

A Pseudo Plane-wave Gravitational Calibrator for Gravitational Wave Observatories

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Gravitational calibration has recently gained interest as a possible improvement to gravitational wave observatories. The precision of existing gravitational calibrators are limited by their dependence on the relative position between the calibrators and the test masses. Here we present a novel geometry consisting of four quadrupole rotors placed at the vertices of a rectangle centered on the test mass. The phases and rotation directions are selected to produce a pseudo plane-wave sinusoidal gravitational acceleration with amplitude of 101.42 fm/s^2 . This acceleration has minimal positioning dependence and can yield $\sim 0.1\%$ acceleration amplitude uncertainty for $\sim 1 \text{ cm}$ test mass positioning uncertainty. In addition, these rotors have significant engineering and safety benefits due to their small size and eliminates the torques acting on the test mass.

I. INTRODUCTION

Gravitational wave astronomy has blossomed into a novel method to observe the universe. The number of gravitational wave observations is expected to grow substantially in the coming years with the continued operation of the LIGO [1] and Virgo [2] interferometers as well the future addition of LIGO-India [3] and the further improvements of KAGRA [4].

These interferometers must be precisely calibrated in order to accurately interpret gravitational wave signals. Whether for binary merger parameter estimation [5], cosmological measurements [6, 7], or searches for deviations from general relativity [8], the strain readouts of the observatories must be precisely and accurately calibrated.

Thus far, the calibration of the current observatories has been accomplished with photon pressure [9]. These photon calibration systems have yielded absolute calibrations with $\sim 0.5\%$ uncertainty and have acted as versatile calibration tools.

Calibrating with a gravitationally induced strain has long been suggested as an alternative calibration technique [10–15] and has recently been explored at many of the observatories [16–19]. Gravitational calibration has the promise of improving the absolute calibration of the observatories by achieving higher-precision injections. Additionally, gravitational calibrators can work in concert with photon calibrators to yield a combined calibration with lower uncertainty.

The geometries explored with current gravitational calibrators [16–19] produce accelerations that have large dependence on the radial distance, r , between the rotor and the test mass. The acceleration is typically proportional to $\sim 1/r^{l+2}$ where l is the order of the dominate mass-multipole moment. For example, a rotor with a

quadrupole mass distribution ($l = 2$) will follow $\sim 1/r^4$. This strong positioning dependence causes the performance of the absolute calibration to be limited by the precision of the positioning measurements.

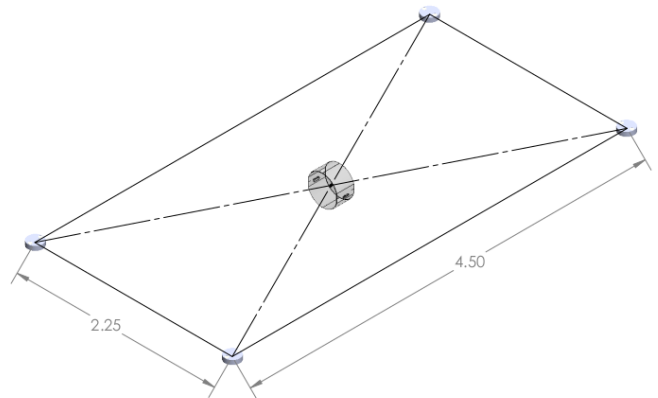


FIG. 1. A rendering of the geometry of the rotors with the test mass at the center of the rectangle.

Here, we present a novel geometry consisting of four quadrupole rotors that produces a pseudo plane-wave gravitational acceleration. This geometry produces an acceleration which has minimal first-order dependence on the position of the rotors allowing for improved calibration precision with limited positioning precision. Additionally, this geometry eliminates the torques acting on the test mass and eases much of the engineering and safety concerns of previous rotors.

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Parameter	Mean	Uncertainty
Cylinder Mass	1 kg	0.3 g
Cylinder Radius	2 cm	$2.5 \mu\text{m}$
Cylinder Length	5 cm	$5 \mu\text{m}$
Quadrupole Radius	6 cm	$5 \mu\text{m}$
Test Mass	40 kg	10 g
Test Mass Length	200 mm	0.1 mm
Test Mass Radius	170 mm	0.05 mm
Test Mass Flat Width	327 mm	0.05 mm
Rotor Positions	$(\pm 2.25 \text{ m}, \pm 1.125 \text{ m}, 0 \text{ m})$	(1 mm, 1 mm, 1 mm)
Test Mass Position	(0 m, 0 m, 0 m)	(1 cm, 1 cm, 1 cm)

TABLE I. Parameters describing the rotors, the test mass, and their respective positions.

II. GEOMETRY

The pseudo plane-wave calibrator consists of four identical rotors placed at the vertices of a 2.25-m by 4.50-m rectangle centered on the test mass. Figure 1 shows a rendering of the geometry. The rotors are designed with the similar dimensions as the LIGO NCal [19] but without a hexapole mass arrangement. Each rotor is a 17 cm diameter, 5 cm tall aluminum disk with two holes cut at a radius of 6 cm separated by 90° . These holes are filled in with 4 cm diameter, 5 cm tall tungsten cylinders which produce a quadrupole mass distribution. The parameters of the geometry are displayed in Table I.

