

# An open-source discontinuous Galerkin solver in Python

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# Introduction

Quail is an open-source discontinuous Galerkin (DG) code written in Python for numerically solving systems of partial differential equations (PDEs). The objective of this code is to serve as a teaching and prototyping platform for DG methods, with particular focus on code clarity, modularity, and ease of use. Vectorized NumPy operations are extensively utilized to improve computational efficiency. A suite of commonly employed physical models, numerical techniques, and processing tools is available in the code. Currently, Quail solves hyperbolic PDEs on 1D/2D unstructured meshes. This document provides a basic overview of the mathematical formulation and solver features. It provides instructions on how to use the solver and guidelines for software design and future code development. Links to relevant video tutorials are given as well.

# Mathematical formulation

### 2.1 Spatial discretization

Two discretization schemes are available in Quail: a standard DG discretization and an ADER-DG discretization. This section outlines the derivation of the local semidiscrete form of each scheme. Additional details on the standard DG discretization can be found in Ref. [1]

QUAIL solves linear and nonlinear hyperbolic systems of PDEs of the following form:

$$\partial_t U + \nabla \cdot F = S, \tag{2.1}$$

where  $U(\boldsymbol{x},t): \mathbb{R}^{N_d} \times \mathbb{R}^+ \to \mathbb{R}^{N_s}$  is the conservative state vector,  $F(\boldsymbol{U}): \mathbb{R}^{N_s} \to \mathbb{R}^{N_s \times N_d}$  is the flux, and  $S(\boldsymbol{U}): \mathbb{R}^{N_s} \to \mathbb{R}^{N_s}$  is the source term. In addition,  $\boldsymbol{x} \in \mathbb{R}^{N_d}$  is the spatial coordinate vector,  $t \in \mathbb{R}^+$  is the time,  $N_s$  is the number of state variables, and  $N_d$  is the number of spatial dimensions.

Let  $\Omega$  denote the computational domain, which is partitioned into  $N_e$  non-overlapping discrete elements such that  $\Omega = \bigcup_{e=1}^{N_e} \Omega_e$ .  $\partial \Omega_e$  is the boundary of element  $\Omega_e$ . The space of test functions is defined as

$$\mathcal{V}_h^p = \{ \phi \in L^2(\Omega), \phi |_{\Omega_e} \in \mathcal{P}_p(\Omega_e) \ \forall \ \Omega_e \in \Omega \},$$
(2.2)

where  $\phi$  is the test function and  $\mathcal{P}_p$  denotes the space of polynomial functions of degree no greater than p. The approximation to the global solution,  $U_h \simeq U$ , can be expanded as

$$U_h = \bigoplus_{e=1}^{N_e} U_h^e, \tag{2.3}$$

where  $U_h^e$  is the local discrete solution,

$$U_h^e(\boldsymbol{x},t) = \sum_{n=1}^{N_b} \widetilde{U}_n^e(t)\phi_n(\boldsymbol{x}), \qquad (2.4)$$

 $\widetilde{\pmb{U}}_n^e(t): \mathbb{R}^+ \to \mathbb{R}^{N_s}$  is the nth vector of basis coefficients, and  $\{\phi_n\}_{\{n=1,\dots,N_b\}}$  is a basis of  $\mathcal{P}_p(\Omega_e)$ .

#### 2.1.1 DG

To solve for the local discrete solution, we require  $U_h^e$  to satisfy

$$\int_{\Omega_e} \phi_m \partial_t \boldsymbol{U}_h^e d\Omega + \int_{\Omega_e} \phi_m \nabla \cdot \boldsymbol{F}(\boldsymbol{U}_h^e) d\Omega = \int_{\Omega_e} \phi_m \boldsymbol{S}(\boldsymbol{U}_h^e) d\Omega \ \forall \ \phi_m.$$
 (2.5)

Combining the first term in Eq. (2.5) with Eq. (2.4) allows us to write

$$\int_{\Omega_e} \phi_m \partial_t \boldsymbol{U}_h^e d\Omega = \sum_{n=1}^{N_b} d_t \widetilde{\boldsymbol{U}}_n^e(t) \int_{\Omega_e} \phi_m \phi_n d\Omega = \sum_{n=1}^{N_b} d_t \widetilde{\boldsymbol{U}}_n^e(t) M_{mn}^e, \tag{2.6}$$

where  $M_{mn}^e = \int_{\Omega_o} \phi_m \phi_n d\Omega$  represents the element-local mass matrix.

The second integral in Eq. (2.5) is the convective term. Upon performing integration by parts, this term can be expressed as

 $\int_{\Omega_e} \phi_m \nabla \cdot \boldsymbol{F}(\boldsymbol{U}_h^e) d\Omega = -\int_{\Omega_e} \nabla \phi_m \cdot \boldsymbol{F}(\boldsymbol{U}_h^e) d\Omega + \oint_{\partial \Omega_e} \phi_m \widehat{\boldsymbol{F}}(\boldsymbol{U}_h^{e+}, \boldsymbol{U}_h^{e-}, \widehat{\boldsymbol{n}}) d\Gamma, \tag{2.7}$ 

where  $\hat{n}$  is the outward-pointing unit normal vector,  $(\cdot)^+$  and  $(\cdot)^-$  denote interior and exterior information on  $\partial\Omega_e$ , respectively, and  $\hat{F}$  is the numerical flux (or flux function). The second term on the RHS assumes an element not adjacent to a boundary. Boundary treatment will be discussed in Section 2.6.1.

Combining Eqs. (2.5), (2.6), and (2.7) gives the following:

$$\sum_{n=1}^{N_b} d_t \widetilde{\boldsymbol{U}}_n^e(t) M_{mn}^e = \boldsymbol{R}_m = \int_{\Omega_e} \nabla \phi_m \cdot \boldsymbol{F}(\boldsymbol{U}_h^e) d\Omega - \oint_{\partial \Omega_e} \phi_m \widehat{\boldsymbol{F}}(\boldsymbol{U}_h^{e+}, \boldsymbol{U}_h^{e-}, \widehat{\boldsymbol{n}}) d\Gamma + \int_{\Omega_e} \phi_m \boldsymbol{S}(\boldsymbol{U}_h^e) d\Omega, \tag{2.8}$$

where  $R_m$  is the mth residual vector. The time derivative on the LHS is treated using the explicit time stepping schemes described in Section 2.5.1.

