ISL6420B

DESIGN CALCULATIONS

FOR THE

FIREMC-PIHAT (FIREMC-3.14)

5 VOLTS DC

REQUIRED REFERENCES:

INTERSIL ISL6420B DATASHEET <http://www.intersil.com/en/products/power-MANAGEMENT/SWITCHING-CONTROLLERS/SINGLE-OUTPUT---BUCK-CONTROLLERS/ISL6420B.HTML>

ST MICROELECTRONICS STD86N3LH5 DATASHEET < HTTP://www.st.com/content/st_com/en/products/power-transistors/power-mosfets/n-channel-stripfet-12-v-to-30-v/std86N3LH5.html>

SCHELLE, D. ET AL: (2006, JUNE). BUCK-CONVERTER DESIGN DEMYSTIFIED. POWER ELECTRONICS TECHNOLOGY. RETRIEVED FROM http://powerelectronics.com/dc-dc-converters/buck-converter-design-demystified

$$\begin{array}{lll} V_{IN_{MIN}} = 11V & V_{IN_{NOM}} = 12V & V_{IN_{MAX}} = 13V \\ V_{OUT} = 5V & V_{OUT_{RIPPLE}} = 0.02 \cdot V_{OUT} = 0.1V & I_{OUT_{MAX}} = 5A \\ f_{SW} = 300kHz & LIR = 0.3 & T_{J_{MAX}} = 115^{\circ}\text{C} \\ T_{A_{MAX}} = 60^{\circ}\text{C} & \Delta V = 0.1V & V_{IN_{RIPPLE}} = 0.075V \end{array}$$

$$L = \frac{(V_{IN_{MAX}} - V_{OUT}) \cdot V_{OUT}}{V_{IN_{MAX}} \cdot f_{SW} \cdot LIR \cdot I_{OUT_{MAX}}}$$

$$L = 6.838 \mu H$$
 Choose 6.8 μH

$$\begin{split} \Delta I_L &= LIR \cdot I_{OUT_{MAX}} = \frac{(V_{IN_{MAX}} - V_{OUT}) \cdot V_{OUT}}{V_{IN_{MAX}} \cdot f_{SW} \cdot L} \\ \Delta I_L &= 1.5A \\ \Delta I_{L_{ACT}} &= 1.509A \end{split}$$

$$\begin{split} I_{OUT_{PK}} &= I_{OUT_{MAX}} + \frac{\Delta I_{L_{ACT}}}{2} \\ I_{OUT_{PK}} &= 5.76 A \end{split}$$

$$\begin{split} I_{L_{SAT}} &> I_{OUT_{PK}} \cdot 1.2 \\ I_{L_{SAT}} &> 6.912 A \end{split}$$

$$C_{O} = \frac{L \cdot \left(I_{OUT_{MAX}} + \frac{\Delta I_{L_{ACT}}}{2}\right)^{2}}{(\Delta V + V_{OUT})^{2} - V_{OUT}^{2}} = \frac{L \cdot I_{OUT_{PK}}^{2}}{(\Delta V + V_{OUT})^{2} - V_{OUT}^{2}}$$

$$C_{O} = 223.4 \mu F$$

$$C_{O_{ACT}} = C_0 \cdot 1.2$$

$$C_{O_{ACT}} = 268.05 \mu F$$

CHOOSE 3x 150µF

$$\begin{split} V_{OUT_{CAP}} &= \frac{1}{2 \cdot C_O} \cdot \frac{V_{IN_{MAX}} - V_{OUT}}{L} \cdot \left(\frac{V_{OUT}}{V_{IN_{MAX}}} \cdot \frac{1}{f_{SW}} \right)^2 \\ V_{OUT_{ESR}} &= \Delta I_{L_{ACT}} \cdot ESR_{CO} \end{split}$$

$$\begin{aligned} V_{OUT_{RIPPLE}} &= V_{OUT_{CAP}} + V_{OUT_{ESR}} = \frac{1}{2 \cdot C_O} \cdot \frac{V_{IN_{MAX}} - V_{OUT}}{L} \cdot \left(\frac{V_{OUT}}{V_{IN_{MAX}}} \cdot \frac{1}{f_{SW}} \right)^2 + \Delta I_{L_{ACT}} \cdot ESR_{CO} \\ ESR_{CO} &= \frac{1}{\Delta I_{L_{ACT}}} \cdot \left(V_{OUT_{RIPPLE}} - \frac{1}{2 \cdot C_O} \cdot \frac{V_{IN_{MAX}} - V_{OUT}}{L} \cdot \left(\frac{V_{OUT}}{V_{IN_{MAX}}} \cdot \frac{1}{f_{SW}} \right)^2 \right) \end{aligned}$$

