Supplementary information supporting the paper: Warnatzsch and Reay (2019) Assessing Climate Change Projections and Impacts on Central Malawi's Maize Yield: The Risk of Maladaptation.

1. Supplementary Tables and Figures

Table 1: Regional Climate Models (RCM) sources. All of the models other than CanRCM4_r2 were accessed through The Earth System Grid Federation (ESGF) data index (ESGF, 2017). The CanRCM4_r2 model was accessed through the Canadian Centre for Climate Modelling and Analysis website (CCCma, 2017).

RCM	Institution	Lateral Boundary Conditions	Original Calendar	Reference	
CCLM4-8-17_v1		CNRM-CM5 r1i1p1	365-days	(COSMO,	
	Climate Limited-area	HadGEM2-ES r1i1p1	360-days		
	Modelling Community (CLMcom)	EC-EARTH r12i1p1	366-days	2017)	
	(CLIVICOIII)	MPI-ESM-LR r1i1p1	366-days		
HIRHAM5_v2	Danmarks Meteorologiske Insitut (DMI)	EC-EARTH r3i1p1	366-days	(Christensen et al., 2007)	
RACMO22T_v1	Koninklijk Nederlands Meteorologisch Instituut	HadGEM2-ES r1i1p1	360-days	(van Meijgaard	
	(KNMI)	EC-EARTH r1i1p1	366-days	et al., 2008)	
		CanESM2 r1i1p1	366-days		
		CNRM-CM5 r1i1p1	366-days		
		CSIRO-MK3-6-0 r1i1p1	365-days		
		GFDL-ESM2M r1i1p1	365-days		
RCA4_v1	Sveriges Meteorologiska och Hydrologiska Institut (SMHI)	IPSL-CM5A-MR r1i1p1	365-days	(Samuelsson et al., 2015)	
		HadGEM2-ES r1i1p1	360-days	, ,	
		EC-EARTH r12i1p1	366-days		
		MIROC5 r1i1p1	365-days		
		MPI-ESM-LR r1i1p1	366-days		
		NORESM1-M r1i1p1	365-days		
REMO2009 v1	Climate Service Centre Germany (CSC) and Max	EC-EARTH r12i1p1	366-days	(Jacob et al.,	
VEIAIO5002_A1	Planck Institut (MPI)	MPI-ESM-LR r1i1p1	366-days	2012)	
CanRCM4_r2	Canadian Centre for Climate Modelling and Analysis (CCCma)	CanESM2 r1i1p1	365-days	(Scinocca et al., 2016)	

Table 2: Observed data sources

Dataset	Variable Used	Resolution	Time-Period Available	Source	Reference
Climate Research Unit (CRU) version 4.0	Tas, TasMin, TasMax and Pr	0.5° Monthly Land Only	1901-2015	Gridded Station Data	(Harris et al., 2014)
University of Delaware (UDel) version 4.01	Tas and Pr	0.5° Monthly Land Only	1901-2010	Gridded Station Data	(Willmott and Matsuura, 2001)
Global Precipitation Climatology Centre (GPCC) version 7	Pr	1.0° Monthly	1901-2010	Satellite and Station Data	(Schneider et al., 2015)

Table 3: List of data sources for the 13 climate files used in the crop models. Note that all RCMs referred to in this table are listed in Table 1 and the observed data referred to in this table are from the sources listed in Table 2.

File	Time Scale	RCP	Temperature	Reference Evapotranspiration	Precipitation	CO ₂ concentration								
1	1971- 2000	N/A	Mean of observed monthly data for minimum and maximum temperature		Observed monthly data for precipitation rates	AquaCrop Mauna Loa CO ₂								
2			temperature		Projected ensemble minimum precipitation rate									
3		4.5			Projected ensemble mean precipitation rate	AquaCrop IPCC RCP 4.5								
4	2020-				Projected ensemble maximum precipitation rate									
5	2049	8.5	8.5	8.5									Projected ensemble minimum precipitation rate	
6						Calculated using methodology	Projected ensemble mean precipitation rate	AquaCrop IPCC RCP 8.5						
7								Projected ensemble mean daily	described in Section 2	Projected ensemble maximum precipitation rate				
8							minimum and maximum temperature		Projected ensemble minimum precipitation rate					
9					Projected ensemble mean precipitation rate	AquaCrop IPCC RCP 4.5								
10	2040-							Projected ensemble maximum precipitation rate						
11	2069						Projected ensemble minimum precipitation rate							
12		8.5			Projected ensemble mean precipitation rate	AquaCrop IPCC RCP 8.5								
13					Projected ensemble maximum precipitation rate									

