



Physics based block preconditioning with sparse approximate inverses in MueLu

An application to beam solid interaction



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Overview

1. Goal & Motivation

Problem description

2. Schur-type block preconditioning in MueLu

Basic multigrid algorithm Building blocks in MueLu

3. Sparse Approximate Inverses

Sparsity pattern selection

4. Application

Weak scaling study Composite plate Reinforced concrete beam



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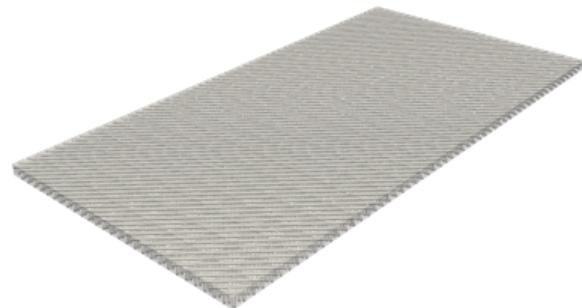
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Goal & Motivation

- Beam / Solid interactions occur in a wide variety of scenarios:
 - Engineering (steel-reinforced concrete, composite materials)
 - Biomechanics (collagen fibers in connective tissue)
- Time-to-solution dominated by cost for linear solver
 - Scalability through multilevel methods
 - Algebraic Multigrid (AMG) for its flexibility
 - **But:** Ill-conditioned matrix due to discretization and penalty regularization prohibit out-of-the-box block smoothing



Goal

Scalable AMG method for beam / solid interaction problems in penalty formulation



Problem description

The coupling of beam-like structures with solid continua is described with the following coupled linearized system for beam/solid interaction:

$$\begin{pmatrix} \mathbf{K}_S + \epsilon \mathbf{M}^T \kappa^{-1} \mathbf{M} & -\epsilon \mathbf{M}^T \kappa^{-1} \mathbf{D} \\ -\epsilon \mathbf{D}^T \kappa^{-1} \mathbf{M} & \mathbf{K}_B + \epsilon \mathbf{D}^T \kappa^{-1} \mathbf{D} \end{pmatrix} \begin{pmatrix} \Delta \mathbf{d}_S \\ \Delta \mathbf{d}_B \end{pmatrix} = - \begin{pmatrix} \mathbf{r}_S \\ \mathbf{r}_B \end{pmatrix}$$

Legend

$(.)_S$	solid contribution
$(.)_B$	beam contribution
\mathbf{d}	displacement DOFs
\mathbf{r}	residual
ϵ	penalty parameter
κ	scaling factor



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- **Solid DOFs**
- **Beam DOFs**
- **Coupling constraints**



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Challenges:

- Highly non-diagonal dominant and ill-conditioned block matrix due to penalty regularization
- Block matrix may be nonsymmetric due to beam formulation



Schur-type block preconditioning in MueLu

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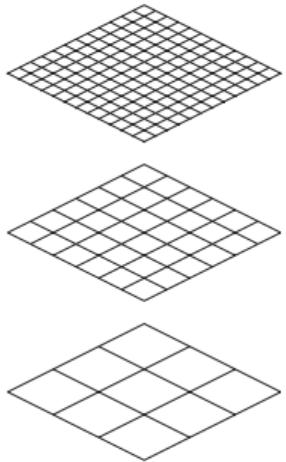
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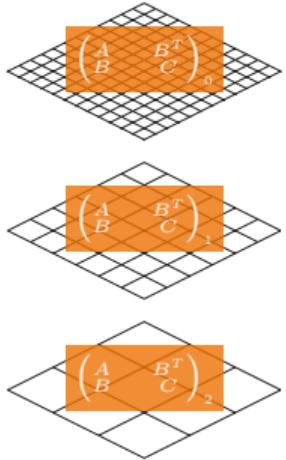
Basic multigrid algorithm



Basic ideas

- Attack different components of the error on different grids / levels.

Basic multigrid algorithm

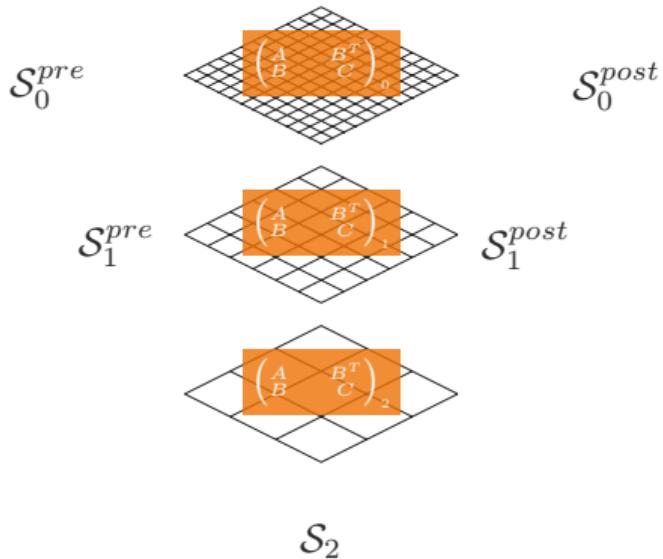


Basic ideas

- Attack different components of the error on different grids / levels.
- Reconstruct the fine level solution from information of coarse representations of the fine problem.



