## Spintronic Technology For Energy-Efficient In Memory Computing

Part 3 - Magnetic Tunnel Junction

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## Lecture Outline

- 1 Device Structure and Working Principle of MTJ
- 2 MTJ Modeling
- **3** Analytical Compact Model for nanoscaled perpendicular MTJs
- 4 MTJ within Circuit Design Flow
- **6** Summary

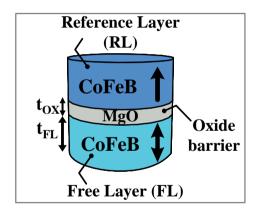


- ① Device Structure and Working Principle of MTJ
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## Basic Device Structure of MTJ

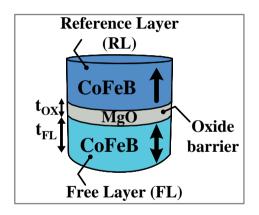
- Composed of at least two ferromagnetic layers: RL and FL
- FM layers commonly built with a CoFeB material
- Barrier usually constructed with MgO
- Resistance states can be high or low based on the magnetization orientation





## Basic Device Structure of MTJ

- The resistance states can be high (antiparallel orientation) or low (parallel orientation), based on the relative orientation of magnetization of the RL and FL.
  - $R_P$  or  $R_L$
  - $R_{AP}$  or  $R_H$
- The MTJ structure fulfills the three basic memory requirements
  - Read
  - Write
  - Data storage





## Magnetoresistive Effect for Reading

- Three different types of MR effects have been studied:
  - Anisotropic MagnetoResistance (AMR)
  - Q Giant MagnetoResistance (GMR)
  - **3** Tunnel MagnetoResistance (TMR)
- MTJ exploits the tunnel magneto resistance (TMR) phenomenon

$$TMR = \left(\frac{R_{AP} - R_P}{R_P}\right) \cdot 100\%$$

 TMR exhibits the highest MR due to the presence of MgO crystal as an insulator

## Magnetoresistive (MR) effect

A change in electrical resistance is caused by a change in the applied magnetic field

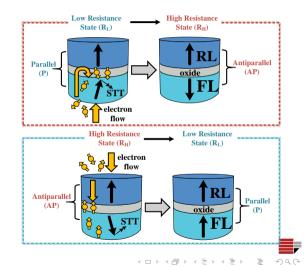
- The higher the TMR, the better. However, it depends on the application
  - Stand-alone memories demand TMR values as high as 300%
  - Embedded memory applications require TMR of around 200%





## Spin-Transfer Torque for Writing

- The write operation of MTJ devices is based on the STT phenomenon
- Two resistance states are possible due to the presence of the oxide barrier
- Switching transitions are performed by injecting a current greater than the critical switching current of the MTJ
- The direction of the injected current causes the device switching
- Remember: when electrons are not polarized by RL, higher currents are needed.



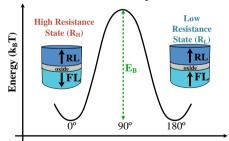
## MTJ Resistance State and Energy Barrier – Data Retention

- The MTJ readout and data storage are related to the resistance of the MTJ device
- MTJ must be stable enough to maintain is data (i.e., the magnetization state)
- The energy barrier (E<sub>b</sub>) prevents switching between the two possible states
  - It follows the thermal stability factor expression:  $\Delta = \frac{E_b}{k_b T}$

 $k_b$ : Boltzmann constant

T: Operating temperature K

- Δ indicates the difficulty of switching between the two stable magnetization states at a given temperature
- $\Delta >$  45 is required to assure a data retention time of 10 years

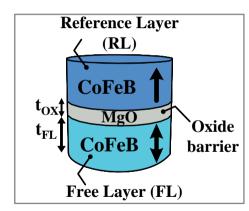


Free layer magnetization polar angle (degrees)



# Ferromagnetic Material: In-Plane Magnetic Anisotropy and Perpendicular Magnetic Anisotropy

- The E<sub>b</sub> of the MTJ is related to: type of magnetic anisotropy energy of FM material that provides nonvolatile data retention.
- Two types of magnetic anisotropy energy
  - in-plane magnetic anisotropy (IMA)
  - perpendicular MA (PMA)
- PMA is used to achieve high integration density and a "low" switching critical current
- PMA occurs at the interface between the MgO and CoFeB layers





## MTJ Issues

- Write Operation
  - The switching (STT) of the MTJ is an stochastic process
  - Thermal fluctuations can cause changes in the magnetic moment of the material, affecting the switching process
  - Write failure: the FL switching depends on the applied pulse and its duration
- 2 Read Operation
  - Read failures: The TMR is not high enough to differentiate between  $R_{AP}$  and  $R_{P}$  orientations.