Table 4: Absolute AquaCrop output data for historic 1971-2000 climate using three different soil types

Cultivar	Planting Date	AquaCrop Default Soil	AquaCrop Default Sandy Clay Loam Soil	Calibrated Sandy Clay Loam Soil
Slow-	15 Nov	12.293	12.05	12.052
0.0	10 Dec	12.861	12.861	12.861
Development	30 Dec	13.323	12.834	12.249
Foot	15 Nov	7.727	7.384	7.383
Fast-	10 Dec	7.961	7.961	7.961
Development	30 Dec	8.243	8.243	8.243

Table 5: Absolute AquaCrop output data for projected climates under RCP 4.5 using three different soil types

		Planting		2020-2049			2040-2069	
Cultivar	Soil Type	Date	Min. Rain	Ave. Rain	Max. Rain	Min. Rain	Ave. Rain	Max. Rain
Class		15 Nov	9.781	12.15	12.229	8.142	12.197	12.284
Slow-		10 Dec	9.024	12.958	12.958	7.615	12.324	12.324
Development	AquaCrop	30 Dec	4.682	13.699	13.699	4.324	13.299	13.299
F	Default Soil	15 Nov	6.162	7.844	7.947	5.691	7.683	7.81
Fast-		10 Dec	7.894	8.065	8.065	7.613	7.901	7.901
Development		30 Dec	8.388	8.388	8.388	8.093	8.157	8.157
Class		15 Nov	5.502	11.985	12.229	4.628	12.021	12.284
Slow-	AquaCrop	10 Dec	3.031	12.958	12.958	2.994	12.324	12.324
Development	Default	30 Dec	0.995	13.699	13.699	1.004	13.299	13.299
Fast	Sandy Clay	15 Nov	1.716	7.611	7.947	1.431	7.435	7.81
Fast-	Loam Soil	10 Dec	7.419	8.065	8.065	6.344	7.901	7.901
Development		30 Dec	7.391	8.388	8.388	6.957	8.157	8.157
Class		15 Nov	5.497	11.984	12.229	4.800	12.025	12.284
Slow-	C-1:1+1	10 Dec	2.683	12.958	12.958	2.725	12.324	12.324
Development	Calibrated	30 Dec	0.792	13.699	13.699	0.804	13.299	13.299
Foot	Sandy Clay	15 Nov	1.675	7.601	7.947	1.344	7.433	7.810
Fast-	Loam Soil	10 Dec	7.410	8.065	8.065	6.060	7.901	7.901
Development		30 Dec	7.032	8.388	8.388	6.596	8.157	8.157

Table 6: Absolute AquaCrop output data for projected climates under RCP 8.5 using three different soil types

		Dianting		2020-2049			2040-2069	
Cultivar	Soil Type	Planting Date	Min. Rain	Ave. Rain	Max. Rain	Min. Rain	Ave. Rain	Max. Rain
Sla		15 Nov	8.337	12.317	12.423	4.884	11.962	12.077
Slow-		10 Dec	8.44	12.863	12.863	8.615	12.186	12.186
Development	AquaCrop	30 Dec	5.013	13.324	13.324	5.191	12.667	12.667
Fact	Default Soil	15 Nov	5.604	7.749	7.891	4.218	7.284	7.433
Fast-		10 Dec	7.635	7.962	7.962	7.15	7.527	7.527
Development		30 Dec	8.206	8.244	8.244	7.775	7.819	7.819
Class		15 Nov	3.771	12.112	12.423	3.548	11.747	12.077
Slow-	AquaCrop	10 Dec	2.91	12.863	12.863	3.299	12.186	12.186
Development	Default	30 Dec	1.112	13.324	13.324	1.509	12.667	12.667
Foot	Sandy Clay	15 Nov	1.413	7.448	7.891	1.107	6.963	7.433
Fast- Development	Loam Soil	10 Dec	6.602	7.962	7.962	5.6	7.527	7.527
Development		30 Dec	7.249	8.244	8.244	7.172	7.819	7.819
Class		15 Nov	3.799	12.121	12.423	4.352	11.759	12.077
Slow-	Calibratad	10 Dec	2.816	12.863	12.863	3.402	12.186	12.186
Development	Calibrated	30 Dec	0.878	13.324	13.324	1.275	12.667	12.667
Foot	Sandy Clay Loam Soil	15 Nov	1.358	7.449	7.891	1.029	6.970	7.433
Fast- Development	LUAIII 30II	10 Dec	6.473	7.962	7.962	5.421	7.527	7.527
Development		30 Dec	6.895	8.244	8.244	6.905	7.819	7.819

