

# **MARKING GUIDELINE**

# NATIONAL CERTIFICATE STRENGTH OF MATERIALS AND STRUCTURES N6

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This marking guideline consists of 10 pages.

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1.1 at 200 mm : 
$$a + \frac{b}{0.2^2} = 25 \times 10^6 \dots \dots (1)$$

at 200 mm : 
$$a - \frac{b}{0.2^2} = -5 \times 10^6 \dots$$
 (2)  $\checkmark$ 

$$(1) + (2) : 2a = 20 \times 10^6$$

$$a = 10 \times 10^6 \checkmark$$

$$b = 600 \times 10^3 \checkmark$$

at 300 mm : 
$$\sigma_R = a + \frac{b}{0.3^2}$$

$$= 10 \times 10^6 + \frac{600 \times 10^3}{0.3^2}$$

$$\sigma_R = 16,667 \text{ MPa} \checkmark \tag{5}$$

1.2 
$$at 300 \text{ mm} : \sigma_H = a - \frac{b}{0.3^2}$$

$$=10\times10^6-\frac{600\times10^3}{0.3^2}$$

$$\sigma_H = 3{,}333 \text{ MPa} \checkmark \text{ (compressive) } \checkmark$$
 (2)

1.3 
$$\sigma_H = 0 \text{ where: } a - \frac{b}{D_r^2} = 0$$

$$10 \times 10^6 - \frac{600 \times 10^3}{D_x^2} = 0$$

$$D_x = 244,949 \text{ mm } \checkmark$$
 (1)

1.4 at 300 mm : 
$$a + \frac{b}{0.3^2} = 16.667 \times 10^6 \dots \dots (1)$$

at 300 mm : 
$$a - \frac{b}{0.3^2} = -65 \times 10^6 \dots \dots \dots \dots (2)$$

$$(1) + (2): 2a = -48,333 \times 10^6$$

$$a = -24,167 \times 10^6$$

$$b = 3.675 \times 10^6 \checkmark$$

$$a + \frac{b}{D^2} = 0$$

$$-24,167 \times 10^6 + \frac{3,675 \times 10^6}{D^2} = 0$$

$$D = 389.9 \text{ mm} \checkmark$$
 (5)

[13]

#### **QUESTION 2**

2.1 
$$y_B = \frac{F_{TB}}{w} = \frac{6000}{40} = 150 \text{ m} \checkmark$$

$$y_A = y_B - h = 150 - 6 = 144 \text{ m} \checkmark$$

$$F_{TA} = wy_A = 40 \times 144 = 5760 \text{ N} \checkmark$$
 (3)

2.2 
$$y_0 = y_A - d = 144 - 4 = 140 \text{ m}$$

$$\ell_A = \sqrt{y_A^2 - y_0^2} = \sqrt{144^2 - 140^2} = 33,705 \text{ m} \checkmark$$

$$\ell_B = \sqrt{y_B^2 - y_0^2} = \sqrt{150^2 - 140^2} = 53,852 \,\mathrm{m} \,\checkmark$$

$$\ell_T = \ell_A + \ell_B = 87,556 \,\mathrm{m} \,\checkmark$$
 (4)

2.3

$$F_{va} = F_{TA} \cos \alpha = 5760 \times \cos 30 = 4988,306 \text{ N} \checkmark$$

$$F_{va} = F_{va} + F_{vc} = 6336,49 \text{ N} \checkmark$$
(3)

2.4 
$$F_{Hc} = wy_0 = 40 \times 140 = 5600 \text{ N} = F_{Ha} \checkmark$$

 $F_{vc} = w\ell_A = 40 \times 33,705 = 1348,184 \text{ N} \checkmark$ 

$$F_{Ta} = \frac{F_{Ha}}{\sin \theta} = \frac{5600}{\sin 30} = 11200 \text{ N} \checkmark$$
 (2)

#### **QUESTION 3**

3.1
$$\Delta_{1} = \frac{w\ell_{1}^{4}}{8EI} + \frac{w\ell_{1}^{3} \times \ell_{2}}{6EI}$$

$$= \frac{10 \times 10^{3} \times 2,5^{4}}{8 \times 200 \times 10^{9} \times I} + \frac{10 \times 10^{3} \times 2,5^{3} \times 1,5}{6 \times 200 \times 10^{9} \times I} \checkmark$$

$$\Delta_{1} = \frac{439,453 \times 10^{-9}}{I} \checkmark$$

$$\Delta_2 = \frac{FL^3}{3EI} = \frac{20 \times 10^3 \times 4^3}{3 \times 200 \times 10^9 \times I} = \frac{2,133 \times 10^{-6}}{I} \checkmark$$

$$\Delta_T = \Delta_1 + \Delta_2$$

$$11 \times 10^{-3} = \frac{439,453 \times 10^{-9}}{I} + \frac{2,133 \times 10^{-6}}{I} \checkmark$$

$$I = 233,89 \times 10^{-6} \, m^4 \, \checkmark$$

$$I = \frac{\pi (D^4 - d^4)}{64}$$

$$233,89 \times 10^{-6} = \frac{\pi((2d)^4 - d^4)}{64} \checkmark$$

$$d = 133,502 \text{ mm} \checkmark$$
  
 $D = 267,004 \text{ mm} \checkmark$ 

(8)

