# Nonlinearities and Noise Identification in an Active Suspension System

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# 1.Introduction

## 1.1. Background, Aims & Objectives

Suspensions systems are a crucial element to ensuring a safe and pleasant driving experience, not only improving a passenger's comfort, but also reducing the severity of impact in the unfortunate event of an accident. There are three main types of suspension systems used in vehicles; passive, semi-active and active.

'Contemporary car suspension systems predominantly contain passive control elements, namely springs and dampers, and have evolved to the point at which it seems reasonable to suppose that they will not improve much without changes in principle" (Sharp et al., 1987). This has led to much more research into active suspension, such as Fayyad's study (2012), into constructing a control system for active suspension and the study done by Milanese and Novara (2004) into 'set membership identification of nonlinear systems', and more recently, the study into the application of multi-input uncorrelated periodic signals for identification of active suspension systems (Kioutsoukis et al., 2022).

The aim of this project is to try to identify the nonlinearities in an active suspension system as their presence was proven in the study by Kioutsoukis et al., (2022). If these nonlinearities can be identified, they can be reproduced in simulated environments, which can advance the development of active suspension systems in the future. One practical application of this data would be developing a nonlinear compensator with appropriate noise filtering techniques, this could then be integrated into a suspension system and would be able to further improve the performance of that suspension system.

The project's primary method for identification will be using the Hammerstein-Weiner model to attempt to identify these nonlinearities from the experimental data collected in Kioutsoukis et al., (2022). A Hammerstein-Wiener model 'consists of three subsystems, where a linear block is embedded between two nonlinear subsystems' (Hammar et al., 2019). This model is a particular kind of nonlinear system 'where the nonlinear block is static and follows or is followed by a linear system' (Bai 2002). The model in question will be a block-oriented model and there are several advantages to this: '(1) low cost in identification tests; (2) low cost in identification computation; (3) it is easy to comprehend and to incorporate a priori process knowledge and (4) they are easy to use in control' (Zhu 2002).

The initial hypothesis for this study is that the experimental data comprises of a linear component, a nonlinear component and some noise component. It is my aim to identify and isolate this nonlinear component.

## 1.2 Risk Management

Due to the nature and the time-constraint placed upon the project, the main risk to the project's level of success is finding an appropriate model for the nonlinearities. With this in mind, all results and findings, positive or negative will be recorded in this report so that this project may continue in future, with the added benefit of having the additional research covered in this report.

The other major risk in this report is that to personal health and well-being - due to long periods of time sat down at a desk, testing models in software on a laptop. The best way to mitigate this is to ensure frequent breaks and exercise.

## 1.3 Remaining Structure of the Paper

The remainder of the paper will follow the following structure: Chapter 2 discusses the background of the project, going into detail on different suspension types, vehicle models, the Hammerstein-Weiner model and noise filters. Chapter 3 discusses how the experimental data was gathered from the previous study that this project is based upon, and Chapter 4 discusses how the tools available in MATLAB are utilised in this project. Chapter 5 gives more detail into optimising a noise filter and Chapter 6 contains the results from all the nonlinear models used in this project. Chapter 7 offers a conclusion and suggestions for future works, followed by the references given in full in Chapter 8 which have been cited throughout the paper using the Harvard convention. Appendices are given in Chapter 9.

# 2. Background & Literature Review

## 2.1. Suspension Types

A suspension system in a passenger vehicle is crucial to improving ride comfort and passenger experience (Jiregna et al., 2020). Suspension systems can typically be broken down into three categories: passive, semi-active and active suspension. A passive suspension system will consist of a spring and a damper, and 'cannot satisfy the comfort requirements when subjected to different road profiles' unlike a semi-active or active suspension system may be able to (Kumar et al., 2020), this is because the characteristics of the springs and dampers are fixed (Ahmadian, 2001). These characteristics would be set by the designer, usually with a specific use in mind. A typical passive suspension system is shown in figure 1.

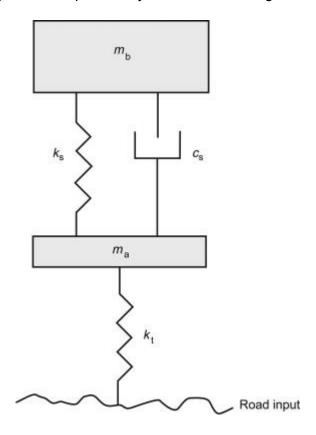


Figure 1: Passive Suspension System (Ahmadian, 2001)

In figure 1,  $m_b$  represents the mass of the vehicle body (sprung mass) and  $m_a$  represents the tyre-axle assembly (unsprung mass),  $k_s$  is the suspension spring and the damper is  $c_s$  which is positioned between the vehicle body and axle. The stiffness of the tyre is represented by  $k_t$  (Ahmadian, 2001).

Semi-active suspension consists of a spring and damper much like a passive system, however the difference is semi-active suspension has "elastic parameter stiffness and shock absorber damping [that] can adjust according to the need for adjustment and control" (Jibril et al., 2020).

A semi-active system only needs a low power controller which is cheaper than a fully active system however semi-active system does lack other 'important secondary advantages' when compared to a fully active system (Giua et al., 2004).

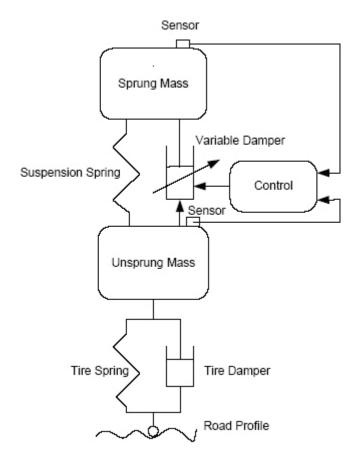


Figure 2: Semi-active Suspension System (Khajavi et al., 2007)

As shown in figure 2, a semi-active system contains an additional controller and a sensor, compared with a passive system, allowing for the damper coefficient to be adjusted. In this example only the damper is adjustable.

An active suspension system improves ride comfort, stability and handling of a passenger vehicle to a greater extent than semi-active or passive can. Active suspension systems can be adjusted to the designer's desires of performance (El-Beheiry, 2000), as well as being more elastic and efficient than a semi-active or passive system (Lin et al., 2011). These suspension systems do however have a higher production cost (Yoshimura et al., 2001).

Active suspension systems make use of control algorithms to improve ride comfort 'such that the effect of the rough road surfaces will be minimally felt by the passengers' (Kioutsoukis et al., 2022). 'Active suspension systems dynamically respond to changes in the road profile because of their ability to supply energy that can be used to produce relative motion between the body and wheel' (Sam et al., 2004). These suspension systems usually 'include sensors

to measure suspension variables such as body velocity, suspension displacement, wheel velocity and wheel or body acceleration' (Sam et al., 2004). A diagram for an active suspension system is shown in figure 3.

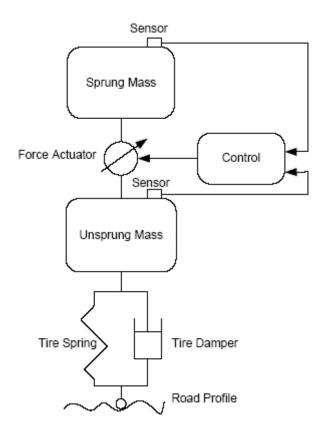


Figure 3: Active Suspension System (Khajavi et al., 2007)

One drawback to an active suspension system is that if it is subject to a surface that excites certain frequencies, these frequencies can resonate and cause discomfort (Majjad, 1997). The challenge lies within identifying these resonant frequencies in order to counter them, therefore reducing the effects of the excited frequencies. Currently, this has only been proven possible with a 'noise-free linear system', since 'one can easily obtain the transfer function and compute the [frequency response function] in a straightforward manner' (Kioutsoukis et al., 2022). However, in practice, a system in the real world will never be noise-free so this does not provide a practical solution for everyday use, which is where the main challenge for this project arises – attempting to identify these noise and nonlinearities effects.

#### 2.2. Vehicle Modelling Types

There are three main modelling approaches when it comes to suspension systems full-car model, half-car and quarter-car model. A 'full vehicle model consists of the car body (spring mass) connected by the suspension system to four wheels (unsprung masses)' (Chamseddine et al., 2007). As demonstrated in figure 4, each 'active suspension system is modelled as a

linear viscous damper, a linear spring and a force actuator', with each wheel being modelled as a linear spring.

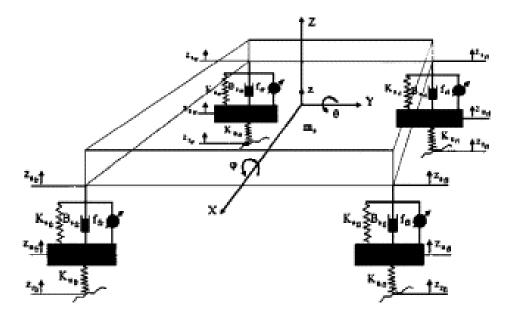


Figure 4: Full-car model (Chamseddine et al., 2007)

In this full-car model the car body is free to heave, pitch and roll and the wheels are free to bounce vertically with respect to the car body (Chamseddine et al., 2007). A full-car model has 7 degrees of freedom.

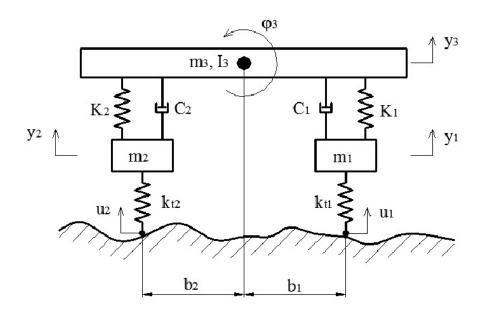


Figure 5: Half-car model (Goga et al., 2012)

A half-car model (shown in figure 5) only has 4 degrees of freedom and uses half of a full model for simplicity. However, seeing as we only are interested in analysing the vertical acceleration of the system a quarter-car model is more appropriate. By using a quarter-car

model we are reducing the complexity as much as possible, a 'quarter vehicle model is the simplest representation of a vehicle in dynamic analysis' (Soong et al., 2017). This was also the conclusion in a recent study by Desai et al. (2021), 'for a bump road profile, the quarter car model, which is considerably simpler, maybe preferred if computing time or complexity is a constraint'. Quarter-car models are typically used for suspension analysis due to their simplicity whilst filtering out unnecessary features of the full-car model such as pitch and roll, and still retaining the useful information regarding the vertical accelerations of the tyre and body, as shown in figure 6.

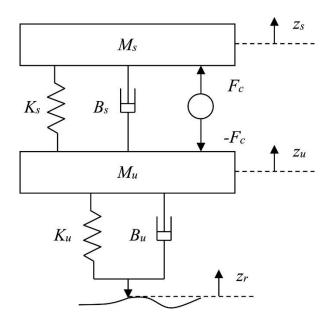


Figure 6: Quarter-car model (Tan et al., 2022)

#### 2.3. Hammerstein-Weiner Model

A Hammerstein-Wiener model (sometimes referred to as N-L-N model) is going to be used to try and identify nonlinearities within the experimental data. Hammerstein-Weiner models are 'known as a particular class of block-oriented nonlinear models where a Linear (L) subsystem is embedded in two static Nonlinear subsystems (N)' (Sun et al., 2022). The Hammerstein model was first discussed in Narendra et al. (1966) and the Wiener model was first developed in a study relating to an interest in 'a nonlinear system using Volterra expansions' (Wills et al., 2013).

The N-L-N model works by attempting to model the data through the nlhw function in MATLAB, this can also be achieved using the MATLAB System Identification (SysID) Toolbox. The model takes an input u(t) and passes it through the input nonlinearity function block which then is passed to a linear block before being passed through the output nonlinearity block to give an output y(t) as depicted in figure 7.

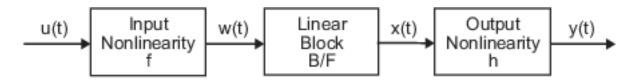


Figure 7: Hammerstein-Weiner model (Mathworks Inc., 2023)

The Hammerstein-Weiner model was chosen as a starting point over other modelling techniques such a Nonlinear ARX model or sparse identification of nonlinear dynamics (SINDy) as, within MATLAB, there are many modelling options for nonlinearity block choice in the MATLAB SysID toolbox. Another reason for choosing Hammerstein-Weiner model is that it uses 'two nonlinear elements instead of one', meaning that the model 'offers convenient higher modelling capabilities for nonlinear systems' (Sun et al., 2022).

The Hammerstein-Weiner model has been successful in identifying nonlinearities in previous studies, for example the study by Sasai et al. (2020) into optical transmitters, which made use of the Hammerstein-Weiner model for nonlinear identification. This model has not yet been applied to an active suspension system and the MATLAB SysID toolbox is specifically designed towards estimating nonlinear system dynamics through various options of modelling techniques, suggesting that the N-L-N model may prove useful in identifying nonlinearities in the experimental data.

#### 2.4. Noise

There is also noise present in the experimental data that will need to be filtered out, several approaches could be taken to tackle this problem. The first approach is to use a moving average filter and see if that reduces the noise present in the data. A moving average filter is one of the most popular and widely used techniques owing to its simple digital realization, low computational burden, and overall effectiveness (Golestan et al., 2014).

A moving average filter works excellently with time-domain encoded signals however, it struggles with frequency domain encoded signals, the experimental data is time-domain encoded so this works well for what the filter needs to achieve (Analog.com, n.d). If this approach does not yield any positive results, there are also other filters that could be used instead such as the Gaussian filter (Cahill et al., 1993) or the multiple-pass moving average filter (Solis et al., 2007).

# 3. Experimental Data

#### 3.1. Quanser Laboratory-scale Suspension System

The experimental data used in this project was collected using the active suspension system described in Kioutsoukis et al., 2022 (figure 8), which is a laboratory-scale system developed by Quanser (which is based on the quarter-car model). The 'platform can also be used to teach

mass-spring-damper modelling and control at a fundamental level, as well as applications of IMU measurement and processing' (Quanser, 2023). The dimensions of the suspension system are 30.5cm in length, 30.5cm in width and 61cm in height with a total weight of 15kg (Kioutsoukis et al., 2022). The scaled down system uses three masses to represent the road (silver plate), vehicle tyre (red plate) and body (blue plate). These masses move along stainless steel shafts using linear bearings. 'The upper mass is connected to a high-quality DC motor through a capstan to emulate an active suspension system' (Quanser, 2023), 'the lower plate is driven by a powerful DC motor connected to a lead screw and cable transmission system'. The system features adjustable weight and spring stiffness as well as an accelerometer mounted to the top plate to measure vehicle body acceleration.



Figure 8: Laboratory-scale active suspension system developed by Quanser (Quanser, 2023)

The system is then fed multisine signals that are 'uncorrelated and orthogonal with one another' (Kioutsoukis et al., 2022). A multisine signal is defined by

$$u(n) = \sum A_p \cos \omega_p n + \emptyset_p$$

'where n denotes the discrete time index,  $\gamma$  represents the set consisting of nonzero harmonics (excluding zero harmonics),  $A_p$  is the amplitude,  $\omega_p = \frac{2\pi p}{N}$  is the normalised angular frequency with period N and  $\phi_p$  is the phase associated with harmonic p' (Kioutsoukis et al., 2022).

#### 3.2 System Equations

The system of differential for a quarter car suspension model is as follows (x-engineer.org, n.d.):

$$m_1 \ddot{z}_1 = k_1 (z_2 - z_1) + c_1 (\dot{z}_2 - \dot{z}_1)$$

$$m_2 \ddot{z}_2 = k_2 (u - z_2) + c_2 (\dot{u} - \dot{z}_2) - k_1 (z_2 - z_1) - c_1 (\dot{z}_2 - \dot{z}_1)$$

In this equation,  $m_1$  is the mass [kg] of the vehicle body and  $m_2$  is the mass [kg] of the wheel and suspension. The spring constant of the suspension system [N/m] is represented by  $k_1$ ,  $k_2$  is the spring constant [N/m] of the wheel and tyre. The damping constants [Ns/m],  $c_1$  and  $c_2$  are for the suspension system and the wheel and tyre respectively. The displacement [m] of the vehicle body is denoted by  $z_1$  and displacement [m] of the wheel is denoted by  $z_2$ , these displacements are considered the outputs. The road profile change [m], u, is the input.

By treating initial conditions as zero and applying Laplace's transform to these equations we can obtain a transfer function for the displacement of the vehicle body mass (x-engineer.org, n.d.):

$$Z_1(s) = (m_1 s^2 + c_1 s + k_1) = Z_2(s)(c_1 s + k_1)$$

$$Z_2(s) = (m_2 s^2 + k_2 + c_2 s + c_1 s + k_1) = U(s)(c_2 s + k_2) + Z_1(s)(c_1 s + k_1)$$

$$Z_2(s) = Z_1(s) \frac{m_1 s^2 + c_1 s + k_1}{c_1 s + k_1}$$

$$H_1(s) = \frac{Z_1(s)}{U(s)}$$

$$=\frac{c_1c_2s^2+(k_1c_2+k_2c_1)s+k_1k_2}{m_1m_2s^4+(m_1c_1+m_1c_2+m_2c_1)s^3+(m_1k_1+m_1k_2+k_1m_2+c_1c_2)s^2+(c_1c_2+c_1k_2+k_1c_2)s+k_1k_2}$$

The displacement for the tyre can also be obtained through this method, however the rest of the project focuses on the displacement of the body and the experimental data containing the tyre displacement is not used.

This displacement data obtained in the study conducted by Kioutsoukis et al. (2022), was based upon a Simulink model used in the study which can be found in appendix 9A, as this project was continuation of the study the experimental data had been provided by M. Foo. The experimental data for the displacement of the body can be seen in figure 9.

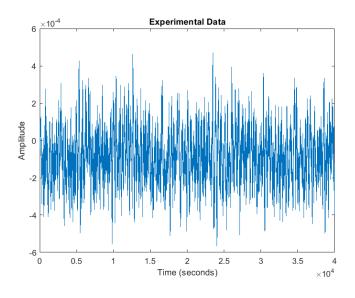


Figure 9: Experimental Data collected in the previous study

# 4.MATLAB System Identification Toolbox

#### 4.1. GUI Toolbox

The project commenced with exploring what the MATLAB System Identification toolbox had to offer. The toolbox allows the user to import a dataset, set parameters for a chosen model and estimate a predicted model based on the input. Within these model choices in the toolbox there is a section which allows you to select Hammerstein-Weiner models. Within the Hammerstein-Weiner window there are options to select 7 types of nonlinear blocks (piecewise linear, sigmoid network, saturation, dead zone, wavelet network and one-dimensional network, you also have the option to select 'none') for input and output nonlinearities. You would also have to dictate the properties of the linear block (numerator order, denominator order and delay).

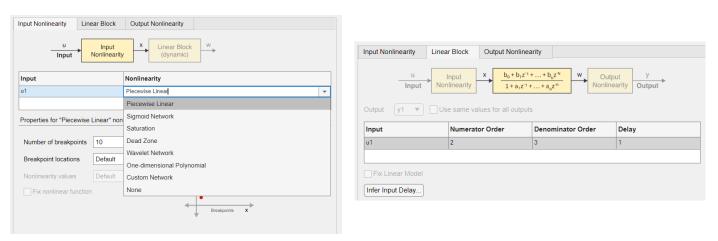


Figure 10: Left: SysID Nonlinear input options. Right: SysID linear block options

To begin, we wanted to find how altering different parameters on a small portion of the data affects how well the model fits to the data. Datapoints between 200000 and 200200 from the data collected from the vehicle 'body' were chosen to start with. Then the sigmoid network was selected as a starting point for the nonlinear blocks, however the focus at this point was finding the best order and delay for the linear block. During this testing, the units for the sigmoid blocks were also altered just to see what effect this would have on the fit value for the model.

	Input NL	Linear Block	Output NL	fi	t
input(u)	sigmoid (10 units)	1.2.1	sigmoid (10 units)	output(y)	58.14
	sigmoid (10 units)	2.3.1	sigmoid (10 units)		59.56
	sigmoid (20 units)	1.2.1	signoid (20 units)		3.948
	sigmoid (10 units)	2.4.1	sigmoid (10 units)		34.68
	sigmoid (10 units)	3.4.1	sigmoid (10 units)		45.32
	sigmoid (10 units)	1.4.1	sigmoid (10 units)		70.05
	sigmoid (5 units)	1.4.1	sigmoid (5 units)		68.06
	sigmoid (20 units)	1.4.1	sigmoid (20 units)		70.92
	sigmoid (50 units)	1.4.1	sigmoid (50 units)		35.85
	sigmoid (30 units)	1.4.1	sigmoid (30 units)		40.07
	sigmoid (20 units)	2.4.1	sigmoid (20 units)		31.35
	sigmoid (10 units)	2.4.1	sigmoid (10 units)		34.68
	sigmoid (10 units)	1.8.1	sigmoid (10 units)		36.9
	sigmoid (10 units)	2.8.1	sigmoid (10 units)		2.827
	sigmoid (20 units)	1.4.5	sigmoid (20 units)		57.31
	sigmoid (20 units)	1.4.2	sigmoid (20 units)		13.97
	sigmoid (20 units)	1.4.10	sigmoid (20 units)		38.99
	sigmoid (20 units)	4.8.1	sigmoid (20 units)		63
	sigmoid (20 units)	2.8.1	sigmoid (20 units)		9.743
	sigmoid (25 units)	1.4.1	sigmoid (25 units)		51.71
	sigmoid (15 units)	1.4.1	sigmoid (15 units)		79.26
	sigmoid (12 units)	1.4.1	sigmoid (12 units)		74.97
	sigmoid (16 units)	1.4.1	sigmoid (16 units)		70.06
	sigmoid (14 units)	1.4.1	sigmoid (14 units)		70.97

Figure 11: Initial test results from SysID toolbox for finding best linear order

From this set of trials (figure 11), we can see that a linear block with a numerator order of 1, denominator order of 4 and a delay size of 1 produces the best results when combined with a sigmoid input and output NL block with unit size 15 (79.26%, highlighted in green in figure 11, plotted against experimental data in figure 12). From this set of data, we can also see that increasing the numerator order has a negative effect on the fit value, likewise, increasing the denominator order past a value of 4 also has a negative effect on the fit. In instances where the delay size has been increased more than 1 the fit value also does not improve. From this initial test we can assume that, for now, a fourth order linear block with no delay is the optimal choice although this could be verified at a later stage with further testing. From this set of data, we can also observe that between the values of 5 to 50 units there is no obvious trend between unit size for the sigmoid network block and the fit value. The only thing we can say for sure is that for that range of units tested, the fit value peaks at 15 sigmoid units.