#### 2.1.2 ADER-DG

The "Arbitrary high-order scheme using derivatives" (ADER) follows the work of Dumbser et al., where we utilize a DG discretization in space and time [2]. This scheme was first introduced in the context of finite volume schemes [2], but was later extended to DG methods with applications to stiff source terms [3]. The method is cast as a predictor-corrector type scheme. First, a predicted space-time solution is found through a weak solution to our system of partial differential equations (PDEs), without considering jump conditions through the interaction between neighboring elements. Then, we utilize the predicted solution vector to advance our solution in time through a DG discretization in space-time.

To solve for the local discrete solution, we multiply the governing PDE system in Eq. (2.1) by the basis and integrate over a space-time control volume  $\Omega_e^{st} = \Omega_e \times [t_n, t_{n+1}]$ . This leads to

$$\int_{t_n}^{t_{n+1}} \int_{\Omega_e} \phi_m \partial_t \boldsymbol{U}_h^e d\Omega dt + \int_{t_n}^{t_{n+1}} \int_{\Omega_e} \phi_m \nabla \cdot \boldsymbol{F}(\boldsymbol{U}_h^e) d\Omega dt = \int_{t_n}^{t_{n+1}} \int_{\Omega_e} \phi_m \boldsymbol{S}(\boldsymbol{U}_h^e) d\Omega dt \ \forall \ \phi_m.$$
 (2.9)

For ADER-DG, higher-order accuracy in time is not achieved through multiple stages but rather through an element-local space-time predictor solution.

#### 2.1.2.1 Space-Time Predictor Step

We introduce the element local space-time predictor solution as

$$\mathbf{q}_h^e(\mathbf{x},t) = \sum_k \psi_k(\mathbf{\xi},\tau) \widetilde{\mathbf{q}}_k^e$$
 (2.10)

to represent the predictor solution of our space-time element. We note that  $q_h^e(x, t^n) = U_h^e(x)$ . The set of basis functions  $\{\psi_k\}_{k=1,\dots,N_b^{st}}$  are constructed using tensor products of the one dimensional basis (here chosen to be Lagrange polynomials). To solve for this local discrete solution, we require  $q_h^e$  to satisfy Eq. (2.9). Therefore, our equation governing the predicted solution is as follows

$$\int_{t_n}^{t_{n+1}} \int_{\Omega_e} \psi_k \partial_t \mathbf{q}_h^e d\Omega dt + \int_{t_n}^{t_{n+1}} \int_{\Omega_e} \psi_k \nabla \cdot \mathbf{F}(\mathbf{q}_h^e) d\Omega dt = \int_{t_n}^{t_{n+1}} \int_{\Omega_e} \psi_k \mathbf{S}(\mathbf{q}_h^e) d\Omega dt \ \forall \ \psi_k.$$
 (2.11)

At this point, rather than integrating the convective flux term by parts, we instead integrate the first term in Eq. (2.11) by parts. This leads to

$$\int_{\Omega_{e}} \psi_{k} \boldsymbol{q}_{h}^{e} d\Omega|_{t_{n+1}} - \int_{\Omega_{e}} \psi_{k} \boldsymbol{U}_{h}^{e} d\Omega|_{t_{n}} - \int_{t_{n}}^{t_{n+1}} \int_{\Omega_{e}} \frac{\partial \psi_{k}}{\partial t} \boldsymbol{q}_{h}^{e} d\Omega dt + \int_{t_{n}}^{t_{n+1}} \int_{\Omega_{e}} \psi_{k} \nabla \cdot \boldsymbol{F}(\boldsymbol{q}_{h}^{e}) d\Omega dt = \int_{t_{n}}^{t_{n+1}} \int_{\Omega_{e}} \psi_{k} \boldsymbol{S}(\boldsymbol{q}_{h}^{e}) d\Omega dt \tag{2.12}$$

The first two terms in Eq. (2.12) can be thought of as an upwind temporal flux where the solution  $U_h^e(x,t_n)$  is known. Next, the polynomial representations of  $q_h^e$  and  $U_h^e$  are substituted into Eq. (2.12) and we recast our integrals in reference space. We define our reference coordinates in space-time to be  $\xi$ ,  $\tau$  respectively where  $-1 \le \xi \le 1$  and  $-1 \le \tau \le 1$  and  $\Omega_e^{st} \in \mathbb{R}^{N_d+1}$ . Changing to reference space gives us

$$\int_{\boldsymbol{\xi}} \psi_{k} \psi_{l} d\boldsymbol{\xi} \widetilde{\boldsymbol{q}}_{l}^{e}|_{\tau=1} - \int_{\boldsymbol{\xi}} \psi_{k} \phi_{m} d\boldsymbol{\xi} \widetilde{\boldsymbol{U}}_{m}^{e}|_{\tau=-1} - \int_{-1}^{1} \int_{\boldsymbol{\xi}} \frac{\partial \psi_{k}}{\partial \tau} \psi_{l} d\boldsymbol{\xi} d\tau \widetilde{\boldsymbol{q}}_{l}^{e} 
+ \frac{\Delta t}{2} \int_{-1}^{1} \int_{\boldsymbol{\xi}} \psi_{k} \nabla_{\boldsymbol{\xi}} \cdot \boldsymbol{F}(\psi_{l} \widetilde{\boldsymbol{q}}_{l}^{e}) \boldsymbol{J}_{e}^{-T} d\boldsymbol{\xi} d\tau = \frac{\Delta t}{2} \int_{-1}^{1} \int_{\boldsymbol{\xi}} \psi_{k} \boldsymbol{S}(\psi_{l} \widetilde{\boldsymbol{q}}_{l}^{e}) d\boldsymbol{\xi} d\tau,$$
(2.13)

where, for brevity, we rely on index notation to imply summing over repeated indices.  $J_e$  is the geometric Jacobian for  $\Omega_e$ , which will be further described in Section 2.2.

We choose to represent the flux and source terms as polynomials with the same form as in Eq. (2.10).

$$\mathcal{F}_h^{*e}(\boldsymbol{\xi}, \tau) = \sum_k \psi_k(\boldsymbol{\xi}, \tau) F_k^{*e}$$
(2.14)

$$\boldsymbol{\mathcal{S}}_{h}^{*e}(\boldsymbol{\xi},\tau) = \sum_{k} \psi_{k}(\boldsymbol{\xi},\tau) \boldsymbol{S}_{k}^{*e}$$
(2.15)

where  $F^* = F \frac{\Delta t}{2}$  and  $S^* = S \frac{\Delta t}{2}$ . This then leads to the following equation for  $\widetilde{q}_h^e$ .

