

وَمَا أُوتِيتُمْ مِنَ الْعِلْمِ إِلَّا قَلِيلًا

Analog IC Design

Lecture 07 Cascode Amplifiers

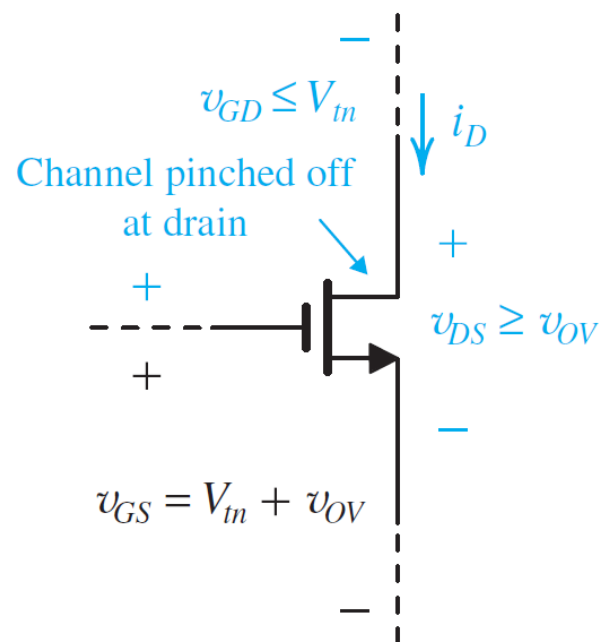
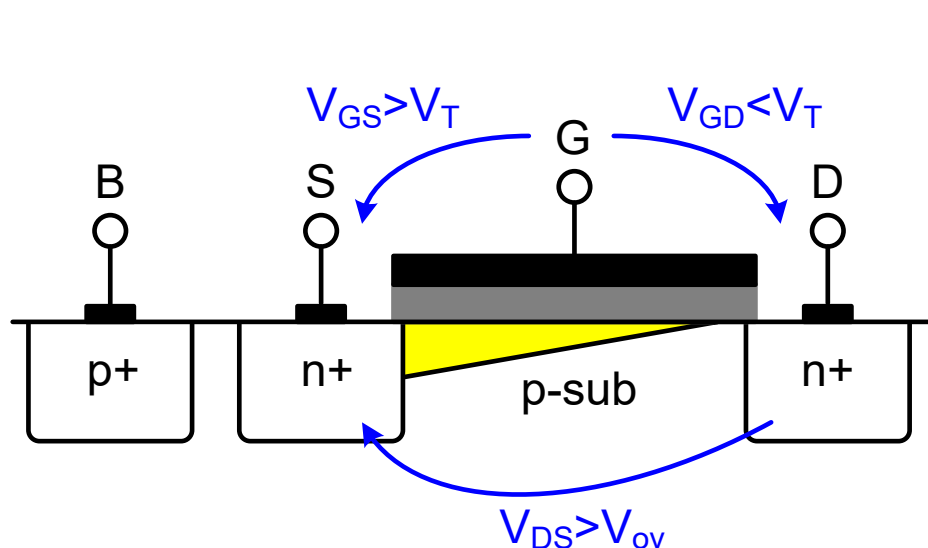
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MOSFET in Saturation

- ❑ The channel is pinched off if the difference between the gate and drain voltages is not sufficient to create an inversion layer

$$I_D = \frac{\mu_n C_{ox}}{2} \frac{W}{L} \cdot V_{ov}^2 (1 + \lambda V_{DS})$$



Regions of Operation Summary

OFF
(Subthreshold)

$$V_{GS} < V_T$$

ON

$$V_{GS} > V_T$$

Triode

$$V_{DS} < V_{ov}$$

Or

$$V_{GD} > V_T$$

Pinch-Off
(Saturation)

$$V_{DS} \geq V_{ov}$$

Or

$$V_{GD} \leq V_T$$

$$I_D = \mu C_{ox} \frac{W}{L} \left(V_{ov} V_{DS} - \frac{V_{DS}^2}{2} \right)$$

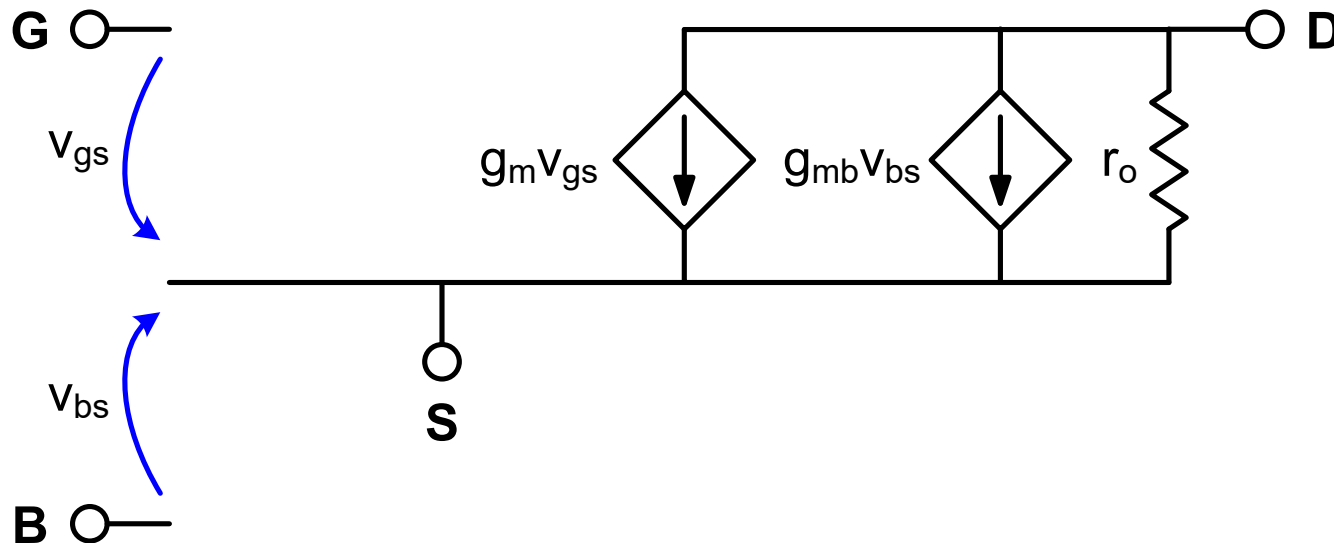
$$I_D = \frac{\mu C_{ox}}{2} \frac{W}{L} V_{ov}^2 (1 + \lambda V_{DS})$$

