Sveučilište u Rijeci

## TEHNIČKI FAKULTET

Sveučilišni preddiplomski studij elektrotehnike



Električna postrojenja Konstrukcijski zadatak

> Denis Mijolović 0069066432

# 1. ZADATAK I PODACI ELEMENATA MREŽE

Zadatak broj: 31

Za elektroenergetski sustav zadan shemom i podacima u priloženim tablicama ( transformator T8 je van pogona) potrebno je za slučaj 2pz kratkog spoja na sabirnici 11, izračunati:

- 1. Strujne i naponske prilike na mjestu kratkog spoja,
- 2. Udio pojedinih izvora u struji kratkog spoja,

Tablica 1, Podaci o generatorima

| Generatori | U <sub>n</sub> (kV) | $\cos  ho_n$ | S <sub>n</sub> (MVA) | $X_d^{\prime\prime}$ % | X <sub>d</sub> % | X <sub>i</sub> % | $R_{ m g}\Omega$ | uzemljenje |
|------------|---------------------|--------------|----------------------|------------------------|------------------|------------------|------------------|------------|
| G1         | 20                  | 0,85         | 150                  | 14                     | 180              | 14               | 0,002            |            |
| G2         | 10                  | 0,9          | 100                  | 16                     | 200              | 16               | 0,005            | •••        |
| G3         | 10                  | 0,8          | 10                   | 10                     | 180              | 10               | 0,018            |            |

Tablica 2, Podaci o dvonamotnim transformatorima

|        |             |                 |           | 1         |           |           |         | 1          |          |
|--------|-------------|-----------------|-----------|-----------|-----------|-----------|---------|------------|----------|
|        | $S_n (MVA)$ | $U_{n1}/U_{n2}$ | $u_k(\%)$ | $u_r(\%)$ | $R_0/R_d$ | $X_0/X_d$ | Grupa   | uzemljenje |          |
|        |             |                 |           |           |           |           | spoja   |            |          |
|        |             |                 |           |           |           |           | spoju   | primar     | sekundar |
|        |             |                 |           |           |           |           |         | primar     | Sekundar |
| TD:1   | 150         | 110/20          | 1.6       | 0.5       | 1         | 0.05      | XD 1 15 | :22        |          |
| T1     | 150         | 110/20          | 16        | 0,5       | 1         | 0,95      | YNd5    | j22        | •••      |
|        |             |                 |           |           |           |           |         |            |          |
| T2     | 100         | 110/10          | 12        | 0,5       | 1         | 1         | Yd5     |            | ,,,      |
|        |             |                 |           |           |           |           |         |            |          |
| T5     | 31,5        | 110/10          | 12        | 0,5       | 1         | 1         | Yy0     |            |          |
| 13     | 31,3        | 110/10          | 12        | 0,5       | 1         | 1         | 1 y0    | • • • •    | •••      |
| - TO 6 | 21.7        | 440/40          | 10        | 0.7       |           |           | ** 0    |            | 0.0      |
| T6     | 31,5        | 110/10          | 12        | 0,5       | 1         | 1         | Yyn0    | •••        | 80       |
|        |             |                 |           |           |           |           |         |            |          |
| T7     | 1           | 10/0,4          | 5         | 1,03      | 1         | 1         | Dyn5    |            | kruto    |
|        |             | ĺ               |           |           |           |           | •       |            |          |
| Т8     | 0,63        | 10/0,4          | 4,4       | 0,9       | 1         | 1         | Dyn5    |            | kruto    |
| 10     | 0,03        | 10/0,4          | 7,4       | 0,9       | 1         | 1         | Dyns    | • • • •    | Kiuto    |
|        |             |                 |           |           |           |           |         |            |          |

Tablica 3, Podaci o tronamotnim transformatorima

|    |                              | ,                           |  |  | -                             |        |        |          |          |
|----|------------------------------|-----------------------------|--|--|-------------------------------|--------|--------|----------|----------|
|    | $S_{n1}/S_{n2}/S_{n3}$ (MVA) | $U_{n1}/U_{n2}/U_{n3}$ (kV) | u <sub>k12</sub> /u <sub>k13</sub> /u <sub>k23</sub> (%) | u <sub>k012</sub> /u <sub>k013</sub> /u <sub>k02</sub> 3 (%) | $u_{r12}/u_{r13}/u_{r23}$ (%) | Grupa  | uze    | emljenje |          |
|    |                              |                             |  |  |                               | spoja  | primar | sekundar | tercijar |
| Т3 | 350/350/50                   | 380/110/30                  | 21/10/7  | 19,12/9,51/6,3   | 0,26/0,16/0,16                | Yyn0d5 |        | kruto    |          |
| T4 | 350/350/50                   | 380/110/30                  | 21/10/7  | 19,12/9,51/6,3   | 0,26/0,16/0,16                | YNy0d5 | kruto  |          |          |

