ECE 742 Final Project

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1 Theory

1.1 PML

Perfectly Matched Layer (PML) boundary conditions are absorbing boundary conditions. PML BCs decay the wave within a boundary layer at the edge of the simulation. The edge of the simulation BC can be implemented as PEC. Well-implemented PML BCs completely decay the wave from the time it enters the boundary layer to the time after it reflects and attempts to leave.

1.2 Finite-Difference Derivation

Let's start with equation:

$$\nabla \times \vec{H} = j\omega \epsilon \bar{s}\vec{E} \tag{1}$$

Evaluate the cross product and write in matrix form:

$$\begin{bmatrix} \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} \\ \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} \\ \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} \end{bmatrix} = j\omega\epsilon \begin{bmatrix} \frac{s_y s_z}{s_x} & 0 & 0 \\ 0 & \frac{s_x s_z}{s_y} & 0 \\ 0 & 0 & \frac{s_x s_y}{s_z} \end{bmatrix} \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix} (2)$$

Where the values in the second rank tensor can be described by:

$$s_x = \kappa_x + \frac{\sigma_x}{j\omega\epsilon_0} \tag{3}$$

$$s_y = \kappa_y + \frac{\sigma_y}{j\omega\epsilon_0} \tag{4}$$

$$s_z = \kappa_z + \frac{\sigma_z}{j\omega\epsilon_0} \tag{5}$$

To make the calculation computationally more managable, we can define the following relations:

$$D_x = \epsilon \frac{s_z}{s_x} E_x \tag{6}$$

$$D_y = \epsilon \frac{s_x}{s_y} E_y \tag{7}$$

$$D_z = \epsilon \frac{s_y}{s_z} E_z \tag{8}$$

such that now:

$$\begin{bmatrix} \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} \\ \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} \\ \frac{\partial H_y}{\partial x} - \frac{\partial H_z}{\partial y} \end{bmatrix} = j\omega \begin{bmatrix} s_y & 0 & 0 \\ 0 & s_z & 0 \\ 0 & 0 & s_x \end{bmatrix} \begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix}$$
(9)

Using the defined values of s and that $\frac{\partial}{\partial t} = j\omega$:

$$\begin{bmatrix} \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} \\ \frac{\partial H_x}{\partial x} - \frac{\partial H_z}{\partial x} \\ \frac{\partial H_y}{\partial x} - \frac{\partial H_z}{\partial y} \end{bmatrix} = \frac{\partial}{\partial t} \begin{bmatrix} \kappa_y & 0 & 0 \\ 0 & \kappa_z & 0 \\ 0 & 0 & \kappa_x \end{bmatrix} \begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix} + \frac{1}{\epsilon_0} \begin{bmatrix} \sigma_y & 0 & 0 \\ 0 & \sigma_z & 0 \\ 0 & 0 & \sigma_x \end{bmatrix} \begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix}$$
(10)

This has too much info. Since we are doing 2D, $\kappa_z = 1$, $\sigma_z = 0$ in this simulation. We are doing TM as well, so $D_x = D_y = 0$ and $H_z = 0$. Equation reduces to:

$$\begin{bmatrix} \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} \\ \frac{\partial H_z}{\partial z} - \frac{\partial H_z}{\partial x} \\ \frac{\partial H_y}{\partial x} - \frac{\partial H_z}{\partial y} \end{bmatrix} = \frac{\partial}{\partial t} \begin{bmatrix} \kappa_y & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & \kappa_x \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ D_z \end{bmatrix} + \frac{1}{\epsilon_0} \begin{bmatrix} \sigma_y & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & \sigma_x \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ D_z \end{bmatrix}$$
(11)

This leaves us with one equation to find an update quation for D_z :

$$\frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = \kappa_x \frac{\partial}{\partial t} D_z + \frac{\sigma_x}{\epsilon_0} D_z \tag{12}$$

Using semi-implicit definition

$$D^{n+1/2} = \frac{D^{n+1} + D^n}{2} \tag{13}$$

If we discretize around point i,j,k at timestep n This equation discretizes to:

$$\frac{1}{\Delta_x} (H_y^{n+1/2}(i+1/2,j) - H_y^{n+1/2}(i-1/2,j))
- \frac{1}{\Delta_y} (H_x^{n+1/2}(i,j+1/2) - H_x^{n+1/2}(i,j-1/2)) =
\frac{\kappa_x}{\Delta_t} (D_z^{n+1}(i,j) - D_z^n(i,j)) + \frac{\sigma_x}{2\epsilon_0} (D_z^{n+1}(i,j) + D_z^n(i,j))$$
(14)

