

# Forces on a body with a vortex-dominated wake

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77th annual meeting of the  
APS Division of Fluid Dynamics  
Salt Lake City, UT

Nov 24, 2024

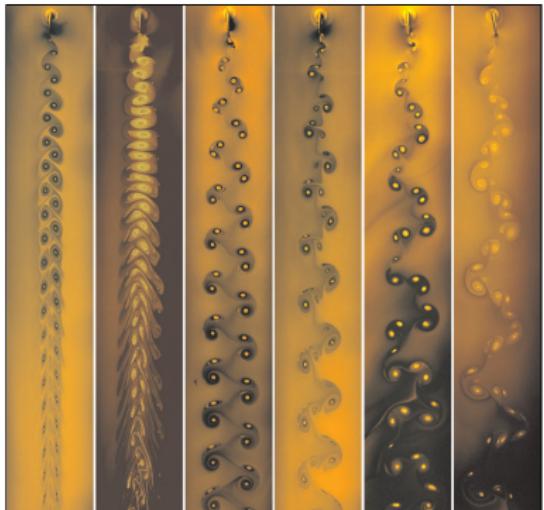
## Wakes are often dominated by vortex structures



van Dyke

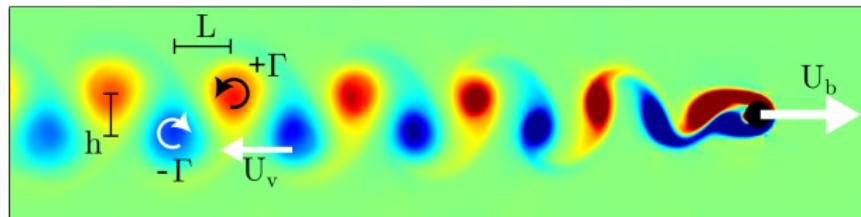


Leeward vortices in the atmosphere



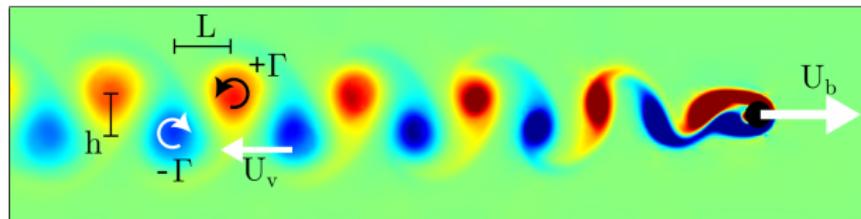
Schnipper et. al (2009)

Kármán found a way to relate the wake vortex structure to forces on the body



numerical simulation of 2D flow past a circular cylinder at low Re

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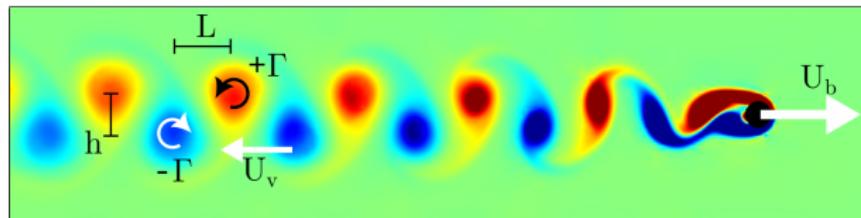


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$$F_D = \rho \Gamma \frac{h}{L} (U_b - 2U_v) + \frac{\rho \Gamma^2}{2\pi L} \quad (1)$$

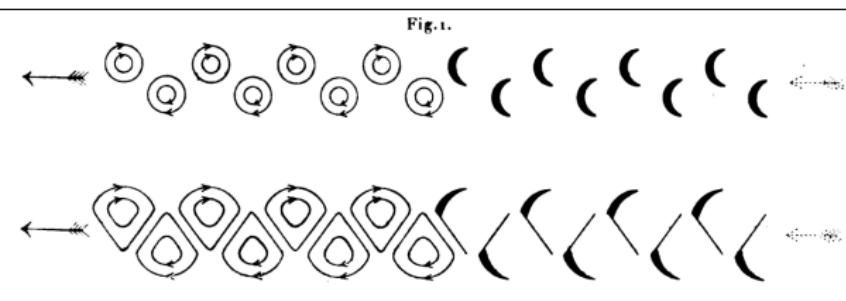
Kármán (1911)

