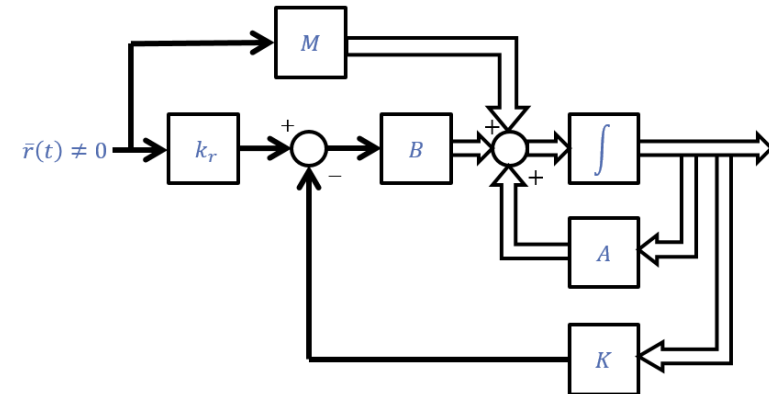


FROM LAST TIME...

Tracking and integral control

- Tracking Systems
- State Feedback with Integration



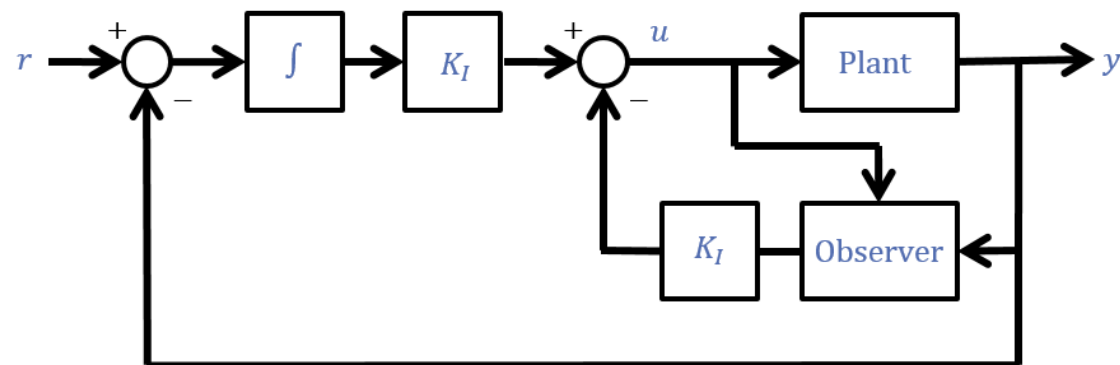
$$\dot{x} = (A - BK)x$$

$$\dot{x} = (A - BK)x + (M + Bk_r)\bar{r}$$

Same CL poles
(eigenvalues of $A - BK$)

$$u = -Kx = K_I \int (r - y)dt$$

$$-\dot{x} = r - y$$



OPTIMAL CONTROL

Topics

- Calculus of Variations
- Optimal Control
- Linear Quadratic Regulator

At the end of this section, students should be able to:

- Design state feedback controllers using the LQR method.

$$k = \text{lqr}(\text{sys}, \dots)$$

ASIDE: OPTIMAL CONTROL ORIGINATED WITH THE BRACHISTOCHRONE PROBLEM

BRACHISTOCHRONE PROBLEM

HOW DO WE DESIGN THE “BEST” CONTROLLER FOR A GIVEN APPLICATION?

