



**higher education
& training**

Department:
Higher Education and Training
REPUBLIC OF SOUTH AFRICA

MARKING GUIDELINE

NATIONAL CERTIFICATE

FLUID MECHANICS N5

18 November 2020

This marking guideline consists of 12 pages.

NOTE: ✓ = ONE mark
 ✓ = ½ mark

QUESTION 1

- 1.1 1.1.1
$$W = \frac{2\sigma\pi r^2}{r}$$

$$= 2\sigma\pi r \quad \checkmark$$

$$= 2 \times 0,085 \times \pi \times 3 \times 10^{-3} \quad \checkmark$$

$$\therefore W = 1,602 \times 10^{-3} N \quad \checkmark \quad (3)$$
- 1.1.2
$$\Delta P = \frac{W}{A}$$

$$= \frac{1,602 \times 10^{-3}}{\pi \times 0,003^2} \quad \checkmark$$

$$= 56,667 Pa \quad \checkmark \quad (2)$$
- 1.2 1.2.1
$$From, F_{viscous} = \frac{\mu v A}{t}$$

$$= \frac{0,11 \times 0,65 \times 1,5}{0,3 \times 10^{-3}} \quad \checkmark$$

$$\therefore F_{viscous} = 357,5 N \quad \checkmark \quad (2)$$
- 1.2.2
$$From, WD = Fv \quad \checkmark$$

$$= 357,5 \times 0,65 \quad \checkmark$$

$$\therefore WD = 232,375 J / s \text{ or } 232,375 W \quad \checkmark \quad (2)$$
- 1.2.3
$$From, v = \frac{\mu}{\rho}$$

$$since, \rho_{rel} = \frac{\rho_{substance}}{\rho_{water}}$$

$$\rho_{substance} = \rho_{rel} \times \rho_{water} \quad \checkmark$$

$$= 0,95 \times 1000 \quad \checkmark$$

$$\therefore \rho_{substance} = 950 kg / m^3 \quad \checkmark$$

$$thus, v = \frac{0,11}{950} \quad \checkmark$$

$$\therefore v = 115,79 \times 10^{-6} m^2 / s \quad \checkmark \quad (4)$$

1.2.4

$$\text{From, } F = \frac{\mu v A}{t}$$

$$\text{where, } WD = Fv$$

$$90 = F \times 0,78 \quad \checkmark$$

$$\therefore F = 115,38462N \quad \checkmark$$

$$F = \frac{\mu v A}{t} \quad \checkmark$$

$$\therefore A = \frac{115,38462 \times 0,2 \times 10^{-3}}{0,07} \quad \checkmark$$

$$\therefore A = 329,67034 \times 10^{-3} m^2 \quad \checkmark$$

$$\text{thus, } A = w \times l$$

$$w = \frac{329,67034 \times 10^{-3}}{0,6} \quad \checkmark$$

$$\therefore w = 549,451mm \quad \checkmark$$

(7)
[20]**QUESTION 2**

2.1 Property of matter of either of liquid or gaseous phase, ✓ which measures the ability to resist any form of compression (compressibility) when a force is applied to it ✓

(2)

2.2 2.2.1 Applying Pascal's principle:

$$\text{where, } P_{ram} = P_{plunger}$$

$$\text{as, } P = \frac{F}{A}$$

$$\text{now, } F_{ram} = 6 \times 10^6 \times \frac{\pi \times 0,06^2}{4} \quad \checkmark$$

$$\therefore F_{ram} = 16,965kN \quad \checkmark$$

(2)

2.2.2 from, $F_{plunger} = PA_{plunger}$

$$= 6 \times 10^6 \times \frac{\pi \times 0,02^2}{4} \quad \checkmark$$

$$\therefore F_{plunger} = 1,88496kN \quad \checkmark$$

$$\text{also, } MA = \frac{F_{plunger}}{F_{lever}}$$

$$F_{lever} = \frac{1,88496 \times 10^3}{8} \quad \checkmark$$

$$= 235,62N \quad \checkmark$$

(3)