$$TMR = \left(\frac{R_{AP} - R_P}{R_P}\right) \cdot 100\%$$

- Read disturbance: an unwanted switching may occur during the read operation.
- Retention Retention
  - The magnetization of the FL can switch even without an injected current due to the influence of the thermal field.

$$\Delta = \frac{E_b}{k_b 7}$$



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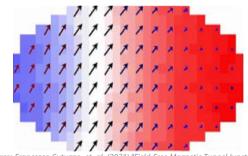


## Micromagnetic Modeling

#### **Micromagnetic Modeling**

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- A more detailed method of simulating magnetization dynamics that takes into account the microscopic details of the magnetic material
- Requires a larger number of cells to represent the magnetization **distribution** in the material
- Can capture more complex phenomena, such as domain wall motion, magnetic noise, and thermal effects
  - Uses non-linear partial differential equations



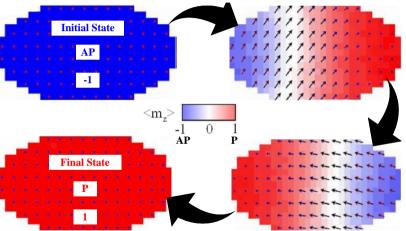
Source: Francesco Cutugno, et. al. (2021) "Field-Free Magnetic Tunnel lunction for Logic Operations Based on Voltage-Controlled Magnetic Anisotropy", IEEE





## Micromagnetic Modeling

• Magnetization snapshots for different times

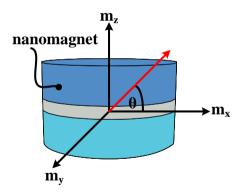


Source: Francesco Cutugno, et. al. (2021) "Field-Free Magnetic Tunnel Junction for Logic Operations Based on Voltage-Controlled Magnetic Anisotropy". IEEE MAGNETICS LETTERS.

## Modeling Approaches: Macrospin and Micromagnetism

#### **Macrospin Modeling**

- A simplified method of simulating magnetization dynamics in magnetic materials
- Represents magnetization by a single macrospin
- Provides a **fast and efficient** way of simulating the effects of spin transfer torque on the magnetization dynamics of the magnetic layers in STT-MTIs
- Can analyze the critical current required to induce magnetization switching and the spin transfer torque generated during the switching





## Macrospin vs. Micromagnetic Modeling: Advantages and Limitations

## **Macrospin Modeling**

- Advantages:
  - Fast and efficient, useful for designing and optimizing STT-MTJ-based devices
- Limmitations:
  - May not capture some of the detailed behavior of the material

#### **Micromagnetic Modeling**

- Advantages:
  - More accurate, can capture complex behavior of the material
- Limmitations:
  - Computationally expensive, may require more time and resources

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**Macrospin modeling** is more simplified and provides a **good approximation** that can guide the design and optimization of STT-MTJ-based devices

Choosing the appropriate modeling approach depends on the specific research question, the available resources, and the desired level of accuracy

## Macrospin Model: Techniques

- There are several techniques for Classical Macrospin modeling:
  - Numerical simulations using the Landau-Lifshitz-Gilbert (LLG) equation
  - Analytical methods: analytical Macrospin model
  - Semi-analytical methods such as the Modified Landau-Lifshitz-Bloch (MLLB) equation

- Analytical Macrospin Modeling
  - Fast runtime ©
  - Easy to calibrate with experimental data ©
  - Not so accurate in the sub-nanosecond range ©

From here we will briefly describe an analytical compact developed in collaboration between different research groups in Italy





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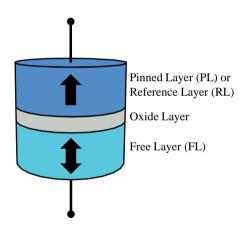
## Analytical Macrospin Compact Model

- The model was developed and published in IEEE Transactions Journal
  - De Rose, R., et al. "A compact model with spin-polarization asymmetry for nanoscaled perpendicular MTJs." IEEE Transactions on Electron Devices 64.10 (2017): 4346-4353.
- Additional resources:
  - SpinLib, Beihang University
  - NanoHub, Purdue University
  - SPICE-compatible compact model: Panagopoulos, Georgios D., Charles Augustine, and Kaushik Roy. "Physics-based SPICE-compatible compact model for simulating hybrid MTJ/CMOS circuits." IEEE Transactions on Electron Devices 60.9 (2013): 2808-2814.



