



**higher education
& training**

Department:
Higher Education and Training
REPUBLIC OF SOUTH AFRICA

MARKING GUIDELINE

NATIONAL CERTIFICATE MECHANOTECHNICS N4

12 August 2021

This marking guideline consists of 8 pages.

NOTE: ✓ half mark
✓ full mark

QUESTION 1

- 1.1
- Multi-purpose machines ensure flexibility of production
 - Production is not limited to certain work processes
 - Machines can be fully utilised
 - There is no interruption if one machine breaks down
 - Faulty parts found during inspection are not rejected
 - Effective control over manufacturing cost

(Any 5 × 1) (5)

Please check – the above seems to be incorrect

- 1.2 1.2.1 Air spray painting

(1)

- 1.2.2
- A – Air pressure
 - B – Spray nozzle
 - C – Suction pipe
 - D – Paint

(4)

- 1.3
- Gravity-feed lubrication
 - Grease lubrication
 - Splash lubrication
 - Forced lubrication
 - Pressure-feed lubrication

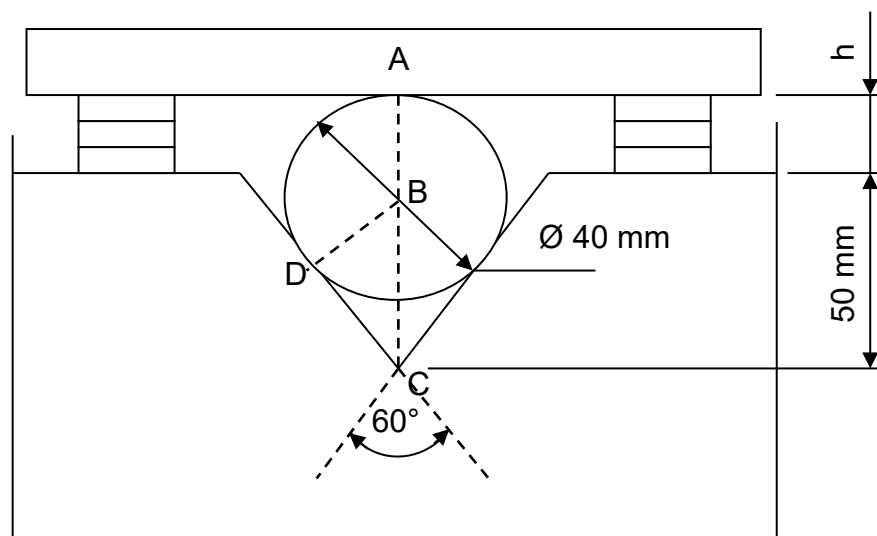
(5)

[15]**QUESTION 2**

- 2.1
- 1 – Straight edge
 - 2 – Gauge block
 - 3 – Roller
 - 4 – V-block

(4)