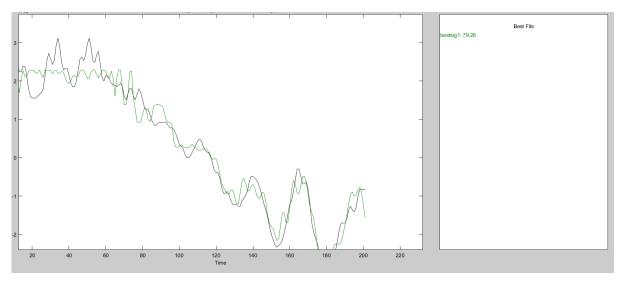


Figure 12: 4th order sigmoid network model fit against experimental data

The SysID toolbox was also used to test the effect of a moving average filter on the data to see if it makes any improvement to the fit value as the data exhibits a lot of high frequency noise which could be negatively affecting how well the models generated are fitting to the data. With a basic average noise filter applied to the data, the data was tested with sigmoid nonlinear blocks from units 1 to 100, with unfiltered versus filtered data to see if it had an improvement on the average fit (figure 13). The full set of this dataset can be found in appendix 9B.

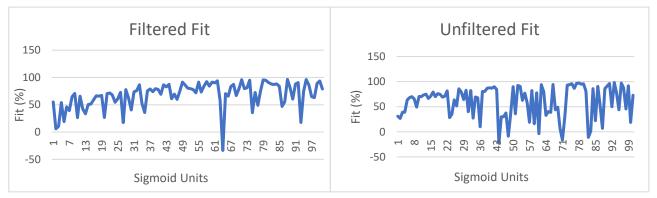


Figure 13: Left: Filtered data fit. Right: Unfiltered data fit.

The results show an average increase in fit for the models generated where the data is preprocessed with a moving average filter, with an average fit of 68% for filtered data versus a 60.6% fit for unfiltered data. This demonstrates that a moving average filter does help with the high frequency noise to some degree. With additional testing the optimal window size for the filter could be found to see if the effects of the filter can be optimised any further.

## 4.2. Automation (Using MATLAB nlhw Function)

Testing the model repeatedly, from units 1-100 with the SysID toolbox, took a very long time to compute. This is because inputting the non-linear units and linear order for every model, then waiting for it to process and output a result which then needs to manually be stored is extremely time-consuming. Before continuing with testing, a more efficient way of generating the models was developed, which could save the fit values automatically, allowing me to process many combinations of nonlinear blocks in a shorter time frame.

The MATLAB code for generating the nonlinear Hammerstein-Weiner models automatically in MATLAB went through several iterations because there are multiple ways that you can create these models in a MATLAB script. After some testing and trial and error, using the nlhw() command appeared to be the simplest and most efficient way of doing this, as you can select the linear block parameters and the nonlinear blocks you want to use all in one line of code. The function nlhw() 'creates and estimates a Hammerstein-Wiener model using the estimation data, model orders and delays', you can then specify input and output nonlinearities as well, otherwise they will be the default piecewise linear functions (Mathworks, 2023b). The script is essentially a for loop which allows you to increment the parameters for the nonlinear blocks and then it will store the fit values in an array, meaning it is no longer required to have to record the results individually for every model generated. Much like the SysID toolbox, the script still takes a cut of the overall data to avoid it taking too long to process.

The MATLAB script also has the option to plot the model against the data to visually analyse how well a certain model might fit against the data. The script works by pre-processing and cutting the simulated (or linear) data and experimental data and then applying a noise filter to fit in line with the current hypothesis that the experimental data is made up of a combination of a linear component, a nonlinear component, and some unidentified noise component. The cut of experimental data and the filtered linear data is then fed into the iddata object along with the sampling interval  $T_s$ . The iddata object encapsulates input and output measurement data for a system, system identification functions can then be used to estimate a model using nlhw (Mathworks, 2023a).

With the script functioning as intended, it is then possible to test different combinations of nonlinear blocks and parameters to see what kind of fits would be achievable.

One issue with this method is that occasionally the script would produce an error with a few specific combinations of parameters, but this does not affect the overall results, so when an error is encountered, the for loop would have to be resumed manually, skipping over the iteration that causes the error. The script can be found in full in appendix 9C, only the sigmoid

network function is displayed in the appendix, however this can be easily changed to whichever nonlinear block needs to be used in the N-L-N model.

# 5. Noise Filter Testing

# 5.1. Moving Average Filter

A moving average filter was tested to see how well the high frequency noise could be removed from the experimental data, with the aim of creating a better fit for the nonlinear models that would be tested against this data. A moving average filter in MATLAB can be achieved with the movmean function with the input parameters being the input data and the window size. Using the automated MATLAB script, the optimal window size was found to be 25. The results from this test can be seen in figure 14.

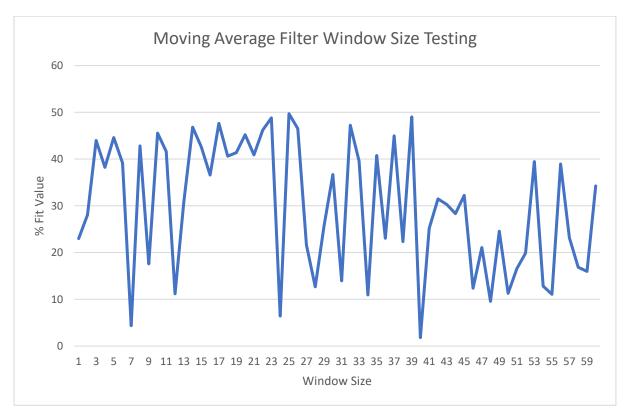


Figure 14: Moving Average Filter test results for changing Window Size

#### 6. Nonlinear Models

This chapter details the process and results for testing different nonlinear blocks in MATLAB. Unless stated otherwise, all models in this chapter were generated using a dataset cut from 200000 to 201200 datapoints to ensure some consistency between tests. Each model was then validated with a cut of data the same size from the next period (+100000 datapoints) due to the periodic nature of the data. Tables for these test results in full can be found in appendix 9D.

## 6.1. Sigmoid Network

The first set of models created were done with the Sigmoid Network nonlinear blocks. The default unit option is 10 (see figure 15) however this can be altered. Initially, models were created using units from 1 to 300 and having the input and output nonlinearities exhibit the same unit value at any given instance.



Figure 15: Sigmoid Network Parameters

The purpose of increasing the unit value over a range was to see if any trends became apparent as the value increased. In figure 16, 'Series1' is how well the model fits the estimation (or training) data, 'Series2' is how well the model fits the validation (or testing) data (this applies for all further instances in the paper where 'Series1' and 'Series2' are used in plots). This is for the cut of data between datapoints 200000 and 201200. The validation data set is the same size as the estimation data but from datapoints 300000-301200 as the data follows a periodic trend.

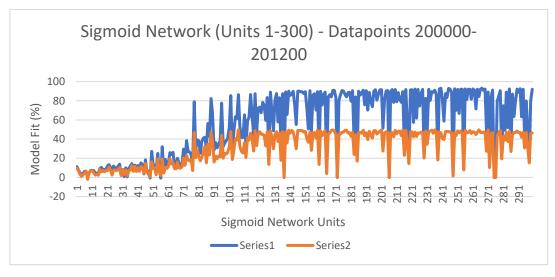


Figure 16: Sigmoid Network Models (Units 1-300, Datapoints 200000-201200)

The overall trend observed is that increasing the units in the sigmoid network does improve the model fit up to around 130 units and after that the improvement to the model fit is minimal. Despite this, the results are not very consistent, with a lot of dips in the data, however these results are still useful as they demonstrate a rough correlation between the sigmoid network units and the model fit which can be seen in figure 17.

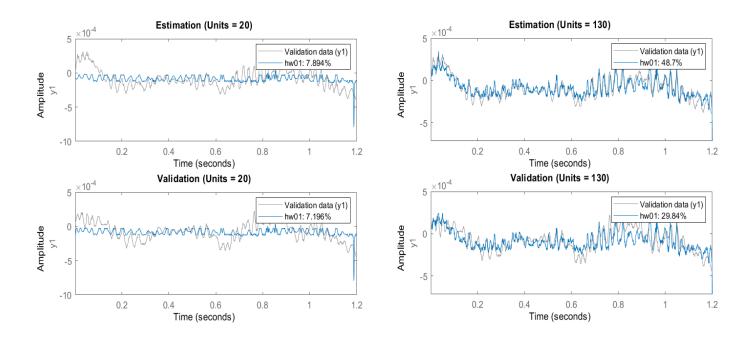


Figure 17: Comparison of Sigmoid Models (Units 20 and 130) against validation data

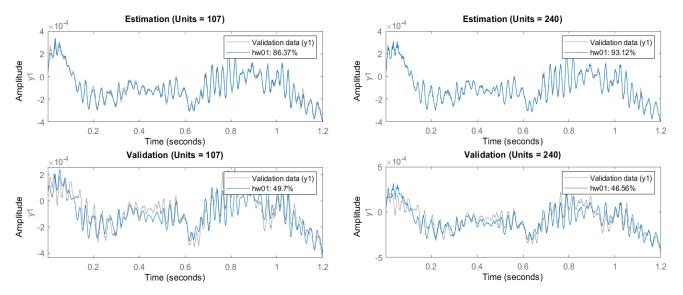


Figure 18: Comparison of Sigmoid Models (Units 107 and 240) against validation data

In figure 17, the 20-unit sigmoid network does not fit either dataset very well, but as the units increase to 130, there is an improved fit, not only numerically but also visually we can start to see it is picking up the trends in the estimation and validation data.

Two of the best models that were generated were done with 107 and 240 units (see figure 18), with 107 giving the best fit with the validation data numerically and 240 giving the best fit with the estimation data numerically. Despite the actual fit value being roughly half of the value given for the estimation data in more cases, the model does pick up on the overall trend of the validation data.

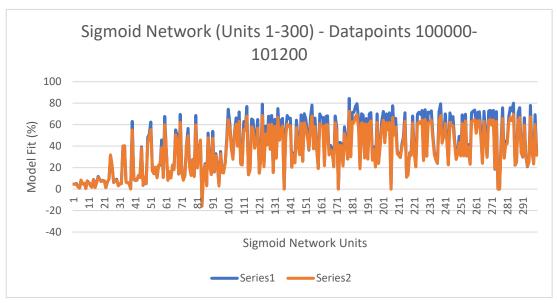


Figure 19: Sigmoid Network Models (Units 1-300, Datapoints 100000-101200)

As this nonlinear model produced the best fits out of all the models tested, further models were generated using different cuts of data to see how well the model held up with other sections of the data. A set of models were then generated using datapoints 100000-101200 (see figure 19), which followed a similar trend to the previous set of datapoints (figure 16), but the model fit for the validation data was closer to the estimation data this time around. In figure 19, 'Series1' is the model fit compared with the estimation data and 'Series2' is the model fit compared with the validation data.

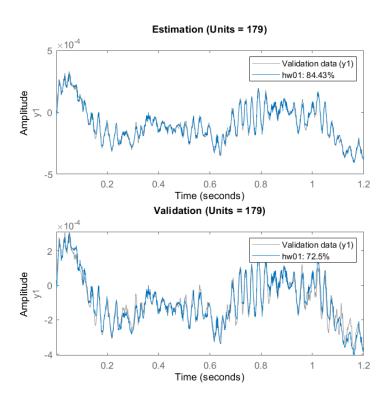


Figure 20: Sigmoid Model generated with 179 units (datapoints 100000-101200)

With the alternative dataset, the model in figure 20 follows the trend of both estimation and validation data well. If we compare the same units with the previous dataset (200000 – 201200) with a sigmoid network model with the 179 units (see figure 21), we see it fits the data well and follows the trends of the data well too.

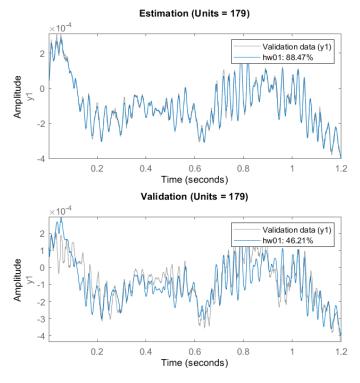


Figure 21: Sigmoid Model generated with 179 units (datapoints 100000-101200)

The model generated with input and output nonlinearities as a sigmoid network with 179 units follows the trends of both datasets, which suggests that it could be a good case for modelling the nonlinearities, however it does not follow all the trends so there is potential for a better model. This was the best model for the nonlinearity that could be achieved using the nonlinear Hammerstein-Weiner model in MATLAB.

Due to the sigmoid network providing the most promising set of results, more models were generated with a single sigmoid network input nonlinearity block and then an additional set with just a single sigmoid network output nonlinearity block to see if the model fits the data with only one nonlinearity instead of two as previously tested. The data below (see figures 22 and 23) was generated using a smaller dataset of datapoints 200000 to 200200 to improve the computation time.

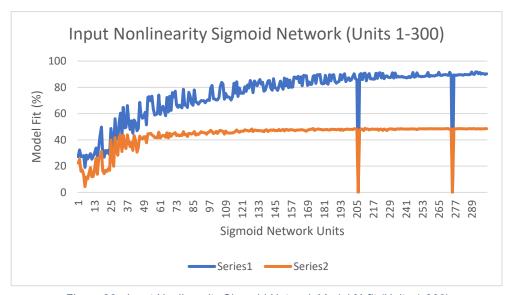


Figure 22: Input Nonlinearity Sigmoid Network Model % fit (Units 1-300)

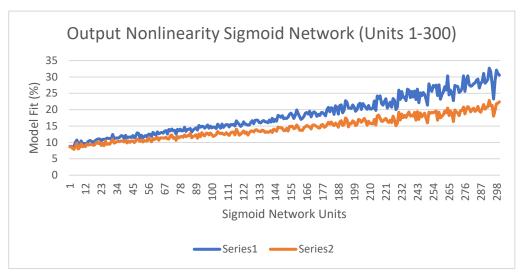


Figure 23: Output Nonlinearity Sigmoid Network Model % fit (Units 1-300)

The single input nonlinearity gives a more consistent trend than two nonlinear blocks, the maximum fit values are very similar for both estimation and validation data. In contrast, the single output nonlinearity does not provide a very good fit for the units tested.

Depending on how many units are chosen either a single input sigmoid network could be a better choice versus the usual input and output sigmoid network blocks.

#### 6.2. One Dimensional Polynomial Network

Another nonlinear model that was tested against the data from the suspension system was generated using a one-dimensional polynomial network. The default setting for this network is one degree of polynomial (see figure 24), however this can be increased. The number of coefficients can also be altered; however, you cannot change both at the same time, one of these parameters must be set to its default value.

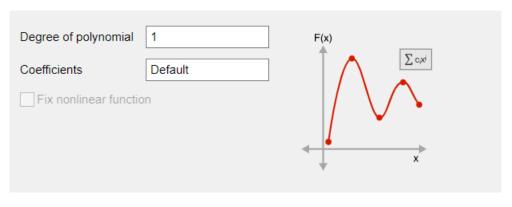


Figure 24: One Dimensional Polynomial Network Parameters

After testing this model against a section of the data, it showed the best fit with the default setting of one degree of polynomial, with two degrees of polynomial there was a significant drop, after that, the fit did not change at all, staying the same as the results obtained from two degrees.

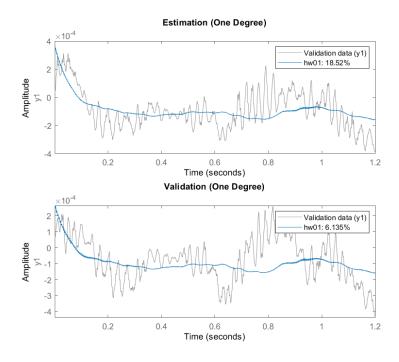


Figure 25: One Dimensional Polynomial Model generated with One Degree (datapoints 200000-201200)

From the results generated, with an input and output polynomial block, a one-dimensional polynomial network does not really pick up on the high frequency trends in the data (see figure 25). With a single input block (see figure 26, the fit against the data is improved slightly, however still not picking up on the higher frequency information. A single output does not provide any benefits versus the single input and changing coefficients does not help improve the fit at all.

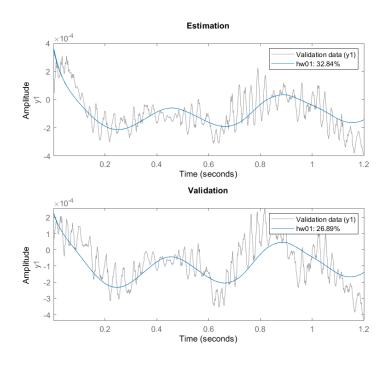


Figure 26: One Dimensional Polynomial Model versus Validation data (Second Degree, Input Block only)

#### 6.3. Piecewise Linear Function

One of the types of nonlinear models that can be generated using the nlhw function is the piecewise linear function (see figure 27). The number of breakpoints can be adjusted for this nonlinear model, the default value is 10. After incrementing the number of breakpoints and testing the fit against the estimation and validation data the best fit value achieved was a 41% for the estimation data and 34% for the validation data, which does not show promising results and most likely not taking this function any further with testing (results plotted in figures 26 and 29).

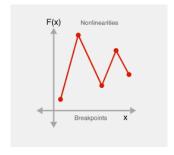


Figure 27: Piecewise Linear Function

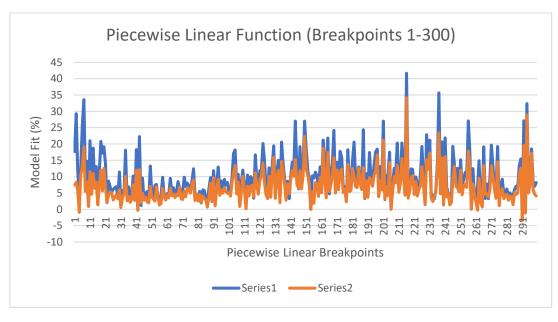


Figure 28: Piecewise Linear Function Model % fit (Breakpoints 1-300)

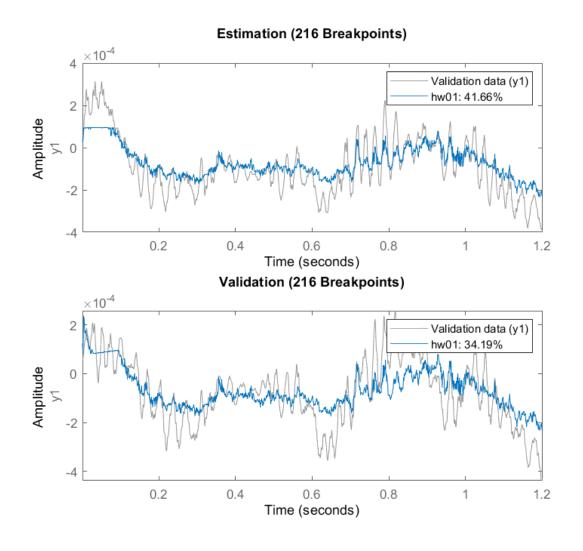


Figure 29: Piecewise Linear Function Model versus Validation data (216 Breakpoints)

## 6.4. Wavelet Network

Another set of nonlinear models that were generated in MATLAB were created using the wavelet network. The default units for the wavelet network are 10 however this can be altered (see figure 30), a set of models were generated with unit values 1-300 for a cut of datapoints between 200000-201200.

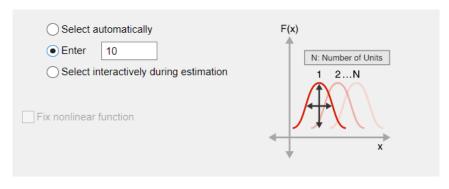


Figure 30: Wavelet Network Parameters

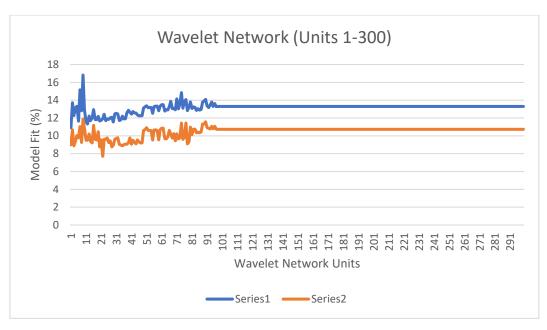


Figure 31: Wavelet Network Model % fit (Units 1-300)

The fit value varies for unit values below 100, after that there is a consistent low fit value, as shown in figure 31. When comparing the unit value with the highest fit value against the plotted data, we can see that the model does pick up the occasional trend, however generally it is not a good model for the data, as can be seen in figure 32.

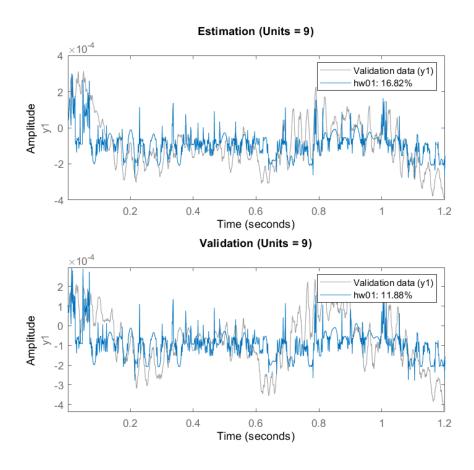


Figure 32: Piecewise Linear Function Model versus Validation data (Units = 9)

#### 6.5. Saturation

One of the other nonlinear models tested from the SysID toolbox is the Saturation nonlinearity. This nonlinear model has two parameters that can be altered – the upper limit and lower limit of each block - so a few different combinations of parameters can be tested. As well as adjusting all limits in equal increments in tests, several more combinations were tested in terms of what limits incremented and which stayed the same. The list of 6 different combinations where the limits change is; the input upper limit, both upper limits, output upper limit, input lower limit, both lower limits and output lower limit. None of these 6 sets of tests produced any results with any suitable fits (see appendix 9D). Incrementing all limits simultaneously produced marginally better results than what was achieved by altering only some of the limits, however there were still no models that followed the data anywhere near as well as the sigmoid networks. The results obtained for the models generated by incrementing all limits simultaneously are shown in the figure 33.