Tablica 4, Podaci o zračnim vodovima (dalekovodima)

| Vod       | U (kV) | Duljina (km) | $Z_{dv}\left(\Omega/km ight)$ | $Z_{0v}\left(\Omega/km\right)$ |
|-----------|--------|--------------|-------------------------------|--------------------------------|
| ZV1, ZV1a | 110    | 20           | 0,12 + j0,39                  | 0,32 + j1,26                   |
| ZV2       | 110    | 10           | 0,12+j0,39                    | 0,32 + j1,26                   |
| ZV3       | 110    | 15           | 0,12 + j0,386                 | 0,22 + j1,1                    |

## Tablica 5, Podaci o kabelima

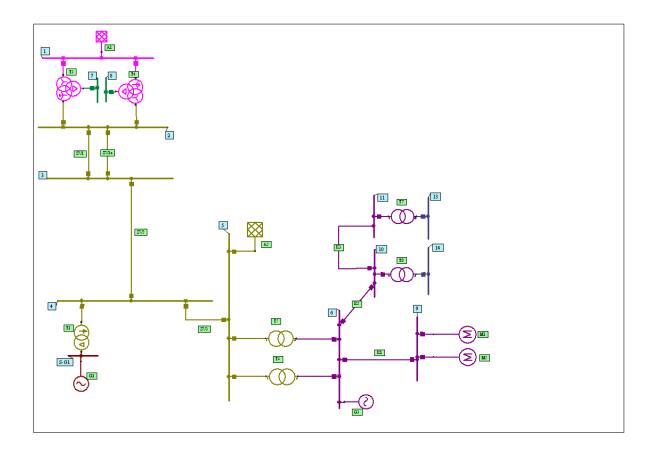
|    | U (kV) | Duljina (km) | $Z_{dv}\left(\Omega/km\right)$ | $Z_{0v}\left(\Omega/km\right)$ |
|----|--------|--------------|--------------------------------|--------------------------------|
| K1 | 10     | 1            | 0,253 + j0,107                 | 0,9361 + j0,963                |
| K2 | 10     | 7            | 0,253 + j0,095                 | 1,606 + j1,1875                |
| К3 | 10     | 5,5          | 0,253 + j0,107                 | 0,9361 + j0,963                |

## Tablica 6, Podaci o aktivnim mrežama

|    | U (kV) | $R_d/X_d$ | $R_0/X_0$ | $X_0/X_d$ | $S_{k3}^{\prime\prime}$ (MVA) |
|----|--------|-----------|-----------|-----------|-------------------------------|
| A1 | 380    | 0,1       | 0,15      | 3         | 25011                         |
| A2 | 110    | 0,1       | 0,2       | 3,3       | 3048,4                        |

# Tablica 7, Podaci o motorima

|    | U (kV) | P (MW) | p | $\cos  ho_n$ | $\eta_n$ | $I_p/I_n$ | $R\left(\Omega\right)$ |
|----|--------|--------|---|--------------|----------|-----------|------------------------|
| M1 | 10     | 5      | 1 | 0,88         | 0,975    | 5         | 0                      |
| M2 | 10     | 2      | 2 | 0,89         | 0,968    | 5,2       | 0                      |
| M3 | 10     | 2      | 2 | 0,89         | 0,968    | 5,2       | 0                      |
| M4 | 10     | 0,0031 | 2 | 0,85         | 0,959    | 4         | 0                      |



Slika 1, Shema elektroenergetske mreže

# 2. PRORAČUN NADOMJESNIH IMPEDANCIJA ELEMENATA MREŽE

 $U_{REF} = 10 \text{ kV}$  – odabrani refernetni (bazni) napon na koji se preračunavaju sve impendacije zbog kratkog spoja na sabirnici 11, koja se nalazi na 10 kV,

#### G1

$$X''_{dG1} = X''_{dg1} \frac{U^2_{REF}}{S_{nG1}} = 0,0933 \, [\Omega]$$

$$R_{dG1} = R_{g1} \left(\frac{U_{REF}}{U_{nG1}}\right)^2 = 0,0005 \, [\Omega]$$

$$X_{iG1} = x_{iG1} \frac{U^2_{REF}}{S_{nG1}} = 0,0933 \, [\Omega]$$

$$Z''_{dG1} = R_{dG1} + jX''_{dG1} = 0,0005 + j0,0933 \, [\Omega]$$

$$Z_{iG1} = R_{iG1} + jX_{iG1} = 0,0005 + j0,0933 \, [\Omega]$$

#### G2

 $Z_{0G1} = \infty$ 

$$\begin{split} X_{dG2}^{\prime\prime} &= x_{dg2}^{\prime\prime} \frac{U_{REF}^2}{S_{nG2}} = 0,16 \ [\Omega] \\ R_{dG2} &= R_{g2} \left( \frac{U_{REF}}{U_{nG2}} \right)^2 = 0,005 \ [\Omega] \\ X_{iG2} &= x_{iG2} \frac{U_{REF}^2}{S_{nG2}} = 0,16 \ [\Omega] \\ Z_{dG2}^{\prime\prime} &= R_{dG2} + j X_{dG2}^{\prime\prime} = 0,005 + j0,16 \ [\Omega] \\ Z_{iG2} &= R_{iG2} + j X_{iG2} = 0,005 + j0,16 \ [\Omega] \\ Z_{0G2} &= \infty \end{split}$$