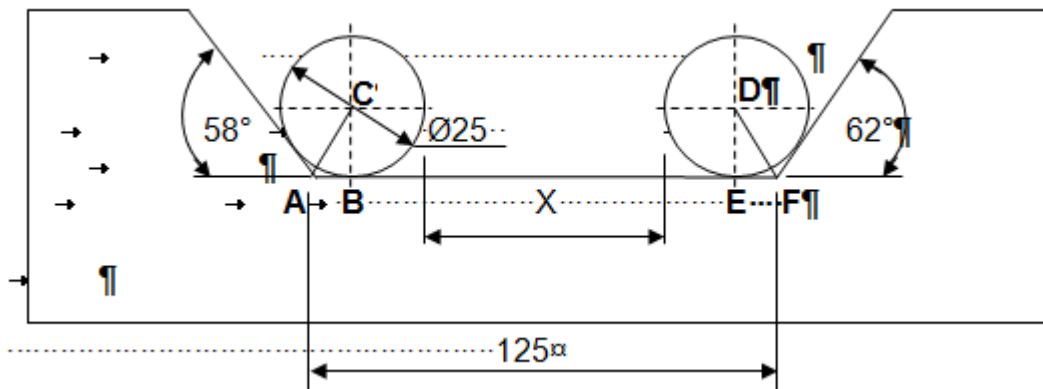
2.2



$$\begin{aligned}
 h &= AC - 50 & \text{OR } h + 50 &= AB + BC \\
 AC &= AB + BC & h + 50 &= 20 + BC \\
 BC \text{ in } BCD & & BC &= \frac{20}{\sin 30^\circ} \\
 \sin \theta &= \frac{BD}{BC} & &= 40 \text{ mm} \\
 BC &= \frac{20}{\sin 30^\circ} \checkmark & h + 50 &= 20 + 40 \\
 &= 40 \text{ mm} \checkmark & h &= 60 - 50 \\
 AC &= AB + BC & h &= 10 \\
 AC &= 40 + 20 \checkmark \\
 N_D &= 1000 \text{ r/min} \checkmark \\
 h &= AC - 50 \\
 &= 60 - 50 \checkmark \\
 &= 10, \text{ mm} \checkmark
 \end{aligned}$$

(6)

2.3



$$\begin{aligned}
 X &= 125 - 2r - AB - EF \checkmark \\
 r &= 12,5 \checkmark
 \end{aligned}$$

$$\text{In } \triangle ABC \tan 61^\circ = \frac{12,5}{AB} \checkmark$$

$$\begin{aligned}
 AB &= \frac{12,5}{\tan 61^\circ} \\
 AB &= 6,929 \text{ mm} \checkmark
 \end{aligned}$$

$$\text{In } \triangle DEF \tan 59^\circ = \frac{12,5}{EF}$$

$$\begin{aligned}
 EF &= \frac{12,5}{\tan 59^\circ} \\
 EF &= 7,511 \text{ mm} \checkmark
 \end{aligned}$$

$$\begin{aligned}
 X &= 125 - 2r - AB - EF \\
 X &= 125 - 2(12,5) - 6,929 - 7,511 \\
 X &= 85,56 \text{ mm} \checkmark
 \end{aligned}$$

(5)
[15]

QUESTION 3

$$\begin{aligned}
 3.1 \quad PCD_{pinion} &= mxT_{pinion} \\
 &= 6 \times 30 \\
 &= 180mm \checkmark
 \end{aligned}$$

$$VR = \frac{5}{3}$$

$$T_A = \frac{5}{3} T_B \checkmark$$

$$\begin{aligned}
 T_A &= \frac{5}{3} \times 30 \checkmark \\
 &= 50 \text{ teeth} \checkmark
 \end{aligned}$$

$$\begin{aligned}
 PCD_B &= mxT_{Gear} \\
 &= 6 \times 50 \\
 &= 300mm \checkmark
 \end{aligned} \tag{5}$$

$$\begin{aligned}
 3.2 \quad C &= \frac{m}{2} (T_A + T_B) \\
 C &= \frac{6}{2} (50 + 30) \checkmark \\
 &= 240mm \checkmark
 \end{aligned} \tag{2}$$

$$\begin{aligned}
 3.3 \quad D_{OA} &= mx(T_A + 2) \\
 D_{OA} &= 6 \times (50 + 2) \checkmark \\
 &= 312mm \checkmark \\
 D_{OB} &= mx(T_A + 2) \\
 D_{OB} &= 6 \times (30 + 2) \checkmark \\
 &= 192mm \checkmark
 \end{aligned} \tag{4}$$

$$\begin{aligned}
 3.4 \quad Depth_{Total} &= addendum + dedendum \\
 Addendum &= 6mm \checkmark \\
 Dedendum &= 1,157xm \\
 &= 1,157 \times 6 \checkmark \\
 &= 6,942mm \checkmark \\
 Depth_{Total} &= 6 + 6,942 \\
 &= 12,942mm \checkmark
 \end{aligned} \tag{4}$$

[15]

QUESTION 4

$$\begin{aligned}
 4.1 \quad v &= \frac{\pi(D+t)N}{60} \\
 &= \frac{\pi(0,6 + 0,02) \times 600}{60} \checkmark \\
 &= 19,478 \text{ m/s} \checkmark \\
 T_C &= mv^2 \\
 &= 0,5(19,478)^2 \\
 &= 189,696 \text{ N} \checkmark
 \end{aligned}
 \tag{3}$$

$$\begin{aligned}
 4.2 \quad T_1 &= \sigma \cdot w \cdot t \\
 &= 4 \times 10^6 \times 0,155 \times 0,02 \checkmark \\
 &= 12400 \text{ N} \checkmark
 \end{aligned}
 \tag{2}$$

[5]

