

higher education & training

Department:
Higher Education and Training
REPUBLIC OF SOUTH AFRICA

MARKING GUIDELINE

NATIONAL CERTIFICATE STRENGTH OF MATERIALS AND STRUCTURES N6

6 AUGUST 2018

This marking guideline consists of 8 pages.

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1.1
$$at 80 \ mm : a - \frac{b}{0,08^{2}} = -54 \times 10^{6} \dots \dots (1) \checkmark$$

$$at 120 \ mm : a + \frac{b}{0,12^{2}} = 0 \dots (2) \checkmark$$

$$(1) - (2) : 156,25b - 69,444b = -54 \times 10^{6}$$

$$b = 239,262 \times 10^{3} \checkmark$$

$$a = -16,615 \times 10^{6} \checkmark$$

$$at 80 \ mm : \sigma_{R} = a + \frac{b}{0,08^{2}}$$

$$= -16,615 \times 10^{6} - \frac{239,262 \times 10^{3}}{0,08^{2}}$$

$$\sigma_{R} = 20,769 \ MPa \checkmark$$
(5)

1.2 $W = p \times A = 20,769 \times 10^6 \times \pi \times 0,04^2 = 104,398 \, kN \checkmark$

$$m = \frac{W}{g} = \frac{104,398 \times 10^3}{9,81} = 10641,951 \, kg \checkmark \tag{2}$$

1.3
$$\sigma_L = \frac{pd^2}{D^2 - d^2} = \frac{20,769 \times 10^6 \times 0,08^2}{0,12^2 - 0,08^2} \checkmark = 16,615 \, MPa\checkmark \tag{2}$$

1.4
$$\epsilon = \frac{(\sigma_H - \vartheta \times \sigma_R)}{E} = \frac{-54 \times 10^6 - 0.29 \times 20.769 \times 10^6}{200 \times 10^9} \checkmark = -300.115 \times 10^{-6} \checkmark$$
 (2)

1.5
$$\Delta d = \varepsilon \times d = -300,115 \times 10^{-6} \times 0,08 \checkmark = 24,009 \times 10^{-6} \, \text{m}\checkmark$$
 (2) [13]

2.1 Consider the deflection limit

$$\Delta = \frac{wl_1^4}{8EI} + \frac{wl_1^3 \times l_2}{6EI}$$

$$0.013 = \frac{10 \times 10^3 \times 4^4}{8 \times 200 \times 10^9 \times I} + \frac{10 \times 10^3 \times 4^3 \times 3}{6 \times 200 \times 10^9 \times I} \checkmark$$

$$I = 246.154 \times 10^{-6} \, m^4 \checkmark$$

Select $457 \times 191 \times 67,1 \, kg/m\checkmark$

Consider the stress limit

$$M = \frac{wl^2}{2} = \frac{10 \times 10^3 \times 4^2}{2} = 80 \text{ kNm}$$

$$Z = \frac{M}{\sigma} = \frac{80 \times 10^3}{90 \times 10^6} = 888,889 \times 10^{-6} \text{ m}^3$$

Select $406 \times 178 \times 53,8 \, kg/m$ √

Correct profile = $457 \times 191 \times 67,1 \, kg/m\checkmark$

This profile will satisfy both limits✓

(8)

2.2
$$\Delta = \frac{wl_1^4}{8EI} + \frac{wl_1^3 \times l_2}{6EI}$$

$$= \frac{10 \times 10^{3} \times 4^{4}}{8 \times 200 \times 10^{9} \times 294.1 \times 10^{-6}} + \frac{10 \times 10^{3} \times 4^{3} \times 3}{6 \times 200 \times 10^{9} \times 294.1 \times 10^{-6}} \checkmark$$

 $\Delta = 10.88 \, mm \checkmark$

$$\sigma = \frac{M}{Z} = \frac{80 \times 10^3}{1297 \times 10^{-6}} \checkmark = 61,681 \, MPa \checkmark \tag{4}$$

QUESTION 3

3.1
$$\sigma_d = \frac{F}{A} = \frac{180 \times 10^3}{2 \times 1,787 \times 10^{-3}} \checkmark = 50,364 \, MPa\checkmark \tag{2}$$

