

3D Elastodynamics

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1 Model

The elastodynamic equation for the local mechanical displacement \mathbf{u} is written as

$$\rho \frac{\partial^2 u_i}{\partial t^2} + \beta \frac{\partial u_i}{\partial t} = \nabla_j \sigma_{ij} + f_i \quad (1)$$

Which can be expressed using expressions for velocities $v_i = \partial u_i / \partial t$ and stresses $\sigma_{ij} = c_{ijkl} \epsilon_{kl}$

$$\begin{cases} \rho \frac{\partial v_i}{\partial t} + \beta v_i = \nabla_j \sigma_{ij} + f_i \\ \frac{\partial \sigma_{ij}}{\partial t} = c_{ijkl} \frac{1}{2} \left(\frac{\partial v_k}{\partial t} + \frac{\partial v_l}{\partial k} \right) \end{cases} \quad (2)$$

Now we have system of nine first order DE which we will solve using leapfrog scheme[1,2,3]. Velocities and stresses are shifted in space and time in half of integrating steps di , dt . Free BC in direction normal to i $\{\sigma_{ij} = 0\}_j$ leads to

$$\begin{cases} \partial v_i / \partial i = -c_{12} / c_{11} (\partial v_j / \partial j + \partial v_k / \partial k) \\ \partial v_j / \partial i = -\partial v_i / \partial j \end{cases} \quad (3)$$

To obtain an open BC let's rewrite (2) with respect to Φ vector which is constructed as $(v_x, v_y, v_z, \sigma_{xx}, \sigma_{yy}, \sigma_{zz}, \sigma_{yz}, \sigma_{xz}, \sigma_{xy})^T$. This hyperbolic system has 9 characteristic curves along which Riemann invariants are conserved and may be inflowing or outflowing at boundaries. These invariants are widely used in mathematics to deal with hyperbolic equations.

$$\frac{\partial \Phi}{\partial t} = \beta \Phi + \sum_i A_i \frac{\partial \Phi}{\partial i} + \mathbf{f} \quad (4)$$

for example Ax has form

$$\begin{pmatrix} 0 & 0 & 0 & 1/\rho & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1/\rho \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1/\rho & 0 \\ c_{11} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ c_{12} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ c_{12} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & c_{44} & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & c_{44} & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix}. \quad (5)$$

Diagonalization of this system as in [4] leads to 9 eigenvalues λ_n and eigenvectors W_n . Riemann invariants or new characteristic variables vector has form $\phi = E^{-1} \Phi$, where E is matrix constructed from eigenvectors of matrix A_i . Now we define characteristic amplitudes as $L_n = \lambda_n \phi_n / \partial i$ where i is direction normal to open boundary. And finally set of $L_n = 0$ is open BC. These conditions take form

$$\begin{cases} \frac{\partial V_i}{\partial i} = \pm \frac{1}{\sqrt{c_{11}\rho}} \frac{\sigma_{ii}}{\partial i} \\ \frac{\partial V_j}{\partial i} = \pm \frac{1}{\sqrt{c_{44}\rho}} \frac{\sigma_{ij}}{\partial i} \end{cases} \quad (6)$$

Here sign \pm denotes to right and left boundaries.

2 Results

2.1 Poisson's coefficient

First of all let's simulate a compression of CoFe cube with cell numbers $l_x = l_y = l_z = 80$ and cell sizes $dx = dy = dz = 3$ nm. We apply constant f_z at upper surface $z = l_z$ of cube and fix $v_z = 0$ at lower surface $z = 0$ and let all the rest boundaries be free. Stationary spatial distributions of strains at layer number $l_z/2$ are shown on fig.1.

