

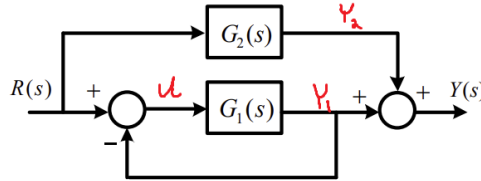
# Homework 6

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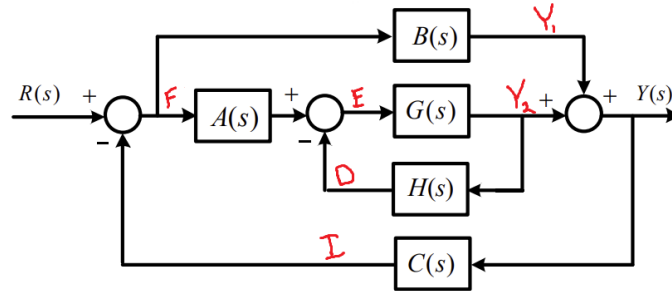
16 November 2023

**Problem 1****Statement:**

Find the transfer function for the block diagrams:



(a)



(b)

Figure 1: Problem 1

**Solution**

$$\begin{aligned} \text{a) } Y(s) &= Y_1(s) + Y_2(s) = G_1(s)U(s) + G_2(s)R(s), \\ U(s) &= R(s) - G_1(s)U(s) \implies (1 + G_1(s))U(s) = R(s) \implies U(s) = \frac{R(s)}{1 + G_1(s)} \\ \text{So, } Y(s) &= \left[ \frac{G_1(s)}{1 + G_1(s)} + G_2(s) \right] R(s) \end{aligned}$$

b) So we are going to start in the inside and go outside.

$$\begin{aligned} Y_2(s) &= G(s)E(s) \\ E(s) &= A(s)F(s) - H(s)Y_2(s) \\ Y_2(s) &= G(s)A(s)F(s) - G(s)H(s)Y_2(s) \\ Y_2(s) &= \frac{G(s)A(s)F(s)}{1 + G(s)H(s)} \end{aligned}$$

Now this gives us the middle component. Now we can use this to find the outer component.  $Y_1(s) = B(s)F(s)$  is easy. And our last equation:  $F(s) = R(s) - C(s)Y(s)$  will bring

everything together. We know

$$\begin{aligned}
 Y(s) &= Y_1(s) + Y_2(s) \\
 &= B(s)F(s) + \frac{G(s)A(s)F(s)}{1 + G(s)H(s)} \\
 &= \left[ B(s) + \frac{G(s)A(s)}{1 + G(s)H(s)} \right] F(s) \\
 &= \left[ B(s) + \frac{G(s)A(s)}{1 + G(s)H(s)} \right] [R(s) - C(s)Y(s)] \\
 Y(s) &= \left[ B(s) + \frac{G(s)A(s)}{1 + G(s)H(s)} \right] R(s) - \\
 &\quad \left[ B(s)C(s) + \frac{G(s)A(s)C(s)}{1 + G(s)H(s)} \right] Y(s) \\
 Y(s) \left[ 1 + B(s)C(s) + \frac{G(s)A(s)C(s)}{1 + G(s)H(s)} \right] &= \left[ B(s) + \frac{G(s)A(s)}{1 + G(s)H(s)} \right] R(s) \\
 Y(s) &= \frac{\left[ B(s) + \frac{G(s)A(s)}{1 + G(s)H(s)} \right]}{\left[ 1 + B(s)C(s) + \frac{G(s)A(s)C(s)}{1 + G(s)H(s)} \right]} R(s)
 \end{aligned}$$

**Problem 2****Statement:**

Determine the time constant of the system:

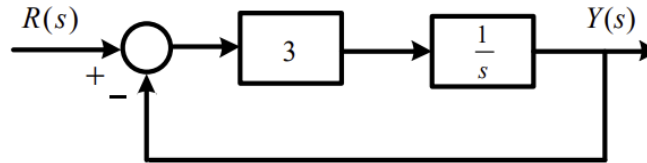


Figure 2: Problem 2

**Solution**

First we need to write the transfer function for the system. We can do this by using the block diagram.  $Y(s) = \frac{3}{s}U(s)$ , and  $U(s) = R(s) - Y(s)$ , so