2.2.3 *from, $SV_{plunger} = SV_{ram}$*
 $n \times A_{plunger} \times SL_{plunger} = A_{ram} \times SL_{ram}$ ✓
 $n = \left(\frac{60}{20}\right)^2 \times \frac{120}{35}$ ✓
 $\therefore n = 30,857$ ✓
thus, a total of 31 strokes is required to lift the ram 120mm ✓ (3)

2.2.4 *from, $\frac{1}{K_e} = \frac{1}{K_l} + \frac{1}{K_{cyl}} + \frac{V_{air}}{V_{total} K_{air}}$*
with no air in the system and modulus of elasticity
thus, $\frac{1}{K_e} = \frac{1}{K_l}$ ✓
 $K_e = K_l = 1,9GPa$ ✓
as, $K_e = \frac{\Delta P \times V}{\Delta V_{play}}$ ✓
 $\Delta L_{play} = \frac{\Delta P \times L}{K_e}$ ✓
 $= \frac{6 \times 10^6 \times 120}{1,9 \times 10^9}$ ✓
 $\therefore \Delta L_{play} = 378,947mm$ ✓ (4)

2.2.5

$$\text{from, } \frac{1}{K_e} = \frac{1}{K_l} + \frac{1}{K_{cyl}} + \frac{V_{air}}{V_{total} K_{air}}$$

$$\text{with } V_{air} = 1,55 \text{ ml}$$

$$\text{also, } K_{air} = P\gamma$$

$$= 6 \times 10^6 \times 1,4 \quad \checkmark$$

$$\therefore K_{air} = 8,4 \text{ MPa} \quad \checkmark$$

$$\text{and, } V_{total} = AL$$

$$= \frac{\pi \times 0,06^2}{4} \times 0,12 \quad \checkmark$$

$$\therefore V_{total} = 339,29201 \times 10^{-6} \text{ m}^3 \quad \checkmark$$

$$\text{thus, } \frac{1}{K_e} = \frac{1}{1,9 \times 10^9} + \frac{1,55 \times 10^{-6}}{339,29201 \times 10^{-6} \times 8,4 \times 10^6} \quad \checkmark$$

$$\frac{1}{K_e} = 526,31579 \times 10^{-12} + 543,84956 \times 10^{-12} \quad \checkmark$$

$$\frac{1}{K_e} = 1,07017 \times 10^{-6} \quad \checkmark$$

$$\therefore K_e = 934,435 \text{ MPa} \quad \checkmark$$

$$\Delta L_{play} = \frac{\Delta P \times L}{K_e}$$

$$= \frac{6 \times 10^6 \times 120}{934,435 \times 10^6} \quad \checkmark$$

$$\therefore \Delta L_{play} = 770,519 \text{ mm} \quad \checkmark$$

(6)
[20]**QUESTION 3**

- 3.1 3.1.1 Upward thrust or force of fluid reacting (opposing direction) against any object which exerts a force (weight) along the surface of equal magnitude
- 3.1.2 Distance measured from liquid surface to base or lowest point of an object below floating or submerged below the surface of the liquid displaced by the object

(2 × 1) (2)

3.2 3.2.1

$$\begin{aligned} \text{since, } \bar{y} &= 3 + \frac{0,9}{2} \quad \checkmark \\ &= 3,45\text{m} \quad \checkmark \\ \text{and, } A &= \frac{\pi \times 0,9^2}{4} \quad \checkmark \\ &= 636,17251 \times 10^{-3} \text{m}^2 \quad \checkmark \\ F_{\text{hydrostatic}} &= \rho g \bar{y} A \\ &= 1020 \times 9,81 \times 3,45 \times 636,17251 \times 10^{-3} \quad \checkmark \\ &= 21,962 \text{kN} \quad \checkmark \end{aligned} \quad (5)$$

3.2.2

$$\begin{aligned} \text{from, } \bar{h} &= \frac{I_G \sin^2 \theta}{A \bar{y}} + \bar{y} \\ \text{as, } I_G &= \frac{\pi \times 0,9^4}{64} \quad \checkmark \\ &= 32,20623 \times 10^{-3} \text{m}^4 \quad \checkmark \\ \text{thus, } \bar{h} &= \frac{32,20623 \times 10^{-3} \times \sin^2 90}{636,17251 \times 10^{-3} \times 3,45} + 3,45 \quad \checkmark \\ &= 14,67391 \times 10^{-3} + 3,45 \quad \checkmark \\ \therefore \bar{h} &= 3,465\text{m} \quad \checkmark \end{aligned} \quad (4)$$

