

# ECE4643: Power Electronics

## Assignment 4: Solution

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**Q1:**

**Q2**

A  $1\phi$  half-bridge inverter is fed with  $V_s = 48$  V(dc), to supply a resistive load of  $R_L = 2.4 \Omega$  at 60 Hz. for this inverter determine:

- a) The rms value of the fundamental component of the output voltage.

The rms value of the fundamental component of the output voltage  $V_{O1}$  for a half-bridge inverter is determined as:

$$V_{O1} = \frac{2V_s}{\sqrt{2}\pi} = \frac{2 \times 48}{\sqrt{2}\pi} = 21.6 \text{ V}$$

- b) The output power,

The output power  $P_O$  can be determined as:

$$P_O = \frac{V_{O1}^2}{R_L} = \frac{21.6^2}{2.4} = 194.4 \text{ W}$$

- c) The output current peak and rms values.

The output peak current can be calculated as:

$$(i_O)_{Peak} = \sqrt{2} \times \frac{V_O}{R_L} = \sqrt{2} \times \frac{48/2}{2.4} = 14.14 \text{ A}$$

The rms value of the output current  $I_O$  is determined as:

$$I_O = \frac{V_O}{R_L} = \frac{48/2}{2.4} = 10 \text{ A}$$

d) The value of  $THD_V$ .

$$THD_V = \frac{\left(\sum_{n=1,3,\dots}^{\infty} V_{O_n}^2\right)^{\frac{1}{2}}}{V_{O1}}$$

where:

$$\left(\sum_{n=1,3,\dots}^{\infty} V_{O_n}^2\right)^{\frac{1}{2}} = \left(V_O^2 - V_{O1}^2\right)^{\frac{1}{2}} = \sqrt{24^2 - 21.6^2} = 10.46$$

The value of  $THD_V$  can be evaluated s:

$$THD_V = \frac{10.46}{21.6} = 48.43\%$$

### Q3:

Repeat **Q2** for a full-bridge inverter.

a) The rms value of the fundamental component of the output voltage.

The rms value of the fundamental component of the output voltage  $V_{O1}$  for a full-bridge inverter is determined as:

$$V_{O1} = \frac{4V_s}{\sqrt{2}\pi} = \frac{4 \times 48}{\sqrt{2}\pi} = 43.2 \text{ V}$$

b) The output power,

The output power  $P_O$  can be determined as:

$$P_O = \frac{V_{O1}^2}{R_L} = \frac{43.2^2}{2.4} = 777.6 \text{ W}$$

c) The output current peak and rms values.

The output peak current can be calculated as:

$$(i_O)_{Peak} = \sqrt{2} \times \frac{V_O}{R_L} = \sqrt{2} \times \frac{48}{2.4} = 28.28 \text{ A}$$

The rms value of the output current  $I_O$  is determined as:

$$I_O = \frac{V_O}{R_L} = \frac{48}{2.4} = 20 \text{ A}$$

d) The value of  $THD_V$ .

$$THD_V = \frac{\left(\sum_{n=1,3,..}^{\infty} V_{On}^2\right)^{\frac{1}{2}}}{V_{O1}}$$

where:

$$\left(\sum_{n=1,3,..}^{\infty} V_{On}^2\right)^{\frac{1}{2}} = \left(V_O^2 - V_{O1}^2\right)^{\frac{1}{2}} = \sqrt{48^2 - 43.2^2} = 20.92$$

The value of  $THD_V$  can be evaluated s:

$$THD_V = \frac{20.92}{43.2} = 48.43\%$$

#### Q4

A  $1\phi$  full-bridge inverter is switched using the bipolar SPWM for  $V_s = 300 \text{ V(d.c)}$ ,  $m_a = 0.8$ ,  $m_f = 39$ , and  $f_o = 47 \text{ Hz}$ . For this inverter, determine the rms value of the fundamental component of the output voltage, and the first 5 dominant harmonic components. The rms values of the harmonic components due the bipolar SPWM can be stated as:

$$(V_O)_n = \frac{V_s}{\sqrt{2}} \times (V_{On})_{p.u}$$

where  $(V_{On})_{p.u}$  is the associated p.u value of the harmonic components as stated in the table of lecture 23. For  $n = 1$  (the fundamental component):

$$(V_O)_1 = \frac{300}{\sqrt{2}} \times 0.8 \times 0.49 = 103.94 \times 0.8 = 83.16$$

