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Improving Nb₃Sn cavity performance using centrifugal barrel polishing

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Abstract

In this study we will show a new method of polishing for Nb₃Sn cavities known as centrifugal barrel polishing (CBP). Using this method, Nb₃Sn coated samples are polished to a surface roughness comparable to a traditional Nb cavity after electropolishing. We also investigate different methods of cleaning the Nb₃Sn surface after CBP to remove residual abrasive particles. The polished Nb₃Sn surface is analyzed using confocal laser microscopy, and scanning electron microscopy is used to image the surface and measure the surface roughness after polishing. Transmission electron microscopy is also used for high resolution analysis of the surface after polishing. Finally, we show that CBP can improve the performance of a Nb₃Sn superconducting radiofrequency cavity.

Keywords: superconducting radiofrequency cavities, Nb₃Sn thin film technology, surface treatments

1. Introduction

Superconducting radiofrequency (SRF) cavities are an essential component of particle accelerators used in various fields of science and industry, including high-energy physics, material science, and medical isotope production [1]. These cavities accelerate charged particles to very high energies and can achieve higher accelerating gradients at continuous operation than normal conducting cavities.

The performance of SRF cavities is determined by the superconducting properties of the surface layer of the cavity. The low-temperature superconductor Nb₃Sn has a higher superconducting transition temperature (T_c), 18 K compared to 9 K, and a higher super-heating magnetic field (H_{sh}), around 440 mT compared to 250 mT for the more commonly used niobium [2–5]. SRF cavities coated with a layer of Nb₃Sn can, therefore, achieve a much higher accelerating field, up

to 100 MV m⁻¹ in theory, and have a lower surface resistance than Nb SRF cavities at higher temperatures allowing for cavity operation at 4 K. Whereas Nb cavities are typically operated at 2 K e.g. the LCLS-II cryomodules [6]. These properties make Nb₃Sn SRF cavities a promising research topic for future accelerators such as high-energy linacs or small-scale industrial accelerators.

Nb₃Sn cavities are typically manufactured by coating a Nb cavity with a thin film of Nb₃Sn using Sn vapor-diffusion [7–9], exposing a Nb cavity to tin vapor at 1100 °C to create Nb₃Sn. The reaction forms a 2–3 μm thick Nb₃Sn film with grains approximately 1 μm large. The grains are faceted, and the grain boundaries are thermally etched resulting in approximately 100–150 nm of surface roughness.

Using the Sn vapor-diffusion coating technique [7, 8, 10], Nb₃Sn cavities have only been able to reach a maximum accelerating gradient of 24 MV m⁻¹ [11], a result that was achieved using a thinner Nb₃Sn coating which is smoother than the typical coating. However, this result has not been reproducible, and the performance is lower than the theoretical maximum of Nb₃Sn cavities.

Surface roughness is thought to be one of the limiting factors of Nb₃Sn SRF cavity performance. Surface roughness

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has been shown to be a cause of Q slope and quench in niobium cavities treated with buffered chemical polishing (BCP) due to sharp grain boundary steps [12, 13]. Simulations of the magnetic field near a typical Nb₃Sn surface show that the magnetic field is increased by up to 60 percent in some areas compared to a smooth surface [14, 15] and could be higher for particularly rough areas. By reducing the field enhancement caused by surface roughness, a corresponding increase in the cavity accelerating gradient can be expected.

One method to achieve smoother Nb₃Sn surfaces is polishing. Nb₃Sn polishing has been a topic of study for some time. Chemical methods such as electropolishing (EP) [16–18], BCP [17, 18], and oxy-polishing [16, 17] have been studied, but have failed to produce any meaningful improvement in surface roughness. The expected reason for this is that a large amount of material removal is required to produce a substantial smoothing effect when utilizing chemical methods. EP treatments for Nb typically remove between 5 μm and 10 μm of material to achieve a smooth surface depending on its initial roughness. This amount of material removal is infeasible for Nb₃Sn films, since their thickness is only 2–3 μm . Additionally, niobium and Sn react differently to the chemicals used, which can lead to different removal rates for each element, thus changing the surface stoichiometry. Even a small change in the stoichiometry away from Nb₃Sn can cause a decrease in T_c [19].

To circumvent these issues, we instead use a technique known as centrifugal barrel polishing (CBP), a procedure commonly used for mechanically polishing Nb SRF cavities, and apply it to Nb₃Sn cavities. First, Nb₃Sn coated samples are polished to determine the effectiveness of the CBP method and to determine the optimum polishing parameters such as tumbling duration and the abrasive material. The results of the sample experiments are used to decide the polishing parameters for a Nb₃Sn coated, 1.3 GHz, TESLA geometry SRF cavity. The RF performance of the cavity is tested before and after the CBP treatment. Finally, the cavity is treated with a low temperature Sn coating process to repair the surface and the RF performance is once again tested.

