

$$\text{wave length} = \frac{c}{f} \rightarrow \text{Frequency}$$

$$\frac{3 \times 10^8 \text{ m/s}}{\text{speed of light}}$$

5. Horn Antenna
6. Vivaldi Antenna
7. Telescopes.

Other Antennas:-

1. NFC Antenna
2. Fractal Antenna
3. Wearable Antenna.

4nec2

Numeric Electromagnetic Codes-

C EMA Ex-1

19/1/2023

1. Configure a linear wire antenna so as to operate at  $f = 400 \text{ MHz}$ ,

$$l = \frac{c}{f} = \frac{3 \times 10^8}{4 \times 10^8} = \frac{3}{4}$$

1) Symbols

$$= \frac{3}{4} \quad \frac{3 \times 10^2}{4} \quad l = 0.75 \text{ m}$$

odd value greater than 9

$$\text{lambda} = l = 0.75 \text{ m}$$

Type Wire 1 27 0 0 - 1/2 0 0 + 1/2 0.0001m


2) Geometry

3) Size

11

### 3) Source/load

Type	Tag	Seg	(opt)	Real	Imag	Magn	Phase
Voltage- src	1	14	00	1	0	1	0


  
Middle of previous seg.

### 4) Freq/Ground

Frequency  $\rightarrow$  400MHz From question.

Environment  $\rightarrow$  Free-space

Run button Green color. upper right side.

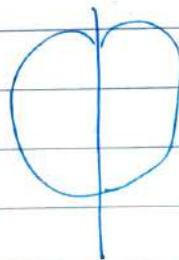
Select. Far field  
Resolution 5

Click generate.

Omni directional pattern.

E Non-directional pattern in given plane  
& directional pattern in its orthogonal plane.

Dipole Antenna



Mono pole  $\rightarrow$





## Variable Name

1. It can be only one word.
2. It can use only letters, numbers and the underscore (-) character.
3. It can't begin with a number.

input() function → Store value in form of string.

len() function

In python, ~~onedata~~ type can change onedata type to another data type.

EMA Practical - 2      27/01/2023

Title:- Performance comparison of half wave dipole verses, quarterwave ~~monowave~~ pole antenna.

$$c = 3 \times 10^8 \text{ m/s}$$

$$f = 500 \text{ MHz} = 500 \times 10^6$$

$$\lambda = \frac{c}{f} = \frac{3}{5} = 0.6$$

$$\lambda = 0.6 \text{ m}$$

$$\lambda = \text{lambda} / 2$$

## Geo.metry

Type	Tag	Segs	X <sub>1</sub>	Y <sub>1</sub>	Z <sub>1</sub>	X <sub>2</sub>	Y <sub>2</sub>	Z <sub>2</sub>	Radius
Wire	1	21	0	0	-1/2	0	0	1/2	0.0001

Source / Load

Type	Tag	Seg	opt	Real	Imag	Magn	Phase
Vtg. source		11	no	0.1	0.0	0.1	0

Environment - Free-space.

For halfwave dipole - at  $f = 500 \text{ MHz}$

- ① Gain = 2.17 dB
- ② HPBW = Half pwr beamwidth = 80 dg
- ③ Impedance =  $80.5 + j46.4 \Omega$

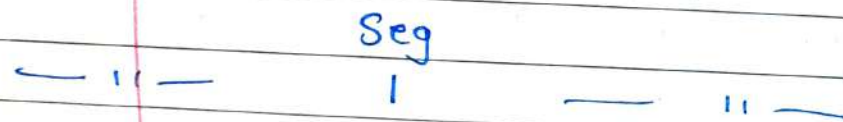
For quarterwave monopole

$$L = \lambda_{\text{wavelength}} / 4$$

Geometry.



Source / Load



Freq<sup>n</sup> / Gnd

Environment - perfect ground

For quarterpole dipole at  $f = 500 \text{ MHz}$

- ① Gain = 5.18 dB
- ② HPBW = 40 dg
- ③ Impedance =  $40.3 + j23.6 \Omega$



# Expt. 3

Study of effect of variation of length of linear wire antenna on radiation pattern and associated parameters.

