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# EE564 First Project: Transformer Design a for X-Ray Device

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## ID

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`function []=meka_mutlu_XRAY()`

## Specifications

- **Single Phase, High Frequency High Voltage Transformer**
- **Primary Winding Voltage:**  $\pm 417$  V (peak to peak 834 V for pulsing)
- **Secondary Winding Voltage:**  $\pm 12.5$  kV (peak to peak 25 kV for pulsing)
- **Rated Power:** 30 kW (for maximum 100 millisecond)
- **Switching Frequency:** Minimum 100 kHz
- **Ambient Temperature:** 0-40 °C

```
Prated      = 30e3; % Rated power [W]
fs          = 100e3; % switching frequency [Hz]

Vp_peak     = 417; % Primary side peak voltage [V]
Vp_fund_peak= Vp_peak*4/pi; % Peak of fundamental of primary voltage [V]
Vp_f_rms    = Vp_fund_peak/sqrt(2); % RMS value of fundamental [V]

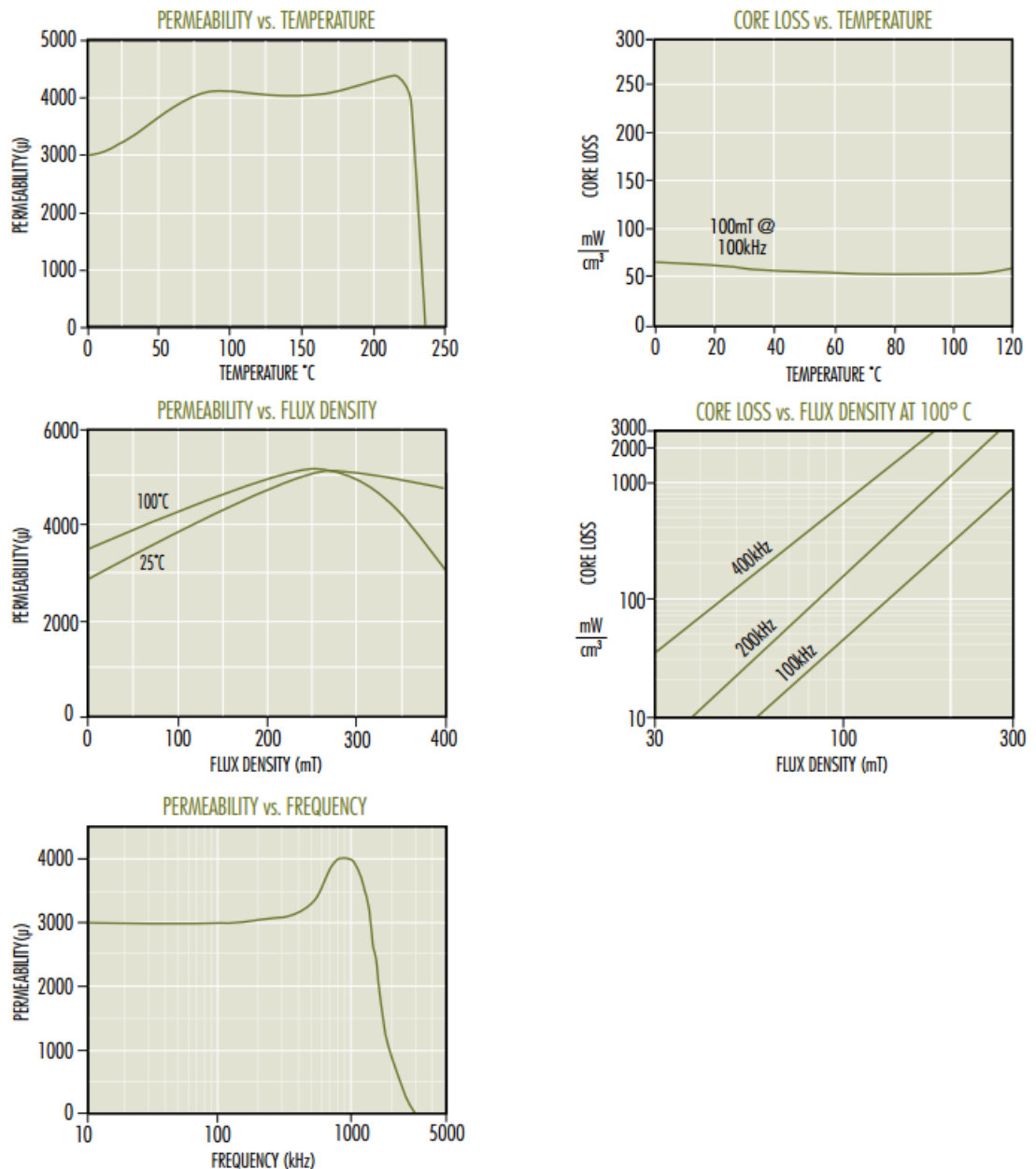
Vs_peak     = 12.5e3; % Secondary side peak voltage [V]
Vs_fund_peak= Vs_peak*4/pi; % Peak of fundamental of secondary voltage [V]
Vs_f_rms    = Vs_fund_peak/sqrt(2); % RMS value of fundamental [V]
```

```
Ip_rms      = Prated/Vp_f_rms; % Primary side RMS current [A]
Is_rms      = Prated/Vs_f_rms; % Secondary side RMS current [A]
```

