

Cooperative effects in motor-driven cargo transport

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Overview

- 1 Introduction
 - Motivation
 - The mean-field model by Li et al.
 - Discussion

- 2 The explicit model
 - Adjustments and comparison to the mean-field model
 - Analysis of the transport process

- 3 Summary

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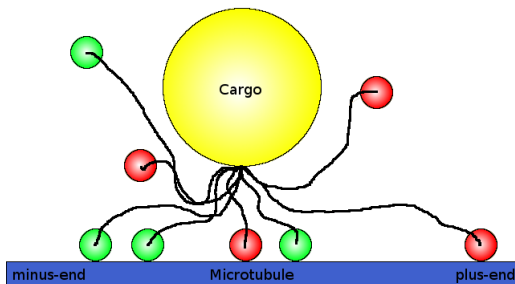
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Intracellular Cargo Transport

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- Bi- and unidirectional transport subject of much research
- Different attempts of modeling these kinds of transport
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The model

- One slow and one fast team of kinesins pulling the cargo
- N_f and N_s motors available, n_f and n_s numbers of bound motors
- Force independent binding rates π_{0s} and π_{0f}
- Force dependent unbinding rates

$$\epsilon(F) = \epsilon_0 \exp\left(\frac{F}{F_d}\right)$$

- Force dependent velocities

$$\begin{aligned} V_s(F) &= v_s (1 - F/F_{ss}) & \text{for } F \leq 0 < F_{ss} \\ V_f(F) &= v_f (1 - F/F_{sf}) & \text{for } 0 \leq F < F_{sf}, \end{aligned}$$

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$$n_f F_+ = -n_s F_- \equiv F(n_f, n_s),$$

- Assumption of equal velocities of all motors

$$V_s(F_-) = V_f(F_+) = v(n_f, n_s),$$

- These lead to the transport velocity

$$v(n_f, n_s) = \frac{V_s V_f}{\left(1 - \frac{n_f}{n}\right) v_f + \frac{n_f}{n} v_s},$$

uniquely determined by the numbers n_f and n_s

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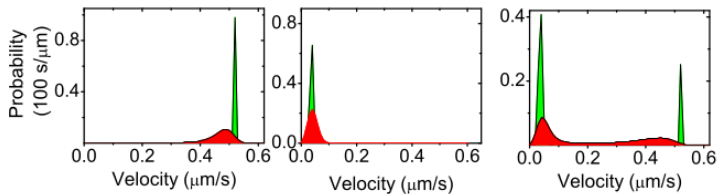
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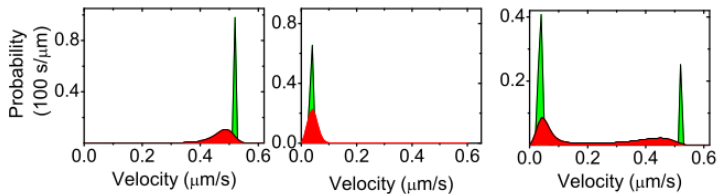
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- => the system of motors and cargo is always stepping as a complete unit
- -> unrealistic scenario

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Idea

- Introducing a new model which takes the explicit motor positions into account
- Comparing the results of this explicit model to the results of the mean-field model

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Adjustments

- Stalks of the motors modeled as cable-like Hookean springs: slack up to a length of L_0 and linear force relation beyond L_0 . The force of the i -th motor on the cargo reads

$$F_i = \begin{cases} \alpha (x_i(t) - x_C(t) + L_0), & x_i(t) - x_C(t) < -L_0, \\ 0, & |x_i(t) - x_C(t)| < L_0, \\ \alpha (x_i(t) - x_C(t) - L_0), & x_i(t) - x_C(t) > L_0. \end{cases}$$

- Stepping rates for each motor

$$s_s(F_i) = \begin{cases} \frac{v_s}{d}, & F_i < 0, \\ \frac{v_s}{d} \left[1 - \frac{F_i}{F_{ss}} \right], & 0 \leq F_i \leq F_{ss}, \\ \frac{v_s^B}{d}, & F_i > F_{ss} \end{cases}$$