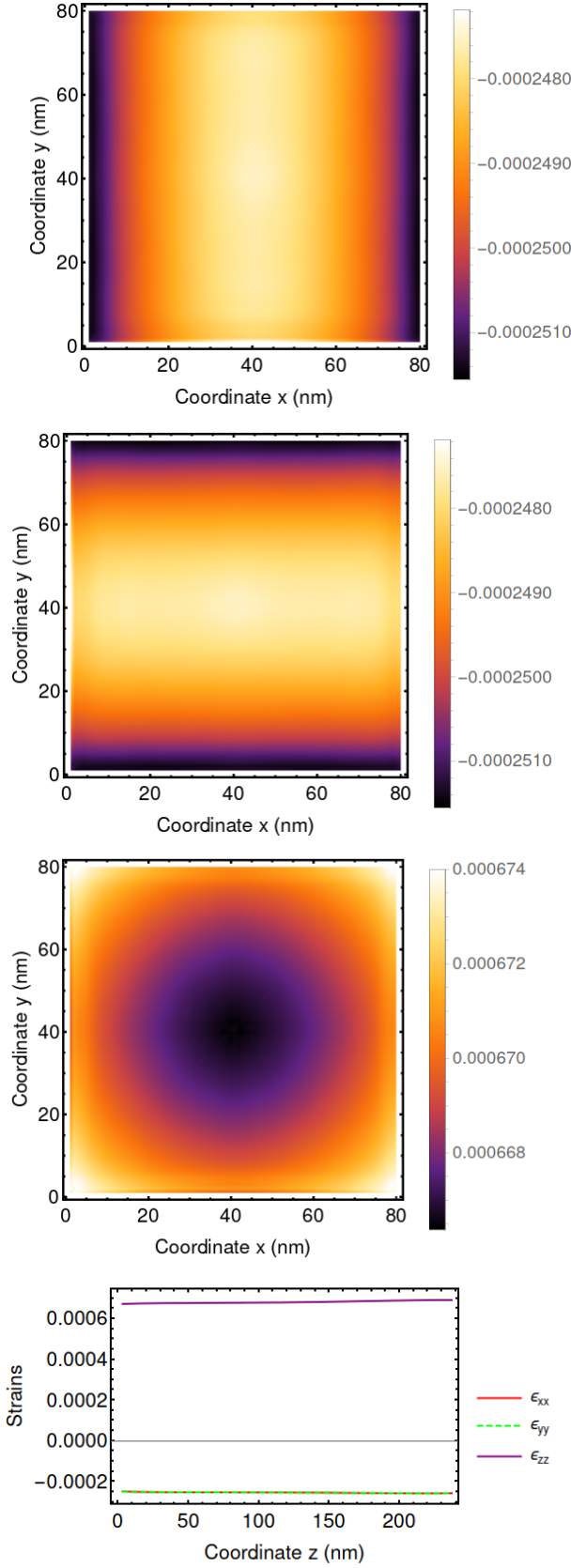


Fig. 1 $\epsilon_{xx}(x, y)$, $\epsilon_{yy}(x, y)$, $\epsilon_{zz}(x, y)$, $\epsilon_{xx,yy,zz}(z)$

Analytical Poisson's coefficient $c_{12}/(c_{11} + c_{12})$ and resulting $\epsilon_{xx}/\epsilon_{zz}$ at point $(l_x/2, l_y/2, l_z/2)$ are -0.372133 and -0.372881 respectively.

2.2 Isotropic inplane strains

Now let's consider a case when we have an applied inplane stretching forces f_x and f_y at bottom ($z = 0$) of CoFe film with geometry $l_x = l_y = 100$, $l_z = 2$, $dx = dy = 3$ nm, $dz = 1.5$ nm. Forces are calculated as $f_i = \sigma_{ii}^{ext}/\Delta i$ with chosen external strains $\epsilon_{xx}^{ext} = \epsilon_{yy}^{ext} = 1\%$ and Δi is a computational cell size. All directions of the plotted strain functions intersect at the point $(l_x/2, l_y/2, l_z/2)$. The results are shown on fig 2.

