

# Space feedback control

## Pole placement

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June 2020



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# Pole placement

So far we have learnt how a state feedback looks like and when it is possible to design a state feedback controller to stabilize a system:

$$\dot{x} = Ax + Bu$$

$$u = -Kx + k_r r$$

$$\dot{x} = (A - BK)x + Bk_r r$$

$K$  ubica los polos de LC y  $k_r$  se encarga de eliminar el error de estado estacionario

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The questions that remain are: *How do we design a state feedback controller and Where do we place the closed loop system's poles?*

# Pole placement

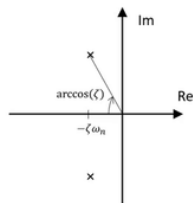
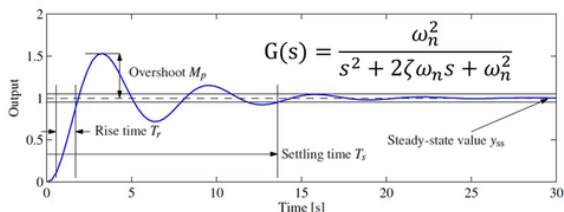
## Pole placement for time domain analysis

rise time: 10 a 90% rta

settling time: +-1%

## Specifications and pole placement

Property	Value	$\zeta = 0.5$	$\zeta = 1/\sqrt{2}$	$\zeta = 1$
Rise time (inverse slope)	$T_r = e^{\varphi/\tan\varphi} / \omega_0$	$1.8/\omega_0$	$2.2/\omega_0$	$2.7/\omega_0$
Overshoot	$M_p = e^{-\pi\zeta/\sqrt{1-\zeta^2}}$	16%	4%	0%
Settling time (2%)	$T_s \approx 4/\zeta\omega_0$	$8.0/\omega_0$	$5.6/\omega_0$	$4.0/\omega_0$



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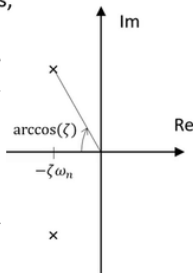
Where do we place the closed loop system's poles?

Nos enfocamos en los polos dominantes que dominan la rta en el transitorio

**Idea:**

- Use time domain specifications to place the dominant poles, as a second order system,  $s^2 + 2\zeta\omega_n s + \omega_n^2$ .

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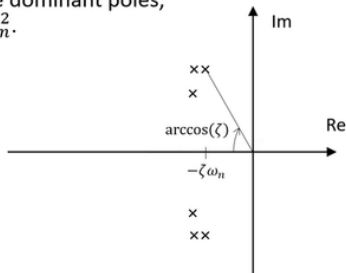


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**Idea:**

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- Place the rest of the poles so they become faster than the dominant poles.



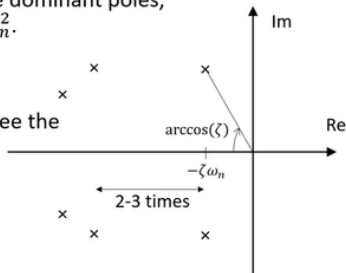
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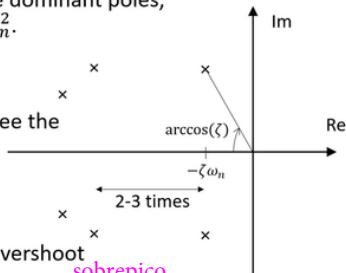
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Usually you end up with some zeros as well:

- Zeros in the left half plane give additional overshoot
- Zeros in the right half plane give a negative undershoot



## Pole placement (Ackermann's formula)

Pole placement is performed by matching the desired characteristic polynomial with the closed loop system's characteristic polynomial.

From earlier example (vehicle steering) we have seen:

$$\lambda^2 + 2\zeta\omega_n\lambda + \omega_n^2 \equiv \lambda^2 + \frac{v_0}{b}(ak_1 + k_2)\lambda + \frac{k_1v_0^2}{b}$$
$$k_1 = \frac{b\omega_n^2}{v_0^2} \quad k_2 = \frac{2\zeta\omega_nb}{v_0} - \frac{ab\omega_n^2}{v_0^2}$$

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For low order systems it is ok, but for larger systems this is boring work.

*Ackermann's formula offers us a method to do this in one computational step.*

## Pole placement (Ackermann's formula)

Consider a system  $\dot{x} = Ax + Bu$  with the characteristic polynomial

$$a(s) = s^n + a_1s^{n-1} + \cdots a_{n-1}s + a_n.$$

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If the system is reachable, then there exist a control law,  $u = -Kx$ , that gives a closed loop system with the characteristic polynomial

$$p(s) = s^n + p_1s^{n-1} + \cdots p_{n-1}s + p_n.$$

acá p no son los polos. Ojo

## Pole placement (Ackermann's formula)

The feedback gain is given by **p no son polos**

$$K = [p_1 - a_1 \quad p_2 - a_2 \quad \dots \quad p_n - a_n] \tilde{W}_r W_r^{-1}$$

where  $W_r$  is the reachability matrix

$$W_r = [B \quad AB \quad \dots \quad A^{n-1}B] \quad \begin{array}{l} \text{Alcanzable cuando} \\ W_r \text{ tiene inversa} \end{array}$$

and

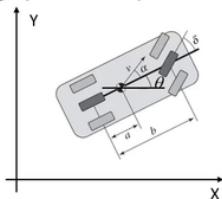
$$\tilde{W}_r = \begin{bmatrix} 1 & a_1 & a_2 & \dots & a_{n-1} \\ 0 & 1 & a_1 & \dots & a_{n-2} \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ 0 & 0 & \dots & 1 & a_1 \\ 0 & 0 & 0 & \dots & 1 \end{bmatrix}^{-1}$$

This is called **Ackermann's formula**.

## Revisit Example - Vehicle steering (Ex 7.4)

Consider the following system:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & v_0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} av_0/b \\ v_0/b \end{bmatrix} u$$
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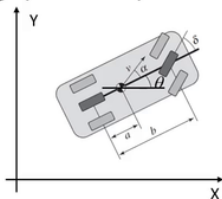
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Determine the characteristic polynomial for the system:

$$\det(sI - A) = \begin{vmatrix} s & -v_0 \\ 0 & s \end{vmatrix} = s^2 = s^2 + 0s + 0$$



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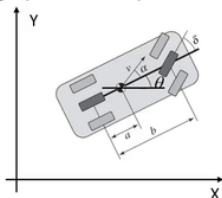
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Desired characteristic polynomial for the closed loop system:

$$p(s) = s^2 + 2\zeta\omega_n s + \omega_n^2$$





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- Karl J. Astrom and Richard M. Murray *Feedback Systems*. Version v3.0i. Princeton University Press. September 2018. Chapter 7.