$$\underbrace{\left(\int_{\boldsymbol{\xi}} \psi_{k} \psi_{l} d\boldsymbol{\xi}|_{\tau=1} - \int_{-1}^{1} \int_{\boldsymbol{\xi}} \frac{\partial \psi_{k}}{\partial \tau} \psi_{l} d\boldsymbol{\xi} d\tau\right)}_{\boldsymbol{K}} \widetilde{\boldsymbol{q}}_{l}^{e} = \underbrace{\int_{\boldsymbol{\xi}} \psi_{k} \phi_{m} d\boldsymbol{\xi}|_{\tau=-1}}_{\boldsymbol{F}_{o}} \widetilde{\boldsymbol{U}}_{m}^{e} \\
- \underbrace{\int_{-1}^{1} \int_{\boldsymbol{\xi}} \psi_{k} \nabla_{\boldsymbol{x}} \psi_{l} d\boldsymbol{\xi} d\tau}_{\boldsymbol{K}^{e}} \cdot \boldsymbol{\mathcal{F}}_{h}^{*e} + \underbrace{\int_{-1}^{1} \int_{\boldsymbol{\xi}} \psi_{k} \psi_{l} d\boldsymbol{\xi} d\tau}_{\boldsymbol{M}^{st}} \boldsymbol{\mathcal{S}}_{h}^{*e} \tag{2.16}$$

This is a local non-linear equation for the predicted solution vector in space-time that requires no knowledge of any neighboring elements. We solve this system using a fixed-point Picard iteration approach where

$$\widetilde{\boldsymbol{q}}_{l}^{n+1} = \boldsymbol{K}^{-1} \left( \boldsymbol{F}_{o} \boldsymbol{U}_{m}^{e} - \boldsymbol{K}_{x}^{e} \boldsymbol{\mathcal{F}}_{l}^{*e}(\widetilde{\boldsymbol{q}}_{l}^{n}) + \boldsymbol{M}^{st} \boldsymbol{\mathcal{S}}_{l}^{*e}(\widetilde{\boldsymbol{q}}_{l}^{n}) \right)$$

$$(2.17)$$

In the case of stiff source terms, Eq. (2.17) is not entirely sufficient. To account for the stiffness, we take the source term coefficients implicitly such that

$$\widetilde{\boldsymbol{q}}_{l}^{n+1} - \boldsymbol{K}^{-1} \boldsymbol{M}^{st} \boldsymbol{\mathcal{S}}_{l}^{*e}(\widetilde{\boldsymbol{q}}_{l}^{n+1}) = \boldsymbol{K}^{-1} \left( \boldsymbol{F}_{o} \widetilde{\boldsymbol{U}}_{m}^{e} - \boldsymbol{K}_{\boldsymbol{x}}^{e} \boldsymbol{\mathcal{F}}_{l}^{*e}(\widetilde{\boldsymbol{q}}_{l}^{n}) \right). \tag{2.18}$$

The source term is then represented using a simple linearization:

$$\boldsymbol{\mathcal{S}}_{l}^{*e,n+1} \approx \boldsymbol{\mathcal{S}}_{l}^{*e,n} + \Delta t \left( \widetilde{\boldsymbol{q}}_{l}^{n+1} - \widetilde{\boldsymbol{q}}_{l}^{n} \right) \left( \frac{\partial \boldsymbol{S}}{\partial \boldsymbol{U}} \right) \Big|_{\bar{\boldsymbol{U}}}^{T}$$
(2.19)

After substituting Eq. (2.19) into Eq. (2.18) we can cast the iterative approach in the following way

$$\underbrace{\left(\frac{(\boldsymbol{M}^{st})^{-1}\boldsymbol{K}}{\Delta t}\right)}_{\boldsymbol{A}} \widetilde{\boldsymbol{q}}_{l}^{n+1} + \widetilde{\boldsymbol{q}}_{l}^{n+1} \underbrace{\left(-\frac{\partial \boldsymbol{S}}{\partial \boldsymbol{U}}\right)\Big|_{\bar{\boldsymbol{U}}}^{T}}_{\boldsymbol{B}} = \underbrace{\frac{1}{\Delta t} \boldsymbol{\mathcal{S}}_{l}^{*e,n} - \widetilde{\boldsymbol{q}}_{l}^{n} \left(\frac{\partial \boldsymbol{S}}{\partial \boldsymbol{U}}\right)\Big|_{\bar{\boldsymbol{U}}}^{T} + \underbrace{\frac{(\boldsymbol{M}^{st})^{-1}}{\Delta t} \left(\boldsymbol{F}_{o} \widetilde{\boldsymbol{U}}_{m}^{e} - \boldsymbol{K}_{x}^{e} \boldsymbol{\mathcal{F}}_{l}^{*e} (\widetilde{\boldsymbol{q}}_{l}^{n})\right)}_{\boldsymbol{C}} \quad (2.20)$$

In this form, our local nonlinear solver is known as the Sylvester equation, which we solve iteratively [4].

#### 2.1.2.2 Space-Time Correction Step

The polynomial representation of the space-time solution vector is then substituted into Eq. (2.9) followed by integration by parts of the flux function's term. Therefore, our correction step becomes

$$\left(\int_{\Omega_{e}} \phi_{m} \phi_{k} d\Omega\right) \left(\tilde{\boldsymbol{U}}_{m}^{e,n+1} - \tilde{\boldsymbol{U}}_{m}^{e,n}\right) - \int_{t_{n}}^{t_{n+1}} \int_{\Omega_{e}} \nabla \phi_{m} \cdot \boldsymbol{F}(\boldsymbol{q}_{h}^{e}) d\Omega dt + \int_{t_{n}}^{t_{n+1}} \oint_{\partial \Omega_{e}} \phi_{m} \widehat{\boldsymbol{F}}(\boldsymbol{q}_{h}^{e+}, \boldsymbol{q}_{h}^{e-}, \widehat{\boldsymbol{n}}) d\Gamma dt = \int_{t_{n}}^{t_{n+1}} \int_{\Omega_{e}} \phi_{m} \boldsymbol{S}(\boldsymbol{q}_{h}^{e}) d\Omega dt$$
(2.21)

Combining Eq. (2.6) and Eq. (2.21) we have:

$$\sum_{n=1}^{N_b} d_t \widetilde{\boldsymbol{U}}_n^e(t) M_{mn}^e = \boldsymbol{R}_m = \int_{t_n}^{t_{n+1}} \int_{\Omega_e} \nabla \phi_m \cdot \boldsymbol{F}(\boldsymbol{q}_h^e) d\Omega dt - \int_{t_n}^{t_{n+1}} \oint_{\partial \Omega_e} \phi_m \widehat{\boldsymbol{F}}(\boldsymbol{q}_h^{e+}, \boldsymbol{q}_h^{e-}, \widehat{\boldsymbol{n}}) d\Gamma dt + \int_{t_n}^{t_{n+1}} \int_{\Omega_e} \phi_m \boldsymbol{S}(\boldsymbol{q}_h^e) d\Omega dt$$
(2.22)

Here, the jump conditions between element neighbors are taken into consideration via a numerical flux function. The current version of Quail only supports one-dimensional problems for ADER-DG.