## Compact Model Overview

- Effects considered in the compact model:
  - Resistance and Bias Dependent TMR
  - Critical Switching Currents and Thermal Stability
  - Statistical Switching Model
  - Voltage Dependent PMA
  - Temperature Dependence and Joule Heating
  - $t_{OX}$  and  $t_{FL}$  Variations

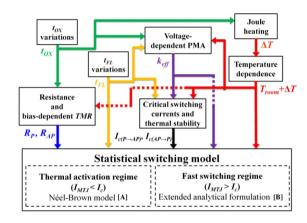






## Compact Model Overview

- In contrast to the model published by De Rose, et al. The effect of temperature has been modified.
   Temperature-dependent equations are mainly based on the following works:
  - Kou, X., et al. Applied Physics Letters. 2006
  - Zhang, Y., et al. IEEE TED. 2015



Source: De Rose, R., et al. IEEE TED. 2017

[A] Zhang, Yue, et al. IEEE TMAG. 2013 [B] Siracusano, G., et al. arXiv preprint. 2017



## Preliminaries (Variables)

#### Temperature-dependence & resistance and TMR variables

- Temperature-dependent variables:
  - T<sub>eff</sub> [ K ]: effective temperature of the FL
  - $M_S$  [A/m]: saturation magnetization
  - $k_i$  [J/m<sup>2</sup>]: interfacial PMA constant
  - ξ [ J/( V m)]: magnetoelectric coefficient
  - *P* []: spin polarization
- Parameters for temperature dependence:
  - $T^*$  [K]: fitting parameter
  - M<sub>S0</sub> [A/m]: sat. mag. at 0 K
  - $k_{i0}$  [J/ m<sup>2</sup>]: interfacial PMA constant at 0 K
  - $\xi_0$  [J/(V m)]: VCMA coef. at 0 K
  - $P_0$  []: spin polarization at 0 K

- Variables for resistance and TMR model
  - $G_0$  [S]: fitting variable for conductance
  - $\lambda_G$  []: variable to compute conductance prefactor for direct elastic tunneling
  - $G_T$  [S]: conductance prefactor for direct elastic tunneling
  - *G<sub>si</sub>* [S]: inelastic spin-independent conductance
  - $R_P$  [ $\Omega$ ]: resistance in P state
  - $R_{AP}$  [ $\Omega$ ]: resistance in AP state
  - $\mathit{TMR}_{\mathsf{T},0}$  []: temperature-dependent TMR at zero voltage bias
  - TMR<sub>T,V</sub> []: temperature-dependent TMR with voltage bias effect

#### Resistance and TMR Model

- Parameters:
  - $\Phi_B = 0.4$  [eV]: energy barrier height for MgO
  - $V_h = 0.5$  [ V ]: voltage bias when the TMR is  $1/2 \cdot TMR_{T,0}$ . (experimental value for MgO)
  - $S = \times 10^{-12}$  []: spin independent conductance factor for oxide barrier
  - F []: fitting factor for RA product and hence MTJ resistance
- Initial calculations for resistance and TMR model

$$G_0 = 3.16 \times 10^{10} \cdot \sqrt{\Phi_B} \cdot \exp(-1.025 \cdot t_{OX} \cdot 1 \times 10^{10} \cdot \sqrt{\Phi_B}) \cdot \text{Area} \cdot 10^4 \cdot \text{F}/(t_{OX} \cdot 10^{10})$$

$$\lambda_{G} = 1.387 \cdot 10^{-4} \cdot t_{OX} \cdot 10^{10} / \sqrt{\Phi_{B}}$$



## Resistance and TMR Model (Cont.)

$$P = P_0 \cdot (1 - (2 \times 10^{-5} \cdot T_{eff}^{1.5}))$$

$$G_T = G_0 \cdot \lambda_G \cdot T_{\it eff} / \sin(\lambda_G \cdot T_{\it eff})$$

$$G_{si} = S \cdot T_{eff}^{1.33}$$

 Now we can define the MTJ resistance and TMR:

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$$R_P = 1/(G_T \cdot (1 + P \cdot P) + G_{si})$$

$$TMR_{T,0} = (2 \cdot P \cdot P)/((1 - P \cdot P) + (G_{si}/G_T))$$

$$TMR_{T,V} = TMR_{T,0}/(1 + (V_b \cdot V_b)/(V_h \cdot V_h))$$

$$R_{AP} = R_P \cdot (1 + TMR_{T,V})$$



## Preliminaries (Variables)

#### Switching model

- Variables for switching model:
  - k<sub>eff</sub> []: normalized effective PMA constant with temperature dependence
  - N<sub>z</sub> []: normalized demagnetizing factor along z-axis
  - N<sub>perp</sub> []: normalized demagnetizing factor along x- and y-axis
  - $\beta_N$  []: variable to compute normalized demagnetizing factors
  - $c_P$  []: variable to model the asymmetry of the spin-torque ( =  $P^2$ )
  - $\beta_P$  []: normalized critical current for  $P \rightarrow AP$  switching
  - haz []: normalized external field

