Coefficients

ecog

You have **2 hours** to complete this exam.

1. [38] The following dataset reports lifetimes of lightbulbs since their first use (measured in days).

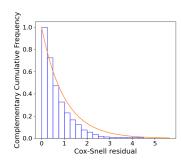
3 33 48 12 54 34 17 35 55 28 39 57 29 48 115

- (a) [8] Calculate an estimate of the survival function.
- (b) [8] Assuming that the data are exponentially distributed, give an estimate of the scale parameter based on the method of moments. Can you justify this assumption?
- (c) [6] Estimate the variance of this estimator and give a 95% confidence interval.
- (d) [6] Test the hypothesis H_0 : the expected lifetime is 6 weeks.
- (e) [4] Give the definition of right-censored data.
- (f) [6] How would you estimate the scale parameter if there were right-censored entries? Justify.
- 2. [40] The survival times of 227 lung cancer patients have been recorded, along with their age (centered on 62), their gender and their ECOG score (it measures the level of disability, a score of 0 corresponds to a fully able person). A Cox proportional hazards model has been fitted to these data.

covariate value female ecog age 0.000086 -0.000182 age 0.01 age 0.000004 female -0.55 female 0.000004 0.028136 -0.000930 0.46 -0.000182 -0.000930 0.012900

Covariance Matrix

- ecog (a) [4] Give the definition of the Cox proportional hazards model.
- (b) [8] Derive a numerical method to estimate the parameters of the model.
- (c) [4] What are the characteristics of the baseline subject?
- (d) [8] Analyse the effect of the covariates and their significance. Give a 95% confidence interval for the coefficients.
- (e) [8] Calculate the hazard ratio between a 50 years old female and a 50 years old male with an identical ECOG score. Give a 95% confidence interval.
- (f) [8] The distribution of the Cox-Snell residuals is given in the figure below. How should you interpret this plot? Demonstrate your statement.



3. [22] 200 steel specimens have been subjected to cycles of a given stress amplitude. For each specimen the stress amplitude and the number of cycles until failure have been recorded in kilopound per square inch (kpsi) and in 1000 cycles respectively. A Weibull accelerated failure time model has been fitted.

| | coef | se | p-value |
|------------------|------------|------|---------|
| Stress Amplitude | 0.416196 | 0.02 | <0.005 |
| Intercept | -20.546640 | 0.85 | <0.005 |
| Gamma | 0.758578 | 0.05 | <0.005 |

- (a) [4] Give the definition of the general accelerated failure time model.
- (b) [4] In general, how can we choose between the Weibull and the log-logistic baseline?
- (c) [6] Calculate the acceleration factor and give a 95% confidence interval.
- (d) [8] Calculate the median failure time for a specimen subjected to a stress amplitude of 35 kpsi.