2. Sample study

Since Nb₃Sn is a relatively unexplored material, there are no established polishing parameters or abrasive materials to achieve a good surface finish. To allow for rapid iteration and microscopy surface analysis, we first perform polishing experiments on Nb₃Sn samples. To evaluate the performance of CBP, the surface roughness of the polished samples is measured using confocal laser microscopy and the surface is analyzed using scanning and transmission electron microscopy (SEM and TEM). The material removal rate is measured using focused ion-beam tomography.

The samples were prepared using the standard Nb₃Sn coating procedure. About 1 cm disks are cut from a 4 mm sheet of fine-grain, low residual resistivity ratio (RRR) niobium. About 100 μm of material are removed using standard EP [20], followed by 5 μm of removal using cold EP leading to a

root-mean-square (RMS) surface roughness of 20 nm for the initial substrate [21]. The samples are coated with the standard FNAL coating procedure [7]. This coating resulted in an approximately 3 μm thick film with a grain size of 500 nm and a surface roughness of 200 nm as shown in figure 3. The grain size of the Nb substrate had no effect on the film grain size.

2.1. CBP

CBP is another method used to polish SRF cavities utilizing an abrasive material to mechanically smooth the surface. Tumbling was first implemented for SRF cavities by KEK and Nomura Plating Co. in 1995 [22]. This method has been used to repair surface damage and to attain a very smooth surface in Nb SRF cavities [23, 24].

As yet, only very limited attempts to apply this technique to Nb₃Sn cavities have been made. The technique uses a custom-built tumbling machine that can fit up to 9-cell size 1.3 GHz cavities. When a cavity is mounted in the tumbling machine and filled with abrasive slurry, the rotating motion of the cavity accelerates the polishing media against the cavity surface at up to 59 ms^{-2} .

The abrasive material determines the removal rate and minimum surface roughness attainable using CBP. Large-grit material is used to remove material quickly and smooth out large defects like pits and scratches while fine-grit material is used to microscopically smooth the surface. Since the roughness of as-coated Nb₃Sn cavities is on the order of 100–200 nm, our experiments focus on using fine-grit materials. In this experiment, we use a colloidal nanoparticle suspension, purchased from Allied High Tech Products Incorporated, as our abrasive material. About 50 nm diameter alumina and 40 nm diameter silica nanoparticles suspended in water were tested, but we found no discernible difference between the polishing characteristics of the two materials.

Silicon containing ceramics, such as silica, are a major concern for contamination in the tin coating furnace, since they can release a significant amount of silicon at high temperatures into the furnace. Silicon also reacts with Nb₃Sn to form poorly superconducting silicide phases. Alumina, in contrast, is thermally stable at higher temperatures. This is why alumina is typically used to electrically insulate wires such as thermocouples inside the furnace. For these reasons, the alumina abrasive particles are preferable to avoid any risk of furnace contamination.

The nanoparticle suspension was mixed with a large, soft material to act as a carrier. The purpose of the carrier material is to carry the nanoparticles and to apply a force between them and the cavity surface. Two carrier materials were tested, 13 mm diameter wooden balls and 25 mm compressed wool cubes supplied by Congress Tools, Incorporated.

2.2. Coupon cavity

To test the CBP method on Nb₃Sn samples in a realistic environment, we use a coupon cavity [22]. This cavity has multiple ports where samples are mounted. The samples sit flush with the inside surface of the coupon cavity, as is shown in figure 1,

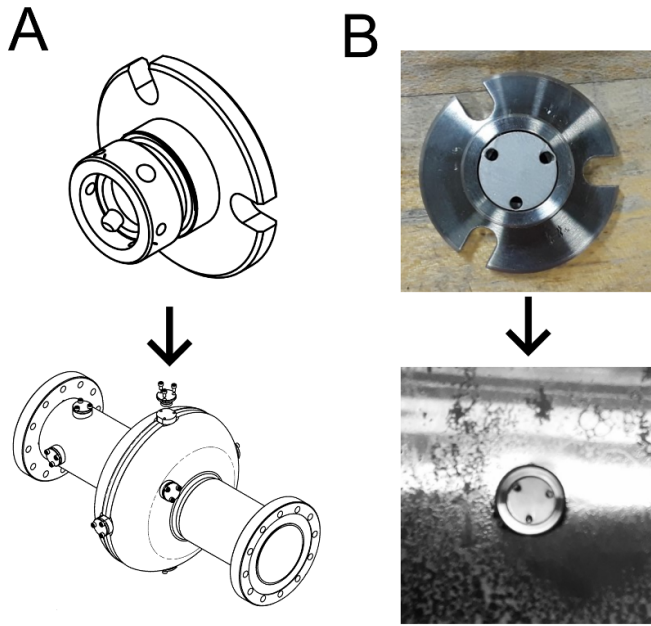


Figure 1. (A) A schematic of the coupon cavity and the sample holder used to polish the Nb_3Sn coated samples. The sample holder can hold 1 cm diameter disks by clamping the sides of the sample with set screws. (B) Pictures of the sample holder sitting outside the coupon cavity with a sample mounted and as seen from the inside of the coupon cavity.

where they experience identical polishing conditions to a real cavity surface. This allows for sample experiments that are representative of the final cavity polishing process. Using this method we inspect the Nb_3Sn surface after polishing under a microscope to determine the best polishing parameters.