Symbols

$$\lambda = 1$$

$$\lambda = \frac{c}{f}$$

$$L = \lambda / 4$$

$$f = \frac{c}{\lambda} = \frac{3 \times 10^8}{1} = 300 \text{ MHz}$$

Geometry

$$\lambda = 1 \text{ m}$$

Type	Tag	Segs	X <sub>1</sub>	Y <sub>1</sub>	Z <sub>1</sub>	X <sub>2</sub>	Y <sub>2</sub>	Z <sub>2</sub>	Radius
wire	1	27	0	0	-L/2	0	0	L/2	0.0001

Serial

no. of wire

Source / Load

Type	Tag	Segs	(opt)	Real	Imag	Magn	Phase (deg)
vtg-src	1	14	00	1	0	1	0

Freq/ Ground

$$\text{Frequency} = 300 \text{ MHz}$$

Environment = Freespace

Far - field ~~region~~ pattern

$$\begin{bmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{bmatrix} \quad \begin{bmatrix} b_1 \\ b_2 \\ b_3 \end{bmatrix}$$

Observation Table:-

Sr. No.	Length of Linear wire antenna	HPBW		Gain (in dB)
		Theoretical	Practical	
1.	$\lambda/4$	87dg	90dg	1.85dB
2.	$\lambda/2$	78dg	80dg	2.17dB
3.	$3\lambda/4$	64dg	60dg	2.8dB
4.	$\lambda$	47.8dg	50dg	3.19dB
5.	$1.25\lambda$	---	30dg	5.09dB

↓ HPBW = Directivity ↑

Gain =

$$G = e \cdot d.$$

Efficiency × Directivity  
of antenna of antenna

Restrict length of  $\lambda$  upto  $1\lambda$ .

∴ there will not be any side lobes.

Q.6) Why log periodic antenna is so called?

In a case of log periodic antenna, the electric properties of the antenna are varying periodically with respect to logarithm of freq<sup>n</sup> ( $\log f$ ). Hence it is so called.

Q.7) The normalised field pattern of a certain antenna is given by  $E(\theta) = \sin\theta$  for  $0 \leq \theta \leq \pi$ , where  $\theta$  is in radians. Compute 3dB beamwidth for this antenna.



Title:- Principle of pattern multiplication.

Aim:- To understand & verify principle of pattern multiplication for a given antenna array configuration.

Software used:-  
~~Mat~~ Scilab.

§  
| Theory:-  
Statement of principle of pattern multiplication

Case 1 : An array of 4 isotropic point sources fed with equal amplitude & equal phase separated by  $d = \lambda/2$ .  
Step 1 to 5.

Case 2 :- An — " — equal amplitude & opposite phase separated by  $d = \lambda/2$ .  
Step 1 to 5.

O/p :- Program print. Case 1 & 5. Case 2  
O/p print (Plot). both.

Conclusion:- Take batch 3.

for Case 1:-

// Principle of Pattern Multiplication.

clear;

clc ;

lambda = 1;

d = lambda / 2;

beta = (2 \* %pi) / lambda ;

delta = 0; // defining delta as a phase of difference between dipoles.

phi = 0: 0.01: 2 \* %pi ; // Variation of the theta from 0 to 360 degrees.

subplot (2, 2, 1);

EP = cos (%pi / 2 \* (cos (phi)));

polarplot (phi, abs(EP)); // plot of single element pattern.

title ('Element ELEMENT PATTERN');

AF = cos(%pi \* (cos(phi) + delta)) // Expression for an Array Factor

subplot (2, 2, 2);

polarplot (phi, abs(AF)); // plot of Array pattern.

title ('ARRAY FACTOR PATTERN');

subplot (2, 2, 3.5);

polarplot (phi, abs(EP) .\* abs(AF));

// Plot of Total Field Pattern of Array.

