The 6th IASTED International Conference on

Modelling, Simulation and Identification ~MSI 2016~

Optimal Control of the Weelchair Wheelie

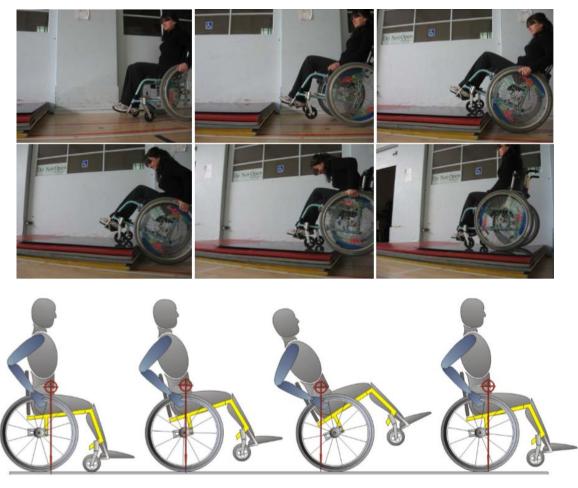
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Introduction

Wheelie in wheelchairs



(Denison, 2013)

Introduction

Manual

Motorized

Power-Assisted





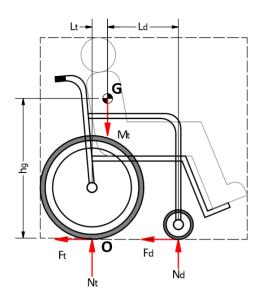


Objective

Propose a control strategy to initiate and sustain the wheelie in power-assisted wheelchairs using a model of the user and wheelchair system and an optimal control formulation.

Model of Phase 1





- Sagittal plane (2D);
- 2 rigid bodies;
- Front wheels on the ground (stable);
- 1 DoF;
- Control: wheel torque
- Equation of motion:

$$\frac{\tau}{R} = \left(M + \frac{J_R}{R^2}\right) \cdot \ddot{x} + F_R$$

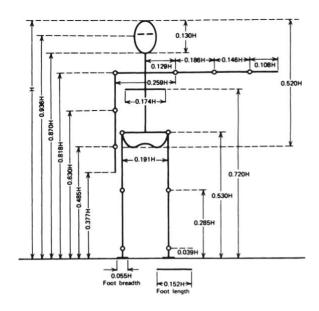
Transition acceleration:

$$\ddot{x}_{nf} = \frac{d_{xcg}}{h_{cg}} \cdot g$$

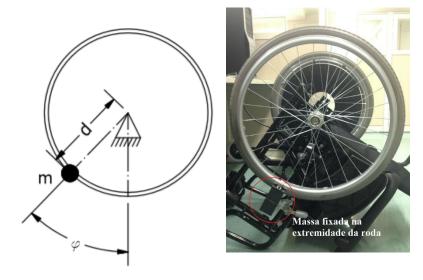
Estimation of Parameters



Center of mass locations



(Winter, 2009)