### 2.2 Geometric mapping

In order to simplify operations such as interpolation and numerical integration, elements and faces are mapped to reference space. In this section, we provide details on these mappings for 2D elements.

#### 2.2.1 Element mapping

The mapping  $x: \widehat{\Omega} \to \Omega_e$ , with  $\widehat{\Omega}$  denoting the reference element, is given as

$$x(\xi, \eta) = \sum_{i=1}^{N_n} \psi_i(\xi, \eta) x_i^e,$$
 (2.23a)

$$y(\xi, \eta) = \sum_{i=1}^{N_n} \psi_i(\xi, \eta) y_i^e,$$
 (2.23b)

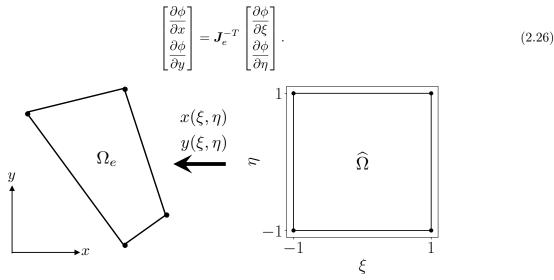
where  $\xi$  and  $\eta$  are the reference space coordinates,  $N_n$  is the number of nodes defining the element geometry,  $\psi_i$  is the *i*th basis function for the geometry interpolation, and  $(x_i^e, y_i^e)$  is the physical position of the *i*th node. Standard Lagrange basis polynomials are chosen for  $\{\psi_i\}$ . Note that the basis functions and polynomial order for solution and geometry approximation can be different. Figure 2.1 shows the geometric mapping for a q=1 quadrilateral and a q=2 triangle, where q refers to the order of the geometry interpolation. The reference element for quadrilaterals is a square with a side length of two, and that for triangles is an isosceles right triangle with unity leg length. In 1D, the reference element is simply a line segment of length two. The geometric Jacobian is given by

$$\mathbf{J}_{e} = \begin{bmatrix} \frac{\partial x(\xi, \eta)}{\partial \xi} & \frac{\partial x(\xi, \eta)}{\partial \eta} \\ \frac{\partial y(\xi, \eta)}{\partial \xi} & \frac{\partial y(\xi, \eta)}{\partial \eta} \end{bmatrix},$$
(2.24)

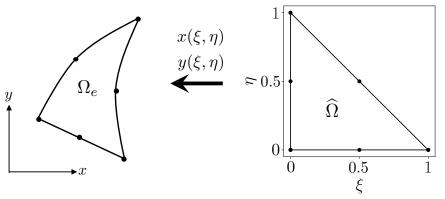
which can be used to "switch" between reference and physical space when computing gradients. Specifically,

$$\begin{bmatrix} \frac{\partial \phi}{\partial \xi} \\ \frac{\partial \phi}{\partial \eta} \end{bmatrix} = \begin{bmatrix} \frac{\partial x(\xi, \eta)}{\partial \xi} & \frac{\partial x(\xi, \eta)}{\partial \eta} \\ \frac{\partial y(\xi, \eta)}{\partial \xi} & \frac{\partial y(\xi, \eta)}{\partial \eta} \end{bmatrix} \begin{bmatrix} \frac{\partial \phi}{\partial x} \\ \frac{\partial \phi}{\partial y} \end{bmatrix} = \boldsymbol{J}_e^T \begin{bmatrix} \frac{\partial \phi}{\partial x} \\ \frac{\partial \phi}{\partial y} \end{bmatrix}, \tag{2.25}$$

and



(a) Geometric mapping for q = 1 quadrilateral elements



(b) Geometric mapping for q = 2 triangular elements

Figure 2.1: Geometric mapping for (a) q=1 quadrilateral elements and (b) q=2 triangular elements.

#### 2.2.2 Face mapping

Here, we focus on the *i*th face,  $\Gamma_i^e$ , of the element boundary,  $\partial \Omega_e$ , where

$$\partial\Omega_e = \bigcup_{i=1}^{N_f} \Gamma_i^e, \tag{2.27}$$

where  $N_f$  is the number of faces comprising the element boundary. The mapping  $\boldsymbol{x}: \widehat{\Gamma} \to \Gamma_i^e$ , with  $\widehat{\Gamma}$  denoting the reference face, is given as

$$x(\zeta) = \sum_{j=1}^{q+1} \Psi_j(\zeta) x_j^{e,i},$$
 (2.28a)

$$y(\zeta) = \sum_{j=1}^{q+1} \Psi_j(\zeta) y_j^{e,i},$$
 (2.28b)

where  $\zeta$  is the reference coordinate,  $\Psi_j$  is the jth basis function for the face geometry interpolation, and  $(x_j^{e,i}, y_j^{e,i})$  is the physical position of the jth node of the ith face. 1D Lagrange basis polynomials are chosen for  $\{\Psi_j\}$ , which are of the same type and order as those for the geometry interpolation of the element (Eq. (2.23)). Figure 2.2 shows the geometric mapping for a q=2 element.

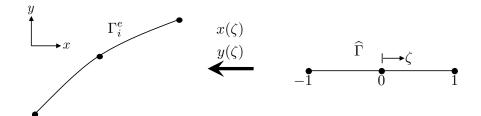


Figure 2.2: Geometric mapping for (a) q = 1 quadrilateral elements and (b) q = 2 triangular elements.

The outward-facing (unnormalized) normal vector is given as

$$\boldsymbol{n} = \frac{dy}{d\zeta}\hat{\boldsymbol{e}}_x - \frac{dx}{d\zeta}\hat{\boldsymbol{e}}_y. \tag{2.29}$$

The unit normal vector can then be computed as

$$\widehat{\boldsymbol{n}} = \frac{\boldsymbol{n}}{|\boldsymbol{n}|}.\tag{2.30}$$

### 2.3 Numerical integration

The integrals in the previous section are evaluated using numerical quadrature. For details on the available quadrature types, see general.QuadratureType in src and src/numerics/quadrature. To simplify integral evaluation, quadrature is performed in reference space (see Section 2.2). An example of using numerical quadrature to evaluate volume integrals is as follows:

$$\int_{\Omega_e} f(\mathbf{x}) d\Omega \approx \sum_{k=1}^{N_q} f(\mathbf{x}_k) \mathbf{j}(\boldsymbol{\xi}_k) w_k, \tag{2.31}$$

where  $N_q$  is the number of quadrature points,  $w_k$  is the kth quadrature weight, and  $\boldsymbol{x}_k = \boldsymbol{x}(\boldsymbol{\xi}_k)$  and  $\boldsymbol{\xi}_k$  are the coordinates of the kth quadrature point in physical space and reference space, respectively. j is the determinant of the geometric Jacobian. An example of using numerical quadrature to evaluate surface integrals is as follows:

$$\oint_{\Gamma_i^e} g(\mathbf{x}) d\Gamma \approx \sum_{k=1}^{N_q} g(\mathbf{x}_k) |\mathbf{n}(\boldsymbol{\xi}_k)| w_k.$$
(2.32)

Note that the number of quadrature points for the surface integral is typically different from that for the volume integral; however, for simplicity, we continue to use  $N_q$  to denote the number of quadrature points.