Low-Frequency Small-Signal Model

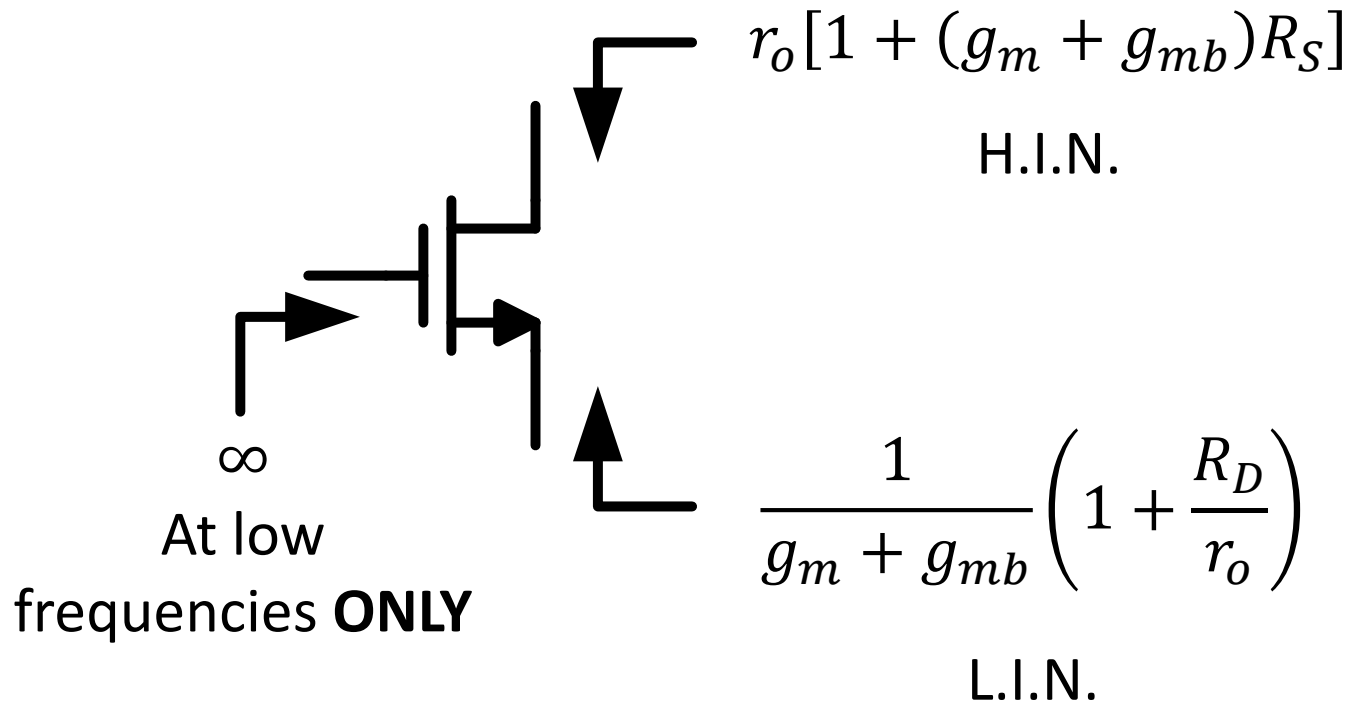
$$g_m = \frac{\partial I_D}{\partial V_{GS}} = \mu C_{ox} \frac{W}{L} V_{ov} = \sqrt{\mu C_{ox} \frac{W}{L} \cdot 2I_D} = \frac{2I_D}{V_{ov}}$$

$$g_{mb} = \eta g_m, \quad \eta \approx 0.1 - 0.25$$

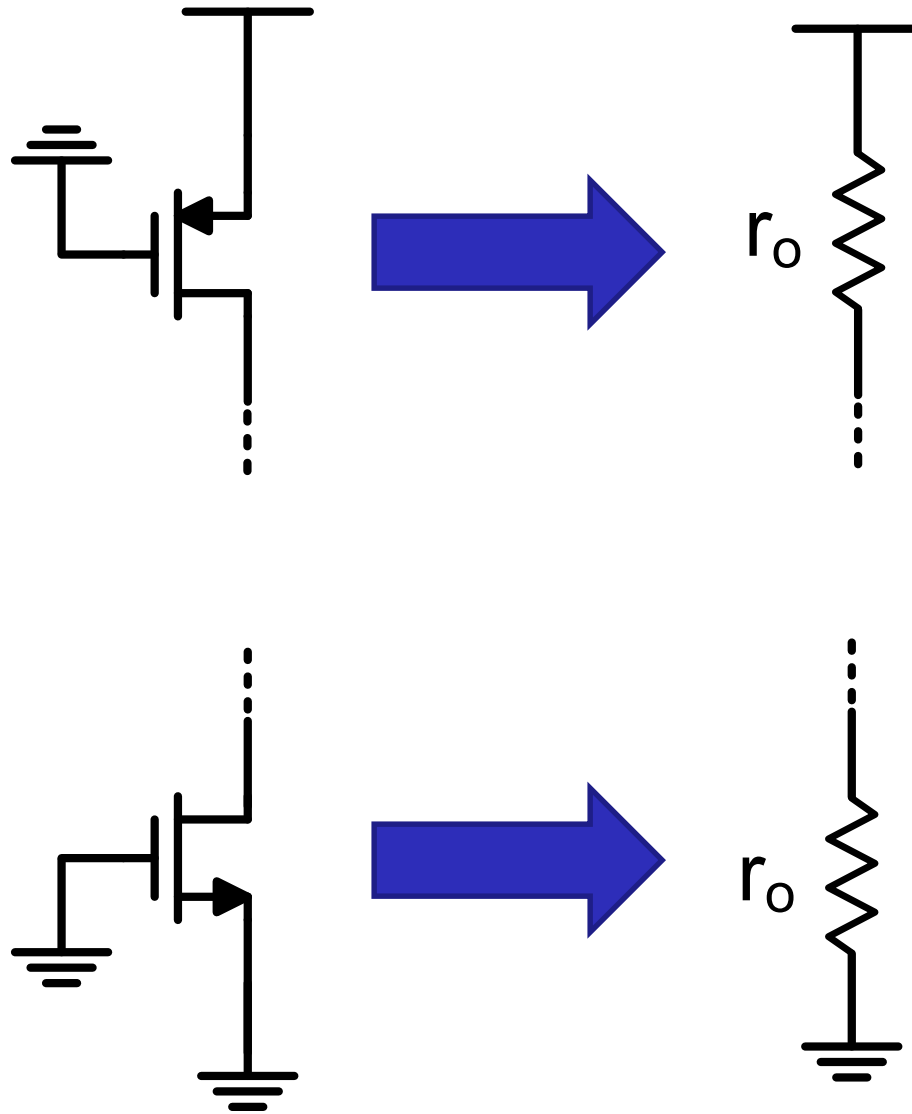
$$r_o = \frac{1}{\frac{\partial I_D}{\partial V_{DS}}} = \frac{1}{\lambda I_D}, \quad \lambda \propto \frac{1}{L}$$