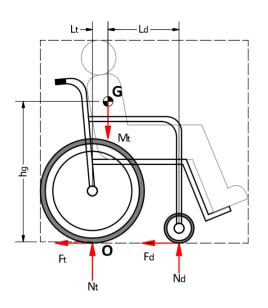
Moments of inertia



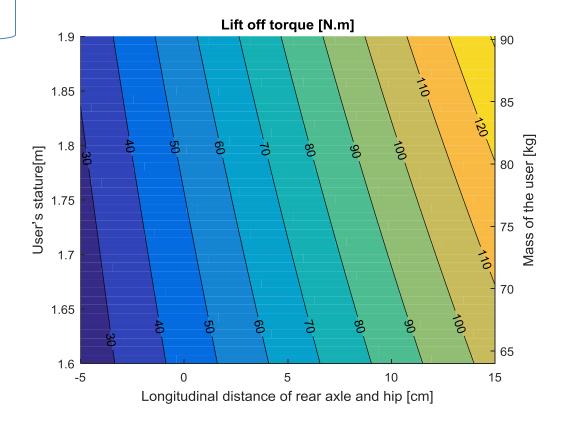
Lift-Off Torque

$$\frac{\tau}{R} = \left(M + \frac{J_R}{R^2}\right) \cdot \ddot{x} + F_R$$

$$\ddot{x}_{nf} = \frac{d_{xcg}}{h_{cg}} \cdot g$$

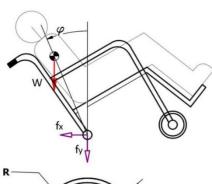


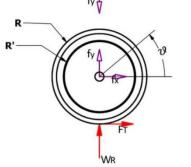
$$\tau_{nf} = \left[\left(M + \frac{J_R}{R^2} \right) \cdot \frac{d_{xcg}}{h_{cg}} \cdot g + F_R \right] \cdot R$$



Model of Phase 2







- Sagittal plane (2D);
- 2 rigid bodies;
- 2 DoF's;
- Front wheels off the ground (unstable);
- Control: wheel torque;
- Equations of motion:

$$\begin{aligned} \tau - F_R \cdot R &= \left[J_R + (M_r + M_c) \cdot R^2 \right] \cdot \ddot{\theta} + (M_c \cdot R \cdot l \cdot \cos \varphi) \cdot \ddot{\varphi} \\ &- M_c \cdot R \cdot l \cdot \dot{\varphi}^2 \cdot \sin \varphi \\ - \tau &= (M_c \cdot l \cdot R \cdot \cos \varphi) \cdot \ddot{\theta} + (J_c + M_c \cdot l^2) \cdot \ddot{\varphi} - M_c \cdot g \cdot l \cdot \sin \varphi \end{aligned}$$

Optimal Control Formulation

Find (optimization variables):

- $\tau(t)$ wheel torque
- $x(t) = [\varphi(t) \ \dot{\varphi}(t) \ \dot{\theta}(t)]$ states

that minimize the cost function:

$$J = \int_0^{tf} \tau^2 \, dt$$

subject to (constraints):

Equations of motion:

$$\tau - F_R \cdot R = [J_R + (M_r + M_c) \cdot R^2] \cdot \ddot{\theta} + (M_c \cdot R \cdot l \cdot \cos \varphi) \cdot \ddot{\varphi}$$
$$-M_c \cdot R \cdot l \cdot \dot{\varphi}^2 \cdot \sin \varphi$$
$$-\tau = (M_c \cdot l \cdot R \cdot \cos \varphi) \cdot \ddot{\theta} + (J_c + M_c \cdot l^2) \cdot \ddot{\varphi} - M_c \cdot g \cdot l \cdot \sin \varphi$$

Solution of Optimal Control Problem (Direct Collocation)

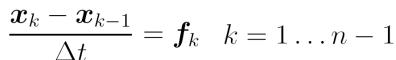
Optimal Control Problem > Nonlinear Programming

Find
$$\boldsymbol{u}(t)$$
 $\boldsymbol{x}(t)$

 $\boldsymbol{x}_k = \boldsymbol{x}(t_k) \ \boldsymbol{u}_k = \boldsymbol{u}(t_k)$

system dynamics

$$\dot{\boldsymbol{x}}(t) = \boldsymbol{f}(\boldsymbol{x}(t), \boldsymbol{u}(t), t)$$



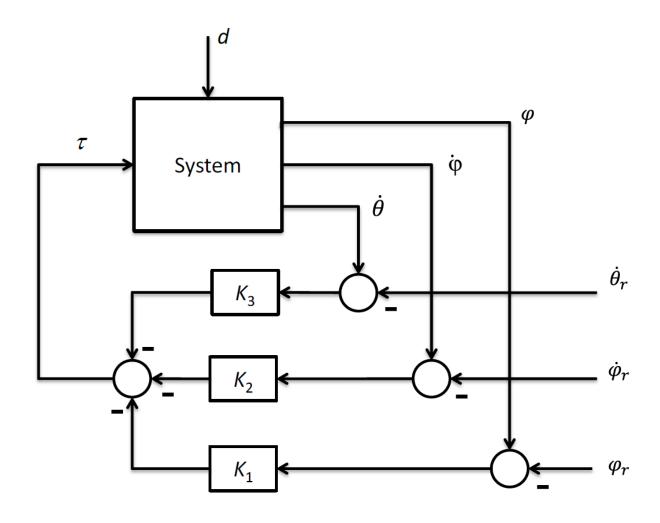
(Kaplan and Heegaard, J. Biomech., 2001); (Ackermann and van den Bogert, J. Biomech., 2010); (Lee and Umberger, PeerJ, 2016)