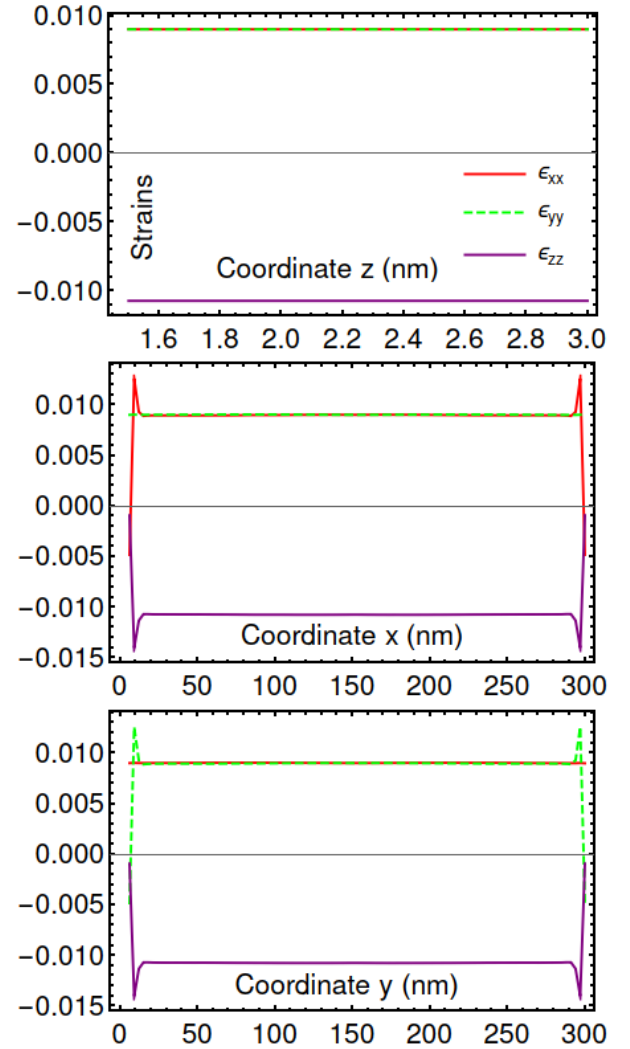


Fig. 2 $\epsilon(x, y, z)$ $l_x = l_y = 100$, $l_z = 2$, $dx = dy = 3$ nm, $dz = 1.5$ nm

Now let's consider a geometry $l_x = l_y = 100$, $l_z = 20$, $dx = dy = 3$ nm, $dz = 1.5$ nm. The results are shown on fig 3.

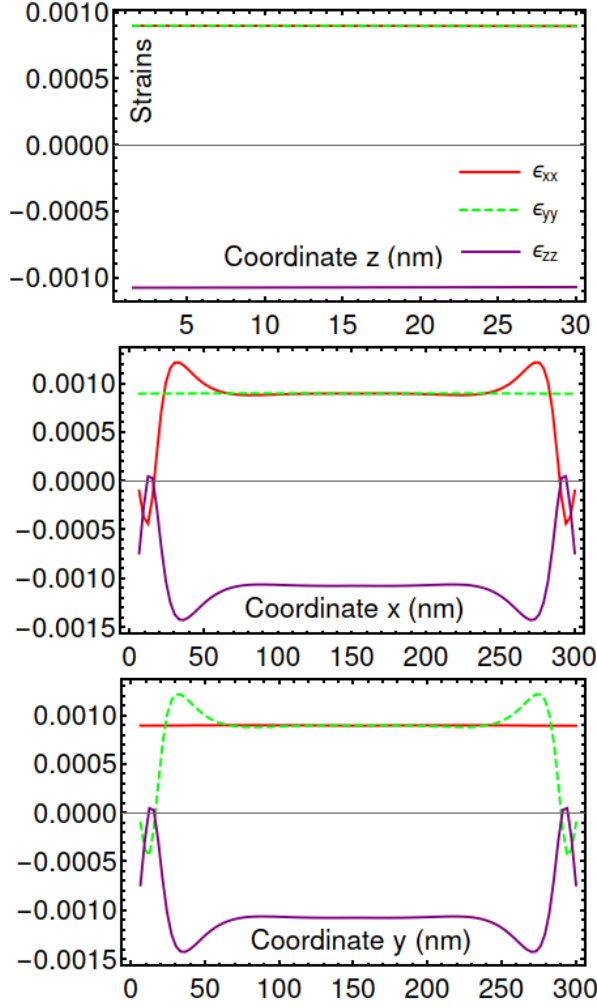


Fig. 3 $\epsilon(x, y, z)$ $l_x = l_y = 100$, $l_z = 20$, $dx = dy = 3$ nm, $dz = 1.5$ nm

Simulation with elongated shape CoFe crystal with $l_x = l_y = 10$, $l_z = 200$, $dx = dy = dz = 3$ nm. Fig 4 illustrates the result.

