

ECE 470: Introduction to Robotics Homework 4

Question 1.

You are tasked to design the joint control for cart with a rod as shown below. Using the control partitioning law, and the dynamics formulated in lecture, fill in the required expression (i)-(iv) in the block diagram shown in Figure 1. You may assume insignificant mass for the link
(5 Points)

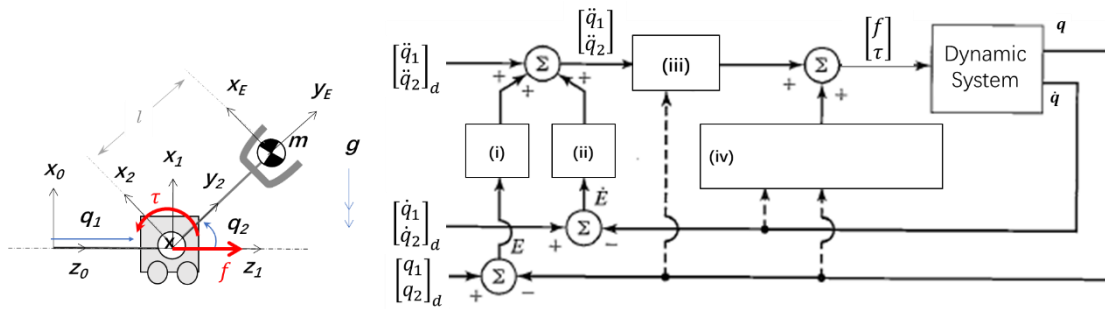


Figure 1.

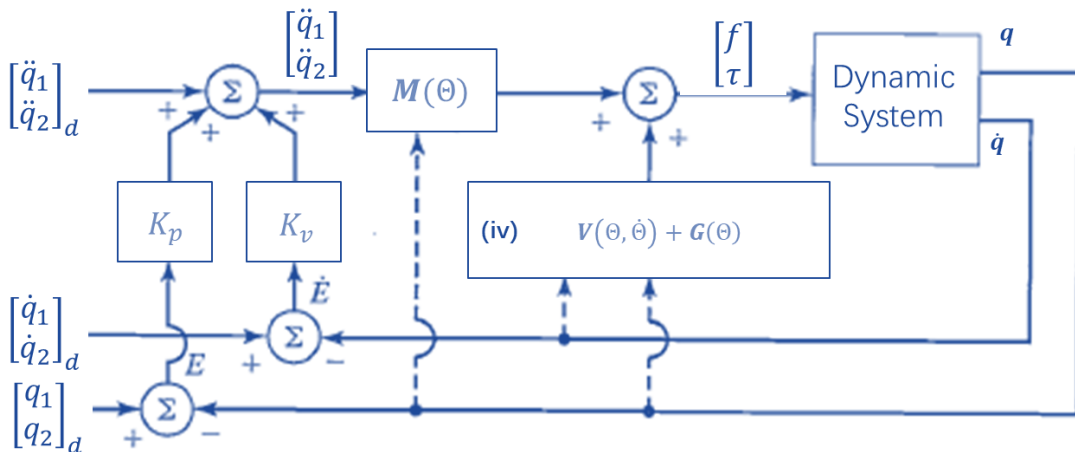
Solution to Question 1

$$\begin{bmatrix} f \\ \tau \end{bmatrix} = \begin{bmatrix} \frac{d}{dt} \frac{\partial L}{\partial \dot{q}_1} - \frac{\partial L}{\partial q_1} \\ \frac{d}{dt} \frac{\partial L}{\partial \dot{q}_2} - \frac{\partial L}{\partial q_2} \end{bmatrix}$$

$$\begin{bmatrix} f \\ \tau \end{bmatrix} = \begin{bmatrix} m\ddot{q}_1 + ml \sin(q_2)\ddot{q}_2 + ml\dot{q}_2^2 \cos(q_2) \\ -ml\ddot{q}_1 \sin(q_2) - ml^2\ddot{q}_2 + mgl \cos(q_2) \end{bmatrix}$$

$$\tau = M(Q) \begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \end{bmatrix} + V(Q, \dot{Q}) + G(Q)$$

$$\therefore \begin{bmatrix} f \\ \tau \end{bmatrix} = \begin{bmatrix} m & ml \sin(q_2) \\ -ml \sin(q_2) & -ml^2 \end{bmatrix} \begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \end{bmatrix} + \begin{bmatrix} ml\dot{q}_2^2 \cos(q_2) \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ mgl \cos(q_2) \end{bmatrix}$$



Question 2.