Rin/out Shortcuts Summary

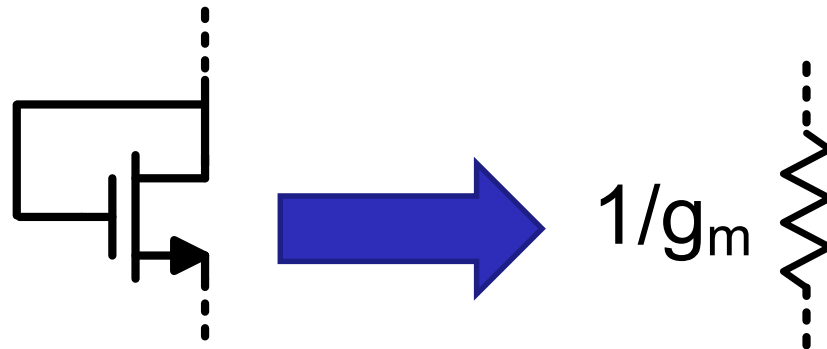
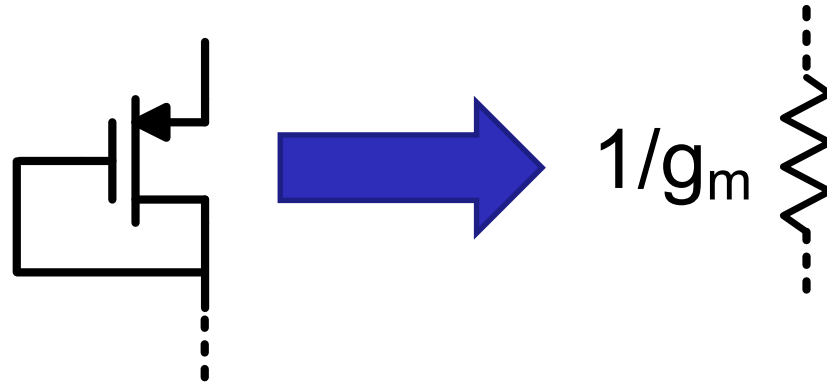


Active Load (Source OFF)



Diode Connected (Source Absorption)

- ❑ Always in saturation
- ❑ Bulk effect: $g_m \rightarrow g_m + g_{mb}$



Why GmRout?

$$R_{out} = \frac{v_x}{i_x} @ v_{in} = 0$$

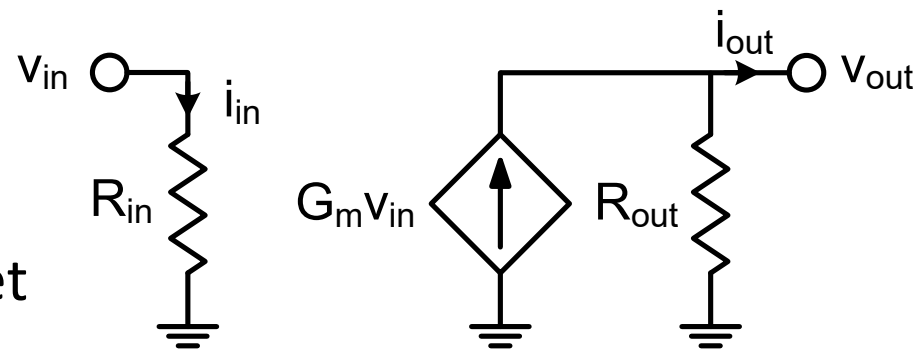
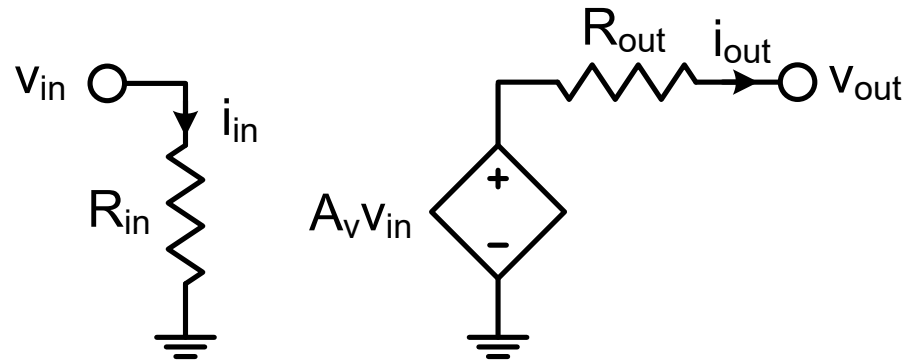
$$G_m = \frac{i_{out,sc}}{v_{in}}$$