- $\beta_{AP}$  []: normalized critical current for  $AP \rightarrow P$  switching
- $I_{cP}$  [ A ]: critical current for  $P \rightarrow AP$  switching
- $I_{cAP}$  [ A ]:critical current for  $AP \rightarrow P$  switching
- $\Delta$  []: thermal stability factor
- $\theta$  [rad]: initial tilting angle of the FL magnetization with respect to z-axis
- $m_{z0}$  []: initial state of the FL magnetization
- $\tau_{sw}$  []: normalized switching time
- *t<sub>write</sub>* [s]: switching time





## Critical Switching Current Model (Cont.)

$$c_P = P \cdot P$$

$$M_S = M_{S0} \cdot (1 - (T_{eff}/T^*)^{1.5})$$
 $k_i = k_{i0} \cdot (M_S/M_{S0})^{2.18}$ 
 $\xi = \xi_0 \cdot (M_S/M_{S0})^{2.83}$ 
 $\beta_N = 2r/t_{fl}$ 

$$N_z = (\beta_N \cdot \beta_N / (\beta_N \cdot \beta_N - 1)) \cdot \left(1 - \frac{\arcsin((\beta_N \cdot \beta_N - 1)^{0.5} / \beta_N)}{(\beta_N \cdot \beta_N - 1)^{0.5}}\right)$$

$$N_{perp} = (1 - N_z)/2$$



## Critical Switching Current Model (Cont.)

#### Voltage-dependent interfacial PMA

- Voltage-dependent PMA model (normalized effective PMA constant):
  - without voltage-dependent PMA

$$k_{\it eff} = (2 \cdot k_{\it i}/(\mu_0 \cdot M_{\it S} \cdot M_{\it S} \cdot t_{\it fl})) - (N_z - N_{\it perp})$$

with voltage-dependent PMA

$$\textit{k}_{\textit{eff}} = (2 \cdot \textit{k}_{\textit{i}} / (\mu_{0} \cdot \textit{M}_{\textit{S}} \cdot \textit{M}_{\textit{S}} \cdot \textit{t}_{\textit{ff}})) - (\textit{N}_{\textit{z}} - \textit{N}_{\textit{perp}}) - (2 \cdot \xi \cdot \textit{V}_{\textit{b}} / (\mu_{0} \cdot \textit{M}_{\textit{S}} \cdot \textit{M}_{\textit{S}} \cdot \textit{t}_{\textit{GX}} \cdot \textit{t}_{\textit{ff}}))$$

Thermal stability factor

$$\Delta = \frac{\mu_0 \cdot M_S \cdot M_S \cdot t_{fl} \cdot Area \cdot k_{eff}}{2 \cdot k_b \cdot T_{eff}}$$



## Critical Switching Current Model (Cont.)

#### Critical switching currents

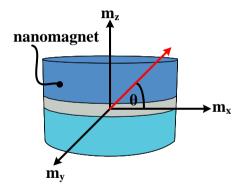
Critical switching currents follows:

$$eta_{P} = lpha \cdot (1 + c_{P}) \cdot (k_{eff} + haz)$$
 $eta_{AP} = lpha \cdot (1 - c_{P}) \cdot (k_{eff} + haz)$ 
 $I_{cP} = eta_{P} \cdot e \cdot \gamma \cdot \mu_{0} \cdot M_{S} \cdot M_{S} \cdot t_{fl} \cdot Area/(\mu_{b} \cdot 2 \cdot P \cdot g)$ 
 $I_{cAP} = eta_{AP} \cdot e \cdot \gamma \cdot \mu_{0} \cdot M_{S} \cdot M_{S} \cdot t_{fl} \cdot Area/(\mu_{b} \cdot 2 \cdot P \cdot g)$ 

- $\gamma$  [Hz/T]: gyromagnetic constant
- $\alpha$  []: Gilbert damping coefficient
- *g* []: Lande factor



- The switching time of the MTJ under the condition of MTJ current ( $I_{MTJ}$ ) greater than the critical switching current of the MTJ ( $I_c$ )
- Two possible switching transitions
  - P → AP (This switching time expression will be discussed hereafter)
  - $AP \rightarrow P$
  - The initial magnetization state  $(m_{z0})$  depends on the direction of the FL magnetization orientation relative to the reference layer