$Y(s) = \frac{3}{s}[R(s) - Y(s)] \implies Y(s) = \frac{1}{1+3/s}R(s) = \frac{s}{s+3}R(s)$ . We want the response to a unit step, so  $R(s) = \frac{1}{s}$ , so  $Y(s) = \frac{1}{s+3}$ , thus  $y(t) = e^{-3t}$ , so our time constant is  $\frac{1}{3}$

**Problem 3****Statement:**

Specify the gain  $K$  of the proportional controller so that the output  $y(t)$  has an overshoot of no more than 10% in response to a unit step

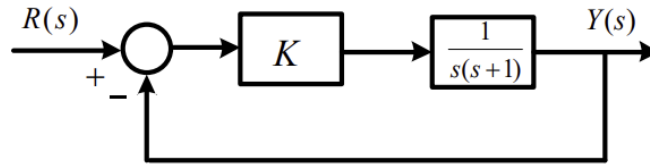


Figure 3: Problem 3

**Solution**

First, we go for the transfer function:  $Y(s) = KG(s)U(s)$ , and  $U(s) = R(s) - Y(s)$ , so  $Y(s) = \frac{KG(s)}{1+G(s)}R(s)$ .

$$\begin{aligned}
 Y(s) &= \frac{KG(s)}{1+G(s)}R(s) \\
 &= \frac{K \frac{1}{s(s+1)}}{1 + \frac{1}{s(s+1)}}R(s) \\
 &= \frac{K \frac{1}{s(s+1)}}{\frac{s(s+1)+1}{s(s+1)}}R(s) \\
 &= \frac{K}{s^2 + s + 1}R(s)
 \end{aligned}$$

We recognize the standard form of a second order system, so we can use the standard formula for the overshoot.  $G(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$ , so in our case  $\omega_n = \sqrt{K}$ , so  $\xi = \frac{1}{2\sqrt{K}}$ ,

then

$$\begin{aligned}
 M_p &= \exp\left(\frac{-\pi\xi}{\sqrt{1-\xi^2}}\right) \\
 &= \exp\left(\frac{-\pi\frac{1}{2\sqrt{K}}}{\sqrt{1-\frac{1}{4K}}}\right) \\
 &= \exp\left(\frac{-\pi\frac{1}{2\sqrt{K}}}{\frac{\sqrt{4K-1}}{2\sqrt{K}}}\right) \\
 &= \exp\left(\frac{-\pi}{\sqrt{4K-1}}\right)
 \end{aligned}$$

We want  $M_p \leq 0.1$ , so we solve:

$$\begin{aligned}
 0.1 &\leq \exp\left(\frac{-\pi}{\sqrt{4K-1}}\right) \\
 \ln(0.1) &\leq \frac{-\pi}{\sqrt{4K-1}} \\
 \ln(0.1)\sqrt{4K-1} &\leq -\pi \\
 \sqrt{4K-1} &\geq -\frac{\pi}{\ln(0.1)} \\
 4K-1 &\geq \frac{\pi^2}{\ln(0.1)^2} \\
 K &\geq \frac{\pi^2}{4\ln(0.1)^2} + \frac{1}{4} \\
 K &\geq 0.715381
 \end{aligned}$$

So pick  $K = 0.75$

### Problem 4

**Statement:**

Consider the system

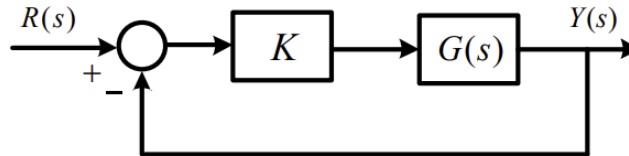


Figure 4: Problem 4

with

a)  $KG(s) = \frac{4(s+2)}{s(s^3+2s^2+3s+4)}$

b)  $KG(s) = \frac{2(s+4)}{s^2(s+1)}$

Use Routh's stability criterion to determine whether the each of the resulting closed-loop system will be asymptotically stable.