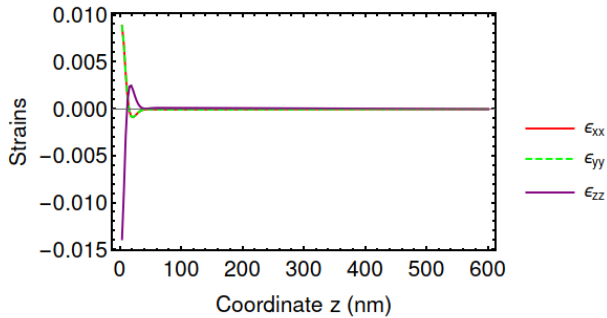


Fig. 4 $\epsilon(z)$ $l_x = l_y = 10$, $l_z = 200$, $dx = dy = dz = 3$ nm

Let's see what happens if we apply isotropic inplane strains at MgO-CoFe-Pt structure with $l_x = l_y = 100$, $l_z = 21$, $dx = dy = 3$ nm, $dz = 0.5$ nm.

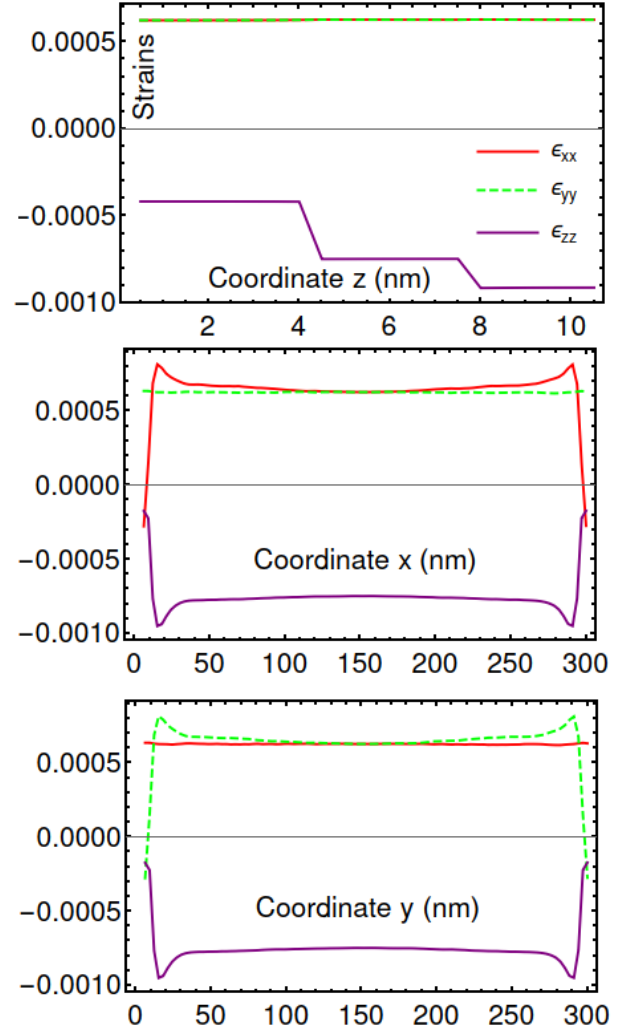


Fig. 5 MgO-CoFe-Pt structure

2.3 Dynamics

In order to check absolute absorption condition and relation of amplitudes of waves passing the interface between different materials we apply a time-dependent values of stresses at $z = 0$:

$$\begin{cases} \sigma_{xx} = \sigma_{yy} = c_{12}\epsilon_{zz} \sin 2\pi\nu t \\ \sigma_{zz} = c_{11}\epsilon_{zz} \sin 2\pi\nu t \\ \sigma_{xy} = \sigma_{xz} = \sigma_{yz} = 0 \end{cases} \quad (7)$$

