EM564 SECOND PROJECT:TRAIN MOTOR DESIGN

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Specification and Design Parameter

This project is relevant to design is a traction asynchronous squirrel cage induction motor with the following specifications:

*Rated Power Output: 1280 kW

*Line-to-line voltage: 1350 V

*Number of poles: 6

*Rated Speed: 1520 rpm (72 km/h) (driven with 78 Hz inverter)

*Rated Motor Torque: 7843 Nm

*Cooling: Forced Air Cooling

*Insulating Class: 200

*Train Wheel Diameter: 1210 mm

*Maximum Speed: 140 km/h

*Gear Ratio: 4.821

The main idea of design motor is to obtain the dimensions of all parts of the motor in order to supply these data to the manufacturer. The outcome of the project are like this:

*Material Properties, Frame size etc.

*Magnetic Circuit Details (flux density calculations at various points: air-gap, teeth, back-core etc, magnetic loading)

*Electric Circuit (Winding selection, electric loading, fill factor, phase resistance, winding factors (for fundamentalsn and for harmonics))

*Rough thermal calculations (cooling method, operating temperature, ways to improve cooling)

*Efficiency, current, torque characteristics

*Mass Calculations (structural mass, copper mass, steel mass etc)

```matlab
P=1280000;
V=1350;
Vph=V/sqrt(3);
 pole=6;
 pole_p=pole/2;
 m=3; % phase number
 q=4;
 Nr=1520;
 f=78;
 Nsyn=f/(pole/2); % synchronous rotor speed in hertz
 Tr=7843;
 Ns=120*f/(pole);
s=(Ns-Nr)/Ns;
power_factor=0.85;
efficiency=0.91;
```

Since January 1, 2015: The legally specified minimum efficiency IE3 must be maintained for power ratings from 7.5 kW to 375 kW or an IE2 motor plus frequency inverter.

```matlab
eff = imread('efficiency_table.png');
figure;
imshow(eff);
title('Efficiency Table','FontSize',18,'FontWeight','Bold');
```

Efficiency Table

Minimum 50 Hz efficiency values defined in IEC/EN 60034-30-1:2014 (based on test methods specified in IEC 60034-2-1:2014)

Output	IE1				IE2				IE3				IE4			
kW	2 pole	4 pole	6 pole	8 pole	2 pole	4 pole	6 pole	8 pole	2 pole	4 pole	6 pole	8 pole	2 pole	4 pole	6 pole	8 pole
0.12	45.0	50.0	38.3	31.0	53.6	59.1	50.6	39.8	60.8	64.8	57.7	50.7	66.5	69.8	64.9	62.3
0.18	52.8	57.0	45.5	38.0	60.4	64.7	56.6	45.9	65.9	69.9	63.9	58.7	70.8	74.7	70.1	67.2
0.20	54.6	58.5	47.6	39.7	61.9	65.9	58.2	47.4	67.2	71.1	65.4	60.6	71.9	75.8	71.4	68.4
0.25	58.2	61.5	52.1	43.4	64.8	68.5	61.6	50.6	69.7	73.5	68.6	64.1	74.3	77.9	74.1	70.8
0.37	63.9	66.0	59.7	49.7	69.5	72.7	67.6	56.1	73.8	77.3	73.5	69.3	78.1	81.1	78.0	74.3
0.40	64.9	66.8	61.1	50.9	70.4	73.5	68.8	57.2	74.6	78.0	74.4	70.1	78.9	81.7	78.7	74.9
0.55	69.0	70.0	65.8	56.1	74.1	77.1	73.1	61.7	77.8	80.8	77.2	73.0	81.5	83.9	80.9	77.0
075	72.1	72.1	70.0	61.2	77.4	79.6	75.9	66.2	80.7	82.5	78.9	75.0	83.5	85.7	82.7	78.4
1.1	75.0	75.0	72.9	66.5	79.6	81.4	78.1	70.8	82.7	84.1	81.0	77.7	85.2	87.2	84.5	80.8
1.5	77.2	77.2	75.2	70.2	81.3	82.8	79.8	74.1	84.2	85.3	82.5	79.7	86.5	88.2	85.9	82.6
2.2	79.7	79.7	77.7	74.2	83.2	84.3	81.8	77.6	85.9	86.7	84.3	81.9	88.0	89.5	87.4	84.5
3	81.5	81.5	79.7	77.0	84.6	85.5	83.3	80.0	87.1	87.7	85.6	83.5	89.1	90.4	88.6	85.9
4	83.1	83.1	81.4	79.2	85.8	86.6	84.6	81.9	88.1	88.6	86.8	84.8	90.0	91.1	89.5	87.1
5.5	84.7	84.7	93.1	81.4	87.0	87.7	86.0	83.8	89.2	89.6	88.0	86.2	90.9	91.9	90.5	88.3
7.5	86.0	86.0	84.7	83.1	88.1	88.7	87.2	85.3	90.1	90.4	89.1	87.3	91.7	92.6	91.3	89.3
11	87.6	87.6	86.4	85.0	89.4	89.8	88.7	86.9	91.2	91.4	90.3	88.6	92.6	93.3	92.3	90.4
15	88.7	88.7	87.7	86.2	90.3	90.6	89.7	88.0	91.9	92.1	91.2	89.6	93.3	93.9	92.9	91.2
18.5	89.3	89.3	88.6	86.9	90.9	91.2	90.4	88.6	82.4	92.6	91.7	90.1	93.7	94.2	93.4	91.7
22	89.9	89.9	89.2	87.4	91.3	91.6	90.9	89.1	92.7	93.0	92.2	90.6	94.0	94.5	93.7	92.1
30	90.7	90.7	90.2	88.3	92.0	92.3	91.7	89.8	93.3	93.6	92.9	91.3	94.5	94.9	94.2	92.7
37	91.2	91.2	90.8	88.8	92.5	92.7	92.2	90.3	93.7	93.9	93.3	91.8	94.8	95.2	94.5	93.1
45	91.7	91.7	91.4	89.2	92.9	93.1	92.7	90.7	94.0	94.2	93.7	92.2	95.0	95.4	94.8	93.4
55	92.1	92.1	91.9	89.7	93.2	93.5	93.1	91.0	94.3	94.6	94.1	92.5	95.3	95.7	95.1	93.7
75	92.7	92.7	92.6	90.3	93.8	94.0	93.7	91.6	94.7	95.0	94.6	93.1	95.6	96.0	95.4	94.2
90	93.0	93.0	92.9	90.7	94.1	94.2	94.0	91.9	95.0	95.2	94.9	93.4	95.8	96.1	95.6	94.4
110	93.3	93.3	93.3	91.1	94.3	94.5	94.3	92.3	95.2	95.4	95.1	93.7	96.0	96.3	95.8	94.7
132	93.5	93.5	93.5	91.5	94.6	94.7	94.6	92.6	95.4	95.6	95.4	94.0	96.2	96.4	96.0	94.9
160	93.8	93.8	93.8	91.9	94.8	94.9	94.8	93.0	95.6	95.8	95.6	94.3	96.3	96.6	96.2	95.1
200	94.0	94.0	94.0	92.5	95.0	95.1	95.0	93.5	95.8	96.0	95.8	94.6	96.5	96.7	96.3	95.4
250	94.0	94.0	94.0	92.5	95.0	95.1	95.0	93.5	95.8	96.0	95.8	94.6	96.5	96.7	96.5	95.4
315	94.0	94.0	94.0	92.5	95.0	95.1	95.0	93.5	95.8	96.0	95.8	94.6	96.5	96.7	96.6	95.4
355	94.0	94.0	94.0	92.5	95.0	95.1	95.0	93.5	95.8	96.0	95.8	94.6	96.5	96.7	96.6	95.4
400	94.0	94.0	94.0	92.5	95.0	95.1	95.0	93.5	95.8	96.0	95.8	94.6	96.5	96.7	96.6	95.4
450	94.0	94.0	94.0	92.5	95.0	95.1	95.0	93.5	95.8	96.0	95.8	94.6	96.5	96.7	96.6	95.4
500-1000	94.0	94.0	94.0	92.5	95.0	95.1	95.0	93.5	95.8	96.0	95.8	94.6	96.5	96.7	96.6	95.4