$$A_v = G_m R_{out}$$

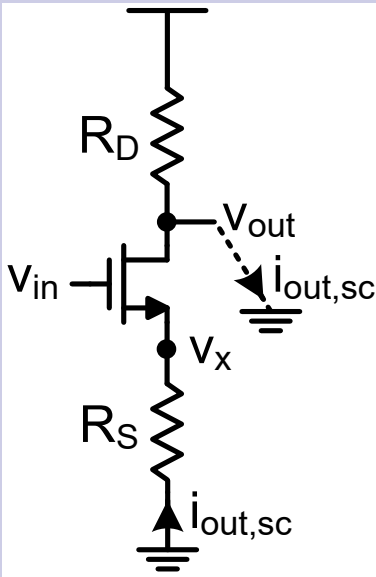
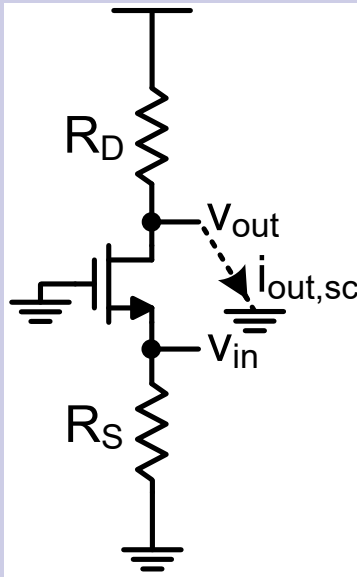
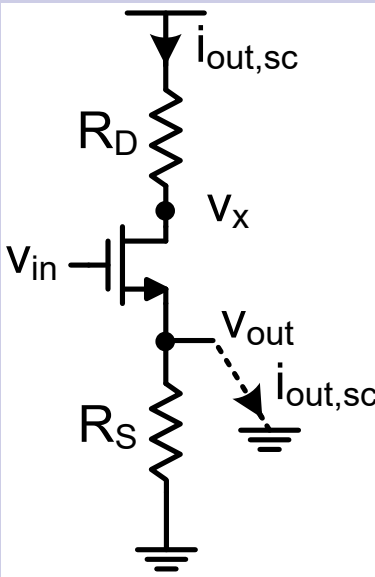
$$A_i = G_m R_{in}$$

□ Divide and conquer

- Rout simplified: $v_{in}=0$
- Gm simplified: $v_{out}=0$
- We already need $R_{in/out}$
- We can quickly and easily get $R_{in/out}$ from the shortcuts

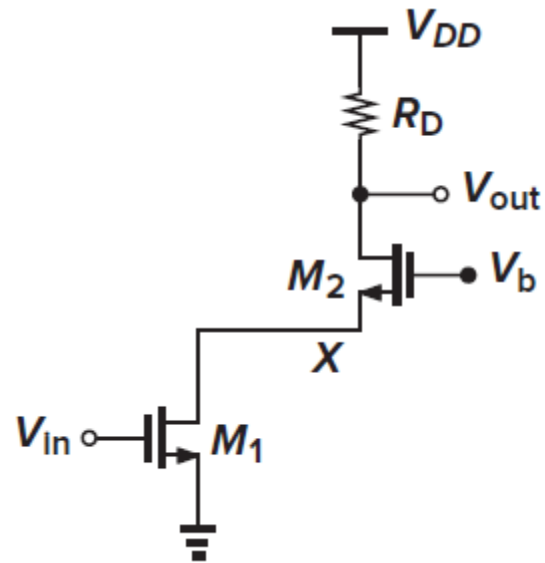


Summary of Basic Topologies

	CS	CG	CD (SF)
			
	Voltage & current amplifier	Current buffer	Voltage buffer
Rin	∞	$R_S // \frac{1}{g_m + g_{mb}} \left(1 + \frac{R_D}{r_o} \right)$	∞
Rout	$R_D // r_o [1 + (g_m + g_{mb})R_S]$	$R_D // r_o$	$R_S // \frac{1}{g_m + g_{mb}} \left(1 + \frac{R_D}{r_o} \right)$
Gm	$\frac{-g_m}{1 + (g_m + g_{mb})R_S}$	$g_m + g_{mb}$	$\frac{g_m}{1 + R_D/r_o}$

Cascode

□ CS + CG



Cascode as a Single Stage

- Transconductance is always related to the input device (VCCS)

$$G_m \approx -g_{m1}$$

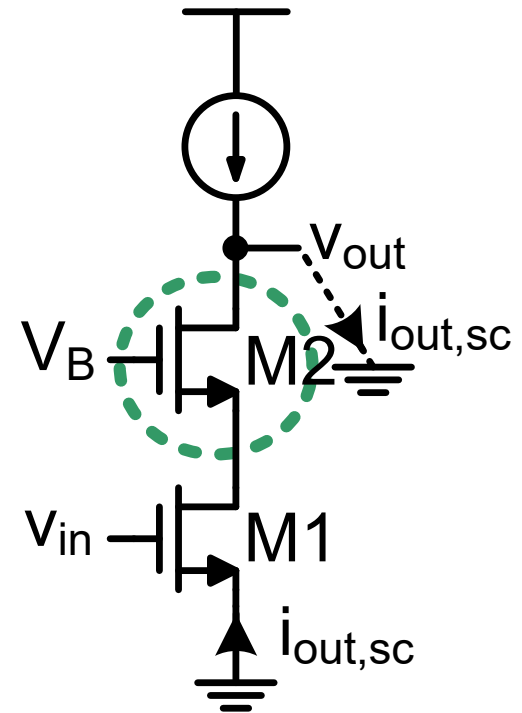
Same Gm of CS

$$\begin{aligned} R_{out} &\approx r_{o2}[1 + (g_{m2} + g_{mb2})r_{o1}] \\ &\approx r_{o2}(g_{m2} + g_{mb2})r_{o1} \end{aligned}$$

Rout significantly boosted

- Assume all g_m and r_o are equal and neglect body effect

$$A_v = -(g_m r_o)^2$$



Cascode as CS + CG

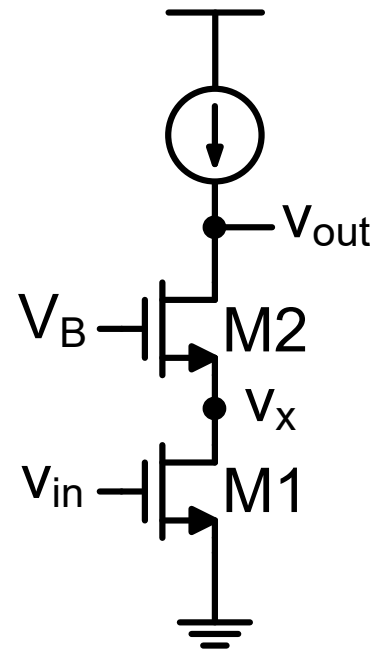
$$CS: \frac{v_x}{v_{in}} = -g_{m1}(r_{o1} // \infty)$$

$$CG: \frac{v_o}{v_x} = (g_{m2} + g_{mb2})r_{o2}$$

$$A_v = \frac{v_x}{v_{in}} \cdot \frac{v_{out}}{v_x} \\ \approx -g_{m1}r_{o1}(g_{m2} + g_{mb2})r_{o2}$$