CBP was applied to samples mounted in the coupon cavity using the tumbling machine at FNAL. A total of four samples were polished for a duration of 2, 4, 6, and 8 h respectively. The machine was run at its maximum speed of 120 RPM for the entire duration.

2.3. Nb_3Sn coating using Sn vapor-diffusion

The Nb_3Sn samples used in this study were coated at Fermilab in a high-vacuum furnace. The coatings were created at 1100 °C with a Sn crucible acting as the Sn source as well as SnCl_2 acting as a nucleating agent. A detailed review of the coating system at Fermilab shows the specific operating details of the coating system [7].

2.4. Surface analysis of mechanically polished Nb_3Sn coated samples

The Nb_3Sn samples were polished for different lengths of time ranging from 2 to 8 h using the wooden spheres or the felt cubes as the carrier material. Height maps of the polished samples measured using confocal laser microscopy is shown in figure 2. The smoothness of the samples clearly improves as longer polishing is applied.

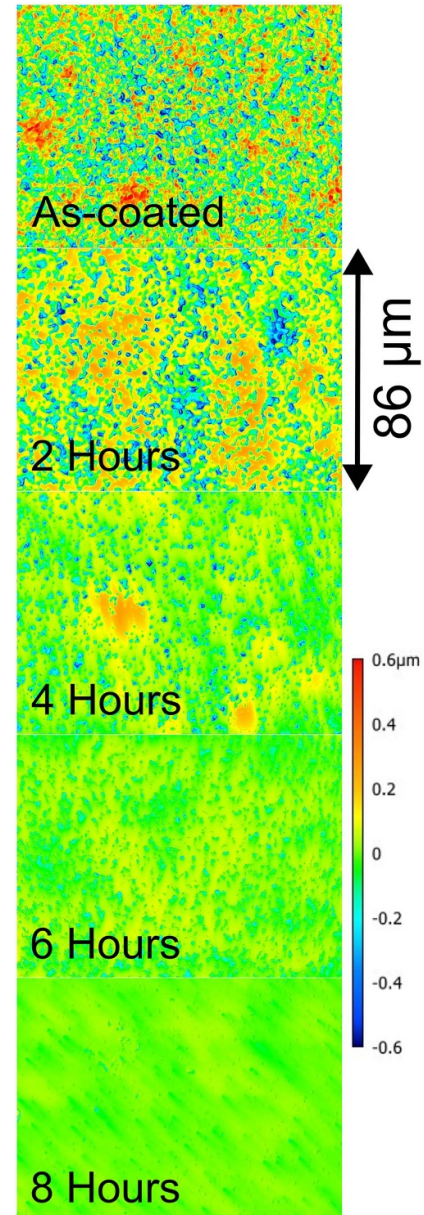


Figure 2. Surface height maps of Nb_3Sn samples mechanically polished for different lengths of time ranging from 2 to 8 h compared to the initial state of the Nb_3Sn coating. Measurements were performed with a Keyence VK-X3000 confocal laser microscope with a pixel size of 20 nm.

By comparing the surface optical micrographs after different amounts of polishing shown in figure 2, it is clear that material is preferentially removed from the highest point on the surface, causing the sharp peaks on the surface to be removed quickly while valleys are left untouched. The phenomenon is also clearly seen in SEM images of the samples shown in figure 4 where the peaks on the grains can be seen to become smoother and then flat as more polishing is applied. This is different from EP, which preferentially smooths areas with high curvature including both peaks and valleys. Due