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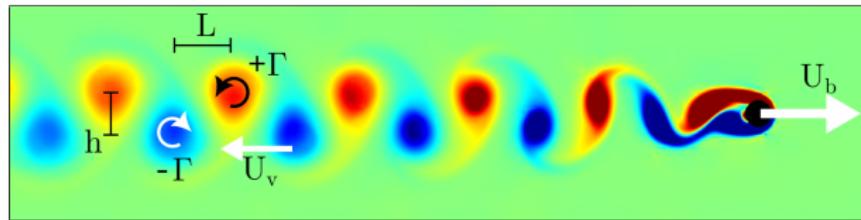
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Henri Bénard, "Formation de centres de giration à l'arrière d'un obstacle en mouvement", Comptes Rendus hebdomadaires des Séances de l'Académie des Sciences 1908

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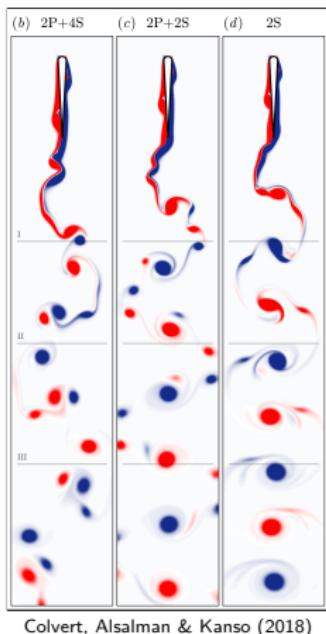
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What assumptions were made by Kármán ?

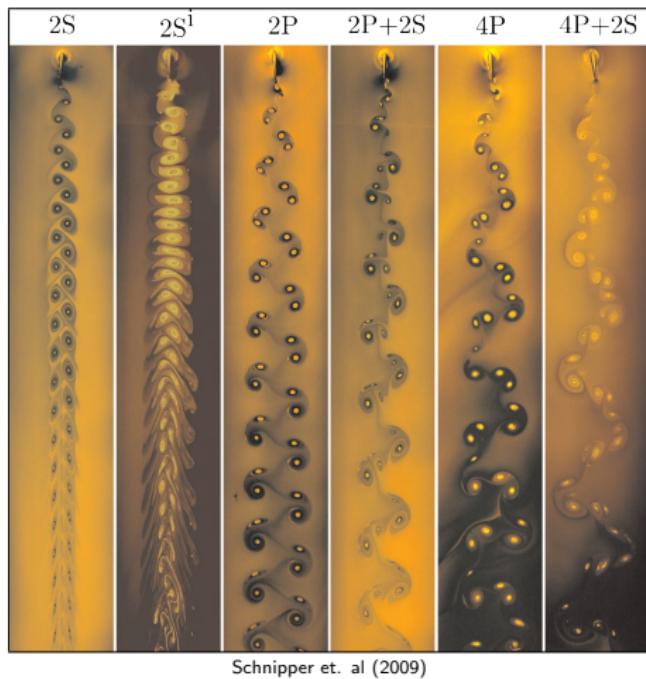
Kármán (1911)

- 2D flow
- Time-periodic flow
- Repeating vortex pattern
- $N = 2$  vortex street
- Horizontal-only motion
- Point vortices, ideal flow
- Vortices in relative equilibrium