Main Dimension of Stator Core

```
cmec = imread('Cmech.png');
figure;
imshow(cmec);
title('Motor constant:Cmec','FontSize',18,'FontWeight','Bold');

Cmec=280;
%x=(pi*(pole_p^(1/3)))/pole;
Din=((P/1000)/(Cmec*Nsyn*x))^(1/3); %m
x=0.5; % aspect ratio
L=x*Din;   %m

ratio = imread('Do-Di value.png');
figure;
imshow(ratio);
title('Inner and outer diameter
 proportion','FontSize',14,'FontWeight','Bold');

Dout=Din/0.7;
Qs=q*m*pole;

Ftan=Tr/(Din/2);
surface_area=pi*Din*L; %m^2
sheer_stress=Ftan*10^-3/surface_area; %kPa
magnetic_loading=0.85; %Magnetic loading
electric_loading=(sheer_stress/magnetic_loading);

airgap=(0.18+0.006*P^(0.4));
```
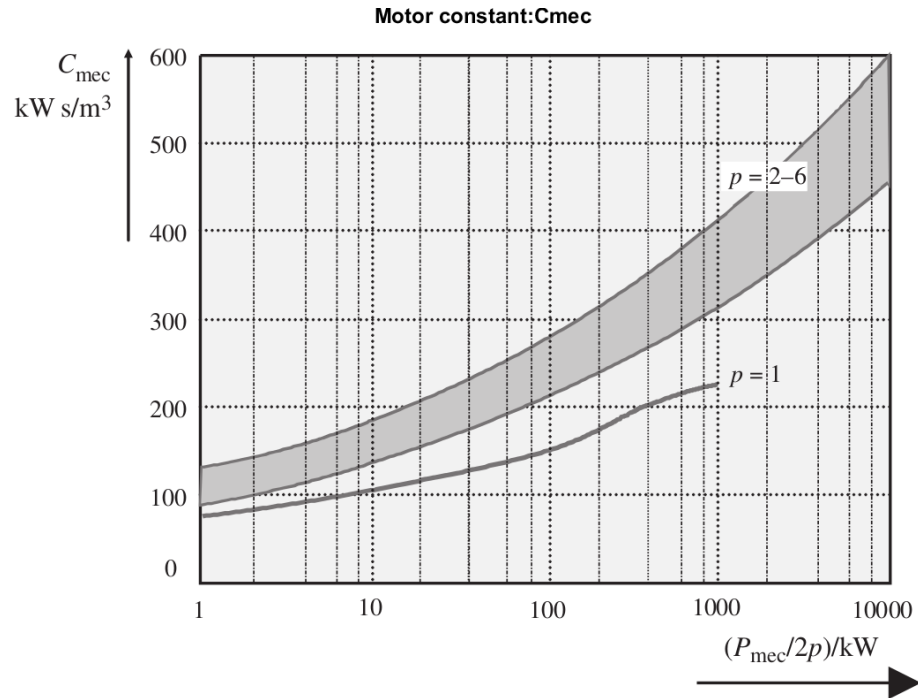
Motor constant:Cmec

Inner and outer diameter proportion

$2p_1$	2	4	6	8
$\dfrac{D_{is}}{D_{out}}$	$0.54 - 0.58$	$0.61 - 0.63$	$0.68 - 0.71$	$0.72 - 0.74$

Stator Winding

```
slot_number = imread('stator and rotor slot number.png');
figure;
imshow(slot_number);
title('Commen stator rotor slot combination
 ','FontSize',18,'FontWeight','Bold');

Qs=q*m*pole;

electrical_angle=(2*pi*pole_p)/Qs;
format rat
electrical_angle_rad=electrical_angle/pi;
format short
```

Commen stator rotor slot combination

p	Q_s	Q_r
	24	28, 16, 22
	36	24, 28, 48, 16
1	48	40, 52
	60	48
	36	24, 40, 42, 60, 30, 44
2	48	60, 84, 56, 44
	60	72, 48, 84, 44
	36	42, 48, 54, 30
3	54	72, 88, 48
	72	96, 90, 84, 54
	36	48
4	48	72, 60
	72	96, 84