Basic multigrid algorithm

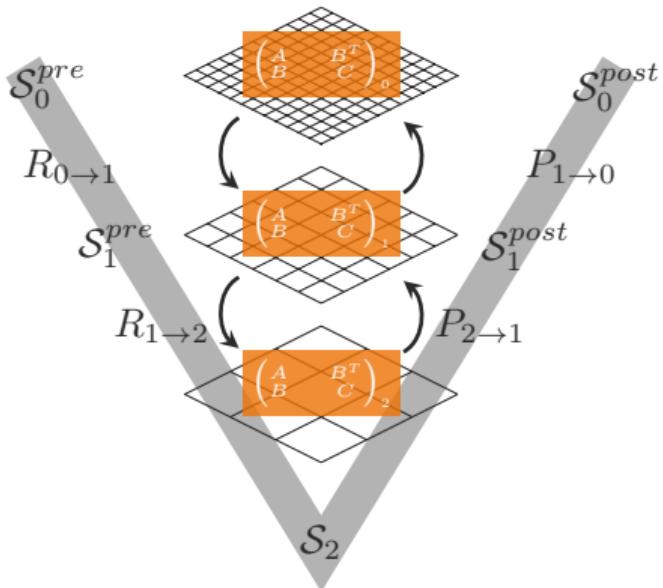


Basic ideas

- Attack different components of the error on different grids / levels.
- Reconstruct the fine level solution from information of coarse representations of the fine problem.
- Apply cheap **smoothers** on each multigrid level.



Basic multigrid algorithm



Basic ideas

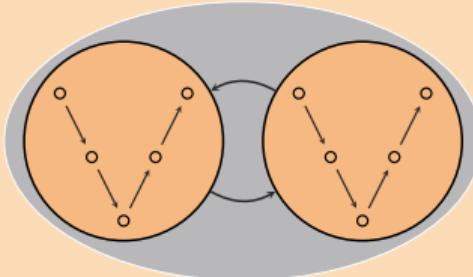
- Attack different components of the error on different grids / levels.
- Reconstruct the fine level solution from information of coarse representations of the fine problem.
- Apply cheap **smoothers** on each multigrid level.
- **Restriction** and **prolongation operators** transfer information between different multigrid levels.



Approximations in Schur complement preconditioners

1. Approximation $\hat{A} \approx A^{-1}$ to form Schur complement S
 - ⇒ Governed by the type of block method
 - ⇒ e.g. $\hat{A} := \text{diag}(A)^{-1}$
2. Approximate block inverses within Schur complement preconditioner by standard AMG
 - ⇒ Approximation quality can be controlled through the AMG settings

BlockMethod(AMG)¹



- Coupling constraints are considered on fine level only
- Block method can be:
 - ⇒ Block LU
 - ⇒ Uzawa
 - ⇒ SIMPLE

¹Wiesner, T. A.; Mayr, M.; Popp, A.; Gee, M. W. and Wall, W. A. (2021): "Algebraic multigrid methods for saddle point systems arising from mortar contact formulations", *Numerical Methods in Engineering*, 122, 15:3749-3779



Factory Layout



- Different Factories make up the Block-Smusher
- Can be specified with appropriate xml-file
- Several user-specific options



Sparse Approximate Inverses

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Sparse approximate inverse

Due to the penalty regularization using just a diagonal approximation of the inverse inside the Schur complement calculation is not sufficient:

- Sparse approximate inverse methods (SPAI²) can produce better approximation
- Use matrix graph of A to calculate inverse \hat{A} on this sparsity pattern
- Based on Frobenius norm minimization:

$$\min_{\hat{A} \in S} \|A\hat{A} - I\|_F$$

with S being the set of all sparse matrices with some known structure

Parallel computation

Decomposition into several least squares problems makes it inherently parallel:

$$\|A\hat{A} - I\|_F^2 = \sum_{k=1}^n \|(A\hat{A}_k - I)e_k\|_2^2,$$

for each row k solve

$$\min_{\hat{A}_k} \|A\hat{A}_k - e_k\|_2$$

with QR-decomposition

²Grothe, M. J. and Huckle, T. (1997): "Parallel preconditioning with sparse approximate inverses", *Journal Of Scientific Computing*, 18, 3:838-853