title ('TOTAL ARRAY PATTERN');

for case 2

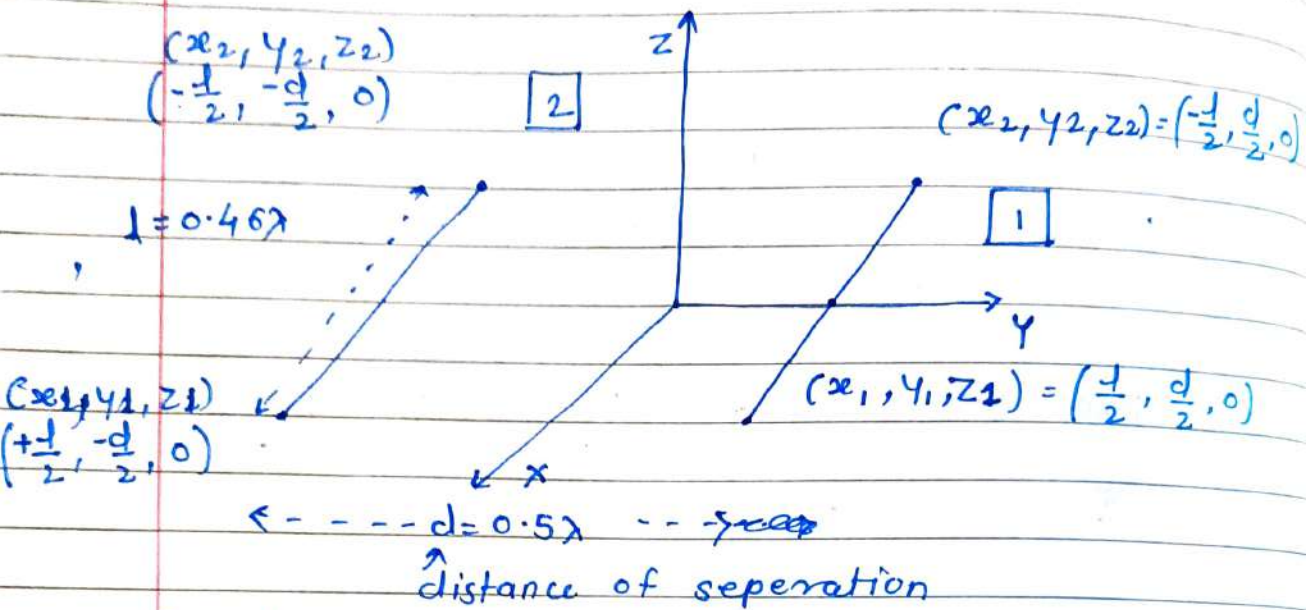
just change

EP = sin (%pi / 2 \* (cos(phi)));



Title:- Performance comparison of broadside array and endfire array.

Two element antenna array.



Broad	Real	Real	Imag
1	1	1	-1
			0

\*End fire \*

Symbols:-  $\lambda = 1$

$$L = 0.5 \times 0.46 \times \lambda$$

$$d = 0.5 \times \lambda$$

Geometry:

Type	Tag	Segs	$x_1$	$y_1$	$z_1$	$x_2$	$y_2$	$z_2$	Radius
Wire	1	27	$\frac{\lambda}{2}$	$\frac{d}{2}$	0	$-\frac{\lambda}{2}$	$\frac{d}{2}$	0	0.001
Wire	2	27	$\frac{\lambda}{2}$	$-\frac{d}{2}$	0	$-\frac{\lambda}{2}$	$-\frac{d}{2}$	0	0.001

Source/Load

Type	Tag	Seg.	(opt)	Real	Imag	Magn	Phase
vtg-src	1	14	00	1	0	1	0
vtg-src	2	14	00	-1	0	1	0

Time varying excitation

Freq/ Ground

$f = 300 \text{ MHz}$

Environment  
Free space.

\* For Broadside \*

Remain all settings are same only change in  
Source / Load:-

Type	Tag	Seg	(opt)	Real	Imag	Magn	Phase
Vtg-Src	1	14	00	1	0	1	0
Vtg-Src	2	14	00	1	0	1	0

10/13/2023

Expt 7

Study of circular loop antenna.

Types of Loop antenna.