Total winding factor (kw) consist of distribution factor (kd) and pitch factor (kp). To eliminate 5.harmonik chording factor is selected 5/6 under pitch

```
chording_factor=5/6;
Kd=sin(pi/(2*m))/(q*sin(pi/(2*m*q)));
Kp=sin((pi/2)*chording_factor);
Kw=Kd*Kp;

pole_pitch=pi*Din/pole; %m
slot_pitch=pole_pitch/(3*q);

mag_flux= imread('magnetic_flux_value.png');
figure;
imshow(mag_flux);
title('Magnetic flux value for the different part of the motor
 ','FontSize',14,'FontWeight','Bold');

Bg=0.7;  % for p=6 Bg=0.7-0.82

Le=L+(2*airgap)/1000;
area_of_one_pole=pi*Din*Le/pole;  %m^2
```

Magnetic flux value for the different part of the motor

	Asynchronous machines
Air gap	0.7–0.90 ($\hat{B}_{\delta 1}$)
Stator yoke	1.4–1.7 (2)
Tooth	1.4–2.1 (stator)
(apparent	1.5–2.2 (rotor)
maximum value)	
Rotor yoke	1–1.6 (1.9)
Pole core	—
Commutating poles	—

Induction motors, both the stator and rotor teeth are saturated at the peak value of the flux density. This leads to a higher reluctance of these teeth when compared with other teeth, and thus ai takes notably higher values than the value corresponding to a sinusoidal distribution. The factor ai (2/pi)has to be iterated gradually to the correct value during the design process. The value ai = 0.64 of an unsaturated machine can be employed as an initial value, unless it is known at the very beginning of the design process that the aim is to design a strongly saturating machine, in which case a higher initial value can be selected.

After calculate magnetic flux using the below equation we can find turn number

E=4.44*f*N*kw*magnetic_flux

```
fundamental_magnetic_flux=(2/pi)*pole_pitch*Bg*L; %Wb
flux=pole_pitch*Le*Bg;
alfa_u=pole*pi/Qs;

format rat
alfa_u_rad=alfa_u/pi;
format short

Kf=1.085;
Ke=0.97;
N=(Ke*Vph)/(4*Kf*Kw*f*fundamental_magnetic_flux);


a1=1;   %number of current path in parallel
```

```
conductor_per_slot=a1*N/(pole_p*q);
number_of_conductor_per_slot=fix(conductor_per_slot); %(ns)
if mod(number_of_conductor_per_slot,2)==0
    number_of_conductor_per_slot_n=number_of_conductor_per_slot;
else
        number_of_conductor_per_slot_n=number_of_conductor_per_slot-1;
end

N_new=number_of_conductor_per_slot*Qs/pole;
```

Number of conductors per slot should be an even number as there are two distinct coils per slot in a double layer winding, Due to changing number of turns per phase we have to recalculate the actual airgap flux density Bg.

```
Bg_new=Bg*N/N_new

Irated=P/(efficiency*power_factor*V*sqrt(3));
```

Bg_new =

    0.7974

J=5-8 A/mm^2 for 2p=6,8

```
J=6.5;

Ac=Irated/J;
d_copper=sqrt(4*Ac/pi);

% because of the skin effect we use paralel conductors.
parallel_branch=12;

d_copper_new=sqrt(4*Ac/(pi*parallel_branch));

awg_area=[107,85,67.4,53.5
 42.4,33.6,26.7,21.2,16.8,13.3,10.6,8.37,6.63,5.26,4.17,3.31,2.63,2.08,1.65,1.31,1
prop=(awg_area*parallel_branch/Ac);
[M,I]=min(prop(prop>1));
awg_size=[11.684,10.405,9.266,8.251,7.348,6.544,5.827,5.189,4.621,4.115,3.665,3.26
wire_cross_section=awg_area(I);
d_co_new=awg_size(I);
```

awg_size =

  Columns 1 through 7

    11.6840   10.4050   9.2660   8.2510   7.3480   6.5440   5.8270

  Columns 8 through 14

     5.1890   4.6210   4.1150   3.6650   3.2640   2.9060   2.5880

```
Columns 15 through 21

  2.3050    2.0530    1.8280    1.6280    1.4500    1.2910    1.1500

Columns 22 through 28

  1.0240    0.9120    0.8120    0.7230    0.6440    0.5730    0.5110
```

Skin Effect

```
mu=4*pi*10^-7;
cop_mu=1.256629*10^-6;
cop_res=1.68*10^-8; % resistivity of the copper for 20C
w=2*pi*f/pole_p;
skin_dept=sqrt((2*cop_res)/(cop_mu*w))*1000; %mm
```

Skin depth is bigger than the wire size and frequency is not very high so we can ignore the skin effect.

Stator Slot Sizing

```
stator_slot= imread('stator_slot_geometry.png');
figure;
imshow(stator_slot);
title('Stator slot geometry','FontSize',18,'FontWeight','Bold');
```


Stator slot geometry
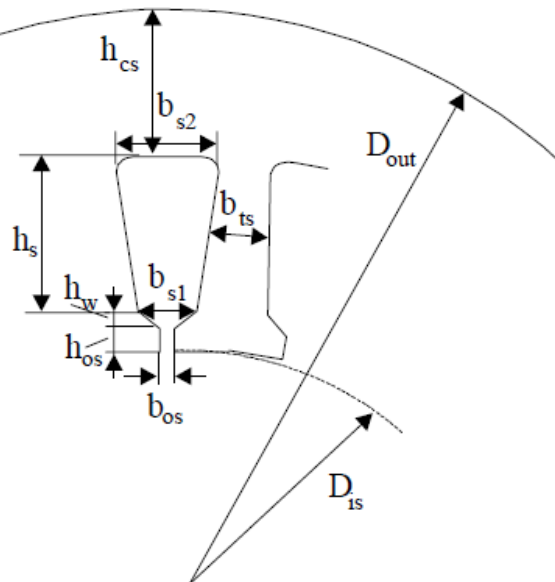
Above 10kW Kfill=0.4-0.44

```matlab
Kfill=0.44;
slot_area=pi*d_co_new^2*parallel_branch*number_of_conductor_per_slot_n/
(4*Kfill); %mm^2

Bts=1.65;
Kfe=0.96; % stator stacking factor
bts=Bg_new*slot_pitch/(Bts*Kfe);    %tooth width
bos=0.0025;
hos=0.001;
hw=0.002;

bs1=(pi*(Din+2*hos+2*hw)/Qs)-bts;  %slot lower width m
bs2 = sqrt(4*slot_area*10^-6*tan(pi/Qs)+(bs1^2));
hs=2*slot_area*10^-6/(bs2+bs1); %m

MMF_airgap=(1.2*airgap*10^-3)*Bg_new/mu;   %airgap mmf
```