Solver: PROPT/SNOPT (Tomlab)

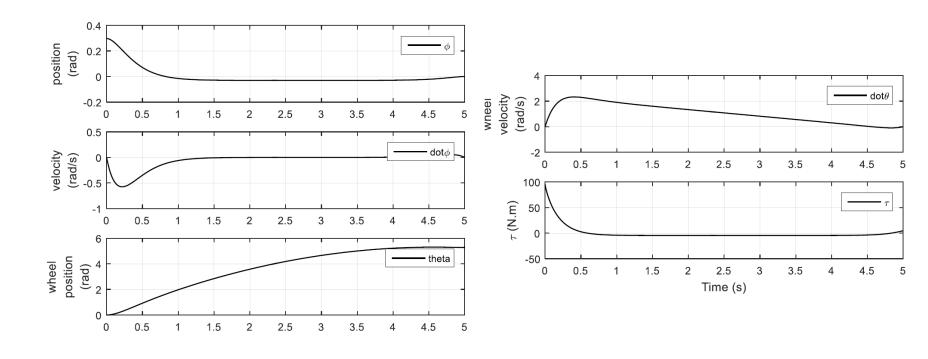
PROPT – transcription

SNOPT – large-scale optimization

Closed-Loop Controller

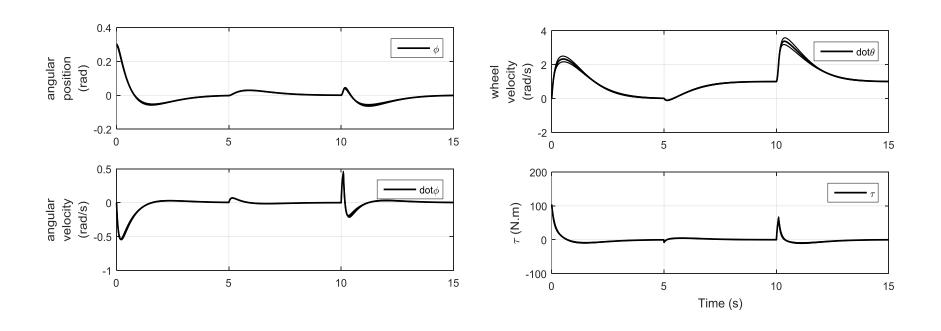


Results: Reference Patterns



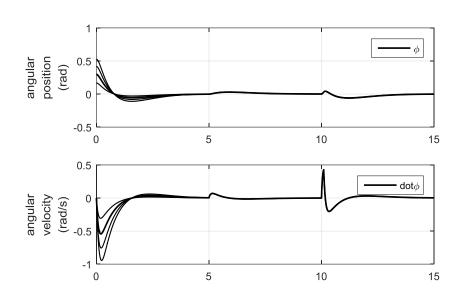
Closed-Loop Response

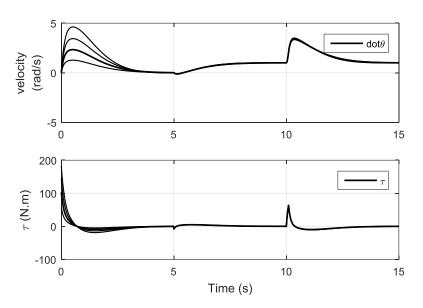
Different Statures: 1.6 m, 1.75 m and 1.90 m



Closed-Loop Response

Different fore-aft adjustments: -0.05 m, 0.00 m and 0.05 m





Discussion and Conclusions

- The modelling approach allowed for global changes in joint stiffness, independent from muscle properties;
- The optimal control framework was shown to have great potential in predicting gait pattern changes in musculoskeletal properties due to aging or desease;
- Observed changes in muscle activation patterns due to stiffening of ankle joint and decrease in muscle force capacity is consistent with findings in the literature;
- Future work: apply the presented approach to investigate typical changes in gait patterns of neuropathic diabetic patients.

Thank you!