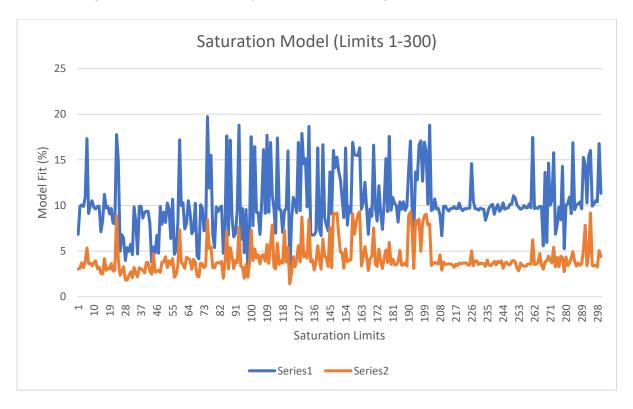


Figure 33: Saturation Model % fit (Limits 1-300)

#### 6.6. Deadzone

Another one of the less successful sets of nonlinear models trialled were the ones generated with input and output deadzone nonlinearity blocks. The deadzone nonlinearity has the option to adjust the upper and lower limits, which, if not changed will resort to their default value (see figure 34).



Figure 34: Deadzone Model Parameters

Several combinations of different limit values were trialled, much like the saturation nonlinearity above, changing the following for six different combinations; input upper limit, both upper limits, output upper limit, input lower limit, both lower limits and outer lower limit. With all these combinations there were no promising fits and all combinations not changing after incrementing past a limit value of 2. In addition, these models had a fit value below 16%. Incrementing all limit values at the same time didn't provide much better results either with the best model fit at 19.73% (see figure 35).

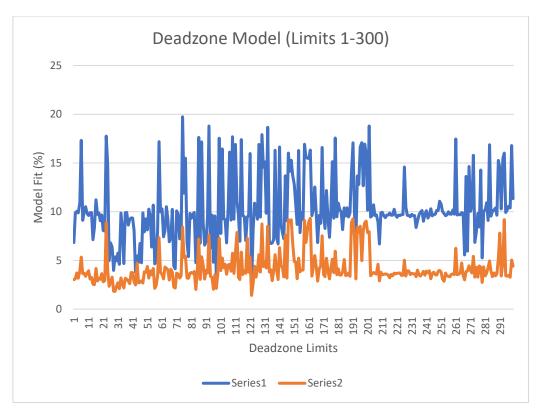


Figure 35: Deadzone Model % fit (Limits 1-300)

As shown in the figure below, a deadzone nonlinearity model does not fit the experimental data well and is not worth investigating any further.

## 6.7 Combining Nonlinear Models

After finding that the two best nonlinear models were sigmoid network and one-dimensional polynomial network, several tests were done to see if combining different nonlinear models would improve the fit, compared to just using one model in the N-L-N model. To trial this idea, the best fitting one-dimensional polynomial network block (second degree) was taken along with a sigmoid network block with incrementing units. These blocks were combined in two combinations, the first being the sigmoid network as the input block and the one-dimensional polynomial block as the output (see figure 36). The second combination was then the opposite of this, having the one-dimensional polynomial block as the input and sigmoid network block as the output (see figure 37).

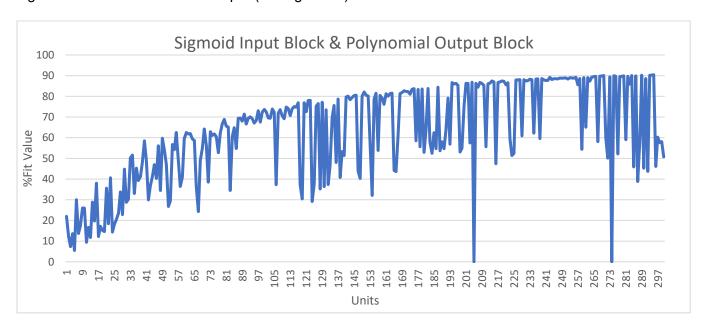


Figure 36: Sigmoid Network Input Block with Second Degree Polynomial Output Block Fit results (Units 1-300)

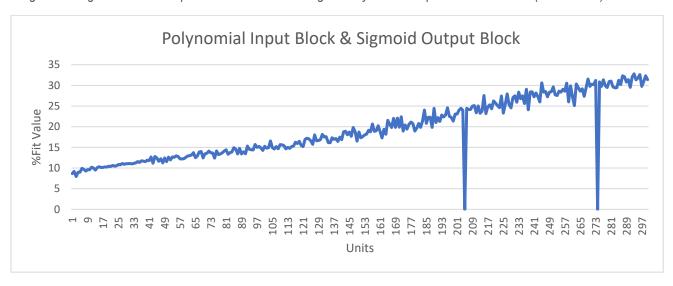


Figure 37: Second Degree Polynomial Input Block with Sigmoid Network Output Block Fit results (Units 1-300)

Out of these two models, the model with the input sigmoid network block performed a lot better than the one generated with a sigmoid network block as the output. These models produce a very similar fit value to the models generated with only a single sigmoid block. This could suggest that the polynomial block in these models is having very little effect on the generation of the model. Despite having reasonable estimated fit data, particularly in the first model, it was decided not to take the approach of combining different nonlinearities any further as the validation fit values produced were extremely low. The validation fit values ranged from 2.79% to -1×10<sup>13</sup> %, which is some of the lowest fit values generated across the whole project.

## 6.8 Overall findings

The models generated with the sigmoid network provided the closest fit to the small cut of experimental data out of all the nonlinear blocks tested. To see how well this model would fit across a wide spread of datapoints, a sigmoid network model with two blocks, 500 units for each block, was generated. The datapoints spanned across a whole period (200,000 to 300,000 datapoints). The fit of this model can be seen in figure 38.

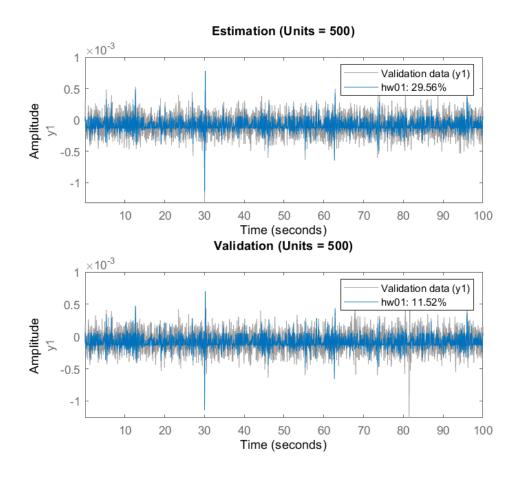


Figure 38: Sigmoid Network generated with a wide spread of datapoints

Whilst the numerical fit value is quite low when you compare this to some of the previous results generated with sigmoid networks, a much larger dataset has been used so this is to be expected. Even though the numerical fit value is low, the model still picks up most of the trends of the experimental data. The experimental data has higher frequency components that the model is failing to pick up, this could be because there is an extra component that was not initially considered in the original hypothesis.

## 7.Conclusion

The objective of this project was to identify the nonlinearities presence in the active suspension system as demonstrated in Kioutsoukis et al. (2022) and similar prior studies, e.g. Fayyad (2012) and Minlanese et al. (2004). Six different nonlinear blocks were used to generate many models which were then compared against the experimental data collected in Kioutsoukis et al. (2022). The initial hypothesis was that the experimental data comprised of a linear component, a nonlinear component and some noise component.

Upon analysing the results, particularly those pertaining to the model generated with sigmoid network blocks, combined with a moving average filter, a model was developed that replicated some of the trends observed in the original experimental data. However, direct comparison of this model with the experimental data revealed an inability to capture certain high-frequency components that the experimental data had. This discrepancy would suggest that an amendment needs to be taken to the original hypothesis, in addition to the linear, nonlinear and noise component, there is an additional high frequency component that has not yet been identified.

The other five nonlinear blocks did not produce very accurate models compared with a sigmoid network. The average moving filter used to reduce the noise did work to some level of success, improving the fit of the model against the data. However, some of the unidentified high frequency component could be attributed to this noise, meaning that the average moving filter did not filter out enough noise. Without knowing the possible fourth unknown component, it is impossible to verify this.

Although the project did not fully achieve its objectives, the work detailed in this report does provide a good foundation for future work and has made some progress in understanding what the experimental data collected in Kioutsoukis et al. (2022) is made up of. Unfortunately, the problem was more complex than initially expected meaning that it could not be completed in the time frame allocated to this project.

#### 7.1. Future Works

Further work on this project could involve testing additional identification methods, such as Sparse Identification of Nonlinear Dynamics (SINDy). SINDy employs a data-driven framework that yields interpretable models that avoid overfitting (Fasel et al., 2021). One key advantage of using SINDy is that it has 'a robustness to noise with less training data' (Kaheman et al., 2022), the noise and high frequency components being something the N-L-N Hammerstein-Weiner model struggled with. This capability may enable SINDy to circumvent these issues. In addition, the ability to produce accurate results with less training data is also a benefit as it will improve computation time for generating models.

Another modelling technique that did not receive attention in this study is a Nonlinear ARX Model (NARX Models). NARX models are better suited to modelling dynamic nonlinearities, compared to Hammerstein-Weiner models which can only model static nonlinearities. NARX models are available in the MATLAB SysID toolbox. This means they can be tested in a similar manner to which the Hammerstein-Weiner models were tested in this project. In addition to this, NARX models have not received much attention in literature (Zhu, 2002), meaning there is potential to try methods which have not yet been investigated fully.

Currently all the analysis done in the MATLAB script has used validation data, which is periodic to the estimation data, however when using validation data that is not periodic, the fit value would be very poor (negative in a lot of cases). In the future, more analysis will need to be done on this as it is important to achieve a strong fit value not only with periodic validation data but also validation data that is not periodic.

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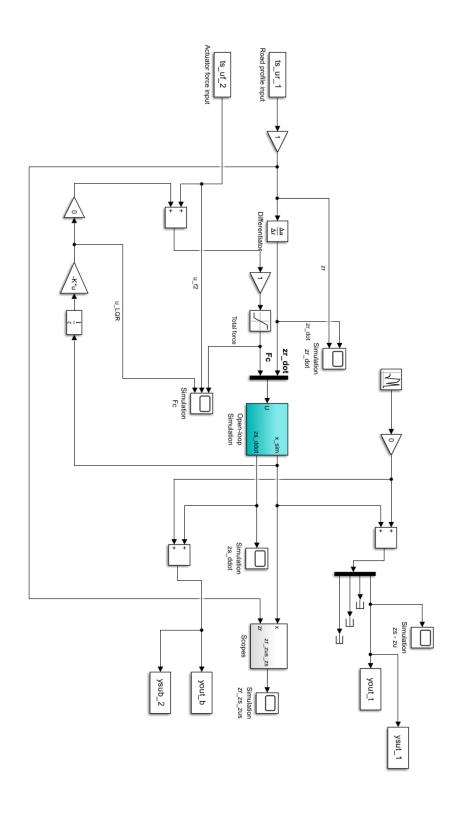
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## 9. Appendices

### 9.A. Simulink Model



## 9.B. Toolbox GUI Test Spreadsheet

	Input NL	Linear Block	Output NL		fit
input(u)	sigmoid (10 units)	1.2.1	sigmoid (10 units)	output(y)	58.14
	sigmoid (10 units)	2.3.1	sigmoid (10 units)		59.56
	sigmoid (20 units)	1.2.1	signoid (20 units)		3.948
	sigmoid (10 units)	2.4.1	sigmoid (10 units)		34.68
	sigmoid (10 units)	3.4.1	sigmoid (10 units)		45.32
	sigmoid (10 units)	1.4.1	sigmoid (10 units)		70.05
	sigmoid (5 units)	1.4.1	sigmoid (5 units)		68.06
	sigmoid (20 units)	1.4.1	sigmoid (20 units)		70.92
	sigmoid (50 units)	1.4.1	sigmoid (50 units)		35.85
	sigmoid (30 units)	1.4.1	sigmoid (30 units)		40.07
	sigmoid (20 units)	2.4.1	sigmoid (20 units)		31.35
	sigmoid (10 units)	2.4.1	sigmoid (10 units)		34.68
	sigmoid (10 units)	1.8.1	sigmoid (10 units)		36.9
	sigmoid (10 units)	2.8.1	sigmoid (10 units)		2.827
	sigmoid (20 units)	1.4.5	sigmoid (20 units)		57.31
	sigmoid (20 units)	1.4.2	sigmoid (20 units)		13.97
	sigmoid (20 units)	1.4.10	sigmoid (20 units)		38.99
	sigmoid (20 units)	4.8.1	sigmoid (20 units)		63
	sigmoid (20 units)	2.8.1	sigmoid (20 units)		9.743
	sigmoid (25 units)	1.4.1	sigmoid (25 units)		51.71
	sigmoid (15 units)	1.4.1	sigmoid (15 units)		79.26
	sigmoid (12 units)	1.4.1	sigmoid (12 units)		74.97
	sigmoid (16 units)	1.4.1	sigmoid (16 units)		70.06
	sigmoid (14 units)	1.4.1	sigmoid (14 units)		70.97
	piecewise (10 breakpoints)	1.4.1	piecewise (10 breakpoin	ts)	64.45
	one-dimensional poly (fourth d	1.4.1	one-dimensional poly (fo	urth degree)	27.53
	sigmoid (15 units)	1.4.1	piecewise (10 breakpoin	ts)	62.33