3.2 For 
$$I = 233,89 \times 10^{-6} \text{ m}^4 \text{ select } 305 \times 305 \times 118 \text{ kg/m} \checkmark$$
 (1)

3.3 
$$M = FL + \frac{w\ell^2}{2}$$
$$= 20 \times 10^3 \times 4 + \frac{10 \times 10^3 \times 2,5^2}{2} \checkmark$$
$$M = 111.25 \text{ kNm } \checkmark$$

$$\sigma = \frac{M}{Z} = \frac{111,25 \times 10^3}{1755 \times 10^{-6}} = 63,39 \text{ MPa} \checkmark$$
(3)

4.1 
$$A = \frac{\pi(D^2 - d^2)}{4} = \frac{\pi(3^2 - 2.5^2)}{4} = 2.16 \text{ m}^2 \checkmark$$

$$W = \rho gAh = 2500 \times 9,81 \times 2,16 \times 15 = 794,553 \text{ kN } \checkmark$$

$$\sigma_D = \frac{W}{A} = \frac{794,553 \times 10^3}{2,16} = 367,875 \text{ kPa (compressive)} \checkmark$$
(3)

4.2 
$$I = \frac{\pi(D^4 - d^4)}{64} = \frac{\pi(3^4 - 2, 5^4)}{64} = 2,059 \text{ m}^4 \checkmark$$

$$M = F \times e = 60 \times 10^3 \times 7.5 = 450 \text{ kNm } \checkmark$$

$$\sigma_b = \frac{MY}{I} = \frac{450 \times 10^3 \times 1,5}{2,059} = 327,892 \text{ kPa} \checkmark$$
(3)

4.3 
$$\sigma_{max} = \sigma_d + \sigma_b = 695,767 \text{ kPa} \checkmark \text{ (compressive)} \checkmark$$

$$\sigma_{min} = \sigma_d - \sigma_b = 39,983 \text{ kPa} \checkmark \text{ (compressive)} \checkmark$$
(4)

4.4 
$$Y_0 = \frac{\sigma_d \times I}{M} = \frac{367,875 \times 10^3 \times 2,059}{450 \times 10^3} = 1,683 \text{ m (from the centroid)} \checkmark$$

Y = 1,683 + 1,5 = 3,183 mm (outside the profile)  $\checkmark$ 

OR

$$\frac{\sigma_{max}}{x} = \frac{\sigma_{min}}{x - D}$$

$$\frac{695,767}{x} = \frac{39,983}{x-3} \checkmark$$

x = 3,183 mm (outside the profile)  $\checkmark$ 

(2) **[12]** 

#### **QUESTION 5**

5.1 
$$W_1 = \rho gA\ell = 2200 \times 9.81 \times 0.5 \times 5 \times b \times 1 = 53.955b \text{ kN } \checkmark$$

$$W_2 = \rho g A \ell = 2200 \times 9.81 \times 2 \times 5 \times 1 = 215.82 \text{ kN} \checkmark$$

$$V = W_1 + W_2 = 53,955b + 215,82 \text{ kN} \checkmark$$

$$\sigma_{max} = \frac{V}{B} + \frac{6Ve}{B^2} - - - (1) \checkmark$$

$$\sigma_{min} = \frac{V}{B} - \frac{6Ve}{B^2} - - - (2) \checkmark$$

(1) + (2): 
$$107,91 + 35,97 = \frac{2V}{B}$$

$$143,88 = \frac{2(53,955b + 215,82)}{2+b} \checkmark$$

$$143,88 \times (2+b) = 2(53,955b + 215,82) \checkmark$$

$$b = 4 \text{ m} \checkmark \text{ and } B = 4 + 2 = 6 \text{ m} \checkmark$$

(10)

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5.2 
$$V = 53,955b + 215,82 = 53,955 \times 4 + 215,82 = 431,64 \text{ kN}$$

$$\sigma_d = \frac{V}{R} = \frac{431,64}{6} = 71,94 \text{ kPa}$$

(4) **[14]** 

(2)

#### **QUESTION 6**

6.1 
$$A = \frac{W_T}{p} = \frac{3 \times 10^6}{187.5 \times 10^3} = 16 \text{ m}^2 \checkmark$$

$$L = \sqrt{A} = \sqrt{16} = 4 \text{ m} \checkmark$$

6.2 
$$M = \frac{W(L - \ell)}{8} = \frac{2,5 \times 10^6 (4 - 0,8)}{8} = 1 \text{ MNm } \checkmark$$

$$Z = \frac{M}{\sigma \times n} = \frac{1 \times 10^6}{100 \times 10^6 \times 5} = 2000 \times 10^{-6} \text{ m}^3 \checkmark$$

lighest I − beam is  $533 \times 210 \times 92,5 \text{ kg/m}$  ✓

(3)