We can solve this to find update equation for D:

$$\begin{split} &\frac{1}{\Delta_{x}}(H_{y}^{n+1/2}(i+1/2,j)-H_{y}^{n+1/2}(i-1/2,j))\\ &-\frac{1}{\Delta_{y}}(H_{x}^{n+1/2}(i,j+1/2)-H_{x}^{n+1/2}(i,j-1/2))=\\ &\qquad \qquad (\frac{\sigma_{x}}{2\epsilon_{0}}+\frac{\kappa_{x}}{\Delta t})D_{z}^{n+1}(i,j)+(\frac{\sigma_{x}}{2\epsilon_{0}}-\frac{\kappa_{x}}{\Delta t})D_{z}^{n}(i,j) \end{split} \tag{15}$$

$$\begin{split} &\frac{1}{\Delta_{x}}(H_{y}^{n+1/2}(i+1/2,j)-H_{y}^{n+1/2}(i-1/2,j))\\ &-\frac{1}{\Delta_{y}}(H_{x}^{n+1/2}(i,j+1/2)-H_{x}^{n+1/2}(i,j-1/2))=\\ &(\frac{\sigma_{x}\Delta t+2\epsilon_{0}\kappa_{x}}{2\epsilon_{0}\Delta t})D_{z}^{n+1}(i,j)+(\frac{\sigma_{x}\Delta t-2\epsilon_{0}\kappa_{x}}{2\epsilon_{0}\Delta t})D_{z}^{n}(i,j) \end{split} \tag{16}$$

$$D_{z}^{n+1}(i,j) = -\frac{\sigma_{x} - 2\epsilon_{0}\kappa_{x}}{\sigma_{x}\Delta t + 2\epsilon_{0}\kappa_{x}}D_{z}^{n}(i,j) + \frac{2\epsilon_{0}\Delta t}{\Delta_{x}(\sigma_{x}\Delta t + 2\epsilon_{0}\kappa_{x})}(H_{y}^{n+1/2}(i+1/2,j) - H_{y}^{n+1/2}(i-1/2,j)) - \frac{2\epsilon_{0}\Delta t}{\Delta_{y}(\sigma_{x}\Delta t + 2\epsilon_{0}\kappa_{x})}(H_{x}^{n+1/2}(i,j+1/2) - H_{x}^{n+1/2}(i,j-1/2))$$
(17)

Update Components for E

Start with rewriting 8:

$$s_z D_z = \epsilon s_y E_z \tag{18}$$

Using 4 and 5:

$$(\kappa_z + \frac{\sigma_z}{j\omega\epsilon_0})D_z = \epsilon(\kappa_y + \frac{\sigma_y}{j\omega\epsilon_0})E_z \tag{19}$$

Take the partial time derivative and use $\frac{\partial}{\partial t} = j\omega$

$$\frac{\partial}{\partial t}(\kappa_z D_z) + \frac{\sigma_z}{\epsilon_0} D_z = \epsilon \left(\frac{\partial}{\partial t}(\kappa_y E_z) + \frac{\sigma_y}{\epsilon_0} E_z\right) \tag{20}$$

Discretize this to find update equation for E:

(21)

Similarly, we can find the B update equations to be:

(22)

(23)

And we can find the H update equations to be:

(24)

(25)