1. Specify a performance index (objective function)
2. Optimize controller using performance index

This is called **optimal control**

Optimal w.r.t THE “COST FUNCTION”
↳ CAPABILITIES / PERFORMANCE

PERFORMANCE INDICES TYPICALLY INVOLVE AN INTEGRAL EXPRESSION

$$J = \int_{t_i}^{t_f} (y_d - y)^2 dt$$

MAKES POSITIVE

Integral of square error

$$J = \int_{t_i}^{t_f} (x_d - x)^T Q (x_d - x) dt$$

WEIGHTING FUNCTION

State error penalty

$$J = \int_{t_i}^{t_f} u^T R u dt$$

Control effort penalty

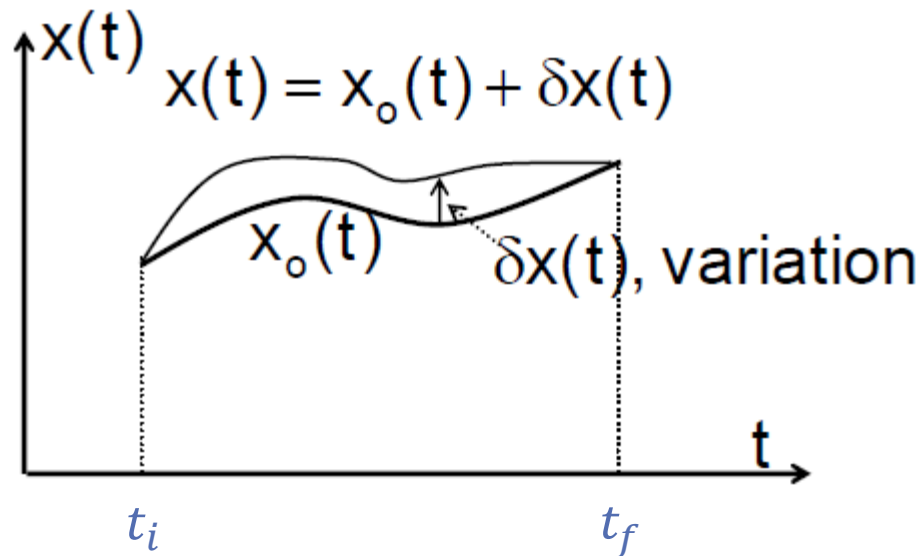
**IN GENERAL, WE WANT TO FIND A
SUFFICIENTLY SMOOTH FUNCTION
 $x_o(t)$ THAT MINIMIZES A
PERFORMANCE INDEX**

x_o denotes optimal state trajectory

$$J(x(t)) = \int_{t_i}^{t_f} L(x, \dot{x}, t) dt$$

This leads to [calculus of variation](#).

CONSIDER SCALAR CASE WITH FIXED END-POINTS



VECTOR → SCALAR

The variation of the functional, J , is given by

$$\Delta J = J(x) - J(x_o) = J(x_o + \delta x) - J(x_o)$$

NON-OPTIMAL OPTIMAL

$$\Delta J = J(x) - J(x_0) = J(x_0 + \delta x) - J(x_0)$$

$$= \cancel{J(x_0)} + \left. \frac{\partial J}{\partial x} \right|_{x=x_0} \Delta x + \left. \frac{\partial^2 J}{\partial x^2} \right|_{x=x_0} (\Delta x)^2 + \dots - \cancel{J(x_0)}$$

$$\Delta J = \left. \frac{\partial J}{\partial x} \right|_{x=x_0} \Delta x + \left. \frac{\partial^2 J}{\partial x^2} \right|_{x=x_0} (\Delta x)^2 + \dots$$

$$\approx \left. \frac{\partial J}{\partial x} \right|_{x=x_0} \Delta x$$

For J to have a minimum at x_0 , it is necessary for the first variation to be zero:

$$\delta J = \left. \frac{\partial J(x)}{\partial x} \right|_{x=x_0} \delta x = 0$$

CONSIDER THE FIRST VARIATION OF THE PERFORMANCE INDEX

$$\begin{aligned}\Delta J &= J(x_o(t) + \delta x(t)) - J(x_o(t)) \\ &= \int_{t_i}^{t_f} [L(x_o(t) + \delta x(t), \dot{x}_o(t) + \delta \dot{x}(t), t) - L(x_o(t), \dot{x}_o(t), t)] dt\end{aligned}$$

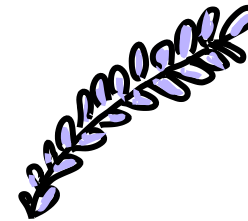
First variation:

$$\begin{aligned}\delta J &= \int_{t_i}^{t_f} \left[\frac{\partial L}{\partial x} \delta x + \frac{\partial L}{\partial \dot{x}} \delta \dot{x} \right] dt \\ \text{Integrate by parts:} \\ \delta J &= \int_{t_i}^{t_f} \left[\frac{\partial L}{\partial x} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{x}} \right) \right] \delta x dt \\ &= \left. \frac{\partial L}{\partial \dot{x}} \delta x \right|_{t_i}^{t_f} - \int_{t_i}^{t_f} \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{x}} \right) \delta x dt\end{aligned}$$

Handwritten notes: The term $\frac{\partial L}{\partial \dot{x}} \delta \dot{x}$ is circled and has an arrow pointing to the integration by parts step. The final result is written as $\left. \frac{\partial L}{\partial \dot{x}} \delta x \right|_{t_i}^{t_f} - \int_{t_i}^{t_f} \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{x}} \right) \delta x dt$.

