

# Other Bias Methods

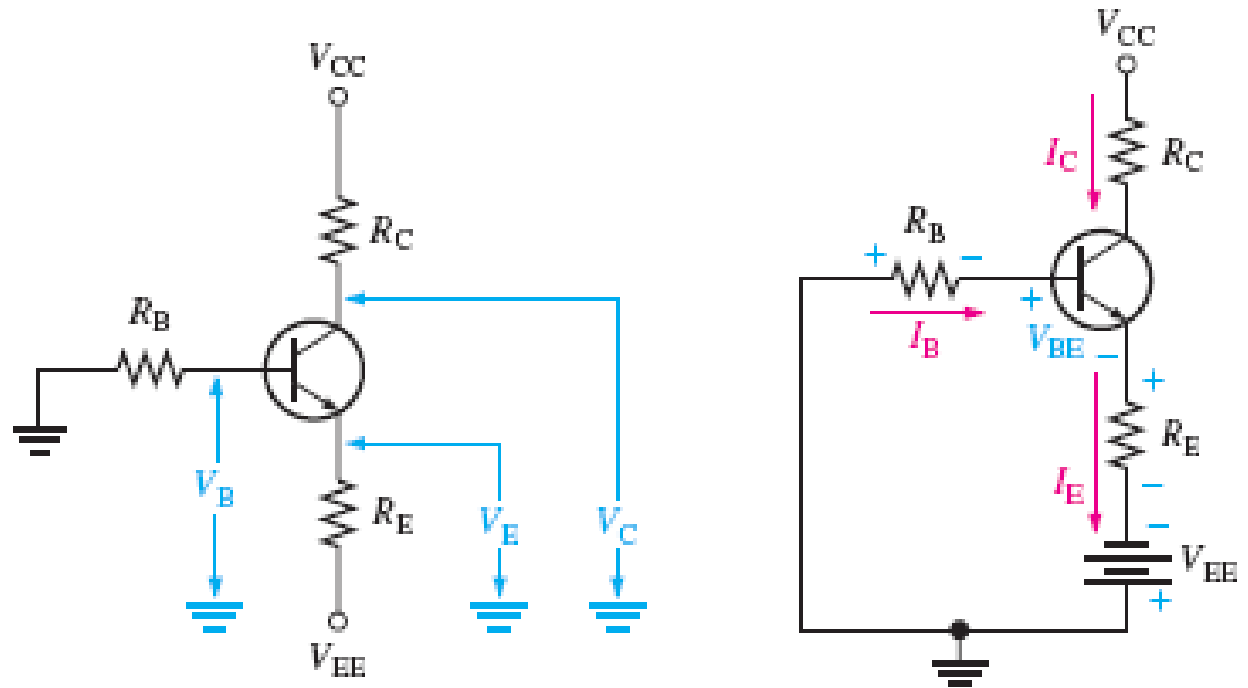
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## Other Bias Methods

### Emitter Bias



Emitter bias provides excellent bias stability in spite of changes in  $\beta$  or temperatures.

$$V_{EE} + V_{R_B} + V_{BE} + V_{R_E} = 0$$

Substituting, using Ohm's law,

$$V_{EE} + I_B R_B + V_{BE} + I_E R_E = 0$$

Substituting for  $I_B \cong I_E / \beta_{DC}$  and transposing  $V_{EE}$ ,

$$\left( \frac{I_E}{\beta_{DC}} \right) R_B + I_E R_E + V_{BE} = -V_{EE}$$

Factoring out  $I_E$  and solving for  $I_E$ ,

$$I_E = \frac{-V_{EE} - V_{BE}}{R_E + R_B / \beta_{DC}}$$

Voltages with respect to ground are indicated by a single subscript. The emitter voltage with respect to ground is