1	units (Sigmoid)	Filtered Fit	Unfiltered Fit	units (Sigmoid)	Filtered Fit	Unfiltered Fit
2 10.55 39.17 51 79.61 92.47 3 53.9 38.97 52 77.74 90.47 4 19.01 63.51 53 71.82 62.61 5 46.19 68.06 54 91.59 77.13 6 39.38 70.03 55 73.46 57.33 7 64.63 65.69 56 83.87 18.97 9 2.4 82.12 9 2.65.51 70.41 58 84.15 16.05 10 65.81 70.05 59 91.65 77.75 11 42.32 73.61 60 89.91 -3.65.6 11 42.32 73.61 60 89.91 -3.65.6 12 33.34 74.97 61 93.93 94.12 13 50.42 66.71 62 58.17 80.12 14 51.43 70.97 63 33.56 32.83 15 59.34 79.26 64 70.31 40.43 16 66.32 70.06 65 65.64 38.91 19 26.6 66.32 70.06 65 65.64 38.91 19 26.6 69.2 68 66.89 49.12 19 26.6 69.2 68 66.89 49.12 20 70.39 70.92 69 79.05 65.55 16.55 12 22 67.65 28.26 71 79.52 30.18 24 61.05 63.69 73 95.16 94.14 25 77.75 79.2 76 49.02 96.55 16.55 17.75 17.75 79.2 76 49.02 96.43 17.75 79.2 76 49.02 96.43 17.75 79.2 76 49.02 96.43 17.75 79.2 76 49.02 96.43 17.75 79.2 76 49.02 96.55 16.55 17.75 79.2 76 49.02 96.55 16.55 17.75 79.2 76 49.02 96.55 16.55 17.75 79.2 76 49.02 96.55 16.55 17.75 79.2 76 49.02 96.55 17.75 17.75 79.2 76 49.02 96.55 17.75 17.75 79.2 76 49.02 96.55 17.75 17.75 79.2 76 49.02 96.55 17.75 17.75 7	0	55.24	31.12	49	86.21	89.91
3		5.949	26.54	50	80.37	35.85
4 19.01 63.51 53 71.82 62.61 56 46.19 68.06 54 91.59 77.12 65.81 63.93.87 70.03 55 73.46 57.33 77 64.63 65.69 56 83.87 18.99 26.51 70.41 58 84.15 16.05 10 65.81 70.05 59 91.65 77.75 11 42.32 73.61 60 89.91 -3.626 12 33.34 74.97 61 93.93 94.12 13 50.42 66.71 62 58.17 80.12 14 51.43 70.97 63 -33.66 32.83 15 59.34 79.26 64 70.31 40.43 16 66.32 70.06 65 65.64 38.91 77 65.81 76.03 66 83.36 42.28 18 67.19 74.53 67 87.38 43.97 19 26.6 69.2 68 66.89 49.14 22 67.65 22 67.65 23 54.9 35.07 72 80.83 93.12 24 61.05 63.69 73 81.49 35.07 72 80.83 93.12 24 61.05 63.69 73 85.67 75 72.41 86.62 77.77 5 79.2 76 49.02 96.48 62.2 67.77 77.75 79.2 76 49.02 96.48 30 73.53 85.67 77 74.25 97.05 31 76.01 82.09 80 90.71 80.91 32 86.59 27.43 81 88.02 -3.64 33.93 52.34 40.07 79 94.69 95.55 31 76.01 82.09 80 90.71 80.91 32 86.59 27.43 81 88.02 -3.64 33.93 52.34 69.35 82.69 78 95.6 94.84 35.97 79.38 86.59 27.43 81 88.02 -3.64 33.93 52.34 69.35 82.89 87.05 10.07 33 77.35 86.67 75 72.41 86.62 39 40.46 82.69 78 95.6 94.84 35.97 79 94.69 95.55 31 76.01 82.09 80 90.71 80.91 32 86.59 27.43 81 88.02 -3.64 33.93 52.34 69.35 82.89 37.05 10.07 33 50.64 82.69 78 95.6 94.84 35.94 67.87 83 88.22 86.18 33.94 67.87 83 88.22 86.18 33.95 75.47 10.06 84 83.93 88.22 86.18 33.97 73.83 80.54 86 55.44 53.5 39 78.12 87.69 88.94 91.16 86.55 90 90 88 90.71 80.91 32 86.59 27.43 81 88.02 -3.68 80.24 82.69 84.44 87 96.42 67.5 34 87.04 87.94		10.55	39.17	51	79.61	92.42
5	3	53.9	38.97	52	77.74	90.47
6 39.38 70.03 55 73.46 57.33 7 64.63 65.69 56 83.87 18.97 8 70.75 49.28 57 92.4 82.12 9 26.51 70.41 58 84.15 16.00 10 65.81 70.05 59 91.65 77.75 11 42.32 73.61 60 89.91 3.622 12 33.34 74.97 61 93.93 94.12 13 50.42 66.71 62 58.17 80.12 14 51.43 70.97 63 -33.66 32.83 15 59.34 79.26 64 70.31 40.43 16 66.32 70.06 65 65.64 38.36 17 65.81 76.03 66 83.36 94.28 18 67.19 74.53 67 87.38 43.97 19 26.6 69.2 68 66.89 49.14 20 70.39 70.92 69 79.05 6.556 21 71.7 81.47 70 95.85 1-6.53 22 67.65 28.26 71 79.52 30.18 23 54.49 35.07 72 80.83 93.12 24 61.05 63.69 73 95.16 94.14 25 72.71 51.71 74 35.37 79.52 26 17.33 85.67 75 72.41 86.62 27 77.75 79.2 76 49.02 96.49 29 40.46 82.69 78 95.6 94.84 30 73.53 40.07 79 94.69 95.5 31 76.01 82.09 80 90.71 80.93 32 86.59 27.43 81 88.02 -10.88 33 52.34 69.35 82 87.05 10.93 34 35.94 67.87 80.4 85 46.94 90.5 35 75.47 10.06 84 83.93 22.25 36 78.79 80.4 85 46.94 90.5 36 78.79 80.4 87 96.42 6.75 37 73.83 80.54 86 55.44 35.5 38 79.54 87.04 87 96.42 6.75 38 79.54 87.04 87 96.42 6.75 38 79.54 87.04 87 96.42 6.75 39 78.12 87.6 88 81.46 86.18 40 69.27 86.97 89 60.36 91.14 86.55 90 90 88 96.34 41 86.55 90 90 88 96.34 42 82.69 84.48 91 90.53 50.06 45.44 60.98 29.8 93 74.66 77.65 46 59.78 37.37 95 85.86 97.19 47 74.55 88.85 96 64.74 87.65 48 91.36 37.2 97 63.06 45.44	4	19.01	63.51	53	71.82	62.61
7         64.63         65.69         56         83.87         18.97           8         70.75         49.28         57         92.4         82.12           9         26.51         70.41         58         84.15         16.00           10         65.81         70.05         59         91.65         77.75           11         42.32         73.61         60         89.91         -3.626           12         33.34         74.97         61         93.93         94.12           13         50.42         66.71         62         58.17         80.12           14         51.43         70.97         63         -33.66         32.31           16         66.32         70.06         65         65.64         38.91           17         65.81         76.03         66         83.36         94.24           20         70.39         70.92         69         79.05         6.55           18         67.17         81.47         70         95.85         -16.53           21         71.7         81.47         70         95.85         -16.53           22         67.65         28.26	5	46.19	68.06	54	91.59	77.19
8	6	39.38	70.03	55	73.46	57.33
9	7	64.63	65.69	.56	83.87	18.97
9	8	70.75	49.28	57	92.4	82.12
11		26.51	70.41	58	84.15	16.09
12	10	65.81	70.05	59	91.65	77.79
13	11	42.32	73.61	60	89.91	-3.626
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16 66.32 70.06 65 65.64 38.91 17 65.81 76.03 66 83.36 94.28 18 67.19 74.53 67 87.38 43.97 19 26.6 69.2 68 66.89 49.14 20 70.39 70.92 69 79.05 6.556 21 71.7 81.47 70 95.85 -16.53 22 67.65 28.26 71 79.52 30.18 23 54.49 35.07 72 80.83 93.12 24 661.05 63.69 73 95.16 94.14 25 72.71 51.71 74 35.37 95.9 26 17.33 85.67 75 72.41 86.62 27 77.75 79.2 76 49.02 96.48 30 73.53 40.07 79 94.69 95.51 31 76.01 82.09 80 90.71 80.91 32 86.59 27.43 81 88.02 -10.88 33 52.34 69.35 82 87.05 1.073 34 35.94 67.87 83 88.22 86.18 35 75.47 10.06 84 83.93 22.25 36 78.79 80.4 85 46.94 90.5 37 73.83 80.54 86 55.44 53.5 38 79.54 87.04 87 96.42 6.75 39 78.12 87.6 88 81.46 86.18 40 69.27 86.97 89 60.36 91.14 41 86.55 90 90 88 91.1 41 86.55 90 90 88 96.34 42 82.69 84.48 91 90.53 50.06 43 87.51 -22.67 92 17.69 98.21 44 60.98 29.8 93 74.66 77.69 45 69.44 30.08 94 96.22 43.89 46 59.78 37.37 95 85.86 97.19						
17       65.81       76.03       66       83.36       94.28         18       67.19       74.53       67       87.38       43.97         19       26.6       69.2       68       66.89       49.14         20       70.39       70.92       69       79.05       6.556         21       71.7       81.47       70       95.85       -16.53         22       67.65       28.26       71       79.52       30.18         23       54.49       35.07       72       80.83       93.12         24       61.05       63.69       73       95.16       94.14         25       72.71       51.71       74       35.37       95.9         26       17.33       85.67       75       72.41       86.62         27       77.75       79.2       76       49.02       96.48         28       62.2       64.43       77       74.25       97.03         29       40.46       82.69       78       95.6       94.84         30       73.53       40.07       79       94.69       95.51         31       76.01       82.09       80       <						
18						
19						
20         70.39         70.92         69         79.05         6.556           21         71.7         81.47         70         95.85         -16.53           22         67.65         28.26         71         79.52         30.18           23         54.49         35.07         72         80.83         93.12           24         61.05         63.69         73         95.16         94.14           25         72.71         51.71         74         35.37         95.9           26         17.33         85.67         75         72.41         86.62           27         77.75         79.2         76         49.02         96.48           28         62.2         64.43         77         74.25         97.05           29         40.46         82.69         78         95.6         94.84           30         73.53         40.07         79         94.69         95.51           31         76.01         82.09         80         90.71         80.91           32         86.59         27.43         81         88.02         1.073           34         35.94         67.87 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td></t<>						
21       71.7       81.47       70       95.85       -16.53         22       67.65       28.26       71       79.52       30.18         23       54.49       35.07       72       80.83       93.12         24       61.05       63.69       73       95.16       94.14         25       72.71       51.71       74       35.37       95.9         26       17.33       85.67       75       72.41       86.62         27       77.75       79.2       76       49.02       96.48         28       62.2       64.43       77       74.25       97.09         29       40.46       82.69       78       95.6       94.84         30       73.53       40.07       79       94.69       95.51         31       76.01       82.09       80       90.71       80.93         32       86.59       27.43       81       88.02       -10.88         33       52.34       69.35       82       87.05       1.073         34       35.94       67.87       83       88.22       86.18         35       75.47       10.06       84						
22       67.65       28.26       71       79.52       30.18         23       54.49       35.07       72       80.83       93.12         24       61.05       63.69       73       95.16       94.14         25       72.71       51.71       74       35.37       95.9         26       17.33       85.67       75       72.41       86.62         27       77.75       79.2       76       49.02       96.48         28       62.2       64.43       77       74.25       97.09         29       40.46       82.69       78       95.6       94.84         30       73.53       40.07       79       94.69       95.51         31       76.01       82.09       80.97       80.99       95.71       80.93         32       86.59       27.43       81       88.02       -10.88         33       52.34       69.35       82       87.05       1.073         34       35.94       67.87       83       88.22       86.18         35       75.47       10.06       84       83.93       22.25         36       78.79       80.4						
23       54.49       35.07       72       80.83       93.12         24       61.05       63.69       73       95.16       94.14         25       72.71       51.71       74       35.37       95.9         26       17.33       85.67       75       72.41       86.62         27       77.73       79.2       76       49.02       96.48         28       62.2       64.43       77       74.25       97.09         29       40.46       82.69       78       95.6       94.84         30       73.53       40.07       79       94.69       95.51         31       76.01       82.09       80       90.71       80.91         32       86.59       27.43       81       88.02       -10.88         33       52.34       69.35       82       88.22       86.13         34       35.94       67.87       83       88.22       86.49         35       75.47       10.06       84       83.93       22.25         36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86						
24       61.05       63.69       73       95.16       94.14         25       72.71       51.71       74       35.37       95.9         26       17.33       85.67       75       72.41       86.62         27       77.75       79.2       76       49.02       96.48         28       62.2       64.43       77       74.25       97.09         29       40.46       82.69       78       95.6       94.84         30       73.53       40.07       79       94.69       95.51         31       76.01       82.09       80       90.71       80.91         32       86.59       27.43       81       88.02       -10.88         33       52.34       69.35       82       87.05       1.073         34       35.94       67.87       83       88.22       86.18         35       75.47       10.06       84       83.93       22.25         36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       <						
25       72.71       51.71       74       35.37       95.9         26       17.33       85.67       75       72.41       86.62         27       77.75       79.2       76       49.02       96.48         28       62.2       64.43       77       74.25       97.09         29       40.46       82.69       78       95.6       94.84         30       73.53       40.07       79       94.69       95.51         31       76.01       82.09       80       90.71       80.9         32       86.59       27.43       81       88.02       -10.88         33       52.34       69.35       82       87.05       1.073         34       35.94       67.87       83       88.22       86.18         35       75.47       10.06       84       83.93       22.25         36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88						
26       17.33       85.67       75       72.41       86.62         27       77.75       79.2       76       49.02       96.48         28       62.2       64.43       77       74.25       97.09         29       40.46       82.69       78       95.6       94.84         30       73.53       40.07       79       94.69       95.51         31       76.01       82.09       80       90.71       80.91         32       86.59       27.43       81       88.02       -10.88         33       52.34       69.35       82       87.05       1.073         34       35.94       67.87       83       88.22       86.18         35       75.47       10.06       84       83.93       22.25         36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td></t<>						
27       77.75       79.2       76       49.02       96.48         28       62.2       64.43       77       74.25       97.09         29       40.46       82.69       78       95.6       94.84         30       73.53       40.07       79       94.69       95.51         31       76.01       82.09       80       90.71       80.91         32       86.59       27.43       81       88.02       -10.88         33       52.34       69.35       82       87.05       1.073         34       35.94       67.87       83       88.22       86.107         35       75.47       10.06       84       83.93       22.25         36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89       60.36       91.14         41       86.55       90       90						
28       62.2       64.43       77       74.25       97.09         29       40.46       82.69       78       95.6       94.84         30       73.53       40.07       79       94.69       95.51         31       76.01       82.09       80       90.71       80.91         32       86.59       27.43       81       88.02       -10.88         33       52.34       69.35       82       87.05       1.073         34       35.94       67.87       83       88.22       86.18         35       75.47       10.06       84       83.93       22.25         36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89       60.36       91.14         41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.						
29       40.46       82.69       78       95.6       94.84         30       73.53       40.07       79       94.69       95.51         31       76.01       82.09       80       90.71       80.91         32       86.59       27.43       81       88.02       -10.88         33       52.34       69.35       82       87.05       1.073         34       35.94       67.87       83       88.22       86.18         35       75.47       10.06       84       83.93       22.25         36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89       60.36       91.14         41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.53       50.08         43       87.51       -22.67       92       1						
30       73.53       40.07       79       94.69       95.51         31       76.01       82.09       80       90.71       80.91         32       86.59       27.43       81       88.02       -10.88         33       52.34       69.35       82       87.05       1.073         34       35.94       67.87       83       88.22       86.18         35       75.47       10.06       84       83.93       22.25         36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89       60.36       91.14         41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.53       50.08         43       87.51       -22.67       92       17.69       98.21         44       60.98       29.8       93       7						
31       76.01       82.09       80       90.71       80.91         32       86.59       27.43       81       88.02       -10.88         33       52.34       69.35       82       87.05       1.073         34       35.94       67.87       83       88.22       86.18         35       75.47       10.06       84       83.93       22.25         36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89       60.36       91.14         41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.53       50.08         43       87.51       -22.67       92       17.69       98.21         44       60.98       29.8       93       74.66       77.69         45       69.44       30.08       94       9						
32       86.59       27.43       81       88.02       -10.88         33       52.34       69.35       82       87.05       1.073         34       35.94       67.87       83       88.22       86.18         35       75.47       10.06       84       83.93       22.25         36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89       60.36       91.14         41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.53       50.08         43       87.51       -22.67       92       17.69       98.21         44       60.98       29.8       93       74.66       77.69         45       69.44       30.08       94       96.22       43.89         46       59.78       37.37       95       8						
33       52.34       69.35       82       87.05       1.073         34       35.94       67.87       83       88.22       86.18         35       75.47       10.06       84       83.93       22.25         36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89       60.36       91.14         41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.53       50.08         43       87.51       -22.67       92       17.69       98.21         44       60.98       29.8       93       74.66       77.69         45       69.44       30.08       94       96.22       43.89         46       59.78       37.37       95       85.86       97.19         47       74.55       -8.885       96       6						
34       35.94       67.87       83       88.22       86.18         35       75.47       10.06       84       83.93       22.25         36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89       60.36       91.14         41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.53       50.08         43       87.51       -22.67       92       17.69       98.21         44       60.98       29.8       93       74.66       77.69         45       69.44       30.08       94       96.22       43.89         46       59.78       37.37       95       85.86       97.19         47       74.55       -8.885       96       64.74       87.62         48       91.36       37.2       97       63						
35       75.47       10.06       84       83.93       22.25         36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89       60.36       91.14         41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.53       50.08         43       87.51       -22.67       92       17.69       98.21         44       60.98       29.8       93       74.66       77.69         45       69.44       30.08       94       96.22       43.89         46       59.78       37.37       95       85.86       97.19         47       74.55       -8.885       96       64.74       87.62         48       91.36       37.2       97       63.06       45.44         98       89.1       91.90						
36       78.79       80.4       85       46.94       90.5         37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89       60.36       91.14         41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.53       50.08         43       87.51       -22.67       92       17.69       98.21         44       60.98       29.8       93       74.66       77.69         45       69.44       30.08       94       96.22       43.89         46       59.78       37.37       95       85.86       97.19         47       74.55       -8.885       96       64.74       87.62         48       91.36       37.2       97       63.06       45.44         98       89.1       91.90						
37       73.83       80.54       86       55.44       53.5         38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89       60.36       91.14         41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.53       50.08         43       87.51       -22.67       92       17.69       98.21         44       60.98       29.8       93       74.66       77.69         45       69.44       30.08       94       96.22       43.89         46       59.78       37.37       95       85.86       97.19         47       74.55       -8.885       96       64.74       87.62         48       91.36       37.2       97       63.06       45.44         98       89.1       91.90						
38       79.54       87.04       87       96.42       6.75         39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89       60.36       91.14         41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.53       50.08         43       87.51       -22.67       92       17.69       98.21         44       60.98       29.8       93       74.66       77.69         45       69.44       30.08       94       96.22       43.89         46       59.78       37.37       95       85.86       97.19         47       74.55       -8.885       96       64.74       87.62         48       91.36       37.2       97       63.06       45.44         98       89.1       91.90						
39       78.12       87.6       88       81.46       86.18         40       69.27       86.97       89       60.36       91.14         41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.53       50.08         43       87.51       -22.67       92       17.69       98.21         44       60.98       29.8       93       74.66       77.69         45       69.44       30.08       94       96.22       43.89         46       59.78       37.37       95       85.86       97.19         47       74.55       -8.885       96       64.74       87.62         48       91.36       37.2       97       63.06       45.44         98       89.1       91.92						
40       69.27       86.97       89       60.36       91.14         41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.53       50.08         43       87.51       -22.67       92       17.69       98.21         44       60.98       29.8       93       74.66       77.69         45       69.44       30.08       94       96.22       43.89         46       59.78       37.37       95       85.86       97.19         47       74.55       -8.885       96       64.74       87.62         48       91.36       37.2       97       63.06       45.44         98       89.1       91.92						
41       86.55       90       90       88       96.34         42       82.69       84.48       91       90.53       50.08         43       87.51       -22.67       92       17.69       98.21         44       60.98       29.8       93       74.66       77.69         45       69.44       30.08       94       96.22       43.89         46       59.78       37.37       95       85.86       97.19         47       74.55       -8.885       96       64.74       87.62         48       91.36       37.2       97       63.06       45.44         98       89.1       91.92						
42     82.69     84.48     91     90.53     50.08       43     87.51     -22.67     92     17.69     98.21       44     60.98     29.8     93     74.66     77.69       45     69.44     30.08     94     96.22     43.89       46     59.78     37.37     95     85.86     97.19       47     74.55     -8.885     96     64.74     87.62       48     91.36     37.2     97     63.06     45.44       98     89.1     91.92						
43 87.51 -22.67 92 17.69 98.21 44 60.98 29.8 93 74.66 77.69 45 69.44 30.08 94 96.22 43.89 46 59.78 37.37 95 85.86 97.19 47 74.55 -8.885 96 64.74 87.62 48 91.36 37.2 97 63.06 45.44						
44     60.98     29.8     93     74.66     77.69       45     69.44     30.08     94     96.22     43.89       46     59.78     37.37     95     85.86     97.19       47     74.55     -8.885     96     64.74     87.62       48     91.36     37.2     97     63.06     45.44       98     89.1     91.92						50.08
45 69.44 30.08 94 96.22 43.89 46 59.78 37.37 95 85.86 97.19 47 74.55 -8.885 96 64.74 87.62 48 91.36 37.2 97 63.06 45.44 98 89.1 91.92						
46     59.78     37.37     95     85.86     97.19       47     74.55     -8.885     96     64.74     87.62       48     91.36     37.2     97     63.06     45.44       98     89.1     91.92						77.69
47 74.55 -8.885 96 64.74 87.62 48 91.36 37.2 97 63.06 45.44 98 89.1 91.92						43.89
48 91.36 37.2 97 63.06 45.44 98 89.1 91.92						97.19
98 89.1 91.92						87.62
	48	91.36	37.2	_		45.44
00 00 00 00 00 00 00 00 00 00 00 00 00						91.92
99 93.05 18.74				99	93.65	18.74
100 78.85 72.93				100	78.85	72.93

#### 9.C. MATLAB Code

#### init

```
load yout_t_scale.mat
load yout_b_scale.mat
load yt_1_0_50_500.mat
load yb_2_0_50_500.mat
```

#### Generate NLHW Model with Sigmoid Network

```
close all
unitstart = 0; %parameters can be changed
unitend = 300;
cut1 = 200000;
cut2 = 200000+1200;
resultsize = 1 + unitend - unitstart;
results = [zeros(resultsize,3)];
for i = unitstart : unitend
   results(i,1) = i;
   Units = i;
   Fs = 1000;
   Ts = 1/Fs;
   % Define orders of linear block
   nb = 1;
   nf = 4;
   nk = 1;
   %data processing
    ysim = ysub 2.data';
    yb2 = yb_2(2,:);
   yexp = yb2;
   yexpcut = yexp(cut1:cut2);
    ysimcut = ysim(cut1:cut2);
    ysimcutma = movmean(ysimcut, 25);
    zbody = iddata(yexpcut',ysimcutma',Ts);
   zbody2 = iddata(yexp(cut1+100000:cut2+100000)',movmean(ysim(cut1+100000:cut2+100000),25)',Ts);
   % Estimate Hammerstein-Wiener Model
   hw01 = nlhw(zbody,[1 4 1],idSigmoidNetwork(i),idSigmoidNetwork(i)); %nonlinear blocks can be altered
    figure()
    subplot(2,1,1)
    compare(zbody,hw01)
    title('Estimation (Units = 500)')
    subplot(2,1,2)
   compare(zbody2,hw01);
   title('Validation (Units = 500)')
   %saving results
[x, fit, xx] = compare(zbody,hw01);
[x2, fit2, xx2] = compare(zbody2,hw01);
results(i,2) = fit;
results(i,3) = fit2;
end
```

# 9.D NLHW Spreadsheet Results (on next page)

Order Sigmoid	200000-2 validation		100000-10 validation -		100000-10 validation		100000-10 validation		200000-20 NL-L (one N		200000-20 L-NL (one i	
Unit	Est. Fit	Val. Fit	Est. Fit	Val. Fit	Est. Fit	Val. Fit	Est. Fit	Val. Fit	Est. Fit	Val. Fit	Est. Fit	Val. Fit
<del> </del>	1 11.18562	9.704693			4.673613	4.553886	4.673613	2.799906	27.19479	22.35191085		8.675294
		6.722862			4.612794	4.616601		2.100022	32.35568	25.15329169	8.808368	8.681789
	3 4.759349 4 3.232369				5.211038 2.223529	4.432286 2.087431	5.211038 2.223529		27.19494 27.45001	16.16693296 17.12433455		8.177790 7.888840
	5 4.139604				0.849574	0.927178	0.849574		28.0724	13.30485068	10.01987	8.589993
	6.35948	4.13363			8.037431	8.502533	8.037431	-0.38279	19.06002	4.384200699	10.71746	9.821705
	7 6.546593				4.804957	4.765183	4.804957		28.39295	11.74667004		7.984612
	8 1.020819				5.298468 0.604779	5.520166	5.298468 0.604779	-0.29213	25.53142	10.39056593		8.505692
		5.149393 1 6.631782			7.578578	0.617679 7.087371	7.578578	0.428676 -283167	27.80473 29.57855	14.74038629 18.73323859	10.5051 9.473097	9.608595 8.658669
		7.073967			6.281542	6.218705		0.028009	25.22147	11.9525509	9.727158	8.968004
	12 7.095562	4.682368			3.994997	3.019052	3.994997	-152.684	27.41212	12.08737646	9.538169	8.755091
		3 2.486133			2.087175	1.668779	2.087175	-2.30075	29.93878	17.85729778		9.527739
		3.330129 2.253662			8.859037 3.992746	8.709303 1.351759	8.859037 3.992746	0.296393 -26.0246	33.84072 27.85463	25.84667249 13.76111231	10.33608 10.59207	9.203060 9.359802
		8.517867			6.120569	5.447646	6.120569	-139507	34.3712	25.80027745	10.42573	9.309628
	17 10.52894	5.760782			11.71405	10.74892	11.71405	-11.4532	42.97245	26.74477676	10.06613	9.260831
		7.369493			9.271283	9.091901	9.271283	-13.9021	49.81643	31.16498676	10.2647	9.123323
		5.910526 7.196149			7.027528 8.194246	7.195536 7.827862		-200.557 -4.54454	28.06886 26.81334	16.2968308 14.26608541	10.62347 10.92341	9.599437 10.19605
		6.892343			7.511476	7.4714		-0.16664	31.95923	16.8215839		9.673270
		10.96866			1.346024	1.337529	1.346024	-0.69965	30.01978	16.00291849	11.0279	9.958727
		7.605862			6.561958	6.610248	6.561958	-1.41357	32.04405	17.93102228	10.5041	9.073656
		3 2.421944			9.529725	9.615291	9.529725	-6.01403	28.6301	16.81999784	10.97245	9.724315
	25 11.84487 26 9.688136	7 7.344525 8 8.04029			21.14632	31.80427 22.57964	31.24719 21.14632	-47384.2 -4.25658	48.69505 39.91996	39.91140467 26.25479089	10.85725 11.03898	9.04370 10.50085
		6.981622			6.147724	6.057551		-9.56545	33.84689	19.87425261	11.32385	9.420814
	28 11.6405	7.911189			7.606513		7.606513	-19680.4	56.14294	41.74244422	11.29525	9.59458
	29 13.78496				9.175218	8.399303	9.175218	-9.35801	40.72116	32.78027702		9.460006
	30 2.078329 31 8.353549				3.388028 5.012381	2.972598 5.096542	3.388028 5.012381	-1.63476 0.952656	40.31182 53.77839	28.2963651 42.3266797	11.10095 12.43281	10.29421 11.01453
		2.739532			5.076398	4.944076	5.076398		60.30165	43.6934502		9.804350
		8.006749			40.13107	39.67193	40.13107	-127894	43.10107	31.07014168	11.3027	10.00842
		1.718632			40.19178	40.43429	40.19178	-107.99	64.74094	43.68408306		10.31558
	35 9.522084	6.99107 7.625114			6.679378 6.140909	6.394339 5.59712	6.679378 6.140909	-0.31645 -862.542	49.16547 49.49853	35.69122484	11.33772 11.6481	10.27873
	36 11.51989 37 14.35349				5.212826	5.208424	5.212826	-0.55354	49.49853	33.47874111 43.74123551		10.23245 10.51360
	38 9.710965				0.385774	-0.0281	0.385774	-2.02716	54.48868	38.0922432		10.45153
		11.46915			63.00406	55.18424	63.00406		47.97965	34.81816971		10.14700
		6.205537			9.340775	8.90226	9.340775	0.442567	54.46103	38.30682103	12.16757	10.59439
		2 10.16829 L 6.375669			9.032312 8.196122	7.945801 8.646472		-2962.93 -3697.67	45.12724 55.15175	31.94590807 43.27313887	11.38588	9.830832
		2 11.51258			12.59771	12.74046		-4.9788	53.10738	39.61966155		10.03033
	44 13.11197	7 10.26719			10.91985	10.72155	10.91985	-201.751	47.00219	30.63294753	11.50394	10.47383
		4.32021					39.28968		48.52221	33.98647696		
		7 14.44373 2 6.306197				3.645118	3.416349 10.92434		68.56512 59.35798			
		3.041504					4.846121		56.49737	40.6619721		
		0.846811					48.33305		57.46189	42.35268596		
		16.12458				48.89299			60.98022			
		9.366104					62.38333		51.47054 72.39522	37.79401685 44.61031877		
		9.94513 3 2.835454					17.10383 14.25578		72.39522	44.61031877		
		9 19.43541					20.15425			44.9875711		
		6.012187					10.96127		73.34067	43.78094577		
		1.645072			21.84419		21.84419		63.38339			
		19.21147 4.583493					22.33543 45.75041		58.90337 59.4166	41.67192058 42.09919102		
		4.363493 3 10.27596				10.67457			60.07817	41.4533987		
		9.458891			67.58872	59.82081	67.58872		74.10957			
		11.26242			35.24233		35.24233		59.42065	41.44047281		
		19.72412					8.212297		63.26976	42.54743114		
	63 23.77376 64 26.18787	3 14.02821 7 15.8168				16.22418	16.27157 12.11098		65.62254 62.42855	43.37445318 43.29949913		
		9.248577					22.38543		58.43998	41.91312742		11.38998
		8.821057			18.22376	18.23302	18.22376	-5172.27	72.32689	45.35607823	12.84087	11.38466
		16.02759				50.72546			61.28735	41.46227879		11.34444
		9.971303					49.68856		73.10074			
		9.588124 3 11.00897					13.93787 69.61471		62.48733 75.9911	42.63283763 44.24748489		
		3 20.28902				15.31274		-2506.02		44.78437479		
	72 17.63107				9.303578		9.303578	-944.351		45.52598049		
		23.03759					12.71576		66.45936			
		18.34776					41.19835		64.71325	43.87623053		
	75 26.5167	7 17.08506			20.44483	49./5/35	56.44483	-276.146	66.5159	43.03249555	12.56243	10.64749