- a) Consider a single-link manipulator as the cart is fixed stationarily shown Figure 2.
- i) Formulate the dynamic equation factoring coulomb and viscous force acting on the joint and loading due to gravity. You may assume that viscous and coulomb frictions result in resisting moment $M_v = b_v \dot{\theta}$ and $M_c = b_c \text{sgn}(\dot{\theta})$, respectively. (2 Points)
- ii) Draw the control block diagram illustrating the use of control law partitioning for the non-linearities in the system. (6 Points)
- You may assume negligible mass distribution for the link and assumed lumped mass at the distal time as shown.
- b) A DC motor is installed to drive the arm with motor torque τ_m input to a gear transmission ratio η . Redraw the control diagram incorporating the dynamics of the actuator. (4 Points)

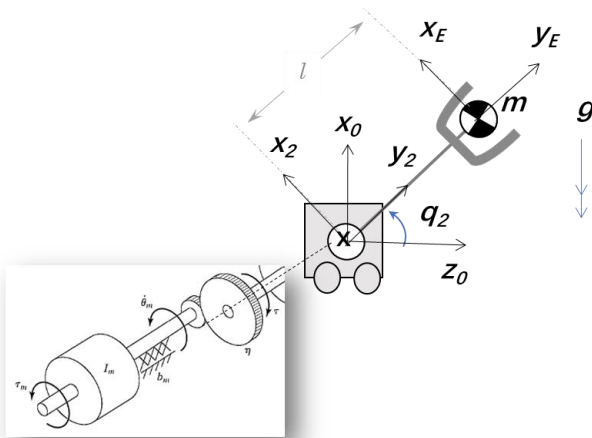


Figure 2.

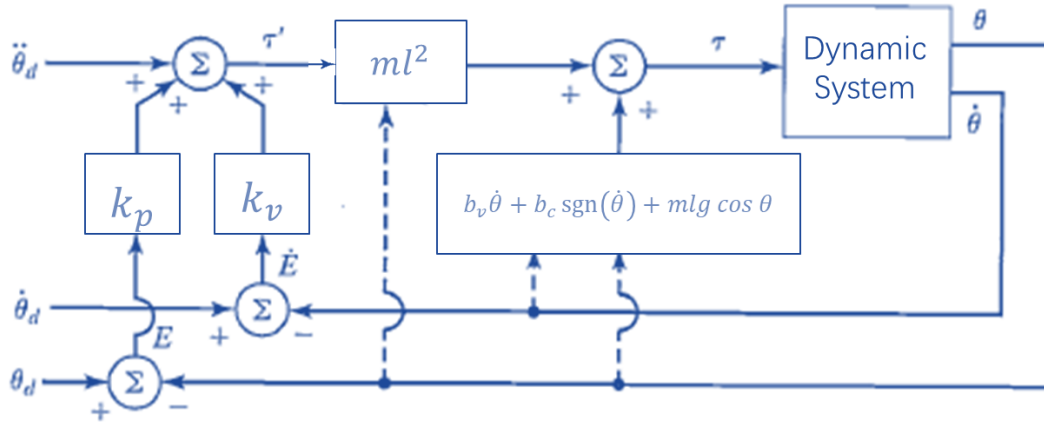
Solution to Question 2:

(a) i)

$$ml^2\ddot{\theta} + b_v\dot{\theta} + b_c \operatorname{sgn}(\dot{\theta}) + mlg \cos \theta$$

ii)

$$\tau = ml^2\ddot{\theta} + b_v\dot{\theta} + b_c \operatorname{sgn}(\dot{\theta}) + mlg \cos \theta$$



b)

