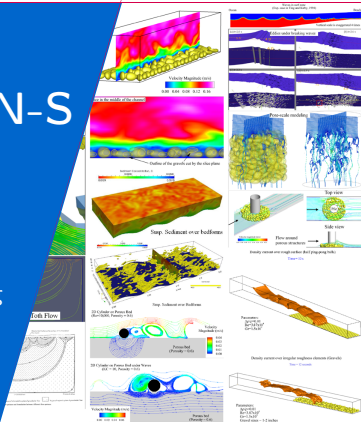


Chapter 5: Solution of N-S Equations-Part 2

Xiaofeng Liu, Ph.D., P.E.
Assistant Professor
Department of Civil and Environmental Engineering
Pennsylvania State University
xliu@engr.psu.edu



Solution of NS Equations
Projection method

What will be covered in this chapter?

- ▶ General overview of the pressure–velocity coupling
- ▶ Solution algorithms
 - **Segregated** algorithms: u , v , w and p fields are solved separately. Coupling between these variables are through velocity and pressure corrections.
 - Iterative algorithms: SIMPLE, PISO, etc.
 - Projection method
 - **Coupled** algorithms: All fields are solved in one shot!
 - Not covered in this course.
 - Can be achieved through the new *block – matrix*

Unsteady, 3D Navier-Stokes equations for incompressible flow on a closed domain V :

$$\nabla \cdot \mathbf{u} = 0 \quad (1)$$

$$\frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot (\mathbf{u}\mathbf{u}) = -\nabla p + \nu \nabla^2 \mathbf{u} \quad (2)$$

For simplicity, assume on the solid boundary conditions $\mathbf{u} = 0$ on ∂V .

History and background:

- ▶ Another class of segregated algorithm to deal with the \mathbf{u} - p coupling
- ▶ Original method proposed in Chorin (1968) and Temam (1969)
- ▶ A lot of further development ever since
- ▶ I have seen/used projection method for high resolution simulations such as DNS for turbulence
 - Easy to be combined with high-order temporal discretization schemes such as RK4
- ▶ The projection method is a generic solution algorithm. It is not bound by any specific spatial discretization scheme.

Important references:

- ▶ A. J. Chorin. Numerical solution of the Navier-Stokes equations. *Mathematics of computation*, 22(104):745-762, 1968.
- ▶ R. Temam. Sur l'approximation de la solution des equations de Navier-Stokes par la methode des pas fractionnaires (ii). *Archive for Rational Mechanics and Analysis*, 33(5):377-385, 1969.
- ▶ J. Kim and P. Moin, Application of a fractional-step method to incompressible Navier-Stokes equations, *J. Comput. Phys.* 59, 308 (1985).
- ▶ J. van Kan. A second-order accurate pressure-correction scheme for viscous incompressible flow. *SIAM Journal on Scientific and Statistical Computing*, 7(3):870-891, 1986.
- ▶ J. B. Bell, P. Colella, and H. M. Glaz. A second-order projection method for the incompressible Navier-Stokes equations. *Journal of Computational Physics*, 85(2):257-283, 1989.
- ▶ D. L. Brown, R. Cortez, and M. L. Minion. Accurate projection methods for the incompressible Navier-Stokes equations. *Journal of Computational Physics*, 168(2):464-499, 2001.

Basic idea of projection method:

- ▶ Basically a fractional-step method.
- ▶ First a flow velocity field is estimated from momentum equation
 - Non-incremental pressure correction scheme: if pressure is not included in the velocity estimation
 - Incremental pressure correction scheme: if pressure is included
- ▶ Then the velocity is **projected** into the space of divergence-free vectors with appropriate boundary condition
- ▶ The mathematical backbone of the projection method is the Helmholtz-Hodge decomposition

Helmholtz-Hodge decomposition:

- ▶ A vector field \mathbf{u} can be decomposed uniquely into a solenoidal (divergence-free) part and an irrotational part

$$\mathbf{u} = \mathbf{u}_S + \mathbf{u}_I \quad (3)$$

where

$$\nabla \cdot \mathbf{u}_S = 0, \quad \nabla \times \mathbf{u}_I = 0 \quad (4)$$

- ▶ If we take divergence on both sides of Eqn. 3, we have

$$\nabla \cdot \mathbf{u} = \nabla \cdot \mathbf{u}_S + \nabla \cdot \mathbf{u}_I \quad (5)$$

$$= \nabla^2 \phi \quad (6)$$

because the irrotational part can be written as a gradient of a scalar function ϕ , i.e. $\mathbf{u}_I = \nabla \phi$.

- ▶ So we have:

$$\mathbf{u}_S = \mathbf{u} - \nabla \phi \quad (7)$$

The original Chorin's projection method:

- ▶ First compute an intermediate velocity \mathbf{u}^* using the momentum equation and ignoring the pressure gradient term

$$\frac{\mathbf{u}^* - \mathbf{u}^n}{\Delta t} = -(\mathbf{u}^n \cdot \nabla)\mathbf{u}^n + \nu \nabla^2 \mathbf{u}^n \quad (8)$$

$$\mathbf{u}^* = 0 \text{ on } \partial V \quad (9)$$

where \mathbf{u}^n is the old velocity at the n -th time step.