77	12.72121	7.073769			12.86623	12.78695	12.86623	-1683.95	64.36104	43.33359996	13.53046	11.3510142
78	79.07325	46.73977			27.74885	27.72955	27.74885	-50.7579	78.56486	46.16328472	14.0571	11.7525424
79	29.12801	20.62749			12.20055	11.63455	12.20055	-51.3079	66.43658	43.95787294	13.51249	11.815189
80	39.21182				68.54974	59.71986	68.54974	-126856	66.55634	44.2774087	13.59042	11.5660108
81	38.1588	22.09056			20.30341	19.62262	20.30341	-8.51448	64.67408	42.57662774	14.65576	12.3101986
82 83	25.11127 37.39391	21.3816			36.00237 45.04609	32.19595 45.76664	36.00237 45.04609	-875.822 -52.9513	76.26764 73.25221	45.02686189 44.89560809	13.38745 13.96931	11.7721191 12.0439444
84	41.10863	25.50421			-12.8489	-15.9877	-12.8489	-2438.34	67.69869	44.39483593	14.05911	12.0680633
85	41.98872				13.98015	13.3788	13.98015	-1230.08	66.28902	45.03869751	14.23428	12.7189085
86	30.79873	15.28111			23.63334	22.63328	23.63334	-402.366	78.00793	46.34856084	13.20063	11.4271157
87	56.30561				4.369836	2.965465	4.369836	-2812.56	69.0416	43.63224918	13.81079	11.8370981
88	42.90087	23.29207			52.09558	47.8078	52.09558	-103991	68.41358	44.46703098	14.15499	11.9923436
89 90	82.2882 66.90931	46.92563 37.57745			23.70726 14.40029	22.22993 13.44114	23.70726 14.40029	-15762.5 -1688	67.22624 68.78406	44.12177811 45.00839812	14.43503 13.77586	12.3286524 11.2742611
91	28.59099	16.08243			53.82509	47.32843	53.82509	-110317	69.88906	46.17038057	15.19209	12.5795224
92	36.41211	22.14961			15.91116	16.58981	15.91116	-776.65	69.85532	45.66050245	14.65545	11.7831329
93	30.89224	19.36206			32.98626	31.29333	32.98626	-631.013	69.72621	45.45026985	14.95049	12.9702731
94	34.64833	22.41779			20.34729	19.6954	20.34729	-3.16989	68.22988	45.2509677	14.87921	12.2359166
95	38.01647	21.51032			4.374659	2.770913	4.374659	-7.66928	69.80468	44.24871323	14.36048	12.0245955
96 97	77.48959 32.43866	44.13082 19.96298			34.9304 16.62204	32.90126 15.27292	34.9304 16.62204	-982.185 -8502.04	70.59813 69.97538	45.78324086 46.02685671	14.79891 15.32448	12.8008042 12.8353059
98	35.96414	25.09412				15.02586	16.86831	-7265.41	79.23298	47.27728989	14.33377	12.3018513
99	38.36669	24.37038			24.60496	24.27704	24.60496	-19958.2	81.39964	46.37093656	15.00129	12.8849895
100	40.8103	26.24749	48.23156	43.73456	48.23156	43.73456	48.23156	-98352.5	71.1875	44.70443668	14.42859	12.3294077
101	52.53371	32.03384	74.36403	64.66812	74.36403	64.66812	74.36403	-55950.5	71.19366		14.73391	11.8305317
102	85.32756	47.90149	60.64709	56.43211	60.64709	56.43211	60.64709	-25.2031	70.33429	46.49606024	14.62267	12.0793712
103 104	28.52282 47.15623	18.63149 27.71734	36.84109 30.11218	37.23656 27.71548	36.84109 30.11218	37.23656 27.71548	36.84109 30.11218	-5.90759 -26889	70.51351 72.1384	44.91906118 46.41612009	14.24526 15.59608	12.4166449 13.3255968
104	63.34661	40.35277	52.84147	52.06324	52.84147		52.84147	-20869	80.48083	47.30234152	14.98722	12.9188317
106	61.27964	38.82771	66.32802	60.43035	66.32802	60.43035	66.32802	-72.663	83.74726	46.82195817	14.35663	12.6980906
107	86.37081	49.70474	41.16706	39.85993	41.16706	39.85993	41.16706	-13.4011	82.65985	46.51608507	15.61897	12.8692966
108	53.48251	32.37764	71.77186	63.10136	71.77186	63.10136	71.77186	-31411.7	70.97447	44.42258009	14.60372	12.4756787
109	41.48983	27.22056	24.39247	23.06768	24.39247	23.06768	24.39247	-3158.46	75.41499	46.75478479	15.12269	12.4381529
110	41.93395	25.57148	24.05201	22.41153	24.05201	22.41153	24.05201	-44553.5	72.58891	45.40467229	15.47398	13.0014149
111 112	65.27955 32.00954	36.06045 20.80898	62.89742 57.33266	55.28553 54.67352	62.89742 57.33266	55.28553 54.67352	62.89742 57.33266	-58.134 -141.378	72.83586 72.0063	45.19132254 45.10638841	15.41651 14.76121	12.4877266 12.1758022
113	59.42851	41.39497	76.90511		76.90511		76.90511	-113483	70.36404		15.48272	12.9271568
114	62.52536	38.85529	14.34332	13.24375		13.24375	14.34332	-10.1487	73.00386	45.22640658	15.37445	13.1946658
115	86.59849	46.31574	18.72717	17.44492	18.72717	17.44492	18.72717	-246708	83.20355	45.71903627	15.50678	13.1225372
116	65.13457	40.71789	65.24315	58.1754	65.24315	58.1754	65.24315	-39.1126	75.56567	46.37351814	15.04309	12.2791635
117 118	44.59581 87.45632	27.54799 48.90295	64.1482 42.00776	56.50711 37.96701	64.1482 42.00776	56.50711 37.96701	64.1482 42.00776	-26.7934	84.24925 72.98487	47.59430732 46.43846809	16.59207 15.9594	14.0516858 13.1373286
119	47.28061	33.25048	49.84126	43.66626	49.84126	43.66626	49.84126	-1218.69 -387.24	79.5086		15.52743	12.1982525
120	72.1341	45.42849	64.77463	56.82623	64.77463	56.82623	64.77463	-9.86081	75.4306		14.89034	12.5495606
121	73.34293	47.62129	15.23847	14.77463	15.23847	14.77463	15.23847	-13244.9	75.55501	46.6153281	15.3112	13.0224791
122	67.54692	45.06234	29.801	28.92747	29.801	28.92747	29.801	-5731.53	75.44912	46.62129801	16.2877	13.5358496
123	78.40699	45.1287	79.1004			68.67924	79.1004	-100680	80.51168		15.62627	12.7409065
124 125		43.85936 32.93697	22.67721 58.55182		22.67721 58.55182	51.4315	58.55182	-27821.1 -94.3517	76.90531 81.84971	47.22810446 47.14349448		13.1771591 12.2422993
126	83.41139	47.62177	43.52949		43.52949		43.52949	-49.0487	79.56139	46.67633716		12.9794805
127	18.04163	13.49494	67.87956		67.87956	60.09878	67.87956	-43.9829	85.18047		16.13397	13.4902412
128	88.98327	48.61327	38.62455	37.00079	38.62455	37.00079	38.62455	-986.543	82.49592	48.34474539	16.6681	13.5304215
129	69.21991		68.4935	60.48205	68.4935	60.48205	68.4935	-9111.23	75.99868	46.40127481		13.1537562
130	48.7049	29.83724	17.40806	15.35365		15.35365	17.40806	-155.927	84.8096	47.48666499	16.75206	13.7719086
131 132	80.33248	44.8045 47.73729	64.89041 30.39995	58.4653 28.79993	64.89041 30.39995	58.4653 28.79993	64.89041 30.39995	-26.0783 -348.969	82.97461 81.21153	47.39412595 46.95526832	16.83505 16.73665	13.9150146 13.5213854
133		37.61561	74.90532		74.90532	66.6795	74.90532	-82669.4	84.06678	47.14596348	16.08585	13.4447391
134	83.14878	46.25248	50.38302		50.38302		50.38302	-18.7705	85.99466	46.91997685	15.94973	13.2811825
135	27.47475	17.84071	63.77663	55.22635	63.77663	55.22635	63.77663	-38779.4	82.41789	46.86966951	16.46716	13.7825479
136	87.40019	47.7374	65.90235	58.72457	65.90235	58.72457	65.90235	-137.738	83.90561	46.97628789	16.6828	13.6103666
137	0	0	0	0	0	0	0	0	77.05671	46.2109515	16.3147	13.0617657
138 139	89.24706 65.68339	47.32488 36.08869	53.50928 68.59868	49.12323 60.59487	53.50928 68.59868	49.12323	53.50928 68.59868	-1235.04 -4851.18	77.8577 81.49504	47.40835936 47.70655269	16.30368	13.2588703 13.056243
140	90.13628	49.17967	65.75982		65.75982		65.75982	-57.5891	84.81084	46.34670187		13.2939381
141	85.51715	46.25463	66.04168	58.81272		58.81272		-63.0882	85.20293	47.08039072	16.231	13.6073895
142	87.17255	49.05131	20.69087		20.69087		20.69087	-9322.06	79.37941	47.50400707		13.0372878
143		47.46502		32.36002		32.36002	33.59409	-8839.79	77.84058	47.25449463	16.34681	14.0764877
144	74.99839	40.4116		24.48302			28.00283	-8069.53	86.54502		17.02296	13.8420435
145 146	55.24118 90.01691	29.79923 49.13228		40.94909	64.25483 44.88786	40.94909	64.25483 44.88786	-26.2418 -8236.39	79.70378 79.19708	46.99907899 47.24907402	16.48234 18.27754	13.4327355 14.6766265
147	89.98058	48.90205		31.89768	33.13211		33.13211	-38901.1	77.70678	46.93107473	18.0875	14.5213818
148	89.38279	48.94698		61.38429	69.11776		69.11776	-59.5044	80.8005	47.96304588	17.66596	14.473484
149	89.33313	48.96162	26.30168	25.73676		25.73676	26.30168	-39247.5	84.74167	46.98182075	18.14441	14.3491406
150	87.48868	47.28	70.12576	61.7776	70.12576		70.12576	-53.7917	80.96847	47.41518931		13.6000652
151		48.02461		57.51125	65.51095		65.51095	-52.0382	78.5596	47.88574028	17.4307	13.6148809
152 153	71.79279 50.55301	40.00442 36.73039	52.958 36.15788	48.835 36.90258	52.958 36.15788	48.835 36.90258	52.958 36.15788	-44.7147 -1862.19	87.07285 81.23348	46.78169153 47.96039943	17.33022 17.72063	14.3172621 13.4916365
154		47.32617	65.5781	57.86753		57.86753	65.5781	-4266.88	86.2725	47.83959998	18.62395	14.8936658
155		28.21258			78.18317			-40392		47.16868669		14.8990613

156	86.10544	46.4484	41.37748	37.3856	41.37748	37.3856	41.37748	-43560	85.51515	47.66927399	18.34365	14.9331926
157	87.46103	46.72328	66.10473	58.19765	66.10473	58.19765	66.10473	-43360	80.11676	47.79101593	17.31666	14.9331920
158	70.38778	40.90957	38.24266	38.40273	38.24266	38.40273	38.24266	-149.763	80.21365	47.47340671	18.27324	14.4178803
159	89.58721	49.50423	20.47419	19.11177	20.47419	19.11177	20.47419	-3173.05	87.7708	47.44628044	19.91532	15.3293525
160	21.31125	13.47389	69.94939	61.12533	69.94939	61.12533	69.94939	-11959.6	87.6141	46.93725559	18.8432	14.7386044
161	89.84085	48.77443	66.61521	58.85465	66.61521	58.85465	66.61521	-237.458	86.73589	47.51423211	17.87857	13.7758572
162	75.54829	43.52123	66.7156	58.87231	66.7156	58.87231	66.7156	-265.575	88.42797	47.40620272	17.0483	13.7317911
163	86.57838	46.86907	23.93969	21.78598	23.93969	21.78598	23.93969	-986.652	83.6439	47.62041128	17.38097	13.6719353
164	89.10866	48.62197	67.59748	59.95865	67.59748	59.95865	67.59748	-58.9975	88.052	47.72457709	17.94418	14.5067829
165	5.777337	3.891817	68.27863	60.10412	68.27863	60.10412	68.27863	-79.2467	81.25323	47.72774735	18.95298	14.7777915
166	84.19291	45.42318	32.49292	31.67502	32.49292	31.67502	32.49292	-995.421	89.14634	47.40473175	19.14512	15.196231
167	86.41826 83.97883	46.65023 49.03787	40.675 37.10349	36.42122 33.60089	40.675 37.10349	36.42122 33.60089	40.675 37.10349	-20.9644 -17012.2	88.72458 88.83457	47.04779761 46.62722737	18.66086	14.9444985
168 169	90.91495	49.03787	23.10366	20.64671	23.10366	20.64671	23.10366	-934.427	81.42138	47.56844682	19.51176 17.8387	14.7602526 14.1218379
170	90.93033	48.53509	68.05118	61.79971	68.05118	61.79971	68.05118	-250.364	84.11368	47.64312202	18.95424	15.284237
171	83.38896	44.48138	57.30323	52.8395	57.30323	52.8395	57.30323	-238.819	82.13704	48.2222256	19.3199	15.3582735
172	0	0	0	0	0	0	0	0	82.37862	48.10231117	19.03767	15.07809
173	80.41207	45.51855	43.51405	40.76884	43.51405	40.76884	43.51405	-1216.52	88.51327	48.66075351	17.99105	14.8817654
174	85.96261	45.25211	42.44528	40.17354	42.44528	40.17354	42.44528	-1535.95	89.00303	47.17229415	18.62128	14.4487131
175	90.75204	47.09767	23.01554	21.46935	23.01554	21.46935	23.01554	-4996.97	83.01046	47.80103086	18.20224	14.417606
176	90.30022	47.32828	57.89516	51.79837	57.89516	51.79837	57.89516	-64.8158	89.61426	48.20197556	19.09474	15.3185517
177	86.77956	49.21935	46.07173	42.88067	46.07173	42.88067	46.07173	-58534.3	89.32907	48.29736535	19.12998	15.4509282
178	84.2859	49.23417	28.25199	27.86257	28.25199	27.86257	28.25199	-2355.7	89.83203	47.91012842	18.65901	14.6410861
179	88.46851	46.21184	84.43315	72.5038	84.43315	72.5038	84.43315	-4389.82	83.15084	47.97769331	18.11825	14.802552
180	88.83888	46.77735	31.27082	30.04616	31.27082	30.04616	31.27082	-4814.8	82.63521	47.60900906	20.02566	15.4304311
181	79.51804	42.74948	71.32927	62.80532	71.32927	62.80532	71.32927	-1859.15	82.9592	47.74204341	20.71465	16.1405766
182	90.55293	47.09096	71.38451	61.84378	71.38451	61.84378	71.38451	-90478.1	89.15931	47.84092273	19.35206	15.575473
183 184	35.74475 84.01889	23.89776 44.53832	76.67525 79.60798	67.22855 69.45918	76.67525 79.60798	67.22855 69.45918	76.67525 79.60798	-10252.9 -9971.15	83.24563 82.48053	47.88685535 47.66927402	20.62114	16.2773092 15.4967721
185	22.8359	16.96316	65.16566	56.83639	65.16566	56.83639	65.16566	-29.7897	89.65223	47.47538072	20.32234	15.4907721
186	90.07506	46.88578	20.73497	18.97904	20.73497	18.97904	20.73497	-381.712	84.97184	48.08037883	21.18886	15.9337821
187	85.9077	46.93495	70.19207	61.63369	70.19207	61.63369	70.19207	-32310.9	89.3402	48.09991049	20.73101	15.4619086
188	88.27313	46.02396	68.81522	61.20973	68.81522	61.20973	68.81522	-8.42412	89.66986	47.85648427	18.65667	14.667751
189	91.07984	49.29336	30.28079	28.82184	30.28079	28.82184	30.28079	-30995.7	84.6695	48.03945121	21.2942	16.2578052
190	75.78267	43.35269	65.6332	60.62612	65.6332	60.62612	65.6332	-213.417	83.12167	47.70704204	21.48679	16.6467152
191	90.57563	46.61927	28.80263	27.88351	28.80263	27.88351	28.80263	-1218.99	84.05081	47.83921719	19.0588	15.1812492
192	70.39002	39.3523	69.99404	61.45166	69.99404	61.45166	69.99404	-89.4675	84.44659	48.12575073	19.80308	15.4590927
193	88.70638	48.24527	71.24717	63.50189	71.24717	63.50189	71.24717	-450.425	89.71142	47.36199919	22.77902	17.4909407
194	79.2974	44.75719	29.1774	26.77763	29.1774	26.77763	29.1774	-7749.1	85.86363	48.12746557	22.28188	16.9814746
195	73.79635	40.89952	39.44194	36.87702	39.44194	36.87702	39.44194	-1129.96	88.98308	47.34187594	20.52922	14.7470694
196	90.02191	48.75191	21.32234	20.5685	21.32234	20.5685	21.32234	-10581.7	90.40655	47.96264093	20.50718	15.8421073
197	91.52512	48.94946 45.20556	70.00545	62.10735	70.00545	62.10735	70.00545	-2372.14	84.33479	47.94141127	20.34351	15.7183318
198 199	80.75704 87.00376	46.97914	25.11956 41.0032	23.78787 40.11359	25.11956 41.0032	23.78787 40.11359	25.11956 41.0032	-138.854 -4020.79	86.14479 87.28268	48.24167647 47.9841825	21.44345 20.76263	16.6171011 16.2516941
200	91.44355	48.34566	63.23558	57.17343	63.23558	57.17343	63.23558	-932.649	85.04823	48.08491206	19.52597	15.1483457
201	91.57798	49.28571	72.31395	64.15636	72.31395	64.15636	72.31395	-1051.64	85.83034	47.91728771	20.0182	15.4740277
202	51.51559	27.48111	46.38007	43.02229	46.38007	43.02229	46.38007	-70.0966	88.18754	47.94271156	21.55617	17.0293609
203	81.14333	46.28832		61.89254		61.89254	69.99018	-55.1293	90.40491	48.58451958		16.8241672
204					62.83136			-2894.73		48.26046796		
205	90.68845	47.15283	71.10269	62.17226	71.10269	62.17226	71.10269	-65.0095	85.82485	48.19465018	21.89201	16.6673669
206	0	0	0	0	0	0	0	0	0	0	21.29291	17.3520411
207	89.95735	46.61911	77.59172	66.67591	77.59172	66.67591	77.59172	-75062.5	89.58948	47.24944571	20.67812	16.5731585
208	91.67817	46.75971			55.53022		55.53022	-45.0494	90.50349	48.2487202	20.12938	15.2494317
209	78.41958				65.8512		65.8512		85.7857	48.1503812		
210					35.29302				90.45989	47.02481105		
211					32.33913				90.79862	48.79653346		
212		48.23739			29.38079			-539.777		48.16788363		
	81.34144			39.5274			41.90529		88.99274	48.34992838		17.022693
	78.43413							-128411		47.57312083 47.93394982		
	89.52778 30.29112			63.25953 10.9679	71.1046		71.1046 11.84725	-54.003	86.40836 86.62212	47.93394982		
	91.65666								86.22329	48.35039222		17.4115949
	54.11478								86.27869	48.18855691		
	22.15901								90.7404	47.9870932		16.495444
	91.42894								86.79132	48.26173283		
	91.48642								90.83662	47.3584549		
222	57.53303	42.34087	21.76387	20.72686	21.76387	20.72686	21.76387	-12900.5	91.03681	48.18885152	20.52658	16.5168017