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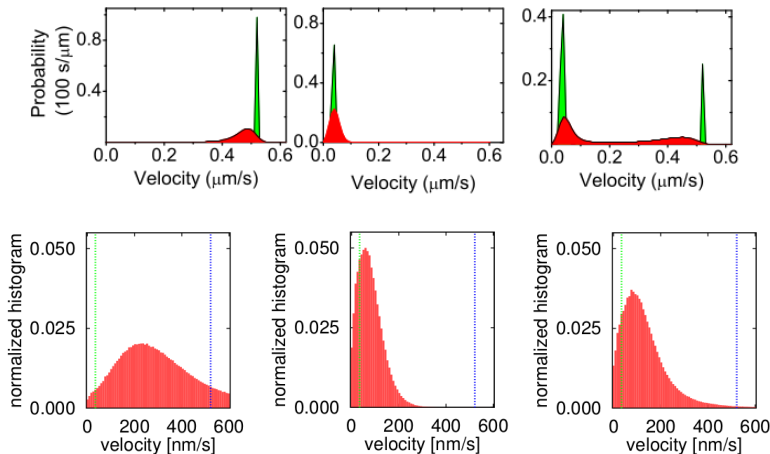
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Comparison to results of Li *et al.*



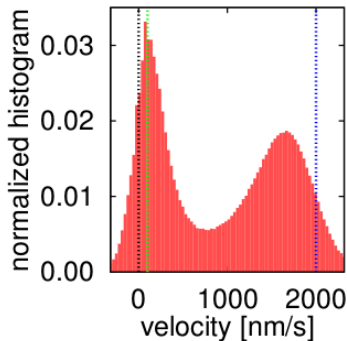
- Different results for same sets of parameters!

Bimodal velocity distributions?

- Are bimodal velocity distributions possible in the explicit model?
- Yes they are, but with different sets of parameters!

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A closer look at the motor parameters

- In order to understand the underlying effects, which lead to the shown bimodal velocity distribution, changes to the following parameters have been examined:
 - Slow and fast velocities v_s and v_f
 - Attachment rate κ_a
 - Stall forces F_{ss} and F_{sf}
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Velocities, attachment rate and stall forces

- Bimodal velocities: $v_s = 100 \frac{\text{nm}}{\text{s}}$, $v_f = 2000 \frac{\text{nm}}{\text{s}}$
Increasing the velocity of slow motors leads to a vanishing distinctness of the bimodal velocity distribution
- Bimodal attachment rate: $\kappa_a = 5 \text{ s}^{-1}$
For very low attachment rates ($< 0.1 \text{ s}^{-1}$) transport is stalling most of the time and is carried out by only one attached motor at a time. Very high attachment rates ($> 100 \text{ s}^{-1}$) lead to unimodal velocity distributions, as all motors are involved into transport.
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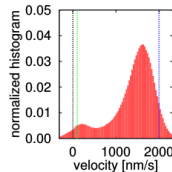
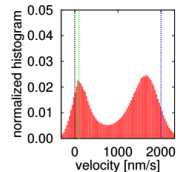
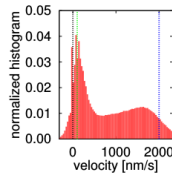
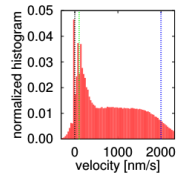
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Force free detachment rate

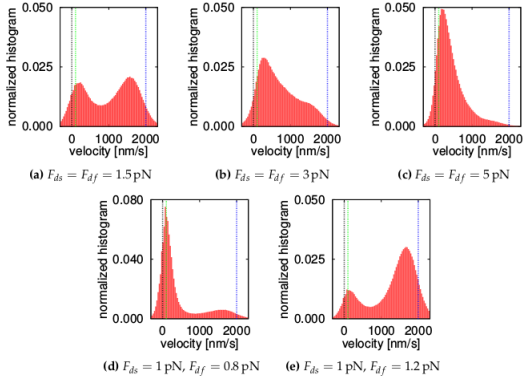
- Bimodal force free detachment rate: $\kappa_d^0 = 1 \text{ s}^{-1}$
- Reminder: $\kappa_d(F_i) = \kappa_d^0 \exp\left(\frac{|F_i|}{F_d}\right)$

- Bimodal for roughly
 $0.1 \text{ s}^{-1} \leq \kappa_d^0 \leq 5 \text{ s}^{-1}$

(a) $\kappa_d^0 = 0.1 \text{ s}^{-1}$ (b) $\kappa_d^0 = 0.5 \text{ s}^{-1}$ (c) $\kappa_d^0 = 5 \text{ s}^{-1}$ (d) $\kappa_d^0 = 10 \text{ s}^{-1}$

Detachment forces

- Bimodal detachment forces: $F_d = 1$ pN
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Summary of the parameter analysis

In order to obtain bimodal velocity distribution one needs:

- $F_{sf} > F_d$
- Only few motors must participate in cargo transport simultaneously
- Detachment forces of fast and slow motors need to be “close”
- A considerable gap between slow and fast motor's velocities

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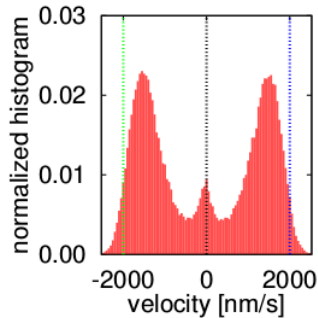
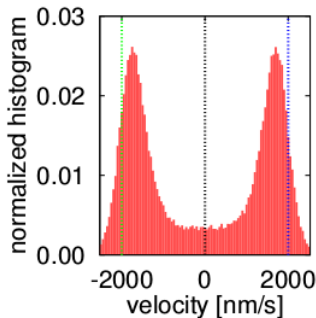
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Extension on bidirectional case

- Bi- and even trimodal velocity distributions obtainable for symmetric motors.