From the B-H curve table H values are selected

```matlab
B_H= imread('magnetization_curve.png');
figure;
imshow(B_H);
title('B-H Magnetization curve','FontSize',18,'FontWeight','Bold');

Hts=3460;  %Bts=1.6T ya kar##l#k olarak tablodan seçilmi#tir
MMF_stator_tooth=Hts*(hs+hos+hw);
Kst=0.4;
Fmtr=Kst*MMF_airgap-MMF_stator_tooth;  % E#er Fmtr<<Fmts (yada
 negatif) olsayd# 1+Kst nin Bg de#erinden küçük olmas# gerekiyor.
bcs=(Dout-(Din+2*(hos+hw+hs)))/2; %stator back iron height
Bcs=fundamental_magnetic_flux/(2*L*bcs);  % back core flux density
```

B-H Magnetization curve

B[T]	H[A/m]	B[T]	H[A/m]
0.05	22.8	1.05	237
0.1	35	1.1	273
0.15	45	1.15	310
0.2	49	1.2	356
0.25	57	1.25	417
0.3	65	1.3	482
0.35	70	1.35	585
0.4	76	1.4	760
0.45	83	1.45	1050
0.5	90	1.5	1340
0.55	98	1.55	1760
0.6	106	1.6	2460
0.65	115	1.65	3460
0.7	124	1.7	4800
0.75	135	1.75	6160
0.8	148	1.8	8270
0.85	162	1.85	11170
0.9	177	1.9	15220
0.95	198	1.95	22000
1.0	220	2.0	34000

Evidently Bcs is too low. There are three main ways to solve this problem. One is to simply decrease the stator outer diameter until Bcs=1.4 to 1.7 T. The second solution consists in going back to the design start and introducing a minor stack aspect ratio which eventually would result in a bigger Dis, and, finally, a narrower back iron height bcs and thus a bigger Bcs. The third solution is to decrease current density and thus increase slot height hs. However, if high efficiency is the target, such a solution is to be used cautiously.

```
Dout_n=0.930;
bcs_n=(Dout_n-(Din+2*(hos+hw+hs)))/2;
Bcs_n=Bcs*bcs_n/(bcs_n+(Dout_n-Dout)/2);
```

Rotor Slot

```
rotor_slot= imread('rotor_slot_geometry.png');
figure;
imshow(rotor_slot);
title('Rotor slot geometry','FontSize',18,'FontWeight','Bold');

% From the common combination Qr =88 is selected
Qr=88;
hor=0.0005; %m
bor=0.0015;  %m
```

Rotor slot geometry

$h_{or}=0.5 \times 10^{-3} \, m$

$b_{or}=1.5 \times 10^{-3} \, m$
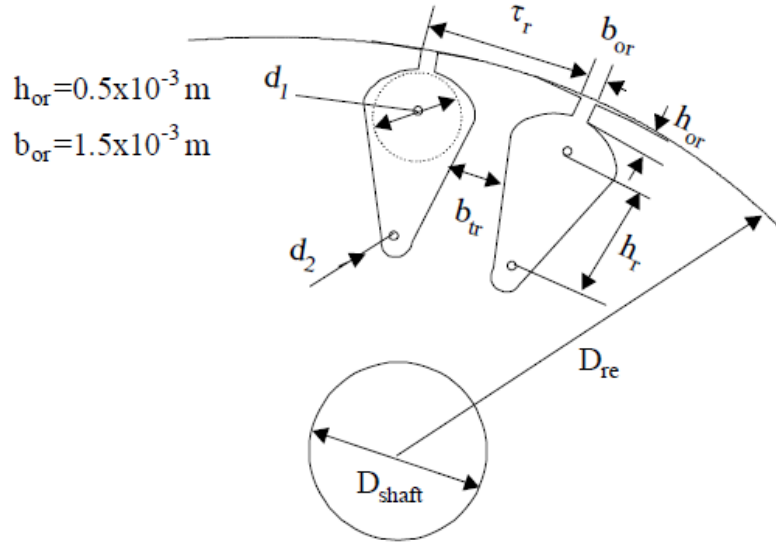
Ki= 1, the rotor and stator mmf would have equal magnitudes. In reality, the stator mmf is slightly larger.

```
Ki=0.8*power_factor+0.2;
I_rotor_bar=(Ki*2*m*N_new*Kw/Qr)*Irated;
J_r = 5; % A/mm^2;  %rotor current density
Ar=I_rotor_bar/(J_r*10^6);    %10^-6 m^2

rotor_slot_area =I_rotor_bar/J_r; % mm^2
I_end_ring=I_rotor_bar/(2*sin(pole_p*pi/Qr));
```