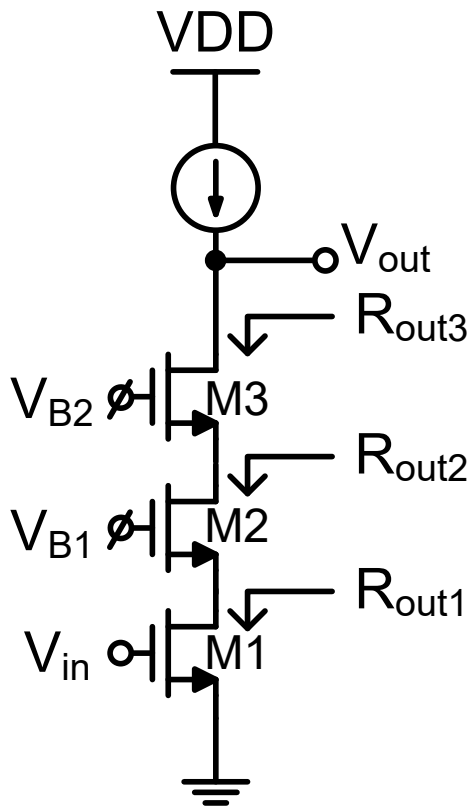
- Assume all g_m and r_o are equal and neglect body effect

$$A_v = -(g_m r_o)^2$$



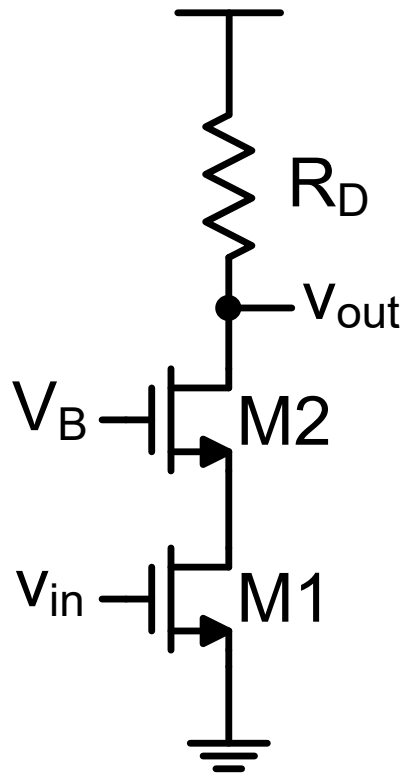
Q: Double Cascode

- Find the voltage gain. Assume all g_m and r_o are equal and neglect body effect.



What if R_D is small?

- ❑ Is this cascode useful?
 - No for gain, but yes for BW



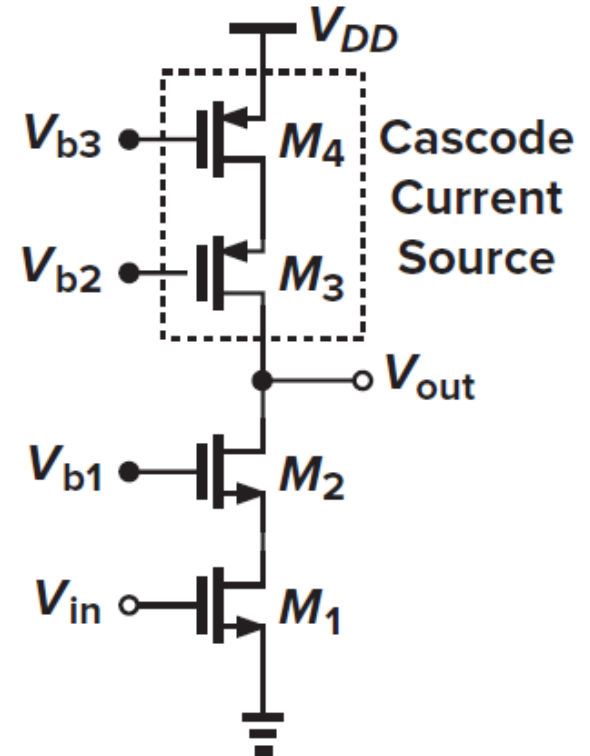
Cascode Load

❑ If you want to keep the large R_{out} , you must use cascode load

❑ Assume all g_m and r_o are equal and neglect body effect

$$A_v = -\frac{(g_m r_o)^2}{2}$$

❑ Output swing $\approx V_{DD} - 4V_{ov}$



Cascode Large Signal Analysis

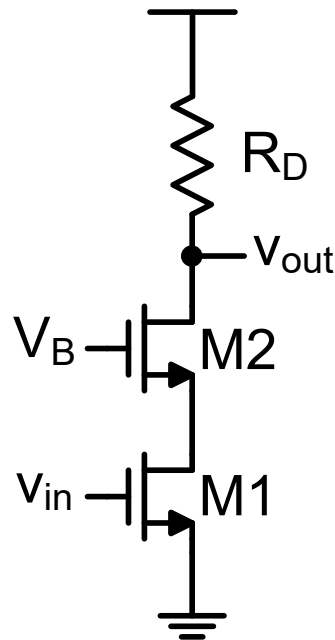
- ❑ Cascode bias voltage

$$V_B \geq V_{TH2} + V_{ov2} + V_{ov1}$$

- ❑ Input and output ranges are coupled oppositely (max vs min)