• Variables for the calculation of the switching time ( $P \rightarrow AP$ , P is the initial state)

$$C1 = \sqrt{4 \cdot \epsilon \cdot c_P \cdot k_{eff} - 2 \cdot haz \cdot c_P \cdot k_{eff} + (haz \cdot c_P) \cdot (haz \cdot c_P) + k_{eff} \cdot k_{eff}}$$

$$C2 = arctanh((k_{eff} + 2 \cdot k_{eff} \cdot c_P \cdot m_{z0} + haz \cdot c_P)/C1)$$

$$C3 = arctanh((k_{eff} + 2 \cdot k_{eff} \cdot c_P \cdot m_{zfP} + haz \cdot c_P)/C1)$$

$$C4 = \ln|k_{eff} \cdot m_{zfP} + k_{eff} \cdot m_{zfP} \cdot m_{zfP} \cdot c_P + haz + haz \cdot c_P \cdot m_{zfP} - \epsilon|$$

$$C5 = \ln|(k_{eff} \cdot m_{z0} + k_{eff} \cdot m_{z0} \cdot m_{z0} \cdot c_P + haz + haz \cdot c_P \cdot m_{z0} - \epsilon|$$

- $\epsilon = \beta/\alpha$
- $\beta = I_{MTJ} \cdot 2 \cdot P \cdot g \cdot \mu_b / (e \cdot \gamma \cdot \mu_0 \cdot M_S \cdot M_S \cdot t_{fl} \cdot Area)$
- $m_{zfP} = -0.9$  is the final state of the magnetization for P to AP switching



• Formula for the normalized switching (P to AP) time:

$$\tau_{SW} = -\frac{1}{2 \cdot \alpha} \cdot \frac{\text{Num}}{\text{Den}}$$

$$Num = k_{eff} \cdot C4 \cdot C1 - k_{eff} \cdot C5 \cdot C1 - \ln(1 + m_{zfP}) \cdot C1 \cdot haz + \ln(1 + m_{zfP}) \cdot C1 \cdot \epsilon - \ln|m_{z0} - 1| \cdot C1 \cdot haz$$

$$-2 \cdot C3 \cdot k_{eff} \cdot k_{eff} - 2 \cdot C3 \cdot \epsilon \cdot c_P \cdot c_P \cdot haz - 2 \cdot C3 \cdot haz \cdot c_P \cdot c_P \cdot k_{eff} - 6 \cdot C3 \cdot \epsilon \cdot c_P \cdot k_{eff}$$

$$+2 \cdot C3 \cdot haz \cdot c_P \cdot k_{eff} + 2 \cdot C3 \cdot k_{eff} \cdot k_{eff} \cdot c_P \cdot c_P - \ln(1 + m_{zfP}) \cdot C1 \cdot k_{eff} + 2 \cdot C2 \cdot haz \cdot c_P \cdot c_P \cdot c_P \cdot k_{eff}$$

$$-2 \cdot C2 \cdot haz \cdot c_P \cdot k_{eff} + 6 \cdot C2 \cdot \epsilon \cdot c_P \cdot k_{eff} + 2 \cdot C2 \cdot \epsilon \cdot c_P \cdot c_P \cdot haz + 2 \cdot C2 \cdot k_{eff} \cdot k_{eff}$$

$$-2 \cdot C2 \cdot k_{eff} \cdot k_{eff} \cdot c_P \cdot c_P + \ln(abs(m_{z0} - 1)) \cdot c_P \cdot c_P \cdot C1 \cdot haz - \ln(abs(m_{z0} - 1)) \cdot c_P \cdot c_P \cdot C1 \cdot k_{eff}$$

$$+ \ln(abs(m_{z0} - 1)) \cdot c_P \cdot C1 \cdot \epsilon + \ln(1 + m_{zfP}) \cdot c_P \cdot c_P \cdot C1 \cdot k_{eff} + \ln(1 + m_{zfP}) \cdot c_P \cdot c_P \cdot C1 \cdot haz$$

$$- \ln(1 + m_{zfP}) \cdot c_P \cdot C1 \cdot \epsilon - \ln(1 + m_{z0}) \cdot c_P \cdot c_P \cdot C1 \cdot k_{eff} - \ln(1 + m_{z0}) \cdot c_P \cdot c_P \cdot C1 \cdot haz$$

$$+ \ln(1 + m_{z0}) \cdot c_P \cdot C1 \cdot \epsilon - \ln(abs(m_{zfP} - 1)) \cdot c_P \cdot c_P \cdot C1 \cdot haz + \ln(abs(m_{zfP} - 1)) \cdot c_P \cdot c_P \cdot C1 \cdot k_{eff}$$

$$- \ln(abs(m_{zfP} - 1)) \cdot c_P \cdot C1 \cdot \epsilon + k_{eff} \cdot c_P \cdot c_P \cdot C5 \cdot C1 - c_P \cdot C5 \cdot \epsilon \cdot C1 - k_{eff} \cdot c_P \cdot c_P \cdot C4 \cdot C1$$