Table 7: Absolute AquaCrop output data for historic (1971-2000) and projected climate under RCP 4.5 and 8.5 using the default Maize crop file and calibrated sandy clay loam soil file.

	Planting		RCP	2020-2049			2040-2069		
Soil Type	Date	1971-2000		Min. Rain	Ave. Rain	Max. Rain	Min. Rain	Ave. Rain	Max. Rain
	4F.N.	14.24	4.5	13.92	14.27	14.33	13.88	14.27	14.33
Calibratad	15 Nov		8.5	13.90	14.25	14.33	13.72	14.24	14.33
Calibrated	10 Doc	10 Dec 14.33	4.5	14.26	14.33	14.33	14.22	14.33	14.33
Sandy Clay Loam Soil	10 Dec		8.5	14.21	14.33	14.33	14.18	14.33	14.33
LOAIII SOII	20 Dec	14.49	4.5	14.49	14.49	14.49	14.48	14.49	14.49
	30 Dec		8.5	14.49	14.49	14.49	14.49	14.49	14.49

15 November Planting - Fast-Development Cultivar 800 Change in Rain 600 (mm) 400 200 0 -200 30 Emergence Stage Vegetative Stage Flowering Stage **Yield Formation Stage** Difference in Water Content in Effective 20 Root Zone (mm) 10 0 -10 RCP 8.5 2035 -20 10 December Planting - Fast-Development Cultivar Change in Rain 600 400 (mm) 200 0 -200 Flowering Stage **Emergence Stage** Vegetative Stage **Yield Formation Stage** 20 Difference in Water Content in Effective Root Zone (mm) 10 0 -10 RCP 8.5 2035 -20 30 December Planting - Fast-Development Cultivar 200 Change in Rain 100 (mm) 0 -100 -200 **Emergence Stage** Vegetative Stage Flowering Stage **Yield Formation Stage** 40 Difference in Water Content in 30 Effective Root Zone (mm) 20 10 0 -10 RCP 4.5 2055 RCP 8.5 2055 -20

Figure 1: Change in total precipitation (mm) and water content in the effective root zone (mm) by developmental stage of the fast-development cultivar maize grown in Central Malawi for the three planting dates as compared to the baseline 1971-2000 period (red line). This data is shown for the three precipitation scenarios: minimum (palest), average (medium shade) and maximum (darkest) precipitation, for the two RPC scenarios and time periods.

■ Minimum ■ Average

Table 8: Number of days exceeding the maximum temperature threshold (32 degrees Celsius) by development stage for each cultivar

	Planting Date	Chago	Historic	RCI	P4.5	RCP8.5	
	Date		HISTORIC	2035	2055	2035	2055
		Emergence	8	6	8	8	7
		Vegetative	1	0	2	1	10
	Nov. 15	Flowering	0	0	0	0	0
		Yield Formation	0	0	0	0	0
		Total	9	6	10	9	17
		Emergence	0	0	0	0	0
Slow-		Vegetative	0	0	0	0	0
Development	Dec. 10	Flowering	0	0	0	0	0
Cultivar		Yield Formation	0	0	0	0	0
		Total	0	0	0	0	0
	Dec. 30	Emergence	0	0	0	0	0
		Vegetative	0	0	0	0	0
		Flowering	0	0	0	0	0
		Yield Formation	0	0	0	0	0
		Total	0	0	0	0	0
	Nov. 15	Emergence	5	5	5	5	5
		Vegetative	4	1	5	4	12
		Flowering	0	0	0	0	0
		Yield Formation	0	0	0	0	0
		Total	9	6	10	9	17
		Emergence	0	0	0	0	0
Fast-		Vegetative	0	0	0	0	0
Development	Dec. 10	Flowering	0	0	0	0	0
Cultivar		Yield Formation	0	0	0	0	0
		Total	0	0	0	0	0
		Emergence	0	0	0	0	0
		Vegetative	0	0	0	0	0
	Dec. 30	Flowering	0	0	0	0	0
		Yield Formation	0	0	0	0	0
		Total	0	0	0	0	0