3.3 3.3.1 *Application of Archimedes law for partially or fully submerged objects*

where, $F_{\text{ball}} = F_{\text{buoyancy}} \quad \checkmark$

$$\begin{aligned} mg &= \rho g V_{\text{water displaced}} \quad \checkmark \\ &= 1000 \times 6,25 \times 4 \times 1,2 \quad \checkmark \\ \therefore m &= 30 \text{tonnes} \quad \checkmark \end{aligned} \quad (2)$$

3.3.2 *Application of Archimedes law for partially or fully submerged objects*

where, $F_{\text{ball}} = F_{\text{buoyancy}} \quad \checkmark$

$$\begin{aligned} mg &= \rho g V_{\text{water displaced}} \quad \checkmark \\ m &= \rho V_{\text{water displaced}} \quad \checkmark \\ 30 \times 10^3 &= 1020 \times 6,25 \times 4 \times \text{draught} \quad \checkmark \\ \therefore \text{draught} &= 1,177\text{m} \quad \checkmark \end{aligned} \quad (3)$$

3.3.3 *Application of Archimedes law for partially or fully submerged objects:*

$$\text{where, } F_{\text{pantoon}} + F_{\text{water}} = F_{\text{buoyancy}} \quad \checkmark$$

$$m_{\text{pantoon}}g + m_{\text{water}}g = \rho g V_{\text{water displaced}} \quad \checkmark$$

$$m_{\text{pantoon}} + m_{\text{water}} = \rho V_{\text{water displaced}} \quad \checkmark$$

$$30 \times 10^3 + m_{\text{water}} = 1000 \times 6,25 \times 4 \times 1,66 \quad \checkmark$$

$$m_{\text{water}} = 41,5 \times 10^3 - 30 \times 10^3 \quad \checkmark$$

$$\therefore m_{\text{water}} = 11500 \text{ l} \quad \checkmark$$

(4)
[20]

QUESTION 4

4.1 4.1.1 Line traced or followed by a given or known particle. ✓ Generated by injecting a dye into the fluid in order to follow the movement of the particle along a path ✓

4.1.2 Line taken or followed by a fluid particle in instantaneous motion. ✓ The particle will lie tangential to the streamline at some particular point or position. ✓

(2 × 2) (4)

4.2 4.2.1

$$\text{from, } \dot{W} = \dot{m} g$$

$$\text{as, } \dot{m} = \rho Q$$

$$\text{now, } \dot{W} = \rho g Q \quad \checkmark$$

$$= 9810 \times \frac{\pi \times 0,065^2}{4} \times 8 \quad \checkmark$$

$$\therefore \dot{W} = 260,421 \text{ N/s} \quad \checkmark$$

(2)

4.2.2 *Application of Bernoulli's energy equation between the inlet and outlet :*

$$\frac{P_i}{\rho g} + \frac{v_i^2}{2g} + Z_i = \frac{P_o}{\rho g} + \frac{v_o^2}{2g} + Z_o + h_{loss}$$

from, $Q_{inlet} = Q_{outlet}$... continuity of flow principle :

$$\text{thus, } v_o = \frac{d_i^2}{d_o^2} \times v_i \quad \checkmark$$

$$= \frac{60^2}{45^2} \times 8 \quad \checkmark$$

$$\therefore v_o = 14,22222 \text{ m/s} \quad \checkmark$$

$$\text{thus, } \frac{P_i}{\rho g} + \frac{\sqrt{8^2}}{19,62} + 0 = \frac{50 \times 10^3}{9810} + \frac{14,22222^2}{19,62} + 5,5 + 3 \quad \checkmark \quad \checkmark$$

$$\frac{P_i}{\rho g} = \frac{50 \times 10^3}{9810} + \frac{14,22222^2}{19,62} + 5,5 + 3 - \frac{8^2}{19,62} \quad \checkmark$$

$$P_i = 9810 \times 20,64432 \quad \checkmark$$

$$\therefore P_i = 202,521 \text{ kPa} \quad \checkmark$$

(6)