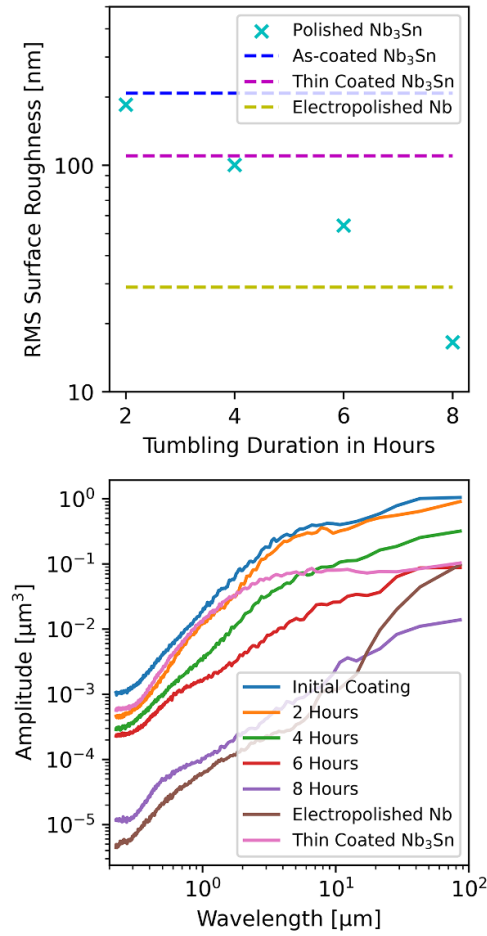


Figure 3. Surface roughness of Nb₃Sn samples mechanically polished for different lengths of time calculated from the surface height maps (top). The power spectral density (PSD) of the surface profile after different amounts of tumbling as well as the PSD of electropolished Nb and a thinly coated Nb₃Sn [11] film (bottom). The PSD is an indicator of the surface roughness of the sample at different length scales.

to this different smoothing mechanism, surface roughness is minimized when the thickness of material removed is equal to the height difference between the highest and lowest point on the surface, which is around 1 μm . This is confirmed by the sample experiments, after 8 h of polishing only the deepest valleys of the initial coating remain.

The surface height maps are used to calculate the RMS surface roughness of the samples and is shown in figure 3. After 6 h of polishing the surface roughness is comparable to the surface roughness of the well performing, thinly coated Nb₃Sn coatings created at FNAL [11]. We also calculate the power spectral density (PSD) of the surface profiles. The PSD is an indicator of the surface roughness at different length scales, indicated by the wavelength [25, 26].

This is verified by SEM micrographs of a thinly coated sample and a polished sample shown in figures 4(A) and (D). After 8 h of polishing, the surface roughness is comparable to a typical Nb surface after EP. This level of smoothness has never been achieved for Nb₃Sn cavities until now. At this level of surface roughness, the performance degradation caused by field enhancement due to surface roughness should be greatly reduced.

The thickness of the film is measured after polishing using FIB/SEM cross-section measurements. Our measurements show that only a small amount of material is removed even after 8 h of polishing. Figure 5 shows the removal rate of different polishing materials. Samples polished using the felt media show an average removal rate of 170 nm h^{-1} whereas the wooden media shows an average of 95 nm h^{-1} removal rate. This measurement corresponds well with measurement performed on Nb cavities by Palczewski *et al* [27]. The starting thickness of the samples is between 3 and 3.5 μm . After 8 h of polishing there is still over 1.5 μm of Nb₃Sn left on the surface. To completely shield the Nb substrate from the RF fields only a few hundred nanometers of material are required, since the London penetration depth of Nb₃Sn is approximately 100 nm [2].

The surface of the polished samples was analyzed using SEM and TEM to look for surface damage or chemical changes on the surface caused by the tumbling or cleaning process. As seen in figures 6 and 7, the Nb₃Sn samples polished using wooden spheres were damaged resulting in microscopic scratches on the surface and a nanometer-scale damaged layer. The damaged layer is theorized to consist of disordered Nb₃Sn

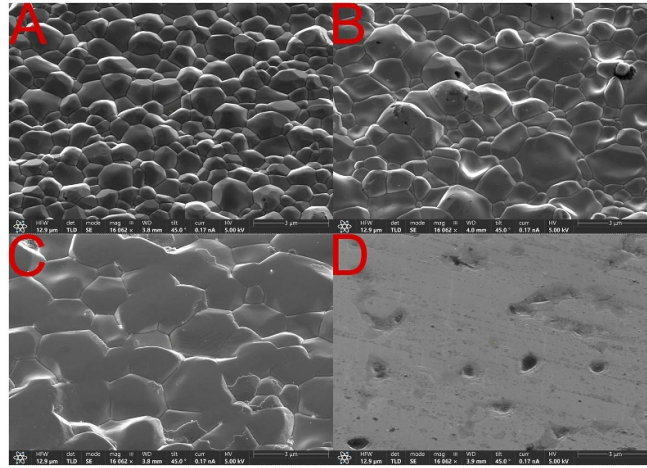


Figure 4. SEM micrographs of a Nb₃Sn thin coated sample (A), standard coated sample (B), a sample after polishing for 2 h (C), and a sample after polishing for 6 h (D).

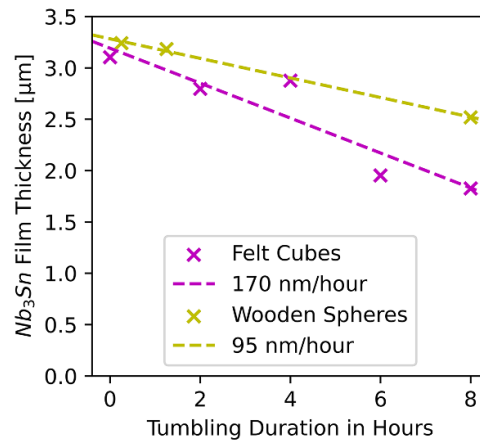


Figure 5. The thickness of the Nb₃Sn film after mechanically polished for different lengths of time using felt cubes or wooden spheres as the polishing media.

layer as no atomic layers are visible and attempts to rotate the sample to align the zone axis in this region were unsuccessful. No surface damage was detected on samples polished using the felt cubes. The surface and oxide layer of the sample polished with felt cubes looks similar to the as coated surface [28, 29]. Since the surface damage may negatively affect the cavity performance, the felt cubes are best to use for polishing Nb₃Sn.