QUESTION 5

$$\begin{aligned}
 5.1 \quad v_1 x A_1 &= v_2 x A_2 \\
 v_1 &= \frac{v_2 x A_2}{A_1} \\
 v_1 &= \frac{v_2 \times 0,1}{0,063} \checkmark \\
 v_1 &= 1,587 v_2 \checkmark \\
 \\
 \frac{P_1}{\rho g} + \frac{v_1^2}{2g} + h_1 &= \frac{P_2}{\rho g} + \frac{v_2^2}{2g} + h_2 \\
 \\
 \frac{35000}{10^3 \times 9,81} + \frac{v_1^2}{2 \times 9,81} + 0 &= \frac{55000}{10^3 \times 9,81} + \frac{v_2^2}{2 \times 9,81} + 3 \checkmark \\
 \\
 3,568 + 0,051(v_1)^2 &= 5,607 + 0,051(v_2)^2 + 3 \checkmark \\
 0,051v_1^2 - 0,051v_2^2 &= 5,039 \\
 0,051(v_1^2 - v_2^2) &= 5,039 \checkmark \\
 (v_1^2 - v_2^2) &= \frac{5,039}{0,051} \checkmark \\
 (v_1^2 - v_2^2) &= 98,804 \\
 (1,587v_2)^2 - v_2^2 &= 98,804 \\
 (2,519v_2^2 - v_2^2) &= 98,804 \checkmark \\
 1,519v_2^2 &= 98,804 \\
 v_2^2 &= \frac{98,804}{1,519} \checkmark
 \end{aligned}$$

$$v_2^2 = 65,045$$

$$v_2 = \sqrt{65,045}$$

$$= 8,065 \text{ m/s} \checkmark$$

$$v_1 = 1,587 v_2$$

$$= 1,587 \times 8,065 \checkmark$$

$$= 12,799 \text{ m/s} \checkmark$$

$$Q = v_1 \times A_1$$

$$Q = 12,799 \times \frac{\pi(0,063)^2}{4} \checkmark$$

$$= 0,0399 \text{ m}^3 / \text{s} \checkmark$$

$$= 39,9 \ell / \text{s} \checkmark$$

(14)