4.2.3 *Energy head at entry :*

$$E_i = \frac{P_i}{\rho g} + \frac{v_i^2}{2g} + Z_i$$

$$= 20,64432 + \frac{8^2}{19,62} + 0 \quad \checkmark$$

$$\therefore E_i = 23,9063 \text{ m} \quad \checkmark$$

$$P_i = \rho g Q E_i$$

$$= 9810 \times \frac{\pi}{4} \times 0,06^2 \times 8 \times 23,9063 \quad \checkmark$$

$$\therefore P_i = 5,305 \text{ kW} \quad \checkmark$$

(3)

4.2.4 *Energy head at exit :*

$$E_o = \frac{P_o}{\rho g} + \frac{v_o^2}{2g} + Z_o$$

$$= \frac{50 \times 10^3}{9810} + \frac{14,22222^2}{19,62} + 5,5 \quad \checkmark$$

$$\therefore E_o = 20,90627 \text{ m} \quad \checkmark$$

$$P_i = \rho g Q E_i$$

$$= 9810 \times \frac{\pi}{4} \times 0,045^2 \times 14,22222 \times 20,90627 \quad \checkmark$$

$$\therefore P_i = 4,639 \text{ kW} \quad \checkmark$$

(3)

4.2.5

$$\eta_o = \frac{P_o}{P_i} \times 100\%$$

$$= \frac{4,639}{5,305} \times 100\% \quad \checkmark$$

$$= 87,446\% \quad \checkmark$$

(2)
[20]

QUESTION 5

- 5.1 Advantages:
- Relatively cheaper
 - They are compact, which makes them easier to fit them between two measuring position, i.e. pipe flanges
- Disadvantages:
- They are less accurate in providing data during flow measuring operation
- (2 + 1) (3)

5.2 5.2.1 *Application of Bernoulli's energy equation between the inlet and outlet :*

$$\frac{P_i}{\rho g} + \frac{v_i^2}{2g} + Z_i = \frac{P_o}{\rho g} + \frac{v_o^2}{2g} + Z_o + h_{loss} \quad \checkmark$$

as, $P_i = P_o \quad \checkmark$

also, $h_{loss} = 0$

now, $\frac{v_o^2}{2g} = \frac{v_i^2}{2g} + Z_i - Z_o \quad \checkmark$

$$\frac{v_o^2}{2g} = \frac{2,55^2}{19,62} + 5 \quad \checkmark$$

$$\therefore v_o = \sqrt{19,62 \left(\frac{2,55^2}{19,62} + 5 \right)} \quad \checkmark$$

$$= 10,228 \text{ m/s} \quad \checkmark$$

(4)

5.2.2 *from, $Q_{inlet} = Q_{outlet}$...continuity of flow principle :*

thus, $v_o \times d_o^2 = d_i^2 \times v_i \quad \checkmark$

$$d_o = \sqrt{\frac{30^2 \times 2,55}{10,228}} \quad \checkmark$$

$$\therefore d_o = 14,98 \text{ mm} \quad \checkmark$$

(2)

5.2.3 *KE per unit weight;*

$$\begin{aligned}\frac{KE}{W} &= \frac{mv_o^2}{2W} \checkmark \\ &= \frac{v_o^2}{2g} \checkmark \\ &= \frac{10,228^2}{19,62} \checkmark \\ &= 5,332m \checkmark\end{aligned}$$

(3)

5.3 *Application of Bernoulli's energy equation between the inlet and throat :*

$$\frac{P_i}{\rho g} + \frac{v_i^2}{2g} + Z_i = \frac{P_t}{\rho g} + \frac{v_t^2}{2g} + Z_t + h_{loss}$$

