# ENPH 257 Lab Report

Brunette, Jacob Fullerton, Dilyn Watt, Ryan Yao, Dickson

Instructor: Dr. Christopher Waltham

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## Introduction

#### 1.1 Conduction

Heat diffusion due to conduction is given by the heat equation

$$\left(\frac{\partial}{\partial t}u(\mathbf{r},t)\right)_{\text{cond}} = \frac{k}{c\rho}\nabla^2 u(\mathbf{r},t),\tag{1.1}$$

where  $u(\mathbf{r},t)$  is the temperature at position  $\mathbf{r}$  and time t, k is the thermal conductivity, c is the specific heat of the material, and  $\rho$  is the mass density of the material.

#### 1.2 Convection

Power gain due to convection for a differential surface element at position  $\mathbf{r}$  may be approximated by

$$P_{\text{conv}}(\mathbf{r},t) = -k_c \delta S(\mathbf{r}) \left( u(\mathbf{r},t) - u_{\text{amb}} \right), \tag{1.2}$$

where  $k_c$  is the convection coefficient,  $\delta S(\mathbf{r})$  is the differential surface element at  $\mathbf{r}$ , and  $u_{\rm amb}$  is the ambient temperature of the surrounding fluid.

Now temperature change due to power for a differential mass element is given by

$$P = \frac{\partial}{\partial t}Q = c \rho \,\delta V \frac{\partial}{\partial t}u,\tag{1.3}$$

so the rate of change of temperature due to convection is given by

$$\left(\frac{\partial}{\partial t}u(\mathbf{r},t)\right)_{\text{conv}} = -\frac{k_c \,\delta S(\mathbf{r})}{c \,\rho \,\delta V(\mathbf{r})} \left(u(\mathbf{r},t) - u_{\text{amb}}\right). \tag{1.4}$$

#### 1.3 Radiation

Power gain due to radiation for a differential surface element at position  $\mathbf{r}$  is given by Planck's Law to be

$$P_{\rm rad}(\mathbf{r},t) = -\epsilon \,\sigma \,\delta S(\mathbf{r}) \left( u(\mathbf{r},t)^4 - u_{\rm amb}^4 \right), \tag{1.5}$$

where  $\epsilon$  is the emissivity and  $\sigma$  is the Stefan-Boltzmann constant.

Again from Equation (1.3), we can obtain the contribution to the rate of change of temperature due to radiation

$$\left(\frac{\partial}{\partial t}u(\mathbf{r},t)\right)_{\text{rad}} = -\frac{\epsilon \,\sigma \,\delta S(\mathbf{r})}{c \,\rho \,\delta V(\mathbf{r})} \left(u(\mathbf{r},t)^4 - u_{\text{amb}}^4\right). \tag{1.6}$$

## 1.4 Heat diffusion equation for a cylindrical rod

For a one-dimensional cylindrical rod of length L and radius R, the heat diffusion equation is

$$\frac{\partial}{\partial t}u(x,t) = \frac{1}{c\rho}\left(k\frac{\partial^2}{\partial x^2}u(x,t) - k_c\frac{\delta S(x)}{\delta V(x)}\left(u(x,t) - u_{\rm amb}\right) - \epsilon\sigma\frac{\delta S(x)}{\delta V(x)}\left(u(x,t)^4 - u_{\rm amb}^4\right) + \frac{P_{\rm in}(x,t)}{\delta V(x)}\right) \quad (1.7)$$

Objective

# Method

- 3.1 Experimental setup
- 3.1.1 Rod dimensions
- 3.1.2 Thermocouple circuit
- 3.2 Calibration
- 3.3 Data aquisition

# Results

# Simulation and optimization

## 5.1 One-dimensional explicit-step simulation

A one-dimensional explicit-step finite difference program was constructed to simulate heat diffusion based on Equation (1.7). Based on the formalism in Appendix A, the explicit finite difference form of Equation (1.7) is

$$\mathbf{u}^{n+1} = \mathbf{u}^n + \delta t \left( \delta \mathbf{u}_{\text{cond}} + \delta \mathbf{u}_{\text{conv}} + \delta \mathbf{u}_{\text{rad}} + \delta \mathbf{u}_{\text{pow}} \right). \tag{5.1}$$