223	92.21424	47.23603	69.74561	61.26924	69.74561	61.26924	69.74561	-45.0809	87.19248	48.20329596	21.33875	16.1109842
224	61.89369	42.66503	71.58612	62.82026	71.58612	62.82026	71.58612	-40.8489	90.54418	47.17552469	22.31637	16.8164817
225	91.84736	46.40948	69.52078	60.94318	69.52078	60.94318	69.52078	-45.5269	86.56601	48.28297662	20.77658	16.0554737
226 227	74.54473 87.60671	46.1189 47.26248	73.20308 27.58809	64.34779 26.44424	73.20308 27.58809	64.34779 26.44424	73.20308 27.58809	-53702.5 -6937.95	88.42512 88.82616	47.85888893 47.0172777	23.40899 22.85341	18.0020994 16.8560167
228	91.88467	47.10149	73.84876	64.87443	73.84876	64.87443	73.84876	-2672.48	87.70847	48.16998386	20.02198	15.0816472
229	22.4585	20.18213	31.02798	30.49995	31.02798	30.49995	31.02798	-79.4542	87.47446	48.24602694	20.81184	15.8500991
230	82.5761	48.22902	71.58925	61.8426	71.58925	61.8426	71.58925	-21900.3	87.66551	48.40793615	25.987	19.2577356
231	46.48015	34.61527	70.79353	62.6403	70.79353	62.6403	70.79353	-55.1517	91.07495	48.01963025	23.12992	16.8233443
232 233	91.89011 80.38042	47.45863 48.352	72.79702 50.59321	64.17624 46.90757	72.79702 50.59321	64.17624 46.90757	72.79702 50.59321	-48.0656 -517.145	87.03682 91.00004	48.27290661 47.72444323	25.53664 23.7313	18.6290363 17.5685474
234	89.5163	49.3493	34.28615	31.59734	34.28615	31.59734	34.28615	-331.193	87.68998	48.33242814	23.84032	18.2560339
235	88.93174	46.16326	27.416	26.7608	27.416	26.7608	27.416	-36.4754	88.49948	48.42522049	22.77664	17.6286819
236	90.99328	49.59909	24.04672	24.38395	24.04672	24.38395	24.04672	-15.2896	87.91156	48.21019184	26.26817	18.5325075
237 238	86.76204	47.93199	72.08086 79.42638	63.18757 68.58879	72.08086 79.42638	63.18757 68.58879	72.08086	-77.9697	87.95956 88.41354	48.48560932	25.94378 23.6965	19.3016425
239	23.29075 92.26159	18.12789 47.37492	46.30112	42.78356	46.30112	42.78356	79.42638 46.30112	-59.0757 -2471.5	87.71147	48.33621722 48.33990004	25.57442	18.0519893 18.3124122
240	93.12275	46.56373	50.23629	49.00901	50.23629	49.00901	50.23629	-13.6477	87.80861	48.33789002	23.90176	18.0318528
241	82.17194	40.57559	70.08947	61.00874	70.08947	61.00874	70.08947	-34.3203	87.31804	48.20218176	25.70969	19.1735949
242	58.81064	39.53423	49.24949	45.98181	49.24949	45.98181	49.24949	-944.41	87.33632	48.26862258	23.10456	16.8143998
243 244	87.50337 83.34353	47.79802 48.013	23.15585 70.90721	22.54403 62.19512	23.15585 70.90721	22.54403 62.19512	23.15585 70.90721	-2343.99 -46.1166	88.2248 87.44491	48.18367371 48.25954214	26.25912 22.13476	19.3695849 17.0166551
245	92.89321	47.97404	64.33683	58.97886	64.33683	58.97886	64.33683	-29.7509	88.06269	48.41514041	25.14387	19.0502321
246	92.16679	47.41501	67.55626	59.23995	67.55626	59.23995	67.55626	-4897.25	91.33337	48.27195475	24.2569	17.8390356
247	89.10831	46.2266	46.32746	42.75449	46.32746	42.75449	46.32746	-2493.53	87.74117	48.29872239	25.26755	18.3766619
248	1.593824	1.534543	29.06929	27.50034	29.06929	27.50034	29.06929	-41.7697	88.14748	48.2448144	24.66453	18.9454141
249 250	92.61713 69.9991	46.69179 43.59347	34.13997 49.09973	32.2607 43.16873	34.13997 49.09973	32.2607 43.16873	34.13997 49.09973	-818.122 -10549	91.02381 88.46475	47.76263202 48.369538	23.19664 21.39122	17.3338372 15.9577437
251	91.89654	48.61071	32.23077	30.82776	32.23077	30.82776	32.23077	-1062.29	88.56045	48.36837708	27.87273	19.2286671
252	66.83315	46.55304	69.1105	61.26597	69.1105	61.26597	69.1105	-650.128	87.98283	48.36221704	26.21402	18.8981747
253	92.04544	48.56197	32.69208	30.84216	32.69208	30.84216	32.69208	-17.4371	88.32308	48.40511154	25.58615	19.1902035
254	92.0897	46.73796	69.68398	63.59543	69.68398	63.59543	69.68398	-16.4388	88.22246	48.46192112	27.39232	19.0237438
255 256	10.79792 92.3779	7.749828 49.25237	31.24774 41.45396	30.48992 39.37306	31.24774 41.45396	30.48992 39.37306	31.24774 41.45396	-30578.9 -949.665	88.48874 88.81299	48.41399598 48.32112994	26.95463 27.51213	19.322548 19.6197617
257	81.41305	46.67035	23.51103	23.04522	23.51103	23.04522	23.51103	-696.128	91.35048	48.47649774	24.33586	16.770688
258	92.02164	46.86738	71.03678	62.97391	71.03678	62.97391	71.03678	-892.288	88.20953	48.42618981	27.61526	19.219235
259	92.05017	48.92917	72.51774	63.62864	72.51774	63.62864	72.51774	-56.5717	89.06375	48.53037237	23.20324	17.5141655
260	81.64265	45.85998	73.60992	64.78775	73.60992	64.78775	73.60992	-70.5494	88.6904	48.42924904	24.5879	17.947628
261 262	92.37286 91.30718	47.83382 47.31181	59.77327 71.41499	52.00869 63.39533	59.77327 71.41499	52.00869 63.39533	59.77327 71.41499	-16499.9 -519.277	88.88331 88.66345	48.43261984 48.41292825	25.44643 27.01382	18.4746679 19.5879637
263	71.46279	44.70669	71.92534	63.78738	71.92534	63.78738	71.92534	-74.053	89.22579	48.40435927	25.97765	19.0219736
264	92.06921	47.12819	50.91038	46.54842	50.91038	46.54842	50.91038	-3008.4	89.26892	48.40955965	30.3191	20.4966147
265	84.51961	49.54823	25.33567	24.05011	25.33567	24.05011	25.33567	-36.5669	91.44809	48.37016619	24.50421	18.2077602
266	92.22361	47.12499	72.39984	63.11787	72.39984	63.11787	72.39984	-55.6868	89.26	48.476981	26.00471	19.6447982
267 268	92.99785 90.88275	46.74205 47.45277	50.26118 29.62175	45.50978 29.82621	50.26118 29.62175	45.50978 29.82621	50.26118 29.62175	-742.71 -75.9936	89.06686 89.51172	48.33198542 48.46900223	25.10108 22.74515	18.7291121 16.4192355
269	92.15264	46.8793	72.77918	63.85968	72.77918	63.85968	72.77918	-48.7912	89.56285	48.46719826	27.39174	19.9372998
270	48.02358	27.19258	73.37203	64.51369		64.51369	73.37203	-70.1764	89.75362	48.56320347	27.15902	19.3097226
271			66.32215							48.52387387		19.0440792
272 273			73.27568 18.49972					-1105.85 -744.953	89.10386 91.44023	48.54730389 47.97229807	25.24374 25.6413	18.1749924 19.726661
273		46.99287			72.17267			-744.953	89.31652	48.32560407		19.7804628
275	0	0			0	0	0	0	0		30.33128	20.7949859
276	0	0			0	0	0	0	89.4848	48.41064664	25.5755	18.7002466
277	79.71159	43.383			41.86695		41.86695	-3672.5	89.26315	48.453371		20.2233231
278 279	84.71144 90.54755					65.72244 28.78577	75.74936 29.54326	-419.15 -1116.39	89.09177 89.46155	48.42810633 48.51324633		20.925317 20.3511333
280						41.29316	44.5085	-2358.84	89.57595	48.53897797		19.3527494
281		42.99015				42.28626		-32.6094	89.57903	48.58324515	27.3662	20.0242996
282		38.95717				62.39675	67.503	-2552.34	89.52646	48.54111539		20.4627723
283	89.12528 51.91215	46.93508				66.54042		-18494.1	89.30475	48.41556147		19.4672227
284 285		37.3151 48.23877				63.62047 69.52478	79.97083	-31.4798	89.81526 89.76496	48.38870949 48.26555412		19.8898666 20.9953167
286		27.08075			22.20537		22.20537	-14.8541		48.44663736		19.6405288
287	87.07165	44.67032			25.00775	25.08565	25.00775	-2145.98	89.75296	48.48653873	28.0797	19.2287933
288	63.59071	46.82983				64.02297		-705.556	89.78745	48.49191347		20.4094647
289		46.84446					75.88461	-2387.72	91.73463	48.35967028		21.5669129
290 291		48.40397 46.68814			34.84843 29.84381	33.7517 30.3661	34.84843 29.84381	-25449 -11.5064	90.12418 89.86359	48.4841958 48.47722337	28.0974 28.63251	20.1553501 20.7452705
292		47.00453					66.37541	-56.1357	91.7251	48.31243213		20.8268794
293		42.13232				30.59951	31.225		91.75884	48.45978254		22.836046
294		47.05186				21.32208		-389.676	90.2954	48.52804012		21.1796932
295 296		30.76559 46.92956				25.55393 67.29343		-4.96935 -396.33	91.31496 90.09833	48.30142792 48.4588368		21.3299543 18.0038251
296		32.15157					35.74587	-396.33		48.4588368		19.8149126
298	17.49762					23.44621		-32.7085		48.46495077		21.8368646
299	79.92932						69.21194	-35.3832	89.88668	48.54968763		21.9547814
300	92.1236	46.48281			34.00352	31.42012	34.00352	-350.669	90.30517	48.57142373	30.51209	22.4221556

1D Poly	Input & Ou	tput NL	Input NL		Output NL			Input NL		Combined NL	20	00000-200200		200000-20	00200
Degree	Est. Fit	Val. Fit		Val. Fit	Est. Fit	Val. Fit	Coefficient		Val. Fit	validation +100000		gmoid + 1D (2nd			egree) + Sigmoid
1		6.134677 5.793243	17.58735 32.84304	6.583075 26.88647	6.971999 6.818794		1 2	12.769431 12.720532				st. Fit Val. Fit 1.95885	-16.63296716	8 649583	Val. Fit 1.015544154
3		5.104862	16.52614	8.770419			3	12.663592				2.44965	-0.792015358		
4		5.104863		8.770419			4	12.470237				.324002	-16.07772168		
5 6		5.104863 5.104863	16.52614 16.52614	8.770419 8.770419			5 6	12.444627 12.589974				3.57555	-152517.2781 -8.643683094	8.977339 8.97936	
7		5.104863		8.770419			7	12.579445				9.99193	-21974.76074		
8	6.520807	5.104863	16.52614	8.770419	4.709876	4.612508	8	12.571535	6.110379		7 1	3.67075	-963339.0846	9.694163	1.363578952
9		5.104863	16.52614	8.770419		4.612508	9	12.565304				7.50491	-1338384.677		
10 11		5.104863 5.104863				4.6471 4.6471	10 11	12.713626 12.712202		1		26.0245 5.98085	-967116.6272 -2201.263018		
12		5.104863				4.6471	12	12.908815		1		.447307	-20.02122838		
13		5.104863	16.52614	8.770419		4.6471	13	12.909432		1:		6.62875	-13.48009212		
14	6.520807 6.520807	5.104863 5.104863	16.52614 16.52614	8.770419 8.770419		4.6471 4.6471	14	12.710293 12.70962		1:		1.73176 8.81416	-10.03677125		
15 16		5.104863				4.6471	15 16	12.708696		1-		19.7326	-135151.3113 -490157.8864		
17	6.520807	5.104863		8.770419		4.6471	17	12.905899		1		38.0165	-1.00557E+13		
18	6.520807	5.104863	16.52614	8.770419		4.6471	18	12.905088		1'		2.18213	-487.9232801		
19 20	6.520807 6.520807	5.104863 5.104863				4.6471 4.6471	19 20	12.707013 12.900974	6.38926	1:		7.15372 5.12876	-1416.05622 -745.0939967		
21	6.520807	5.104863				4.6471	21	12.900296	6.26674	2		14.6502	-117.3573597		
22	6.520807	5.104863		8.770419		4.6471	22	12.705211	6.388857	2		5.59171	-27883.85462		
23		5.104863	16.52614	8.770419		4.6471	23	12.704562		2		8.39936	-508.9900442		
24 25	6.520807 6.520807	5.104863 5.104863		8.770419 8.770419		4.6471 4.679009	24 25	12.89868 12.89829		2:		40.6018 4.41797	-1807.187829 -362.7879864		
26		5.104863	16.52614	8.770419			26	12.708061		2		8.24299	-117.7496976		
27	6.520807	5.104863		8.770419			27	12.707718		2		0.46814	-37.58394167		
28 29	6.520807 6.520807	5.104863 5.104863	16.52614	8.770419 8.770419			28 29	12.707394 12.707074		2		3.53156 3.78409	-2761.678252 -2103.838512	11.0778 10.90059	
30	6.520807	5.104863		8.770419			30	12.707074		2		2.80187	-45.49216838	11.041	
31	6.520807	5.104863					31	12.901672		3		4.77517	-2568.980411		
32	6.520807	5.104863					32	12.901383		3		8.74166	-3306.309586		
33 34		5.104863 5.104863					33 34	12.901093 12.705738		3:		0.22508	-993.6714001 -16638.78315		
35		5.104863					35	12.705738		3.		1.59078	-9044.578492		
36	6.520807	5.104863					36	12.90037	6.266774	3.	5 3	2.99502	-797.6106506	11.53894	
37	6.520807	5.104863					37	12.901722		3		5.22343	-169.1458266		
38 39	6.520807 6.520807	5.104863 5.104863					38 39	12.706318 12.901342		3		9.29451 1.15886	-1374.040199 -1994.478389	11.75674	
40	6.520807	5.104863					40	12.705935		3		8.00018	-2107.278931		
41	6.520807	5.104863					41	12.900969	6.266908	4	0	58.4714	-1283.066529	11.89427	-1.547950344
42		5.104863					42	12.705873		4		9.13573	-4940.344605		
43 44	6.520807 6.520807	5.104863 5.104863					43 44	12.705707 12.705543		4: 4:		9.96065 6.72365	-346.2605277 -184.9610373		
45	6.520807	5.104863					45	12.900616		4		1.27976	-135.5636591		
46	6.520807	5.104863					46	12.900505	6.266808	4	5 4	6.95886	-2494.636346	12.42674	-225566.6599
47	6.520807	5.104863					47	12.705106		4		0.31654	-182.1195927	11.6116	
48 49	6.520807 6.520807	5.104863 5.104863					48 49	12.704962 12.704824		4' 4:		6.11933 4.53536	-357.3649999 -1545.408439	12.2262 11.24849	
50		5.104863					50	12.900022		4		9.75055	-373.6514815	12.4425	
51		5.104863					51	12.899887		5		3.92722	-97.732236		
52 53		5.104863 5.104863					52 53	12.704516 12.704394		5 5:		7.00497 6.79621	-385.461878 -3768.789884		
54							54	12.899635		5:		9.49835	-222.6995537		
55	6.520807	5.104863					55	12.8994	6.266569	5-	4 5	6.72968	-105.7542913	12.59025	-1.71804762
	6.520807						56	12.899362				4.22474	-188.8559114		
57 58		5.104863					57 58	12.703965 12.703859		5		2.51472 8.96875	-6887.330946 -330.5560453		
59		5.104863					59	12.703755		5		6.47432	-13614.69022		
60							60	12.703662		5		0.95621	-1179.463351		
61		5.104863					61	12.898977		6		9.55933	-7734.732891		
62 63							62 63	12.898882 12.899345		6 6:		62.5026 1.83619	-1506.416799 -22268.78274		
64	6.520807	5.104863					64	12.703976	6.389128	6	3 6	2.00428	-640.621853	13.13102	-5.4117335
65							65 66	12.899326		6		9.53469	-132.9599638		
66 67	6.520807 6.520807						66 67	12.703834 12.899183		6: 6:		8.62973 6.31975	-19218.87736 -125413586.8		
68		5.104863					68	12.899125		6		4.26401	-3571.915291		
69							69	12.703608		6		8.99399	-1153.092679		
70 71		5.104863 5.104863					70 71	12.703537 12.703465		6: 7:		4.95645 4.18934	-769.487591 -662.2573268		
71		5.104863					71	12.703465		7		6.19883	-6811.349223		
73							73	12.703421		7:		8.52057	-605.8060188		
74		5.104863					74	12.898777		7: -		2.93285	-187.6978716		
75 76							75 76	12.703295 12.703232		7- 7:		1.10308	-6598.505167 -687.7879782		
70							77	12.703232		7:		0.50908	-6243.059231		
78	6.520807	5.104863					78	12.89854	6.266394	7'	7 5	2.74577	-5152.922194	13.26025	-9.918443793
79							79	12.703069		7:		62.2493	-4849.591141		
80 81		5.104863 5.104863					80 81	12.703016 12.898435		7: 8i		6.87209 8.85587	-5330.978715 -1798.669813		
82		5.104863					82	12.702936		8		5.64818	-1296.371043		
83	6.520807	5.104863					83	12.702887	6.388909	8:	2 6	5.13936	-1144.853599	13.31472	-3.967694376
84 85		5.104863					84 85	12.898153		8: 8.		4.51344	-1346.565081 -1086.455619		
85 86		5.104863					85 86	12.898287 12.702759		8-		0.55961 4.85834	-1086.455619 -2718.530113		
87	6.520807						87	12.898127		8		4.79755	-1204.173345		
88		5.104863					88	12.898136		8		9.42419	-996.1875474		
89 90		5.104863 5.104863					89 90	12.898138 12.898099		8:		9.51228 8.02179	-2941.929594 -804.2200706		
	6.520807						91	12.702771				1.37732	-1347.687475		
										-					

92	6.520807	5.104863	92		6.266317	91	66.60618	-194.6874323		-3.180786613
93	6.520807	5.104863	93	12.702698		92	69.41122	-672.7972514		-6.262092406
94	6.520807	5.104863	94	12.702662		93	70.06135	-13760.47717		-2.597538903
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98	6.520807	5.104863	98	12.702536		97	73.00446	-17349.65167	15.00222	-45.29346161
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106	6.520807	5.104863	106	12.89783		105	72.35875	-9626.770801	14.90724	-24.60901698
107	6.520807	5.104863	107	12.897805		106	37.26863	-65076.94651	14.58893	-30.69403584
108	6.520807	5.104863	108	12.897783	6.266242	107	71.79759	-19281.96718	15.19237	-26.55135668
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115	6.520807	5.104863	115	12.897553		114	73.99356	-28251.69402	14.77873	-16.57898022
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125	6.520807	5.104863	125	12.897394	6.26616	124	29.17482	-171512.2008	17.0357	-5.147969861
126	6.520807	5.104863	126	12.897382		125	37.80784	-150358.8363	16.56195	-13.14143829
127	6.520807	5.104863	127	12.897367		126	75.18953	-238733.9205	15.7353	-12.5644229
128	6.520807	5.104863	128	12.897511		127	76.49463	-22873.67517	18.00091	-33.99199569
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287	6.520807	5.104863	287	12.7031	6.38914	286	89.93818	-1350.583777	30.16021	-37.06617119
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295	6.520807	5.104863	295	12.703057	6.389132	294	90.32218	-998.4516358	31.34278	-69.41891023
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299	6.520807	5.104863	299	12.703044	6.389129	298	57.64407	-1662.017293	30.91103	-77.97842827
300	6.520807	5.104863	300	12.70304	6.389128	299	58.10575	-2765.739714	32.3142	-282.3446067

dation +100000 t	Sig	0000-200200 moid + 1D (2nd Degree) t. Fit	Val. Fit	200000-200200 1D( 2nd Degree) + Sigmoid Est. Fit V	al. Fit	Linear Piecewise Model validation +100000 Breakpoint	5		(2nd Degree)	Wavelet Network validation +100000 Units	200200-201200 Sigmoid + 1D (2nd De Est. Fit	gree) Val. Fit
	1	21.95885395	-16.633	8.649583083 1	1.015544	1		17.64502	7.395817692			8.9924
	2	12.44964797 7.324001792	-0.79202 -16.0777		1.247133 2.789558		_	29.29485 12.14479	8.26874878 5.868986727	:		
	4	13.57555426	-152517		0.20185			3.766683	-0.932368438			
	5	5.475423214	-8.64368	8.979360172 1	1.999149	5	5	12.60834	10.33059638		13.31319822	10.0370
	6	29.99193276	-21974.8		0.03803	_		25.58828	13.00393544	(		
	7 8	13.67075245	-963339 -1338385		1.363579	7	_	33.60655	19.09645935	-		
	9	17.50490547 26.02449982	-967117		L.120677 L.707149	9		9.674747	5.498973968 8.371192516	•		
	10	25.98085018	-2201.26		0.378748	10	-	0.864071	0.891359201	10		
	11	9.447307015	-20.0212		0.57937	11		20.97792	11.58367111	1:		
	12	16.62874594	-13.4801	9.985753372	-0.79369	12	2	7.988411	4.558344161	12	11.32128211	9.5144
	13	11.7317587	-10.0368		0.34386	13		18.71797	10.99991856	13	12.21788856	
	14	28.81416033	-135151		).272695	14		7.742108	6.442350153	14		
	15 16	19.73260307	-490158 -1E+13		-1.31758 -0.18201	15 16		13.07892 1.767495	8.323837515	15		
	17	38.0164981 12.18213485	-487.923		-0.16201 -0.29282	17	-	11.227	1.325569695 7.032855609	17		
	18	17.15372084	-1416.06		-10087.7	18	_	20.80807	12.01575619	18		
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	21	35.59170605	-27883.9	10.39916268 0	0.039806	21		13.88322	6.835544775	2:		
	22	18.39936134	-508.99		-0.74588	22		1.990581	2.102944658	22		
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	24 25	14.4179653 18.24299175	-362.788		-0.34214	24 25		6.880472	5.259222759	24		
	26	20.46813629	-117.75 -37.5839		-3.20424 -0.54524	26		5.22119 6.127153	5.126250033 2.868276502	26		
	27	23.53155808	-2761.68		-3.02872	27		6.574232	3.734465975	2		
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	42 43	29.96065493 36.72364952	-346.261 -184.961		-1.55119 -0.93992	42 43		0.905245 22.26291	-0.359225397 12.14265883	4:		
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	51 52	47.00497156 26.79621386	-385.462 -3768.79		-1.33796 -2.75091	51 52		4.783931 3.209044	3.731474458 3.153315872	5: 52		
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	83 84	34.51343563 60.55961059	-1346.57 -1086.46	13.7235122 13.88088369	-4.2397 -4.58229	83 84		1.926722 5.956437	2.088329513	83		
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105	70.05074010	0626 77	14.00724250	24.600	105	10 2001	12 4200447	105	12 20022761	10.7206000
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162	80.06897909	-1021.48	17.29659688	-74.7944	162	21.2047		162	13.29622761	10.7286089
163	81.33781159	-734.291	19.36654345	-68.1601	163	15.558		163	13.29622761	
164 165	81.55728867 44.15562693	-1459.32 -4315.11	18.16192885 21.54890547	-52.0881 -25.9883	164 165	6.512429 21.8346		164 165	13.29622761 13.29622761	
166	43.66840765	-2555.84	20.62790885	-39.1187	166	4.72762		166	13.29622761	10.7286089
167	61.37251651	-1535.8	19.79334289	-30.3916	167	10.7038	7.433656012	167	13.29622761	
168	81.31116658	-710.411	21.9921097	-11.2945	168	14.6254		168	13.29622761	
169 170	81.8719566 82.70083318	-1003.84 -1077.26	19.82973441 22.09113375	-6.68141 -21 5401		24.1881 5.08081		169 170	13.29622761 13.29622761	
171	82.31489855	-1005.77	19.88285592	-5.87255		14.3793		171	13.29622761	
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173	81.02344394	-1308.7	18.95208793	-9.18364	173			173		
174 175	83.42338102 83.7496061	-1078.89 -4445.66	20.42763982 19.42443448	-39.5745 -7.32667	174 175	15.867 7.13635		174 175	13.29622761 13.29622761	
176	58.45561635	-1081.68		-9.61599		6.88624		176		
177	83.35575118		21.10040673			2.54752		177	13.29622761	
178 179	55.65712421 83.58514069	-3449.35 -3649.71	20.71799567 18.93562153	-6.68256 -19.0767		7.95256		178 179	13.29622761 13.29622761	
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181	63.18885603	-1190.63	20.78111652	-30.2598		14.7191	2 12.46686976	181	13.29622761	10.7286089
182 183	83.82773867 57.86288593	-2098.32 -2711.71	19.85009595 21.34492011	-8.2451 -22 7776		20.59923 9.17426		182 183	13.29622761 13.29622761	
183	52.42846385	-6946.56	24.02695749			8.89009		183		
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186	54.69083738	-611.547	22.28683396	-9.86163		9.67084		186	13.29622761	
187 188	84.4074286 53.7107545	-727.455 -1893.78	22.26161707 19.8411575	-16.0497 -11.4004	187 188			187 188	13.29622761 13.29622761	
189	58.00216141	-514.24	24.4489807	-15.4032		3.25867		189	13.29622761	
190	54.68607185	-1507.97		-13.7149		10.8705		190		
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201 202	86.24625387 86.28225682	-2120.02 -2094.01	23.03739965 23.98962343	-70.9505 -83.8227		27.0049		201 202	13.29622761 13.29622761	
203	57.50110365	-1573	24.43728241	-100.044	203	9.86835	7.025017788	203	13.29622761	10.7286089
204				-104.382		10.7532		204		
205 206	86.2344025	-5343.16	0 24.45751308	-50.3883	205 206	17.5068	7 14.29612553	205 206		
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212	86.07420985	-7759.68	25.01008669	-112.973	212	8.4591	7.636538774	212	13.29622761	10 7286080
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225	51.40899599 52.42922458	-1491.24	23.2771064	-36,9302	224	10.85323	7.220199355	224		
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		-2381.33	30.91102961	-77.9784	297	8.31229	5.933333985	297	13.29622761	
	57.64406742		00.51102501	77.5764						10.7200009
298	57.64406742			-282 245		7 05072			13 20622764	10 7206000
	57.64406742 58.10575069 50.75338635	-2765.74 -2305.27	32.31420076 31.39862442	-282.345 -226.851	299 300	7.05072 8.175441	4.498499844 4.076311577	299 300	13.29622761 13.29622761	10.7286089