3. Polishing a Nb₃Sn cavity using CBP

Given that CBP was able to produce a smooth surface on Nb₃Sn samples, the next step is to apply the polishing to a Nb₃Sn cavity. The cavity used as the substrate for this experiment is a 1.3 GHz niobium elliptical cavity. The cavity is made of 2.8 mm fine grain niobium with a RRR of 300. However, this cavity was treated with nitrogen doping and EP several times before being coated, which changes the actual thickness

and RRR. In preparation for the coating, the cavity was electro-polished for 100 μm using standard EP and an additional 5 μm of cold EP to achieve a smooth surface. Before the coating the cavity was anodized to improve the nucleation of Nb₃Sn grains. During the coating, the cavity was heated to the nucleation temperature at a rate of 3 °C min⁻¹ to 500 °C and held for 5 h. The temperature was then increased to 1100 °C at a rate of 3 °C min⁻¹ and held for another 5 h. The Sn source heater was set to 713 °C for the nucleation stage and 1325 °C for the coating stage.

The Nb₃Sn-coated cavity was polished using the felt cube polishing media with a 50 nm alumina abrasive particle suspension. The cavity was polished for 4 h at 120 RPM using the tumbling machine described in section 2.1 followed by high-pressure water rinsing and ultrasonic cleaning for 30 min to remove any residual abrasive material left by the polishing process. The polishing duration was chosen as a conservative estimate to minimize the possibility of removing the Nb₃Sn film during polishing and allow for more material removal in

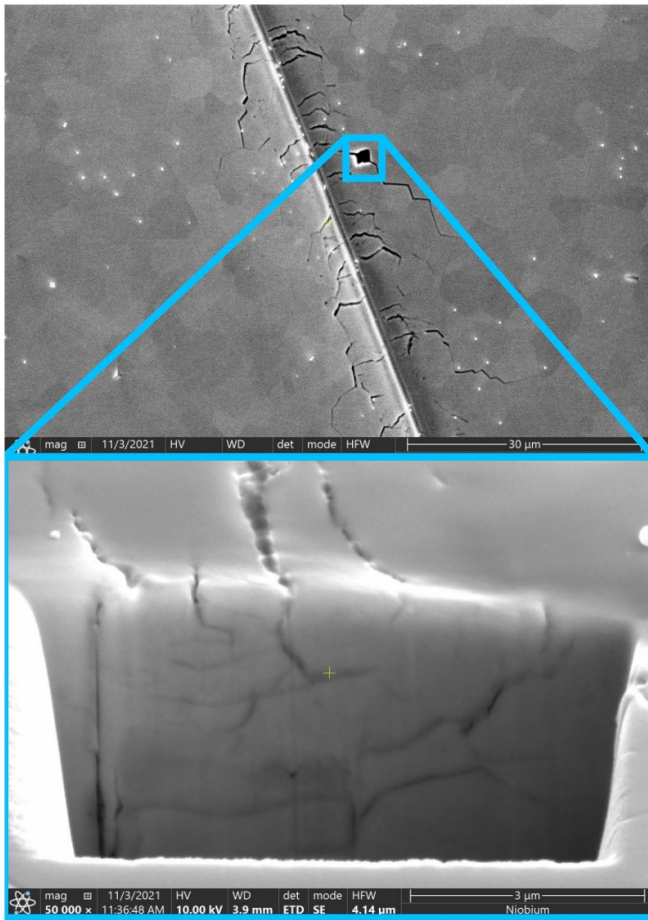


Figure 6. SEM micrograph showing a Nb₃Sn sample polished for 30 h using wooden spheres and a colloidal abrasive suspension. Nb₃Sn films polished using wooden spheres show microscopic scratches and cracks on the surface. A square hole is cut into the surface, visible in the top micrograph to expose a cross-section of a crack. The cross-section shows that the cracks penetrate deep into the film.

the future while still providing a considerable improvement in surface roughness.

Visual inspection of the cavity shows that the surface roughness was improved by the polishing procedure. The as-coated surface of the cavity has a matte finish, which is common on Nb₃Sn-coated surfaces, and after the polishing the cavity has a shiny surface finish. This is indicative of the removal of microscopic surface roughness on the surface of the cavity.