#### G3

 $Z_{0G3} = \infty$ 

$$X''_{dG3} = x''_{dg3} \frac{U_{REF}^2}{S_{nG3}} = 1 [\Omega]$$

$$R_{dG3} = R_{g3} \left(\frac{U_{REF}}{U_{nG3}}\right)^2 = 0,018 [\Omega]$$

$$X_{iG3} = x_{iG3} \frac{U_{REF}^2}{S_{nG3}} = 1 [\Omega]$$

$$Z''_{dG3} = R_{dG3} + jX''_{dG3} = 0,018 + j1 [\Omega]$$

$$Z_{iG3} = R_{iG3} + jX_{iG3} = 0,018 + j1 [\Omega]$$

#### **T1**

$$\begin{split} X_{dT1} &= X_{iT1} = \frac{u_{k\%}}{100\%} \frac{U_{REF}^2}{S_{nT1}} = 0,1067 \ [\Omega] \\ X_{0T1} &= 0,95 \ X_{dT1} = 0,1013 \ [\Omega] \\ R_{dT1} &= R_{iT1} = R_{0T1} = \frac{u_{t\%}}{100\%} \frac{U_{REF}^2}{S_{nT1}} = 0,0033 \ [\Omega] \\ Z_{NT1} &= Z_N \left(\frac{U_{REF}}{U_n}\right)^2 = \text{j}5,5 \ [\Omega] \\ Z_{dT1} &= Z_{iT1} = R_{dT1} + \text{j} \ X_{dT1} = 0,0033 + \text{j}0,1067 \ [\Omega] \end{split}$$

#### *T2*

$$\begin{split} X_{dT2} &= X_{iT2} = \frac{u_{k\%}}{100\%} \frac{u_{REF}^2}{S_{nT2}} = 0,12 \ [\Omega] \\ X_{0T2} &= X_{dT2} = 0,12 \ [\Omega] \\ R_{dT2} &= R_{iT2} = R_{0T2} = \frac{u_{r\%}}{100\%} \frac{u_{REF}^2}{S_{nT2}} = 0,005 \ [\Omega] \\ Z_{dT2} &= Z_{iT2} = Z_{0T2} = R_{dT2} + \mathrm{j} \ X_{dT2} = 0,005 + \mathrm{j}0,12 \ [\Omega] \end{split}$$

 $Z_{0T1} = R_{0T1} + j X_{0T1} + 3 \cdot Z_{NT1} = 0.0033 + j16.6 [\Omega]$ 

#### *T5*

$$\begin{split} X_{dT5} &= X_{iT5} = \frac{u_{k\%}}{100\%} \frac{U_{REF}^2}{S_{nT5}} = 0,38095 \ [\Omega] \\ X_{0T5} &= X_{dT5} = 0,38095 \ [\Omega] \\ R_{dT5} &= R_{iT5} = R_{0T5} = \frac{u_{r\%}}{100\%} \frac{U_{REF}^2}{S_{nT5}} = 0,015873 \ [\Omega] \\ Z_{dT5} &= Z_{iT5} = Z_{0T5} = R_{dT5} + \mathrm{j} \ X_{dT5} = 0,015873 + \mathrm{j} 0,38095 \ [\Omega] \end{split}$$

#### *T6*

$$\begin{split} X_{dT6} &= X_{iT6} = \frac{u_{k\%}}{100\%} \frac{U_{REF}^2}{S_{nT6}} = 0,38095 \ [\Omega] \\ X_{0T6} &= X_{dT6} = 0,38095 \ [\Omega] \\ R_{dT6} &= R_{iT6} = R_{0T6} = \frac{u_{r\%}}{100\%} \frac{U_{REF}^2}{S_{nT6}} = 0,015873 \ [\Omega] \\ Z_{dT6} &= Z_{iT6} = Z_{0T6} = R_{dT6} + \mathrm{j} \ X_{dT6} = 0,015873 + \mathrm{j} 0,38095 \ [\Omega] \\ Z_{NT6} &= Z_{N} \left( \frac{U_{REF}}{U_{n}} \right)^2 = 80 \ [\Omega] \end{split}$$

$$\begin{split} X_{dT7} &= X_{iT7} = X_{0T7} = \frac{u_{k\%}}{100\%} \frac{u_{REF}^2}{S_{nT7}} = 5 \ [\Omega] \\ R_{dT7} &= R_{iT7} = R_{0T7} = \frac{u_{r\%}}{100\%} \frac{u_{REF}^2}{S_{nT7}} = \ 1,03 \ [\Omega] \\ Z_{dT7} &= Z_{iT7} = Z_{0T5} = R_{dT7} + \mathrm{j} \ X_{dT7} = 1,03 + \mathrm{j} 5 \ [\Omega] \end{split}$$