 $ESR_{C_O} \le 0.063\Omega$

COMBINE CAPS IN PARALLEL TO SO EFFECTIVE ESR IS LESS THAN OR EQUAL TO THE ABOVE VALUE.

$$\begin{split} I_{C_{I_{RMS}}} &= I_{OUT_{MAX}} \cdot \frac{\sqrt{V_{OUT} \cdot \left(V_{IN_{MIN}} - V_{OUT}\right)}}{V_{IN_{MIN}}} \\ I_{C_{I_{RMS}}} &= 2.49 A \end{split}$$

$$\begin{split} &C_{IN} \geq 10uF \cdot I_{C_{IRMS}} \\ &C_{IN} \geq \frac{10\mu F}{A} \cdot 2.494 \\ &C_{IN} \geq 24.9\mu F \end{split} \qquad \text{Choose 40} \\ &T_{I_{RISR}} = T_{J_{MAX}} - T_{A_{MAX}} \\ &T_{J_{RISR}} = T_{J_{MAX}} - T_{A_{MAX}} \\ &T_{J_{RISR}} = \frac{T_{J_{MSE}}}{9_{IA}} \qquad \Theta_{JA} \text{ from Std86n31h5 datasheet is 50°C (Rebj-pob On the datasheet)} \\ &P_{D_{TOT}} = \frac{T_{J_{RISE}}}{9_{IA}} \qquad \Theta_{JA} \text{ from Std86n31h5 datasheet is 50°C (Rebj-pob On the datasheet)} \\ &P_{D_{TOT}} = 1.1W \\ &R_{DS(ON)_{HOT}} = R_{DS(ON)_{25}} \cdot \left[1 + 0.005 \cdot \left(T_{J_{HOT}} - 25^{\circ}C\right)\right] \\ &R_{DS(ON)_{25}} \leq \frac{V_{IN_{MIN}}}{V_{OUT}} \cdot \frac{1}{I_{OUT_{MAX}}^{2} \cdot \left[1 + 0.005 \cdot \left(T_{J_{HOT}} - 25^{\circ}C\right)\right]} \cdot P_{D_{TOT}} \cdot 0.6 \\ &R_{DS(ON)_{25}} \leq 0.04220 \qquad R_{DS(ON)_{25}} \text{ from Std86n31h5 datasheet is 0.0065} \\ &R_{DS(ON)_{HOT}} = 0.00930 \\ &P_{D_{RDS}} = \frac{V_{OUT} \cdot I_{OUT_{MAX}}^{2} \cdot R_{DS(ON)_{HOT}}}{V_{IN_{MIN}}} \\ &P_{D_{RDS}} = \frac{V_{OUT} \cdot I_{OUT_{MAX}}^{2} \cdot f_{SW} \cdot I_{OUT_{MAX}}}{I_{GATE}} \qquad \text{Where} \qquad C_{RSS} = 58pF \text{ and } I_{GATE} = 0.7A \\ &P_{D_{SW}} = \frac{C_{RSS} \cdot V_{IN_{MAX}}^{2} \cdot f_{SW} \cdot I_{OUT_{MAX}}}{I_{GATE}} \\ &P_{D} = P_{D_{RDS}} + P_{D_{SW}} \\ &P_{D} = 0.1267W \\ &T_{I_{RISE_{EST}}} = P_{D} \cdot \Theta_{IA} \\ &T_{I_{RISE_{EST}}} = 6.34^{\circ}C \\ &T_{I_{EST}} = T_{I_{RISE_{EST}}} + T_{A_{MAX}} \\ &T_{I_{EST}} = 66.34^{\circ}C \\ &T_{I_{EST}} = 66.34^{\circ}C \\ &T_{I_{EST}} = 66.34^{\circ}C \\ &T_{I_{EST}} = 66.34^{\circ}C \\ &T_{I_{EST}} = 60.910 \text{ estimate} \quad ****** \end{aligned}$$