3.2
$$M = \frac{wL^2}{2} = \frac{2 \times 137,34 \times 4^2}{2} = 2,197 \text{ kNm}\checkmark$$

$$\sigma_{bmin} = \frac{MY}{I} = \frac{2,197 \times 10^3 \times 0,0241}{2 \times 1,017 \times 10^{-6}} = 26,0365 \, MPa\checkmark \, (tensile)\checkmark$$

$$\sigma_{bmax} = \frac{MY}{I} = \frac{2,197 \times 10^3 \times 0,0559}{2 \times 1,017 \times 10^{-6}} = 60,392 \, MPa\checkmark(compressive)\checkmark$$
(5)

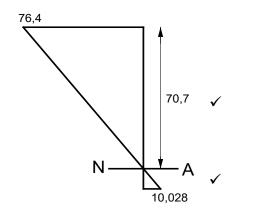
3.3
$$\sigma_{max} = \sigma_d + \sigma_b = 50,364 + 26,0365 = 76,4 \, MPa \checkmark (tensile) \checkmark$$

 $\sigma_{max} = \sigma_d - \sigma_b = 50,364 - 60,392 = 10,028 \, MPa \checkmark (compressive) \checkmark$ (4)

3.4

$$\frac{x}{76.4} = \frac{80 - x}{10.028} \checkmark$$

= 70,7 mm from the top \checkmark



[15]

(4)

QUESTION 4

4.1
$$W_1 = \rho gAl = 2200 \times 9.81 \times 0.5 \times 4 \times y \times 1 = 43.164y \ kN\checkmark$$
 $W_2 = \rho gAl = 2200 \times 9.81 \times 1.5 \times 4 \times 1 = 129.492 \ kN\checkmark$ $V = W_1 + W_2 = 43.164y + 129.492 \ kN\checkmark$

$$\sigma_{max} = \frac{V}{B} + \frac{6Ve}{B^2} - - - (1)\checkmark$$

$$\sigma_{min} = \frac{V}{B} - \frac{6Ve}{B^2} - - - (2)\checkmark$$

(1) + (2):
$$91,342 + 38,15 = \frac{2V}{B} \checkmark$$

$$129,492 = \frac{2(43,164y + 129,492)}{1.5 + y} \checkmark$$

$$129,492 \times (1,5+y) = 2(43,164y + 129,492)\checkmark$$

y = 1,5 m \(\sigma\) and B = 1,5 + 1,5 = 3 m \(\sigma\)

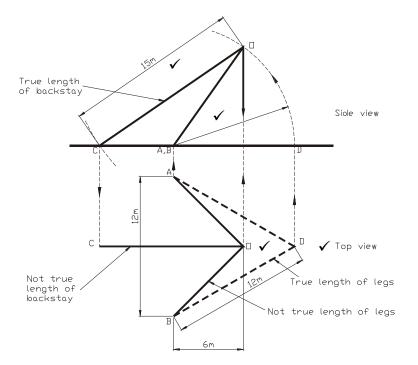
4.2
$$V = 43,164y + 129,492 = 43,164 \times 1,5 + 129,492 = 194,238 \, kN \checkmark$$

$$\sigma_d = \frac{V}{B} = \frac{194,238}{3} = 64,746 \text{ kPa}$$

$$\sigma_b = \sigma_{max} - \sigma_d = 91,342 - 64,746 \checkmark = 26,596 \, kPa \checkmark \tag{4}$$

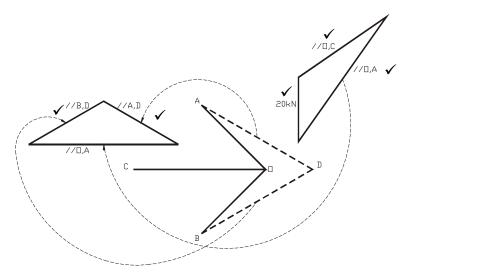
[14]

5.1



(4)

5.2



5.3

MEMBER	MAGNITUDE	NATURE
OC	33,3 kN √	TIE √
OA	27,4 kN √	STRUT√
OB	27,4 kN √	STRUT √

(3)

(5)

$$\frac{\sigma_s}{\sigma_c} = \frac{m(d-n)}{n}$$

$$\frac{140}{7} = \frac{15(0.8 - n)}{n} \checkmark$$

$$n = 0.343 \, m\checkmark \tag{2}$$

6.2
$$M = 0.5\sigma_c A_c l_a = 0.5 \times 7 \times 10^6 \times 0.35 \times 0.343 \times 0.686 \checkmark = 288 \, kNm \checkmark$$
 (2)

