Internship Program

ReportBy

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GUDLAVALLERU ENGINEERING COLLEGE
(An Autonomous Institute with Permanent Affiliation to JNTUK, Kakinada)
(Sponsored by A. A. N. M & V. V. R. S. R Educational Society, Gudlavalleru)
Approved by AICTE, New Delhi and Permitted by AP State Government
Accredited by NAAC with 'A' Grade
Counselling Code : GDLV

In association with

Smart Internz

Contents

Introduction

Internship program arranged by GUDLAVALLERU ENGINEERING COLLEGE in association with Smart Internz, Hyderabad for the benefit of 3rd year EEE batch 2018-2022 on Electrical Detailed design Engineering for Oil& Gas, Power and Utility industrial sectors.

Program organiser

Smart Bridge, Hyderabad.

Pioneer in organising Internships, knowledge workshops, debates, hackathons, Technical

sessions and Industrial Automation projects.

Courtesy

Dr. Sri B. Dasu – HOD – EEE, GEC

Mr. G. Srinivasa Rao – Internship

coordinatorMr. Ramesh V - Mentor

Mr. Vinay Kumar - System Support

Mr. Harikanth – Software/Technical Support

Program details

Smart Internz program schedule: 4 weeks starting from 3rd May 2021

Daily schedule time shall be 4PM to 6.30PM

Mode of Classes: On line through

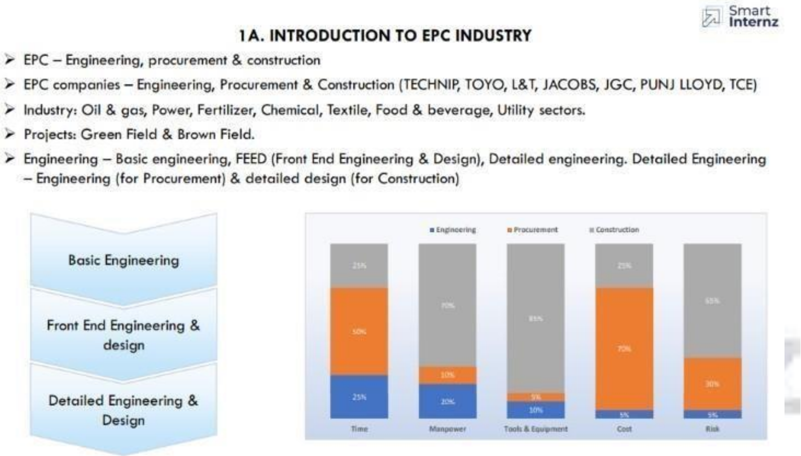
ZOOMPresenter: Mr Ramesh V

Internship program

We have been given the opportunity to learn and interact with industry experienced engineering specialist to learn the Electrical detailed design engineering for various industrial sectors.

3rd May2021: Introduction to EPC Industry

1	EPC Industry & Electrical Detailed Engineering	EPC Industry	Introduction
		Engineering	Types of Engineering
		Procurement	Engineering role in procurement
		Construction	Engineering role during construction

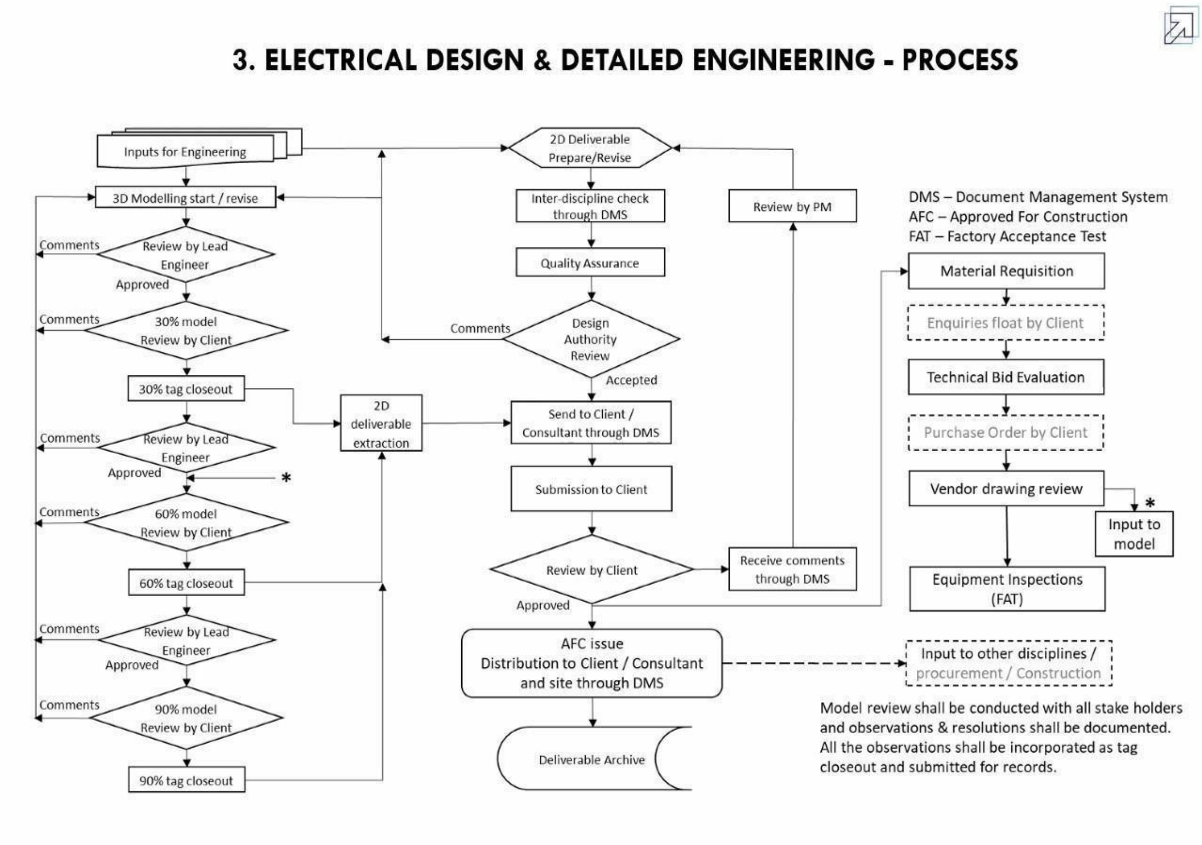


Topic details:

Engineering phases, Engineering deliverables (drawings & documents) list, Design Engineerrole at various phases of project.

4th May2021: Engineering documentation for EPC projects

2	Electrical Design Documentation	Engineering Deliverables list	Sequence of deliverables
		Detailed Engineering work flow	Detailed engineering process
		Document transmission	Document submission and info exchange
		Deliverables types	Different types of deliverables



Topic details:

Engineering deliverables list, detailed engineering flow, engineering support flow,engineering support to procurements.

5 th May2021: Engineering documentation for commands and formulae

3	Document & Drawingtools	MS Word	Report / Calculations formats
		MS Excel	Basic excel commands

3C. AUTOCAD BASIC COMMANDS

Smart Internz

AUTOCAD BASIC KEYS

STANDARD		DRAW		MODIFY		FORMAT	
NEW	Ctrl+N	LINE	L	ERASE	E	PROPERTIES	MO
OPEN	Ctrl+O	RAY	RAY	COPY	CO	SELECT COLOR	COL
SAVE	Ctrl+S	PLINE	PL	MIRROR	MI	LAYER	LA
PLOT	Ctrl+P	3DPOLY	3P	OFFSET	O	LINETYPE	LT
PLOT PREVIEW	PRE	POLIGONE	POL	ARRAY	AR	LINEWEIGHTS	LW
CUT	Ctrl+X	RECTANGLE	REC	MOVE	M	LT SCALE	LTS
COPY	Ctrl+C	ARC	A	ROTATE	RO	LIST	LI
PASTE	Ctrl+V	CIRCLE	C	SCALE	SC	DIMEN. STYLE	D
MATCH PROPE.	MA	SPLINE	SPL	STRECH	S	RENAME	REN
CLOSE	Ctrl+F4	ELLIPSE	EL	TRIM	TR	OPTION	OP
EXIT	Ctrl+Q	BLOCK	B	EXTENED	EX		
		POINT	PO	BRAKE	BR		
		HATCH	H	CHAMFER	CHA		
		GRADIENT	GD	FILLET	F		
		REGION	REG	EXPLODE	X		
		BOUNDARY	BO				
		DONUT	DO				

EXTRA				DRAFTING		PAPER SIZE
UNIT	UN	UCS	UCS	ORTHO	F8, Ctrl+L	A4=210*297
LIMITS	LIMITS	SINGLE TEXT	DT	OSNAP	F3, Ctrl+F	A3=297*420
(0,0; 1000,1000)		MULTILINE TEXT	MT	POLAR	F10, Ctrl+U	A2=420*594
ZOOM	Z	EDIT TEXT	ED	GRID	F7, Ctrl+G	A1=594*841
ALL	A	OBJECT SNAP	OB	OTRACK	F11	A0=841*1189
PAN	P	DIMENTION	DIM	SNAP	F9	
CLEAN SCREEN	Ctrl+0	HORIZONTAL	HOR			
COMMAMD WIN	Ctrl+9	VERTICAL	VER			