ASIDE: THE FUNDAMENTAL LEMMA OF CALCULUS OF VARIATIONS APPLIES HERE

└ FLOCOV



If M is continuous and

$$\int_a^b M(x)h(x)dx = 0$$

for all infinitely differentiable $h(x)$ then

$$M(x) = 0$$

on the open interval (a, b)

APPLYING THE FLOCOV TO OUR CASE:

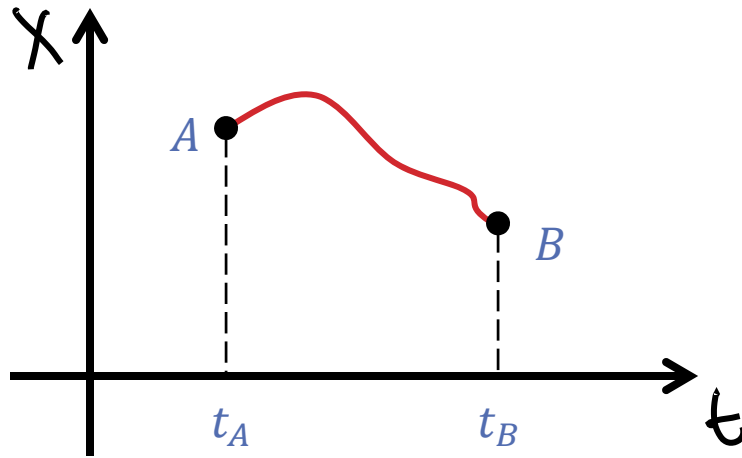
$$\int_{t_i}^{t_f} \left[\frac{\partial L}{\partial x} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{x}} \right) \right] \delta x \, dt = 0 \quad \Rightarrow \quad \frac{\partial L}{\partial x} - \frac{d}{dt} \left[\frac{\partial L}{\partial \dot{x}} \right] = 0$$

For the vector case:

$$x^T = [x_1 \quad x_2 \quad \cdots \quad x_n]$$

$$\Rightarrow \underbrace{\frac{\partial L}{\partial x_i} - \frac{d}{dt} \left[\frac{\partial L}{\partial \dot{x}_i} \right]}_{\text{Euler-Lagrange EQ}} = 0, \quad i = 1, 2, \dots, n$$

AS AN EXAMPLE, FIND THE SHORTEST PATH BETWEEN TWO POINTS IN A PLANE



$$ds = \sqrt{(dt)^2 + (dx)^2}$$

$$= \sqrt{1 + \left(\frac{dx}{dt}\right)^2} dt$$

$$= \sqrt{1 + \dot{x}^2} dt$$

$$L = \sqrt{1 + \dot{x}^2}$$

$$J = \int_{t_A}^{t_B} ds = \int_{t_A}^{t_B} \sqrt{1 + \dot{x}^2} dt$$

WHERE t
IS TIME REP.
IN TERMS OF
SPACE

APPLY THE EULER-LAGRANGE EQUATION:

$$L = \sqrt{1 + \dot{x}^2}$$

$$\frac{\partial L}{\partial x} = 0$$

$$\frac{\partial L}{\partial \dot{x}} = \frac{2\dot{x}}{2\sqrt{1+\dot{x}^2}}$$

$$0 - \frac{d}{dt} \left(\frac{\dot{x}}{\sqrt{1+\dot{x}^2}} \right) = 0$$

$$\frac{\dot{x}}{\sqrt{1+\dot{x}^2}} = C_0 \longrightarrow$$

MUST BE A CONSTANT

$$\dot{x} = \frac{C_0}{\sqrt{1-C_0^2}} = C_1$$

$$\dot{x} = C_1$$

STOPE IS CONSTANT
→ LINE

$$x(t) = C_1(t) + C_2$$

WHERE C_2 IS CONSTANT

OPTIMAL PATH IS A STRAIGHT LINE

CONSIDER THE PROBLEM OF OPTIMAL CONTROL

Given a plant is described by:

$$\dot{x} = f(x, u, t)$$

NON-LTI

$$\dot{x} = Ax + \underbrace{Bu}_{\text{LTI}}$$

and a performance Index:

$$J = \int_{t_i}^{t_f} L(x, u, t) dt$$

We seek the optimal control $u(t)$ or control law $u(x)$ that will take x from $x(t_i)$ to $x(t_f)$ and minimize J .