- 5.1.1 Finite difference equation
- 5.1.2 Implementation
- 5.2 Optimization of one-dimensional simulation
- 5.3 High-level simulation

Analysis

# **Conclusion and Summary**

## Appendix A

# Comparison of Finite Differencing Methods

The following are methods of finite differencing, demonstrated using the simple example of the one-dimensional heat conduction equation

$$\frac{\partial}{\partial t}u(x,t) = \alpha \frac{\partial^2}{\partial x^2}u(x,t). \tag{A.1}$$

### A.1 Explicit method

#### Finite difference equation

In the explicit method for finite differencing, the temperature for each spatial point can be independently determined from the previous step. That is,

$$u_i^{n+1} = u_i^n + \alpha \cdot \frac{\delta t}{\delta x^2} \cdot \left( u_{i-1}^n - 2u_i^n + u_{i+1}^n \right), \tag{A.2}$$

where the superscript  $n \in [0, T]$  signifies the step in time  $t_n$  and the subscript  $i \in [0, X]$  represents the position  $x_i$ .  $\delta t$  and  $\delta x$  are the time steps in time and position respectively.

If we define

$$\zeta = \alpha \cdot \frac{\delta t}{\delta x^2},$$

then this can be written as a linear relationship

$$\mathbf{u}^{n+1} = \mathbf{D}\mathbf{u}^n,\tag{A.3}$$

where  $\mathbf{D}$  is the matrix defined by

$$\mathbf{D}_{ij} = \begin{cases} BC, & i = 0 \text{ or } i = X\\ \zeta, & 0 < i < X \text{ and } |i - j| = 1\\ 1 - 2\zeta, & 0 < i < X \text{ and } i - j = 0\\ 0, & \text{else} \end{cases}$$
(A.4)

The top and bottom rows (i=0 and i=X) are determined from boundary conditions. Note that as  $\zeta$  approaches 0, **D** approaches the identity matrix. Thus  $\zeta$  should be as small as possible for the best approximation. The condition for stability is

$$0 < \zeta < 1$$
.

#### Error in time

The explicit method uses a forward difference in time. The expression for the derivative approximation is derived from the power series expansion in  $\delta t$ 

$$u(x,t+\delta t) = u(x,t) + \frac{\partial}{\partial t}u(x,t) \cdot \delta t + \frac{\partial^2}{\partial t^2}u(x,t) \cdot \frac{\delta t^2}{2!} + \dots$$
(A.5)

Thus we have an approximation for the time derivative

$$\frac{u(x,t+\delta t)-u(x,t)}{\delta t} = \frac{\partial}{\partial t}u(x,t) + O(\delta t). \tag{A.6}$$

The error in time due to this approximation is linear in  $\delta t$ .

#### Error in position

The explicit method uses a central second derivative in space. The expression for the second derivative approximation is derived from the power series expansion in  $\delta x$ .

$$u(x + \delta x, t) = u(x, t) + \frac{\partial}{\partial x}u(x, t) \cdot \delta x + \frac{\partial^2}{\partial x^2}u(x, t) \cdot \frac{\delta x^2}{2!} + \frac{\partial^3}{\partial x^3}u(x, t) \cdot \frac{\delta x^3}{3!} + \dots$$
 (A.7)

At  $-\delta x$ , this is

$$u(x - \delta x, t) = u(x, t) - \frac{\partial}{\partial x}u(x, t) \cdot \delta x + \frac{\partial^2}{\partial x^2}u(x, t) \cdot \frac{\delta x^2}{2!} - \frac{\partial^3}{\partial x^3}u(x, t) \cdot \frac{\delta x^3}{3!} + \dots$$

Thus the approximation for the second spatial derivative is

$$\frac{u(x-\delta x,t)-2u(x,t)+u(x+\delta x,t)}{\delta x^2} = \frac{\partial^2}{\partial x^2}u(x,t)+O(\delta x^2). \tag{A.8}$$

The error in position due to this approximation is quadratic in  $\delta x$ .

## A.2 Implicit method

#### A.3 Crank-Nicolson method