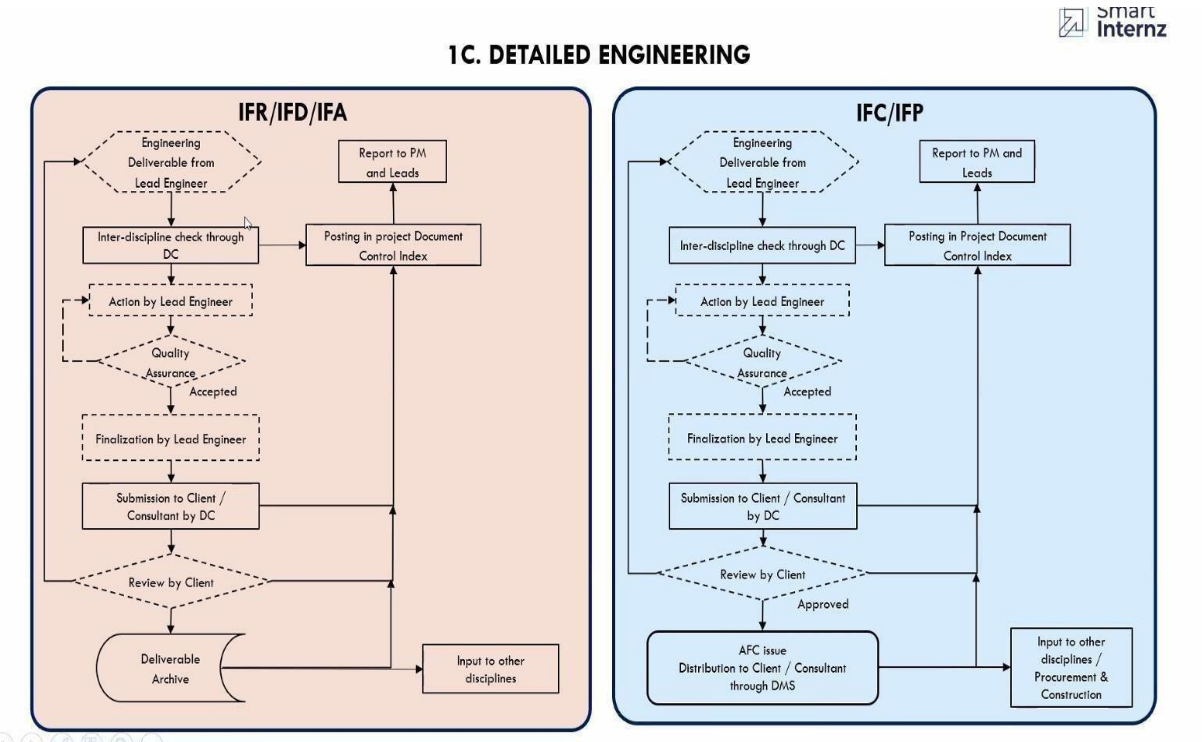
Topic details:

Here we need to learn the basis of the autocadbasic keys like standard, modify,draw,format,papersize etc..

7 th May2021: Engineering documentation for Electrical system design

4	Electrical system design for a small small project	Overall plant description
		Sequence of approach
		Approach to detailed design

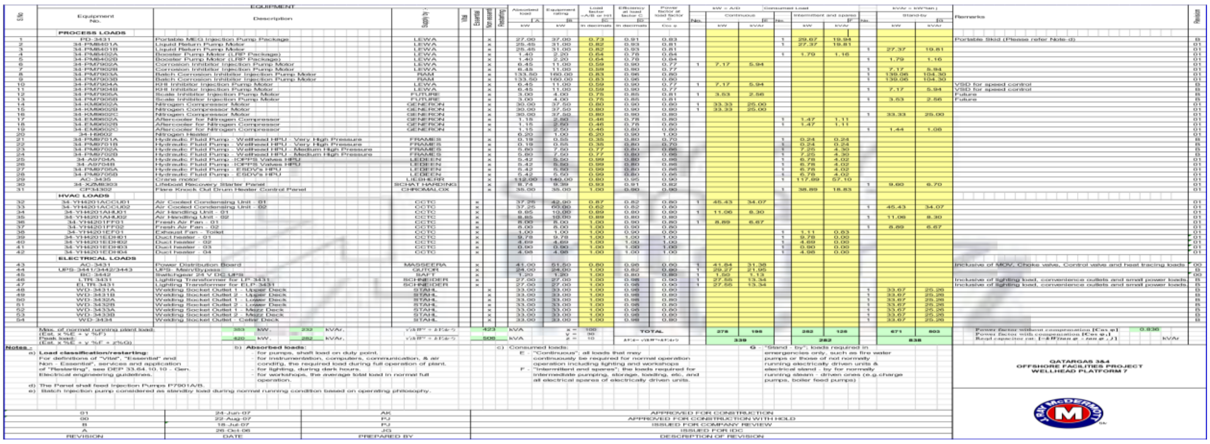
Topic details:



Here we observed that how to do a project and Sequence of approach, Approach to detail design and Overall plant distribution system.

10th May2021: Engineering documentation for Typical diagrams

5	Electrical system design for typical diagrams		
		Load lists shedule	Power flow diagram
		Single line diagram	Typical schematic diagram



S.No	Equipment No.	Description	Supply by	Absorbed load kW
	PROCESS LOADS			
1	PD-3431	Portable MEG Injection Pump Package	LEWA	27.00
2	34-PM8401A	Liquid Return Pump Motor	LEWA	25.45
3	34-PM8401B	Liquid Return Pump Motor	LEWA	25.45
4	34-PM8402A	Booster Pump Motor (LRP Package)	LEWA	1.40
5	34-PM8402B	Booster Pump Motor (LRP Package)	LEWA	1.40
6	34-PM7902A	Corrosion Inhibitor Injection Pump Motor	LEWA	6.45
7	34-PM7902B	Corrosion Inhibitor Injection Pump Motor	LEWA	6.45
8	34-PM7903A	Batch Corrosion Inhibitor Injection Pump Motor	RAM	133.50
9	34-PM7903B	Batch Corrosion Inhibitor Injection Pump Motor	RAM	133.50
10	34-PM7904A	KHI Inhibitor Injection Pump Motor	LEWA	6.45
11	34-PM7904B	KHI Inhibitor Injection Pump Motor	LEWA	6.45
12	34-PM7905A	Scale Inhibitor Injection Pump Motor	FUTURE	3.00
13	34-PM7905B	Scale Inhibitor Injection Pump Motor	FUTURE	3.00
14	34-KM8602A	Nitrogen Compressor Motor	GENERON	30.00
15	34-KM8602B	Nitrogen Compressor Motor	GENERON	30.00
16	34-KM8602C	Nitrogen Compressor Motor	GENERON	30.00
17	34-EM8602A	Aftercooler for Nitrogen Compressor	GENERON	1.15
18	34-EM8602B	Aftercooler for Nitrogen Compressor	GENERON	1.15
19	34-EM8602C	Aftercooler for Nitrogen Compressor	GENERON	1.15
20	34-H8602	Nitrogen Heater		6.20
21	34-PM9701A	Hydraulic Fluid Pump - Wellhead HPU - Very High Pressure	FRAMES	0.19
22	34-PM9701B	Hydraulic Fluid Pump - Wellhead HPU - Very High Pressure	FRAMES	0.19
23	34-PM9702A	Hydraulic Fluid Pump - Wellhead HPU - Medium High Pressure	FRAMES	5.60
24	34-PM9702B	Hydraulic Fluid Pump - Wellhead HPU - Medium High Pressure	FRAMES	5.60
25	34-A9704A	Hydraulic Fluid Pump -IOPPS Valves HPU	LEDEEN	5.42
26	34-A9704B	Hydraulic Fluid Pump -IOPPS Valves HPU	LEDEEN	5.42
27	34-PM9705A	Hydraulic Fluid Pump - ESDV's HPU	LEDEEN	5.42
28	34-PM9705B	Hydraulic Fluid Pump - ESDV's HPU	LEDEEN	5.42
29	AC-3435	Crane motor	LIEBHERR	112.00
30	34-XZM8303	Lifeboat Recovery Starter Panel	SCHAT HARDING	8.74
31	CP34302	Flare Knock Out Drum Heater Control Panel	CHROMALOX	35.00
	HVAC LOADS			
32	34-YH4201ACCU01	Air Cooled Condensing Unit - 01	CCTC	37.25
33	34-YH4201ACCU02	Air Cooled Condensing Unit - 02	CCTC	37.25
34	34-YH4201AHU01	Air Handling Unit - 01	CCTC	8.85
35	34-YH4201AHU02	Air Handling Unit - 02	CCTC	8.85
36	34-YH4201FF01	Fresh Air Fan - 01	CCTC	8.00
37	34-YH4201FF02	Fresh Air Fan - 02	CCTC	8.00
38	34-YH4201EF01	Exhaust Fan - Toilet	CCTC	1.00
39	34-YH4201EDH01	Duct heater - 01	CCTC	9.78
40	34-YH4201EDH02	Duct heater - 02	CCTC	4.69
41	34-YH4201EDH03	Duct heater - 03	CCTC	0.90
42	34-YH4201EDH04	Duct heater - 04	CCTC	4.98
	ELECTRICAL LOADS			
43	AC-3431	Power Distribution Board	MASSEERA	41.00
44	UPS-3441/3442/3443	UPS- Main/Bypass	GUTOR	24.00
45	BC-3442	Switchgear 24 V DC UPS	SAFT	1.20
46	LTR-3431	Lighting Transformer for LP-3431	SCHNEIDER	27.00
47	ELTR-3431	Lighting Transformer for ELP-3431	SCHNEIDER	27.00
48	WD-3431A	Welding Socket Outlet 1 - Upper Deck	STAHL	33.00
49	WD-3431B	Welding Socket Outlet 2 - Upper Deck	STAHL	33.00
50	WD-3432A	Welding Socket Outlet 1 - Lower Deck	STAHL	33.00
51	WD-3432B	Welding Socket Outlet 2 - Lower Deck	STAHL	33.00
52	WD-3433A	Welding Socket Outlet 1 - Mezz Deck	STAHL	33.00
53	WD-3433B	Welding Socket Outlet 2 - Mezz Deck	STAHL	33.00
54	WD-3434	Welding Socket Outlet - Cellar Deck	STAHL	33.00