The current density in the end ring Jer = (0.75 – 0.8)Jb. The higher values correspond to end rings attached to the rotor stack as part of the heat is transferred directly to rotor core.

```
J_er = 0.78*J_r; % A/mm^2 end ring
A_end_ring = I_end_ring/(J_er*10^6); % mm^2
T_rotor_slot = pi*(Din-2*airgap*1e-3)/Qr; % m
B_rotor_tooth = 1.6;
H_tr=2460;
btr = Bg_new*T_rotor_slot/(Kfe*B_rotor_tooth); % m

D_r=Din-2*airgap*10^-3;   %rotor diameter

hw_r=0.003;
br1=(pi*(Din+2*hor+2*hw_r)/Qr)-btr;   %slot lower width m
br2 = sqrt(4*rotor_slot_area*10^-6*tan(pi/Qr)+br1^2);
hr=2*rotor_slot_area*10^-6/(br2+br1); %m

rotor_slot_area = ((pi/8)*(br1^2+br2^2))+((br1+br2)*hr/2); % m^2
Bcr = 1.65; % T
hcr = fundamental_magnetic_flux/(2*L*Bcr); % m
MMF_rotor_teeth=H_tr*(hr+hor+(br1+br2)/2);   %Aturns
```

```
Dshaftmax = Din-(2*airgap*(10^-3))-2*(hor+hr+hcr+(br1+br2)/2); % mm
```

```
Tar = 200*atan(2*(hw-hos)/(bs1-bos))/pi; % grad
```

The shaft diameter corresponds to the rated torque and is given in tables based on mechanical design and past experience. The rated torque is approximately

```
Ten=(P)/(2*pi*(f/pole_p)*(1-s));%rated torque Nm
```

```
Der=D_r-3.5*10^-3;
b=1.0*(hr+hor+(br1+br2)/2);
a=A_end_ring/b;
```

Magnetization Current

```
Y1=bos*bos/(5*airgap*10^-3+bos);
Y2=bor*bor/(5*airgap*10^-3+bor);
Kc1=slot_pitch/(slot_pitch-Y1);
Kc2=T_rotor_slot/(T_rotor_slot-Y2);
Kc=Kc1*Kc2; %Total Carter coefficient
```

Kc is close to 1.2 which is assumed initially when calculating Fmg. Back core mmfs Fmcs and Fmcr are calculated as follows:

Stator back core flux intensity in A/m Bcs=1.43 from the table # choose for the Bcs=1.45

```
Hcs=1050;
Hcr=3460; %Rotor back core flux intensity in A/m
Fmcs=0.88*exp(-0.4*Bcs^2)*(pi*(Dout-bcs)/(2*pole_p))*Hcs; %Stator back
 core mmf in Aturns
Fmcr=0.88*exp(-0.4*Bcr^2)*(pi*(Dshaftmax+hcr)/(2*pole_p))*Hcr; %Rotor
 back core mmf in Aturns
```

```
MMF_magnetization=2*(Kc*airgap*10^-3*Bg_new/mu+MMF_stator_tooth
+MMF_rotor_teeth+Fmcs+Fmcr); %Magnetization mmf in Aturns
Ks=MMF_magnetization/(2*MMF_airgap)-1; %Total saturation factor
```

The total saturation factor Ks takes like this

```
Ks = 0.97;
```

```
Imu=(pi*pole_p*MMF_magnetization/2)/
(3*sqrt(2)*N_new*Kw); %Magnetization current in A
i_mu=Imu/Irated; %Relative (p.u.) value of Iu
```

Resistances and Inductances

```
y=chording_factor*pole_pitch;    %Coil span in m
L_end=pi/2*y+0.018; %End connection length for 2*pole_p=6
L_coil=2*(L+L_end); %Coil length in m
resis_cu=1.78e-8; %Copper resistivity at 20 degrees
resis_cu_80=resis_cu*(1+1/273*(80-20)); %Copper resistivity at 80
 degrees
```

```
Rs=resis_cu_80*L_coil*N_new/(Ac*1e-6*a1);

L_er=pi*(Der-b)/Qr; %End ring segment length in m
Beta_s=sqrt(2*pi*f*mu/(2*resis_cu));
S=1;
eta=Beta_s*hr*sqrt(S);
```

Kr the skin effect resistance coefficient for the bar is approximately:

```
Kr=eta*(sinh(2*eta)+sin(2*eta))/(cosh(2*eta)-cos(2*eta));
R_be = resis_cu_80*(L/slot_area*Kr+L_er/(2*A_end_ring*(sin(pi*pole_p/
Qr))^2)); %Rotor bar/end ring segment equivalent resistance in Ohm
Rrc=(4*m/Qr)*(N_new*Kw)^2*R_be; %Rotor cage resistance reduced to the
 stator in Ohm

lambda_s=(2/3*hs/(bs1+bs2)+2*hw/(bos+bs1)+hos/
bos)*(1+3*chording_factor)/4; %Stator slot connection coefficient
Cs=1-0.033*bos*bos/(airgap*10^-3*slot_pitch);
phi=pi*(6*chording_factor-5.5);
gamma_ds=(0.14*sin(phi)+0.76)*1e-2;  % for q=4
lambda_ds=0.9*slot_pitch*q^2*Kw^2*Cs*gamma_ds/
(Kc*airgap*10^-3*(1.0+Kst)); %Stator differential connection
 coefficient
lambda_ec=0.34*q/L*(L_end-0.64*chording_factor*pole_pitch); %Stator
 end connection specific geometric permeance coefficient
Xsl=2*mu*2*pi*f*L*N_new^2/(pole_p*q)*(lambda_s+lambda_ds
+lambda_ec); %Stator phase reactance in Ohm

lambda_r=0.66+2*hr/(3*(br1+br2))+hor/bor; %Rotor slot connection
 coefficient
gamma_dr=9*((6*pole_p/Qr)^2)*1e-2;
lambda_dr=(0.9*T_rotor_slot*10^3*gamma_dr/
(Kc*airgap*10^-3))*10^-2*(Qr/(6*pole_p))^2; %Rotor differential
 connection coefficient
lambda_er=2.3*(Der-b)/(Qr*L*4*(sin(pi*pole_p/Qr))^2)*log10(4.7*(Der-
b)/(b+2*a));  %Stator end ring permeance coefficient
Kx=3/(2*eta)*(sinh(2*eta)-sin(2*eta))/(cosh(2*eta)-cos(2*eta)); %Skin
 effect coefficient for the leakage reactance
X_be=2*pi*f*mu*L*(lambda_r*Kx+lambda_dr+lambda_er); %Equivalent rotor
 bar leakage reactance in Ohm
Xrl=(4*m*(N_new*Kw)^2/Qr)*X_be; %Rotor leakage reactance in ohm
```