6.3 
$$\ell = b \times n + 0.075(n-1) = 0.2093 \times 5 + 0.075 \times 4 = 1.3465 \text{ m}$$

The given base plate dimension of 1,2 m is not sufficient and must be changed to 1,3465 m  $\checkmark$ 

(2)

6.4 
$$M = \frac{W(L-l)}{8} = \frac{2,5 \times 10^6 (4-1,3465)}{8} = 829,219 \text{ kNm } \checkmark$$

$$Z = \frac{M}{\sigma \times n} = \frac{829,219 \times 10^3}{100 \times 10^6 \times 10} = 829,219 \times 10^{-6} \text{ m}^3 \checkmark$$

lighest I – beam is 
$$406 \times 178 \times 53,8 \text{ kg/m} \checkmark$$
 (3)

6.5 
$$\sigma_T = \frac{M}{Z \times n} = \frac{1 \times 10^6}{2076 \times 10^{-6} \times 5} = 96,339 \text{ MPa} \checkmark$$

$$\sigma_B = \frac{M}{Z \times n} = \frac{829,219 \times 10^3}{927,4 \times 10^{-6} \times 10} = 89,413 \text{ MPa} \checkmark$$
(2)

7.1 
$$\frac{\sigma_s}{\sigma_c} = \frac{m(d-n)}{n}$$

$$\frac{138}{6} = \frac{15(0,6-n)}{n} \checkmark$$

$$23n = 9 - 15n \checkmark$$

$$n = 0,237 \text{ m} \checkmark$$
(3)

7.2 
$$l_a = d - \frac{n}{3} = 0.6 - \frac{0.237}{3} = 0.521 \,\text{m}$$

$$M = \sigma_s A_s l_a = 138 \times 10^6 \times 2 \times 10^{-3} \times 0.521 = 143.811 \text{ kNm } \checkmark$$
 (2)

7.3
$$M = \frac{FL}{4} + \frac{wL^2}{8}$$

$$143,811 = \frac{60 \times 4}{4} \checkmark + \frac{w \times 4^2}{8} \checkmark$$

$$w = 41,905 \text{ kN/m} \checkmark$$
(3)

7.4 
$$M = 0.5\sigma_c A_c l_a$$

$$143.811 \times 10^3 = 0.5 \times 6 \times 10^6 \times b \times 0.237 \times 0.521 \checkmark$$

$$b = 0.388 \text{ m} \checkmark$$
(2)

7.5 
$$M_c = 0.5\sigma_c A_c \frac{2}{3}n$$

$$= 0.5 \times 6 \times 10^6 \times 0.388 \times 0.237 \times \frac{2}{3} \times 0.237 \checkmark$$

$$M_c = 43,579 \text{ kNm } \checkmark$$
(2)

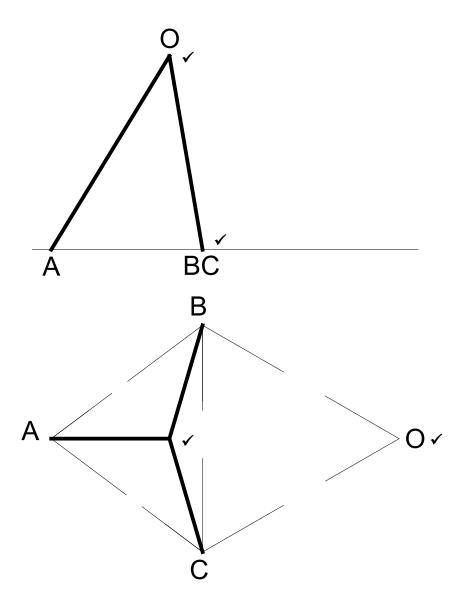
7.6 
$$M_{s} = \sigma_{s} A_{s} (d - n)$$

$$= 138 \times 10^{6} \times 2 \times 10^{-3} (0.6 - 0.237) \checkmark$$

$$M_{s} = 100.232 \ kNm \checkmark$$

(2) **[14]** 

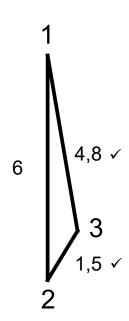
8.1

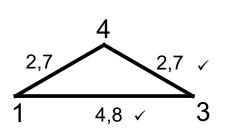


(4)

#### -10-STRENGTH OF MATERIALS AND STRUCTURES N6







MEMBER	MAGNITUDE	NATURE
OA (2-3)	9 kN ✓	Strut
OB (3-4)	16,2 kN ✓	Strut
OC (1-4)	16,2 kN ✓	Strut

(7) **[11]** 

**TOTAL: 100**