#### 2.4 Matrix Form of the DG discretization

This section recasts the DG spatial discretization from Section 2.1.1 in matrix form, which facilitates code implementation. Here, we use matrix as a general term to indicate an array of arbitrary dimensions. For convenience, we adopt the subscript notation employed by the explicit mode of the Numpy function einsum, which is used extensively in Quail. This notation is not exactly the same as Einstein notation in that repeated indices do not necessarily denote summation. For example, suppose there are two matrices,  $[A]_{ijk}$  and  $[B]_{jkl}$ . The operation

$$[A]_{ijk}[B]_{ikl} \to [C]_{ikl} \tag{2.33}$$

indicates summation over the j index and entrywise multiplication over the k index.

The first term is the flux volume integral given by

$$\int_{\Omega_e} \nabla \phi_m \cdot \boldsymbol{F}(\boldsymbol{U}_h^e) d\Omega. \tag{2.34}$$

Since  $\phi_m$  is a scalar, then  $\nabla \phi_m$  is a vector of size  $N_d$ , and its matrix form is indexed as  $[\nabla \phi_m]_l$ .  $F(U_h^e)$  is the flux of each state variable in every direction, so it has shape  $N_s \times N_d$ . The matrix form of the flux will be referred to

as [F] and is indexed as  $[F]_{kl}$ . The dot product between these two quantities is computed along spatial directions, which yields

$$[\nabla \phi_m]_l[F]_{kl} \to k. \tag{2.35}$$

If this operation is performed for all basis functions, then the basis gradient matrix now has shape  $[\nabla \phi]_{nl}$ , so the operation becomes  $nl, kl \to nk$ . This operation is performed for every element and at every quadrature point, so evaluating the gradient of the basis at these points gives

$$[\nabla \phi]_{ijnl}^e[F]_{ijkl} \to ijnk.$$
 (2.36)

Performing numerical quadrature to evaluate the integral involves multiplying by the Jacobian determinant, j, for each element and quadrature point, as well as the quadrature weight w for the jth quadrature point, then summing over quadrature points. This results in

$$\int_{\Omega_e} \nabla \phi \cdot \mathbf{F}(\mathbf{U}_h^e) d\Omega \approx [\nabla \phi]_{ijnl}^e [F]_{ijkl} [\mathbf{j}]_{ij} [w]_j \to ink.$$
(2.37)

The next term is the surface flux integral given by

$$\oint_{\partial\Omega_e} \phi \widehat{F}(U_h^{e+}, U_h^{e-}, \widehat{n}) d\Gamma.$$
(2.38)

Let  $[\widehat{F}]$  denote the matrix form of the numerical flux function. This is evaluated at every element and quadrature point and produces a result of size  $N_e \times N_q \times N_s$ , yielding  $[\widehat{F}]_{ijk}$ . Note that unlike the analytic flux, F, the numerical flux as denoted here is only in the direction normal to the face, so there is no l index for the spatial directions. Additionally, the number of quadrature points for the surface integral is typically different from that for the volume integral; however, for simplicity, we continue to use  $N_q$  and j to denote the number of and index for quadrature points, respectively. The basis function matrix has the same shape as its gradient without the dimensional index, i.e.  $[\phi]_{ijn}^f$ . The integrand then becomes

$$[\phi]_{ijn}^f[\widehat{F}]_{ijk} \to ijnk \tag{2.39}$$

Performing quadrature, the integrand is multiplied by  $[|n|]_i[w]_j$  and summed over the j quadrature points as

$$\oint_{\partial\Omega_e} \phi \widehat{F}(U_h^{e+}, U_h^{e-}, \widehat{n}) d\Gamma \approx [\phi]_{ijn} [\widehat{F}]_{ijk} [|n|]_j [w]_j \to ink$$
(2.40)

The final term is the source term integral given by

$$\int_{\Omega} \phi_m \mathbf{S}(\mathbf{U}_h^e) d\Omega \tag{2.41}$$

The matrix form of the source term is represented as [S]. With one source term per state variable (k), evaluated at each element (i) and quadrature point (j), this results in  $[S]_{ijk}$ . As before, the basis function matrix is  $[\phi]_{ijn}$ , and quadrature is performed by multiplying by  $[j]_i[w]_j$  and summing over the j quadrature points. This yields

$$\int_{\Omega_e} \phi_m \mathbf{S}(\mathbf{U}_h^e) d\Omega \approx [\phi]_{ijn}^e [S]_{ijk} [\mathbf{j}]_j [w]_j \to ink$$
(2.42)

The final matrix form of the residual (Eq. (2.8)),  $[R]_{ink}$ , is given by

$$[R]_{ink} = [\nabla \phi]_{ijnl}^e [F]_{ijkl} [j]_j [w]_j - [\phi]_{ijn}^f [\widehat{F}]_{ijk} [|\mathbf{n}|]_j [w]_j + [\phi]_{ijn}^e [S]_{ijk} [j]_j [w]_j \to ink.$$
 (2.43)

A summary of each index is given below:

- i: elements  $(N_e)$
- j: quadrature points  $(N_q)$
- k: state variables  $(N_s)$
- l: spatial directions  $(N_d)$
- n: basis functions  $(N_b)$

### 2.5 Temporal discretization

QUAIL has two primary approaches for time integration: fully explicit schemes and operator splitting (typically for handling stiff source terms). These are briefly described in the Sections 2.5.1 and 2.5.2 with relevant references. Further details can be found by referencing general. StepperType in src.

#### 2.5.1 Time stepping schemes

#### 2.5.1.1 Forward Euler

The forward Euler scheme is a standard first-order explicit scheme.

#### 2.5.1.2 Fourth-Order Runge-Kutta Scheme (RK4)

The RK4 scheme is a standard four-stage, fourth-order scheme. An example of this method can be found in the text by Hesthaven and Warburton [1].