A priori pattern selection

Using just the pattern of A as input might not result in a satisfactory result, the matrix pattern needs to be enriched for a good sparse inverse approximation:

- Static approach by using recursive powers of graph of matrix $A \rightarrow$ recursion depth defined as level l
- Combining rows of graph $J(A)$ such that³:

$$J(A_k^l) = J(A_k^{l-1})J(A^{l-1})$$

- Pre- and post filtering of input graph and sparse inverse approximation with threshold value τ

SPAI with static pattern selection

1. Thresholding of $J(A)$
2. Determine graph of powers of A: $J(A^l)$
3. Calculate sparse inverse approximation \hat{A}
4. Post filtering of \hat{A}

³Chow E. (2001): "Parallel implementation and practical use of sparse approximate inverse preconditioners with a priori sparsity patterns", *The International Journal Of High Performance Computing Applications*, 15:56-74



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Solid block with random fiber placement



Settings

Discretization

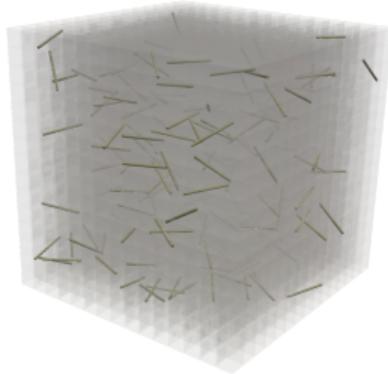
Solid DOFs: 27783
Beam DOFs: 1548
procs: 1

Solver

Newton convergence: 10^{-6} (rel)
GMRES convergence: 10^{-8} (rel)

Material Parameters

Solid: $E_S = 1 \frac{N}{m^2}, \nu_S = 0.3$
hyperelastic Saint Venant-Kirchhoff model
Beam: $E_B = 10 \frac{N}{m^2}, \nu_B = 0.0$
torsion-free Kirchhoff-Love model
Penalty: $p = 10 \frac{N}{m}$

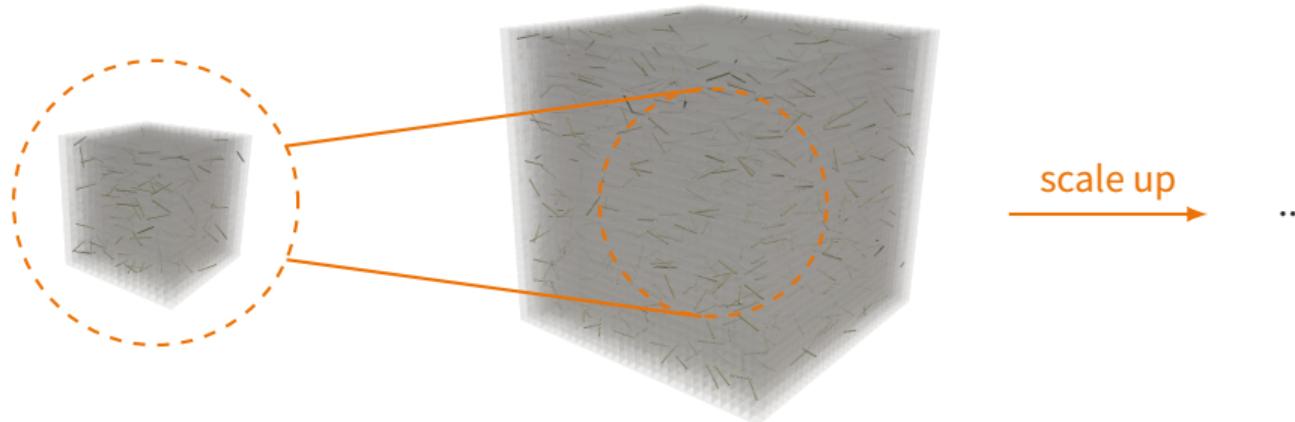


- minimal working problem to be used for weak scaling study
- bottom surface is fixed, tensile surface load on top side



Weak scaling study

Weak scaling study: Cube filled with randomly placed and oriented fibers.