Electrically small

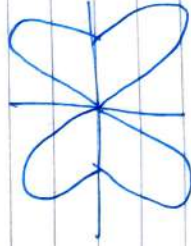
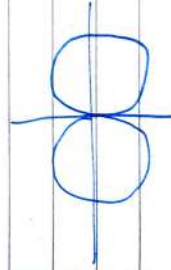
$$D < \frac{\lambda}{10}$$

Electrically large

$$D \geq \lambda$$

$$C_{\lambda} = \frac{C}{\lambda} = \frac{\pi D}{\lambda} < 0.314$$

$$C_{\lambda} = \frac{C}{\lambda} = \frac{\pi D}{\lambda} \geq 3.14$$





For single turn small loop antenna.

$$R_r = 20 \pi^2 \left( \frac{C}{\lambda} \right)^4$$

where  $C = 2\pi a$  is circumference of loop antenna  
For N turns

$$R_r = 20 \pi^2 N^2 \left( \frac{C}{\lambda} \right)^4$$

for large loop ( $C > 3.14 \lambda$ ) Antenna

$$R_r = 60 \pi^2 \left( \frac{C}{\lambda} \right)$$

Symbols:-

$$\lambda = 300 \text{ MHz}$$

$$D = \lambda / 10$$

Geometry

Type	Tag	Segs	Arc-rad	Angl-1	Angl-2	Wire-rad
Arc	1	50	D/2	0	360	0.0001

Source / load

Type	Tag	seg	(opt)	Real	Imag	Magn	Phase
vtgsrc	1	1	00	1	0	1	0

Freq/Gnd

$$F = 300 \text{ MHz}$$

Free-space.

Far-field pattern.

## Observation Table

Sr.No.	Loop Diameter (D)	Max. Gain (in dBi).
1.	$\lambda/10$	1.55
2.	$\lambda/8$	1.47
3.	$\lambda/4$	2.53
4.	$\lambda/2$	3.85
5.	$\lambda$	4.14

Caparison of different circular loop antenna.

Case i) -  $L \approx D (D) = \lambda/10$

Structure  
(Hide pattern)

3D pattern  
(Multicolor)

fig. Loop antenna structure and  
3d radiation pattern.

Vertical plane      Horizontal plane.

fig. 2D vertical & hori field patterns  
of loop antenna.



# Very Very Important

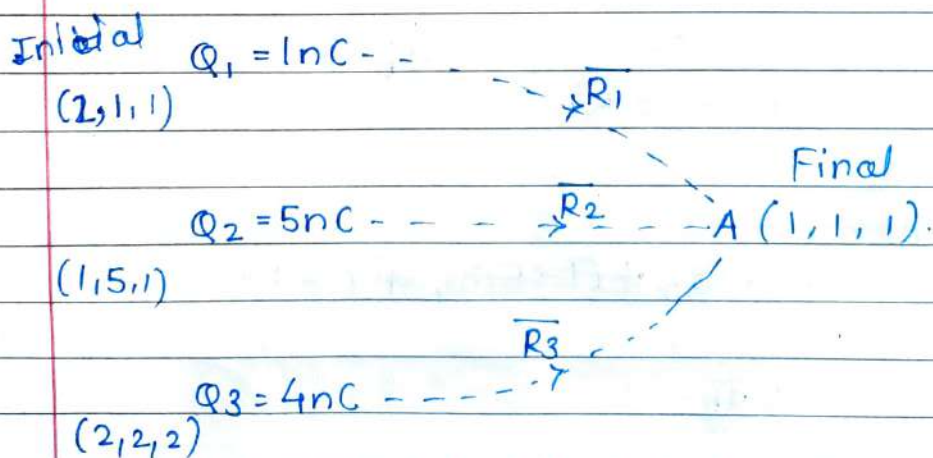
Cartesian	Cylindrical	Spherical.
Differential in length $dL = dx a_x + dy a_y + dz a_z$	$dL = ds a_s + s d\phi a_\phi + dz a_z$	$dL = dr a_r + r d\theta a_\theta + r \sin\theta d\phi a_\phi$
Differential surface.		
$dS_x = dy dz a_x$ $dS_y = dx dz a_y$ $dS_z = dx dy a_z$	$dS_p = s d\phi dz a_s$ $dS_\phi = ds dz a_\phi$ $dS_z = s d\phi ds a_z$	$dS_r = r^2 \sin\theta d\theta d\phi a_r$ $dS_\theta = r \sin\theta dr d\phi a_\theta$ $dS_\phi = r dr d\theta a_\phi$
Differential Volume $dV = dx dy dz$	$dV = s ds d\phi dz$	$dV = r^2 \sin\theta dr d\theta d\phi$

