

This document defines the formulas required for a Kalman filter that is used to localize the EduArt robots globally.

# 1 Prediction Model for Eduard with Mecanum

## 1.1 Acceleration

$$\mathbf{a}_{t-1} = \begin{pmatrix} a_{x_{t-1}} \\ a_{y_{t-1}} \end{pmatrix} \quad (1)$$

$$\mathbf{a}_t = \begin{pmatrix} a_{x_{t-1}} \\ a_{y_{t-1}} \end{pmatrix} \quad (2)$$

## 1.2 Velocity

$$\mathbf{v}_{t-1} = \begin{pmatrix} v_{x_{t-1}} \\ v_{y_{t-1}} \end{pmatrix} \quad (3)$$

$$\mathbf{v}_t = \begin{pmatrix} a_{x_{t-1}} dt + v_{x_{t-1}} \\ a_{y_{t-1}} dt + v_{y_{t-1}} \end{pmatrix} \quad (4)$$

## 1.3 Yaw

$$\phi_{z_t} = \phi_{z_{t-1}} + \frac{d}{dt} \phi_{z_{t-1}} dt \quad (5)$$

$$\frac{d}{dt} \phi_{z_t} = \frac{d}{dt} \phi_{z_{t-1}} \quad (6)$$

## 1.4 Position

$$\mathbf{R}_{t-1} = \begin{pmatrix} \cos(\phi_{z_{t-1}}) & -\sin(\phi_{z_{t-1}}) \\ \sin(\phi_{z_{t-1}}) & \cos(\phi_{z_{t-1}}) \end{pmatrix} \quad (7)$$

$$\mathbf{p}_{t-1} = \begin{pmatrix} p_{x(t-1)} \\ p_{y(t-1)} \end{pmatrix} \quad (8)$$

$$\mathbf{p}_t = \mathbf{p}_{t-1} + \mathbf{R}_{t-1} \mathbf{v}_{t-1} dt + \frac{1}{2} \mathbf{R}_{t-1} \mathbf{a}_{t-1} dt^2 \quad (9)$$

$$= \begin{pmatrix} dt^2 (0.5a_{x_{t-1}} \cos(\phi_{z_{t-1}}) - 0.5a_{y_{t-1}} \sin(\phi_{z_{t-1}})) + dt (v_{x_{t-1}} \cos(\phi_{z_{t-1}}) - v_{y_{t-1}} \sin(\phi_{z_{t-1}})) + p_{x(t-1)} \\ dt^2 (0.5a_{x_{t-1}} \sin(\phi_{z_{t-1}}) + 0.5a_{y_{t-1}} \cos(\phi_{z_{t-1}})) + dt (v_{x_{t-1}} \sin(\phi_{z_{t-1}}) + v_{y_{t-1}} \cos(\phi_{z_{t-1}})) + p_{y(t-1)} \end{pmatrix} \quad (10)$$

## 1.5 Model

$$\mathbf{F}_t = \begin{pmatrix} px_t \\ py_t \\ vx_t \\ vy_t \\ ax_t \\ ay_t \\ \phi_t \\ \frac{d}{dt}\phi \end{pmatrix} = \begin{pmatrix} dt^2 \left( 0.5ax_{t-1} \cos(\phi_{z_{t-1}}) - 0.5ay_{t-1} \sin(\phi_{z_{t-1}}) \right) + dt \left( vx_{t-1} \cos(\phi_{z_{t-1}}) - vy_{t-1} \sin(\phi_{z_{t-1}}) \right) + px(t-1) \\ dt^2 \left( 0.5ax_{t-1} \sin(\phi_{z_{t-1}}) + 0.5ay_{t-1} \cos(\phi_{z_{t-1}}) \right) + dt \left( vx_{t-1} \sin(\phi_{z_{t-1}}) + vy_{t-1} \cos(\phi_{z_{t-1}}) \right) + py(t-1) \\ ax_{t-1} dt + vx_{t-1} \\ ay_{t-1} dt + vy_{t-1} \\ ax_{t-1} \\ ay_{t-1} \\ \phi_{z_{t-1}} + \frac{d}{dt}\phi_{z_{t-1}} dt \\ \frac{d}{dt}\phi_{z_{t-1}} \end{pmatrix} \quad (11)$$