For zero speed (S = 1), both stator and rotor leakage reactances are reduced due to leakage flux path saturation. For the power levels of interest here, with semiclosed stator and rotor slots:

```
Xsl_sat=Xsl*0.75; %Stator leakage reactance at S=1 due to leakage flux
 path saturation
Xrl_sat=Xrl*0.65; %Rotor leakage reactance at S=1 due to leakage flux
 path saturation
```

For rated slip (speed), both skin and leakage saturation effects have to be eliminated (KR = Kx = 1)

```
Rbe_Sn=resis_cu_80*(L/Ar+L_er/(2*A_end_ring*(sin(pi*pole_p/
Qr))^2)); %Rotor bar/end ring segment equivalent resistance at rated
 speed
```

```matlab
Rrc_Sn=Rrc*Rbe_Sn/R_be; %Rotor cage resistance reduced to the stator
 at rated speed
Xbe_Sn=2*pi*f*mu*L*(lambda_r+lambda_dr+lambda_er); %Equivalent rotor
 bar leakage reactance at rated speed
Xrl_Sn=Xrl*Xbe_Sn/X_be; %Rotor leakage reactance at rated speed

Xm=sqrt(((V/sqrt(3))/Imu)-Rs^2)-Xsl; %Magnetization reactance
```

Skewing effect on reactances are considered in the design.

```matlab
K_skew=sin(pi/(2*m*q))/(pi/(2*m*q)); %Skewing factor
Xm=Xm*K_skew; %Magnetization reactance including skewing
Xrl_skew=Xm*(1-(K_skew^2));
Xrl_sat_skew=Xrl_sat+Xrl_skew; %Final value of rotor leakage reactance
 at stand still, S=1
Xrl_Sn_skew=Xrl+Xrl_skew; %Final value of rotor leakage reactance at
 rated speed, S=Sn

equivalent= imread('equivalent_circuit.png');
figure;
imshow(equivalent);
title('Equivalent Circuit for the
 Motor','FontSize',18,'FontWeight','Bold');
```
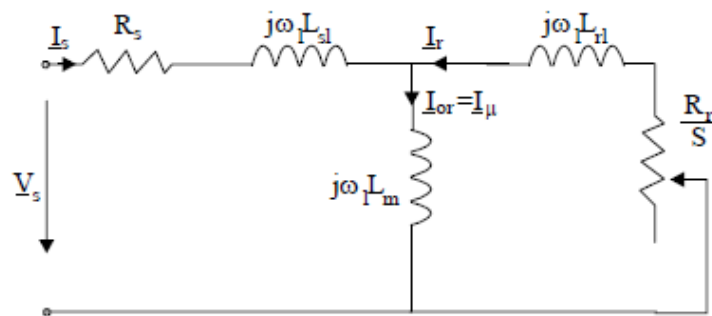

Losses and Efficiency

Total losses for the induction motor are copper losses on stator and rotor windings, core losses on the stator, mechanical/ventilation losses and stray losses. The mechanical/ventilation losses are considered as pmv = 0.03Pn for p1 = 1, 0.012Pn for p1 = 2, and 0.008Pn for p1 = 3,4. Here their standard value pstray = 0.01Pn is considered.

```matlab
P_co_s=3*Irated^2*Rs;
Pcur=3*Rrc_Sn*Ki^2*Irated^2;
Pmv=0.008*P;
Pstray=0.01*P;
```

```
gamma_iron=7800; %Iron density in kg/m^3
Ky=1.7; %Influence of mechanical machining
Gt1=gamma_iron*Qs*bts*(hs+hw+hos)*L*Kfe; %Stator tooth weight in kg
Gy1=gamma_iron*pi/4*(Dout^2-(Dout-2*bcs)^2)*L*Kfe; %Yoke weight in kg

Kt=1.7; %Core loss augmentation due to mechanical machining
p10=2.5; %Specific losses (W/kg) at 1.0 T and 50 Hz
Pt1=Kt*p10*(f/50)^(1.3)*(Bts)^(1.7)*Gt1; %Stator teeth fundamental
 losses (W)
Py1=Ky*p10*(f/50)^(1.3)*(Bcs)^(1.7)*Gy1; %Stator back iron (yoke)
 fundamental losses  (W)
P1_iron=Pt1+Py1; %Fundamental iron losses (W)

Kps=1/(2.2-Bts);
Kpr=1/(2.2-B_rotor_tooth);
Bps=(Kc2-1)*Bg_new; %Stator pulse flux density  (T)
Bpr=(Kc1-1)*Bg_new; %Rotor pulse flux density  (T)

Gtr=gamma_iron*L*Kfe*Qr*(hr+(br1+br2)/2)*btr; %Rotor teeth weight (kg)

Gts=Gt1;
Ps_iron=0.5e-4*((Qr*(f/pole_p)*Kps*Bps)^2*Gts+(Ns*(f/
pole_p)*Kpr*Bpr)^2*Gtr); %Tooth flux pulsation core loss in W
Piron=P1_iron+Ps_iron; %Total iron losses W

Ploss= P_co_s+Pcur+Piron+Pmv+Pstray; %Total losses (W)

efficiency_new=P/(P+Ploss); %Efficiency
```

while starting the design efficiency is selected 91% but now it is 95% and for design it is not change the calculation very much only about 0.04

Operation Characteristics

The operation characteristics are defined as active no load current I0a, rated slip Sn, rated torque Tn, breakdown slip and torque Sk, Tbk, current Is and power factor versus slip, starting current, and torque ILR, TLR

```
I_noload=(Piron+Pmv+3*Imu*Imu*Rs)/(3*V/sqrt(3)); %No load active
 current A
s_rated=Pcur/(P+Pcur+Pmv+Pstray); %Rated slip
Tn=P/(2*pi*(f/pole_p)*(1-s_rated)); %Rated shaft torque in Nm

Cm=1+Xsl/Xm;
T_breakdown=(3*pole_p/(2*w))*((V/sqrt(3))^2)/(Rs+sqrt(Rs^2+(Xsl
+Cm*Xrl)^2));
I_starting=(V/sqrt(3))/(sqrt((Rs+Rrc)^2+(Xsl_sat+Xrl_sat)^2));
T_starting=(3*Rrc*I_starting^2/w)*pole_p;
power_factor_new=P/(3*(V/sqrt(3))*Irated*efficiency_new); % power
 factor

Te=(3*pole_p/w)*((V/sqrt(3))^2*Rrc_Sn/s)/((Rs+Cm*Rrc_Sn/s)^2+(Xsl
+Cm*Xrl_Sn_skew)^2); %Approximate torque vs. slip expression
```

```
tbk=T_breakdown/Tn;
tLR=T_starting/Ten;
iLR=I_starting/Irated;
```