$$+ c_P \cdot C4 \cdot \epsilon \cdot C1 + \ln(1 + m_{z0}) \cdot C1 \cdot haz - \ln(1 + m_{z0}) \cdot C1 \cdot \epsilon + \ln(1 + m_{z0}) \cdot C1 \cdot k_{eff}$$

$$+ \ln|m_{zfP} - 1| \cdot C1 \cdot haz - \ln|m_{zfP} - 1| \cdot C1 \cdot k_{eff}$$

$$- \ln(abz(m_{zfP} - 1) \cdot C1 \cdot k_{eff} \cdot c_P \cdot c_P \cdot C5 \cdot C1 - c_P \cdot C5 \cdot \epsilon \cdot C1 - k_{eff} \cdot c_P \cdot c_P \cdot C4 \cdot C1$$

$$+ \ln|m_{zfP} - 1| \cdot C1 \cdot haz - \ln|m_{zfP} - 1| \cdot C1 \cdot k_{eff}$$

$$- \ln(abz(m_{zfP} - 1) \cdot C1 \cdot k_{eff} \cdot c_P \cdot c_P \cdot C4 \cdot \epsilon \cdot C1 + \ln(m_{zfP} - 1) \cdot C1 \cdot k_{eff}$$

$$- \ln(abz(m_{zfP} - 1) \cdot C1 \cdot k_{eff} \cdot c_P \cdot c_P \cdot C5 \cdot C1 - k_{eff} \cdot c_P \cdot C5 \cdot \epsilon \cdot C1 - k_{eff} \cdot c_P \cdot C6 \cdot C1 \cdot k_{eff}$$

$$- \ln(abz(m_{zfP} - 1) \cdot C1 \cdot k_{eff} \cdot c_P \cdot C4 \cdot \epsilon \cdot C1 + \ln(m_{zfP} - 1) \cdot C1 \cdot k_{eff}$$

$$- \ln(abz(m_{zfP} - 1) \cdot C1 \cdot k_{eff} \cdot c_P \cdot C4 \cdot \epsilon \cdot C1 + \ln(m_{zfP} - 1) \cdot C1 \cdot k_{eff}$$

$$- \ln(abz(m_{zfP} - 1) \cdot C1 \cdot k_{eff} \cdot CP \cdot C4 \cdot C1 + \ln(m_{zfP} - 1) \cdot C1 \cdot k_{eff}$$

$$- \ln(abz(m_{zfP} - 1) \cdot C1 \cdot$$



Denormalizing the switching time

$$t_{write} = au_{sw}/(\gamma \cdot \mu_0 \cdot M_S)$$

- ullet Similar expressions (HERE) correspond to the AP o P switching transition
- P → AP
  - FL initial tilting angle:

$$heta = \sqrt{-\ln\left(1 - WER\right)/\Delta}$$

• FL final state of the magnetization:

$$m_{zfP} = -0.9$$

- AP → P
  - FL initial tilting angle:

$$\theta = \pi - \sqrt{-\ln\left(1 - WER\right)/\Delta}$$

• FL final state of the magnetization:

$$m_{zfAP} = +0.9$$

◆ Go to WER



## MTJ Read and Write errors

- During the MTJ write and read operations, the write and read currents strongly affect the write and read error rates, respectively.
  - Write errors: when the device is unable to write new data onto the MTJ
  - Read errors: when the device is unable to read the stored data of the MTJ
- To ensure error rates close to zero:
  - Write current has to be high enough
  - Read current has to be low enough
- Typically, error rates span from  $10^{-6}$  to  $10^{-11}$



#### Write-Error-Rate (WER)

It is defined as the probability of No-switching during a write event

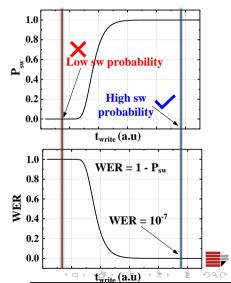
- Write failures can occur when the amplitude and/or duration of the write pulse used to switch the orientation of the free layer magnetization is insufficient.
- The  $I_{write}$  has to be high enough to ensure a low WER.
- MTJ switching is stochastic → We can obtain the Cumulative Distribution Function (CDF) of the switching time
  - CDF provides a complete picture of the distribution of the switching time by showing the probability of all possible values of the switching time.
  - useful in statistical analysis and modeling of MTJ devices



- MTJ switching is stochastic
  - For a given  $I_{write}$  and a write pulse ( $t_{write}$ ), we have a probability of switching ( $P_{sw}$ )
- The WER can be expressed as

$$WER = 1 - P_{sw}$$

 Note: the P<sub>sw</sub> is the Cumulative Distribution Function (CDF)