Max. of normal running plant load (Est. x %E + y %F): 383 kW, 232 kVAr, 423 kVA

Peak load (Est. x %E + y %F + z%G): 420 kW, 282 kVAr, 508 kVA

Notes -

a) Load classification/restarting: For definitions of "Vital", "Essential" and Non - Essential" services and application of "Restarting", see DEP 33.64.10.10 - Gen. Electrical engineering guidelines.

b) Absorbed loads:
- for pumps, shaft load on duty point.
- for instrumentation, computers, communication, & air condit'g, the required load during full operation of plant.
- for lighting, during dark hours.
- for workshops, the average total load in normal full operation.

d) The Panel shall feed Injection Pumps P7901A/B.

e) Batch injection pump considered as standby load during normal running condition based on operating philosophy.

QATARGAS 3&4 OFFSHORE FACILITIES PROJECT WELLHEAD PLATFORM 7

REVISION	DATE	PREPARED BY	DESCRIPTION OF REVISION
01	24-Jun-07	AK	APPROVED FOR CONSTRUCTION
00	22-Aug-07	PJ	APPROVED FOR CONSTRUCTION WITH HOLD
B	18-Jul-07	PJ	ISSUED FOR COMPANY REVIEW
A	26-Oct-06	JG	ISSUED FOR IDC

Topic details:

We conclude here how to do load calculations and Typical diagrams and inernal structure and also about the power flow diagram.

11th May2021: Classification of Transformers and Generators

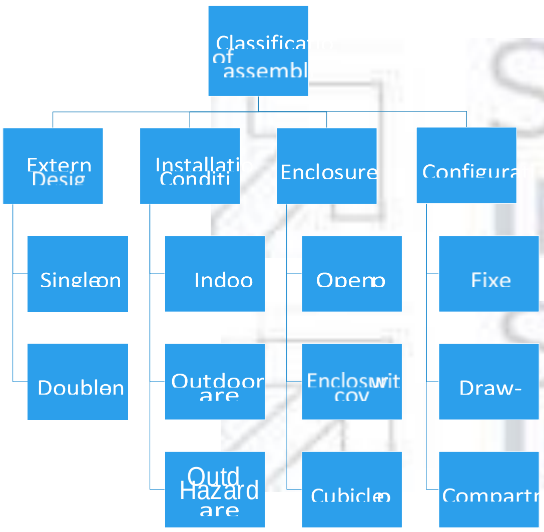
6	Classification of Transformers and Generators	Different types of Transformers	Different types of Generators

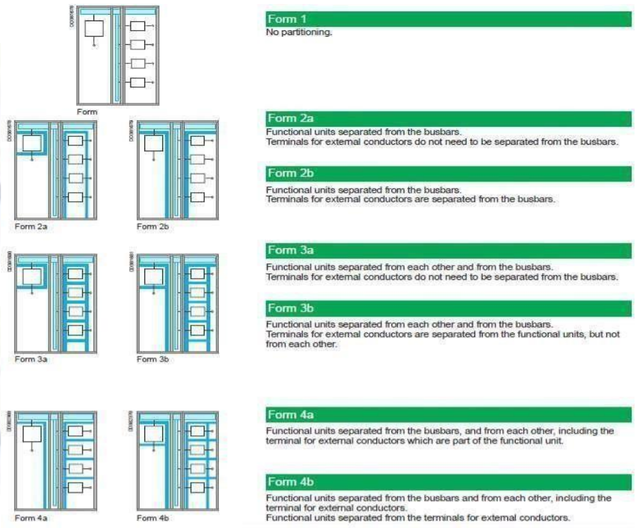
Topic details:

Classification of Transformers and Generators

12th May2021: Classification of Switchgare construction and power factor improvement

7	Classification of Switchgare construction and power factor improvement	Different types of Switchgare assembles	Power factor improvement





Topic details:

Classification of Switchgare contruction and Power Factor Improvement

17th May2021: Detailing about UPS system and Busducts.

8	Detailing about UPS system and Busducts	Uninterruptible power supply system	Busduts of the system

110V or 220V DC UPS System

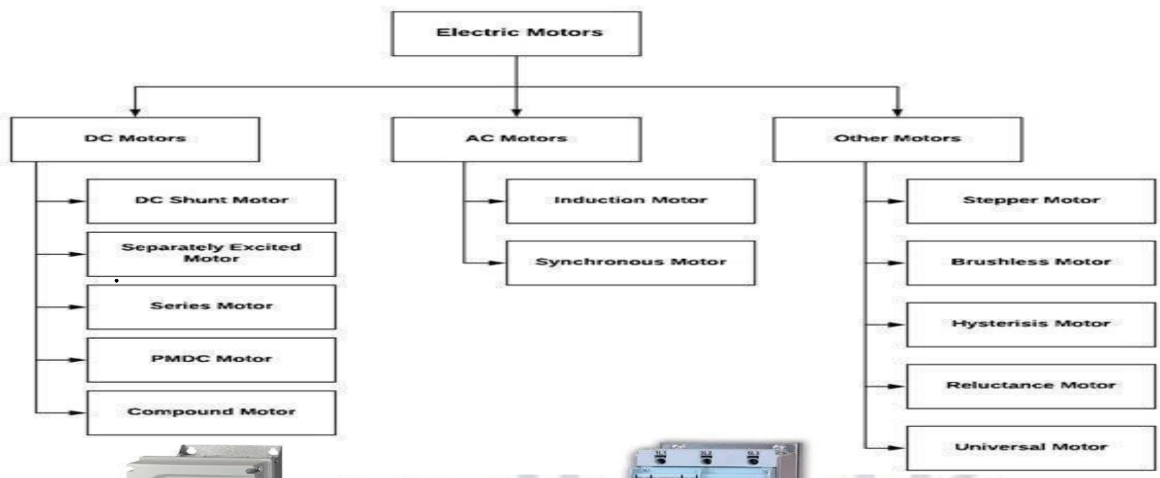
110V or 230V AC UPS System

Topic details: Power distribution of UPS system and Busducts.

UPS systems are designed to provide continuous power to a load, even with an interruption or loss of utility supply power. UPS generally involves a balance of cost Vs need.

18th May2021: Detailing about Motor Starters and Sizing of motors.

9	Detailing about Motor Starters and Sizing of motors	Motor starters and drives	Sizing and selection of motors



Topic details: Detailing about Motor Starter and Sizing of motors and their selection.

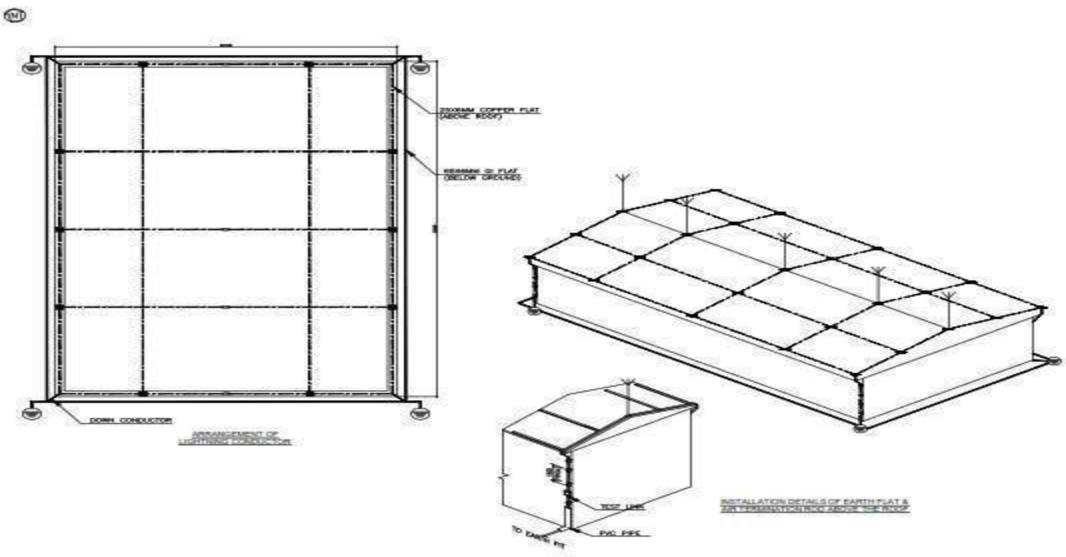
The principal function of a motor starter is to start and stop the respective motor connected with specially designed electromechanical switches which are similar in some ways to relays. The main difference between a relay and a starter is that a starter has overload protection for the motor that is missing in a relay.