OPTIMAL CONTROL

We could solve the plant equation for u in terms of x and \dot{x} , then substitute into J and solve, but this is cumbersome.

Instead, use Lagrange multipliers (λ_i) to remove dynamic constraints:

$$g_i(x, \dot{x}, u, t) = f_i(x, u, t) - \dot{x}_i = 0$$

↓ ADDITION OF CONSTRAINTS
TO BE OPTIMIZED
AS WELL

$$L^*(x, \dot{x}, u, \lambda, t) = L(x, u, t) + \lambda^T (f(x, u, t) - \dot{x}) = L + \sum_{j=1}^n \lambda_j (f_j - \dot{x}_j)$$

x that minimizes L^* also minimizes L

NECESSARY
CONDITION

THE EULER-LAGRANGE EQUATIONS STILL HOLD, BUT NOW WE MUST ALSO CONSIDER CONTROL EFFORT u

$$\frac{\partial L^*}{\partial x_i} - \frac{d}{dt} \left[\frac{\partial L^*}{\partial \dot{x}_i} \right] = 0$$

$$\frac{\partial L^*}{\partial u_i} - \frac{d}{dt} \left[\frac{\partial L^*}{\partial \dot{u}_i} \right] = 0$$

$$\frac{\partial L^*}{\partial \lambda_i} - \frac{d}{dt} \left[\frac{\partial L^*}{\partial \dot{\lambda}_i} \right] = 0$$

APPLY THE EULER-LAGRANGE EQUATION TO THE STATE:

$$\frac{\partial}{\partial x_i} \left[L(x, u, t) + \sum_{j=1}^n \lambda_j [f_j(x, u, t) - \dot{x}_j] \right] - \frac{d}{dt} \frac{\partial}{\partial \dot{x}_i} \left[L(x, u, t) + \sum_{j=1}^n \lambda_j [f_j(x, u, t) - \dot{x}_j] \right] = 0$$

$$\frac{\partial}{\partial x_i} \left[\underbrace{L(x, u, t) + \sum_{j=1}^n \lambda_j f_j(x, u, t)}_H \right] - \frac{d}{dt} \frac{\partial}{\partial \dot{x}_i} (-\lambda^T \dot{x}) = 0$$

APPLY THE EULER-LAGRANGE EQUATION TO THE INPUT:

$$\frac{\partial}{\partial u_i} \left[L(x, u, t) + \sum_{j=1}^n \lambda_j [f_j(x, u, t) - \dot{x}_j] \right] - \frac{d}{dt} \frac{\partial}{\partial \dot{u}_i} \left[L(x, u, t) + \sum_{j=1}^n \lambda_j [f_j(x, u, t) - \dot{x}_j] \right] = 0$$

$$\frac{\partial}{\partial u_i} \left[\underbrace{L(x, u, t) + \sum_{j=1}^n \lambda_j f_j(x, u, t)}_H \right] - 0 = 0$$

CONSIDER THE DEFINITION OF H RELATIVE TO THE MULTIPLIER

$$H = L(x, u, t) + \sum_{j=1}^n \lambda_j f_j(x, u, t) = L + \lambda^T f$$

$$\frac{\partial H}{\partial \lambda} = 0 + f^T = \dot{x}^T$$

USING OPTIMAL METHODS WE DEFINE THE LINEAR QUADRATIC REGULATOR (LQR) DESIGN METHOD

Given: $\dot{x} = Ax + Bu$
 $x(0)$ known

Find:

u_o to minimize

$$J = \frac{1}{2} \int_0^\infty [x^T Q x + u^T R u] dt$$

Handwritten notes:
~ SAME SIZE AS x
~ BASED ON INPUT
WE CHOOSE THESE

Q is symmetric, positive semi-definite

R is symmetric, positive definite

Handwritten: ALL $\lambda_i Q > 0$

Handwritten: ALL $\lambda_i R > 0$

Handwritten: CONSTRAINTS

LQR SOLUTION

Step 1:

$$H = L + \lambda^T f = \underbrace{\frac{1}{2}x^T Qx + \frac{1}{2}u^T Ru}_{L} + \underbrace{\lambda^T [Ax + Bu]}_{f = \dot{x}}$$