3.1. Low temperature recoating procedure

After the Nb₃Sn-coated cavity was polished using CBP, a secondary coating was applied, which we refer to as the recoating procedure. The purpose of this coating is to repair any surface damage caused by CBP or any subsurface defects, such as tin-deficient regions, that may have been exposed.

For the recoating procedure, the furnace temperature was ramped up to 1000 °C at a rate of 3 °C min⁻¹ and then held

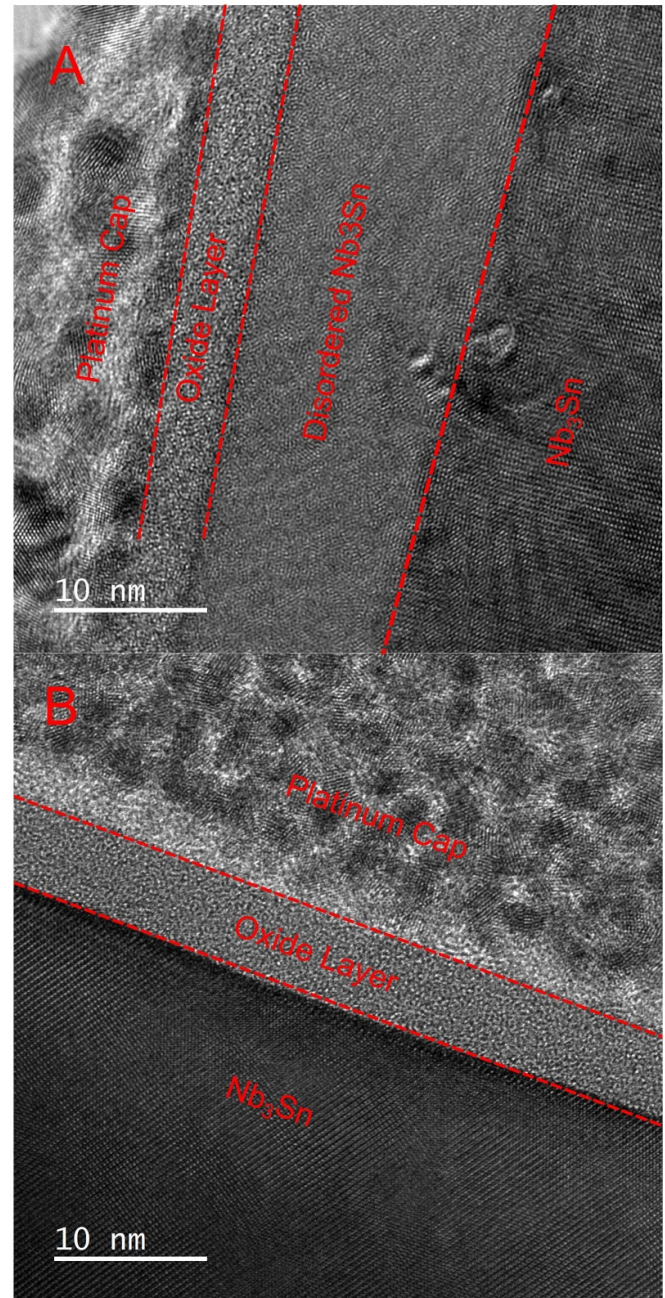


Figure 7. TEM images of a Nb₃Sn sample polished using wooden spheres (A) and felt cubes (B). The polishing procedure creates a 10 nm thick layer of disordered Nb₃Sn, characterized by the absence of visible atomic planes and the clusters of dislocations on the interface with the ordered Nb₃Sn, on the sample polished with wooden spheres which is not present on the sample polished by felt cubes.

for one hour. At the same time the Sn source heater temperature was ramped to and held at 1300 °C. This lower temperature was chosen to minimize any thermal etching of the surface, which could increase the surface roughness. No SnCl₂ was used as it is unnecessary to nucleate any Nb₃Sn grains. One third of the normal amount of Sn, 0.85 g, was used during