Summary

- Bimodal motility states have been obtained by Li *et al.* using the mean field model.
- These bimodal states cannot be reproduced by an explicit model for the same set of parameters but for different sets of parameters.
- The explicit model can be extended on the bidirectional case and, there, leads to bimodal and even trimodal motility states.
- Further improvements:
 - A different modeling approach for the detachment rate could be examined, as the exponential modeling heavily effects the motility state.

Thank you for your attention!

References I



X. Li, R. Lipowsky, and J. Kierfeld.

Bifurcation of Velocity Distributions in Cooperative Transport of Filaments by Fast and Slow Motors.

Biophysical Journal, vol. 104, pp. 666–676, 2013.

Li *et al.* parameters

Parameters used by Li *et al.* for the three different motility regimes

	Larson <i>et al.</i> [2]	Pan <i>et al.</i> [4]	Bieling <i>et al.</i> [3]
Fast motors			
Wild kinesin-I	OSM-3	Xklp1	
Slow motors			
Parameter	Mutant kinesin-I	Kinesin-II	Xkid
Binding rate, fast π_{0f}	5 s^{-1}	5 s^{-1}	5 s^{-1}
Binding rate, slow π_{0s}	5 s^{-1}	5 s^{-1}	5 s^{-1}
Unbinding rate, fast ϵ_{0f}	1 s^{-1}	1 s^{-1}	1 s^{-1}
Unbinding rate, slow ϵ_{0s}	1 s^{-1}	1 s^{-1}	1 s^{-1}
Detachment force, fast F_{df}	3 pN	6 pN*	6 pN*
Detachment force ratio $\eta \equiv \frac{F_{ds}}{F_{df}}$	0.45	3.3*	1.9*
Stall force, fast F_{sf}	6 pN	6 pN	6 pN
Stall force, slow F_{ss}	6 pN	6 pN	6 pN
Zero load velocity, fast v_f	$0.522 \mu\text{m s}^{-1}$	$1.09 \mu\text{m s}^{-1}$	$1.0 \mu\text{m s}^{-1}$
Zero load velocity, slow v_s	$0.034 \mu\text{m s}^{-1}$	$0.34 \mu\text{m s}^{-1}$	$0.1 \mu\text{m s}^{-1}$
$\hat{\pi} \equiv \frac{\pi_{0f}}{\epsilon_{0f}} = \frac{\pi_{0s}}{\epsilon_{0s}}$	5	5	5
$\hat{F} \equiv \frac{F_s}{F_{df}}$	2	1	1
$\hat{v} \equiv \frac{v_s}{v_f}$	0.065	0.31	0.1

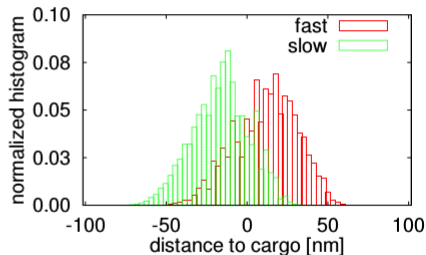
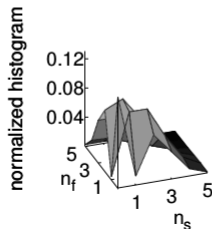
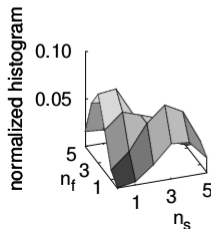
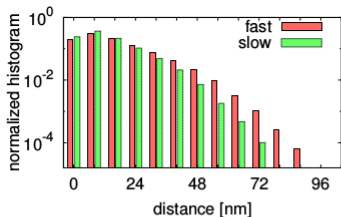
Parameters used for the explicit model simulation for the bistable motility regime