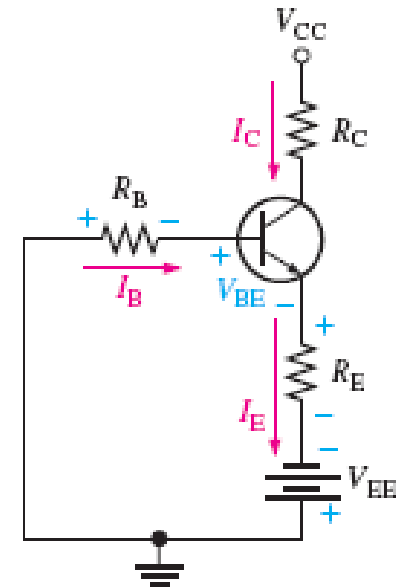
$$V_E = V_{EE} + I_E R_E$$

The base voltage with respect to ground is

$$V_B = V_E + V_{BE}$$

The collector voltage with respect to ground is

$$V_C = V_{CC} - I_C R_C$$



## Base Bias

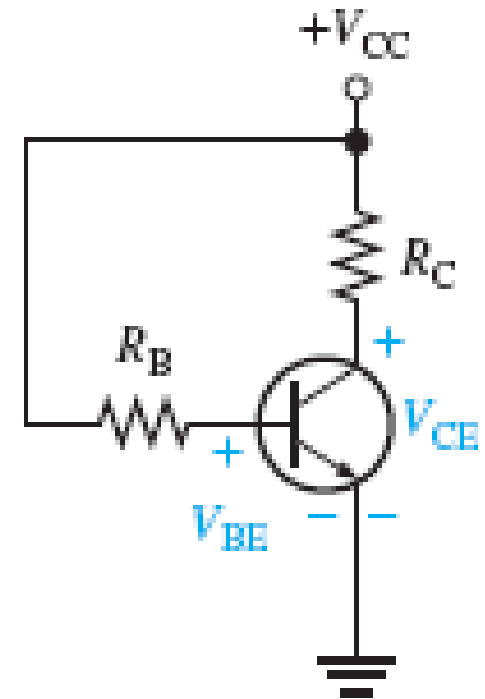
$$V_{CC} - V_{R_B} - V_{BE} = 0$$

Substituting  $I_B R_B$  for  $V_{R_B}$ , you get

$$V_{CC} - I_B R_B - V_{BE} = 0$$

Then solving for  $I_B$ ,

$$I_B = \frac{V_{CC} - V_{BE}}{R_B}$$



$$V_{CC} - I_C R_C - V_{CE} = 0$$

Solving for  $V_{CE}$ ,

$$V_{CE} = V_{CC} - I_C R_C$$

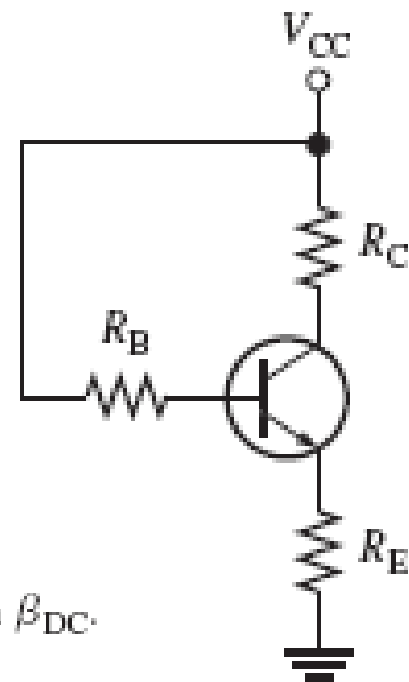
Substituting the expression for  $I_B$  into the formula  $I_C = \beta_{DC} I_B$  yields

$$I_C = \beta_{DC} \left( \frac{V_{CC} - V_{BE}}{R_B} \right)$$

**Q-Point Stability of Base Bias** Notice that Equation 5-11 shows that  $I_C$  is dependent on  $\beta_{DC}$ . The disadvantage of this is that a variation in  $\beta_{DC}$  causes  $I_C$  and, as a result,  $V_{CE}$  to change, thus changing the Q-point of the transistor. This makes the base bias circuit extremely beta-dependent and unpredictable.

Recall that  $\beta_{DC}$  varies with temperature and collector current. In addition, there is a large spread of  $\beta_{DC}$  values from one transistor to another of the same type due to manufacturing variations. For these reasons, base bias is rarely used in linear circuits but is discussed here so you will be familiar with it.

## Emitter Feedback Bias



$$-V_{CC} + I_B R_B + V_{BE} + I_E R_E = 0$$

Substituting  $I_E/\beta_{DC}$  for  $I_B$ , you can see that  $I_E$  is still dependent on  $\beta_{DC}$ .

$$I_E = \frac{V_{CC} - V_{BE}}{R_E + R_B/\beta_{DC}}$$

## Collector Feedback Bias

**Analysis of a Collector-Feedback Bias Circuit** By Ohm's law, the base current can be expressed as

$$I_B = \frac{V_C - V_{BE}}{R_B}$$

Let's assume that  $I_C \gg I_B$ . The collector voltage is

$$V_C \cong V_{CC} - I_C R_C$$

Also,

$$I_B = \frac{I_C}{\beta_{DC}}$$

Substituting for  $V_C$  in the equation  $I_B = (V_C - V_{BE})/R_B$ ,

$$\frac{I_C}{\beta_{DC}} = \frac{V_{CC} - I_C R_C - V_{BE}}{R_B}$$

The terms can be arranged so that

$$\frac{I_C R_B}{\beta_{DC}} + I_C R_C = V_{CC} - V_{BE}$$

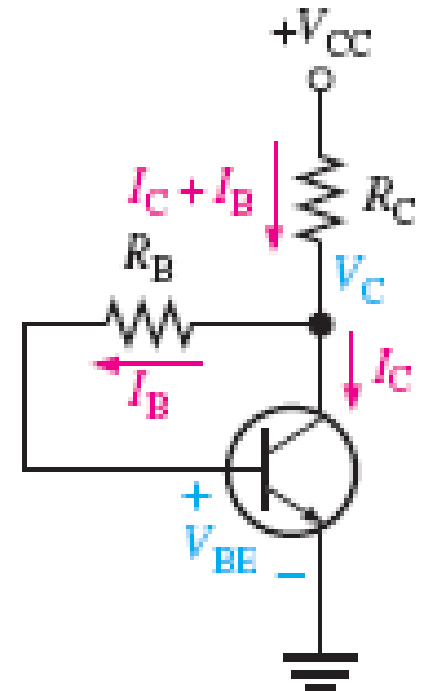
Then you can solve for  $I_C$  as follows:

$$I_C \left( R_C + \frac{R_B}{\beta_{DC}} \right) = V_{CC} - V_{BE}$$

$$I_C = \frac{V_{CC} - V_{BE}}{R_C + R_B/\beta_{DC}}$$

Since the emitter is ground,  $V_{CE} = V_C$ .

$$V_{CE} = V_{CC} - I_C R_C$$



***Q-Point Stability Over Temperature*** Equation 5–13 shows that the collector current is dependent to some extent on  $\beta_{DC}$  and  $V_{BE}$ . This dependency, of course, can be minimized by making  $R_C \gg R_B/\beta_{DC}$  and  $V_{CC} \gg V_{BE}$ . An important feature of collector-feedback bias is that it essentially eliminates the  $\beta_{DC}$  and  $V_{BE}$  dependency even if the stated conditions are met.