These conditions allow us to simulate a longitudinal waves with constant wave front in xy plane. Layer number $z = l_z/2$ is interface, where region $z \leq l_z/2$ is MgO and $z > l_z/2$ is CoFe crystal. We apply an open BC at $z = l_z$ surface and free BC to all the rest

surfaces of 3-dimensional waveguide with $l_x = l_y = 10$, $l_z = 800$, $dx = dy = dz = 5$ nm. Fig 6 shows the results obtained with simulation using $dt = 10^{-15}$ s and applied frequency is 10 GHz. Wave lengths of MgO and CoFe are 886 and 558 nm.

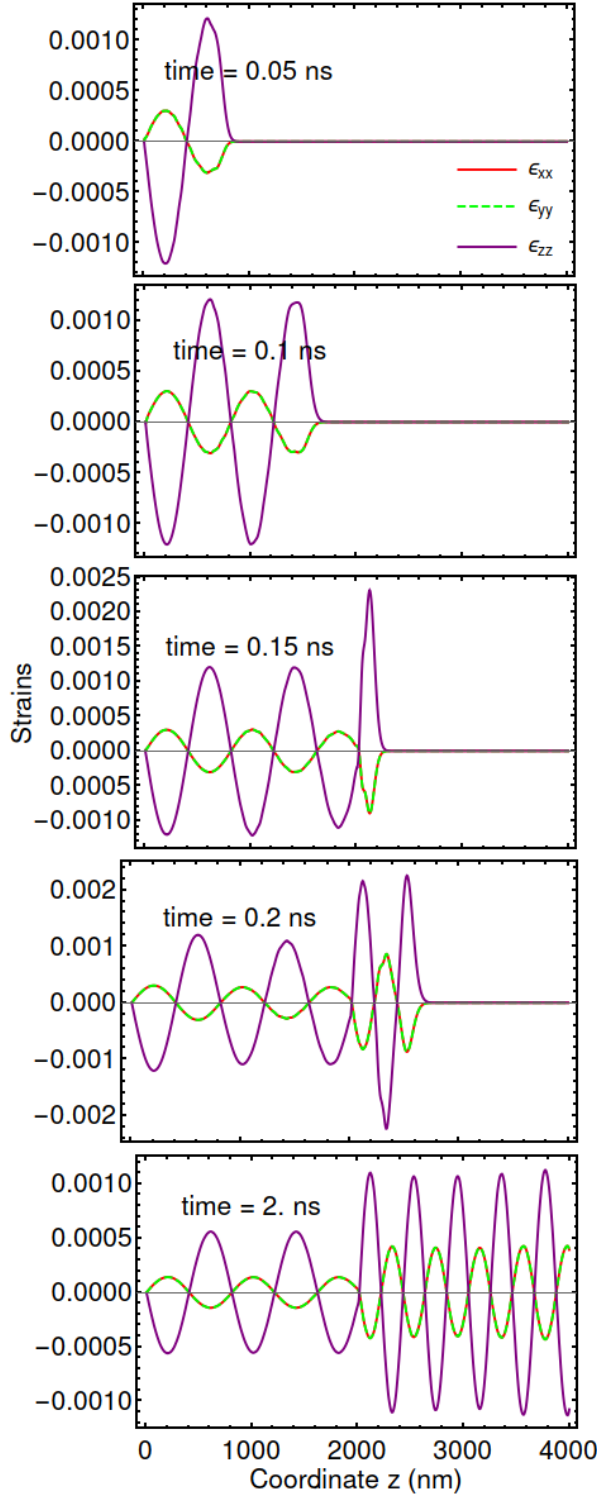


Fig. 6 MgO-CoFe weveguide time series.