# Can we generalize Kármán's drag law for 'exotic' vortex streets?

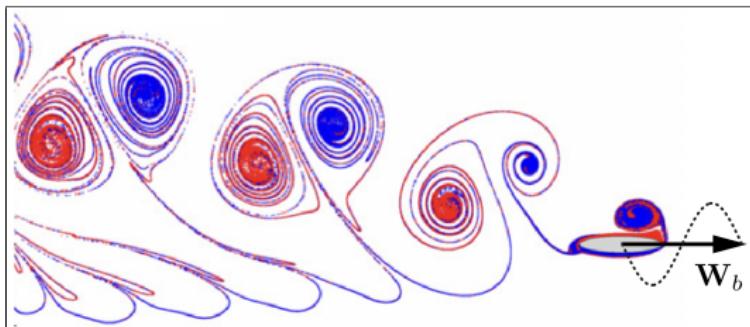


Colvert, Alsalmam & Kanso (2018)



Schnipper et. al (2009)

## Forces on a drag-producing bluff body

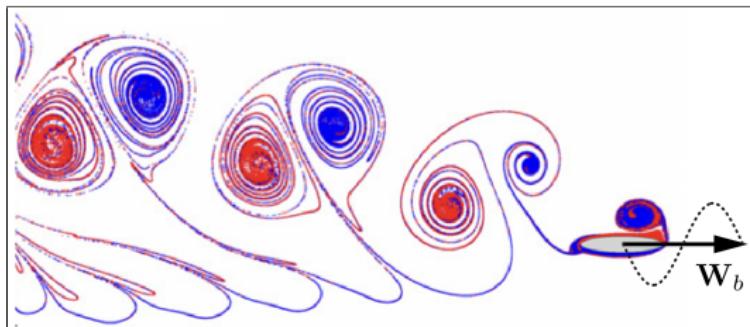


adapted from Kozlowski & Kudela (2014)

We assume:

- 2D flow
- Body moves steadily/periodically with an **average** velocity  $\mathbf{W}_b = (U_b, V_b)$
- Equal positive / negative vorticity shed into the wake
- Wake consists of vortices shed along a common axis with possible inclination
- Vortices move collectively with an **average** velocity  $\mathbf{W}_v = (U_v, V_v)$
- At this stage, point vortices need **not** be assumed

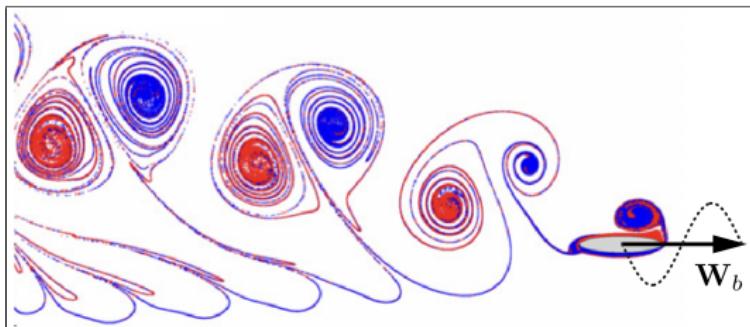
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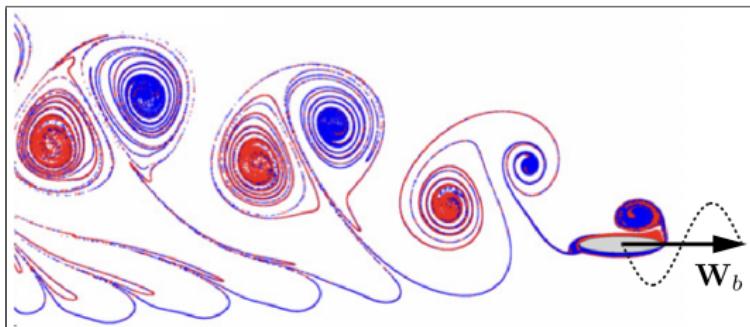