*T3 i T4* – tronamotni transformatori jednakih podataka za direktni i inverzni sustav ( različita shema kod nultog sustava )

$$\begin{split} X_{d12} &= X_{l12} = \frac{u_{k12\%}}{100\%} \frac{U_{REF}^2}{S_{n12}} = 0,06 \ [\Omega] \\ X_{d13} &= X_{l13} = \frac{u_{k13\%}}{100\%} \frac{U_{REF}^2}{S_{n13}} = 0,2 \ [\Omega] \\ X_{d23} &= X_{l23} = \frac{u_{k23\%}}{100\%} \frac{U_{REF}^2}{S_{n23}} = 0,14 \ [\Omega] \\ X_{d1} &= X_{i1} = \frac{1}{2} \left( X_{d12} + X_{d13} - X_{d23} \right) = 0,06 \ [\Omega] \\ X_{d2} &= X_{i2} = \frac{1}{2} \left( X_{d12} + X_{d23} - X_{d13} \right) = 0 \ [\Omega] \\ X_{d3} &= X_{i3} = \frac{1}{2} \left( X_{d13} + X_{d23} - X_{d12} \right) = 0,14 \ [\Omega] \\ R_{d12} &= R_{i12} = \frac{u_{r12\%}}{100\%} \frac{U_{REF}^2}{S_{n12}} = 0,0007486 \ [\Omega] \\ R_{d13} &= R_{i13} = \frac{u_{r13\%}}{100\%} \frac{U_{REF}^2}{S_{n13}} = 0,0032 \ [\Omega] \\ R_{d23} &= R_{i23} = \frac{u_{r23\%}}{100\%} \frac{U_{REF}^2}{S_{n23}} = 0,0032 \ [\Omega] \\ R_{d2} &= R_{i2} = \frac{1}{2} \left( R_{d12} + R_{d13} - R_{d23} \right) = 0,00037143 \ [\Omega] \\ R_{d2} &= R_{i2} = \frac{1}{2} \left( R_{d12} + R_{d23} - R_{d13} \right) = 0,00037143 \ [\Omega] \\ R_{d3} &= R_{i3} = \frac{1}{2} \left( R_{d13} + R_{d23} - R_{d12} \right) = 0,0028286 \ [\Omega] \\ Z_{d1} &= Z_{i1} = R_{d1} + jX_{d1} = 0,00037143 \ [\Omega] \\ Z_{d2} &= Z_{i2} = R_{d2} + jX_{d2} = 0,00037143 \ [\Omega] \\ Z_{d3} &= Z_{i3} = R_{d3} + jX_{d3} = 0,0028286 + j0,14 \ [\Omega] \\ X_{012} &= \frac{u_{k012\%}}{100\%} \frac{U_{REF}^2}{S_{n12}} = 0,027171 \ [\Omega] \\ X_{013} &= \frac{u_{k013\%}}{100\%} \frac{U_{REF}^2}{S_{n12}} = 0,1902 \ [\Omega] \\ \end{split}$$

$$\begin{split} X_{023} &= \frac{u_{k023\%}}{100\%} \frac{U_{REF}^2}{S_{n23}} = 0,126 \ [\Omega] \\ X_{01} &= \frac{1}{2} \left( X_{012} + X_{013} - X_{023} \right) = 0,045686 \ [\Omega] \\ X_{02} &= \frac{1}{2} \left( X_{012} + X_{023} - X_{013} \right) = -0,018514 \ [\Omega] \\ X_{03} &= \frac{1}{2} \left( X_{013} + X_{023} - X_{012} \right) = 0,14451 \ [\Omega] \\ Z_{01} &= R_{01} + jX_{01} = 0,00037143 + j0,045686 \ [\Omega] \\ Z_{02} &= R_{02} + jX_{02} = 0,00037143 - j0,018514 \ [\Omega] \\ Z_{03} &= R_{03} + jX_{03} = 0,0028286 + j0,14451 \ [\Omega] \end{split}$$

#### ZV1, ZV1a

$$\begin{split} Z_{dV1} &= Z_{iV1} = Z_{dV1a} = Z_{iV1a} = Z_{dV1} \cdot 1 \cdot \left(\frac{\textit{U}_\textit{REF}}{\textit{U}_\textit{n}}\right)^2 = 0,\!019835 + j0,\!064463 \; [\Omega] \\ Z_{0V1} &= Z_{0V1a} = Z_0 \cdot 1 \cdot \left(\frac{\textit{U}_\textit{REF}}{\textit{U}_\textit{n}}\right)^2 = 0,\!052893 + j0,\!20826i \; [\Omega] \end{split}$$

#### ZV2

$$Z_{dV2} = Z_{iV2} = Z_{dV2} \cdot 1 \cdot \left(\frac{U_{REF}}{U_n}\right)^2 = 0,0099174 + j0,032231 [\Omega]$$
$$Z_{0V2} = Z_0 \cdot 1 \cdot \left(\frac{U_{REF}}{U_n}\right)^2 = 0,026446 + j0,10413 [\Omega]$$