Apparently the design does not need any iterations. This is pure coincidence "combined" with standard specifications. Higher breakdown or starting ratios tbk, tLR would, for example, need lower rotor leakage inductance and higher rotor resistance as influenced by skin effect. A larger stator bore diameter is again required. In general, it is not easy to make a few changes to get the desired operation characteristics.

Temperature Rise

```
lambda_ins=0.25; %Insulation thermal conductivity in W/mK
h_ins=0.3e-3; %Total insulation thickness from the slot middle to
 teeth wall in m
alpha_cond=lambda_ins/h_ins; %The slot insulation conductivity plus
 its thickness lumped in W/m^2K
alpha_conv=40; %For 6 pole IMs with selfventilators placed outside the
 motor in W/m^2K

A_stator_slot=(2*hs+bs2)*L*Qs; %Stator slot lateral area in m^2
theta_co=P_co_s/(alpha_cond*A_stator_slot); %Temperature differential
 between the conductors in slots and the slot wall

Kfin=3.0; %Finn coefficient
Aframe=pi*Dout*(L+pole_pitch)*Kfin; %Frame area in m^2
theta_frame=Ploss/(alpha_conv*Aframe); %Frame temperature rise with
 respect to ambient air in Celcius degrees

theta_amb=50; %Ambient temperature in Celcius degrees
theta_w=theta_amb+theta_co+theta_frame; %Winding temperature in
 Celcius degrees
```

Total Weight

```
Gs=Gt1+Gy1; %Stator iron weight in kg
Gyr=gamma_iron*pi/4*((D_r-2*(hor+(br1+br2)/2+hr))^2-
(Dshaftmax)^2)*L*Kfe; %Rotor yoke weight
Gr=Gtr+Gyr; %Rotor iron weight in kg
Gcus=8940*L_coil*N_new*Ac*1e-6*m; %Stator copper weight in kg
Gcur=8940*(Ar*L+A_end_ring*L_er)*Qr; %Rotor copper weight in kg
Gshaft=gamma_iron*pi/4*Dshaftmax^2;%Shaft weight in kg
Gtotal=Gs+Gr+Gcus+Gcur+Gshaft; %Total motor weight excluding the
 enclosure, ventilation apparatus etc.
```

Conclusion

The decrease of the aspect ratio, lot of parameters are effected because it is effect firstly lenght of the motor. So motor torque, efficiency, cost etc are changed. Here I only change from 0.75 to 0.5 so changing of the parameter aren't seen clearly. Stator winding losses, rotor cage losses are decrease therefore total loss decreases and it directly effects the efficiency of the motor.

Outputs

Main Dimension of Stator Core

```
fprintf('Stator bore diameter: %f m\n',Din)
fprintf('Stack length: %f m\n',L)
fprintf('Pole pitch: %f m\n',pole_pitch)
fprintf('Slot pitch: %f m\n',slot_pitch)
fprintf('Outer diameter: %f m\n',Dout_n)
fprintf('Rotor diameter: %d m\n',D_r)
fprintf('Airgap: %d mm\n',airgap)
```

Stator bore diameter: 0.615196 m
Stack length: 0.307598 m
Pole pitch: 0.322116 m
Slot pitch: 0.026843 m
Outer diameter: 0.930000 m
Rotor diameter: 6.115085e-01 m
Airgap: 1.843548e+00 mm

Stator Winding

```
fprintf('Number of stator slot: %d\n',Qs)
fprintf('Distribution factor:%f \n',Kd)
fprintf('Pitch factor:%f \n',Kp)
fprintf('Winding factor:%f \n',Kw)
fprintf('Pole flux:%f  Wb\n',fundamental_magnetic_flux)
fprintf('Number of turns per phase:%f turns/phase\n',N_new)
fprintf('Number of conductor per slot:%f
 \n',number_of_conductor_per_slot_n)
fprintf('Rated current:%f  A\n',Irated)
fprintf('Magnetic wire cross section:%f mm^2\n',Ac)
fprintf('Wire gauge diameter:%f mm\n',d_co_new)
```

Number of stator slot: 72
Distribution factor:0.957662
Pitch factor:0.965926
Winding factor:0.925031
Pole flux:0.044154 Wb
Number of turns per phase:48.000000 turns/phase
Number of conductor per slot:4.000000
Rated current:707.709875 A
Magnetic wire cross section:108.878442 mm^2
Wire gauge diameter:3.665000 mm

Stator Slot Sizing

```
fprintf('Slot area:%f mm^2\n',slot_area)
fprintf('Stacking factor:%f\n',Kfe)
fprintf('hos:%f mm\n',hos*1000)
fprintf('bos:%f mm\n',bos*1000)
fprintf('bts:%f mm\n',bts*1000)
fprintf('bs1:%f mm\n',bs1*1000)
fprintf('bs2:%f mm\n',bs2*1000)
```

```
fprintf('bcs:%f mm\n',bcs*1000)
fprintf('hs:%f mm\n',hs*1000)
fprintf('hw:%f mm\n',hw*1000)
```

Slot area:1150.870347 mm^2
Stacking factor:0.960000
hos:1.000000 mm
bos:2.500000 mm
bts:13.513363 mm
bs1:13.591406 mm
bs2:19.639721 mm
bcs:59.563018 mm
hs:69.264599 mm
hw:2.000000 mm