$$\mathbf{J}_t = \mathbf{F} \begin{pmatrix} \frac{\partial}{\partial px} & \frac{\partial}{\partial py} & \frac{\partial}{\partial vx} & \frac{\partial}{\partial vy} & \frac{\partial}{\partial ax} & \frac{\partial}{\partial ay} & \frac{\partial}{\partial \phi} & \frac{\partial^2}{\partial^2 \phi} \end{pmatrix} \quad (12)$$

$$= \begin{pmatrix} 1 & 0 & dt \cos(\phi_{z_{t-1}}) & -dt \sin(\phi_{z_{t-1}}) & 0.5dt^2 \cos(\phi_{z_{t-1}}) & -0.5dt^2 \sin(\phi_{z_{t-1}}) & dt^2 \left( -0.5ax_{t-1} \sin(\phi_{z_{t-1}}) - 0.5ay_{t-1} \cos(\phi_{z_{t-1}}) \right) + dt \left( -vx_{t-1} \sin(\phi_{z_{t-1}}) - vy_{t-1} \cos(\phi_{z_{t-1}}) \right) & 0 \\ 0 & 1 & dt \sin(\phi_{z_{t-1}}) & dt \cos(\phi_{z_{t-1}}) & 0.5dt^2 \sin(\phi_{z_{t-1}}) & 0.5dt^2 \cos(\phi_{z_{t-1}}) & dt^2 \left( 0.5ax_{t-1} \cos(\phi_{z_{t-1}}) - 0.5ay_{t-1} \sin(\phi_{z_{t-1}}) \right) + dt \left( vx_{t-1} \cos(\phi_{z_{t-1}}) - vy_{t-1} \sin(\phi_{z_{t-1}}) \right) & 0 \\ 0 & 0 & 1 & 0 & dt & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & dt & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & dt \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix} \quad (13)$$

## 2 System Noise Model

### 2.1 Via Acceleration

The system noise is partly determined by the acceleration that the robot can experience.

$$a = a_x = a_y \quad (14)$$

$$\mathbf{a} = \begin{pmatrix} a \\ a \end{pmatrix} \quad (15)$$

$$\mathbf{v} = \begin{pmatrix} a \cdot dt \\ a \cdot dt \end{pmatrix} \quad (16)$$

$$\mathbf{p} = \frac{1}{2} \mathbf{R}_{t-1} \mathbf{a} \cdot dt^2 \quad (17)$$

$$= \begin{pmatrix} dt^2 (-0.5a \sin(\phi_{z_{t-1}}) + 0.5a \cos(\phi_{z_{t-1}})) \\ dt^2 (0.5a \sin(\phi_{z_{t-1}}) + 0.5a \cos(\phi_{z_{t-1}})) \end{pmatrix} \quad (18)$$

$$\mathbf{a}_{\text{noise}} = \begin{pmatrix} \mathbf{p} \\ \mathbf{v} \\ \mathbf{a} \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} 0.5\sqrt{2}dt^2 \cos(\phi_{z_{t-1}} + \frac{\pi}{4}) \\ 0.5\sqrt{2}dt^2 \sin(\phi_{z_{t-1}} + \frac{\pi}{4}) \\ dt \\ dt \\ 1 \\ 1 \\ 0 \\ 0 \\ 0 \end{pmatrix} a \quad (19)$$