#### ZV3

$$Z_{dV3} = Z_{iV3} = Z_{dV3} \cdot 1 \cdot \left(\frac{U_{REF}}{U_n}\right)^2 = 0,014876 + j0,047851 [\Omega]$$
$$Z_{0V3} = Z_0 \cdot 1 \cdot \left(\frac{U_{REF}}{U_n}\right)^2 = 0,027273 + j0,13636 [\Omega]$$

#### *K1*

$$Z_{dK1} = Z_{iK1} = Z_{dK1} \cdot 1 \cdot \left(\frac{U_{REF}}{U_n}\right)^2 = 0,253 + j0,107 [\Omega]$$

$$Z_{0K1} = Z_{0K1} \cdot 1 \cdot \left(\frac{U_{REF}}{U_n}\right)^2 = 0,9361 + j0,963 [\Omega]$$

#### *K*2

$$Z_{dK2} = Z_{iK2} = Z_{dK2} \cdot 1 \cdot \left(\frac{U_{REF}}{U_n}\right)^2 = 1,771 + j0,665 [\Omega]$$

$$Z_{0K2} = Z_{0K2} \cdot 1 \cdot \left(\frac{U_{REF}}{U_n}\right)^2 = 11,242 + j8,3125 [\Omega]$$

#### *K3*

$$\begin{split} Z_{dK3} &= Z_{iK3} = Z_{dK3} \cdot 1 \cdot \left(\frac{\textit{U}_\textit{REF}}{\textit{U}_n}\right)^2 = 1,3915 + j0,5885 \; [\Omega] \\ Z_{0K3} &= Z_{0K3} \cdot 1 \cdot \left(\frac{\textit{U}_\textit{REF}}{\textit{U}_n}\right)^2 = 5,1486 + j5,2965 \; [\Omega] \end{split}$$

#### **A1**

$$X_{dA1} = X_{iA1} = \frac{U_{REF}^2}{S_{k3}''} = 0,0039982 [\Omega]$$

$$X_{0A1} = 3 \cdot X_{dA1} = 0.011995 [\Omega]$$

$$R_{dA1} = 0.1 \cdot X_{dA1} = 0.00039982 \ [\Omega]$$

$$R_{0A1} = 0.15 \cdot X_{0A1} = 0.0017992 [\Omega]$$

$$Z_{dA1} = Z_{iA1} = R_{dA1} + jX_{dA1} = 0,00039982 + j0,0039982$$
 [ $\Omega$ ]

$$Z_{0A1} = R_{0A1} + jX_{OA1} = 0.0017992 + j0.011995$$
 [ $\Omega$ ]

#### A2

$$X_{dA2} = X_{iA2} = \frac{\mathit{U}^2_{REF}}{\mathit{S}''_{k3}} = 0,032804 \; [\Omega]$$

$$X_{0A2} = 3.3 \cdot X_{dA2} = 0.098412 [\Omega]$$

$$R_{dA2} = 0.1 \cdot X_{dA2} = 0.0032804 [\Omega]$$

$$R_{0A2} = 0.2 \cdot X_{0A2} = 0.019682 [\Omega]$$

$$Z_{dA2} = Z_{iA2} = R_{dA2} + jX_{dA2} = 0.0032804 + j0.032804 [\Omega]$$

$$Z_{0A2} = R_{0A2} + jX_{OA2} = 0,019682 + j0,098412 \text{ [}\Omega\text{]}$$

#### *M1*

$$X_{\rm dM1} = X_{\rm iM1} = \frac{1}{\frac{I_P}{I_n}} \frac{U_{REF}^2}{P_n} \, \eta \cdot \cos \varphi = 3,432 \, [\Omega]$$

$$X_{0M1} = \infty$$
  $\longrightarrow$   $Z_{0M1} = \infty$  - nije uzemljen

$$Z_{dM1} = Z_{iM1} = j3,432 [\Omega]$$

#### *M2*

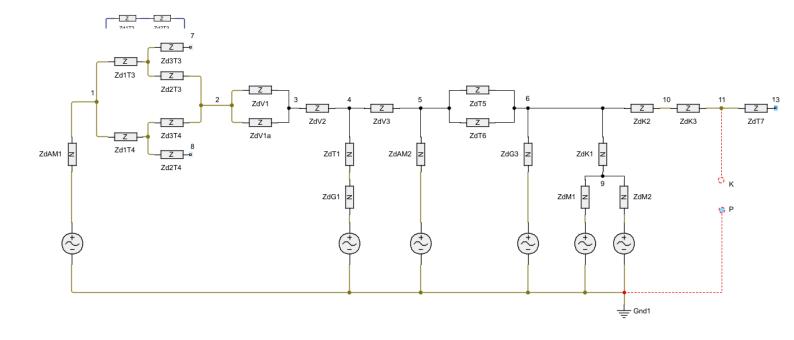
$$X_{\rm dM2} = X_{\rm iM2} = \frac{1}{\frac{I_p}{I_n}} \frac{U_{REF}^2}{P_n} \, \eta \cdot \cos \varphi = 8,2838 \, [\Omega]$$