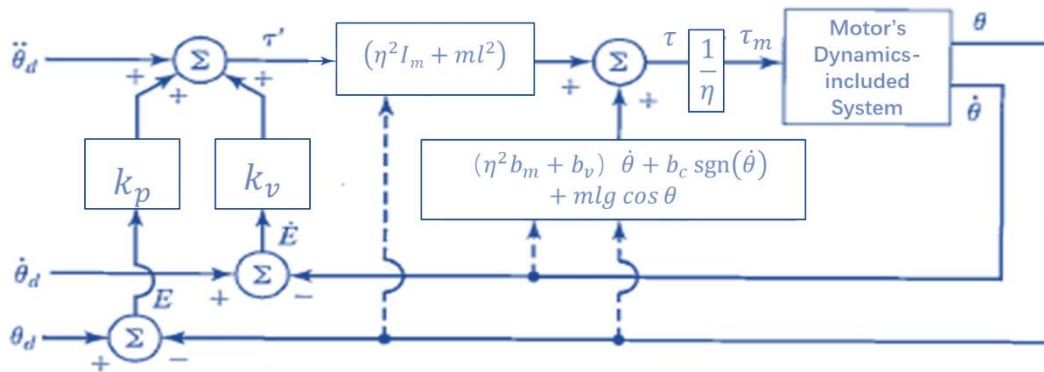
$$\tau - (b_v\dot{\theta} + b_c \operatorname{sgn}(\dot{\theta}) + mlg \cos \theta) - |r_o \times F_m| = ml^2\ddot{\theta}$$

$$\tau = (ml^2\ddot{\theta} + b_v\dot{\theta} + b_c \operatorname{sgn}(\dot{\theta}) + mlg \cos \theta) + |r_o \times F_m|$$

$$|r_o \times F_m| = r_o \frac{\tau_m}{r_i} = \eta \tau_m = \eta (I_m \ddot{\theta}_m + b_m \dot{\theta}_m) = \eta^2 (I_m \ddot{\theta} + b_m \dot{\theta})$$

$$\tau = (ml^2\ddot{\theta} + b_v\dot{\theta} + b_c \operatorname{sgn}(\dot{\theta}) + mlg \cos \theta) + \eta^2 (I_m \ddot{\theta} + b_m \dot{\theta})$$

$$\tau = (\eta^2 I_m + ml^2) \ddot{\theta} + (\eta^2 b_m + b_v) \dot{\theta} + b_c \operatorname{sgn}(\dot{\theta}) + mlg \cos \theta$$



Question 3.

Explain how you would design a hybrid force-displacement control to clean a glass surface as shown. (3 Points)

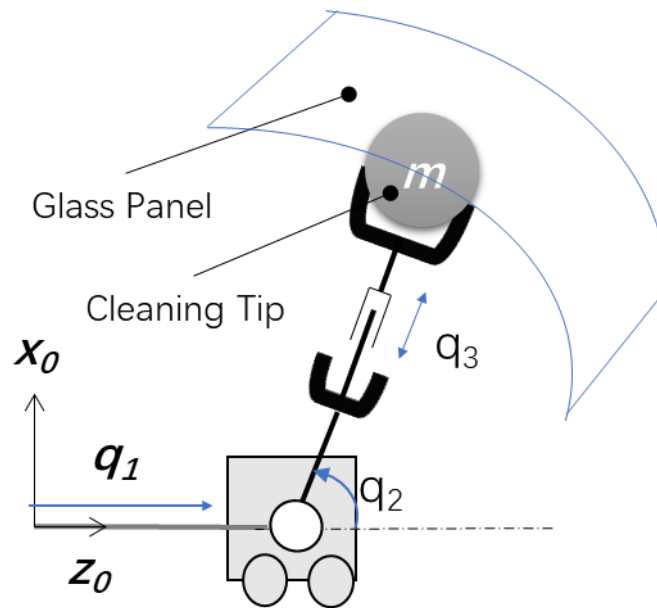


Figure 3

Solution to Question 3:

Considering a planar motion for the cleaning task where the cleaning tip is constrained to the surface of the glass panel with a normal contact force, we can then set the task-space coordinates as (x, z, θ) , where (x, z) is the point of contact and θ is the direction of the normal force vector.

Using hybrid position-force control, we could decouple the joints (q_1, q_2, q_3) to correspond to the 3 independent variables and perform independent joint control where we implement force control with joint 3 to maintain $|\vec{n}|$ and position control with joint 1 and 2 to achieve contact point location at (x, z)

task-space coordinates: (x, z, θ)