THE FOLLOWING CALCULATIONS REQUIRE THE ISL6420B DATASHEET AS THE COMPONENT REFERENCES USED IN THE CALCULATIONS COME RIGHT FROM THE DATASHEET AND NOT THE FIREMC-PIHAT (FIREMC-3.14) DESIGN SCHEMATIC.

$$\begin{split} I_{OC} &> I_{L_{SAT}} \\ I_{OC} &> 6.912A \\ I_{OC} &= 7A \\ I_{OC} &= \frac{I_{OCSET} \cdot R_{OCSET}}{R_{DS(ON)_{MAX}}} \\ R_{DS(ON)_{100}} &\approx 1.45 \cdot R_{DS(ON)_{25}} \end{split}$$

$$R_{DS(ON)_{100}} \approx 0.0095\Omega$$

$$R_{DS(ON)_{100}} = R_{DS(ON)_{MAX}}$$

$$R_{OCSET} = \frac{I_{OC} \cdot R_{DS(ON)_{90}}}{I_{OCSET}}$$

$$I_{OCSET} = rac{I_{OC} \cdot R_{DS(ON)_{90}}}{I_{OCSET}}$$
 WHERE $I_{OCSET} = 100 \mu A = 0.0001 A$

$$R_{OCSET} = 665\Omega$$
 CHOOSE 665 Ω

$$f_{LC}=rac{1}{2\cdot\pi\cdot\sqrt{L\cdot C_O}}$$
 where $C_O=450\mu F$ and $L=6.8\mu H$

$$f_{LC} = 2.877kHz$$

$$f_{ESR} = \frac{1}{2 \cdot \pi \cdot ESR_{C_{O(ACT)}} \cdot c_O}$$
 Where $ESR_{C_{O(ACT)}} = 0.0533\Omega$

$$f_{ESR} = 6.636kHz$$

$$V_{FB} = V_{OUT} \cdot rac{R4}{R1 + R4}$$
 where $V_{FB} = V_{REF} = 0.6 V$ and $R1 = 10 k\Omega$

$$\begin{split} V_{FB} &= V_{OUT} \cdot \frac{_{R4}}{_{R1+R4}} \\ R4 &= \frac{V_{FB} \cdot R1}{V_{OUT} - V_{FB}} \end{split}$$

$$R4 = 1.364k\Omega$$
 CHOOSE 1.37k Ω

$$\frac{R2}{R1} = 5.62$$

$$R2 = 5.62 \cdot R1$$

$$R2 = 56.2k\Omega$$

$$f_{Z1} = 0.75 \cdot f_{LC} = \frac{1}{2 \cdot \pi \cdot R2 \cdot C1}$$

$$C1 = \frac{1}{2 \cdot \pi \cdot R2 \cdot 0.75 \cdot f_{LC}}$$

$$C1 = \frac{1}{2 \cdot \pi \cdot R2 \cdot 0.75 \cdot f_{LC}}$$

$$C1 = 1.312nF$$

$$f_{Z2} = f_{LC} = \frac{1}{2 \cdot \pi \cdot (R1 + R3) \cdot C3}$$

$$f_{Z2} = \frac{1}{2 \cdot \pi \cdot \left(R1 + \left(\frac{1}{2 \cdot \pi \left(\frac{f_{SW}}{2}\right) \cdot C3}\right)\right) \cdot C3}$$

$$C3 = \frac{\frac{f_{SW}}{2 \cdot f_{LC}} - 1}{\frac{2 \cdot \pi \cdot R1 \cdot f_{SW}}{2 \cdot \pi \cdot R1 \cdot f_{SW}}}$$

$$C3 = 5.426$$
nf CHOOSE 5600pF

$$f_{P2} = \frac{f_{SW}}{2} = \frac{1}{2 \cdot \pi \cdot R3 \cdot C3}$$

$$R3 = \frac{1}{2 \cdot \pi \cdot \frac{f_{SW}}{2} \cdot C3}$$

$$R3 = 189.47\Omega$$
 CHOOSE 191 Ω

$$f_{P1} = f_{ESR} = \frac{1}{2 \cdot \pi \cdot R2 \cdot \frac{C1 \cdot C2}{C1 + C2}}$$

$$C2 = \frac{C1}{(f_{ESR} \cdot 2 \cdot \pi \cdot R2 \cdot C1) - 1}$$
 $C2 = 61pF$ CHOOSE 62pF