Different types of motor starters are as follows:

- Direct-On-Line Starter
- Rotor Resistance Starter
- Stator Resistance Starter
- Auto Transformer Starter

19th May2021: Discribing about Earthing system and Lighting Protection.

10	Discribing about Earthing system and Lighting Protection.	Plant Earthing system	Lighting Protection materials



Topic details: Discribing about Earthing system and Lighting Protection.

Lightning protection required for high rise structures and important buildings against lightning currents during thunder storms. Primarily Lightning protection system calculations are done based on soil resistivity, conductor material, coverage structure / Building to determine whether lightning protection is required or not.

20th May2021: Lighting or illumination systems and calculations.

11	Lighting or Illumination systems and Calculations	Lighting or illumination systems	Lighting calculations

Topic details: Lighting or Illumination systems and Calculations.

All outdoor lighting fittings shall be connected with armoured PVC cable of suitable no. of cores and size. Necessary type and no. of junction boxes shall be provided for branch connections. Indoor light fittings shall be connected with FRLS PVC wires laid in cable trunks or conduits.

Inputs required: Equipment and cable routing layouts, lighting calculations, Design basis for type of light fittings to be used, required lux levels

Lighting calculations software: Dialux, Chalmlite, Calculux, Relux, Luxicon,

CG Lux Applicable Standards: IS 6665: Code of practice for industrial

lighting, IS 3646: Code

of practice for interior illumination, IEC 60598: Luminaires, IEC 62493: Assessment of lighting equipment related to human exposure to electromagnetic field

Deliverables: Indoor Lighting layouts, socket outlet layouts, Street lighting and area lighting layouts. BOQ.

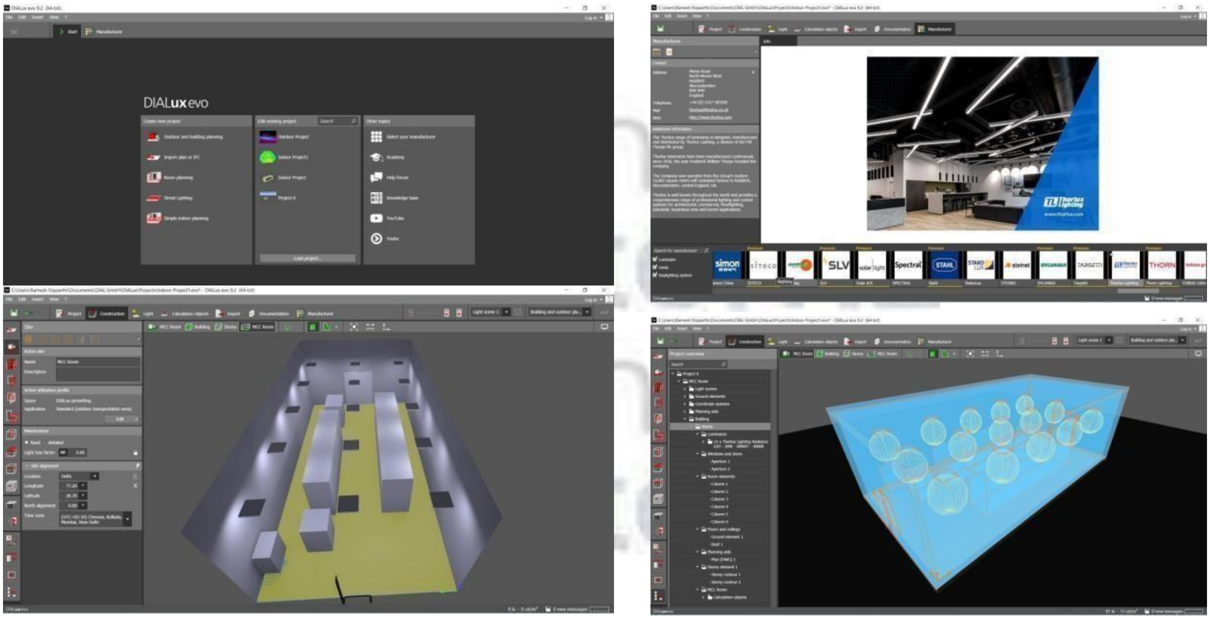
Types of light fittings: Industrial, flame proof type (EX d), increased safety type (Ex e).

21th May2021: Lighting or illumination systems using DIALUX software.

12	Lighting or Illumination using DIALUX software	Lighting or illumination systems	Operation of dialux software

Topic details: Lighting or Illumination Calculations using DIALUX software.

Here we are using this Dialux evo 5.9.2 software windows to construct the power plant and we can perform the operation from this software.



24th May2021: Cabling and their calculations and types.

13	Cabling and their types and claculations	Cabling calculations	Types of cabling materials

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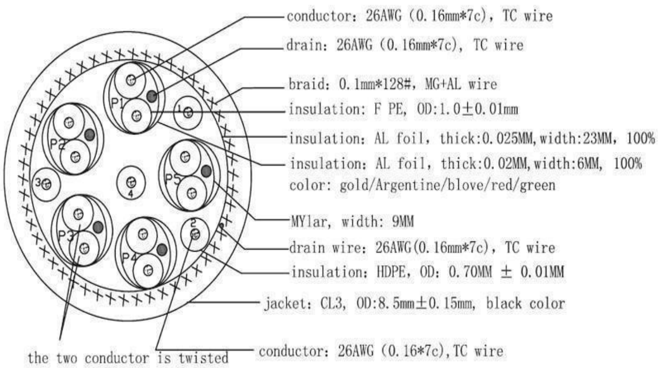
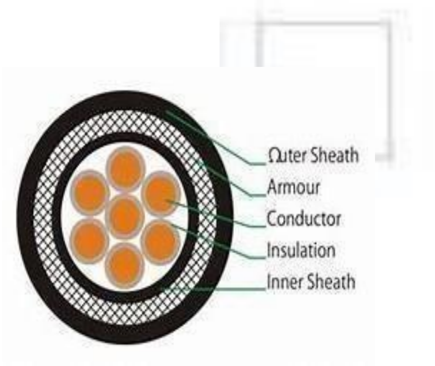
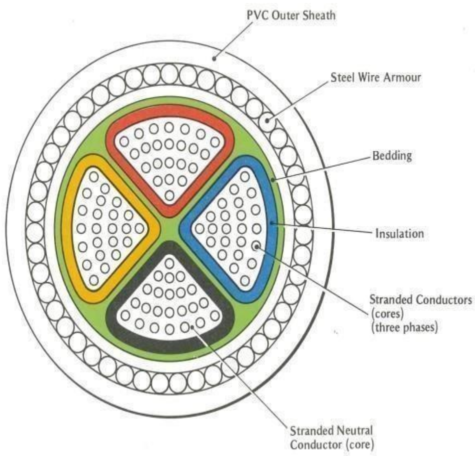
Topic details: Cabling and their types and claculations .







Electrical cables must be properly supported to relieve mechanical stresses on the conductors, and protected from harsh conditions such as abrasion which might degrade the insulation.

Cables generally laid in the cable trays above ground, direct buried underground and in metallic or PVC conduits. Derating factors may be applicable for each type of cable laying conditions.

25th May2021: Cabling calculations and Cable gland selection.

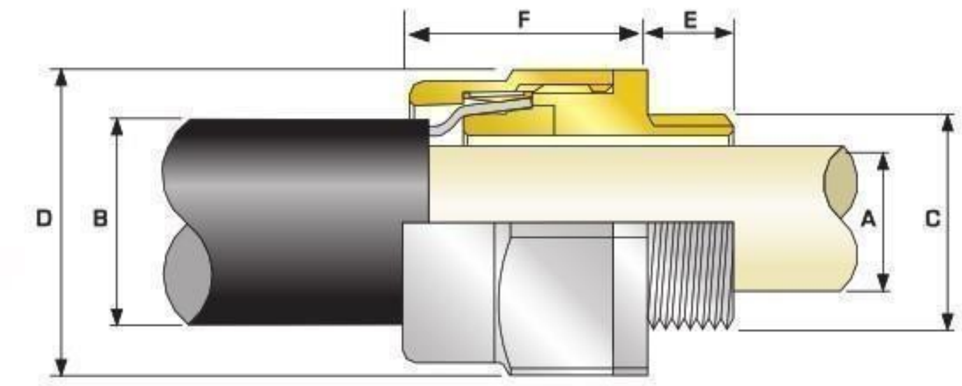
14	Cabling claculations and cable gland selection	Cabling calculations	Cable gland selection

Topic details: Cable sizing calculation and cable gland selection.

Inputs required: Load List, Design basis, Electrical equipment layout, cable schedule, vendor catalogues for cable tray.

Cable tray sizing shall be performed for each branch of cable tray routing up to the load point. Results shall be checked with specified limits mentioned in design basis.

Cable gland:



Cable Gland Selection Table
Refer to illustration at the top of the page.