### Solution

with

a)  $KG(s) = \frac{4(s+2)}{s(s^3+2s^2+3s+4)}$  We multiply this out to get:  $\frac{4s+8}{s^4+2s^3+3s^2+4s}$ , and then we can write the Routh table:

$$\begin{array}{c|cc} s^4 & 1 & 3 \\ s^3 & 2 & 4 \\ s^2 & -\frac{4-6}{2} = 1 & 0 \\ s^1 & 4 & * \\ s^0 & 0 & * \end{array}$$

Which has no sign changes, so there are no poles with a positive real part. So the system is marginally stable.

b)  $KG(s) = \frac{2(s+4)}{s^2(s+1)} = \frac{2s+8}{s^3+s^2}$ . We can write the Routh table:

$$\begin{array}{c|cc} s^3 & 1 & 0 \\ s^2 & 1 & 0 \\ s^1 & 0 \rightarrow 2 & * \\ s^0 & \frac{0}{-2} = 0 & * \end{array}$$

for the  $s^1$  row of zeros:  $s^2 + 4 \rightarrow 2s + 0$ . This also has no sign changes, but the last value is zero. So it is marginally stable.



**Problem 5****Statement:**

Using Routh's stability criterion to determine how many roots with positive real parts the following equations have:

a)  $s^4 + 8s^3 + 32s^2 + 80s + 100 = 0$

b)  $s^5 + 10s^4 + 30s^3 + 80s^2 + 344s + 480 = 0$

**Solution**

a) We write the Routh table:

$$\begin{array}{c|ccc}
 s^4 & 1 & 32 & 100 \\
 s^3 & 8 & 80 & 0 \\
 s^2 & 22 & 100 & 0 \\
 s^1 & \frac{960}{22} & * & * \\
 s^0 & \frac{960 \cdot 100}{22} * \frac{22}{960} = 100 & & 
 \end{array}$$

So no roots have positive real parts.

b) We write the Routh table:

$$\begin{array}{c|ccc}
 s^5 & 1 & 30 & 344 \\
 s^4 & 10 & 80 & 480 \\
 s^3 & 22 & 296 & 0 \\
 s^2 & -\frac{600}{11} & 480 & * \\
 s^1 & -(22 * 480 + \frac{600}{11} * 296) \frac{-11}{600} = \frac{968}{5} + 296 & * & * \\
 s^0 & 480 & * & *
 \end{array}$$

There are two sign changes, so two roots with positive real parts.

### Problem 6

**Statement:**

Consider the closed-loop system:

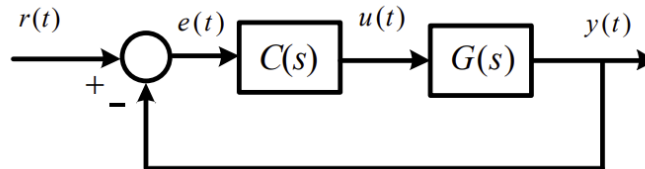


Figure 5: Problem 6

$$G(s) = \frac{1}{s^2}, \text{ and } C(s) = \frac{10(s+2)}{s+5}.$$

Find the system type and determine the steady state tracking errors for:

- a)  $r(t) = 1(t)$
- b)  $r(t) = t1(t)$
- c)  $r(t) = 1/2t^21(t)$

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### Solution

So  $L(s) = G(s)C(s) = \frac{10(s+2)}{s^2(s+5)}$ . So it is a type 2 system with  $L_0 = \frac{10(s+2)}{s+5}$ , we evaluate this at  $s = 0$  to get  $L_0 = 4$ . This is  $K_a$ . So the steady state error is:

- a)  $r(t) = 1(t) \implies 0$
- b)  $r(t) = t1(t) \implies 0$
- c)  $r(t) = 1/2t^21(t) \implies 1/4$

**Problem 7****Statement:**

Sketch the Nyquist plot for an open-loop system with transfer function:

a)  $G(s) = \frac{1}{s^2}$

b)  $G(s) = \frac{1}{s^2+4}$

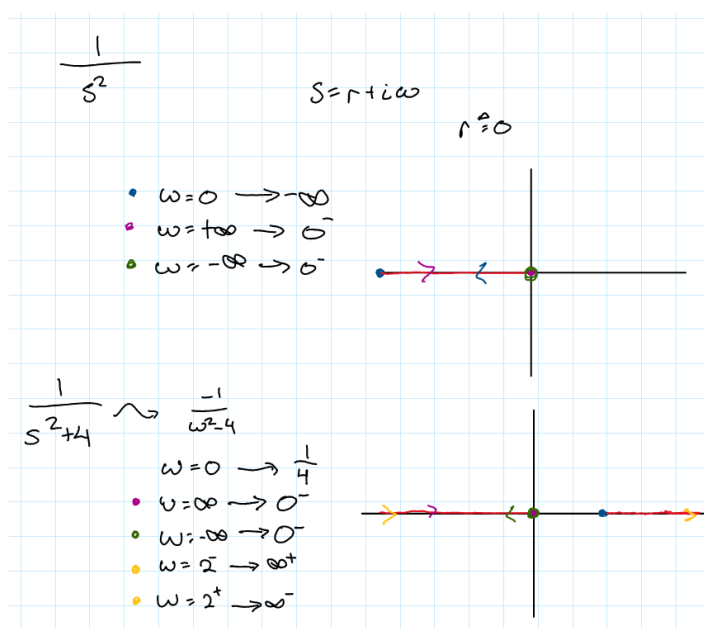
**Solution**

Figure 6

1. First we solve for  $G(i\omega)$ :

$$\begin{aligned}
 G(i\omega) &= \frac{1}{(i\omega)^2} \\
 &= \frac{1}{-\omega^2} \\
 &= -\frac{1}{\omega^2}
 \end{aligned}$$

So this is just the negative real line.

2. First we solve for  $G(i\omega)$ :

$$\begin{aligned} G(i\omega) &= \frac{1}{(i\omega)^2 + 4} \\ &= \frac{1}{-\omega^2 + 4} \\ &= -\frac{1}{\omega^2 - 4} \end{aligned}$$

So this starts at  $1/4$ , goes to  $+\infty$ , then teleports to  $-\infty$  and goes to zero before turning around.

**Problem 8****Statement:**

Consider the system with loop gain

$$L(s) = KG(s) = \frac{K(s+2)}{s+10}$$

Use Matlab command nyquist to plot nyquist plot for  $G(s)$ , and based on the nyquist plot, determine the range of  $K$  for which the closed-loop system is asymptotically stable

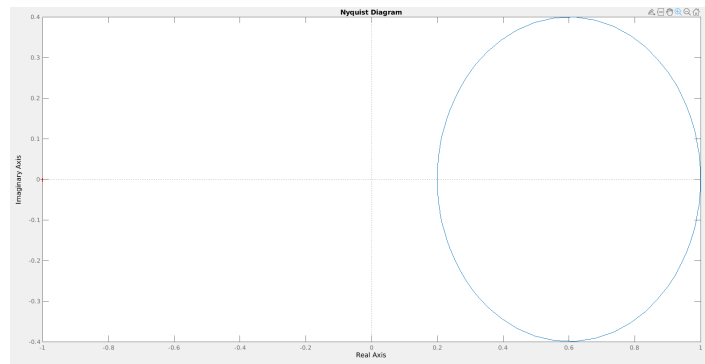
**Solution**

Figure 7

We also solve for

$$\begin{aligned} L(i\omega) &= \frac{K(i\omega + 2)}{i\omega + 10} \\ &= \frac{K(i\omega + 2)(-i\omega + 10)}{(i\omega + 10)(-i\omega + 10)} \\ &= \frac{K(\omega^2 + 8i\omega + 20)}{\omega^2 + 100} \\ &= K \frac{\omega^2 + 20}{\omega^2 + 100} + iK \frac{8\omega}{\omega^2 + 100} \end{aligned}$$

So we can see that the real part is always positive, thus the system can never encircle -1, so the system is always asymptotically stable.

**Problem 9****Statement:**

Is the following system controllable? Observable?

$$\begin{aligned}\dot{x} &= \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix} x + \begin{pmatrix} 0 \\ 1 \end{pmatrix} u \\ y &= (1 \ 0) x\end{aligned}$$

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**Solution**

For controllability, we build the controllability matrix.  $C = [B \ AB] \ AB = \begin{bmatrix} 1 \\ -1 \end{bmatrix}$ , so  $C = \begin{bmatrix} 0 & 1 \\ 1 & -1 \end{bmatrix}$  which is full rank, so it is controllable.

For observability, we build the observability matrix.  $O = \begin{bmatrix} C \\ CA \end{bmatrix} \ CA = [0 \ 1]$ , so  $O = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$  which is full rank, so it is observable.