$1 \times 1 \times 1$ domain

- ~ 25.000 Dofs
- 1 Processor

$2 \times 2 \times 2$ subdomains

- ~ 200.000 Dofs
- 8 Processors

$10 \times 10 \times 10$ subdomains

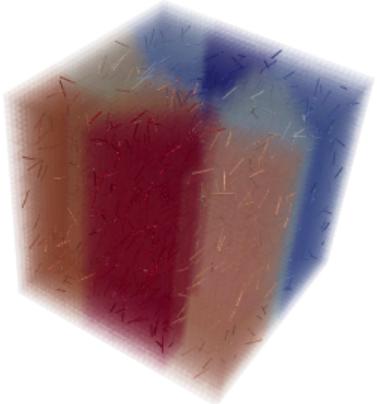
- $\sim 25.000.000$ Dofs
- 1000 Processors



Weak scaling study

Weak scaling hierarchy

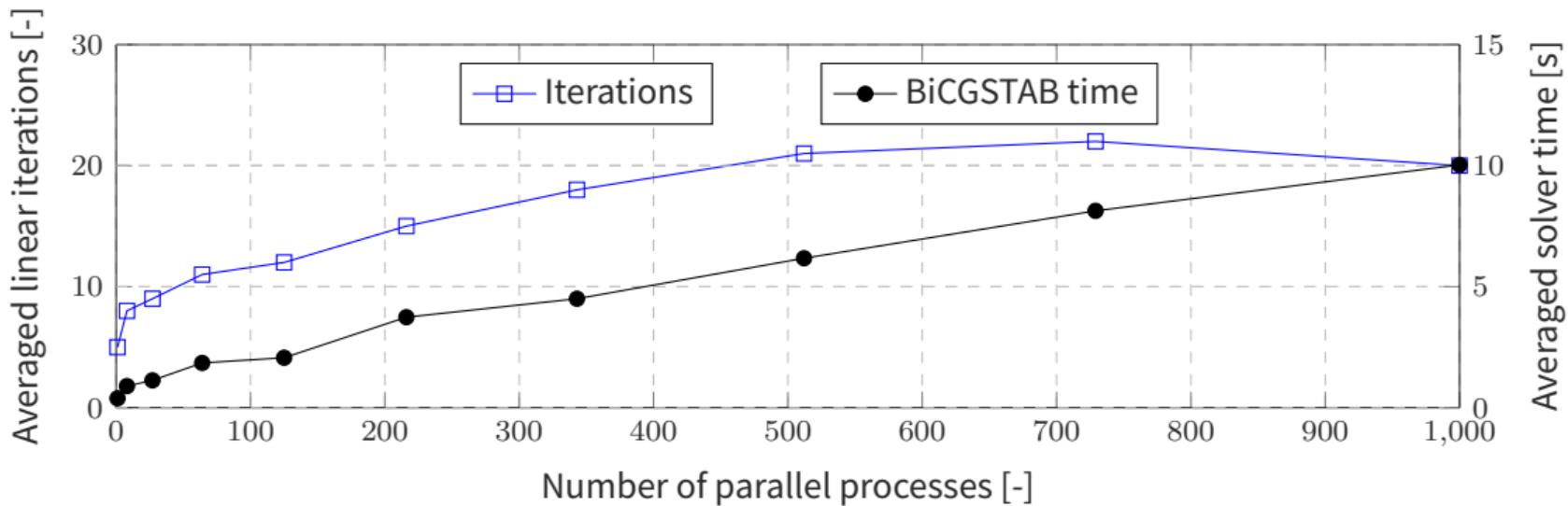
ID	n^{proc}	n_{DOF}^S	n_{DOF}^B	n_{DOF}^{total}	$n_{DOF/proc}^{total}$
1	1	27783	1548	29331	29331.0
2	8	206763	14544	221307	27663.4
3	27	680943	52188	733131	27153.0
4	64	1594323	124788	1719111	26861.1
5	125	3090903	247560	3338463	26707.7
6	216	5314683	432300	5746983	26606.4
7	343	8409663	688956	9098619	26526.6
8	512	12519843	1035876	13555719	26476.1
9	729	17789223	1484736	19273959	26438.9
10	1000	24361803	2037192	26398995	26399.0



*Domain decomposition approach
based on a geometric bisection
for $ID = 2$ with $n^{proc} = 8$*