Step 2:

$$\frac{\partial H}{\partial u} = 0 \quad \Rightarrow \quad Ru + B^T \lambda = 0$$

SINGLE INPUT
ASSUMED
SO $\neq u_i$

$$u_o = -R^{-1}B^T \lambda$$

OPTIMAL
(NEED λ)

Step 3:

$$H_o = \frac{1}{2}x^T Qx + \frac{1}{2}\lambda^T BR^{-1}B^T \lambda + \lambda^T [Ax - BR^{-1}B^T \lambda]$$

Step 4:

$$\dot{x} = \frac{\partial H_o}{\partial \lambda} = Ax - BR^{-1}B^T \lambda$$

$$\dot{\lambda} = -\left(\frac{\partial H_o}{\partial x}\right)^T = -Qx - A^T \lambda$$

Let $\lambda = Px(t)$

UNKNOWN MATRIX

Step 5:

$$u_o = -R^{-1}B^T Px = -Kx$$

$$K = R^{-1}B^T P$$

THIS RESULTS IN THE ALGEBRAIC RICCATI EQUATION (ARE)

$$\lambda = Px \Rightarrow \dot{\lambda} = P\dot{x}$$

$$\dot{\lambda} = -Qx - \underbrace{\lambda^T A}_{\lambda^T P^T} = P(Ax - BR^{-1}B^T \lambda)$$

$$PAx + A^T Px - PBR^{-1}B^T P + Qx = 0$$

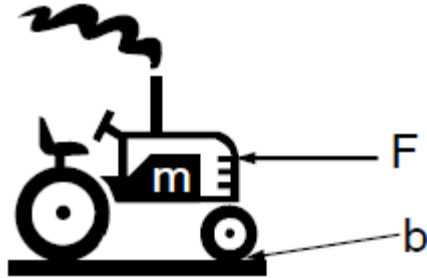
$$A^T P + PA - PBR^{-1}B^T P + Q = 0$$

A.R.E

P is symmetric and positive definite

$$P > 0 \quad \text{EIG} > 0$$

CONSIDER THE ENERGY OPTIMAL DECELERATION OF A TRACTOR



$$m\dot{v} + bv = -F$$

$$m=b=1$$

$$x = v \text{ (SPEED)}$$

$$u = F$$

$$\dot{x} = -x - u$$

$$A = [-1] \quad B = [-1]$$

$$J = \frac{1}{2} \int_0^{\infty} [x^T Q x + u^T R u] dt = \frac{1}{2} \int_0^{\infty} u^2 dt$$

STATE CONTROL

MIN ENERGY
 $Q=0$ $R=1$
 L

CONTROL EFFORT

WEIGHT ON INPUT, HIGH PENALTY FOR LARGE INPUT

The optimal control law is given by

$$u_o = -Kx$$

Where

$$K = R^{-1}B^T P$$

and P is the solution of

A.R.E

$$A^T P + PA - PBR^{-1}B^T P + Q = 0$$

$$-P - P - P^2 + 0 = 0$$

$$2P + P^2 = 0$$

$$\begin{aligned} A &= 1 \\ B &= -1 \\ Q &= 0 \\ R &= 1 \end{aligned}$$

$$P(p+2)=0$$

$$P = \begin{cases} 0 \\ -2 \end{cases}$$

$$P = -2$$

$$V_0 = -(1^{-1} \cdot -1 \cdot -2)x = -2x$$

$$\begin{aligned} \dot{x} &= 1x \\ A &= 1 \\ \text{EIG} &= 1 \end{aligned}$$

$$\dot{x} = -x - (-2x) = x$$

UNSTABLE

$$\dot{x} - x = 0$$

$$x(s-1)$$

$$P = 0$$

$$V_0 = -(1^{-1} \cdot -1 \cdot 0)x = 0$$

In the absence of a penalty on x , the minimum energy solution is to do nothing!

