the slice:

$$=
ho[w(x_i^*)\Delta x]s(x_i^*)$$

$$Fpprox \Sigma_{i=1}^n F_i = \Sigma_{i=1}^n 
ho[w(x_i^*)\Delta x] s(x_i^*)$$

This is a Riemann sum, so as  $n o \infty$ 

$$\lim_{n o\infty} \Sigma_{i=1}^n 
ho[w(x_i^*)\Delta x] s(x_i^*) = \int_a^b 
ho w(x) s(x) dx$$

## Theorem 2.9 Centre of Mass of Objects on a Line

Moment  $M=\Sigma_{i=1}^n m_i x_i$ 

Centre of mass  $ar{x} = rac{M}{m}$ 

## Theorem 2.10 Centre of Mass of Objects in a Plane

#### **Moments**

$$M_x = \Sigma_{i=1}^n m_i x_i$$

$$M_y = \Sigma_{i=1}^n m_i y_i$$

### **Coordinates of Centre of Mass**

$$ar{x} = rac{M_x}{m}$$

$$ar{y} = rac{M_y}{m}$$

## **Theorem 2.11 Symmetry Principle**

If a region R is symmetric about a line l, then the centroid of R lies on l

## Theorem 2.12 Centre of Mass of a Thin Plate in the xy Plane

ho is the density of the lamina

#### **Mass of the Lamina**

$$m = 
ho \int_a^b f(x) dx$$

#### **Moments of the Lamina**

$$M_x = 
ho \int_a^b rac{f(x)^2}{2} dx$$

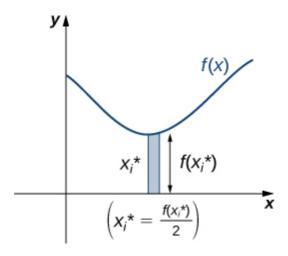
$$M_y = 
ho \int_a^b f(x) x dx$$

### **Centres of Mass of the Lamina**

$$ar{x} = rac{M_x}{m}$$

$$ar{y} = rac{M_y}{m}$$

### **Proof:**



Partition the lamina and let  $x_i^* = \dfrac{x_{i+1} + x_i}{2}$  which is the midpoint

Construct a rectangle and let  $f(x_i^st)$  be the height of the rectangle

Therefore, the centre of mass will be  $(x_i^*, \frac{f(x_i^*)}{2})$ 

Mass of the rectangle will be  $ho f(x_i^*) \Delta x$  where ho is the density

Mass  $m pprox \Sigma_{i=1}^n 
ho f(x_i^*) \Delta x$ 

This is a Riemann sum, hence as  $n \to \infty$ 

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$$m = \lim_{n o \infty} \Sigma_{i=1}^n 
ho f(x_i^*) \Delta x = 
ho \int_a^b f(x) dx$$

### **Finding Moment**

Moment = Mass\*Distance to centre of mass

$$M = 
ho f(x_i^*) \Delta x rac{f(x_i^*)}{2}$$

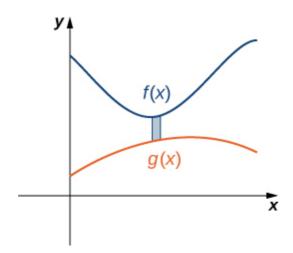
Taking a Riemann sum:

$$M_y = \lim_{n o\infty} \Sigma_{i=1}^n 
ho f(x_i^*) \Delta x rac{f(x_i^*)^2}{2} = 
ho \int_a^b f(x) rac{f(x)^2}{2} dx$$

Similarly

$$M_x = 
ho \int_a^b x f(x) dx$$

## Theorem 2.13: Centre of Mass of a Lamina Bounded by Two Functions



### Mass

Mass 
$$m=
ho\int_a^b f(x)-g(x)dx$$

#### **Proof**

The height of the of the rectangle is  $f(x_i^*) - g(x_i^*)$ 

Therefore the area is  $[f(x_i^*) - g(x_i^*)] \Delta x$ 

Hence the mass is  $m=
ho\int_a^bf(x)-g(x)dx$ 

### **Moment**

$$egin{aligned} M_x &= 
ho \int_a^b x (f(x) - g(x)) dx \ M_y &= 
ho \int_a^b rac{1}{2} [f(x)^2 - g(x)^2] dx \end{aligned}$$

#### **Proof**

The moment is found by multiplying the area  $[f(x_i^*)-g(x_i^*)]\Delta x$  by the distance  $\frac{f(x_i^*)+g(x_i^*)}{2}$ 

Which gives  $rac{1}{2}[f(x)^2-g(x)^2]\Delta x$  for  $M_y$  and  $x[f(x)^2-g(x)^2]\Delta x$  for  $M_x$ 

## **Theorem 2.14 Theorem of Pappus for Volume**

Let R be a region in the plane and let l be a line in the plane that does not intersect R. Then the volume of the solid of revolution formed by revolving R around l is equal to the area of R multiplied by the distance d travelled by the centroid of R.

#### **Proof:**

The area of the region between f(x) and g(x) is  $\int_a^b f(x) - g(x) dx$ 

If the axis of rotation is the y axis, the distance travelled by the centroid of the region depends only on  $\bar{x}$ , which is

$$\bar{x} = \frac{M_y}{m}$$

where

$$egin{aligned} m &= 
ho \int_a^b f(x) - g(x) dx \ M_y &= 
ho \int_a^b x [f(x) - g(x)] dx \end{aligned}$$

Then

$$d=2\pirac{
ho\int_a^bx[f(x)-g(x)]}{
ho\int_a^bf(x)-g(x)dx}$$

Since

 $d=2\pi ar{x}$ , because the distance travelled is a circumference of a circle around the y-axis

Thus

$$dA = 
ho \int_a^b x [f(x) - g(x)] dx$$

Using the method of cylindrical shells, we get

$$V = 
ho \int_a^b x [f(x) - g(x)] dx$$

$$V = d \cdot a$$

## **Exponential Growth Model**

Systems that exhibit exponential growth:

$$y = y_0 e^{kt}$$

## **Exponential Decay Model**

Systems that exhibit exponential decay:

$$y = y_0 e^{-kt}$$

## Half-Life

• Time taken for the quantity to halve

$$\lambda = \frac{\ln 2}{k}$$