System parameters		
Simulation time t_{end}	100 000 s	
Velocity measurement interval Δt	0.1 s	
Motor parameters		
Parameter	Slow	Fast
Number of available motors N	8	2
Stalk length L_0 (*)	10 nm	10 nm
Stepsize d (*)	8 nm	8 nm
Stiffness constant α (*)	$10^{-4} \frac{\text{kg}}{\text{s}^2}$	$10^{-4} \frac{\text{kg}}{\text{s}^2}$
Detachment force F_d	1.35 pN	3 pN
Stall force F_s	6 pN	6 pN
Force free detachment rate κ_d^0	1 s^{-1}	1 s^{-1}
Attachment rate κ_a	5 s^{-1}	5 s^{-1}
Velocity forward v^F	$34 \frac{\text{nm}}{\text{s}}$	$522 \frac{\text{nm}}{\text{s}}$
Velocity backward v^B (*)	$6 \frac{\text{nm}}{\text{s}}$	$6 \frac{\text{nm}}{\text{s}}$

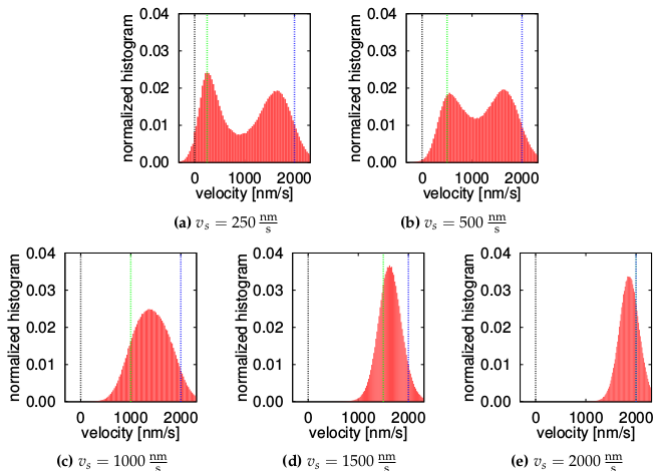
Changes to parameters to obtain bimodal velocity distribution

Motor parameters		
Parameter	Slow	Fast
Number of available motors N	5	5
Detachment force F_d	1 pN	1 pN
Stall force F_s	5 pN	5 pN
Velocity forward v^F	$100 \frac{\text{nm}}{\text{s}}$	$2000 \frac{\text{nm}}{\text{s}}$

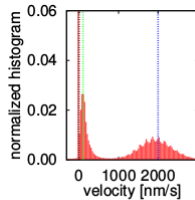
Different transport characteristics to the shown bimodal case



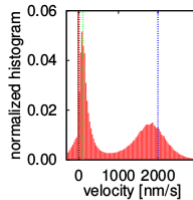
Simulations for differing slow motor velocities



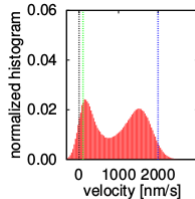
Simulations for differing attachment rates



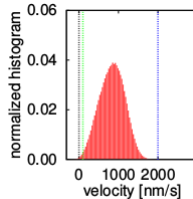
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(b) $\kappa_d = 1.0 \text{ s}^{-1}$

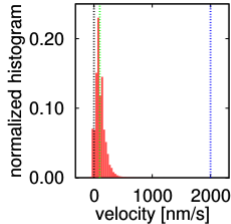


(c) $\kappa_d = 10.0 \text{ s}^{-1}$

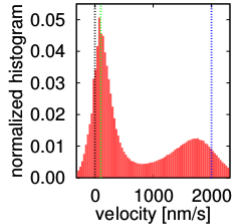


(d) $\kappa_d = 100.0 \text{ s}^{-1}$

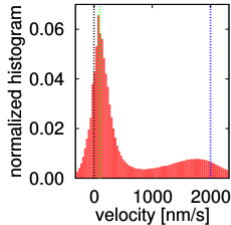
Simulations for differing stall forces of fast motors



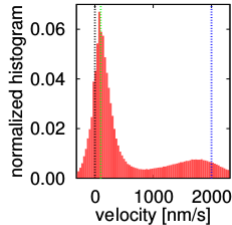
(a) $F_{sf} = 0.1$ pN and $F_{ss} = 5$ pN



(b) $F_{sf} = 10$ pN and $F_{ss} = 5$ pN



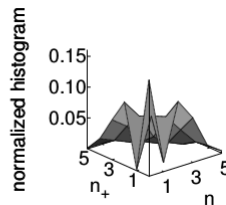
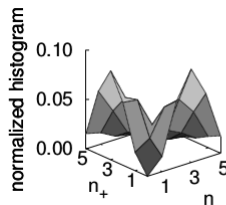
(c) $F_{sf} = 100$ pN and $F_{ss} = 5$ pN



(d) $F_{sf} = 1000$ pN and $F_{ss} = 5$ pN

Motor distributions in the bidirectional case

Bidirectional bimodal velocity distribution: motors attached, motors with $|F| > 0$



Bidirectional trimodal velocity distribution: motors attached, motors with $|F| > 0$