As for the bipolar SPWM, the harmonic patches will be centered at multiples of  $m_f \times f_m$ . The first harmonic patch will be centered at  $(m_f \pm 2) f_m$ . In this inverter case,  $m_f = 39$ , and  $m_a = 0.8$ . Remember that  $n$  is the harmonic order.

for  $n = m_f - 2 = 37$ :

$$(V_O)_{37} = \frac{300}{\sqrt{2}} \times 0.135 = 212.13 \times 0.135 = 28.64$$

for  $n = m_f + 2 = 41$ :

$$(V_O)_{41} = \frac{300}{\sqrt{2}} \times 0.135 = 212.13 \times 0.135 = 28.64$$

There will be another harmonic patch centered at  $(m_f \pm 4) f_m$ , and using the table, these harmonic components will have a p.u value of 0.005 (negligible). The second patch of harmonics will be centered at  $(2m_f \pm 1) f_m$ .

for  $n = 2m_f - 1 = 77$ :

$$(V_O)_{77} = \frac{300}{\sqrt{2}} \times 0.192 = 212.13 \times 0.192 = 40.73$$

for  $n = 2m_f + 1 = 79$ :

$$(V_O)_{79} = \frac{300}{\sqrt{2}} \times 0.192 = 212.13 \times 0.192 = 40.73$$

There will another harmonic patch centered at  $(m_f \pm 5) f_m$ , and using the table, these harmonic components will have a p.u value of 0.008 (negligible).

## Q5

Repeat **Q4** for the unipolar SPWM. The rms values of the harmonic components due the unipolar SPWM can be stated as:

$$(V_O)_n = \frac{V_s}{\sqrt{2}} \times (V_{On})_{p.u}$$

where  $(V_{On})_{p.u}$  is the associated p.u value of the harmonic components as stated in the table of lecture 23. As for the unipolar SPWM, the harmonic patches will be centered at multiples of  $2m_f \times f_m$ . The first harmonic patch will be centered at  $(2m_f \pm 1) f_m$ . In this inverter case,  $m_f = 39$ , and  $m_a = 0.8$ . Remember that  $n$  is the harmonic order.

for  $n = 1$  (the fundamental component):

$$(V_O)_1 = \frac{300}{\sqrt{2}} \times 0.8 \times 0.49 = 103.94 \times 0.8 = 83.16$$

for  $n = 2m_f - 1 = 77$ :

$$(V_O)_{75} = \frac{300}{\sqrt{2}} \times 0.192 = 212.13 \times 0.192 = 40.73$$

for  $n = 2m_f + 1 = 79$ :

$$(V_O)_{77} = \frac{300}{\sqrt{2}} \times 0.192 = 212.13 \times 0.192 = 40.73$$

There will be another harmonic patch centered at  $(2m_f \pm 5) f_m$  with a p.u value of 0.008 (negligible). The second patch of harmonics will be centered at  $(4m_f \pm 1) f_m$ .

for  $n = 4m_f - 1 = 155$ :

$$(V_o)_{155} = \frac{300}{\sqrt{2}} \times 0.064 = 212.13 \times 0.064 = 13.58$$

for  $n = 4m_f + 1 = 157$ :

$$(V_o)_{157} = \frac{300}{\sqrt{2}} \times 0.064 = 212.13 \times 0.064 = 13.58$$

There will be harmonic patches centered at  $(4m_f \pm 5) f_m$  with:

for  $n = 4m_f - 5 = 151$ :

$$(V_o)_{151} = \frac{300}{\sqrt{2}} \times 0.051 = 212.13 \times 0.051 = 10.82$$

for  $n = 4m_f + 5 = 161$ :

$$(V_o)_{161} = \frac{300}{\sqrt{2}} \times 0.051 = 212.13 \times 0.051 = 10.82$$

A third patch of harmonics is centered by  $(4m_f \pm 7) f_m$  with a p.u value of 0.01 (negligible).

**Notes for Q4 and Q5:**

- For the bipolar SPWM, the dominant harmonics are located at  $n = 37, n = 41, n = 77$ , and  $n = 79$ .
- For the unipolar SPWM, the dominant harmonics are located at  $n = 77, n = 79, n = 151, n = 155, n = 157$ , and  $n = 161$ .
- Harmonic components, due to the unipolar and bipolar SPWM, may share magnitude values, however, they are located in different frequency bands.