Cable Gland Size	Available Entry Threads "C" (Alternate Metric Thread Lengths Available)		Cable Bedding Diameter "A"	Overall Cable Diameter "B"	Armour Range		Across Flats "D"	Across Corners "D"	Protrusion Length "F"
	Metric	Thread Length (Metric) "E"	Max	Max	Min	Max	Max	Max	
20S16	M20	10.0	8.7	13.2	0.8	1.25	24.0	26.4	35.2
20S	M20	10.0	11.7	15.9	0.8	1.25	24.0	26.4	32.2
20	M20	10.0	14.0	20.9	0.8	1.25	30.5	33.6	30.6
25	M25	10.0	20.0	26.2	1.25	1.6	36.0	39.6	36.4
32	M32	10.0	26.3	33.9	1.6	2.0	46.0	50.6	32.6
40	M40	15.0	32.2	40.4	1.6	2.0	55.0	60.5	36.6
50S	M50	15.0	38.2	46.7	2.0	2.5	60.0	66.0	39.6
50	M50	15.0	44.1	53.1	2.0	2.5	70.1	77.1	39.1
63S	M63	15.0	50.0	59.4	2.0	2.5	75.0	82.5	52.0
63	M63	15.0	56.0	65.9	2.0	2.5	80.0	88.0	49.8
75S	M75	15.0	62.0	72.1	2.0	2.5	90.0	99.0	63.7
75	M75	15.0	68.0	78.5	2.5	3.0	100.0	110.0	57.3
90	M90	24.0	80.0	90.4	3.15	4.0	114.3	125.7	66.6

28 th May2021: Load calculations and Transformer sizing calculations

15	Load calculations and TR calculations	Load calculations	TR calculations

Topic details:

List of electrical load calculations.

Assignment-1
ELECTRICAL LOAD CALCULATIONS LV MCC

Sl. No.	Equipment No.	Equipment Description	Breaker Rating (A)	Breaker Type	Breaker No. of Poles	ELCB Rating (mA)	Absorbed Load [A] kW	Motor / Load Rating [B] kW	Load Factor [A] / [B] [C] decimal	Efficiency at Load Factor [C] [D] decimal	Power Factor at Load Factor [C] cos φ	Consumed Load (kW = [A] / [D]; kVAR = kW x tan φ) Continuous kW	Continuous kVAR	Intermittent kW	Intermittent kVAR	Stand-by kW	Stand-by kVAR	Remarks
1	PU2315	Silica filter feed pump					101.41	110.00	0.92	0.93	0.82	109.04	76.11					
2	PU 2314-A	Absorbesnt/Neutral oil pump (W)					29.46	30.00	0.98	0.91	0.78	32.4	26.0					
3	PU 2314 -B	Absorbesnt/Neutral oil pump (S)					25.33	30.00	0.84	0.91	0.78					27.8	22.3	
4	PU2305	Feed Pump (Seperator)					102.42	110.00	0.93	0.93	0.82	110.1	76.9					
5	MX2305	MIXER (W)					103.21	110.00	0.94	0.93	0.82	111.0	77.6					
6	MX 2308	MIXER (S)					103.21	110.00	0.94	0.93	0.82					111.0	77.6	
7	BW2313	Blower					44.31	45.00	0.98	0.91	0.78	48.7	39.1					
8	Rotary valve	TK 2313B (I)					4.30	4.70	0.91	0.85	0.73			5.1	4.7			
9	SC2314	Screw conveyor (I)					9.95	11.00	0.90	0.85	0.73			11.71	10.96			
10	AG 2324A	Citric acid tan agitator (W)					7.48	7.50	1.00	0.85	0.73	8.80	8.24					
11	AG 2324B	Citric acid tank agitator (S)					7.48	7.50	1.00	0.85	0.73					8.8	8.2	
12	AG 2305	Citric oil rection vessel agitator					27.17	30.00	0.91	0.91	0.73	29.86	27.96					
13	AG 2309	Lye oil reaction vessel agitator					9.89	11.00	0.90	0.85	0.73	11.64	10.89					
14	AG 2310	Lye oil reaction vessel agitator					9.89	11.00	0.90	0.85	0.73	11.64	10.89					
15	AG 2314	Soap Adsorbant Tank Agitator					17.30	18.50	0.94	0.85	0.73	20.35	19.06					
											TOTAL	493.50	372.52	16.76	15.70	147.61	109.03	
											kVA	618.31		22.97		182.92		

Maximum of normal running plant load : (Est. x%E + y%F) 499.5 kW 377.2 kVAR sqrt (kW² +kVAR²) = 625.2 kVA

Peak Load : (Est. x%E + y%F + z%G) 513.3 kW 388.0 kVAR sqrt (kW² +kVAR²) = 643.5 kVA

Assumptions

1) Load factor, Efficiency and Power factor.

Load Rating (kW)	Efficiency	Power factor
<= 20	0.85	0.73
> 20 - <= 45	0.91	0.78
> 45 - < 150	0.93	0.82
>= 150	0.94	0.91

2) Coincidence factors x= 1.0, y= 0.3, and z=0.1 considered for contnious, intermittent and standby load.

T/F calculation:

Assignment - 2

Calculation for Transformer Capacity

1.0 Example of calculation for Transformer Capacity

1.1 Calculation for consumed load

Consumed loads used for this example are as follows :

	kW	kVar	kVA	
a. Continuous load	493.5	372.5	618.31	— (I)
b. Intermittent load / Diversity Factor	16.76	15.7	22.96	— (II)
c. Stand-by load required as consumed load	147.61	108.0	182.92	— (III)
Max. Consumed load = ((I) + 30% (II) + 10% (III)) =	513.3	388.0	643.46	
Future expansion load (20% capacity)	102.7	77.6	128.69	
Total Load =	615.9	465.6	772.15	

1.2 Calculation for 3.3kV / 0.433 kV transformer capacity

Max. Consumed load = 643.5 KVA
Spare capacity = 128.7 KVA
Required capacity = 772.1 KVA
Transformer rated capacity = 750 KVA

1.3 Voltage regulation check

During starting or reacceleration of max. capacity motor (3400 kW), while all the other loads running , the voltage regulation is as follows :

P_T = 750 KVA (%Z)= 5.19 & Ratio X/R = 5.4

Hence , %R = = 0.941 %

%X = = 5.10 %

P_M = 110 KW having (K = 6 & C = 1 & Cos θ = 0.82 & Eff.η = 0.93 & Cos θs = 0.25

P_S = = 865.46 KVA

Cos $θ_S$ = 0.25 ,Corresponding to Angle $θ_s$ = 75.5225 Degrees for which Sin $θ_s$ = 0.97

P_B = 405 KVA & PB in KW is = 344.25 & P_B in Kvar = 202.5 ∴ Cos $θ_B$ = 0.850

Cos $θ_B$ = 0.85 ,Corresponding to Angle $θ_s$ = 31.7883 Degrees, for which Sin $θ_s$ = 0.53

P_{CP} = = 560.615 KW
P_{CQ} = = 1040.48 KVAR
P_C = = 1181.9 KVA
Cos $θ_C$ = = 0.47433 , where as Sin $θ_C$ = 0.880

Voltage Regulation ε = 7.8 %

Result: During starting of max. capacity motor, while all other loads are running , the voltage regulation at Transformer secondary terminals is approx. 6.5% , which meets the criteria to maintain less than 15% voltage regulation.

1.4 Selection of rated capacity

750 KVA transformer selected.

29th May2021: DG set calculations

16	DG set calculations

Topic details:

Transformer and DG set calculations,types ,sizing or selections

Assignment 3

DG SIZING CALCULATIONS

	Design Data		
	Rated Volatge	415	KV
	Power factor (CosØ)	0.764	Avg
	Efficiency	0.88	Avg
	Total operating load on DG set in KVA at 0.764 power factor	625.2	
	Largest motor to start in the sequence - load in KW	115	KW
	Running KVA of last motor (CosØ= 0.91)	171	KVA
	Starting current ratio of motor	6	(Considering starting method as Soft starter)
	Starting KVA of the largest motor (Running KVA of last motor X Starting current ratio of motor)	1026	KVA
	Base load of DG set in KVA (Total operating load in KVA – Running KVA of last motor)	454	KVA
A	**Continous operation under load -P1**		
	Capacity of DG set based on continuous operation under load P1	454	KVA
B	**Transient Voltage dip during starting of Last motor P2**		
	Total momentary load in KVA (Starting KVA of the last motor+Base load of DG set in KVA	1480	KVA
	Subtransient Reactance of Generator (Xd'')	7.91%	(Assumed)
	Transient Reactance of Generator (Xd')	10.065%	(Assumed)
	Xd''' =(Xd''+Xd')/2	0.089875	
	Transient Voltage Dip	15%	(Max)
	Transient Voltage dip during Soft starter starting of Last motor P2 = Total momentary load in KVA x Xd''' x (1-Transient Voltage Dip) / (Transient Voltage Dip)	754	KVA
C	**Overload capacity P3**		
	Capacity of DG set required considering overload capacity		
	Total momentary load in KVA	1480	KVA
	overcurrent capacity of DG (K) (Ref: IS/IEC 60034-1, Clause 9.3.2)	150%	
	Capacity of DG set required considering overload capacity (P3) = Total momentary load in KVA / overcurrent capacity of DG (K)	987	KVA
	Considering the last value amongst P1, P2 and P3		
	Continous operation under load -P1	454	KVA
	Transient Voltage dip during Soft starter starting of Last motor P2	754	KVA
	Overload capacity P3	987	KVA
	Considering the last value amongst P1, P2 and P3	987	KVA
	Hence, Existing Generator 987 KVA is adequate to cater the loads as per re-scheduled loads		
	NOTE:VOLTAGE DIP CONSIDERED - 15%		

2nd june2021: Caluculations of Earthing and Lighting protection.