| | Table 1: Standard normal distribution table | | | | | | | | | |
|-----|---|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | 0 | 0.001 | 0.002 | 0.003 | 0.004 | 0.005 | 0.006 | 0.007 | 0.008 | 0.009 |
| 0 | 0.5000 | 0.5040 | 0.5080 | 0.5120 | 0.5160 | 0.5199 | 0.5239 | 0.5279 | 0.5319 | 0.5359 |
| 0.1 | 0.5398 | 0.5438 | 0.5478 | 0.5517 | 0.5557 | 0.5596 | 0.5636 | 0.5675 | 0.5714 | 0.5753 |
| 0.2 | 0.5793 | 0.5832 | 0.5871 | 0.5910 | 0.5948 | 0.5987 | 0.6026 | 0.6064 | 0.6103 | 0.6141 |
| 0.3 | 0.6179 | 0.6217 | 0.6255 | 0.6293 | 0.6331 | 0.6368 | 0.6406 | 0.6443 | 0.6480 | 0.6517 |
| 0.4 | 0.6554 | 0.6591 | 0.6628 | 0.6664 | 0.6700 | 0.6736 | 0.6772 | 0.6808 | 0.6844 | 0.6879 |
| 0.5 | 0.6915 | 0.6950 | 0.6985 | 0.7019 | 0.7054 | 0.7088 | 0.7123 | 0.7157 | 0.7190 | 0.7224 |
| 0.6 | 0.7257 | 0.7291 | 0.7324 | 0.7357 | 0.7389 | 0.7422 | 0.7454 | 0.7486 | 0.7517 | 0.7549 |
| 0.7 | 0.7580 | 0.7611 | 0.7642 | 0.7673 | 0.7704 | 0.7734 | 0.7764 | 0.7794 | 0.7823 | 0.7852 |
| 0.8 | 0.7881 | 0.7910 | 0.7939 | 0.7967 | 0.7995 | 0.8023 | 0.8051 | 0.8078 | 0.8106 | 0.8133 |
| 0.9 | 0.8159 | 0.8186 | 0.8212 | 0.8238 | 0.8264 | 0.8289 | 0.8315 | 0.8340 | 0.8365 | 0.8389 |
| 1 | 0.8413 | 0.8438 | 0.8461 | 0.8485 | 0.8508 | 0.8531 | 0.8554 | 0.8577 | 0.8599 | 0.8621 |
| 1.1 | 0.8643 | 0.8665 | 0.8686 | 0.8708 | 0.8729 | 0.8749 | 0.8770 | 0.8790 | 0.8810 | 0.8830 |
| 1.2 | 0.8849 | 0.8869 | 0.8888 | 0.8907 | 0.8925 | 0.8944 | 0.8962 | 0.8980 | 0.8997 | 0.9015 |
| 1.3 | 0.9032 | 0.9049 | 0.9066 | 0.9082 | 0.9099 | 0.9115 | 0.9131 | 0.9147 | 0.9162 | 0.9177 |
| 1.4 | 0.9192 | 0.9207 | 0.9222 | 0.9236 | 0.9251 | 0.9265 | 0.9279 | 0.9292 | 0.9306 | 0.9319 |
| 1.5 | 0.9332 | 0.9345 | 0.9357 | 0.9370 | 0.9382 | 0.9394 | 0.9406 | 0.9418 | 0.9429 | 0.9441 |
| 1.6 | 0.9452 | 0.9463 | 0.9474 | 0.9484 | 0.9495 | 0.9505 | 0.9515 | 0.9525 | 0.9535 | 0.9545 |
| 1.7 | 0.9554 | 0.9564 | 0.9573 | 0.9582 | 0.9591 | 0.9599 | 0.9608 | 0.9616 | 0.9625 | 0.9633 |
| 1.8 | 0.9641 | 0.9649 | 0.9656 | 0.9664 | 0.9671 | 0.9678 | 0.9686 | 0.9693 | 0.9699 | 0.9706 |
| 1.9 | 0.9713 | 0.9719 | 0.9726 | 0.9732 | 0.9738 | 0.9744 | 0.9750 | 0.9756 | 0.9761 | 0.9767 |
| 2 | 0.9772 | 0.9778 | 0.9783 | 0.9788 | 0.9793 | 0.9798 | 0.9803 | 0.9808 | 0.9812 | 0.9817 |
| 2.1 | 0.9821 | 0.9826 | 0.9830 | 0.9834 | 0.9838 | 0.9842 | 0.9846 | 0.9850 | 0.9854 | 0.9857 |
| 2.2 | 0.9861 | 0.9864 | 0.9868 | 0.9871 | 0.9875 | 0.9878 | 0.9881 | 0.9884 | 0.9887 | 0.9890 |
| 2.3 | 0.9893 | 0.9896 | 0.9898 | 0.9901 | 0.9904 | 0.9906 | 0.9909 | 0.9911 | 0.9913 | 0.9916 |
| 2.4 | 0.9918 | 0.9920 | 0.9922 | 0.9925 | 0.9927 | 0.9929 | 0.9931 | 0.9932 | 0.9934 | 0.9936 |
| 2.5 | 0.9938 | 0.9940 | 0.9941 | 0.9943 | 0.9945 | 0.9946 | 0.9948 | 0.9949 | 0.9951 | 0.9952 |
| 2.6 | 0.9953 | 0.9955 | 0.9956 | 0.9957 | 0.9959 | 0.9960 | 0.9961 | 0.9962 | 0.9963 | 0.9964 |
| 2.7 | 0.9965 | 0.9966 | 0.9967 | 0.9968 | 0.9969 | 0.9970 | 0.9971 | 0.9972 | 0.9973 | 0.9974 |
| 2.8 | 0.9974 | 0.9975 | 0.9976 | 0.9977 | 0.9977 | 0.9978 | 0.9979 | 0.9979 | 0.9980 | 0.9981 |
| 2.9 | 0.9981 | 0.9982 | 0.9982 | 0.9983 | 0.9984 | 0.9984 | 0.9985 | 0.9985 | 0.9986 | 0.9986 |
| 3 | 0.9987 | 0.9987 | 0.9987 | 0.9988 | 0.9988 | 0.9989 | 0.9989 | 0.9989 | 0.9990 | 0.9990 |

| | Tab | ole 2: C | hi-Squa | re dist | ribution | table | with 1 | degree | of freed | om | |
|---------|--------|----------|---------|---------|----------|-------|--------|--------|----------|-------|--------|
| 0.95 | 0.9 | 0.5 | 0.2 | 0.1 | 0.05 | 0.025 | 0.02 | 0.01 | 0.005 | 0.002 | 0.001 |
| 0.00393 | 0.0158 | 0.455 | 1.642 | 2.706 | 3.841 | 5.024 | 5.412 | 6.635 | 7.879 | 9.550 | 10.828 |