$$\mathbf{Q}_{\mathbf{a}} = \sigma_{\mathbf{a}}^2 \cdot \mathbf{a}_{\text{noise}} \cdot \mathbf{a}_{\text{noise}}^T = \sigma_{\mathbf{a}}^2 \begin{pmatrix} \frac{p_x^2}{a^2} & \frac{p_x p_y}{a^2} & \frac{dt p_x}{a} & \frac{dt p_x}{a} & \frac{p_x}{a} & \frac{p_x}{a} & 0 & 0 \\ \frac{p_x p_y}{a^2} & \frac{p_y^2}{a^2} & \frac{dt p_y}{a} & \frac{dt p_y}{a} & \frac{p_y}{a} & \frac{p_y}{a} & 0 & 0 \\ \frac{dt p_x}{a} & \frac{dt p_y}{a} & dt^2 & dt^2 & dt & dt & 0 & 0 \\ \frac{dt p_x}{a} & \frac{dt p_y}{a} & dt^2 & dt^2 & dt & dt & 0 & 0 \\ \frac{p_x}{a} & \frac{p_y}{a} & dt & dt & 1 & 1 & 0 & 0 \\ \frac{p_x}{a} & \frac{p_y}{a} & dt & dt & 1 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix} \quad (20)$$

### 2.2 Via Yaw Rate

The system noise is partly determined by the yaw rate that the robot can experience.

$$\phi_z = \dot{\phi}_z dt \quad (21)$$

$$\dot{\phi}_{z_{\text{noise}}} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ \dot{\phi}_z \\ \dot{\phi}_z \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ dt \\ 1 \end{pmatrix} \dot{\phi}_z \quad (22)$$

$$\mathbf{Q}_{\text{yaw}} = \sigma_{\text{yaw}}^2 \cdot \dot{\phi}_{z_{\text{noise}}} \cdot \dot{\phi}_{z_{\text{noise}}}^T = \sigma_{\text{yaw}}^2 \begin{pmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & dt^2 & dt \\ 0 & 0 & 0 & 0 & 0 & 0 & dt & 1 \end{pmatrix} \quad (23)$$

### 2.3 Final System Noise Matrix

$$\mathbf{Q} = \mathbf{Q}_j + \mathbf{Q}_{\text{yaw}} = \begin{pmatrix} \frac{\sigma_a^2 p_x^2}{a^2} & \frac{\sigma_a^2 p_x p_y}{a^2} & \frac{\sigma_a^2 dt p_x}{a} & \frac{\sigma_a^2 dt p_x}{a} & \frac{\sigma_a^2 p_x}{a} & \frac{\sigma_a^2 p_x}{a} & 0 & 0 \\ \frac{\sigma_a^2 p_x p_y}{a^2} & \frac{\sigma_a^2 p_y^2}{a^2} & \frac{\sigma_a^2 dt p_y}{a} & \frac{\sigma_a^2 dt p_y}{a} & \frac{\sigma_a^2 p_y}{a} & \frac{\sigma_a^2 p_y}{a} & 0 & 0 \\ \frac{\sigma_a^2 dt p_x}{a} & \frac{\sigma_a^2 dt p_y}{a} & \sigma_a^2 dt^2 & \sigma_a^2 dt^2 & \sigma_a^2 dt & \sigma_a^2 dt & 0 & 0 \\ \frac{\sigma_a^2 dt p_x}{a} & \frac{\sigma_a^2 dt p_y}{a} & \sigma_a^2 dt^2 & \sigma_a^2 dt^2 & \sigma_a^2 dt & \sigma_a^2 dt & 0 & 0 \\ \frac{\sigma_a^2 p_x}{a} & \frac{\sigma_a^2 p_y}{a} & \sigma_a^2 dt & \sigma_a^2 dt & \sigma_a^2 & \sigma_a^2 & 0 & 0 \\ \frac{\sigma_a^2 p_x}{a} & \frac{\sigma_a^2 p_y}{a} & \sigma_a^2 dt & \sigma_a^2 dt & \sigma_a^2 & \sigma_a^2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \sigma_{\phi_z}^2 dt^2 & \sigma_{\phi_z}^2 dt \\ 0 & 0 & 0 & 0 & 0 & 0 & \sigma_{\phi_z}^2 dt & \sigma_{\phi_z}^2 \end{pmatrix} \quad (24)$$