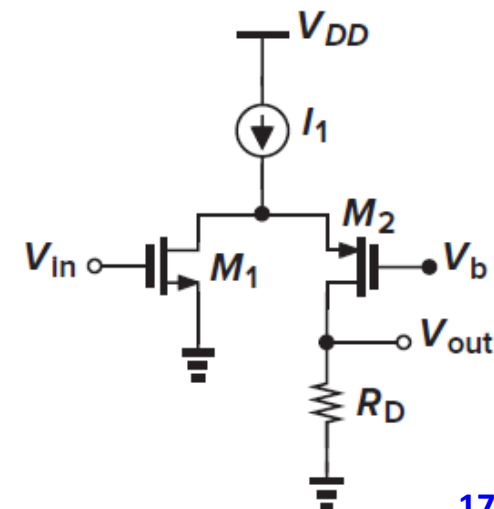
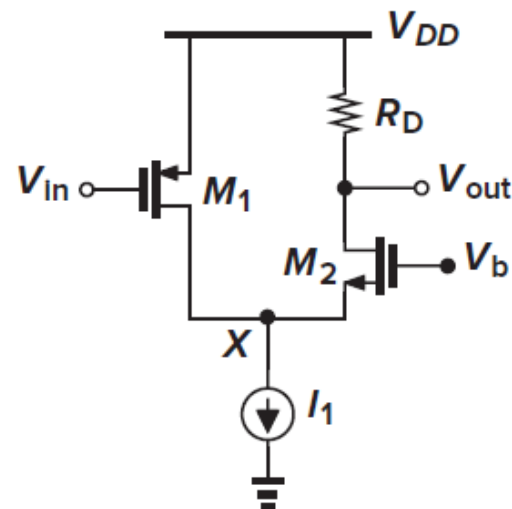
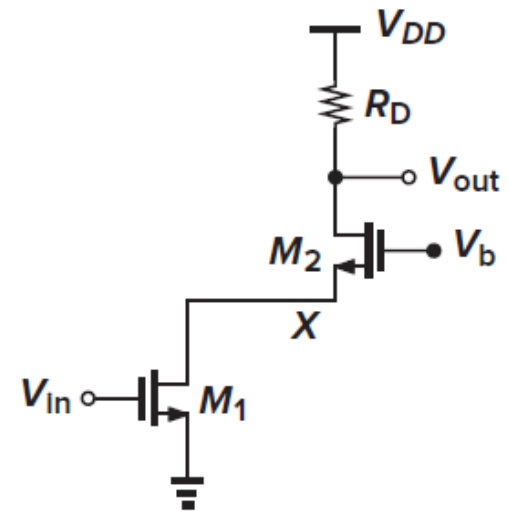
$$V_{in,max} = V_{TH1} + V_{DS1}$$

$$V_{out,min} = V_{ov2} + V_{DS1} = V_{ov2} + V_{in,max} - V_{TH1}$$



Telescopic vs Folded Cascode

- ❑ Telescopic: CS + CG (both NMOS or both PMOS)
 - Both CS and CG use same bias current
- ❑ Folded: CS + CG (NMOS-PMOS combination)
 - The small signal current is folded up or down
 - Extra bias current is needed
 - R_{out} is lower (due to IDC)
 - Why is it useful?



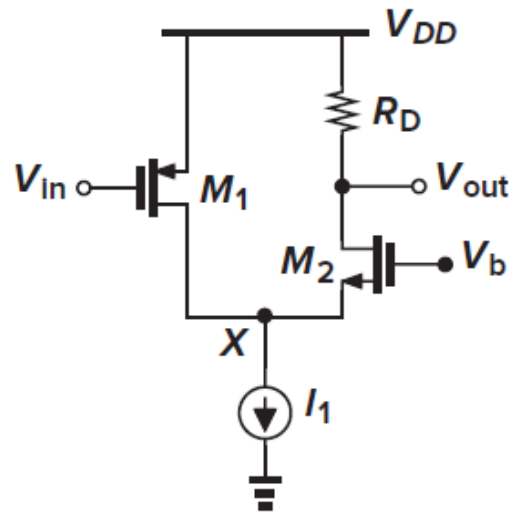
Folded Cascode

- ❑ Input and output ranges are NOT coupled oppositely

$$V_{in,min} = -|V_{TH1}| + V_{ISS}$$

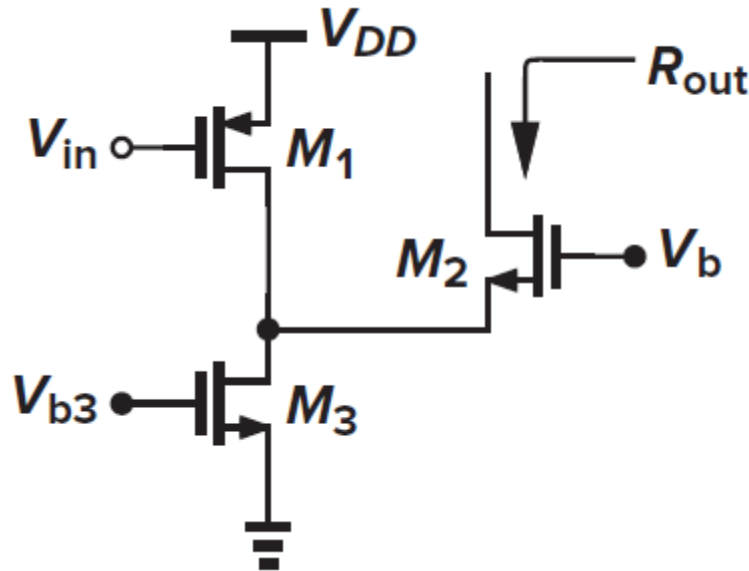
$$V_{out,min} = V_{ov2} + V_{ISS} = V_{ov2} + V_{in,min} + |V_{TH1}|$$

- ❑ More on this point when we study OTAs



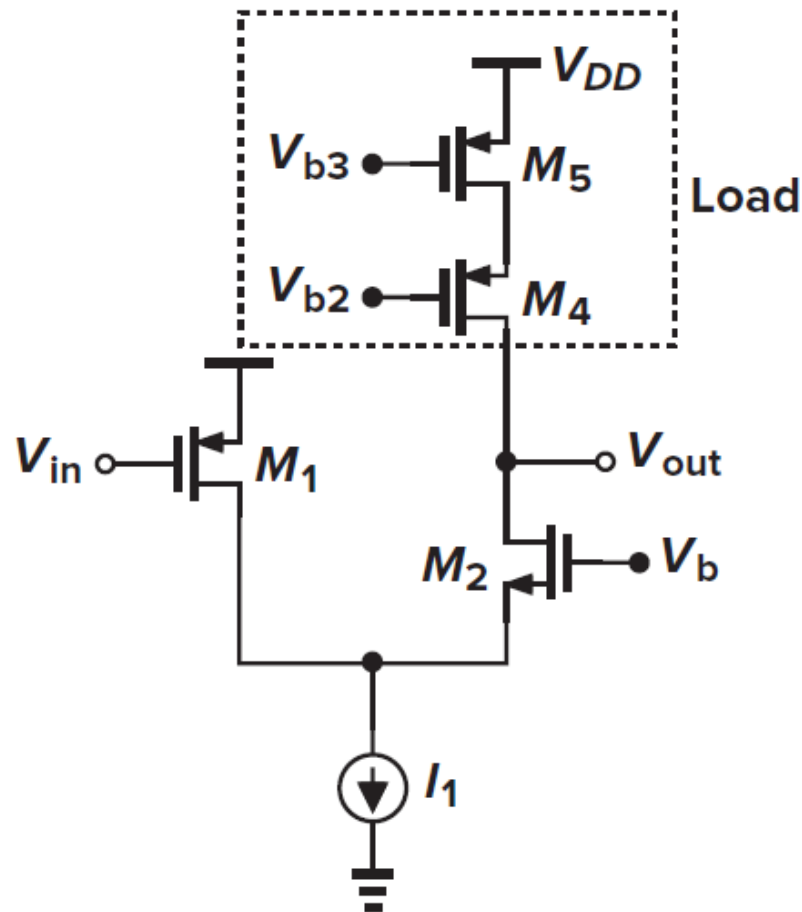
Q: Rout of Folded Cascode

- Assume all transistors have same g_m and r_o , and neglect body effect. Calculate R_{out} .