## Choosing Initial Material

First step of transformer design is selecting an appropriate core material. After some researches on internet and company application guides, it is decided to use a ferrite material for XRAY transformer application at 100kHz switching frequency.

After this decision, Magnetics' ferrite catalog is read and different types of materials are compared. In that comparison, power losses of materials at 25°C and 100kHz is used as basic elimination parameter and it is decided to use T material. It is possible to find its parameters below:



## Choosing Operation Flux Density

For the second phase of design, it is going to be chosen operation flux density. T material's saturation flux density is 470mT for this project's defined temperature range. Our value should be smaller than saturation point. But how much? Let's consider over the formula below:

$$e = -\frac{2\pi}{\sqrt{2}} N 2\pi f B_{peak} * A$$

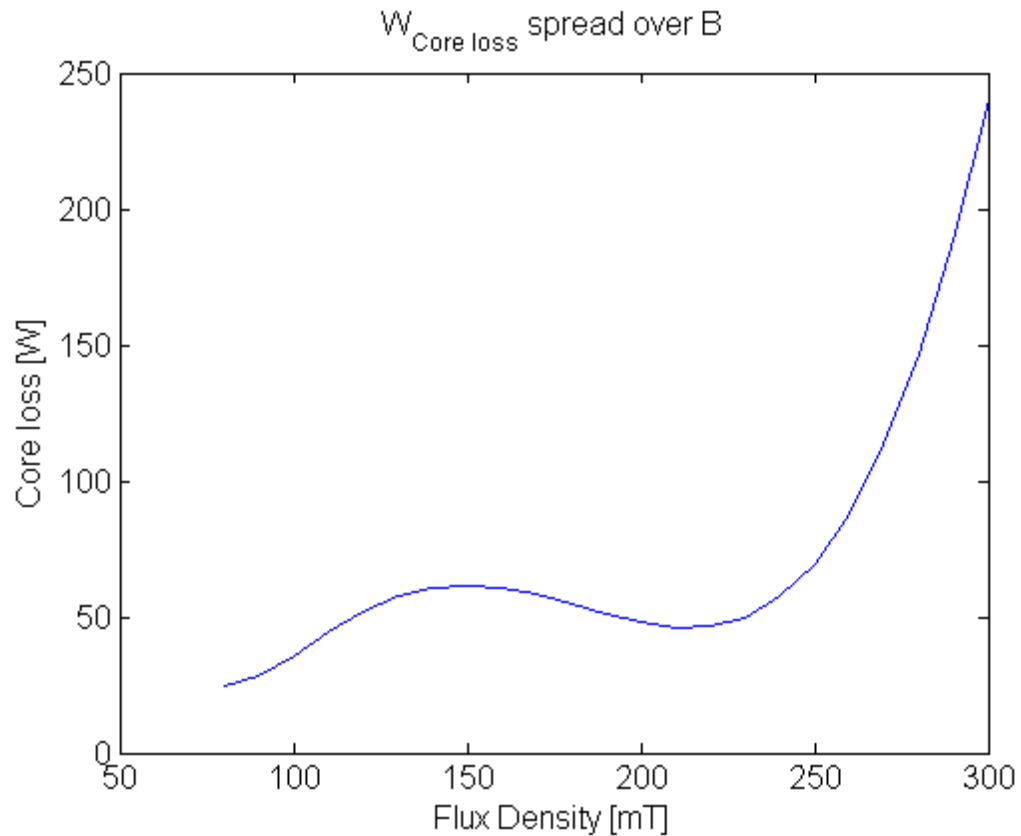
If only selectable parameters are considered, it is possible to see the trade-off between number of turns, flux density and area. Selecting high number of turns come with difficulties of cabling and copper losses. Cable size is decided over current values so it is constant in this discussion. Area is important for transformer's size and weight values. It also effects cable length and core loss (over weight). Flux density is directly related with core losses.