1.3 Code Implementation

1.3.1 Update Equations

Using the derivation above, we can update field values in a loop. It is computationally more efficient to calculate the coefficients for these field values as an array outside of the loop. This gives us 18 coefficients and their corresponding simplified field update equations:

$$Ez$$
 (26)

$$CBX1 = \frac{2\epsilon_0 \kappa_y - \sigma_y \Delta t}{2\epsilon_0 \kappa_y + \sigma_y \Delta t}$$
 (27)

$$CBX2 = \frac{2\epsilon_0 \Delta t}{2\epsilon_0 \kappa_y + \sigma_y \Delta t} \tag{28}$$

$$CHX1 = \frac{2\epsilon_0 \kappa_z - \sigma_z \Delta t}{2\epsilon_0 \kappa_z + \sigma_z \Delta t}$$
 (29)

$$CHX2 = \frac{1}{2\epsilon_0 \kappa_z + \sigma_z \Delta t} \tag{30}$$

$$CHX3 = 2\epsilon_0 \kappa_x + \sigma_x \Delta t \tag{31}$$

$$CHX4 = 2\epsilon_0 \kappa_x - \sigma_x \Delta t \tag{32}$$

$$CBY1 = \frac{2\epsilon_0 \kappa_z - \sigma_z \Delta t}{2\epsilon_0 \kappa_z + \sigma_z \Delta t}$$
(33)

$$CBY2 = \frac{2\epsilon_0 \Delta t}{2\epsilon_0 \kappa_z + \sigma_z \Delta t} \tag{34}$$

$$CHY1 = \frac{2\epsilon_0 \kappa_x - \sigma_x \Delta t}{2\epsilon_0 \kappa_x + \sigma_x \Delta t}$$
 (35)

$$CHY2 = \frac{1}{2\epsilon_0 \kappa_x + \sigma_x \Delta t} \tag{36}$$

$$CHY3 = 2\epsilon_0 \kappa_y + \sigma_y \Delta t \tag{37}$$

$$CHY4 = 2\epsilon_0 \kappa_y - \sigma_y \Delta t \tag{38}$$

$$CDZ1 = \frac{2\epsilon_0 \kappa_x - \sigma_x \Delta t}{2\epsilon_0 \kappa_x + \sigma_x \Delta t}$$
 (39)

$$CDZ2 = \frac{2\epsilon_0 \Delta t}{2\epsilon_0 \kappa_x + \sigma_x \Delta t} \tag{40}$$

$$CEZ1 = \frac{2\epsilon_0 \kappa_y - \sigma_y \Delta t}{2\epsilon_0 \kappa_y + \sigma_y \Delta t} \tag{41}$$

$$CEZ2 = \frac{1}{2\epsilon_0 \kappa_y + \sigma_y \Delta t} \tag{42}$$

$$CEZ3 = 2\epsilon_0 \kappa_z + \sigma_z \Delta t \tag{43}$$

$$CEZ4 = 2\epsilon_0 \kappa_z - \sigma_z \Delta t \tag{44}$$

Some of these coefficients are identical, but we stored them separately for the purpose of organization and readable naming scheme.

1.3.2 Graded PML

The purpose of PML is to have the wave decay as the wave enters the PML, and a nonzero conductivity value will achieve this decay. However, a large discrepancy between the values of conductivity in the simulation region and the PML can result in unwanted reflections.

The Reflection Factor is given by the equation:

$$R(\theta) = \exp^{-2\eta\cos(\theta)\int_0^d \sigma_x(x)dx(45)}$$

Where σ_x is the graded conductivity of the PML material. θ is the angle of incidence of the wave. So steeper angles of θ will result in higher values of reflection error.

We want to minimize reflection R but also make sure the wave decays completely within the PML.

Figure 1: Plot of the difference of numerical solution with respect to analytical solution of the derivative of a gaussian waveform U evaluated at different timestep dx.

1.3.3 Polynomial grading

One type of grading, and the one we have implemented, is the polynomial grading. We can describe the grading in our code by the factors σ and κ Where the graded conductivity for the PML in the x direction is:

$$\sigma_x = (\frac{x}{d})^m \sigma_{x,max}$$

And the graded value for κ for the PML in the x direction is:

$$\kappa_x = 1 + (\kappa_{x,max} - 1)(\frac{x}{d})^m$$

We will vary the values for κ_{max} and σ_{max} in our numerical experiments to test how different PML material conditions affect the effectiveness of the PML.

An optimal expression for the value of σ_{max} for a polynomial grading has been found numerically to be:

$$\sigma_{x,optimal} = \frac{0.8(m+1)}{\eta_0 \Delta x} \tag{46}$$

2 Experiment

3 Error Analysis

In order to test how well the PML is working to absorb the incoming reflection, we will calculate the relative error with respect to the case of no boundary conditions.

4 Bibliography

Followed Beringer's Derivation in Susan's book - third edition