$$X_{0M2} = \infty$$
  $\longrightarrow Z_{0M2} = \infty$  - nije uzemljen

$$Z_{\text{dM2}} = Z_{i\text{M2}} = j8,\!2838i \; [\Omega]$$

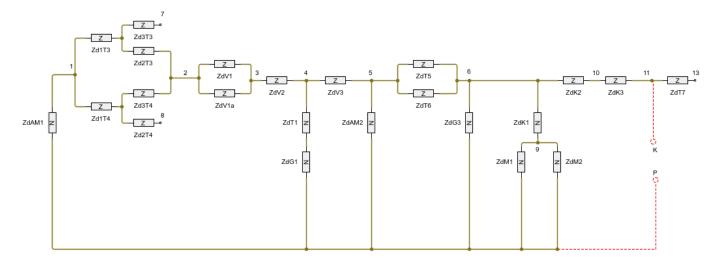
# 3. NADOMJESNE SHEME EEM U SUSTAVU SIMETRIČNIH KOMPONENTI

## 3.1.Nadomjesna shema za direktni sustav



 $Z''_{dUK} = 3,1707 + j1,4191 [\Omega]$ 

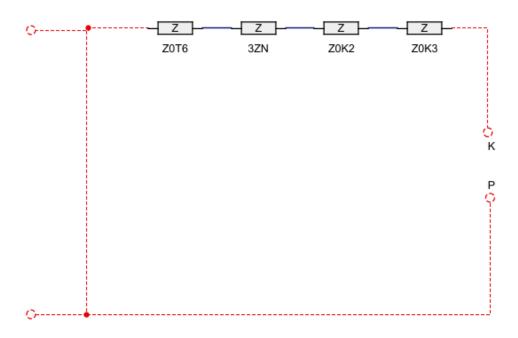
## 3.2.Nadomjesna shema EEM u inverznom sustavu



$$Z_{iUK} = Z''_{dUK} = 3,1707 + j1,4191 [\Omega]$$

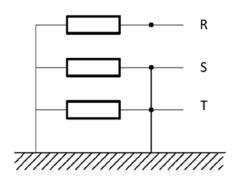
# 3.3.Nadomjesna shema EEM u nultom sustavu

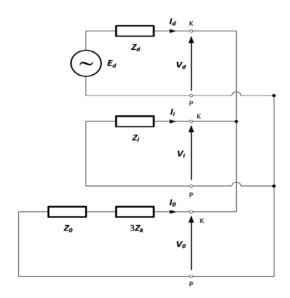
#### NULTI SUSTAV



$$Z_{0UK} = 96.4064 + j13.9900 [\Omega]$$

#### 3.4.U - I prilike na mjestu kvara (sabirnica 11)





Slika 3,4, Nadomjesna shema 2pz KS s pripadajućim vrijednostima impedancija

U-I prilike na mjestu KS ako je KS nastao među fazama S i T:

$$ar{V}_S$$
 = 0 ,  $ar{V}_T$  = 0 ,  $ar{V}_d$  = $ar{V}_i$  = $ar{V}_0$ 

$$\bar{I}_R = 0$$
 ,  $\bar{I}_d^{"} + \bar{I}_i + \bar{I}_0 = 0$ 

$$\bar{I}_{K2pz}^{"} = -\frac{\sqrt{3} \cdot U_{REF} \cdot Z_i}{Z_d Z_i + Z_d Z_0 + Z_i Z_0} = 0,087399 \angle 171,468784^{\circ} \text{ [kA]}$$

$$\bar{I}_d^{"} = \frac{U_{REF}}{\sqrt{3}} \cdot \frac{Z_0 + Z_i}{Z_d Z_i + Z_d Z_0 + Z_i Z_0} = 0,845051 \angle -23,846432^{\circ} \text{ [kA]}$$

$$\bar{I}_i = -\frac{U_{REF}}{\sqrt{3}} \cdot \frac{Z_0}{Z_d Z_i + Z_d Z_0 + Z_i Z_0} = 0,816988 \angle 155,613912^{\circ} \text{ [kA]}$$

$$\bar{I}_0 = -\frac{U_{REF}}{\sqrt{3}} \cdot \frac{Z_i}{Z_d Z_i + Z_d Z_0 + Z_i Z_0} = 0,029133 \ \angle 171,468784^{\circ} \text{ [kA]}$$

$$\bar{I}_S = \frac{U_{REF}}{\sqrt{3}} \cdot \frac{Z_i(a^2-1) + Z_0(a^2-a)}{Z_d Z_i + Z_d Z_0 + Z_i Z_0} = 1,451700 \angle -115,773304^{\circ} \text{ [kA]}$$

$$\bar{I}_T = \frac{U_{REF}}{\sqrt{3}} \cdot \frac{Z_i(a-1) + Z_0(a-a^2)}{Z_d Z_i + Z_d Z_0 + Z_i Z_0} = 1,428235 \angle 67,577203^{\circ} \text{ [kA]}$$

$$\overline{V}_d \!= \overline{E}_d - \overline{I}_d^{\prime\prime} \cdot Z_{dUK}^{\prime\prime} \!= 2,\!838042 \, \angle \, -0,\!27 \, -77,\!6486754384^{\rm o} \, [\rm kV]$$

$$\bar{V}_i = -\bar{I}_i \cdot Z_{iUK} = 2,838042 \angle -0,274384^{\circ} [\text{ kV}]$$