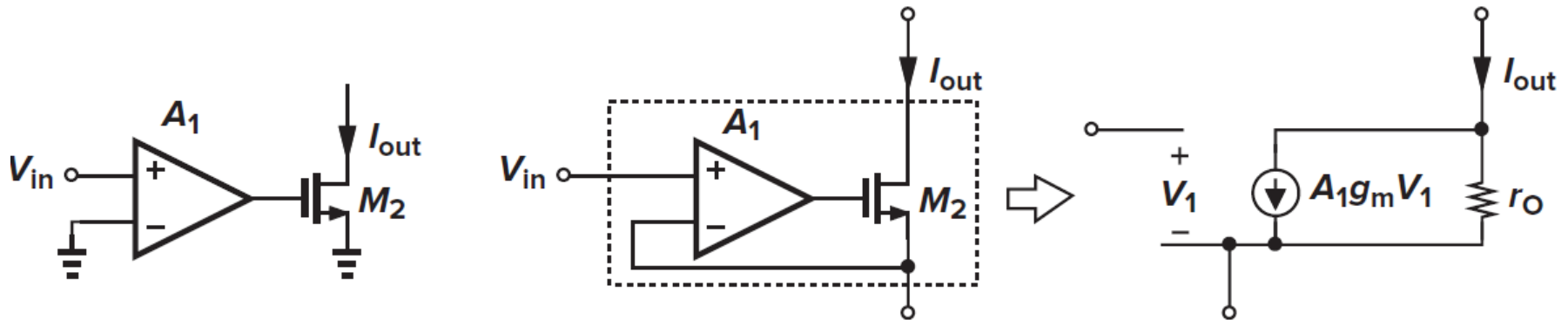
Folded Cascode With Cascode Load

- Calculate $A_v = G_m R_{out}$. Assume all transistors have same g_m and r_o , and neglect body effect. Assume I_1 is implemented using a single NMOS.



Gain Boosting: Super Transistor

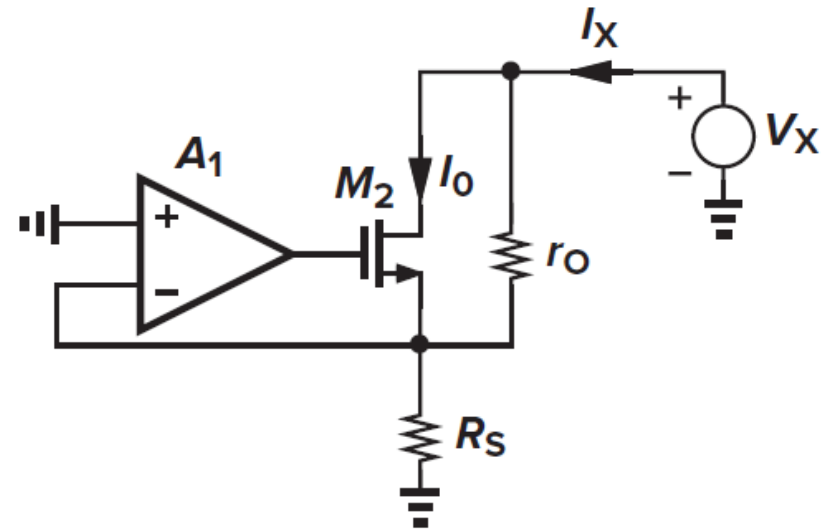
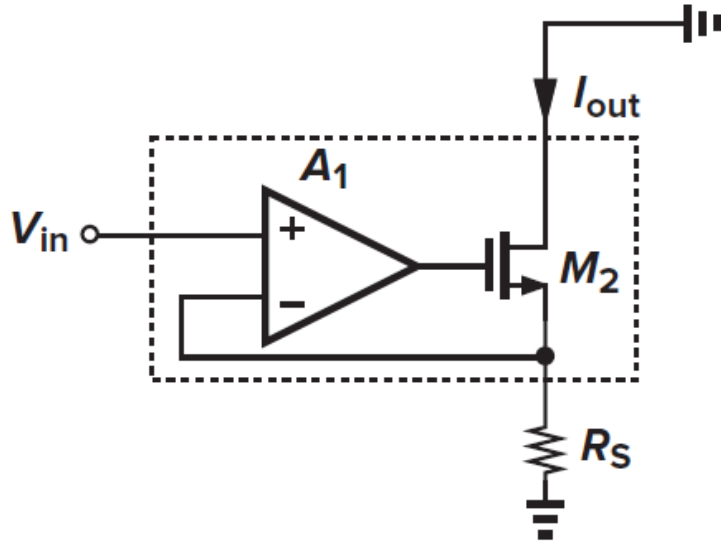
- ❑ Assume $A_1 \gg 1$
- ❑ $g_{m,super} = A_1 g_m$
- ❑ $r_{o,super} = r_o$