#### 2.5.1.3 Low Storage Fourth-Order Runge-Kutta Scheme (LSRK4)

The LSRK4 scheme is a fourth-order RK scheme that minimizes storage requirements. For more details, see Carpenter and Kennedy [5].

#### 2.5.1.4 Strong Stability Preserving Third-Order Runge-Kutta Scheme (SSPRK3)

The SSPRK3 scheme employed here is a total-variation-diminishing, low-storage third-order scheme first presented by Spiteri et al. [6]

#### 2.5.1.5 ADER Space-Time Discretization

The ADER-DG scheme uses a predictor-corrector type method for advancing in time. Details of the ADER-DG scheme are found in section 2.1.2.

#### 2.5.2 Operator splitting

Operator splitting schemes are often used when a stiff source term significantly restricts the time step selection of an explicit scheme. In these methods, we typically use an implicit scheme for the source term. In QUAIL, we currently have a simple backwards difference scheme (BDF1) and the Trapezoidal method (see general.SourceStepperType in src).

#### 2.5.2.1 Strang Splitting

This is a common second-order splitting technique first proposed by Strang in 1968 where interchanging the order of your split method leverages the advantage of symmetry in the system [7]. For example, consider the advection-reaction system:

$$\frac{d}{dt}U = \mathcal{T}(U) + S(U) \tag{2.44}$$

where  $\mathcal{T} = \nabla \cdot \mathbf{F}$  and  $\mathbf{S}$  is composed of the source term operators.

This system is naturally split by the physics so it is advantageous to use operator splitting. Following the Strang procedure we have the following operations:

$$d_t U^{(1)} = \mathcal{T}(U^{(1)}), \quad U^{(1)}(t_n) = U_n$$
 (2.45)

$$d_t U^{(2)} = S(U^{(2)}), \quad U^{(2)}(t_n) = U^1(t_n + \Delta t/2)$$
 (2.46)

$$d_t U^{(3)} = \mathcal{T}(U^{(3)}), \quad U^{(3)}(t_n + \Delta t/2) = U^2(t_n + \Delta t)$$
 (2.47)

$$U_{n+1} = U^{(3)}(t_n + \Delta t) \tag{2.48}$$

This method is second-order-accurate and strongly stable.

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#### 2.5.2.2 Simpler balanced splitting

In simpler balanced splitting, first proposed by Wu et al. [8], stores a vector as:

$$c_n = -\mathcal{T}(U_n) \tag{2.49}$$

From this definition, it is actually possible to reduce the amount of operations due to the first step being in equilibrium. Therefore, the system proceeds as:

$$d_t U^{(1)} = S(U^{(1)}) - c_n, \quad U^{(1)}(t_n) = U_n$$
(2.50)

$$d_t U^{(2)} = \mathcal{T}(U^{(2)}) + c_n, \quad U^{(2)}(t_n + \Delta t/2) = U^1(t_n + \Delta t)$$
 (2.51)

$$U_{n+1} = U^{(2)}(t_n + \Delta t) \tag{2.52}$$

### 2.6 Physics

#### 2.6.1 Boundary conditions

In QUAIL, boundary conditions (BCs) are treated with, adopting the terminology introduced by Mengaldo et al. [9], either a weak-prescribed or weak-Riemann approach. In the former, the boundary flux in the surface integral (second term on RHS of Eq. 2.7) is computed using the analytic flux,  $\mathbf{F}$ , instead of the numerical flux.  $\mathbf{U}_h^b$  denotes the prescribed boundary state used to calculate  $\mathbf{F}$ . The surface integral at a given boundary face,  $\Gamma_b$ , for the convective flux is then written as

$$\boldsymbol{B}^{b} = \oint_{\Gamma_{b}} \phi_{m} \boldsymbol{F}(\boldsymbol{U}_{h}^{b}) \cdot \hat{\boldsymbol{n}} d\Gamma. \tag{2.53}$$

In the weak-Riemann approach, the boundary flux is computed using the numerical flux, giving

$$\boldsymbol{B}^{b} = \int_{\Gamma_{b}} \phi_{m} \widehat{\boldsymbol{F}}(\boldsymbol{U}_{h}^{e+}, \boldsymbol{U}_{h}^{b}, \widehat{\boldsymbol{n}}) d\Gamma.$$
(2.54)

Two BCs that are applicable to all available equation sets are the StateAll and Extrapolate BCs. The former employs a weak-Riemann approach, with  $\boldsymbol{U}_h^b$  fully prescribed by an analytical expression. The latter uses a weak-prescribed approach, with  $\boldsymbol{U}_h^b = \boldsymbol{U}_h^{e+}$ . The Extrapolate BC is useful for boundaries with no incoming characteristics (such as supersonic outflow when solving the Euler equations). Other BCs specific to certain equation sets are described below.

#### 2.6.2 Equation sets

In this section, we describe the various equation sets available in QUAIL. See general. Physics Type in src and src/physics for more information. Only the basic equations are provided (without any source terms). For information regarding the available source terms, refer to functions. SourceType in each respective physics module.

#### Scalar advection

The scalar advection equation is given as

$$\frac{\partial u}{\partial t} + \nabla \cdot (cu) = 0, \tag{2.55}$$

where c is the advection velocity (currently assumed constant in QUAIL).

#### 1D Burgers equation

The 1D inviscid Burgers equation takes the following form:

$$\frac{\partial u}{\partial t} + \nabla \cdot \left(\frac{1}{2}u^2\right) = 0. \tag{2.56}$$

This equation is nonlinear and often used as a model problem for more complicated conservation laws that can involve discontinuities.

#### **Euler equations**

The compressible Euler equations models continuum fluid flow without viscous effects. Assuming a calorically perfect gas, the state variables and inviscid flux are written as

$$\boldsymbol{U} = \begin{bmatrix} \rho \\ \rho \boldsymbol{u} \\ \rho E \end{bmatrix}, \quad \boldsymbol{F} = \begin{bmatrix} \rho \boldsymbol{u} \\ \rho \boldsymbol{u} \otimes \boldsymbol{u} + P \mathbb{I} \\ \boldsymbol{u}(\rho E + P) \end{bmatrix}, \tag{2.57}$$

where  $\rho$  is the fluid density,  $\boldsymbol{u}$  is the velocity vector, P is the pressure,  $\mathbb{I}$  is the identity matrix, and  $E = R_g/(\gamma - 1)T + \frac{1}{2}|\boldsymbol{u}|^2$  is the total energy per unit mass (with  $R_g$  denoting the specific gas constant,  $\gamma$  the specific heat ratio, and T the temperature). Pressure is computed from the ideal gas law,  $P = \rho R_g T$ .