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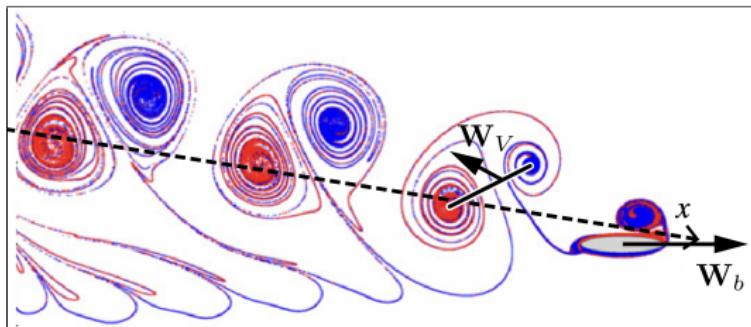
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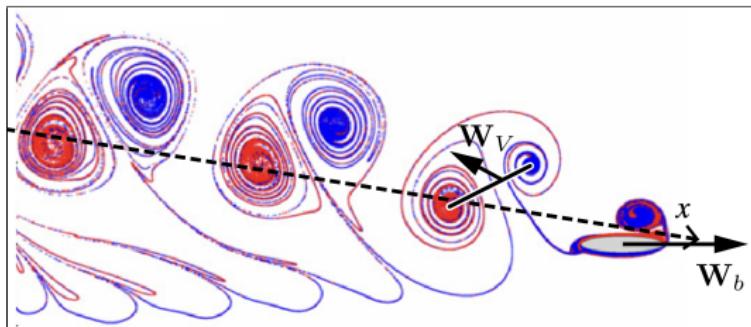
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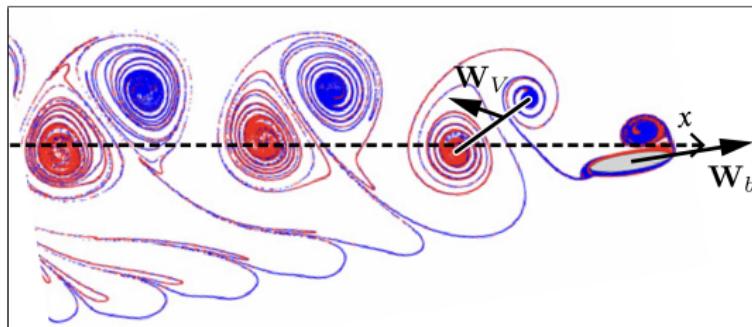


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Consider a control volume moving with the vortices



adapted from Kozlowski & Kudela (2014)

- Control volume moves with  $\mathbf{W}_v$ , the **average speed of the vortices**
- Define new variables

$$\mathbf{x}_r = (\xi, \eta) = \mathbf{x} - \mathbf{W}_v t$$

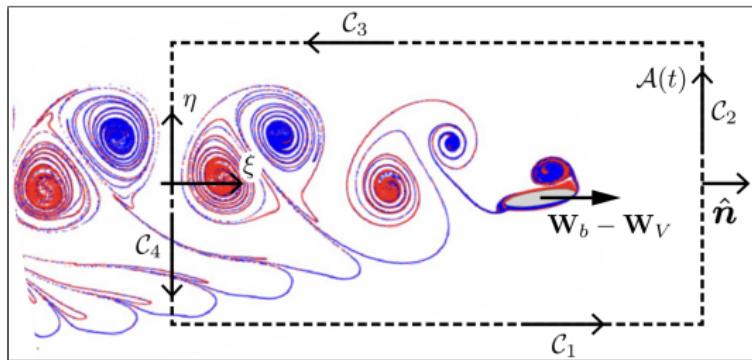
$$\zeta = \xi + i\eta = z - W_v t$$

$$\mathbf{v}_r = (u_r, v_r) = \mathbf{v} - \mathbf{W}_v$$

$$w_r = u_r - iv_r = w - W_v$$

- The body still has motion relative to the control volume
- New vortices are created over time in the interior

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## Newton's 2nd Law for the control volume (per unit depth into page)

$$\frac{D}{Dt} \int_{\text{sys}} \rho \mathbf{v} dA = \frac{\partial}{\partial t} \int_{\mathcal{A}(t)} \rho \mathbf{v} dA + \oint_{\mathcal{C}} \rho \mathbf{v} (\mathbf{v} - \mathbf{W}_v) \cdot \mathbf{n} ds = \mathbf{f}(t) \quad (2)$$