We should add a nonzero Q

ADD A NONZERO Q WEIGHTING

$$J = \frac{1}{2} \int_0^{\infty} [Qx^2 + u^2] dt$$

The new ARE becomes:

$$-2P - P^2 + Q = 0$$

CONSIDER THE EFFECT OF A MORE GENERAL FORMULATION

$$U_0 = -K^{-1} B^T P X \quad J = \frac{1}{2} \int_0^\infty [Qx^2 + Ru^2] dt \quad \begin{matrix} A = -1 \\ B = -1 \end{matrix}$$

$$B = -1 \quad u = \frac{P}{R} x$$

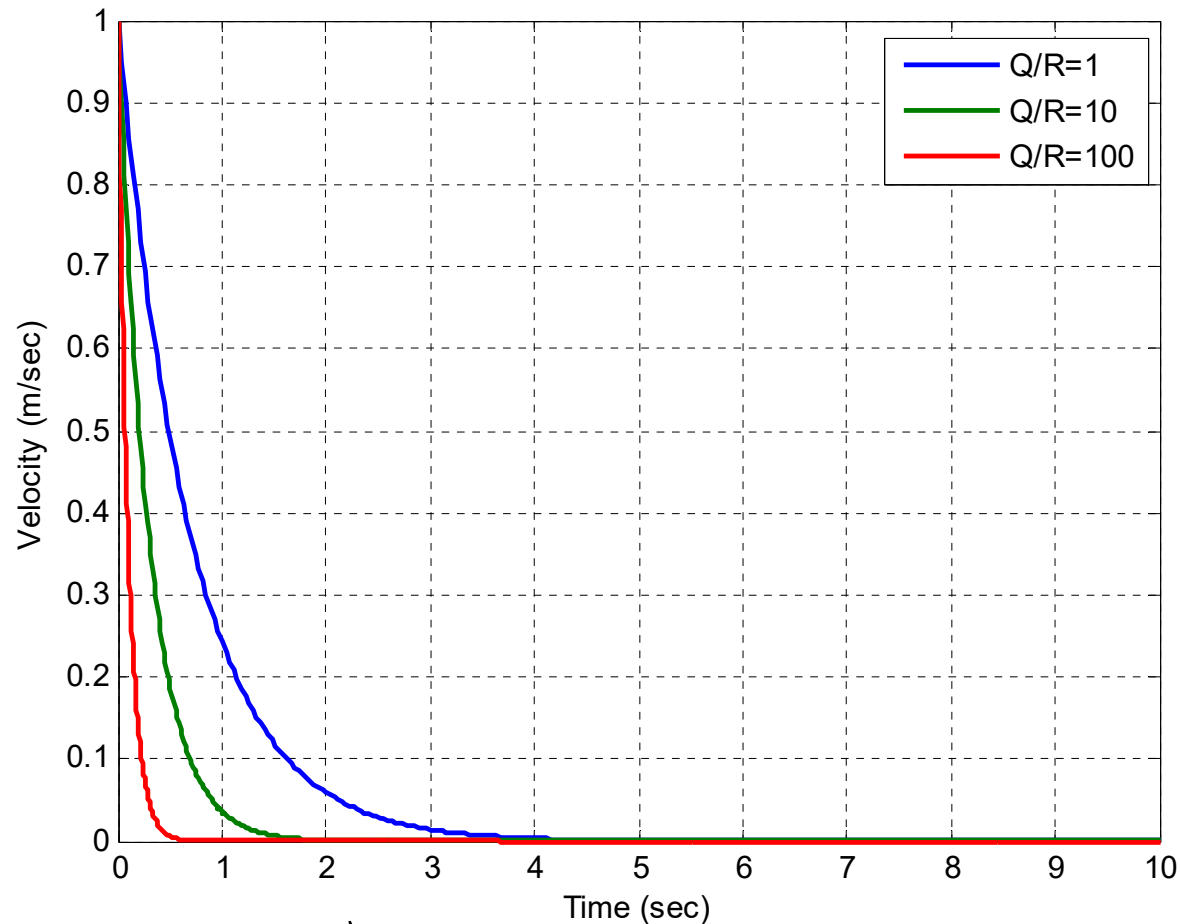
$$-2P - \frac{P^2}{R} + Q = 0$$