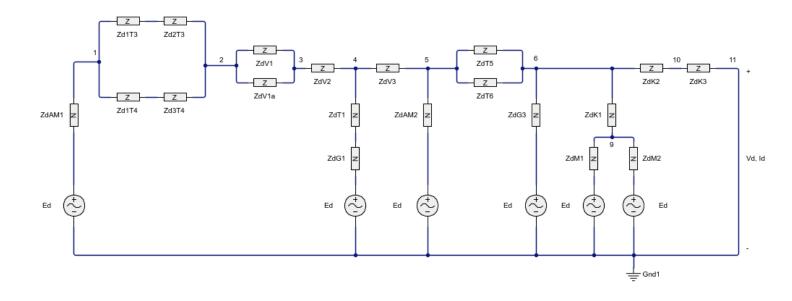
$$\bar{V}_0 = -\bar{I}_0 \cdot Z_{0UK} = 2,838042 \angle -0,274384^{\circ} \text{ [kV]}$$

$$\bar{V}_R = \bar{V}_d + \bar{V}_i + \bar{V}_0 = 8,514126 \angle -0,274384^{\circ} \text{ [kV]}$$

## 4. UDIO POJEDINIH IZVORA U STRUJI KRATKOG SPOJA

#### DIREKTNI SUSTAV

DIREKTNI SUSTAV



 $\bar{I}_{dM1} = 0,402266 \ \angle 75,782591^{\circ} \ [\text{kA}]$ 

 $\bar{I}_{dM2} = 0,166659 \angle 75,782591^{\circ} \text{ [kA]}$ 

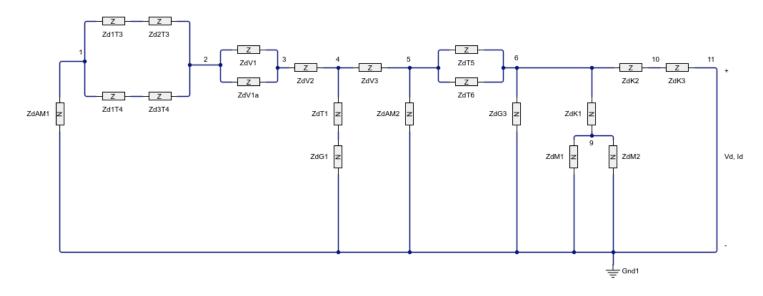
 $\bar{I}_{dG1} = 28,888772 \ \angle \, 91,065720^{\circ} \, [\text{kA}]$ 

 $\bar{I}_{dG2} = 1,112485 \angle -83,378530^{\circ} \text{ [kA]}$ 

 $\bar{I}_{dAM1} = 19,234885 \angle -85,285946^{\circ} \text{ [kA]}$ 

 $\bar{I}_{dAM2} = 175,287157 \angle 95,678278^{\circ} \text{ [kA]}$ 

#### INVERZNI SIISTA V



$$I_{dM1} = 1,296082 \angle -85,628237^{\circ}$$
 [kA]

$$\bar{I}_{dM2} = 0.536967 \angle -85.628237^{\circ} \text{ [kA]}$$

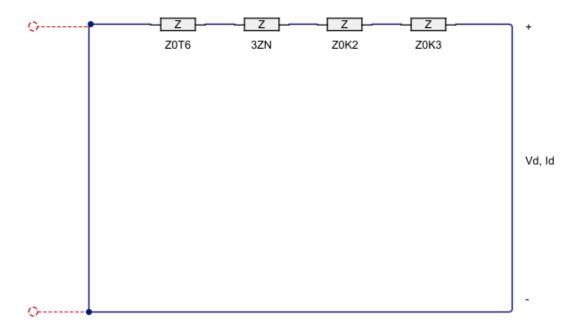
$$\bar{I}_{dG1} = 0.385397 \angle -77.866433^{\circ} \text{ [kA]}$$

$$\bar{I}_{dG2} = 1,075542 \angle -83,918187^{\circ}$$
 [kA]

$$\bar{I}_{dAM1} = 39,445081 \angle -74,255016^{\circ} \text{ [kA]}$$

$$\bar{I}_{dAM2} = 2,338459 \angle -73,253874^{\circ} \text{ [kA]}$$

### NULTI SUSTAV



Obzirom da se nulta struja može zatvarati samo preko uzemljenog transformatora T6, te kabela K2 i K3, izvori EMS-a u zadanom EES-u ne sudjeluju u nultoj struji,