validation +100000 Upper Limit	Input	01200	200200-20 Output	1200	200200-20 Both	1200	Saturation validation +100000	200200- Both Blo		Deadzone validation +100000	200200 Both Bl
	Est. Fit	Val. Fit	Est. Fit	Val. Fit	Est. Fit	Val. Fit	Both Limits	Est. Fit	Val. Fit	Both Limits	Est. Fit
	1 6.834595 2 9.61593		6.834595 -3.70299	3.030762 -2.62463	6.834595 -3.70299	3.030762 -2.62463	1 2			1 2	13.950
	3 9.61593	3.564461	-3.70299	-2.62463	-3.70299	-2.62463	3			3	-20.35
	4 9.61593 5 9.61593			-2.62463 -2.62463		-2.62463 -2.62463	4 5		6 3.167037 5 3.910362	4 5	13.902 15.347
	6 9.61593	3.564461	-3.70299	-2.62463	-3.70299	-2.62463	6	17.3209	5.33922	6	-20.35
	7 9.61593 8 9.61593			-2.62463 -2.62463		-2.62463 -2.62463	7		8 3.65091 5 3.684447	7	15.386
	9 9.61593	3.564461	-3.70299	-2.62463	-3.70299	-2.62463	9	10.5117	4 3.376019	9	15.52
	10 9.61593 11 9.61593	3.564461 3.564461		-2.62463 -2.62463		-2.62463 -2.62463	10 11		1 3.736549 1 3.938789	10 11	15.342 15.301
1	12 9.61593	3.564461	-3.70299	-2.62463	-3.70299	-2.62463	12	9.89500	1 3.089269	12	-20.35
		3.564461 3.564461		-2.62463 -2.62463		-2.62463 -2.62463	13 14			13 14	15.534 15.353
1	15 9.61593	3.564461	-3.70299	-2.62463	-3.70299	-2.62463	15	8.32914	5 2.510818	15	15.137
		3.564461 3.564461		-2.62463 -2.62463		-2.62463 -2.62463	16 17		7 4.171932 1 2.886534	16 17	13.450 -20.35
1	18 9.61593	3.564461	-3.70299	-2.62463	-3.70299	-2.62463	18	9.87690	1 3.187912	18	15.550
		3.564461 3.564461		-2.62463 -2.62463		-2.62463 -2.62463	19 20			19 20	15.4 15.338
							21	8.06391	5 2.808796	21	15.30
Saturation validation +100000	200200-2 Input	01200	200200-20 Output	1200	200200-20 Both	1200	22 23			22 23	15.292 14.240
Lower Limit	Est. Fit	Val. Fit	Est. Fit	Val. Fit	Est. Fit	Val. Fit	24	14.8463	4.039992	24	-20.35
	1 6.834595 2 9.61593		18.52415 6.898387	6.134677 5.793243	6.834595 -3.70299	3.030762 -2.62463	25 26			25 26	15.526 15.554
	3 9.61593	3.564461	6.520805	5.104862	-3.70299	-2.62463	27	6.37872	3 3.293305	27	15.554
	4 9.61593 5 9.61593			5.104863 5.104863		-2.62463 -2.62463	28 29			28 29	15.285 15.474
	6 9.61593 7 9.61593		6.520807	5.104863	-3.70299	-2.62463	30 31	4.95956	2 2.351412	30 31	15.152
	7 9.61593 8 9.61593			5.104863 5.104863		-2.62463 -2.62463	31 32			31 32	14.705 13.426
	9 9.61593	3.564461	6.520807	5.104863	-3.70299	-2.62463	33	9.84964	3 3.202278	33	14.506
		3.564461 3.564461		5.104863 5.104863	-3.70299 -3.70299	-2.62463 -2.62463	34 35		5 2.60362 5 2.173018	34 35	-20.35 15.570
		3.564461 3.564461		5.104863 5.104863		-2.62463 -2.62463	36 37			36 37	15.604 15.613
		3.564461 3.564461		5.104863 5.104863	-3.70299	-2.62463 -2.62463	37 38	8.62000	3 2.894768	37 38	15.613 15.431
		3.564461 3.564461		5.104863 5.104863		-2.62463 -2.62463	39 40		7 2.613585 6 3.768287	39 40	15.481 15.338
1	17 9.61593	3.564461	6.520807	5.104863	-3.70299	-2.62463	41	9.35316	6 3.734263	41	14.8
		3.564461 3.564461		5.104863 5.104863		-2.62463 -2.62463	42 43		6 2.808793 4 2.476986	42 43	15.292 15.37
		3.564461		5.104863		-2.62463	44	5.45734	4 4.726015	44	15.282
Deadzone	200200-2	01200	200200-20	11200	200200-20	1200	45 46		9 2.700619 8 2.759969	45 46	15.463
validation +100000	Input		Output		Both		47	4.77133	2 2.904549	47	14.30
Upper Limit	Est. Fit 1 13.95084	Val. Fit 7.94392	Est. Fit 13.95084	Val. Fit 7.94392	Est. Fit 13.95084	Val. Fit 7.94392	48 49		2 2.680594 4 3.821015	48 49	-20.359 15.634
	2 14.81842	8.463161	14.96017	8.334507	15.65745	8.775967	50	9.26826	4 3.776556	50	15.53
		8.463161 8.463161					51 52		5 4.375724 4 3.195109	51 52	15.56 15.59
	5 14.81842						53	9.5790	9 3.922706	53	15.510
Deadzone	200200-2	01200	200200-20	1200	200200-20	1200	54 55		2 3.530265 1 4.178733	54 55	15.494
validation +100000	Input		Output		Both	14.1.50	56		5 2.141249	56	15.354
Lower Limit	Est. Fit 1 13.95084	Val. Fit 7.94392	Est. Fit 13.95084	Val. Fit 7.94392	Est. Fit 13.95084	Val. Fit 7.94392	57 58		3 2.43127 3 3.429003	57 58	15.426 15.531
		8.463161 8.463161		8.334507 8.334507			59 60			59 60	15.408
		8.463161					61			61	15.191
	5 14.81842	8.463161	14.96017	8.334507	15.65745	8.775967	62			62	14.705
								0.03650		62	
							63 64	10.5117	1 4.192129	63 64	14.777
								10.5117 9.27247	1 4.192129 3 4.034139		14.777 13.424 13.081
							64 65 66 67	10.5117 9.27247 6.91335 7.31254	1 4.192129 3 4.034139 5 2.989756 5 4.095954	64 65 66 67	14.777 13.424 13.081 14.154 13.298
							64 65 66	10.5117 9.27247 6.91335 7.31254 10.2428	4.192129 3 4.034139 5 2.989756 5 4.095954 5 3.7809	64 65 66	14.705 14.777 13.424 13.081 14.154 13.298 -20.35
							64 65 66 67 68 69 70	10.5117 9.27247 6.91335 7.31254 10.2428 4.44402 4.14494	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 3.7809 8 2.269772 6 2.164136	64 65 66 67 68 69 70	14.777 13.424 13.081 14.154 13.298 -20.35 15.607 15.638
							64 65 66 67 68 69 70 71	10.5117 9.27247 6.91335 7.31254 10.2428 4.44402 4.14494 10.0823	4.192129 3 4.034139 5 2.989756 5 4.095954 5 3.7809 8 2.269772	64 65 66 67 68 69	14.777 13.424 13.081 14.154 13.298 -20.35
							64 65 66 67 68 69 70 71 72 73	10.5117 9.27247 6.91335 7.31254 10.2428 4.44402 4.14494 10.0823 9.74094 7.2203	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 3.7809 8 2.269772 6 2.164136 8 3.689233 3 3.597664 4 3.182386	64 65 66 67 68 69 70 71 72 73	14.777 13.424 13.081 14.154 13.298 -20.35 15.607 15.638 15.664 15.689 15.473
							64 65 66 67 68 69 70 71 72 73 74	10.511. 9.2724. 6.9133. 7.31254. 10.2428. 4.4440. 4.14494. 10.0823. 9.74094. 7.2003. 7.40880.	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 3.7809 8 2.269772 6 2.164136 8 3.689233 3 3.597664 4 3.182386 7 3.433799 6 8.434971	64 65 66 67 68 69 70 71 72 73 74 75	14.777. 13.424. 13.081. 14.154. 13.29820.35. 15.607. 15.638. 15.664. 15.689. 15.473. 15.650. 15.45.
							64 66 67 68 69 70 71 72 73 74 75 76	10.511. 9.2724. 6.9133. 7.31254. 10.2428. 4.4440. 4.14494. 10.0823. 9.74094. 7.220. 7.40886. 19.7348. 11.9066.	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 3.7809 8 2.269772 6 2.164136 8 3.689233 3 3.597664 4 3.182386 7 3.433799	64 65 66 67 68 69 70 71 72 73	14.777 13.424 13.081 14.154 13.298 -20.35 15.607 15.638 15.664 15.689 15.473 15.650 15.45 15.363
							64 66 67 67 68 66 65 77 72 73 74 75 76	10.511; 9.2724; 6.9133; 7.31254; 10.2426; 4.4440; 4.1449; 10.082; 9.7429; 7.220; 7.4088; 19.7346; 11.906; 15.489; 6.8191;	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 3.7809 8 2.269772 6 2.164136 8 3.689233 3 3.597664 4 3.182386 7 3.433799 6 8.434971 9 5.446333 1 3.183447	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78	14.777. 13.424 13.081 14.154 13.298 -20.35 15.607 15.638 15.664 15.689 15.473 15.650 15.45 15.363 15.316
							64 66 67 68 68 70 71 72 73 74 75 77 77 78	10.511; 9.2724; 6.9133; 7.31254; 10.2428; 4.4440; 4.1449; 10.082; 9.74094; 7.220; 7.4088; 19.7348; 11.906( 15.4898; 6.8191; 5.3838;	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 4.095954 6 2.164136 8 3.689233 3 3.597664 4 3.182386 7 3.433799 6 8.434371 9 5.298939 5 5.446333	64 65 66 67 68 69 70 71 72 73 74 75 76	14.777 13.424 13.081 14.154 13.298 -20.35 15.607 15.638 15.664 15.473 15.650 15.45 15.363 15.316 15.482
							64 65 66 67 68 68 67 77 72 73 74 75 77 77 78 80	10.511; 9.2724; 6.9133; 7.3125; 10.2428; 4.4440; 4.1449; 10.082; 9.7409; 7.220; 7.4088; 11.906; 15.489; 6.8191; 6.8191; 5.383; 9.8288; 9.3255;	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 3.7809 6 2.164136 8 3.689233 3.597664 4 3.182386 7 3.433799 6 8.434971 9 5.29893 5 5.446333 1 3.183447 1 3.174887 4 3.685641 6 3.757101	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 80	14.777 13.424 13.081 14.154 13.298 -20.35 15.607 15.638 15.664 15.689 15.473 15.650 15.45 15.363 15.452 15.288 15.262 15.418
							64 65 66 66 66 65 71 72 73 74 75 76 76 76 88 88	10.511; 9.2724; 6.9133; 7.31254; 10.2428; 4.44400; 4.14494; 10.082; 9.74094; 7.220; 7.4088; 19.7348; 11.9060; 15.489; 6.8191; 5.3838; 9.8288; 9.3255; 9.72668;	1 4.192129 3 4.034139 5 2.999756 5 4.095954 5 3.7809 8 2.269772 6 2.164136 8 3.689233 4 3.182386 7 3.433799 6 8.434971 9 5.298939 5 5.446333 1 3.183447 1 3.183447 4 3.685641	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79	14.777 13.424 13.081 14.154 13.298 -20.35 15.607 15.638 15.669 15.473 15.650 15.45 15.336 15.45 15.288 15.288 15.262
							64 66 67 68 68 70 71 72 73 74 75 77 77 78 80 81 81 82 83 84	10.511; 9.2724; 6.9133; 7.31254; 10.242; 4.4440; 4.1449; 10.082; 9.74080; 19.734; 11.906; 15.488; 9.8288; 9.8288; 9.3255; 9.7266; 9.9216; 4.7648;	1 4.192129 35 2.989756 5 4.095954 5 2.089756 8 2.689772 6 2.164136 8 3.689233 3 3.597664 4 3.182386 7 3.433799 6 5.24933 1 3.183447 1 3.183447 1 3.183447 1 3.183644 1 3.685641 6 3.757101 3 3.663875 2 3.860824 4 2.0254435	64 65 66 67 68 69 70 71 72 73 73 74 75 76 77 78 80 80 81 82 83 83	14.777 13.424 13.081 14.154 13.298 -20.35 15.607 15.638 15.650 15.473 15.650 15.365 15.365 15.365 15.482 15.288 15.482 15.282 15.282 15.282 15.282 15.282 15.282 15.282
							64 66 67 66 68 69 71 71 72 73 74 75 76 76 88 81 83	10.5117 9.2724 6.9133 7.3125 10.2428 4.4440 4.1482 10.0822 9.7409 7.2207 7.4088 19.7348 11.906 15.4898 6.81917 5.3838 9.3255 9.7266 9.92160 4.7644 7.79124	1 4.192129 3 5 2.989756 5 4.099564 5 4.099564 6 2.164136 8 3.689233 3 3.597664 4 3.182386 6 8.434971 9 5.299939 5 5.446333 1 3.183447 1 3.174887 4 3.685641 6 3.657101 6 3.669875 2 3.660875	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 82 83	14.777 13.424 13.081 14.154 13.298 15.607 15.638 15.664 15.473 15.650 15.452 15.363 15.316 15.482 15.282 15.282 15.282 15.282 15.282 15.282 15.282 15.282 15.282 15.282 15.282 15.312
							64 65 66 66 66 70 73 73 74 75 76 76 88 88 88 88	10.5117 9.27241 6.91333 7.3125- 10.2428 4.44402 4.14494 10.0822 9.74094 7.2201 7.4088 19.7348 11.9060 15.4899 6.81917 5.3833 9.92566 9.92166 4.7644 7.79124 17.6225 6.7628	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 4.095954 6 2.164136 8 3.689233 3 3.97664 4 3.18236 7 3.433799 6 8.446333 1 3.182447 1 3.653641 6 3.757101 3 3.663875 2 3.860824 4 2.029435 6 6 3.919937 7 4 3.05612	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86	14.777 13.424 13.081 14.154 13.298 13.298 15.607 15.638 15.664 15.689 15.473 15.316 15.482 15.262 15.418 14.689 15.32 15.253 15.316 15.32 15.331
							64 65 66 66 66 66 71 71 72 73 74 75 76 76 80 81 81 82 83 84 85 86 86 86 86 86 86 86 86 86 86 86 86 86	10.5117 9.27247 10.2428 7.3125-5 10.2428 9.7409 7.220 9.7409 11.966 15.488 9.228 9.3255 9.3255 9.7266 6.7628 7.7912 17.6256 6.7628 8.7603	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 3.7809 8 2.69772 6 2.164136 8 3.69233 3 3.597664 4 3.182386 7 3.182386 1 3.182387 1 3.183447 1 3.174887 2 3.660541 6 3.757101 3 3.663575 2 3.660824 4 2.029435 6 7.20176 4 3.05012	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 82 83 84 85 86 87 88 88	14,777 13,424 13,081 14,154 13,298 -20,35 15,607 15,689 15,478 15,650 15,45 15,363 15,316 15,468 15,282 15,418 14,689 15,327 15,311 15,406 15,320 15,321 15,320 15,331
							64 65 66 66 66 66 77 71 72 73 74 75 76 80 81 81 83 84 88 88	10.5117 9.272421 10.242421 10.242421 10.08222 7.3125- 10.242421 10.08222 7.2002 7.40880 19.7342 9.82888 9.82888 9.92555 9.92666 7.79122 17.6556 6.6628 17.16556 6.66719	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 3.7809 8 2.269772 8 2.69772 8 2.69772 9 3.182389 1 3.182389 1 3.182389 1 3.182389 1 3.182381 1 3.182347 1 3.174887 1 3.174887 1 3.174887 2 3.865081 2 3.860824 4 2.029435 9 7.20176 4 3.05512 8 5.380354 2 4.480978 9 3.085482 2 4.480978	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 82 83 84 85 86 87 87 88	14,777 13.424 13.081 14.154 15.667 15.667 15.668 15.473 15.656 15.482 15.22 15.418 14.689 15.22 15.316 15.320 15.320 15.320 15.320
							64 68 66 66 66 70 71 72 73 74 75 76 76 81 81 83 88 86 86 87 88	10.5117 9.272427 10.24224 10.24224 10.04224 10.0627 7.4086 19.7482 9.3255 9.325 9.3255	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 4.095954 8 2.689772 8 2.689772 9 3.182386 8 3.689233 1 3.182386 1 3.182386 1 3.182386 1 3.182347 1 3.182447 1 3.174887 4 3.685641 6 3.757101 3 3.663875 2 3.860824 4 4.025913 6 7.0176 6 3.051937 6 7.0176 6 3.051937 6 3.050824 6 3.051937 6 3.050824 6 3.051937 6 3.050824 6 3.051937 6 3.050824 6 3.051937 6 3.050824 6 3.051937 6 3.050824 6 3.051937 7 3.050824 7 3.	64 65 66 67 68 69 70 71 71 72 73 74 75 76 77 78 80 81 81 82 82 83 84 85 86 87 87 88 89 99	14,777 13,424 13,081 14,154 13,298 -20,35 15,607 15,638 15,664 15,689 15,473 15,363 15,316 15,482 15,282 15,297 15,311 15,406 15,320 15,297 15,311 15,406 15,320 15,297 15,311 15,406
							64 65 66 66 66 66 70 71 72 73 74 75 76 77 76 80 81 83 84 85 86 87 88 88 88 88	10.5117. 9.2724.7 10.2428.7 10.2428.7 11.0.2628.7 10.2428.7 11.966.8	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 3.7809 8 2.269772 6 8 3.689233 3 .597664 4 3.182236 7 3.433799 6 8.443971 1 3.183487 1 3.183487 1 3.174887 1 3.185641 6 3.757101 3 3.663875 2 3.660824 6 2.029435 6 3.919937 9 7.20176 4 3.05612 2 3.680824 2 4.480978 9 3.085643 3 3.9905525	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 81 82 82 83 84 85 86 87 87 88 89 99	14.777 13.424 13.081 14.154 13.298 -20.35 15.607 15.638 15.664 15.689 15.45 15.316 15.482 15.288 15.282 15.281 15.481 14.689 15.32 15.311 15.406 15.314 14.778
							64 65 66 66 66 66 66 67 71 72 72 74 75 76 88 81 83 84 84 85 86 86 87 97 97 98 99 99 99 99 99 99 99 99 99 99 99 99	10.5117. 9.2724.71 10.2428. 11.2428. 11.2428. 12	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 4.095954 8 2.689772 8 2.689772 8 3.689233 3 3.689233 3 3.182386 6 3.434971 1 3.142487 1 3.142487 1 3.182346 6 3.767101 1 3.165347 2 3.6806875 2 3.6806875 2 3.6806875 2 3.6806875 2 3.6806875 2 3.6806875 2 3.680875 2 3.680875 3 3.369875 3 3.369875 3 3.369875 6 3.37798 1 1 3.245594 6 3.37798 1 1 3.245594	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 82 83 84 85 86 87 88 89 90 90 91 91 92 93	14.777 13.424 13.081 14.154 13.298 -20.35 15.667 15.638 15.664 15.689 15.565 15.438 15.316 15.438 15.316 15.428 15.328 15.328 15.328 15.328 15.328 15.328 15.328 15.328 15.328 15.328 15.328 15.328 15.328 15.328 15.328 15.328
							64 65 66 66 66 66 77 71 72 73 74 75 76 76 80 81 81 82 83 83 84 85 86 86 87 87 88 88 88 88 88 88 88 88 88 88 88	10.5111 6.9133 7.3125 4.44402 10.0822 9.7409 7.2202 11.092 9.725 9.325 9	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 4.095954 8 2.69772 6 2.164136 8 3.69233 3 3.597664 4 3.182386 6 3.434971 4 3.685641 6 3.757101 6 3.767101 6 3.767101 6 3.768564 6 3.919937 6 7.2017 6 3.06512 8 7.2017 6 3.06512 8 7.2017 6 3.065463 3 3.768253 3 7.682563 3 3.768256 6 3.37796 6 3.37796 6 3.37796 1 3.265544	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 82 83 84 85 86 87 88 89 90 91 91 92	14,777 13,424 13,081 14,154 13,288 -20,35 15,667 15,638 15,668 15,473 15,658 15,473 15,658 15,473 15,568 15,473 15,458 15,363 15,316 15,482 15,262 15,483 15,320 15,481 15,483 15,262 15,283 15,284 15,285 16,441 16,485 16
							64 66 66 66 66 66 66 66 66 66 66 66 66 6	10.51246 6.91333 7.31254 4.4440 10.0823 9.7409 11.9606 15.4898 9.8288 9.8288 9.8288 9.9216 17.6528 17.7512 17.6528 18.7612 18.7652 18.7612 18.7652 18.7612 18.7652 18.	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 4.095954 5 3.7809 8 2.269772 6 2.184303 3 3.597664 4 3.182236 7 3.432799 6 8.434971 9 5.29893 5 5.446333 1 3.597641 4 3.685641 6 3.639541 6 3.639541 6 3.639541 6 3.919935 6 4 3.990512 8 3 3.990525 3 3.795612 8 3.990525 6 3.37798 7 1.324594 7 1.324594 7 1.324594 7 2.525231 7 2.2455231 7 2.2455231	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98	14,777 13,424 13,281 14,154 13,282 -20,35 15,604 15,609 15,638 15,156 15,482 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15,282 15,288 15
							64 65 66 66 66 77 73 77 77 76 76 77 78 88 88 88 88 88 90 91 93 93 94 95 95 95 96 96 96 96 96 96 96 96 96 96 96 96 96	10.5111 6.9133 7.3125-6 10.0822 4.44403 10.0822 9.74099 11.906 15.4899 9.226 15.4899 9.226 16.581 17.625 17	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 4.095954 8 2.689772 8 2.689772 8 3.689233 3 3.182386 8 3.689233 1 3.182386 1 3.182386 1 3.182386 1 3.182347 1 3.183447 1 3.174887 4 3.085564 4 3.085564 3 3.095025 3 3 3.095025 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96	14,777 13,424 13,081 14,154 13,081 14,154 13,081 15,660 15,660 15,660 15,452 15,689 15,473 15,689 15,473 15,316 15,482 15,282 15,283 15,297 15,311 15,402 15,202 15,202 15,203 15,418 14,785 15,218 14,785 14,785 14,785 14,785 14,785 15,5716 15,716
							64 65 66 66 65 70 71 72 73 74 75 76 76 88 88 88 88 89 99 91 92 93 94 95 95 95 97 96 96 97 97 98 98 98 99 99 99 99 99 99 99 99 99 99	10.511/ 6.913333/ 7.3125-5 4.444020 10.08223 7.74099 9.74099 11.9061 15.4899 9.2265 9.2265 8.7603 8.7791 9.74099 9.7409 9.740	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 4.095954 8 2.289772 6 2.164136 8 3.689233 3 3.597684 4 3.182386 6 3.787101 6 3.7680624 6 3.7680624 6 3.7680624 6 3.7680624 6 3.7680624 6 3.7780625 7 6.7680624 7 2.7680624	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 82 83 84 85 86 87 88 89 90 91 91 92 93 94 95 96 99 99 99 99	14,777 13,424 13,081 14,154 13,081 14,154 13,081 15,660 15,660 15,660 15,45 15,660 15,45 15,680 15,45 15,316 15,482 15,282 15,418 14,689 15,262 15,418 14,689 15,262 15,218 15,262 15,218 15,218 15,218 15,218 15,220 15,20 15
							64 65 66 66 66 66 77 71 72 73 74 75 76 83 84 84 85 86 86 87 99 99 99 99 99 99 99	10.5112   10.512   10	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 3.7809 8 2.269772 6 2.164138 3 3.689233 3 3.597664 4 3.182386 7 3.433799 6 5.298939 5 1 3.182346 6 3.757101 1 3.174887 4 3.685641 6 3.757101 2 3.860824 6 2.029435 6 3.757101 3 1.56412 8 7.20176 6 3.37798 1 7.20176 6 3.37798 1 3.24594 3 2.305233 3 3.718354 3 3.37798 3 3 3.78354 3 2 3.555231 6 2 3.555231 6 2 3.555231 6 2 3.555231 6 2 3.555231 6 2 3.555231 6 2 3.555231 6 3 3.37798 6 2 3.555231 6 3 3.37798 7 2 3.555231 6 3 3.37483 8 3 3.535448 8 3 3.535448	64 65 66 67 68 69 70 71 72 73 74 75 78 79 80 81 82 83 84 85 86 87 88 89 90 90 91 92 93 94 95 96 97 98 99	14,777 13,424 13,081 14,154 13,081 14,154 13,081 14,154 15,690 15,638 15,660 15,463 15,363 15,316 15,473 15,650 15,473 15,565 15,473 15,565 15,473 15,565 15,473 15,565 15,473 15,565 15,473 15,565 15,473 15,565 15,473 15,481 14,178 14,125 15,202 15,202 15,202 15,202 15,203 15,141 14,778 14,125 15,562 15,115 15,481 15,566
							64 65 66 66 66 67 71 71 72 73 74 75 76 81 81 83 84 85 86 99 91 91 92 93 94 94 95 96 96 97 97 98 98 98 99 99 99 99 99 99 99 99 99 99	10.5112   10.512   10	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 4.095954 8 2.689772 8 2.689772 9 3.182386 8 3.689233 1 3.182386 1 3.182386 1 3.182386 1 3.182347 1 3.182347 1 3.182347 1 3.182347 1 3.182347 2 3.685641 3 3.695875 2 3.680924 2 4.69623 3 3.990525 3 3.718336 3 3.918336 3 3.918336 4 3.05512 2 4.480078 6 3.37798 6 3.37798 6 3.37984 7 3.28594 7 3.28594 7 3.28594 7 3.28594 7 4.28937 7 4.28937 7 4.28937 7 4.28937 7 5.238875 4 4.25934	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 81 82 83 84 85 86 87 87 88 89 90 91 92 93 94 95 96 99 99 99 99 99	14,777 13,424 13,081 14,154 13,288 15,607 15,638 15,664 15,689 15,473 15,650 15,45 15,363 15,316 15,423 15,520 15,288 15,288 15,282 15,202 15,200 15,418 14,689 15,323 15,218 14,778 14,219 15,218 14,135 15,202 15,200 15,418 14,778 15,502 15,203 15,203 15,204 15,205 15,206 15,207 15,208 15,
							64 66 66 66 66 66 66 67 71 72 72 74 75 76 77 76 81 81 82 83 84 84 85 86 97 91 94 94 95 96 96 97 97 98 99 99 99 99 99 99 99 99 99 99 99 99	10.5111/ 9.27244 6.9133346 6.9133347 6.91246 6.913347 6.91246 10.0822 9.740994 10.0822 9.740994 11.9060 11.549994 11.9060 9.32889 9.3255 9.32555 9.32555 17.6556 17.6556 18.76	1 4.192129 3 4.034139 5 2.989756 5 2.989756 5 3.7809 8 2.289772 6 2.161308 8 3.689233 3 3.597664 9 3.182386 1 3.182386 1 3.182386 1 3.182386 1 3.182386 1 3.183447 1 3.174887 2 3.680541 6 3.757101 3 3.663875 2 3.660824 4 2.029435 2 3.60824 6 3.9937 8 7.20176 4 3.05012 8 7.20176 4 3.05012 8 7.20176 6 3.37796 1 3.24594 3 3.63357 6 3.37796 1 3.24594 3 3.63353 3 3.633548 6 3.37796 1 3.24594 3 3.636353 3 3.633548 6 3.37796 1 3.24594 3 3.63635448 6 3.993168 7 7.286875	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 82 83 84 85 86 87 89 90 90 91 92 93 93 94 95 96 97 98 99 99 90 100 101 102	14,7777 13.424 13.081 14.154 13.298 -20.35 15.607 15.638 15.654 15.689 15.473 15.656 15.316 15.482 15.282 15.418 14.689 15.320 15.320 15.320 15.320 15.320
							64 65 66 66 66 66 66 67 77 77 78 76 76 88 81 83 84 84 85 96 97 97 99 99 96 99 99 90 90 90 90 90 90 90 90 90 90 90	10.5112   10.512   10	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 4.095954 8 2.269772 8 2.689772 8 2.689772 9 2.181433 1 3.182386 1 3.833799 1 2.20176 4 3.685641 6 3.7798 1 3.182347 2 3.860824 4 2.0259435 2 3.860824 4 2.0259435 2 3.860824 4 2.0259435 3 3.963875 2 3.860824 4 2.0259435 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.37798 1 3.24559 6 3.358531 6 3.358531 6 3.358584 6 3.358531 6 3.358584	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 81 82 83 84 85 86 86 87 87 89 90 91 91 92 92 93 94 95 96 97 97 98 98 99 90 101 102 103 104 104 105 105 105 105 105 105 105 105 105 105	14.777 13.424 13.081 14.154 15.638 15.667 15.638 15.673 15.658 15.473 15.658 15.311 15.452 15.311 15.452 15.311 15.452 15.311 15.452 15.311 15.452 15.311 15.452 15.311 15.452 15.311 15.452 15.311 15.452 15.311 15.452 15.311 15.452 15.311 15.452 15.311 15.452 15.311 15.452 15.311 15.452 15.311 15.453
							64 65 66 66 67 77 77 77 77 78 88 88 88 88 89 99 91 91 92 93 94 94 95 95 96 96 97 97 98 98 98 99 99 90 90 90 90 90 90 90 90 90 90 90	10.5111/ 9.272474 6.91338 7.31254 10.24224 11.2424 11.2424 12.	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 4.095954 5 2.589772 6 2.164136 8 3.689233 3 3.997684 6 3.78910 6 3.787101 6	64 65 66 67 68 69 70 71 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 88 89 90 91 91 92 93 94 95 95 96 97 98 99 99 90 91	14.777 13.424 13.081 14.154 15.693 15.693 15.693 15.693 15.693 15.693 15.693 15.693 15.693 15.693 15.693 15.693 15.693 15.693 15.693 15.492 15.292 15.293 15.293 15.293 15.293 15.293 15.293 15.293 15.293 15.293 15.293 15.293 15.293 15.293 15.293 15.293 15.293 15.293 15.594 15.595 15.593 15.594 15.595 15
							64 65 66 66 66 67 71 72 73 74 75 76 76 86 81 81 82 83 83 84 95 95 95 95 95 95 95 95 95 95 95 95 95	10.5111/ 9.27247/ 10.24224 10.24224 10.24224 11.2424 1	1 4.192129 3 4.034139 5 2.989756 5 2.989756 8 2.289772 8 2.289772 8 3.37990 8 3.432971 9 5.298939 3 3.633759 1 3.182347 4 3.685641 6 3.757101 6 3.757101 6 3.767101 6 3.767101 6 3.7685641 6 3.757101 6 3.7685641 6 3.76912 8 2.039032 1 3.183447 1 3.174887 2 3.660824 2 4.2029435 3 3.63375 6 3.30354 2 4.59633 3 3.63357 6 3.37796 1 3.24594 3 3.768275 6 3.37796 1 3.24594 3 3.636376 4 3.95316 7 2.286574 4 3.95316 4 3.95316 5 2.386224 4 4.255231 5 2.386244 4 4.255231 5 2.386244 4 4.255231 5 3.3685644 4 4.255231 5 3.3685644 4 4.255231 5 3.3685644 4 4.255231 5 3.3685644 5 4.25237 6 3.3685644 6 4.25237 6 3.368623 3 3.3686548 6 4.265231 6 3.37796 6 3.	64 65 66 67 68 69 70 71 72 73 74 75 78 79 80 81 82 83 84 85 86 87 88 89 90 91 91 92 93 94 95 96 97 97 98 99 90 100 101 102 103 104 105 106 106 107 107 108 109 109 109 109 109 109 109 109 109 109	14.777 13.424 13.081 14.154 15.607 15.638 15.667 15.638 15.667 15.638 15.636 15.45 15.638 15.316 15.45 15.288 15.228 15.32 15.316 15.418 14.689 15.32 15.316 15.418 14.689 15.32 15.520 15.5418 14.689 15.32 15.5418 14.585 15.528 15.538 15.538 15.538 15.538 15.538 15.538 15.538 15.538 15.538 15.538 15.538 15.538 15.538
							64 68 66 66 67 71 71 72 73 74 75 76 88 88 88 88 89 90 91 92 93 94 95 96 96 97 97 98 99 99 99 90 90 90 90 90 90 90 90 90 90	10.5111/ 9.272474 6.91338 7.3125-24 10.24224 10.0822 9.74099 11.9606 1	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 2.989772 6 2.164138 8 3.689233 3 3.1822386 7 3.433799 6 5.246433 1 3.1823447 1 3.174887 4 3.685641 4 2.02435 2 3.680924 4 2.02435 3 3.636376 3 3.036345 3 3.036345 3 3.036345 3 3.036345 3 3.036345 4 3.05612 6 3.37798 1 3.24594 3 3.056123 2 7.602875 6 3.37998 1 3.24594 3 3.056123 2 7.602875 6 3.37998 1 3.24594 3 3.056123 3 3.636346 4 2.25942 3 3.565231 4 3.95612 3 3.363548 3 3.363548 3 3.363548 3 3.363548 3 3.363548 3 3.363548 3 3.363548 3 3.363548 3 3.363548 3 4.527273 4 3.555231 3 3.635483	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 82 83 84 85 86 87 87 88 89 90 91 91 92 93 94 95 96 97 97 98 99 99 99 99 90 100 101 101 102 103 104 105 105 105 105 105 105 105 105 105 105	14.777 13.424 13.081 14.154 15.607 15.607 15.638 15.669 15.45 15.638 15.45 15.320 15.45 15.320 15.45 15.320 15.45 15.282 15.320 15.41 15.282 15.320 15.45 15.320 15.45 15.320 15.45 15.320 15.45 15.320 15.45 15.525 15.526
							64 65 66 66 67 71 71 72 73 74 75 76 88 88 88 88 89 91 91 92 93 94 94 95 95 96 96 97 97 98 99 99 99 90 90 90 90 90 90 90 90 90 90	10.5112   10.512   10	1 4.192129 3 4.034139 5 2.989756 5 4.099554 5 4.099554 5 2.589772 6 2.164136 8 3.689233 3 3.597664 4 3.182386 6 3.787101	64 65 66 67 68 69 70 71 72 73 74 75 76 77 77 78 79 80 81 82 83 83 84 84 86 87 87 88 89 90 91 91 92 93 93 94 95 96 97 97 98 99 90 91 91 91 91 91 91 91 91 91 91 91 91 91	14.777 13.424 13.081 14.154 15.687 15.638 15.667 15.638 15.766 15.451 15.320 15.766 15.320 15.766 15.320 15.528 15.222 15.320 15.528
							64 65 66 66 66 66 66 66 66 66 66 66 66 66	10.5112   10.242	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 4.095954 5 3.7809 8 2.689772 6 2.164138 6 3.182386 7 3.433799 6 5.298939 1 3.182386 1 3.182386 1 3.182386 1 3.182386 1 3.182386 1 3.182387 1 3.182347 1 3.174887 1 3.174887 1 3.174887 2 3.685681 2 3.685687 2 3.860827 2 3.860828 2 4.2029435 2 3.685875 2 3.860828 3 3.693875 2 3.860828 3 3.718353 3 3.718353 3 3.718353 3 3.718353 3 3.718353 4 3.255231 4 3.255231 4 3.255231 5 2.355231 5 2.355531 5 2.36875 4 4.25394 2 4.596823 3 3.635488 3 7.26863 3 3.635488 3 3.635488 3 3.635488 3 3.635588 3 3.635888 3 5.755505 5 7.86511	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 82 83 84 85 86 87 87 89 90 91 91 92 92 92 92 93 94 95 96 99 90 101 102 102 103 104 105 105 106 106 107 107 108 108 109 109 109 109 109 109 109 109 109 109	14.174 13.081 14.154 13.081 14.154 15.630 15.630 15.630 15.650 15.45 15.630 15.418 15.620 15.418 15.288 15.297 15.316 15.428 15.297 15.317 15.288 15.297 15.317 15.318 15.297 15.318 15.297 15.318 15.297 15.318 15.297 15.318 15.297 15.318 15.297 15.318 15.297 15.318 15.520
							64 65 66 66 66 66 67 71 72 72 73 74 75 76 86 81 83 83 84 85 86 87 91 92 93 94 94 95 96 96 97 97 97 98 98 98 99 90 90 90 90 90 90 90 90 90 90 90 90	10.5112   10.412   10	1 4.192129 3 4.034139 5 2.989756 5 4.095954 5 2.989772 6 2.164138 6 2.164138 6 3.689233 3 3.1822386 7 3.433799 6 5.2464333 1 3.182346 6 3.757101 6 3.365367 1 3.183447 1 3.174887 4 3.685564 4 2.029433 2 7.60243 8 7.362534 2 4.40978 9 7.20176 4 3.95612 8 3.363548 1 3.363548 1 3.363548 2 4.40978 3 3.363548 1 3.24594 3 3.95183 2 7.60287 4 3.95612 3 3.363548 1 3.24594 3 3.363548 1 3.24594 3 3.363548 1 3.24594 3 3.363548 1 3.24594 3 3.363548 1 3.255231 2 7.60287 4 4.52727 3 3.363548 4 4.52727 4 4.52727 4 4.52727 5 7.526675 4 4.52727 4 4.52727 5 7.526675 4 4.52727 5 7.526675 4 4.52727 5 7.526675 5 7.526675 5 7.526675 5 7.576675 5 7.786751 5 7.576675 5 7.786751 5 7.786751	64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 80 81 82 83 84 85 86 87 88 89 90 91 91 92 93 93 94 95 96 96 97 97 98 99 100 101 102 103 104 105 105 105 105 105 105 105 105 105 105	14.772 13.424 13.081 14.154 15.638 15.607 15.638 15.638 15.638 15.658 15.451 15.638 15.545 15.316 15.452 15.316 15.452 15.316 15.452 15.316 15.452 15.316 15.452 15.316 15.458 15.552 15.316 15.458 15.552 15.558