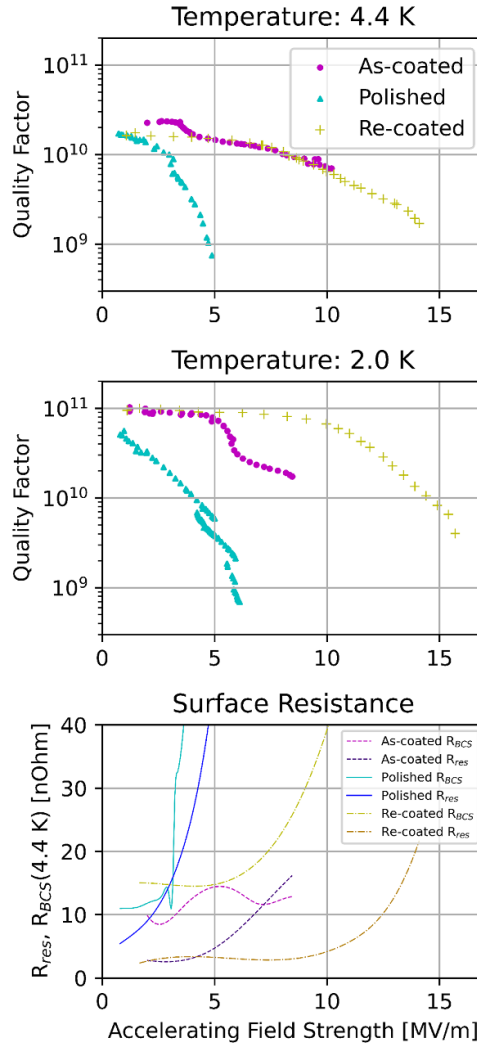


Figure 8. The RF performance of the Nb₃Sn-coated SRF cavity before and after mechanically polished and after a recoating treatment. The residual resistance of the cavity is calculated from the 2.0 K measurements under the assumption that the BCS resistance is negligible at this temperature. We assume that the additional resistance measured at 4.4 K is entirely BCS resistance. These assumptions may be false if there are multiple Nb₃Sn phases on the surface.

the coating. The coating was performed at Fermilab using the coating furnace mentioned in section 2.3.

3.2. SRF cavity RF-performance testing

The RF performance of the Nb₃Sn-coated cavity was tested three times; first, in the as-coated state with no polishing applied; second, after the CBP treatment; lastly, after the recoating procedure. The performance was tested using the vertical test stand at FNAL [30].

3.3. Testing the polished Nb₃Sn SRF cavity

The as-coated performance of the cavity was poor compared to most other Nb₃Sn cavities reaching an accelerating gradient of around 10 MV m⁻¹ with a Q of 10¹⁰ at 4.4 K. The quality factor exhibits an unusual decrease around 6 MV m⁻¹ at 2.0 K which does not appear at 4.4 K. The cause of this decrease is

unknown, but may be due to a surface defect with a lower T_c such as a tin-depleted regions which becomes normal conducting as the accelerating gradient increases.

After the polishing is applied, the cavity exhibits Q-slope (the quality factor decreases with increasing accelerating field), and the maximum gradient was only 5 MV m⁻¹. The cavity was then treated with the recoating treatment, detailed in section 3.1, the Q-slope is ameliorated and the maximum accelerating gradient increases to 15 MV m⁻¹. The quality factor dip seen in the as-coated state at 2.0 K was also removed, which could indicate the removal of a surface defect, but the quality factor at 4.4 K remained unchanged. Figure 8 shows the performance of the cavity after each step.

4. Discussion

Using mechanical polishing, we are able to produce smooth Nb₃Sn films with surface roughness less than 20 nm. This level

of surface roughness has thus far been impossible to achieve using existing methods [11, 16–18]. We have also shown that this smoothing can be achieved with only a few hundred nanometers of material removal, much less than what would be required for chemical polishing methods.

This study also shows that mechanical polishing can be used to improve the performance of Nb₃Sn cavities when used in conjunction with a recoating procedure. There are several reasons why polishing a Nb₃Sn might lead to performance improvements. The most obvious is the reduction in surface roughness, which reduces the field enhancement factor around sharp edges. This should lead to a decrease in Q-slope and an increase in quench field [12, 13] due to a reduction in the volume of normal conducting material interacting with the RF field. However, only one of these effects is experimentally measured, the increase in quench field, while the Q-slope remains mostly unchanged.

Another effect of polishing is a reduction in the film thickness. Nb₃Sn is a poor thermal conductor compared to Nb, which can lead to a buildup of heat on the cavity surface. Higher surface temperatures lower the super heating critical magnetic field and increases BCS resistance causing a premature quench. By decreasing the film thickness, the thermal properties are improved which could lead to a higher quench field [31]. From our sample experiments we measured a removal of approximately 700 nm after 4 h of polishing. Assuming a 3 μ m starting thickness and one dimensional heat diffusion through the film, this reduction could lead to a 30% increase in the maximum heat flux. This effect is more significant if there is a point source of heat on the surface caused by a defect [32]. In this case, the quench field is determined by the thermal stability of the defect. A reduction in film thickness can lead to better thermal stability and allow the cavity to reach higher gradients.

The immediate effect of polishing reduces the quality factor and accelerating gradient of the cavity despite improving the surface finish and decreasing film thickness. The exact cause of this performance degradation is not known. There are two types of defects that could cause a degradation in performance; pre-existing subsurface defects that were created during the initial coating of the cavity and defects that were created by the tumbling process.

Pre-existing defects existing below the surface of the as coated film such as tin-depleted regions [33] and other poorly conducting Nb₃Sn phases are known to exist below the surface of the film and could be exposed to the surface by the removal of material through polishing. In a previous study, we have shown that tin-depleted regions and regions where the film becomes very thin are common in tin vapor-diffusion coated samples near the surface where they could be exposed by the polishing process [34].