17	Calculation of Earthing and Lighting protection calculations	Earthing calculations	Lighting protection calculation

Topic details:

Calculation of Earthing and Lighting protection calculations

Assignment 4

Earthing	2	
Maximum line-to-ground fault in kA for 1 sec	17	
Earthing material (Earth rod & earth strip)	GI	
Depth of earth flat burrial in meter	0.5	
Average depth / length of Earth rod in meters	4.5	
Soil resistivity Ω-meter	7.5	
Ambient temperature in deg C	55	
Plot dimensions (earth grid) L x B in meters	80	140
Number of earth rods in nos.	6	

Earth electrode sizing:

Ac - Required conductor cross section in sq.mm

$$I_{lg} = A_c x \sqrt{\left[\frac{TCAPx10^{-4}}{t_c X \alpha_r X \rho_r}\right] x l_n \left[\frac{K_o + T_m}{K_o + T_a}\right]}$$

αr - Thermal co-efficient of resistivity, at 20 oC	0.0032
ρr - Resistivity of ground conductor at 20 oC	20.10
Ta - Ambient Temperature is °C	50
I_{l-g} - RMS fault current in kA = 50 KA	14
tc - Short circuit current duration sec	1
Thermal capacity factor, TCAP J/(cm3.oC)	3.93
Tm - Maximum allowable temperature for copper conductor, in oC	419
K0 - Factor at oC	293
The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:	
14 = Ac *	0.123
Ac - Required conductor cross section in sq.mm	114
Earth rod dia in mm	12
Earth rod dia (including 25% corrosion allowance) in mm	15

Earth flat sizing:

Ac - Required conductor cross section in sq.mm

$$I_{lg} = A_c x \sqrt{\left[\frac{TCAPx10^{-4}}{t_c X \alpha_r X \rho_r}\right] x l_n \left[\frac{K_o + T_m}{K_o + T_a}\right]}$$

αr - Thermal co-efficient of resistivity, at 20 oC	0.0032
ρr - Resistivity of ground conductor at 20 oC	20.10
Ta - Ambient Temperature is °C	50
I_{l-g} - RMS fault current in kA = 50 KA	14
tc - Short circuit current duration sec	1
Thermal capacity factor, TCAP J/(cm3.oC)	3.93
Tm - Maximum allowable temperature for copper conductor, in oC	419
K0 - Factor at oC	293
The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:	
14 = Ac *	0.123

Assignment 5

	1
Location	Khammam
Building	Concrete, Industrial
Type of Building	Flat Roofs (a)
Building Length (L)	11
Building breadth (W)	7
Building Height (H)	9

Risk Factor Calculation

1	Collection Area (A_c)			
	A_c		=	(L*W) + (2*L*H) + (2*W*H) + (3.14*H*H)
				655.34
2	Probability of Being Struck (P)			
	P		=	A_c * N_g * 10^{-6}
				0.001245146
3	Overall weighing factor			
	a) Use of structure (A)		=	1.0
	b) Type of construction (B)		=	1.4
	c) Contents or consequential effects (C)		=	0.8
	d) Degree of isolation (D)		=	1.0
	e) Type of country (E)		=	0.3
	Wo - Overall weighing factor		=	A * B * C * D * E
			=	0.336
4	Overall Risk Factor	Po	=	P * Wo
		Po	=	0.000418369
		Pa		10^{-5}

As per clause no. 9.7 of BS- 6651, suggested acceptable risk factor (Po) has been taken as 10^{-5}
Since Po > Pa lightning protection required.

5	Air Terminations			
	Perimeter of the building	=	2(L+W)	
		=	36	Mts.
6	Down Conductors			
	Perimeter of building	=	36	Mts.
	No. of down conductors based on perimeter	=	2	Nos.

Hence 2 nos. of Down conductors have been selected.

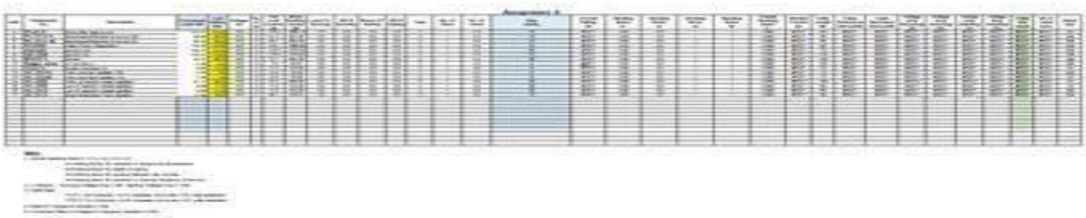
Size of Down conductor = 20 X 2.5 mm Galvanized Steel Strip
(As per BS6651, lightning currents have very short duration, therefore thermal factors are of little consequence in deciding the cross-section of the conductor. The minimum size of Down conductors - 20mm X 2.5 mm Galvanized Steel Strip)

5 th june 2021: Cable sizing and cable tray sizing calculations.

18	Cable sizing and cable tray sizing calculations	Cable sizing calculations	Cable tray calculation

Topic details:

Cable sizing and cable tray sizing calculations for LV cables and MV/HV cables.



Conclusion

We have been taught many aspects of engineering activities during the EPC stages for all electrical and related other disciplines also.

Feedback

Smart Bridge

They conduct summer internships, work shops, debates, hackthons, technical sessions.

Method of conducting program

Online virtual program with presentation slides and explanation on the topic and practical usage of topic and with some examples.

Program highlights

It is for the detailed design of any industrial sectors.

Material

The material was good .

Benefits

It has been given the opportunity to learn and interact with industry experienced engineering specialist to learn the Electrical detailed design engineering for various industrial sectors.

Assignment-1

ELECTRICAL LOAD CALCULATIONS LV

MCC

Sl. No.	Equipment No.	Equipment Description	Breaker Rating	Breaker Type	Breaker No. of Poles	ELCB Rating	Absorbed Load [A]	Motor / Load Rating [B]	Load Factor [A] / [B] [C]	Efficiency at Load Factor [C] [D]	Power Factor at Load Factor [C]	Consumed Load (kW = [A] / [D]; kVAR = kW x tan φ) Continuous		Intermittent		Stand-by		Remarks
			A			mA	kW	kW	decimal	decimal	cos φ	kW	kVAR	kW	kVAR	kW	kVAR	
1	PU2315	Silica filter feed pump					101.41	110.00	0.92	0.93	0.82	109.04	76.11					
2	PU 2314-A	Absorbesnt/Neutral oil pump (W)					29.46	30.00	0.98	0.91	0.78	32.4	26.0					
3	PU 2314 -B	Absorbesnt/Neutral oil pump (S)					25.33	30.00	0.84	0.91	0.78					27.8	22.3	
4	PU2305	Feed Pump (Seperator)					102.42	110.00	0.93	0.93	0.82	110.1	76.9					
5	MX2305	MIXER (W)					103.21	110.00	0.94	0.93	0.82	111.0	77.5					
6	MX 2308	MIXER (S)					103.21	110.00	0.94	0.93	0.82					111.0	77.5	
7	BW2313	Blower					44.31	45.00	0.98	0.91	0.78	48.7	39.1					
8	Rotary valve	TK 2313B (I)					4.30	4.70	0.91	0.85	0.73			5.1	4.7			
9	SC2314	Screw conveyor (I)					9.95	11.00	0.90	0.85	0.73			11.71	10.96			
10	AG 2324A	Citric acid tan agitator (W)					7.48	7.50	1.00	0.85	0.73	8.80	8.24					
11	AG 2324B	Citric acid tank agitator (S)					7.48	7.50	1.00	0.85	0.73					8.8	8.2	
12	AG 2305	Citric oil rection vessol agitator					27.17	30.00	0.91	0.91	0.73	29.86	27.95					
13	AG 2309	Lye oil reaction vessel agitator					9.89	11.00	0.90	0.85	0.73	11.64	10.89					
14	AG 2310	Lye oil reaction vessel agitator					9.89	11.00	0.90	0.85	0.73	11.64	10.89					
15	AG 2314	Soap Adsorbant Tank Agitator					17.30	18.50	0.94	0.85	0.73	20.35	19.06					

Maximum of normal running plant load : 498.5 kW 377.2 kVAR sqrt (kW² +kVAR²) = 625.2 kVA
(Est. x%E + y%F)

Peak Load : 513.3 kW 388.0 kVAR sqrt (kW² +kVAR²) = 643.5 kVA
(Est. x%E + y%F + z%G)

	Continuous kW	Continuous kVAR	Intermittent kW	Intermittent kVAR	Stand-by kW	Stand-by kVAR
TOTAL	493.50	372.52	16.76	15.70	147.61	108.03
kVA	618.31		22.97		182.92	

<u>Assumptions</u>

1) Load factor, Efficiency and Power factor.