Two boundary conditions for this equation set available in QUAIL are the SlipWall and PressureOutlet. The SlipWall BC uses a weak-prescribed approach, with

$$\boldsymbol{U}_{h}^{b} = \begin{bmatrix} \rho^{+} \\ (\rho u)^{+} - \rho^{+} (\boldsymbol{u}^{+} \cdot \widehat{\boldsymbol{n}}^{+}) \widehat{n}_{x}^{+} \\ (\rho v)^{+} - \rho^{+} (\boldsymbol{u}^{+} \cdot \widehat{\boldsymbol{n}}^{+}) \widehat{n}_{y}^{+} \\ (\rho E)^{+} \end{bmatrix},$$

$$(2.58)$$

in 2D.

The PressureOutlet BC for subsonic outflow uses a weak-prescribed approach, with one input parameter,  $P^b$ , the outlet pressure. This BC relies on the outgoing Riemann invariant,  $J^+ = u^+ \cdot \hat{n}^+ + \frac{2a^+}{\gamma-1}$ , where a is the speed of sound. The following steps are taken to compute the boundary state:

- Calculate  $\rho^b$  by extrapolating the boundary entropy from the interior, i.e.  $s^b = s^+ = \ln \frac{P}{\rho^{\gamma}} \Big|_{U_h^+}$ , and solving for  $\rho^b$
- From  $J^+$ ,  $a^b = \sqrt{\frac{\gamma P^b}{\rho^b}}$ , and the tangential interior velocity  $\boldsymbol{u}_t^+ = \boldsymbol{u}^+ (\boldsymbol{u}^+ \cdot \hat{\boldsymbol{n}}^+) \hat{\boldsymbol{n}}^+$ , calculate the boundary velocity as

$$\boldsymbol{u}^{b} = \left(J^{+} - \frac{2a^{b}}{\gamma - 1}\right)\hat{\boldsymbol{n}}^{+} + \boldsymbol{u}_{t}^{+}$$
(2.59)

- Calculate  $(\rho \boldsymbol{u})^b$  using  $\rho^b$  and  $\boldsymbol{u}^b$
- Calculate  $(\rho E)^b$  using  $\rho^b$ ,  $\boldsymbol{u}^b$ , and  $P^b$

### 2.7 Numerical flux functions

The local Lax-Friedrichs flux function is defined as

$$\widehat{F}(U_h^{e+}, U_h^{e-}, \widehat{n}) = \frac{1}{2} \left[ \widehat{F}(U_h^{e+}) + \widehat{F}(U_h^{e-}) \right] \cdot \widehat{n} + \frac{\lambda}{2} (U_h^{e+} - U_h^{e-}), \tag{2.60}$$

where  $\lambda$  is the maximum wave speed of the system, i.e. the maximum absolute value of the eigenvalues of the flux Jacobian,  $\partial F/\partial U$ .

The Roe flux function is available in QUAIL for the Euler equations. Details on this flux function can be found in Refs. [1] and [10].

# 2.8 Limiting

The positivity-preserving limiter by Zhang and Shu [11] is available in QUAIL for the Euler equations. This limiter can guarantee positivity of density and pressure, although spurious oscillations may not be suppressed. Additional details can be found in Ref. [12].

# Using Quail

### 3.1 Running the solver

To run QUAIL, the user should add the quail script file to their \$PATH.From here, assuming an appropriate input deck, just run the driver script with the following syntax:

```
quail <input_deck>
```

The driver has a few additional options. Running quail-h results in the following output:

```
usage: quail [-h] [-p POST] [inputdeck]
```

This script is the driver for Stanford's Quail solver

```
positional arguments:
```

inputdeck this file contains all requested parameters for the

solver

optional arguments:

```
-h, --help show this help message and exit
-p POST, --post POST post-processing script to execute
```

For more information on running QUAIL, see the tutorials and example directories.

# 3.2 Post-processing

QUAIL'S solver and post-processing scripts operate separately. This allows users to run each individually or together. Each post-processing script can be quite unique. Readers are referred to the example directory for a variety of cases and options. In a typical QUAIL setup, the solver will output a pickle file (\*.pkl) that stores the state of the solver based on a set of instantiated classes. This allows the user to access the most recent state executed by the solver. Given a pickle file and a post-processing script we utilize the following command to execute post-processing:

```
quail -p <post_process_script>
```

In this script, we would unpack the pickle file and can utilize QUAIL'S built-in plotting functions (or third-party plotters) to visualize the data. A user can automatically call the post-processing script at the end of the run-time using the AutoProcess flag in the Output dictionary (see Sec. 3.3 for more details on input dictionaries). This flag is by default set True and will automatically search for a file called post\_process.py at the end of the solve. For more information on post-processing with QUAIL, see the tutorials and example directories.

Another feature of QUAIL is the option to define custom functions in separate files to perform case-specific data processing. These custom functions are run before the time loop and then once per time step. See the following directory for an illustrative example: examples/scalar/1D/damping\_sine\_wave.

### 3.3 Input deck

QUAIL input deck's utilize Python dictionaries to pass information into the solver. By using Python dictionaries, input decks can then use other Python features (e.g. numpy, sympy, ...). The major groups of dictionaries include Restart, TimeStepping, Numerics, Mesh, Physics, InitialCondition, ExactSolution, BoundaryConditions, SourceTerms, and Output.

For a detailed list of the available input parameters and appropriate syntax, users are directed to src/defaultparams.py. For more detailed information, see the tutorials and example directories.

### 3.4 Mesh generation

Two options are available in QUAIL for mesh generation. First, q=1 uniform meshes (q refers to the order of the geometry approximation) in 1D and for 2D rectangular domains can be directly generated using input parameters in the input deck. In 2D, quadrilateral and triangular elements are supported. See the example cases and src/defaultparams.py for additional information. The second option is to use GMSH [13], an open-source high-order mesh generator<sup>1</sup>. Versions 2.2 and 4.1 of MSH ASCII files can be read. Segments, triangles, and quadrilaterals are supported. Currently, only one element type per mesh is permitted. See the example cases and src/meshing/gmsh.py for details.

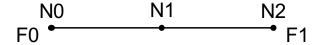
The number of nodes as a function of q for each supported element type is given in Table 3.1. The node positions for a given element are equidistant. The node ordering (N0, N1, etc.) and face ordering (F0, F1, etc.) for q = 2 line segments, triangles, and quadrilaterals are given in Figure 3.1. For q = 1 elements, only the corner vertices, i.e. principal nodes, are included. The orderings for other polynomial orders follow directly. Note that the pattern for node orderings employed in QUAIL is different from that in GMSH.