Table 9: Average annual precipitation rate (mm) for each RCM in 2035 (2020-2049) and 2055 (2040-2069) and a comparison to the 1971-2000 average precipitation rate of 1081.4mm

		RCP 4.	5		RCP 8.5				
	Average	Annual	Chang	Change from		Annual	Change from		
RCM	-	ected	1971	-2000	_	ected	1971	-2000	
	Precipitat	tion (mm)	Ave	rage	Precipitat	tion (mm)	Ave	rage	
	2035	2055	2035	2055	2035	2055	2035	2055	
CCCmaCanRCM	1117.1	1160.3	3%	7%	1155.9	1215.2	7%	12%	
CCCmaSMHI	994.7	991.5	-8%	-8%	969.1	1047.6	-10%	-3%	
CNRM	1104.6	1070.1	2%	-1%	1170.0	1101.1	8%	2%	
CNRMSMHI	1009.7	1020.2	-7%	-6%	1098.7	1083.0	2%	0%	
CSIRO	1056.7	961.1	-2%	-11%	1117.5	1002.1	3%	-7%	
ICHECDMI	1001.1	920.5	-7%	-15%	943.0	904.9	-13%	-16%	
ICHECCCLM	1010.7	974.3	-7%	-10%	932.9	933.0	-14%	-14%	
ICHECKNMI	1063.5	1025.2	-2%	-5%	1047.0	1073.2	-3%	-1%	
ICHECMPI	996.6	976.4	-8%	-10%	934.0	907.4	-14%	-16%	
ICHECSMHI	1065.9	1077.9	-1%	0%	1066.9	1077.4	-1%	0%	
IPSL	1089.4	1160.3	1%	7%	1139.6	1205.3	5%	11%	
MIROC	1039.6	1028.0	-4%	-5%	1068.3	1034.2	-1%	-4%	
MOHCCCLM	1002.0	986.1	-7%	-9%	982.5	990.6	-9%	-8%	
MOHCKNMI	1015.5	1006.9	-6%	-7%	1045.8	1015.1	-3%	-6%	
MOHCSMHI	1062.8	1096.8	-2%	1%	1098.7	1049.4	2%	-3%	
MPICCLM	980.4	971.4	-9%	-10%	995.3	959.2	-8%	-11%	
MPIREMO	1037.5	1019.9	-4%	-6%	1031.0	1021.9	-5%	-6%	
MPISMHI	1080.4	1052.6	0%	-3%	1089.9	1039.3	1%	-4%	
NCCSMHI	1088.3	1105.9	1%	2%	1121.6	1109.0	4%	3%	
NOAA	1075.7	1114.4	-1%	3%	1100.5	1048.2	2%	-3%	

2. Methodology for Calculating Reference Evapotranspiration for Central Malawi

To calculate evapotranspiration for Central Malawi, the FAO Penman Monteith (FPM) model was applied (Allen et al., 1998a).

Equation 1
$$ETo = \frac{0.408\Delta(R_n-G) + \gamma \frac{900}{T+273}u_2(e_S-e_a)}{\Delta + \gamma(1+0.34u_2)}$$

Where:

- ETo is the reference evapotranspiration (mm day⁻¹)
- R_n is the net radiation at the crop surface (MJ m2 day⁻¹),
- G is the soil heat flux density (MJ m-2 day⁻¹)
- T is the mean daily air temperature (°C)
- u₂ is wind speed at 2 m height (m s⁻¹)
- e_s is the saturation vapour pressure (kPa)
- e_a is the actual vapour pressure (kPa), see Equation 10
- e_s e_a is the saturation vapour pressure deficit (kPa)
- Δ is the slope vapour pressure curve (kPa°C⁻¹)
- γ is the psychrometric constant (kPa °C⁻¹)

It is not possible to get data for all of the above variables for Central Malawi, either from observed data of the past, or from climate models used to hindcast the past or forecast future climates. Therefore, temperature-based calculation methods were applied for climatic variables with no primary data available (Allen et al., 1998b). This methodology has been tested for Malawi by Wang et al. (2011), and for South Malawi by Ngongondo et al. (2012) and deemed to be appropriate for use.