Rotor Slot

```
fprintf('Number of stator slot: %f\n',Qr)
fprintf('Rated rotor bar current:%f A \n',I_rotor_bar)
fprintf('Rotor slot area:%f m^2 \n',Ar)
fprintf('End ring cross section:%f m^2\n',A_end_ring)
fprintf('Rotor slot pitch:%f mm \n',T_rotor_slot*1000)
fprintf('hor:%f mm\n',hor*1000)
fprintf('bor:%f mm\n',bor*1000)
fprintf('btr:%f mm\n',btr*1000)
fprintf('br1:%f mm\n',br1*1000)
fprintf('br2:%f mm\n',br2*1000)
fprintf('hcr:%f mm\n',hcr*1000)
fprintf('hr:%f mm\n',hr*1000)
fprintf('hw_r:%f mm\n',hw_r*1000)
fprintf('Maximum diameter of the shaft:%f mm\n',Dshaftmax*1000)
```

Number of stator slot: 88.000000
Rated rotor bar current:1885.401577 A
Rotor slot area:0.000377 m^2
End ring cross section:0.002261 m^2
Rotor slot pitch:21.830801 mm
hor:0.500000 mm
bor:1.500000 mm
btr:11.333564 mm
br1:10.878765 mm
br2:13.123161 mm
hcr:43.498675 mm
hr:31.420839 mm
hw_r:3.000000 mm
Maximum diameter of the shaft:436.667499 mm

End Ring Cross Section

```
fprintf('End ring width:%f mm\n',a*1000)
fprintf('End ring heigth:%f mm\n',b*1000)
```

End ring width:51.483876 mm
End ring heigth:43.921801 mm

Magnetization Current

```
fprintf('Magnetization current:%f A\n',Imu)
fprintf('Airgap mmf:%f Aturns\n',MMF_airgap)
fprintf('Rotor teeth mmf:%f Aturns\n',MMF_rotor_teeth)
fprintf('Stator tooth mmf:%f Aturns\n',MMF_stator_tooth)
fprintf('Magnetization mmf:%f Aturns\n',MMF_magnetization)
fprintf('Carter coefficient:%f \n',Kc)
```

Magnetization current:102.194513 A
Airgap mmf:1403.827709 Aturns
Rotor teeth mmf:108.047631 Aturns
Stator tooth mmf:250.035513 Aturns
Magnetization mmf:4085.263347 Aturns
Carter coefficient:1.030180

Flux Density & Magnetical and Electrical Loading

```
fprintf('Bg:%f T\n',Bg_new)
fprintf('Bcs:%f T\n',Bcs_n)
fprintf('Bcr:%f T\n',Bcr)
fprintf('Brt:%f T\n',B_rotor_tooth)
fprintf('Bts:%f T\n',Bts)
fprintf('Magnetic loading:%f T\n',magnetic_loading)
fprintf('Electrical loading:%f \n',electric_loading)
```

Bg:0.797422 T
Bcs:0.926636 T
Bcr:1.650000 T
Brt:1.600000 T
Bts:1.650000 T
Magnetic loading:0.850000 T
Electrical loading:50.458444

Resistance and Inductance

```
fprintf('Stator phase reactance:%f ohm\n', Xsl)
fprintf('Stator phase resistance:%f ohm\n',Rs)
fprintf('Rotor leakage reactance:%f ohm\n', Xrl)
fprintf('Rotor phase resistance:%f ohm\n',Rrc_Sn)
fprintf('Magnetization:%f  ohm\n',Xm)
```

Stator phase reactance:0.271750 ohm
Stator phase resistance:0.014305 ohm
Rotor leakage reactance:0.575759 ohm
Rotor phase resistance:0.007036 ohm
Magnetization:2.482785 ohm

Current

```
fprintf('No load active current: %d m\n',I_noload)
fprintf('Rated current: %d m\n',Irated)
fprintf('Starting current: %d m\n',I_starting)
fprintf('End ring current: %d m\n',I_end_ring)
```

No load active current: 9.922118e+00 m
Rated current: 7.077099e+02 m
Starting current: 1.347799e+03 m

End ring current: 8.818932e+03 m

Losses & Efficiency

```
fprintf('Stator winding losses:%f  W\n',P_co_s)
fprintf('Rotor cage losses:%f W\n',Pcur)
fprintf('Mechanical/ventilation losses:%f  W\n',Pmv)
fprintf('Stray losses:%f W\n',Pstray)
fprintf('Stray losses:%f W\n',Pstray)
fprintf('Total losses:%f W\n',Ploss)
fprintf('Efficiency:%f  \n',efficiency_new*100)
```

Stator winding losses:21494.452005 W
Rotor cage losses:8187.121746 W
Mechanical/ventilation losses:10240.000000 W
Stray losses:12800.000000 W
Stray losses:12800.000000 W
Total losses:65233.952081 W
Efficiency:95.150736

Operation Characteristic

```
fprintf('Starting torque:%f  Nm\n',T_starting)
fprintf('Breakdown torque:%f Nm\n',T_breakdown)
fprintf('rated shaft torque:%f Nm\n',Tn)
fprintf('Stray losses:%f W\n',Pstray)
fprintf('Power factor:%f  \n',power_factor_new)
```

Starting torque:227.641465 Nm
Breakdown torque:18092.130018 Nm
rated shaft torque:7884.550323 Nm
Stray losses:12800.000000 W
Power factor:0.812921

Mass

```
fprintf('Rotor iron weight:%f  kg\n',Gr)
fprintf('Shaft weight:%f  kg\n',Gshaft)
fprintf('Stator iron weight:%f  kg\n',Gs)
fprintf('Rotor yoke weight:%f  kg\n',Gyr)
fprintf('Stator copper weight:%f  kg\n',Gcus)
fprintf('Rotor copper weight:%f  kg\n',Gcur)
fprintf('Total motor weight:%f  kg\n',Gtotal)
```

Rotor iron weight:250.883925 kg
Shaft weight:1168.116669 kg
Stator iron weight:515.057788 kg
Rotor yoke weight:151.135500 kg
Stator copper weight:209.476638 kg
Rotor copper weight:127.075785 kg
Total motor weight:2270.610805 kg

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