Table 3.1: Number of nodes as a function of q, the order of the geometry approximation, for each supported element type.

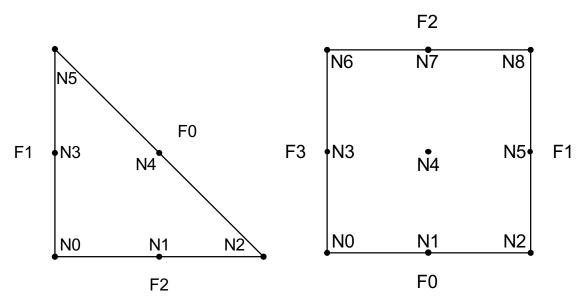
Segments Triangles Quadrilaterals 
$$q+1$$
  $\frac{(q+1)(q+2)}{2}$   $(q+1)^2$ 

<sup>&</sup>lt;sup>1</sup>See https://gmsh.info/ for downloads, documentation, and tutorials.

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(a) Node and face orderings for q=2 line segments



- (b) Node and face orderings for q=2 triangles
- (c) Node and face orderings for q=2 quadrilaterals

Figure 3.1: Node (N0, N1, etc.) and face (F0, F1, etc.) orderings for q = 2 line segments, triangles, and quadrilaterals.

# 3.5 Examples

A suite of example cases can be found in the examples directory. Below is a list of the current cases, organized by physics type and number of spatial dimensions. Additional details are found in README files in the corresponding directories.

- Scalar
  - -1D
    - \* Constant advection of a sine wave
    - \* Constant advection of a sine wave with a damping source term
    - \* Burgers equation with an initial sine wave
  - -2D
    - \* Constant advection of a Gaussian profile
- Euler
  - -1D
    - \* Smooth isentropic flow
    - \* Moving shock wave
    - \* Sod shock tube problem
    - \* Sinusoidal density wave with a stiff source term

- -2D
  - \* Isentropic vortex propagation
  - \* Inviscid Taylor-Green vortex
  - \* Subsonic flow over a cosine-shaped bump

### 3.6 Additional tools

In the tools directory are additional tools for performing dissipation and dispersion analysis and plotting basis functions. See the README file in the root QUAIL directory for more information.

# Developing QUAIL

#### 4.1 Code structure

The driver function for QUAIL is in src/quail. Other top-level modules are: src/errors.py, which contains user-defined exceptions; src/defaultparams, which contains default parameters for input decks, along with descriptions; and src/general.py, which contains constants and general Enumerations. Sub-directories in src are as follows:

- meshing, which contains modules for mesh-related classes and functions. Mesh generation tools are included here. For additional information on mesh generation, node ordering, and face ordering, see Section 3.4.
- numerics, which contains modules for basis functions, quadrature, limiters, and time stepping.
- physics, which contains modules for various equation sets and related analytic functions, boundary conditions, and numerical fluxes.
- processing, which contains modules for plotting, post-processing, and reading and writing data files.
- solver, which contains modules for various solvers (DG and ADER-DG).

# 4.2 Code style

xSome general guidelines to follow are:

- Use tabs with a length of four spaces
- Indent continued lines twice
- Limit lines to a maximum of 78 characters

For more detailed guidelines, please refer to the PEP 8 style guide for Python code<sup>1</sup>, which we largely aim to follow.

#### 4.2.1 Commenting style

The following subsections outline how functions and classes should be commented.

#### 4.2.1.1 Classes

,,,
Class: ClassName
----This class contains information about "blank"

<sup>1</sup>https://www.python.org/dev/peps/pep-0008/

Attributes:

# 4.3 Debugging

This section provides some debugging tips. Breakpoints can be set by inserting either of the following lines to the code:

- import pdb; pdb.set\_trace()
  - To continue running the code, use the continue command.
  - To exit the program, press CTRL+d or use the exit() command.
- import code; code.interact(local=locals())
  - To continue running the code, type CTRL+d
  - To exit the program, use the exit() command.

# 4.4 Glossary

Table 4.2 provides a glossary of commonly used variable names.

U, Uc	State coefficients (degrees of freedom)
Uq	State variables evaluated at a set of points (typically quadrature points)
res	Residual vector
dim	Number of dimensions
order	Order of solution approximation
gorder	Order of geometric approximation
ns	Number of state variables
ne, num_elems	Number of elements
nf	Number of faces
nbf	Number of boundary faces
nq	Number of quadrature points

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	AT 1 C 1
nq_st	Number of quadrature points in space-time
nb	Number of basis functions (per state variable)
nb_st	Number of space-time basis functions (per state variable)
quad_pts	Coordinates of quadrature points in ref. space
quad_wts	Quadrature weights
jac	Jacobian $\nabla_{\boldsymbol{\xi}} x$
ijac	Inverse of the Jacobian
djac	Determinant of the Jacobian
normals	Outward-pointing normals
basis_val	Basis value (evaluated at a set of points)
basis_ref_grad	Basis reference space gradient (evaluated at a set of points)
basis_phys_grad	Basis physical space gradient (evaluated at a set of points)
Fq	Flux evaluated at a set of points (typically quadrature points)
Sq	Source term evaluated at a set of points (typically quadrature points)
[x, y]	Coordinates in physical space
MM	Mass matrix
iMM	Inverse mass matrix
interior_face, int_face	Interior face
boundary_face, bface	Boundary face
boundary_group, bgroup	Boundary group
*L	Left quantity
*R	Right quantity
*I	Interior quantity
*B	Boundary quantity
u	Scalar (for scalar equations)
[u, v]	Velocity (for hydrodynamics)
rho	Density (for hydrodynamics)
rhou, rhov	Momentum (for hydrodynamics)
rhoE	State energy variable (for hydrodynamics)
p	Pressure (for hydrodynamics)
T	Temperature (for hydrodynamics)
gamma	Ratio of specific heats (for hydrodynamics)
R	Specific gas constant (for hydrodynamics)

Table 4.2: Glossary of variable names

# **Tutorials**

This chapter discusses video tutorials on using and developing Quail. These videos can be found on our YouTube channel at  $https://www.youtube.com/channel/UCElNsS\_mm\_0c6X41qVKBMew$ . More videos will be added soon.

### 5.1 Using QUAIL

These videos focus on using QUAIL. Please refer to the electronic version to click on the corresponding links.

- Getting Started with QUAIL
- Adding a New Physics Module

### 5.2 Developing QUAIL

These videos focus on developing QUAIL. Please refer to the electronic version to click on the corresponding links.

• Adding Initial Condition and Exact Solutions

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