Another possible cause for performance degradation is surface damage or other defects caused by the polishing process. Residual abrasive particles can be seen in the SEM images of the polished samples. Cleaning the surface removes most of the contamination, but there may still be some abrasive particles left on the surface, which could cause performance

degradation. Surface damage such as cracks or scratches on the film could also degrade performance, although this seems unlikely as no surface damage was detected on the Nb₃Sn samples polished with felt cubes. It is also possible that the oxide that forms on the Nb₃Sn surface after polishing is unfavorable for performance compared to the oxide that forms in the furnace after the coating process.

After the recoating process was applied, the cavity performance was improved over the unpolished state. We theorize that the re-coating procedure can eliminate both of the aforementioned defect types. A short, low-temperature coating is sufficient to diffuse more Sn into any exposed tin-depleted regions that may have been exposed during the polishing. It is also possible that the Sn vapor can diffuse into and repair any small cracks that may have been created during tumbling. Also, by raising the temperature of the Nb₃Sn, the surface oxide layer created during the tumbling is dissolved, and a new surface oxide is created when the cavity is exposed to air. Only the residual alumina particles are unaffected by the recoating, since they are thermally stable at 1000 °C. However, it is difficult to determine the exact effects of the recoating without performing a thorough cutout analysis on the cavity. Further studies are under way to determine the cause of the performance degradation after mechanical polishing and the effects of the recoating procedure on the Nb₃Sn surface.

It is also worth studying the recoating process on its own to determine if there is any effect on unpolished cavities. The extra Sn provided by the recoating could improve the stoichiometry of the surface and eliminate tin-deficient regions. Additionally, the effects of annealing the cavity at 1000 °C could also be causing a performance increase.

Even after polishing and recoating, the accelerating gradient of the mechanically polished cavity is still below that of the current record holding cavity [11]. This suggests that there are multiple mechanisms that contribute towards cavity quench with surface roughness being one of them. By using mechanical polishing to eliminate the effects of surface roughness on the cavity performance, we can isolate these other mechanisms. We plan to apply mechanical polishing to Nb₃Sn cavities with better as-coated performance. If the performance improvement shown in this paper can be realized in cavities with better initial performance, we could see a drastic increase in the maximum accelerating gradient.

Utilizing CBP for Nb₃Sn SRF cavities is still an under-explored process, and the research presented in this paper only shows our initial attempts at optimizing the process. At the moment we have only a single cavity to base our results on, which limits our ability to understand the process. There are many parameters that can be tweaked to potentially improve the cavity performance, and many questions that are left unanswered. Therefore, we must polish more cavities to understand the effects of each step of the process on the final performance.

We still do not know the effect residual abrasive particles have on the cavity performance. The alumina abrasive is not expected to contribute any significant resistive losses, but could contribute dielectric losses. The combination of

ultrasonic cleaning and high pressure water rinsing shown in this study is likely not sufficient to entirely remove residual abrasives. Further research is necessary to find a reliable cleaning method for polished cavities. Chemical cleaning methods such as HF rinsing may be promising in this regard. Further polishing could help prevent alumina from sticking to the surface by removing crevices that alumina can gather in.

Another step that must be studied further is the recoating. The temperature, duration, and amount of Sn used are chosen to minimize any surface roughness caused by the recoating due to thermal etching mechanisms and also to prevent the growth of an excessively thick film which could negatively impact the thermal characteristics of the cavity. However, it is unclear how prominent thermal etching is or what other impact these parameters have on the film microstructure. Work still needs to be done to determine the optimum parameters for repairing the damage caused by the polishing while also minimizing any thermal etching and negative side effects. It is also worth investigating the effects of the recoating on unpolished cavities to see if any performance improvements can be made by introducing more Sn at a lower temperature after the initial coating is complete.

The ability to smooth the surface of the Nb₃Sn cavities also opens opportunities to experiment with coatings of different thicknesses and grain structure which can then be polished to achieve a smoother surface than is currently possible. Having precise control of the coating thickness as well as the removal rate of the polishing step could allow for much thinner and smoother films with better thermal conduction properties. Future research should incorporate Nb₃Sn coatings with different initial thicknesses.

5. Conclusion

The work presented in this paper shows that CBP is a promising treatment for Nb₃Sn cavities. Through a series of sample studies, we were able to develop a mechanical polishing procedure that can produce surface roughness that was previously unobtainable. We have found that it is possible to attain films with a surface roughness of 20 nm or lower.

Furthermore, we have shown that this surface polishing technique can be used to improve the performance of Nb₃Sn coated cavities when it is paired with a recoating step, which consists of a short, low-temperature Sn coating.

We also stress the fact that CBP is still a highly unexplored process for Nb₃Sn SRF cavities. More research is needed to find the optimum parameters for improving cavity performance.

Data availability statement

The data that support the findings of this study are openly available at the following URL/DOI: <https://doi.org/10.21985/n2-4a9x-n698>.

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