2.1. Net Radiation at the Crop Surface

 R_n is the net radiation at the crop surface (MJ m2 day⁻¹) and can be calculated as follows: Equation 2 $R_n = R_{ns} - R_{nl}$

Where:

• R_{ns} is the net incoming shortwave radiation (MJm-2 day-1) and can be calculated as follows: Equation 3 $R_{ns} = (1-\alpha)R_s$

Where:

- \propto is the albedo or canopy reflection coefficient, which is 0.23 for the hypothetical grass reference crop
- R_s is the fraction of the solar radiation not reflected from the surface (MJm-2 day-1) and can be calculated as follows:

Equation 4
$$R_s = k_{Rs} \sqrt{T_{max} - T_{min}} R_a$$

Where:

- K_{RS} is adjustment coefficient. For inland regions not influenced by large bodies of water, K_{RS} = 0.16; for coastal regions, or regions where the air mass is influenced by a large nearby water body, K_{RS} = 0.19. Since Central Malawi is highly influenced by the presence of a large water body (Lake Malawi). K_{RS} is considered to be 0.19 in this study.
- T_{max} is the maximum air temperature (°C)
- T_{min} is the minimum air temperature (${}^{\circ}$ C)
- R_a is extra-terrestrial radiation (MJm-2 day-1) and can be calculated as follows:

Equation 5
$$R_a = \frac{24(60)}{\pi} G_{sc} d_r [\omega_s \sin(\varphi) \sin(\delta) + \cos(\varphi) \cos(\delta) \sin(\omega_s)]$$

Where:

- G_{SC} is the solar constant = 0.0820 MJm⁻²min⁻¹
- d_r is the inverse relative since earth-Sun (rad) which can be calculated as follows:

Equation 6
$$d_r = 1 + 0.033 \cos\left(\frac{2\pi}{365}J\right)$$

Where:

- J is the number of days in the year between 1 (1 January) and 365 or 266 (31 December). J at the middle of each month = 30.4M-15 where M is the month number
- ω_s is the sunset hour angle (rad) which can be calculated as follows:

Equation 7
$$\omega_s = \arccos[-\tan(\varphi)\tan(\delta)]$$

Where:

- φ is the latitude (rad)
- δ is the solar declination (rad) which can be calculated as follows:

Equation 8
$$\delta = 1 + 0.409 \sin\left(\frac{2\pi}{365}J - 1.39\right)$$

R_{nl} is in the net outgoing longwave radiation (MJm-2 day-1) and can be calculated as follows:

Equation 9
$$R_{nl} = \sigma \left[\frac{T_{maxK^4} + T_{minK^4}}{2} \right] \left(0.34 - 0.14 \sqrt{e_a} \right) \left(1.35 \frac{R_s}{R_{so}} - 0.35 \right)$$

Where:

- σ is the Stefan-Boltzmann constant [4.903 x 10⁻⁹ MJ K⁻⁴ m⁻² day⁻¹
- $T_{max,K}$ is the maximum absolute temperature during the 24-hour period [K = °C + 273.16],
- $T_{min, K}$ minimum absolute temperature during the 24-hour period [K = $^{\circ}$ C + 273.16],
- ea actual vapour pressure [kPa], which can be calculated as follows:

Equation 10
$$e_a = e^o(T_{dew}) = 0.6108exp\left(\frac{17.27T_{dew}}{T_{dew} + 237.3}\right)$$

Where:

■ T_{dew} is the dew point temperature. T_{dew} is near the minimum temperature (T_{min}) when the relative humidity is nearly 100%. In semi-arid regions, T_{dew} is estimated by subtracting 2°C from T_{min} . As Central Malawi's humidity is typically under 90%, the T_{dew} can be calculated as follows:

Equation 11
$$T_{dew} = T_{min} - 2$$

- R_s is the solar radiation [MJ m-2 day-1], see Equation 4.
- R_{so} is the clear-sky solar radiation [MJ m-2 day-1], which can be calculated as follows:

Equation 12
$$R_{SO} = (0.75 + 0.00002(h))R_a$$

Where:

- h is the elevation above sea level (m)
- R_a is extra-terrestrial radiation, (MJm-2 day-1), see Equation 5.