The parameters that are common with the LIGO NCal are assigned uncertainties equal to what was previously achieved [19]. The rest of the parameters are assigned uncertainties based on what is reasonably achievable with standard measurement techniques. For example, since the rotors would be outside the interferometer's vacuum system, their positions can be readily measured to the mm-precision with standard surveying equipment.

The relative phases of the rotors and the rotation directions are set to achieve pseudo plane-wave nature. The four rotor with a positive x-coordinate are rotated by 90° from the rotors with negative x-coordinate. Additionally, the rotors with positive y-coordinate rotate clockwise while those with negative y-coordinates rotate counter-clockwise.

III. ENGINEERING SIMPLICITY

Since the four rotor array produces more acceleration at a given separation than a single rotor, the array can be placed at a larger radius to produce a similar amplitude acceleration on the test mass. This allows the array to place well away from the existing infrastructure of the

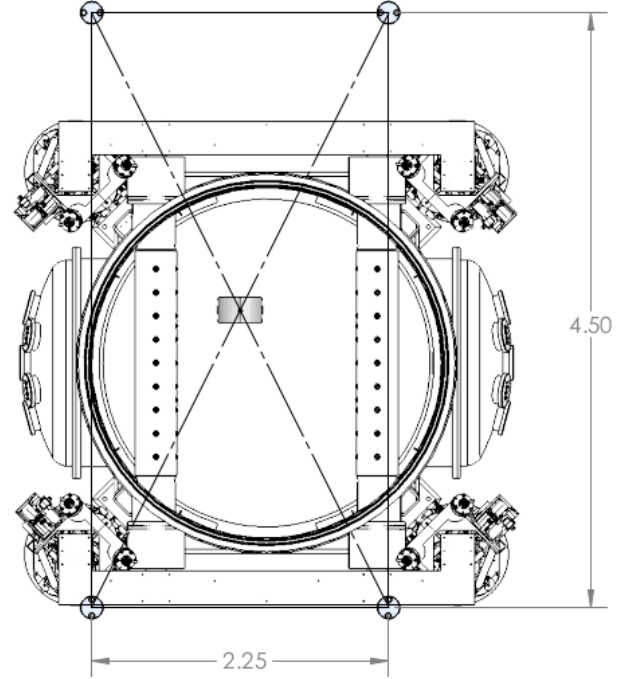


FIG. 2. A rendering of the geometry of the rotors around the LIGO BSC chamber.

observatories. Here we have chosen a geometry that fits around the LIGO BSC vacuum chamber and seismic isolation system, as shown in Figure ???. This significantly simplifies the structure that holds the rotors as it does not need to be incorporated into the existing structural components. Additionally, placing the rotors at a larger distance decreases the concerns of damaging the vacuum chamber or isolation in the unlikely scenario that a rotor catastrophically fails.

The use of only quadrupole mass distributions further

decreases the safety concerns as the rotors have a smaller radius than similar rotors with multiple multipole mass distributions. This smaller radius decreases the rotor's kinetic energy thus decreasing the likelihood of a catastrophic failure. Due the decreased moment of inertia, a

smaller radius also decreases the torques needed to spin the rotor up and maintain a fixed rotation speed which loosens the requirements on the drive motor as well as decreases spurious electromagnetic effects caused by the motors.

Parameter	Mean	Uncertainty	Fractional Contribution
Cylinder Mass	1 kg	0.3 g	3.40×10^{-4}
Cylinder Radius	2 cm	$2.5 \mu\text{m}$	1.80×10^{-8}
Cylinder Length	5 cm	$5 \mu\text{m}$	2.52×10^{-8}
Quadrupole Radius	6 cm	$5 \mu\text{m}$	1.97×10^{-4}
Test Mass	40 kg	10 g	2.83×10^{-4}
Test Mass Length	200 mm	0.1 mm	3.50×10^{-6}
Test Mass Radius	170 mm	0.05 mm	4.78×10^{-6}
Test Mass Flat Width	327 mm	0.05 mm	1.74×10^{-15}
Rotor Positions	($\pm 2.25 \text{ m}$, $\pm 1.125 \text{ m}$, 0 m)	(1 mm, 1 mm, 1 mm)	1.04×10^{-3}
Test Mass Position	(0 m, 0 m, 0 m)	(1 cm, 1 cm, 1 cm)	1.51×10^{-4}
Quadrature Sum			1.15×10^{-3}

TABLE II. Individual uncertainty contributions for the input parameters of the simulation.

IV. PSEUDO PLANE-WAVE NATURE

To verify the performance of such a rotor array, we simulated the system with a finite-element analysis using the *PointGravity* algorithms of the **newt** libraries [20, 21]. This simulation breaks each of the rotor cylinders and the test mass into independent clouds of point masses. The force between each pair of point masses, one from the rotors and the other from the test mass, is calculated. The forces from the individual pairs of point masses is then summed to yield the acceleration in all three directions. We extract only the x-acceleration as this is the primary sensitive direction of the interferometer.