#### Udio aktivne mreže 1 (A1) u struji kratkog spoja:

$$\begin{split} &I_{A1R} = (I_{dA1} + I_{iA1}) \cdot \frac{u_{REF}}{u_n} = 1,537910 \angle -77,865691^{\circ} \text{ [kA]} \\ &I_{A1S} = (a^2 \cdot I_{dA1} + a \cdot I_{iA1}) \cdot \frac{u_{REF}}{u_n} = 0,996058 \angle 74,468729 \text{ [kA]} \\ &I_{A1T} = (a \cdot I_{dlijevo} + a^2 \cdot I_{ilijevo}) \cdot \frac{u_{REF}}{u_n} = 0,802414 \angle 137,329307^{\circ} \text{ [kA]} \end{split}$$

## Udio aktivne mreže 2 (A2) u struji kratkog spoja:

$$\begin{split} &I_{A2R} = (I_{dA2} + I_{iA2}) \cdot \frac{\textit{U}_{REF}}{\textit{U}_n} = 15,726616 \ \angle 95,529595^{\circ} \text{ [kA]} \\ &I_{A2S} = (a^2 \cdot I_{dA2} + a \cdot I_{iA2}) \cdot \frac{\textit{U}_{REF}}{\textit{U}_n} = 16,005433 \ \angle -23,601858^{\circ} \text{ [kA]} \\ &I_{A2T} = (a \cdot I_{dA2} + a^2 \cdot I_{iA2}) \cdot \frac{\textit{U}_{REF}}{\textit{U}_n} = 16,075655 \ \angle -144,892977^{\circ} \text{ [kA]} \end{split}$$

#### Udio generatora 1 (G1) u struji kratkog spoja:

$$\begin{split} & I_{G1R} = (I_{dG1} \cdot e^{\frac{-jk\pi}{6}} + I_{iG1} \cdot e^{\frac{jk\pi}{6}}) \cdot \frac{U_{REF}}{U_n} = 2,131593 \angle -77,865691^{\circ} \text{ [kA]} \\ & I_{G1S} = (a^2 \cdot I_{dG1} \cdot e^{\frac{-jk\pi}{6}} + a \cdot I_{iG1} \cdot e^{\frac{jk\pi}{6}}) \cdot \frac{U_{REF}}{U_n} = 1,380569 \angle 74,468729^{\circ} \text{ [kA]} \\ & I_{G1T} = (a \cdot I_{dG1} \cdot e^{\frac{-jk\pi}{6}} + a^2 \cdot I_{iG1} \cdot e^{\frac{jk\pi}{6}}) = 1,112171 \angle 137,329307^{\circ} \text{ [kA]} \end{split}$$

#### Udio generatora 3 (G3) u struji kratkog spoja:

$$\begin{split} &I_{G3R} = (I_{dG3} + I_{iG3}) \cdot \frac{\textit{U}_{REF}}{\textit{U}_n} = 12,619660 \ \angle \ 95,529595^{\circ} \ [kA] \\ &I_{G3S} = (a^2 \cdot I_{dG3} + a \cdot I_{iG3}) \cdot \frac{\textit{U}_{REF}}{\textit{U}_n} = 14,031268 \ \angle \ -13,206055^{\circ} \ [kA] \\ &I_{G3T} = (a \cdot I_{dG3} + a^2 \cdot I_{iG3}) \cdot \frac{\textit{U}_{REF}}{\textit{U}_n} = 14,803910 \ \angle \ -152,876381^{\circ} \ [kA] \end{split}$$

## Udio asinkronog motora 1 u struji kratkog spoja:

$$\begin{split} &\mathbf{I}_{\text{M1R}} = (\mathbf{I}_{\text{dM1}} + \mathbf{I}_{\text{iM1}}) \cdot \frac{u_{REF}}{u_n} = 0,913768 \ \angle -79,355665^{\circ} \text{ [kA]} \\ &\mathbf{I}_{\text{M1S}} = (a^2 \cdot \mathbf{I}_{\text{dM1}} + a \cdot \mathbf{I}_{\text{iM1}}) \cdot \frac{u_{REF}}{u_n} = 1,405147 \ \angle 18,915227^{\circ} \text{ [kA]} \\ &\mathbf{I}_{\text{M1T}} = (a \cdot \mathbf{I}_{\text{dM1}} + a^2 \cdot \mathbf{I}_{\text{iM1}}) \cdot \frac{u_{REF}}{u_n} = 1,648659 \ \angle 163,961203^{\circ} \text{ [kA]} \end{split}$$

#### Udio asinkronog motora 2 u struji kratkog spoja:

$$\begin{split} &I_{M2R} = (I_{dM2} + I_{iM2}) \cdot \frac{\textit{U}_{REF}}{\textit{U}_n} = 0,382709 \ \angle \ -77,648675^{\circ} \text{ [kA]} \\ &I_{M2S} = (a^2 \cdot I_{dM2} + a \cdot I_{iM2}) \cdot \frac{\textit{U}_{REF}}{\textit{U}_n} = 0,592890 \ \angle \ 18,377599^{\circ} \text{ [kA]} \\ &I_{M2T} = (a \cdot I_{dM2} + a^2 \cdot I_{iM2}) \cdot \frac{\textit{U}_{REF}}{\textit{U}_n} = 0,671075 \ \angle \ 163,826558^{\circ} \text{ [kA]} \end{split}$$