As B is increased, core loss is increased (nonlinearly). If we take BxA value constant, then increasing B will decrease A and therefore volume and weight will be less and it means less core loss. So here, by assuming area and weight are proportional, an optimization will be made over core loss.

```
B_opr = optimize_B();
```

Flux density vs core loss graphic has some missing points due to its nonlinearity. To be able to find required missing points Lagrange polynomial method is used (Function used in this project was written by me during my 3rd class undergraduate studies). After completion is done, assuming area effects weight proportionally, a basic multiplication is made. In coreloss plot unit and magnitude aren't considered but result shows how core loss changes as operation point of flux density is increased.

```
plot(B_req, Coreloss);  
set(gca, 'FontSize', 12);  
xlabel('Flux Density [mT]');  
ylabel('Core loss [W]');  
title('W_{Core loss} spread over B');
```



This plot shows us selecting an arbitrary operation point may result bad efficiency. Selecting the 2nd minimum point 210mT may be an advantage to not have a bigger transformer and still have less core lose. But if the absolute minimum point is considered and 80mT is selected, than core loss will be 85% smaller. It may mean having 2.5 times bigger transformer but it is going to be possible to compensates this value by changing number of turns. Also here, it is needed to be asked: "Should it be really small?". Perhaps this XRAY machine will be put in somewhere and stay there until someone needs to clean under it. A small research is done about "portable" XRAY machines. Here is the smallest result:



This XRAY machine is for dentists and just 60W. So our transformer is used for something bigger:



No.	Name	Parameters
01	Input power	Power supply voltage: AC220V $\pm$ 22 v; Power frequency: 50/60 hz $\pm$ 1 hz;
02	Output	kV: 40kv $\sim$ 120 kV, mA: 16 mA $\sim$ 200 mA, Working frequency: $\geq$ 30 kHz
03	Working environment	Environmental temperature: + 10 $^{\circ}$ C $\sim$ + 40 $^{\circ}$ C; Relative humidity: 30% $\sim$ 75%; Atmospheric pressure: 70 kpa $\sim$ 106 kpa.

This one's specs are given and when maximum points of voltage and current are multiplied result is 24kW and still smaller than our application. In such big machines, size of transformer may be ignored, its weight is also not so dominant. To be able to operate in a condition with less core loss 80mT is selected as operation flux density.

## Determination of Core Dimensions & Number of turns

Comments

## Determination of Core and Copper Losses

Comments

## Determination of Operating Temperature

Comments

## Determination of mass, cost etc.

Comments

```
function [output] = optimize_B()
    B_given = [80 90 100 200 300];
    Coreloss_coef = [25 32 45 120 900];
    B_req = 80:10:300;
    for i=1:length(B_req)
        Coreloss_coef2(i)=lagrange(B_given, Coreloss_coef, B_req(i));
        Coreloss(i) = Coreloss_coef2(i)*B_req(1)/B_req(i);
    end;
    output = B_req(find(Coreloss==min(Coreloss)));
end

function L=lagrange(x,y,k)
    n=length(x);
    l=1;
    L=0;
    for i=1:n
        for j=1:n
            if i~=j
                l=l*(k-x(j))/(x(i)-x(j));
            end;
        end;
        L=L+l*y(i);
        l=1;
    end;
end;

end
```

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