Weak scaling study



Fiber-Reinforced Composite Plate⁴



Settings

Discretization

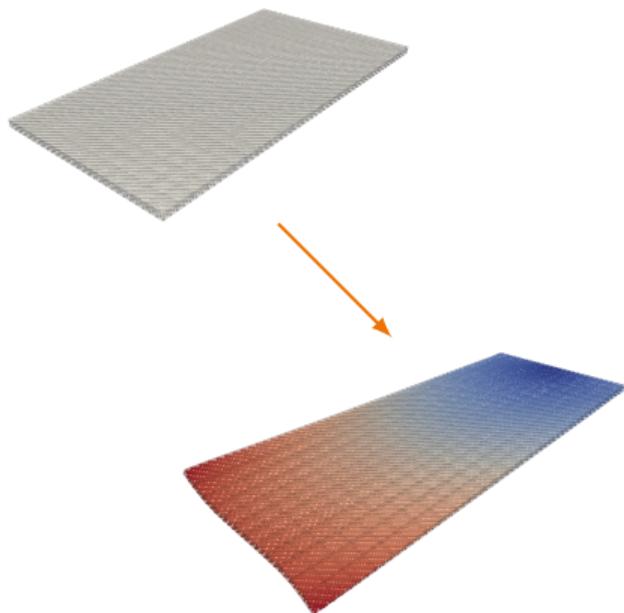
Solid DOFs: 1950
Beam DOFs: 10992
procs: 6

Solver

Newton convergence: 10^{-6} (rel)
BiCGSTAB convergence: 10^{-8} (rel)

Material Parameters

Solid: $E_S = 10 \frac{N}{m^2}, \nu_S = 0.3$
hyperelastic Saint Venant-Kirchhoff model
Beam: $E_B = 1000 \frac{N}{m^2}, \nu_B = 0.0$
torsion-free Kirchhoff-Love model
Penalty: $p = 1000 \frac{N}{m}$



Deformation of the plate due to tensile load

⁴Steinbrecher, I.; Mayr, M.; Grill, M. J.; Kremheller, J.; Meier, C. and Popp, A. (2020): "A mortar-type finite element approach for embedding 1D beams into 3D solid volumes", *Computational Mechanics*, 66:1377-1398

Steel-Reinforced Concrete Beam



Settings

Discretization

Solid DOFs: 5376
Beam DOFs: 1686
procs: 6

Solver

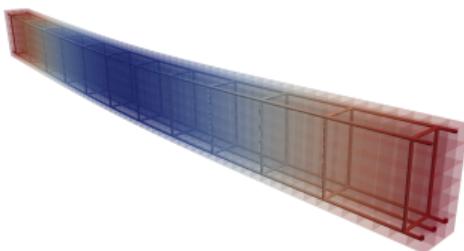
Newton convergence: 10^{-6} (rel)
BiCGSTAB convergence: 10^{-8} (rel)

Material Parameters

Solid: $E_S = 30 \frac{N}{m^2}, \nu_S = 0.3$
hyperelastic Saint Venant-Kirchhoff model
Beam: $E_B = 210 \frac{N}{m^2}, \nu_B = 0.0$
torsion-free Kirchhoff-Love model
Penalty: $p = 1000 \frac{N}{m}$



Four-point bending test under static loading⁵

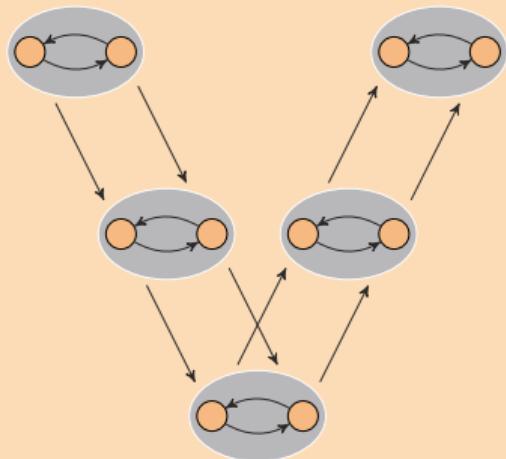


⁵Braml, T.; Wimmer, J. and Varabei, Y. (2022): "Erfordernisse an die Datenaufnahme und -verarbeitung zur Erzeugung von intelligenten Digitalen Zwillingen", Innsbrucker Bautage 2022 (eds Berger, J.) (Studia, 2022), 31-49



Outlook

AMG(BlockMethod)



- Consider coupling constraints on all levels
- Assembly of the beam DOFs nullspace specific to beam formulation

- For now only considered torsion-free Kirchhoff–Love beam elements:
 - ⇒ Sufficient for a broad range of applications
 - ⇒ Restriction to straight center line in reference configuration
- Extend to other beam formulations in the near future.



Thank you!

Collaborators:

- Matthias Mayr
- Alexander Popp
- Ivo Steinbrecher

References:

Open-source implementation will be available in

Trilinos/MueLu: <https://trilinos.github.io/muelu.html>



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