Load Rating (kW)	Efficiency	Power factor
<= 20	0.85	0.73
> 20 - <= 45	0.91	0.78
> 45 - < 150	0.93	0.82
>= 150	0.94	0.91

2) Coincidence factors x= 1.0, y= 0.3, and z=0.1 considered for contnious, intermittent and standby load.

Assignment - 2

Calculation for Transformer Capacity

1.0 Example of calculation for Transformer Capacity

1.1 Calculation for consumed load

Consumed loads used for this example are as follows :

	kW	kVar	kVA	
a. Continuous load	493.5	372.5	618.31	--- (i)
b. Intermittent load / Diversity Factor	16.76	15.7	22.96	--- (ii)
c. Stand-by load required as consumed load	147.61	108.0	182.92	--- (iii)
Max. Consumed load = ((i) + 30% (ii) + 10% (iii)) =	513.3	388.0	643.46	
Future expansion load (20% capacity)	102.7	77.6	128.69	
Total Load =	615.9	465.6	772.15	

1.2 Calculation for 3.3kV / 0.433 kV transformer capacity

Max. Consumed load	=	643.5 kVA
Spare capacity	=	128.7 kVA
Required capacity	=	772.1 kVA
Transformer rated capacity	=	750 kVA

1.3 Voltage regulation check

During starting or reacceleration of max. capacity motor (3400 kW) , while all the other loads running , the voltage regulation is as follows : P_T =

750 KVA (%Z)= 5.19 & Ratio X/R = 5.4

Hence , **%R** = = 0.941 %

%X = = 5.10 %

P_M = 110 KW having (K = 6 & C = 1 & Cosθ 0.82 & Eff. 0.93 & Cos s 0.25

P_S = = 865.46 KVA

Cos θ_S = 0.25 ,Corresponding to Angle θ_s = 75.5225 Degrees for which Sin $_s$ = 0.97

P_B = 405 KVA & PB in KW is = 344.25 & P_B in Kvar = 202.5 Cos θ_B = 0.850

Cos θ_B = 0.85 ,Corresponding to Angle θ_s = 31.7883 Degrees, for which Sin θ_s = 0.53

P_{CP} = = 560.615 KW

P_{CQ} = = 1040.48 KVAR

P_C = = 1181.9 KVA

Cos θ_C = = 0.47433 , where as Sin θ_C = 0.880

Voltage Regulation = 7.8 %

Result: During starting of max. capacity motor, while all other loads are running , the voltage regulation at Transformer secondary terminals is approx. 6.5% , which meets the criteria to maintain less than 15% voltage regulation.

1.4 Selection of rated capacity

750 kVA transformer selected.

Assignment 3

DG SIZING CALCULATIONS

Design Data		
Rated Volatge	415	KV
Power factor (CosØ)	0.764	Avg
Efficiency	0.88	Avg
Total operating load on DG set in kVA at 0.764 power factor	**625.2**	
Largest motor to start in the sequence - load in KW	115	KW
Running kVA of last motor (CosØ= 0.91)	171	KVA
Starting current ratio of motor	6	(Considering starting method as Soft starter)
Starting KVA of the largest motor (Running kVA of last motor X Starting current ratio of motor)	**1026**	KVA
Base load of DG set in KVA (Total operating load in kVA – Running kVA of last motor)	**454**	KVA
A **Continous operation under load -P1**		
Capacity of DG set based on continuous operation under load P1	**454**	**KVA**
B Transient Voltage dip during starting of Last motor P2		
Total momentary load in KVA (Starting KVA of the last motor+Base load of DG set in KVA	1480	KVA
Subtransient Reactance of Generator (Xd’’)	7.91%	(Assumed)
Transient Reactance of Generator (Xd’)	10.065%	(Assumed)
Xd’’’ =(Xd"+Xd')/2	0.089875	
Transient Voltage Dip	15%	(Max)
Transient Voltage dip during Soft starter starting of Last motor P2 = Total momentary load in KVA x Xd''' x $\frac{\text{(1-Transient Voltage Dip)}}{\text{(Transient VoltageDip)}}$	**754**	**KVA**
C Overload capacity P3		
Capacity of DG set required considering overload capacity		
Total momentary load in KVA	1480	KVA
overcurrent capacity of DG (K) (Ref: IS/IEC 60034-1, Clause 9.3.2)	150%	
Capacity of DG set required considering overload capacity (P3) = $\frac{\text{Total momentary load in KVA}}{\text{overcurrent capacity of DG (K)}}$	**987**	**KVA**
Considering the last value amongst P1, P2 and P3		
Continous operation under load -P1	454	KVA
Transient Voltage dip during Soft starter starting of Last motor P2	754	KVA
Overload capacity P3	987	KVA
Considering the last value amongst P1, P2 and P3	**987**	**KVA**

Hence, Existing Generator 987 KVA is adequate to cater the loads as per re-scheduled loads

NOTE:VOLTAGE DIP CONSIDERED - 15%

Assignment 4
Earthing

2

Maximum line-to-ground fault in kA for 1 sec	17	
Earthing material (Earth rod & earth strip)	GI	
Depth of earth flat burrial in meter	0.5	
Average depth / length of Earth rod in meters	4.5	
Soil resistivity Ω-meter	7.5	
Ambient temperature in deg C	55	
Plot dimensions (earth grid) L x B in meters	80	140
Number of earth rods in nos.	6	

Earth electrode sizing:
Ac - Required conductor cross section in sq.mm

$$I_{lg} = A_c x \sqrt{\left[\frac{TCAPx10^{-4}}{t_c x \alpha_r x \rho_r}\right] x l_n \left[\frac{K_0 + T_m}{K_0 + T_a}\right]}$$

αr - Thermal co-efficient of resistivity, at 20 oC	0.0032
ρr - Resistivity of ground conductor at 20 oC	20.10
Ta - Ambient Temperature is °C	50
$I_{l\text{-}g}$ - RMS fault current in kA = 50 KA	14
tc - Short circuit current duration sec	1
Thermal capacity factor, TCAP J/(cm3.oC)	3.93
Tm - Maximum allowable temperature for copper conductor, in oC	419
K0 - Factor at oC	293
The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:	
14 = Ac *	0.123
Ac - Required conductor cross section in sq.mm	114
Earth rod dia in mm	12
Earth rod dia (including 25% corrosion allowance) in mm	15

Earth flat sizing:
Ac - Required conductor cross section in sq.mm

$$I_{lg} = A_c x \sqrt{\left[\frac{TCAPx10^{-4}}{t_c x \alpha_r x \rho_r}\right] x l_n \left[\frac{K_0 + T_m}{K_0 + T_a}\right]}$$

αr - Thermal co-efficient of resistivity, at 20 oC	0.0032
ρr - Resistivity of ground conductor at 20 oC	20.10
Ta - Ambient Temperature is °C	50
$I_{l\text{-}g}$ - RMS fault current in kA = 50 KA	14
tc - Short circuit current duration sec	1
Thermal capacity factor, TCAP J/(cm3.oC)	3.93
Tm - Maximum allowable temperature for copper conductor, in oC	419
K0 - Factor at oC	293
The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:	
14 = Ac *	0.123

Ac - Required conductor cross section in sq.mm	114
Earth flat area in mm	12
Earth flat area (including 25% corrosion allowance) in mm	15
Selected flat size W * Thk in sq mm	20

Rg - Grid resistance

Grid resistance can be calculated using Eq. 52 of IEEE 80

ρ - Soil resistivity in Ω-meter=	7.5
L - Total buried length of ground conductor in meter	440
h - Depth of burial in meter	0.5
A - Grid area in sq. meter	11200
Rg - Grid resistance	0.048

Rr - Earth Electrode resistance

Grid resistance can be calcu lated using Eq. 55 of IEEE 80

$$R_r = \frac{\rho}{2 \times \pi \times n_r \times L_r}\left[\ln\left(\frac{4 \times L_r}{b}\right) - 1 + \frac{2 \times k_1 \times L_r}{\sqrt{A}}\left(\sqrt{n_r} - 1\right)^2\right]$$

ρ - Soil resistivity in Ω-meter, 16.96	7.5
n - No of earth electrodes	6
Lr - Length of earth electrode in meter	4.5
b - Diameter of earth electrode in meter	0.020
k1 - co-efficient	1
A - Area of grid in square metre	11200
Rr - Earth Electrode resistance	2.75561

Grounding system resistance

Grounding system resistance can be calculated using equation 53 of IEEE 80 as follows:

$$R_s = \frac{R_g \times R_2 - R_m^2}{R_g + R_2 - 2R_m}$$

R_m - Mutual ground resistance between the group of ground conductors, R_g and group of electrodes, R_r in Ω. Neglected R_m, since this is for homogenous soil

Rs - Total earthing system resistance 0.048 Ohms

The calculated resistance grounding system is less than the allowable 1 Ω value.

Assignment 5

1

Location	Khammam
Building	Concrete, Industrial
Type of Building	Flat Roofs (a)
Building Length (L)	11
Building breadth (W)	7
Building Height (H)	9

Risk Factor
Calculation1 Collection Area (A_c)

A_c		=	(L*W) + (2*L*H) + (2*W*H) + (3.14*H*H)
			655.34

2 Probability of Being Struck(P)

P		=	$A_c * N_g * 10^{-6}$
			0.001245146

3 Overall weighing factor

a) Use of structure (A)		=	1.0
b) Type of construction (B)		=	1.4
c) Contents or consequential effects (C)		=	0.8
d) Degree of isolation (D)		=	1.0
e) Type of country (E)		=	0.3
Wo - Overallweighing factor		=	A * B * C * D *E
		=	0.336
4 Overall Risk Factor	Po	=	P * Wo
	Po	=	0.000418369
	Pa		10

As per clause no. 9.7 of BS- 6651, suggested acceptable risk factor (Po) has been taken as 10^{-5}
Since Po > Pa lightning protection required.