5.2

$$A_t = \frac{\pi d_t^2}{4}$$

$$A_t = \frac{\pi 0,045^2}{4}$$

$$A_t = 0,0016 \text{ m}^2 \checkmark$$

$$v_t = \sqrt{2gh}$$

$$v_t = \sqrt{2(9.81)4}$$

$$v_t = 8,859 \text{ m/s} \checkmark$$

$$Q_t = V_t \times A_t$$

$$Q_t = 8,859 \times 0,0016$$

$$Q_t = 0,0142 \text{ m}^3 / \text{s} \checkmark$$

$$C_d = \frac{Q_a}{Q_t}$$

AND

$$Q_a = C_d \times Q_t$$

$$Q_a = 0,64 \times 0,0142 \checkmark$$

$$Q_a = 0,00909 \text{ m}^3 / \text{s} \checkmark$$

$$Q_a = 32724 \ell / \text{h} \checkmark$$

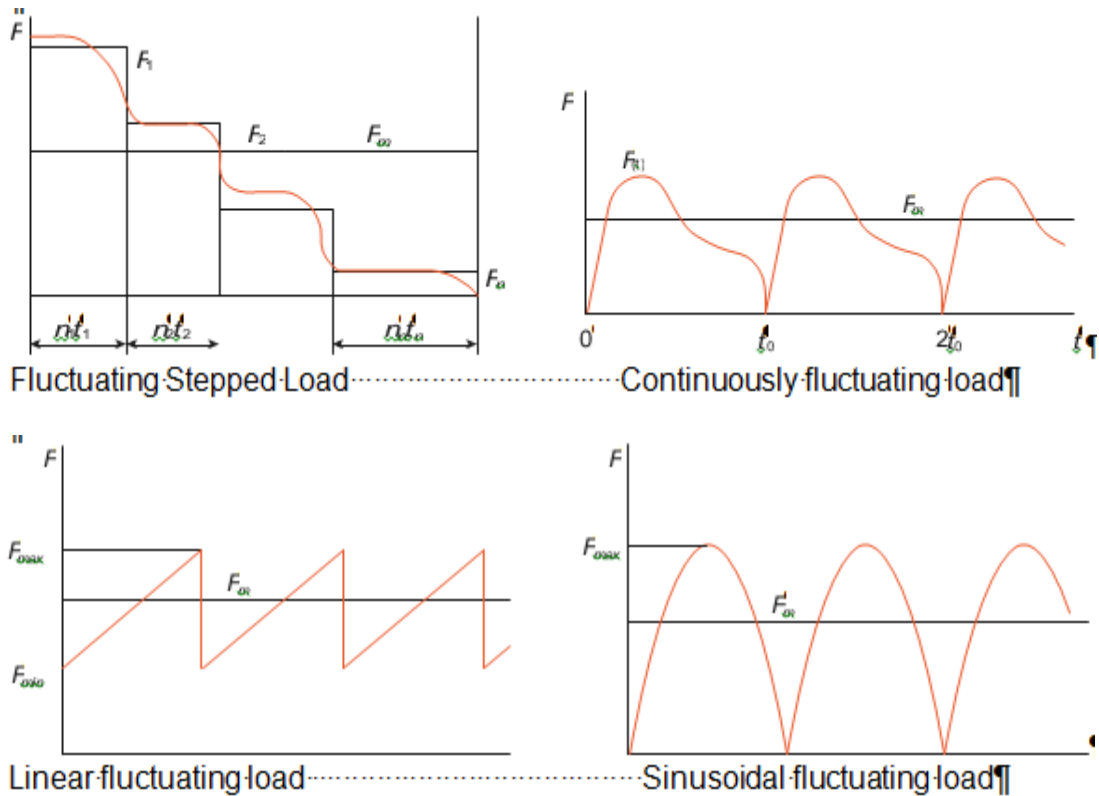
(6)
[20]

QUESTION 6

- 6.1
- Fluctuating stepped load
 - Linear fluctuating load
 - Sinusoidal fluctuating load
 - Continuously fluctuating load

(Any 3 × 1) (3)

6.2



(TWO marks for the correct sketch and TWO marks for the labelling in each graph)

(12)

[15]

I was unable to edit the labelling above – E.g. Fluctuation stepped load NOT Stepped Load

QUESTION 7

7.1 7.1.1
$$P = \frac{2\pi NT}{60}$$

$$\begin{aligned}
 T &= \frac{Px60}{2\pi N} \\
 &= \frac{3000 \times 60}{2\pi \times 1500} \checkmark \\
 &= 19,099 \text{ N.m} \checkmark
 \end{aligned}$$

(2)

7.1.2
$$\eta = \frac{P_o}{P_i}$$

$$\begin{aligned}
 P_o &= 3000 \times 0,8 \checkmark \\
 &= 2400 \text{ W} \checkmark
 \end{aligned}$$

$$\begin{aligned}
 P &= \frac{2\pi NT}{60} \\
 T &= \frac{Px60}{2\pi N} \\
 &= \frac{2400 \times 60}{2\pi \times 3600} \checkmark \\
 &= 6,366 N.m \checkmark
 \end{aligned}
 \tag{4}$$

$$\begin{aligned}
 7.1.3 \quad P &= \frac{2\pi NT}{60} \\
 T &= \frac{Px60}{2\pi N} \\
 &= \frac{2400 \times 60}{2\pi \times 40} \checkmark \\
 &= 572,957 N.m \checkmark
 \end{aligned}
 \tag{2}$$

$$\begin{aligned}
 7.2 \quad 7.2.1 \quad P &= \frac{W}{t} \\
 &= \frac{Fxs}{t} \\
 &= \frac{1200 \times 0,275}{13} \checkmark \\
 &= 25,385 W \checkmark \\
 &= 0,025 kW \checkmark
 \end{aligned}
 \tag{3}$$

$$\begin{aligned}
 7.2.2 \quad T &= Fxr & \text{OR} & \quad v = \frac{\pi DN}{60} \\
 &= 1000 \times 0,175 \checkmark & & \quad v = \frac{\pi(0,35) \times (350)}{60} \checkmark \\
 &= 175 N.m \checkmark & & \quad = 6,414 m/s \checkmark \\
 P &= \frac{2\pi NT}{60} & & \quad P = F \cdot xv \\
 &= \frac{2\pi \times 350 \times 175}{60} \checkmark & & \quad = 1000 \times 6,414 \checkmark \\
 &= 6414,085 W & & \quad = 6414 W \\
 &= 6,414 kW \checkmark & & \quad = 6,414 kW \checkmark
 \end{aligned}
 \tag{4}$$

[15]**TOTAL: 100**