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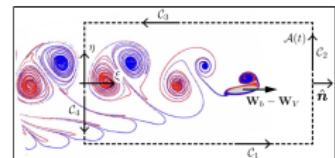
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Rate of change of linear momentum  $\mathbf{J}$  inside  $\mathcal{A}$ .

$$\mathbf{J}(t; \mathcal{A}) = (J_x, J_y) \equiv \int_{\mathcal{A}(t)} (\mathbf{v}_r + \mathbf{W}_V) dA = \mathbf{J}_r(t; \mathcal{A}) + \mathbf{W}_V A$$

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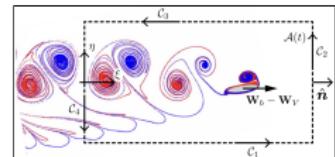
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$$\mathbf{J}_r(t; \mathcal{A}) = \underbrace{\int_{\mathcal{A}(t)} \mathbf{x}_r \times \boldsymbol{\omega}_r dA}_{\text{vortical impulse } \mathbf{I}_{\mathcal{A}}} - \underbrace{\oint_{\mathcal{C}} [\mathbf{x}_r \times (\mathbf{n} \times \mathbf{v}_r)] ds}_{\text{potential impulse } \mathbf{I}_{\mathcal{C}}}$$

$\mathbf{J}_r$  is the sum of a **vortical impulse** and a **potential impulse** — Wu et.al (2015)

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$$\frac{D}{Dt} \int_{\text{sys}} \rho v dA = \frac{\partial}{\partial t} \int_{\mathcal{A}(t)} \rho v dA + \oint_C \rho v (v - \mathbf{W}_V) \cdot n ds = f(t) \quad (2)$$



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In complex form,

$$\mathbf{I}_{\mathcal{A}}(t; \mathcal{A}) = H_{rx} + iH_{ry} = -i \int_{\mathcal{A}(t)} \zeta \boldsymbol{\omega}_r dA$$

Flow in  $\mathcal{A}$  is allowed to be rotational.

$$\mathbf{I}_C(t; \mathcal{C}) = -i \underbrace{\oint_C \phi_r d\zeta}_{\text{Let } \partial_t \text{ of this be } (*)}$$

Flow on  $\mathcal{C}$  is irrotational.

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Flux of linear momentum  $\mathbf{J}$  across the contour  $\mathcal{C}$

$$\begin{aligned} \oint_{\mathcal{C}} \rho \mathbf{v} (\mathbf{v} - \mathbf{W}_V) \cdot \mathbf{n} ds &= \rho \oint_{\mathcal{C}} \mathbf{v}_r (\mathbf{v}_r \cdot \mathbf{n}) ds + \rho \mathbf{W}_V \int_{\mathcal{A}(t)} (\nabla_r \cdot \mathbf{v}_r) dA \\ &= \rho \oint_{\mathcal{C}} \mathbf{v}_r d\psi_r, \quad \text{where } u_r = \frac{\partial \psi_r}{\partial \eta}, \quad v_r = -\frac{\partial \psi_r}{\partial \xi} \end{aligned}$$

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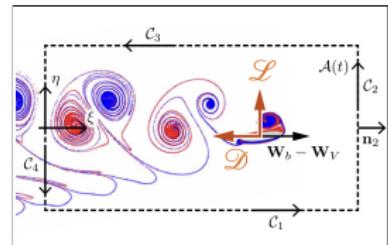
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Instantaneous external force on  $\mathcal{A}$  in complex form:

$$\mathbf{f}(t) = f_x(t) + i f_y(t) = \mathcal{D}(t) - i \mathcal{L}(t) + i \oint_C p d\zeta$$

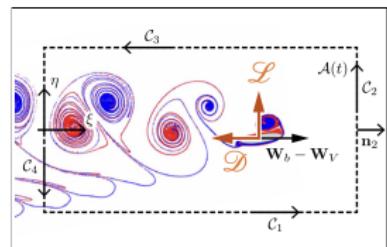


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unsteady form of Bernoulli's equation.