5 Air Terminations

Perimeter of the building	=	2(L+W	
	=	)	Mts.
		36	

6 Down Conductors

Perimeter of building	=	36	Mts.
No. of down conductors based on perimeter	=	2	Nos.

Hence 2 nos. of Down conductors have been selected.

Size of Down conductor = 20 X 2.5 mm Galvanized Steel Strip(As per BS6651, lightning currents have very short duration, therefore thermal factors are of little consequence in deciding the cross-section of the conductor. The minimum size of Down conductors - 20mm X 2.5 mm Galvanized Steel Strip)

Assignment -6

S.NO.	Equipment No.	Description	Consumed Load KW	Load Rating KW	Voltage (V)	No. of ph	Full Load Current (A)	Motor Starting Current (A)	Load P.F. Running	SIN Φ Running	Motor P.F Staring	SIN Φ Staring	Type	No. of Runs	No. of Cores	Size (mm2)
3	PU2315	Silica filter feed pump	101.41	110.00	415	3	176.4	1058.15	0.8	0.6	0.8	0.5	2	1	4.0	70
4	PU 2314-A	Absorbesnt/Neutral oil pump (W)	29.46	30.00	415	3	51.2	307.40	0.8	0.6	0.8	0.5	2	1	4.0	16
5	PU 2314 -B	Absorbesnt/Neutral oil pump (S)	25.33	30.00	415	3	44.1	264.30	0.8	0.6	0.8	0.5	2	1	4.0	10
6	PU2305	Feed Pump (Seperator)	102.42	110.00	415	3	178.1	1068.69	0.8	0.6	0.8	0.5	2	1	4.0	70
7	MX2305	MIXER (W)	103.21	110.00	415	3	179.5	1076.93	0.8	0.6	0.8	0.5	2	1	4.0	50
8	MX 2308	MIXER (S)	103.21	110.00	415	3	179.5	1076.93	0.8	0.6	0.8	0.5	2	1	4.0	70
9	BW2313	Blower	44.31	45.00	415	3	77.1	462.35	0.8	0.6	0.8	0.5	2	1	4.0	35
10	Rotary valve	TK 2313B (I)	4.30	4.70	415	3	7.5	44.87	0.8	0.6	0.8	0.5	2	1	4.0	4
11	SC2314	Screw conveyor (I)	9.95	11.00	415	3	17.3	103.82	0.8	0.6	0.8	0.5	2	1	4.0	6
12	AG 2324A	Citric acid tan agitator (W)	7.48	7.50	415	3	13.0	78.05	0.8	0.6	0.8	0.5	2	1	4.0	6
13	AG 2324B	Citric acid tank agitator (S)	7.48	7.50	415	3	13.0	78.05	0.8	0.6	0.8	0.5	2	1	4.0	6
14	AG 2305	Citric oil rection vessol agitator	27.17	30.00	415	3	47.3	283.50	0.8	0.6	0.8	0.5	2	1	4.0	25
15	AG 2309	Lye oil reaction vessel agitator	9.89	11.00	415	3	17.2	103.20	0.8	0.6	0.8	0.5	2	1	4.0	25
16	AG 2310	Lye oil reaction vessel agitator	9.89	11.00	415	3	17.2	103.20	0.8	0.6	0.8	0.5	2	1	4.0	35
17	AG 2314	Soap Adsorbant Tank Agitator	17.30	18.50	415	3	30.1	180.51	0.8	0.6	0.8	0.5	2	1	4.0	10

S.NO.	Current Rating (A)	Derating factor k1	Derating factor k2	Derating factor k3	Derating factor k4	Overall Derating factor k	Derated Current (A)	Cable Length (M)	Cable Resistance (Ohms/kM)	Cable Reactance (Ohms/kM)	Voltage drop (Running) (V)	Voltage drop (Running) (%)	Voltage drop (Starting) (V)	Voltage drop (starting) (%)	Cable size result	OD of Cable (mm)	Gland size
3	#REF!	0.98	0.9	1	1	0.882	#REF!	95	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20
4	#REF!	0.98	0.9	1	1	0.882	#REF!	95	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
5	#REF!	0.98	0.9	1	1	0.882	#REF!	60	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
6	#REF!	0.98	0.9	1	1	0.882	#REF!	85	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
7	#REF!	0.98	0.9	1	1	0.882	#REF!	75	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
8	#REF!	0.98	0.9	1	1	0.882	#REF!	105	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
9	#REF!	0.98	0.9	1	1	0.882	#REF!	100	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
10	#REF!	0.98	0.9	1	1	0.882	#REF!	100	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
11	#REF!	0.98	0.9	1	1	0.882	#REF!	75	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20
12	#REF!	0.98	0.9	1	1	0.882	#REF!	110	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
13	#REF!	0.98	0.9	1	1	0.882	#REF!	75	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20
14	#REF!	0.98	0.9	1	1	0.882	#REF!	105	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20
15	#REF!	0.98	0.9	1	1	0.882	#REF!	85	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	32
16	#REF!	0.98	0.9	1	1	0.882	#REF!	95	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s
17	#REF!	0.98	0.9	1	1	0.882	#REF!	65	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	#REF!	20s

Basis:

1. Overall derating factor k = k1 x k2 x k3 x k4

   K1=Rating factor for variation in air/ground temperature

   K2=Rating factor for depth of laying

   K3=Rating factor for spacing between two circuits

   K4=Rating factor for variation in thermal resistivity of the soil

2. LT Motors : Running Voltage Drop = 3%, Starting Voltage Drop = 15%
3. Cable type:

   TYPE 1: Al Conductor, XLPE Insulated, Armoured, PVC outer sheathed TYPE 2:

   Cu Conductor, XLPE Insulated, Armoured, PVC outer sheathed

4. Effect of Frequency Variation ± 5%
5. Combined Effect of Voltage & Frequency Variation ±10%

Assignemnt -7

LT CABLES

CABLE TRAY: FROM	LT-4		TO	LT-5				

Sr. No.	Cable Route (From-To)	Type & Cable Size	Size of Cable (mm2)	No. of Cable	Overall Diameter of each Cable (mm)	Sum of Cable OD (mm)	Self Weight of Cable (Kg/Mt)	Total Weight of Cable (Kg/Mt)	Remarks
1	PU2315	4.0	70	1	29	**29**	3.25	**3.25**	
2	PU 2314-A	4.0	16	1	21	**21**	1	**1**	
3	PU 2314 -B	4.0	10	1	18	**18**	0.9	**0.9**	
4	PU2305	4.0	70	1	29	**29**	3.25	**3.25**	
5	MX2305	4.0	50	1	26	**26**	2.3	**2.3**	
6	MX 2308	4.0	70	1	29	**29**	3.25	**3.25**	
7	BW2313	4.0	35	1	24	**24**	1.8	**1.8**	
8	Rotary valve	4.0	4	1	17	**17**	0.6	**0.6**	
9	SC2314	4.0	6	1	18	**18**	0.7	**0.7**	
10	AG 2324A	4.0	6	1	18	**18**	0.7	**0.7**	
11	AG 2324B	4.0	6	1	18	**18**	0.7	**0.7**	
12	AG 2305	4.0	25	1	22	**22**	1.4	**1.4**	
13	AG 2309	4.0	25	1	22	**22**	1.4	**1.4**	
14	AG 2310	4.0	35	1	24	**24**	1.8	**1.8**	
15	AG 2314	4.0	10	1	18	**18**	0.9	**0.9**	
16									
17									
18									
19									
20									
21									
	Total								

Calculation

Maximum Cable Diameter:	**70**	**mm**
Consider Spare Capacity of Cable Tray:	**30%**	
Distance between each Cable:	**0**	**mm**
Calculated Width of Cable Tray:	**0**	**mm**
Calculated Area of Cable Tray:	**0**	**Sq.mm**
No of Layer of Cables in Cable Tray:	**1**	
Selected No of Cable Tray:	**1**	**Nos.**
Selected Cable Tray Width:	**600**	**mm**
Selected Cable Tray Depth:	**100**	**mm**
Selected Cable Tray Weight Capacity:	**90**	**Kg/Meter**
Type of Cable Tray:	**Ladder**	
Total Area of Cable Tray:	**60000**	**Sq.mm**

Result

Selected Cable Tray width:	**O.K**	
Selected Cable Tray Depth:	**O.K**	
Selectrd Cable Tray Weight:	**O.K**	**Including Spare Capacity**
Selected Cable Tray Size:	**O.K**	**Including Spare Capacity**
Required Cable Tray Size:	**600 x 100**	**mm**
Required Nos of Cable Tray:	**1**	**No**
Required Cable Tray Weight:	**90.00**	**Kg/Meter/Tray**
Type of Cable Tray:	**Ladder**	
Cable Tray Width Area Remaning	**100%**	
Cable Tray Area Remaning:	**100%**	