*as, $Z_i = Z_t$...horizontal**also, h_{loss} ...are ignored*

$$\text{thus, } \frac{P_i - P_t}{\rho g} = \frac{v_t^2 - v_i^2}{2g} \checkmark$$

from, $Q_{inlet} = Q_{outlet}$...continuity of flow principle :

$$\text{thus, } v_t \times d_t^2 = d_i^2 \times v_i \checkmark$$

$$v_i = \frac{d_t^2}{d_i^2} v_t \checkmark$$

$$\text{now, } \frac{P_i - P_t}{\rho g} = \frac{v_t^2 - \left(\frac{d_t^2}{d_i^2} v_t \right)^2}{2g}$$

$$\frac{25 \times 10^3}{9,81 \times 900} = \frac{v_t^2 - \left(\frac{40^2}{65^2} v_t \right)^2}{19,62} \checkmark$$

$$55,55556 = 0,85659 v_t^2 \checkmark$$

$$\therefore v_t = \sqrt{\frac{55,55556}{0,85659}} \checkmark$$

$$= 8,05337m/s \checkmark$$

$$Q_t = A_t v_t$$

$$= \frac{\pi \times 0,04^2}{4} \times 8,05337 \checkmark$$

$$= 10,12017 l/s \checkmark$$

$$Q_{actual} = 0,87 \times 10,12017 \checkmark$$

$$= 8,805 l/s \checkmark$$

(8)
[20]

QUESTION 6

- 6.1 6.1.1 False
 6.1.2 False
 6.1.3 True

(3 × 1) (3)

6.2 6.2.1

$$\begin{aligned}
 \text{from, } \sum \left(\frac{l}{d} \right)_{\text{system}} &= \left(\frac{l}{d} \right)_{\text{valve}} + \left(\frac{l}{d} \right)_{\text{filter}} + \left(\frac{l}{d} \right)_{\text{pipe}} + \left(\frac{l}{d} \right)_{\text{bend}} \\
 &= 50 + \frac{3,5}{4 \times 0,0015} + \frac{15}{15,5 \times 10^{-3}} + 2 \left(\frac{0,8}{4 \times 0,0015} \right) \\
 &= 50 + 583,33333 + 967,74194 + 266,66667 \\
 &= 1867,742
 \end{aligned}$$

(5)

6.2.2

$$\begin{aligned}
 \text{from, } hf &= \frac{4flv^2}{2gd} \\
 \text{thus, } hf &= \frac{4 \times 0,0015 \times 4,15^2}{19,62} \times 1867,742 \quad \checkmark \\
 \therefore hf &= 9,837m \quad \checkmark
 \end{aligned}$$

(2)

- 6.3 6.3.1 *Application of Bernoulli's energy equation between the inlet and throat :*

$$\frac{P_i}{\rho g} + \frac{v_i^2}{2g} + Z_i = \frac{P_t}{\rho g} + \frac{v_t^2}{2g} + Z_t + h_{\text{loss}}$$

as, $v_i = v_o \dots$ constant pipe diameter

$$\text{where, } \frac{Z_i - Z_t}{L} = \sin \theta$$

$$Z_i - Z_t = 580 \times \frac{1}{110} \quad \checkmark$$

$$= 5,273m \quad \checkmark$$

$$\frac{400 \times 10^3}{9810} + 5,273 = \frac{4 \times 0,0012 \times 580 v_{\text{pipe}}^2}{19,62 \times 0,03} + \frac{6,25 v_{\text{pipe}}^2}{19,62}$$

$$v_{\text{pipe}}^2 = \frac{46,04772}{\left(\frac{4 \times 0,0012 \times 580}{19,62 \times 0,03} + \frac{6,25}{19,62} \right)} \quad \checkmark$$

$$= \sqrt{9,12121} \quad \checkmark$$

$$\therefore v_{\text{pipe}} = 3,02m/s \quad \checkmark$$

(6)

6.3.2 $P_{loss} = \rho g Q h_{loss}$

where, $h_{loss} = \frac{kv_{pipe}^2}{2g} + \frac{4flv_{pipe}^2}{2gd}$

$= \frac{4 \times 0,0012 \times 580 \times 3,02^2}{19,62 \times 0,03} + \frac{6,25 \times 3,02^2}{19,62}$

$\therefore h_{loss} = 46,04361m \quad \checkmark$

$= 9810 \times \frac{\pi \times 0,03^2}{4} \times 3,02 \times 46,04361 \quad \checkmark$

$= 964,225W \quad \checkmark$

(4)
[20]

TOTAL: 100