17/3/2023

## Expt. 8

Study of Principle of superposition for calculation of Electric Field Intensity due to 'N' point charges

EQ. 1) Calculate the electric field intensity at point A(1,1,1) due to three point charges each of magnitude 1nC, 5nC, 4nC located at (2,1,1); (1,5,1) and (2,2,2) respectively.



$$\vec{E}_1 = \frac{Q_1}{4\pi \cdot \epsilon_0 R_1^2} \cdot \vec{a}_{R_1}$$

But here,

$$\vec{R}_1 = (1-2)\vec{a}_x + (1-1)\vec{a}_y + (1-1)\vec{a}_z$$

$$|\vec{R}_1| = \sqrt{(-1)^2} = 1$$

$$\vec{a}_{R_1} = \frac{\vec{R}_1}{|\vec{R}_1|} = \frac{-\vec{a}_x}{1} = -\vec{a}_x$$

Now,  $\vec{E}_1 = 8.98 (-\vec{a}_x) \text{ V/m}$

$$\vec{E}_1 = \frac{1 \times 10^{-9}}{4\pi \times (8.854 \times 10^{-12}) \times 1} \vec{a}_x$$

$$\boxed{\vec{E}_1 = 8.98 (-\vec{a}_x) \text{ V/m}}$$

$$* \boxed{\vec{E}_1 = -8.98 \vec{a}_x \text{ V/m}}$$

$$\vec{E}_2 = \frac{Q_2}{4\pi \cdot \epsilon_0 R_2^2} \cdot \vec{a}_{R_2}$$

But here,

$$\vec{R}_2 = (1-1)\vec{a}_x + (1-5)\vec{a}_y + (1-1)\vec{a}_z$$

$$= -4\vec{a}_y$$

$$|\vec{R}_2| = \sqrt{(-4)^2} = 4$$



$$\bar{a}_{R_2} = \frac{\bar{R}_2}{|\bar{R}_2|} = \frac{-\bar{a}_y}{4} = -\frac{1}{4}\bar{a}_y - \bar{a}_y$$

$$\bar{E}_2 = \frac{5 \times 10^{-9}}{4\pi \times (8.854 \times 10^{-12}) \times (4)^2} (-\bar{a}_y)$$

$$\boxed{\bar{E}_2 = -2.808 \bar{a}_y \text{ V/m}}$$

$$\bar{E}_3 = \frac{Q_3}{4\pi \epsilon_0 R^2} \bar{a}_{R_3}$$

But here,

$$\begin{aligned} \bar{R}_3 &= (1-2)\bar{a}_x + (1-2)\bar{a}_y + (1-2)\bar{a}_z \\ &= -\bar{a}_x - \bar{a}_y - \bar{a}_z \end{aligned}$$

$$|\bar{R}_3| = \sqrt{(-1)^2 + (-1)^2 + (-1)^2} = \sqrt{3}$$

$$\bar{a}_{R_3} = \frac{\bar{R}_3}{|\bar{R}_3|} = \frac{-\bar{a}_x - \bar{a}_y - \bar{a}_z}{\sqrt{3}}$$

$$\begin{aligned} \bar{E}_3 &= \frac{4 \times 10^{-9}}{4\pi \times (8.854 \times 10^{-12}) \cdot (\sqrt{3})^2} \cdot \frac{-\bar{a}_x - \bar{a}_y - \bar{a}_z}{\sqrt{3}} \\ &= \frac{11.983 \cdot (-\bar{a}_x - \bar{a}_y - \bar{a}_z)}{\sqrt{3}} \end{aligned}$$

$$\boxed{\bar{E}_3 = -6.9187(\bar{a}_x + \bar{a}_y + \bar{a}_z) \text{ V/m}}$$

$$\boxed{\bar{E}_3 = -6.9187(\bar{a}_x + \bar{a}_y + \bar{a}_z) \text{ V/m}}$$

$$= -6.9187\bar{a}_x - 6.9187\bar{a}_y - 6.9187\bar{a}_z \text{ V/m}$$

$$|\vec{E}_1| = \sqrt{(8.98)^2} = 8.98 \text{ V/m}$$

$$|\vec{E}_2| = \sqrt{(-2.808)^2} = 2.808 \text{ V/m}$$

$$|\vec{E}_3| = \sqrt{(-6.9187)^2 + (-6.9187)^2 + (-6.9187)^2} = 11.983 \text{ V/m}$$