- Recalling the FL initial tilting angle ( $\theta$ ) in regard to the STT switching, we can obtain the write time ( $t_{write}$ ) required to achieve a WER. Go to initial tilting angle
- How? the  $\theta$  is calculated as follows
  - 1. From the probability distribution function (PDF) of the switching time ( $au_{sw}$ ), we get the CDF

$$\begin{split} PDF(\tau_{sw,P\to AP}) = & 2\Delta exp\left(-\Delta arccos^2\left(g^{-1}(\tau_{sw,P\to AP})\right)\right) \\ & \cdot |\alpha\left(k_{eff}g^{-1}(\tau_{sw,P\to AP}) - \beta/\alpha\left(1 + c_Pg^{-1}(\tau_{sw,P\to AP})\right)^{-1}\right) \cdot \\ & \left(1 - \left(g^{-1}(\tau_{sw,P\to AP})\right)^{-1}\right)| \end{split}$$

 Note: Several probability distributions have been proposed for the fast switching regime. The one mentioned in this lecture fits well for our model.



- Recalling the FL initial tilting angle ( $\theta$ ) in regard to the STT switching, we can obtain the write time ( $t_{write}$ ) required to achieve a WER. Go to initial tilting angle
- How?... the  $\theta$  is calculated as follows
  - 1. From the probability distribution function (PDF) of the switching time ( $\tau_{sw}$ ), we get the CDF

$$\begin{split} PDF(\tau_{\mathit{SW},P\to\mathit{AP}}) = & 2\Delta exp\left(-\Delta arccos^2\left(g^{-1}(\tau_{\mathit{SW},P\to\mathit{AP}})\right)\right) \\ & \cdot |\alpha\left(k_{\mathit{eff}}g^{-1}(\tau_{\mathit{SW},P\to\mathit{AP}}) - \beta/\alpha\left(1 + c_{\mathit{P}}g^{-1}(\tau_{\mathit{SW},P\to\mathit{AP}})\right)^{-1}\right) \cdot \\ & \left(1 - \left(g^{-1}(\tau_{\mathit{SW},P\to\mathit{AP}})\right)^{-1}\right)| \\ & CDF(\tau_{\mathit{SW},P\to\mathit{AP}}) = exp\left(-\Delta arccos^2\left(g^{-1}(\tau_{\mathit{SW},P\to\mathit{AP}})\right)\right) \end{split}$$



### Write-Error-Rate (WER)

- Recalling the FL initial tilting angle ( $\theta$ ) in regard to the STT switching, we can obtain the write time ( $t_{write}$ ) required to achieve a WER. Go to initial tilting angle
- How?... the  $\theta$  is calculated as follows.
  - 2. CDF and switching time

$$CDF( au_{sw,P o AP}) = exp\left(-\Delta arccos^2\left(g^{-1}( au_{sw,P o AP})
ight)
ight) \ au_{sw,P o AP} = g(m_{z0}) o g^{-1}( au_{sw,P o AP}) = m_{z0} \ au_{sw,P o AP} = arccos(g^{-1}( au_{sw,P o AP})) = arccos(m_{z0})$$





### Write-Error-Rate (WER)

- Recalling the FL initial tilting angle ( $\theta$ ) in regard to the STT switching, we can obtain the write time ( $t_{write}$ ) required to achieve a WER. Go to initial tilting angle
- How?... the  $\theta$  is calculated as follows
  - 3. Rewriting the CDF in terms of  $\theta$  Remember:  $m_{z0} = cos(\theta)$

$$\theta = arccos(m_{z0}) = arccos(g^{-1}( au_{sw,P 
ightarrow AP}))$$

$$\therefore CDF(\tau_{sw,P \to AP})) = exp(-\Delta \theta^2)$$





## Write-Error-Rate (WER)

- Recalling the FL initial tilting angle ( $\theta$ ) in regard to the STT switching, we can obtain the write time ( $t_{write}$ ) required to achieve a WER. Go to initial tilting angle
- How?... the  $\theta$  is calculated as follows
  - 4. FL tilting angle,  $\theta$ , as a function of the WER

$$WER( au_{sw,P o AP})) = 1 - CDF( au_{sw,P o AP})) = 1 - exp(-\Delta heta^2)$$
  $heta(WER) = \sqrt{-\ln(1 - WER)/\Delta}$ 





## Read Disturbance Rate (RDR)

### Read Disturbance Rate (RDR)

It is defined as the probability to disturb or flip (i.e., unwanted switching) the stored data during a reading event

- Read failures can occur when the read current (I<sub>read</sub>) is close to the critical switching current of the MTJ device.
- The I<sub>read</sub> has to be low enough to avoid unwanted switching of the FL magnetization, and ensure a low RDR
- RDR is defined as:

$$RDR = 1 - exp \left\{ -rac{t_{read}}{ au_0} exp \left( -\Delta \left( 1 - rac{I_{read}}{I_{c0}} 
ight) 
ight) 
ight\}$$