Gain Boosting: Super Transistor

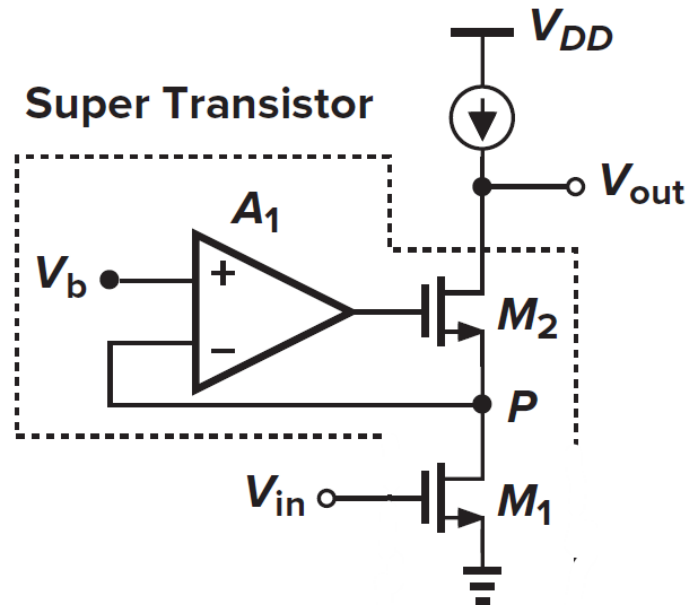
$$\square \quad G_m \approx \frac{g_{m,\text{super}}}{1 + g_{m,\text{super}}R_S} \approx \frac{A_1 g_m}{1 + A_1 g_m R_S} \approx \frac{1}{R_S}$$

$$\square \quad R_{\text{out}} = r_o(1 + g_{m,\text{super}}R_S) = r_o(1 + A_1 g_m R_S)$$



Super Cascode

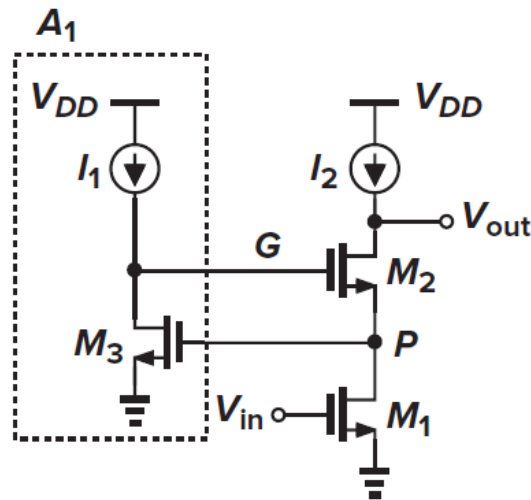
- ❑ A.k.a. regulated cascode or gain boosted cascode
- ❑ $G_m \approx g_{m1}$
- ❑ $R_{out} = r_{o2}(1 + g_{m2,super}r_{o1}) = r_{o2}(1 + A_1 g_{m2}r_{o1})$
- ❑ $A_v \approx A_1(g_{m1}r_{o1})(g_{m2}r_{o2})$
- ❑ Gain is boosted while preserving headroom
- ❑ But more power and noise



Super Cascode Implementation

❑ NMOS CS

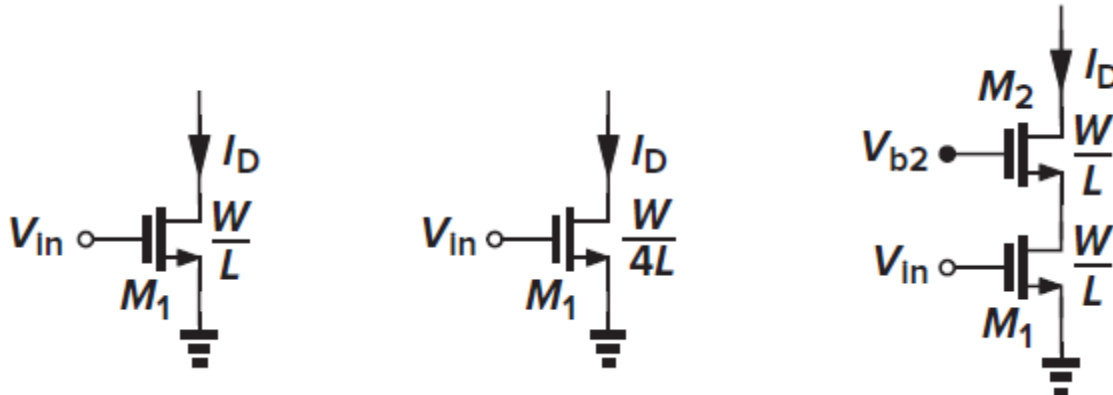
- Headroom limitation
- $V_P = V_{TH} + V_{ov3}$ instead of V_{ov1}



Thank you!

Cascode vs Longer Device

- ❑ Assuming same bias current and headroom requirement
- ❑ For single device
 - Double V_{ov} means 4 times L can be used ($I_D \propto (W/L)V_{ov}^2$)
 - $r_o = 1/\lambda I_D$ multiplied by 4, but g_m divided by 2 ($g_m = 2I_D/V_{ov}$)
 - Overall gain increases by a factor of 2
- ❑ For cascode
 - Rout multiplied by $g_m r_o$, and g_m unchanged
 - Overall gain increases by a factor of $g_m r_o$
 - But we need extra bias voltage



Poor Man's Cascode

- ❑ Can we eliminate the extra bias voltage?

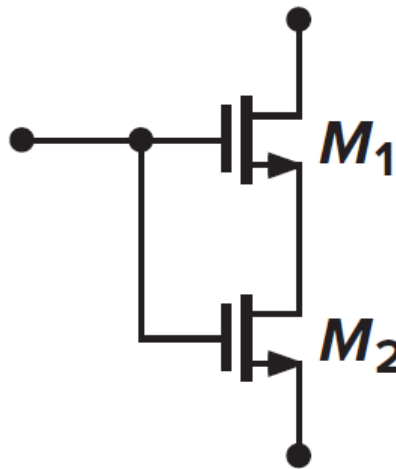
$$V_{DS2} = V_{GS2} - V_{GS1} = V_{ov2} - V_{ov1} < V_{ov2}$$

M2 ALWAYS in triode \rightarrow Not a cascode, just twice the length

- ❑ But what if $V_{T2} > V_{T1}$ (devices with different threshold voltages)?

$$V_{DS2} = V_{GS2} - V_{GS1} = (V_{ov2} - V_{ov1}) + (V_{T2} - V_{T1}) > V_{ov2}$$

M2 in saturation if: $(V_{T2} - V_{T1}) > V_{ov1}$



Gain Boosting Implementation

- ❑ NMOS CS (a): headroom limitation
 - $V_P = V_{TH} + V_{ov3}$ instead of V_{ov1}
- ❑ PMOS CS (b): M3 will be in triode
 - $V_G - V_P > V_{TH}$
- ❑ Folded cascode (c): M4 provide level shift