By principle of Superposition.

$$\vec{E} = \vec{E}_1 + \vec{E}_2 + \vec{E}_3$$

$$\vec{E} = (8.98 + 2.808 + 11.983) \text{ V/m}$$

$$\vec{E} = 23.771 \text{ V/m}$$

// Program for Electric Field Intensity due to <sup>N</sup> point charges

clc; clear all;

N = input('Enter the number of point charges: ');

p = input('Enter the coordinates of a point at which  
E is to be calculated in the form [x y z]: ');

eps0 = input('Enter the value of permittivity of  
the medium: ');

E = 0;

for M = 1:N

Q = input('Enter the magnitude of a point charge: ');

T = input('Enter the point at which charge is  
located as [x y z]: ');

R = norm(P - T);

EN = Q / (4 \* % pi \* eps0 \* R \* R);

E = E + EN

end

disp('The Resultant Electric Field Intensity =', E, 'V/m');



Selement Yagi Uda antenna:-

Symbols:-

where  $\lambda = 0.75$  for  $f = 400 \text{ MHz}$

$$A_{ct} = 0.48 \times \lambda$$

$$R_{ef} = 0.525 \times \lambda$$

$$D_{ir1} = 0.42 \times \lambda$$

$$D_{ir2} = 0.4 \times \lambda$$

$$D_{ir3} = 0.37 \times \lambda$$

$$S_1 = 0.2 \times \lambda$$

$$S_2 = 0.3 \times \lambda$$

$$S_3 = 0.55 \times \lambda$$

$$S_4 = 0.8 \times \lambda$$

$$H = \lambda$$

Geometry

Type	Tag	Segs	X1	Y1	Z1	X2	Y2	Z2	Radius
Wire	1	21	0	$-A_{ct}/2$	H	0	$A_{ct}/2$	H	0.0001
—  —	2	21	$+S_1$	$-R_{ef}/2$	H	$S_1$	$R_{ef}/2$	H	—  —
—  —	3	21	$-S_2$	$-D_{ir1}/2$	H	$S_2$	$D_{ir1}/2$	H	—  —
—  —	4	21	$-S_3$	$-D_{ir2}/2$	H	$S_3$	$D_{ir2}/2$	H	—  —
—  —	5	21	$-S_4$	$-D_{ir3}/2$	H	$S_4$	$D_{ir3}/2$	H	—  —

Source / Load

Type	Tag	Seg	(opt)	Real	Img	Magn	Phase
Vtg-src	1	11	00	1	0	1	0

Freq / Gnd

$F = 400 \text{ MHz}$

Environment

→ Free Space.

Far field pattern.

3 element Yagi-Uda antenna:-

Symbols:-

$$\lambda = 0.75$$

$$A_{eff} = 0.48 \times \lambda$$

$$R_{eff} = 0.525 \times \lambda$$

$$D_{eff} = 0.42 \times \lambda$$

$$S_1 = 0.2 \times \lambda$$

$$S_2 = 0.3 \times \lambda$$

$$H = \lambda$$

Geometry

Type	Tag	Seg	X <sub>1</sub>	Y <sub>1</sub>	Z <sub>1</sub>	X <sub>2</sub>	Y <sub>2</sub>	Z <sub>2</sub>	Radius
Wire	1	21	0	-A <sub>eff</sub> /2	z	0	A <sub>eff</sub> /2	H	0.0001
-  -	2	21	S <sub>1</sub>	-R <sub>eff</sub> /2	z	S <sub>1</sub>	R <sub>eff</sub> /2	H	0.0001
-  -	3	21	-S <sub>2</sub>	-D <sub>eff</sub> /2	z	-S <sub>2</sub>	-D <sub>eff</sub> /2	H	0.0001

Source / Load

Type	Tag	Seg	(opt)	Real	Img	Mag	Phase
Vtg-src	1	11	00	1	0	1	0

Freq / Gnd

$$F = 400 \text{ MHz}$$

Environment

Free space

Far field pattern.