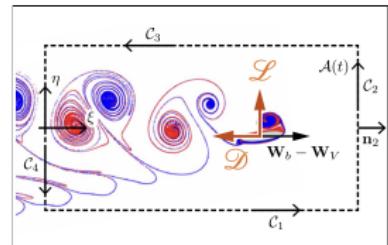
$$\begin{aligned} i \oint_C p d\zeta &= -i\rho \oint_C \frac{\partial \phi_r}{\partial t} d\zeta - i\frac{\rho}{2} \oint_C (\overline{w_r + W_V}) (w_r + W_V) d\zeta \\ &= \underbrace{\quad}_{(*)} + \oint_C (\overline{w_r + W_v})^2 d\bar{\zeta} + \rho \underbrace{\oint_C \overline{w_r} d\psi_r}_{(**)} \end{aligned}$$

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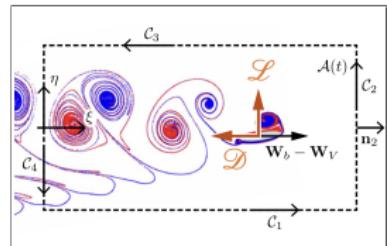
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Terms (\*) and (\*\*) appear on both sides of Newton's 2nd Law

## Putting it all together

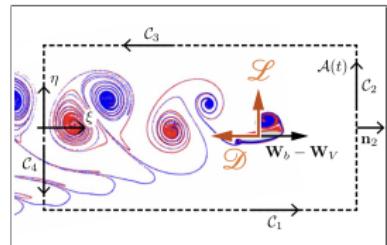
- Take the complex conjugate of Newton's 2nd Law
- Make  $\mathcal{A}$  so large that  $w_r = W_v$  on  $\mathcal{C}_1$ ,  $\mathcal{C}_2$ , and  $\mathcal{C}_3$  (but not on  $\mathcal{C}_4$ )



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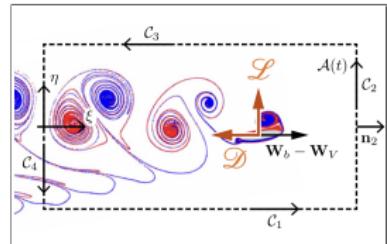
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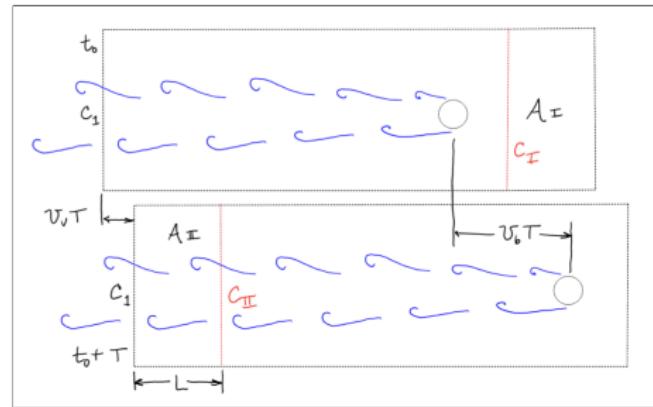
Integrate over period and divide by  $T$  to find the average forces

$$\mathcal{D} + i\mathcal{L} = \frac{1}{T} \int_{t_0}^{t_0+T} \hat{\sigma}(t) dt + \frac{\rho}{T} \underbrace{\Delta \mathbf{I}_{\mathcal{A}}}_{\substack{\text{change in vortical impulse} \\ \text{inside } \mathcal{A} \text{ over one period}}}$$