$$\left(\frac{P}{R}\right)^2 + 2\left(\frac{P}{R}\right) - \frac{Q}{R} = 0$$

$$\frac{P}{R} = -1 + \sqrt{1 + \frac{Q}{R}}$$

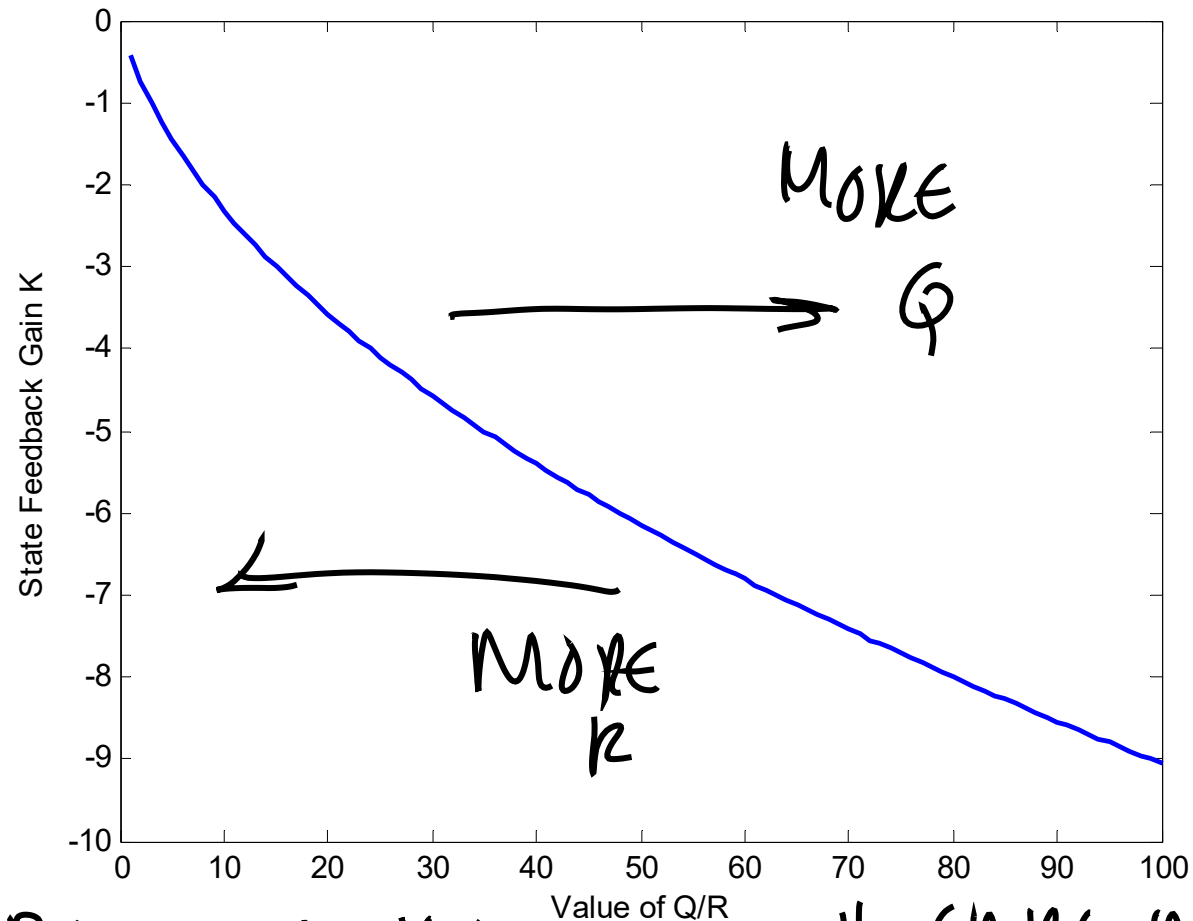
$$K = 1 - \sqrt{1 + \frac{Q}{R}}$$

HOW DOES THE TRACTOR DECELERATION CHANGE WITH Q/R ?



decelerating
SLOWER FOR LESS EFFORT

HOW DOES THE STATE FEEDBACK GAIN CHANGE WITH Q/R ?



RATIO OF HOW MUCH YOU CARE ABOUT
THE STATES VS. CONTROL EFFORT

COMING UP...

Case Study

More LQR

Linear Matrix Inequalities (LMIs)

Review

Final Exam