6.3
$$M = \sigma_s A_s l_a$$

$$288 \times 10^3 = 140 \times 10^6 \times A_s \times 0,686 \checkmark$$

$$A_{\rm s} = 3 \times 10^{-3} \, m^2 \, \checkmark$$

Select
$$203 \times 102 \times 25.3 \ kg/m\checkmark$$
 (3)

$$6.4 M = \sigma_s A_s l_a$$

$$288 \times 10^3 = \sigma_s \times 3,226 \times 10^{-3} \times 0,686 \checkmark$$

$$\sigma_s = 130,192 \, MPa\checkmark \tag{2}$$

6.5
$$M_c = 0.5\sigma_c A_c \frac{2}{3}n$$
$$= 0.5 \times 7 \times 10^6 \times 0.35 \times 0.343 \times \frac{2}{3} \times 0.343 \checkmark$$

$$M_c = 96 \, kNm \checkmark$$

$$M_{S} = \sigma_{S} A_{S} (d - n)$$

$$= 130,192 \times 10^6 \times 3,226 \times 10^{-6} (0,8-0,343) \checkmark$$

$$M_{S} = 192 \text{ kNm }\checkmark \tag{4}$$

$$[13]$$

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7.1

$$\frac{x}{L-x} = \sqrt{\frac{d}{d+h}}$$

$$\frac{x}{130 - x} = \sqrt{\frac{8}{12}} \checkmark$$

$$x = 58,434 \, m\checkmark$$
 (2)

7.2

$$F_H = \frac{wx_1^2}{2d} = \frac{12 \times 58,434^2}{2 \times 8} = 2560,87 \ kN\checkmark$$

$$F_{V2} = wx_2 = 12 \times 71,566 = 858,796 \, kN \checkmark$$

$$F_{T2} = \sqrt{F_H^2 + F_{V2}^2} = \sqrt{2560,87^2 + 858,796^2} = 2701,0342 \, kN \checkmark \tag{3}$$

7.3 $F_{Va} = F_H \tan \theta = 2560,87 \times \tan 40 = 2148,825 \, kN \checkmark$

$$R = F_{V2} + F_{Va} = 858,796 + 2148,825 = 3007,621 \, kN \checkmark \tag{2}$$

7.4

$$x_3 = 80 - 58,434 = 21,566 \, m\checkmark$$

$$F_{V3} = wx_3 = 12 \times 21,566 = 258,796 \, kN \checkmark$$

$$F_{T3} = \sqrt{F_H^2 + F_{V3}^2} = \sqrt{2560,87^2 + 258,786^2} = 2573,914 \, kN \checkmark \tag{3}$$

8.1
$$\tau = \frac{\tau_{ult}}{FOS} = \frac{200}{4} = 50 \text{ MPa} \checkmark$$

$$T_e = \frac{\pi (D^4 - d^4)\tau}{16D} = \frac{\pi (0,1^4 - 0,075^4) \times 50 \times 10^6}{16 \times 0,1} \checkmark = 6711,166 \text{ Nm} \checkmark$$

$$T_e = \sqrt{T^2 + M^2}$$

$$T=2122,257\ Nm\checkmark$$

$$M = 6366,771 \, Nm\checkmark \tag{6}$$

8.2
$$M_e = 0.5(M + T_e)$$

= 0.5(6366,771 + 6711,166)

 $6711,166 = \sqrt{(T)^2 + (3T)^2} \checkmark$

$$M_e = 6538,968 \, Nm \checkmark$$

$$\sigma = \frac{32 \times M_e \times D}{\pi \times (D^4 - d^4)} = \frac{32 \times 6538,968 \times 0,1}{\pi \times (0,1^4 - 0,075^4)} \checkmark = 97,434 \, MPa \checkmark$$
(3)

8.3
$$d^3 = \frac{D^4 - d^4}{D} = \frac{0.1^4 - 0.075^4}{0.1} = 683.59375 \times 10^{-6} \checkmark$$

$$d = 88,1 \, mm\checkmark \tag{2}$$

TOTAL: 100