2.2. Soil Heat Flux Density

G is the soil heat flux density (MJ m-2 day-1)

- For daily assessment, G is assumed to be zero (0) as the soil heat flux is relatively small Equation 13: $G_{day} = 0$
- For monthly assessments,

Equation 14:
$$G = 0.07 (T_{month,i+1} - T_{month,i-1})$$

Where:

- T_{mon, i-1} is the mean air temperature of the previous month (°C)
- T_{mon, i+1} is the mean air temperature of the next month (°C)

2.3. Mean Temperature

T is the mean daily air temperature (°C), which can be calculated as follows:

Equation 15:
$$T_{mean} = \frac{T_{min} + T_{max}}{2}$$

Where:

- T_{max} is the maximum air temperature (°C)
- T_{min} is the minimum air temperature (°C)

2.4. Wind Speed at 2m height

 u_2 is wind speed at 2 m height (m s⁻¹). We can use a default value of 172 km day⁻¹ which is the average value over different weather stations around the globe. This was recommended by Allen et al. (1998). To convert to the correct units for the equation above (m s⁻¹) we can do the following:

Equation 16:
$$\frac{172 \text{km}}{\text{day}} \times \frac{\text{day}}{24 \text{ hours}} \times \frac{\text{hour}}{60 \text{ minutes}} \times \frac{\text{minute}}{60 \text{ seconds}} \times \frac{1000 \text{ meters}}{\text{km}} = \frac{172,000 \text{ meters}}{86,400 \text{ seconds}}$$

2.5. Vapour Pressure

To calculate ETO, various vapour pressure variables are required, including the saturation vapour pressure (e_a), the actual vapour pressure (e_a) and the slope vapour pressure curve (Δ).

• e_s is the saturation vapour pressure (kPa), it can be calculated as follows:

Equation 17:
$$e_s = \frac{e^o(T_{max}) + e^o(T_{min})}{2}$$

Where:

 e⁰(T_{max}) is the vapour pressure at maximum temperature, and can be calculated as follows:

Equation 18:
$$e^{o}(T_{max}) = 0.6108exp\left(\frac{17.27T_{max}}{T_{max}+237.3}\right)$$

Where:

- T_{max} is the maximum air temperature (°C)
- e⁰(T_{min}) is the vapour pressure at minimum temperature, and can be calculated as follows:

Equation 19:
$$e^{o}(T_{min}) = 0.6108exp\left(\frac{17.27T_{min}}{T_{min}+237.3}\right)$$

Where:

- T_{min} is the minimum air temperature (°C)
- e_a is the actual vapour pressure (kPa), see Equation 10
- Δ is the slope vapour pressure curve (kPa°C⁻¹)

Equation 20:
$$\Delta = \frac{4098 \left[0.6108 exp \left(\frac{17.27T}{T+237.3} \right) \right]}{(T+237.3)^2}$$

Where:

- T is the mean air temperature (°C), see Equation 15
- exp[...] 2.7183 (base of natural logarithm) raised to the power [...]

2.6. Psychrometric Constant

γ is the psychrometric constant (kPa °C⁻¹), it can be calculated as follows:

Equation 21:
$$\gamma = \frac{c_p P}{\varepsilon \lambda}$$

Where:

- C_P is the specific heat at a constant pressure, $C_P = 1.013 \times 10^{-3} \text{ MJ kg}^{-1} \, ^{\circ}\text{C}^{-1}$
- P is atmospheric pressure (kPa), which can be calculated as follows:

Equation 22:
$$P = 101.325(293 - 0.0065(h))^{5.25588}$$

Where:

- h is the altitude above sea level in meters (m)
 - For Central Malawi, the average altitude above sea level (h) is 948.1944444m (determined using data from JISAO (2014))
- ε is the ratio molecular weight of water vapour / dry air, ε = 0.622
- λ is the latent heat of vaporization, λ = 2.45 MJ kg⁻¹

3. References

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