The superposition of the gravitational fields from the four rotors produces an oscillating gravitational acceleration field which at the center of the rectangle is only in the x-direction and has an amplitude of 101.42 fm/s^2 . This amplitude corresponds to a strain of 7.1×10^{-22} at 30 Hz for a 4-km long interferometer. Note that although the acceleration amplitude is frequency independent, the strain amplitude will follow $\sim 1/f^2$. The acceleration field changes weakly with deviations from the center of the rectangle (i.e. a pseudo plane-wave). The percentage change in acceleration amplitude verse offset from the center of the rectangle is shown in Figure 3 for offsets in each direction. A relatively large offset of 10 cm in any direction changes the acceleration by $< 1\%$. Additionally, the change in amplitude is well-described by

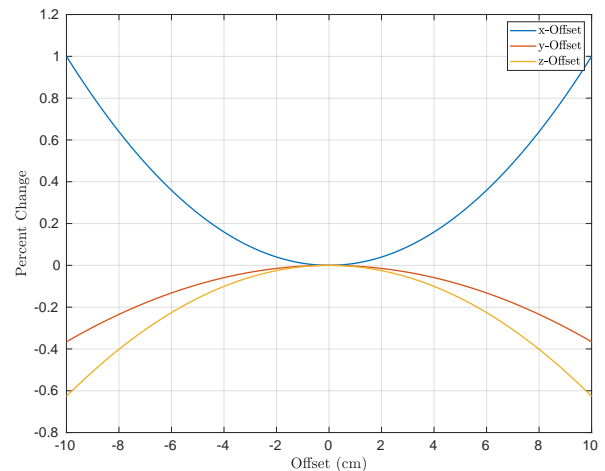


FIG. 3. The percentage change of acceleration amplitude with a test mass offset from the center of the rectangle.

a parabola for small offsets displaying the second-order nature of this effect.

Since the rotor array is in-plane and symmetric about the x-z plane, the rotors apply no net torque on the test mass. If the array is out-of-plane then the test mass would experience a torque about the y-axis. Similarly, if

the array is asymmetric it would apply a z-axis torque. Such torques are common in existing gravitational calibrators and can substantially impact the precision of the subsequent calibrations.

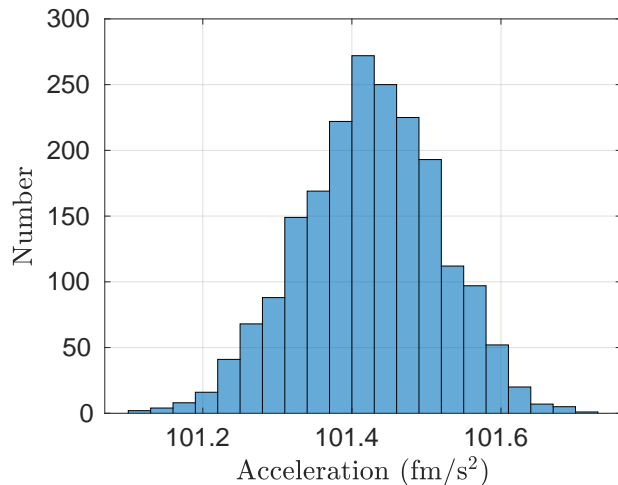


FIG. 4. Distribution of predicted accelerations.

V. NUMERICAL UNCERTAINTY ANALYSIS

Since the performance of such a calibrator does not only depend on the test mass offset, we performed a Monte Carlo simulation of the applied acceleration to accounting for the set of parameters which describe the calibrator. We model each parameter as a Gaussian distribution centered on the mean listed in Table I with σ -value equal to the uncertainty. The acceleration of the test mass is then calculated with parameters sampled from these distributions. This is repeated 2000 times to yield a distribution of the gravitational acceleration, shown in Figure 4, which takes into account all non-linearities and

degeneracies.

The simulation yields an injected acceleration of $a = 101.42 \pm 0.10 \text{ fm/s}^2$ (0.09 %) where the central value is the mean and the uncertainty is the 68%-interval. To assess how each parameter contributes to this total uncertainty, the acceleration uncertainty was recomputed with only one parameter varying. This was then repeated for each parameter to yield the results in Table II. All four rotor positions were simultaneously varied in all three directions and the test mass position was also varied in all three directions.

Table II shows the acceleration uncertainty is strongly dominated by the rotor positions with the test mass position contribution being 3.5 times smaller. This contribution may be further reduced with a precision machined mounting frame for the rotors or with higher precision surveying than is assumed here.

VI. CONCLUSION

We have described an four-rotor gravitational calibrator that causes a psuedo-plane wave acceleration field. Simulation of the acceleration amplitude uncertainty shows that such a system can achieve $\sim 0.1\%$ precision absolute calibration injections. This is approximately an order of magnitude improvement over previously deployed geometries.[19]

Gravitational calibration is a promising avenue for high precision absolute calibration of gravitational wave observatories. By deploying arrays which minimize the first-order contributions of the applied gravitational field around the test mass, such calibrators may exceed the performance of excising calibration techniques.

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