- ▶ Then project (update) the intermediate velocity to get the new velocity \mathbf{u}^{n+1}

$$\mathbf{u}^{n+1} = \mathbf{u}^* - \Delta t \nabla p^{n+1} \quad (10)$$

Compare with the Helmholtz-Hodge decomposition:

$$\mathbf{u}_S = \mathbf{u} - \nabla \phi \quad (11)$$

The original Chorin's projection method:

- ▶ As we mentioned, the projection method is in fact a two-step (fractional) method:

$$\frac{\mathbf{u}^* - \mathbf{u}^n}{\Delta t} = -(\mathbf{u}^n \cdot \nabla) \mathbf{u}^n + \nu \nabla^2 \mathbf{u}^n \quad (12)$$

$$\frac{\mathbf{u}^{n+1} - \mathbf{u}^*}{\Delta t} = \nabla p^{n+1} \quad (13)$$

- ▶ But how do we get p^{n+1} ? Answer: divergence-free condition.
- ▶ We want our new velocity field \mathbf{u}^{n+1} to be divergence free. Take divergence on both sides of Eqn. 13:

$$\frac{\nabla \cdot \mathbf{u}^{n+1} - \nabla \cdot \mathbf{u}^*}{\Delta t} = \nabla \cdot (\nabla p^{n+1}) \quad (14)$$

then we get a familiar PPE:

$$\nabla^2 p^{n+1} = \frac{1}{\Delta t} \nabla \cdot \mathbf{u}^* \quad (15)$$

The original Chorin's projection method:

- ▶ On a solid boundary, we take dot production of Eqn. 13 with surface normal \mathbf{n} , and can get the boundary condition for pressure p^{n+1} :

$$\mathbf{n} \cdot (\nabla p^{n+1}) = \frac{\mathbf{n} \cdot \mathbf{u}^{n+1} - \mathbf{n} \cdot \mathbf{u}^*}{\Delta t} = 0 \quad (16)$$

- ▶ Careful examination of the pressure B.C. reveals that it only guarantees no-penetration, not no-slip.
- ▶ As a result, there might be some small slip velocity on a solid boundary from projection method solution.

To recap the original Chorin's projection method:

- ▶ First step: estimate \mathbf{u}^*

$$\frac{\mathbf{u}^* - \mathbf{u}^n}{\Delta t} = -(\mathbf{u}^n \cdot \nabla) \mathbf{u}^n + \nu \nabla^2 \mathbf{u}^n \quad (17)$$

$$\text{B.C.: } \mathbf{u}^* = 0 \text{ on } \partial V \quad (18)$$

- ▶ Second step: solve PPE to project into divergence free vector space

$$\nabla^2 p^{n+1} = \frac{1}{\Delta t} \nabla \cdot \mathbf{u}^* \quad (19)$$

$$\text{B.C.: } \mathbf{n} \cdot (\nabla p^{n+1}) = 0 \quad (20)$$

- ▶ Update \mathbf{u}^{n+1} :

$$\mathbf{u}^{n+1} = \mathbf{u}^* - \Delta t \nabla p^{n+1} \quad (21)$$

Implementation of the original Chorin's projection method in OpenFOAM® :

- ▶ Very easy!
- ▶ Just solve one unsteady, advection-diffusion equation and one diffusion equation.
- ▶ Demo: ChorinProjectionFOAM

Drawback of the original projection method:

- ▶ Momentum is explicitly solved: limitation on time step size (Courant number)
- ▶ Ambiguity in specifying the B.C. for the intermediate velocity \mathbf{u}^*
 - In the prediction of \mathbf{u}^* , since pressure gradient is not included, \mathbf{u}^* could be far away from \mathbf{u}^{n+1}
 - As a result, specifying the same B.C. for \mathbf{u}^* as \mathbf{u}^{n+1} is not accurate.
- ▶ Formal analysis reveals that the boundary condition for pressure lowers the overall solution accuracy to zero order!
- ▶ In projection method terminology, this will create an artificial numerical boundary layer and contaminate the whole solution field.

Improvements to the original projection method:

- ▶ Increase the implicitness of momentum solution.
- ▶ For example, Kim and Moin (1986) used extrapolation scheme (second-order accurate Adams-Bashforth) for the advection term and a Crank-Nicholson scheme for the diffusion term:

$$\frac{\mathbf{u}^* - \mathbf{u}^n}{\Delta t} = -\frac{3\mathbf{u}^n \cdot \nabla \mathbf{u}^n - \mathbf{u}^{n-1} \cdot \nabla \mathbf{u}^{n-1}}{2} + \frac{\nu}{2} (\nabla^2 \mathbf{u}^* + \nabla^2 \mathbf{u}^n) \quad (22)$$

- ▶ They also added some corrections to the \mathbf{u}^* boundary condition
- ▶ A good paper to read is Brown et al., JCP, 2001.

Development in OpenFOAM® :

- ▶ Official release of OpenFOAM® does not implement any projection method
- ▶ However, there has been some development by several researchers:
 - projectionFoam: <https://github.com/asimonder/projectionFoam>
 - Onder, A., Meyers, J. (2013). HPC realization of a controlled turbulent jet using OpenFOAM. Open Source CFD International Conference 2013. Hamburg, 24-25 October 2013
 - Onder, A., Meyers, J. (2014). Modification of vortex dynamics and transport properties of transitional axisymmetric jets using zero-net-mass-flux actuation, Physics of Fluids, 26, 075103 (2014)
 - v. Vuorinen at Aalto University School of Engineering, Finland
 - V. Vuorinen, J.-P. Keskinen, C. Duwig, B.J. Boersma, On the implementation of low-dissipative Runge-Kutta projection methods for time dependent flows using OpenFOAM, Computers & Fluids, Volume 93, 10 April 2014, Pages 153-163
 - V. Vuorinen, A. Chaudhari, J.-P. Keskinen, Large-eddy simulation in a complex hill terrain enabled by a compact fractional step OpenFOAM solver, Advances in Engineering Software, Volume 79, January 2015, Pages 70-80

Questions?