120	9.624469	3.802848	120	15.23029	9.6355
121	15.97087	5.379818	121	12.82192	3.4555
122	2.332506	1.409961	122	15.38214	9.0845
123		2.626748	123	14.54042	8.6473
124	10.87828	4.405381	124	14.56003	8.7574
125	10.30733	3,284545	125	14.80397	7.9748
126		4.093885	126		
127		5.582296	127		
	9,439171			13.38756	
	17.90091		129	12.52154	
130		4.368571	130	12.7961	
	15.12012			14.34402	
132		4.224125		12.72898	
	18.65455			13.49748	
	6.843027		134	11.11847	
135			135		
	6.789497		136	-20.3597	
137	7.134513		137	15.62117	
	16.29746			15.65018	
			139		
	7.413569 6.694005			15.67576 15.69772	
	16.64865				
			141	15.71575	9.332
	8.650527			15.72984	
	7.839746			15.73889	
144				15.74292	
	13.68071			15.55409	
146			146	14.80176	
	16.01711			14.19267	
148				14.55599	
	15.28167			14.70153	
150	13.7229	6.774075	150	14.83958	9.9693
151	12.79887	4.896528	151	14.9691	9.9373
152	10.7568	4.820853	152	15.08387	9.8826
153	8.683568	3.124362	153	14.39481	9.9803
154	16.28403	5.244805	154	14.57489	9.9755
155	7.848326	3.83415	155	14.74285	9.9566
156	9.901088	4.021896	156	14.89738	9.9230
157	9.221153	4.015282	157	15.02472	9.8658
158	16.92408	9.100592	158	15.02321	9.7712
	15.57277			14.36437	
160	15.48968	8.075528	160	14.57054	9.8601
	15.45896		161		
	16.32689			13.98106	9.786
163		3.381889	163		
	10.34338		164	14.15095	
	12.53313		165	15.01207	
	9.824238			15.35991	
167	6.836198		167	15.33844	
	9.623915		167		
	8.804498		169 170		
	16.59906			15.33069	
	9.696334			15.50201	
172	8.283419		172	15.45926	
	12.17285		173		
	9.185701		174		
175	7.378257		175		
	10.27034			15.18266	
	15.12814		177	15.4046	
	9.325366			15.28019	
179	17.56538	5.943033	179	15.1481	9.5587

400				
	9.485372 10.87227		180 181	
	10.22398 9.990301			14.3
184	8.167986	3.809611	184	14.1
185 186	10.39925 9.567496	5.085486 3.456925		13.51
187	10.40682	3.490117		13.448
189	9.463978 9.8949	3.376734		14.277
	13.9351 17.06185		190 191	
192	9.837055	7.477594	192	-20.359
193 194	6.913146 13.67278		193 194	-20.359
195		7.926364		15.5726
	17.08212		197	
198	12.66587 16.93066	8.08498		15.4555 15.4868
200	15.96875	9.038068	200	15.56598
201 202	10.1452 18.79131	7.85403 7.954519		15.59293 15.61898
	9.447252 9.595365			15.64328 15.66737
205	10.70937	3.76426	205	15.68911
206 207	9.603465 9.67402	3.682494 3.597169		15.70900 15.7270
208	8.958281 6.682991	4.598699		15.74209
210	9.884526	3.79955		15.76281
211	9.94126 9.592936	3.533938	211	15.7684 15.52823
213	9.402459	3.613623	213	15.46441
	9.655149 9.654527	3.503771	215	15.51518 15.09454
216	9.86223	3.222359	216	14.3123
218	9.639683 9.643337	3.411741	217 218	14.6022
219 220	10.24642 9.635964	3.703578		14.73892 14.86064
221	9.422952	3.680081	221	14.98248
222 223	9.666649 9.615741	3.69552 3.712088	223	
224	9.68978	3.46893 3.489371	224	14.49524
226	14.59242	5.020964	226	14.79729
227	10.4926 9.634228	3.395636		14.9398
229	9.634209 9.487435	3.923257	229	14.38913
230 231	9.717744	3.678464	230 231	
232	9.59819 9.598213	3.627281	232	13.913 13.8304
234	8.373061	3.334267	234	13.1658
236	9.043356 9.704897	4.01504 3.489047	236	
237		3.402197	237	13.27273 13.34713
239	9.022371	3.871545	239	8.412003
240 241	9.696169 10.09708	3.48056 3.893555	240 241	12.95285 15.03971
242	9.355259 9.623231	3.719483	242	12.60655
244	10.29456	3.123205	243 244	11.98875
245 246	9.582752 9.700286	3.624918 3.801359		14.58451 14.52352
247	9.737122	3.532924 3.494761	247	14.58064
249	10.12398	3.899601	249	
250 251	11.06944 10.79532	3.981217	250 251	
252	10.04155	3.104617	252	14.74008
	9.805565 9.594983	3.694802	253 254	14.0268
255 256	9.66991	3.423566 3.364569	255	14.25237 13.34842
257	9.754551	3.325223	257	13.05686
258 259	9.736865 10.19182		259	
260		3.557622	260	
262	9.658581	3.529412	262	14.30812
	9.750214 9.684524		263 264	14.22678 13.43312
265	9.898976	4.73457 3.45986	265	14.37564
266 267	5.576709	3.008274	267	4.150081 12.96942
268 269	13.61371 5.944846		268 269	12.95338
270	14.63215	4.444944	270	-20.3597
271 272	10.54788	3.960001 3.708076	271 272	
273 274	15.78105	5.413944	273	
275	7.853138	4.303832	275	11.22568
276 277	9.816997 8.422279			11.30571 11.38565
278	14.28073	4.298717	278	11.46549
	10.03224	4.337528	280	11.54522 11.62481
281		3.418788	281	11.70421
283	9.100572	4.274907	283	11.86241
285	16.86776 9.53691	3.886789	285	11.94115 12.01959
286 287	10.03992	3.340596	286	12.09769
288	10.37529	3.425214	288	12.17542 12.25272
289 290	9.645957 15.26357	3.628066 5.15434	289	12.32955 10.54905
291	14.50874	7.810087	291	7.81853
292 293	10.28092 15.43037	3.402904 4.704159	293	7.958134 8.097462
294	16.01682	9.190826	294	6.122178
296		3.379195	296	
297	10.55707			8.021402 8.177056
100		J.200041		8.330512
	16.7839 11.33177			8.48474