Spatial distributions of \mathbf{u} along z axis are shown on fig. 7. Analytical value of ratio of misfits is $u_{CoFe}/u_{MgO} = Z_{MgO}/(Z_{MgO} + Z_{CoFe}) = 0.798$, where Z equals wave velocity times mass density. Numerical value of $u_{CoFe}/u_{MgO} = 0.815$.

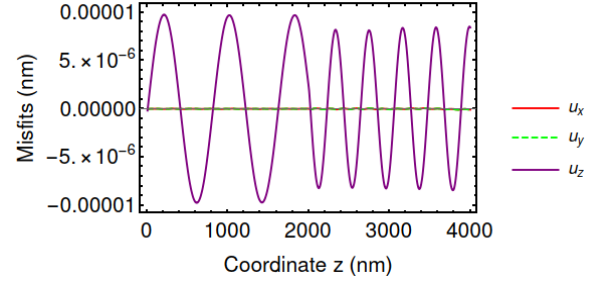


Fig. 7 MgO-CoFe weveguide misfits amplitudes.

2.4 Impulse reflection from MgO-CoFe interface

Finally let's consider a structure with geometry from 2.3 but now we will generate an impulse at $z = 0$ boundary. In order to study \mathbf{u} reflected from interface open BC will be applied at all other surfaces. This is a semi infinite crystal case and we expect \mathbf{u} to be distributed uniformly in xy plane. Impulse has form

$$\begin{cases} \epsilon_{zz} = 0.001 & t \leq 0.01ns \\ \epsilon_{zz} = 0 & t > 0.01ns \end{cases}$$

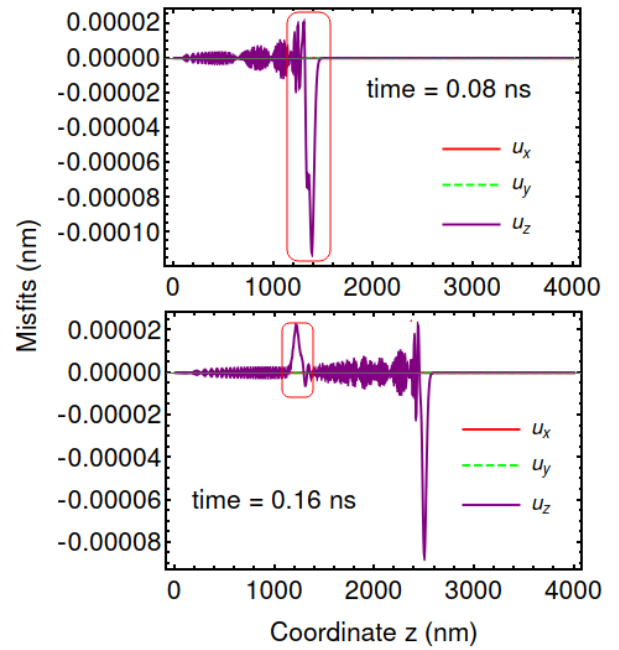


Fig. 8 MgO-CoFe infinite crystal misfits amplitudes.

Ratio of primary and reflected amplitudes $(Z_{MgO} - Z_{CoFe}) / (Z_{MgO} + Z_{CoFe}) = -0.2$. And numerical value of ratio is -0.2, what can be seen from time series shown on fig 8.

References

- [1] C. T. Schroder, W. R. Scott and G. D. Larson, "Elastic waves interacting with buried land mines: a study using the FDTD method," in IEEE Transactions on Geoscience and Remote Sensing, vol. 40, no. 6, pp. 1405-1415, June 2002, doi: 10.1109/TGRS.2002.800435.
- [2] Ursula Iturrarán-Viveros and Miguel Molero-Armenta 2015 Comput. Sci. Discov. 8 014006
- [3] D.C. Calvo and K.E. Rudd and M. Zampolli and W.M. Sanders and L.D. Bibee "Simulation of acoustic scattering from an aluminum cylinder near a rough interface using the elastodynamic finite integration technique", Wave Motion,2010,0165-2125,<https://doi.org/10.1016/j.wavemoti.2010.05.002>
- [4] <https://hal.inria.fr/inria-00134856/document>