### Read Disturbance Rate (RDR)

$$RDR = 1 - exp\left\{-\frac{t_{read}}{\tau_0}exp\left(-\Delta\left(1 - \frac{I_{read}}{I_{c0}}\right)\right)\right\}$$
(1)

- $t_{read}$  [s]: read pulse width
- $\tau_0$  [s]: attempt period (typically around 1 ns)
- $I_{c0}$  [ A ]: refers to that associated with the  $P \to AP$  (or  $AP \to P$ ) transition
- Note:
  - Lower the  $t_{read}$ , lower the RDR
  - Lower the  $I_{read}/I_{c0}$ , lower the RDR
  - Higher the  $\Delta$ , lower the *RDR*
- Generally, we need to set the  $l_{read}$ . From (1), we can estimate the  $l_{read}/l_{c0}$  for a target RDR and given  $\Delta$ ,  $t_{read}$

$$\frac{I_{read}}{I_{c0}} = 1 + \frac{\ln\left[-(\tau_0/t_{read}) \cdot \ln(1 - RDR)\right]}{\Delta}$$



## Retention Failure Rate (RFR)

Temperature Effect on the Retention Capability

#### Retention Failure Rate (RFR)

It is defined as the probability of an unwanted bit flipping due to thermal noise also in absence of injected currents

• The retention failure is obtained from RDR equation when  $I_{read}=0$ 

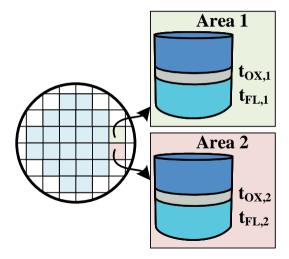
$$RFR = 1 - exp \left\{ rac{t_{retention}}{ au_0 \cdot exp(\Delta)} 
ight\}$$

• RDR depends on the thermal stability, i.e.,  $\Delta$ 



# MTJ process variations

- The analytical compact model takes into account the effect of process variations
  - oxide thickness
  - FL thickness
  - cross-section area
- It is generated n samples for the above variables. These follow a normal distribution with that corresponds to a given standard deviation.
- The variations are taken from state-of-the-art physical experiments

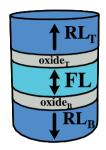




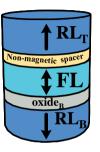
## Summary & Advanced STT-MTJ structures



Single-barrier MTJ (SMTJ)



Double-barrier MTJ (DMTJ)



Double Spin-torque MTJ (DS-MTJ)

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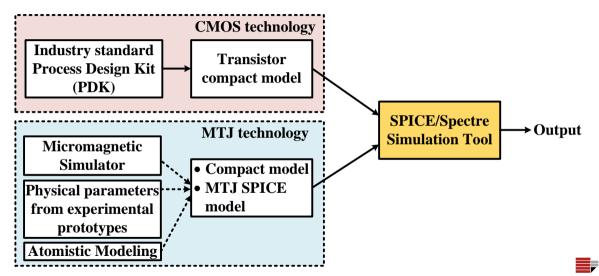
Source: Compact model SMTJ: De Rose, R., et. al., TED,2017 Source: Compact model DMTJ: De Rose, R., et. al., TNANO, 2019 Source: DS-MTI: Hu. G., et. al., IEDM, 2021



- Device Structure and Working Principle of MTJ
- 2 MTJ Modeling
- 3 Analytical Compact Model for nanoscaled perpendicular MTJs
- 4 MTJ within Circuit Design Flow
- Summary

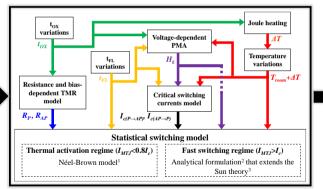


## Overall Circuit Design Flow



## Example Top-Level View of Verilog-A Compact Model

#### Verilog-A Compact model





- MTJ Switching time
- State of the MTJ (parallel or antiparallel)

INPUTS:

Experimental data

Simulation

parameters

- Device Structure and Working Principle of MTJ
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## Summary

- Macrospin model: simulation of magnetization dynamics in magnetic materials that treats the magnetization as a classical vector.
- Macrospin model: good alternative to evaluate MTJ devices and design hybrid CMOS/MTJ circuits
- Different model flavors available in the literature.
- The MTJ devices have write, read, and data retention "issues"/"constraints" that have to been taken into account
- Compact models have to be compatible with circuit design tools
- The presented analytical compact model consider all the necessary effects to make accurate assessments in hybrid CMOS/MTJ circuit design.