Q. How much does the vortical impulse change over one period?

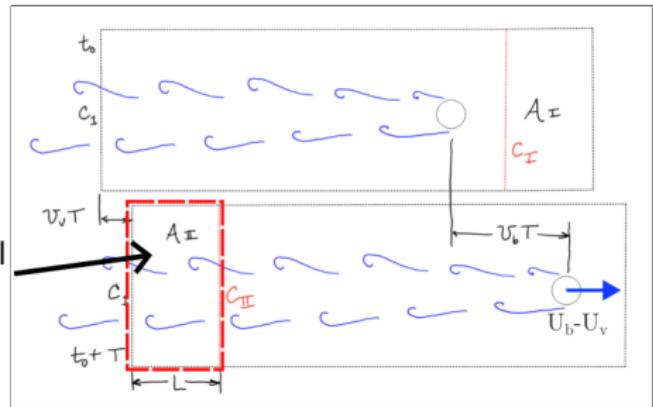
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Q. How much does the vertical impulse change over one period?

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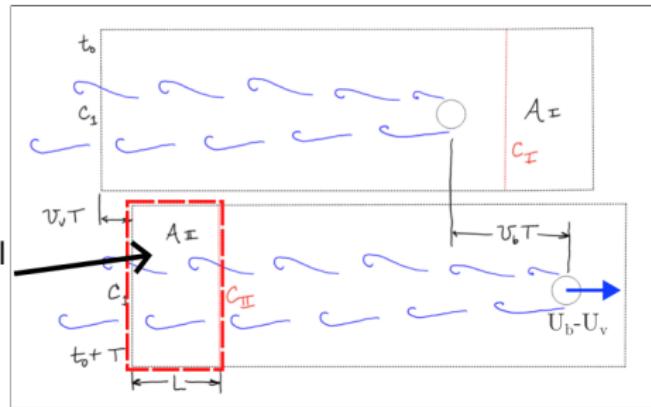
**Answer:** equal to the vertical impulse in here!



Q. How much does the vortical impulse change over one period?

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Answer: equal to the vortical impulse in here!



Also, the period  $T = \frac{L}{U_b - U_v}$ , hence we get

$$\mathcal{D} + i\mathcal{L} = \frac{1}{T} \int_{t_0}^{t_0+T} \hat{\sigma}(t) dt + \rho \left( \frac{U_b - U_v}{L} \right) \overline{\mathbf{I}_{\mathcal{A}_{II}}}$$

where  $\mathbf{I}_{\mathcal{A}_{II}} = -i \int_{\mathcal{A}_{II}} \zeta \omega_r dA$

Assuming a point-vortex description of the wake ...

For point vortices,  $\mathbf{I}_{\mathcal{A}_{II}} = P - iQ$

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if the vortices are in relative equilibrium

Also valid for finite-area vortices —  
Saffman & Schatzman (1982) followed by O'Neil (2009)  
have shown this for  $N = 2$

We obtain a generalized Kármán-like drag law for  $N$ -vortex streets

$$\mathcal{D} + i\mathcal{L} = \rho \left( \frac{U_b - 2U_V}{L} \right) P + \frac{\rho}{4\pi L} \sum_{j=1}^N \Gamma_j^2 + i \begin{pmatrix} \dots \end{pmatrix} \quad (3)$$

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### Summary & Conclusions

- Given some assumptions about periodic vortex streets with  $N$  vortices per period:
- The forces are found to depend on the **vortical impulse** in one period of the wake and the **pressure** on the boundary  $\mathcal{C}_4$
- Forces depend only on the **vortical impulse**, **self-induced speed of the vortices**, and the **sum of the strengths squared**
- Relative equilibria of  $N > 2$  vortices on singly-periodic domain are candidates for models of 'exotic' wakes
- Near-equilibrium configurations may also be doable

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Finally, Kármán's ultimate objective with his vortex wake model was to establish a formula for the drag on the bluff body producing the wake. In this he succeeded with what we today know as the *Kármán drag law*. The vortex-street patterns with three vortices per period, e.g., those illustrated in Fig. 8, should also yield a drag law much like von Kármán's. However, it may be possible to extend this further and derive a drag law even for cases where the three-vortex-per-cycle wake is evolving downstream. We leave this as an open problem to which we intend to return.

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Aref, Stremler & Ponta J. Fluid Struct. (2006)

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