

```
ClearAll["Global`*"]
```

# Timoshenko Beam

## Stiffness Matrix For Simple Cross-Section

$$C_{\text{simple}} = \begin{pmatrix} GAK_x & 0 & 0 & 0 & 0 & 0 \\ 0 & GAK_y & 0 & 0 & 0 & 0 \\ 0 & 0 & EA & 0 & 0 & 0 \\ 0 & 0 & 0 & EI_{xx} & 0 & 0 \\ 0 & 0 & 0 & 0 & EI_{yy} & 0 \\ 0 & 0 & 0 & 0 & 0 & GJ \end{pmatrix};$$

$$\Phi = \begin{pmatrix} u' & 0 & 0 & 0 & -\gamma & 0 \\ 0 & v' & 0 & \psi & 0 & 0 \\ 0 & 0 & w' & 0 & 0 & 0 \\ 0 & 0 & 0 & \psi' & 0 & 0 \\ 0 & 0 & 0 & 0 & \gamma' & 0 \\ 0 & 0 & 0 & 0 & 0 & \phi' \end{pmatrix};$$

## Element Strain Energy Matrix

```
K = MatrixForm[Simplify[Transpose[Φ].Csimple.Φ]]
```

$$\begin{pmatrix} GAK_x (u')^2 & 0 & 0 & 0 & -GAK_x \gamma u' & 0 \\ 0 & GAK_y (v')^2 & 0 & GAK_y \psi v' & 0 & 0 \\ 0 & 0 & EA (w')^2 & 0 & 0 & 0 \\ 0 & GAK_y \psi v' & 0 & GAK_y \psi^2 + EI_{xx} (\psi')^2 & 0 & 0 \\ -GAK_x \gamma u' & 0 & 0 & 0 & GAK_x \gamma^2 + EI_{yy} (\gamma')^2 & 0 \\ 0 & 0 & 0 & 0 & 0 & GJ (\phi')^2 \end{pmatrix}$$

## Stiffness Matrix For Complex Cross-Sections

$$\mathbf{C_{gen}} = \begin{bmatrix} C_{11} & C_{12} & C_{13} & C_{14} & C_{15} & C_{16} \\ C_{12} & C_{22} & C_{23} & C_{24} & C_{25} & C_{26} \\ C_{13} & C_{23} & C_{33} & C_{34} & C_{35} & C_{36} \\ C_{14} & C_{24} & C_{34} & C_{44} & C_{45} & C_{46} \\ C_{15} & C_{25} & C_{35} & C_{45} & C_{55} & C_{56} \\ C_{16} & C_{26} & C_{36} & C_{46} & C_{56} & C_{66} \end{bmatrix};$$

$$\mathbf{\bar{\Phi}} =$$

$$\begin{bmatrix} u1'[x] & u2'[x] & 0 & 0 & 0 & 0 & 0 & 0 & -\gamma1[x] & -\gamma2[x] & 0 \\ 0 & 0 & v1'[x] & v2'[x] & 0 & 0 & \psi1[x] & \psi2[x] & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & w1'[x] & w2'[x] & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \psi1'[x] & \psi2'[x] & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \gamma1'[x] & \gamma2'[x] & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \phi1'[x] \end{bmatrix};$$

### Element Strain Energy Matrix

$$\mathbf{K1} = \text{Expand}[\text{Simplify}[\text{Transpose}[\mathbf{\bar{\Phi}}] \cdot \mathbf{C_{gen}} \cdot \mathbf{\bar{\Phi}}]]; \\ (*\text{MatrixForm}[\mathbf{K1}]*)$$

### Initialize Shape Functions

#### Linear Shape Functions

$$\mathbf{N1}[x_] = \left(1 - \frac{x}{h}\right); \\ \mathbf{N2}[x_] = \frac{x}{h};$$

## Substitute Shape Functions Into Strain/Displacement Matrix and Force Vector

```

K1int[x_] =
  K1 /. {u1'[x] → N1'[x], u2'[x] → N2'[x], v1'[x] → N1'[x], v2'[x] → N2'[x],
    w1'[x] → N1'[x], w2'[x] → N2'[x], ψ1'[x] → N1'[x], ψ2'[x] → N2'[x],
    γ1'[x] → N1'[x], γ2'[x] → N2'[x], φ1'[x] → N1'[x], φ2'[x] → N2'[x],
    ψ1[x] → N1[x], ψ2[x] → N2[x], γ1[x] → N1[x], γ2[x] → N2[x]};
MatrixForm[K1int[x]]

      vx N1[x]
      vx N2[x]
      vy N1[x]
      vy N2[x]
      pz N1[x]
      pz N2[x]
f[x_] = mx N1[x];
      mx N2[x]
      my N1[x]
      my N2[x]
      tz N1[x]
      tz N2[x]

      Qx1
      Qx2
      Qy1
      Qy2
      P1
      P2
Q = Mx1;
      Mx2
      My1
      My2
      T1
      T2

```

$$\begin{pmatrix}
 \frac{C11}{h^2} & -\frac{C11}{h^2} & \frac{C12}{h^2} & -\frac{C12}{h^2} & \frac{C13}{h^2} & -\frac{C13}{h^2} \\
 -\frac{C11}{h^2} & \frac{C11}{h^2} & -\frac{C12}{h^2} & \frac{C12}{h^2} & -\frac{C13}{h^2} & \frac{C13}{h^2} \\
 \frac{C12}{h^2} & -\frac{C12}{h^2} & \frac{C22}{h^2} & -\frac{C22}{h^2} & \frac{C23}{h^2} & -\frac{C23}{h^2} \\
 -\frac{C12}{h^2} & \frac{C12}{h^2} & -\frac{C22}{h^2} & \frac{C22}{h^2} & -\frac{C23}{h^2} & \frac{C23}{h^2} \\
 \frac{C13}{h^2} & -\frac{C13}{h^2} & \frac{C23}{h^2} & -\frac{C23}{h^2} & \frac{C33}{h^2} & -\frac{C33}{h^2} \\
 -\frac{C13}{h^2} & \frac{C13}{h^2} & -\frac{C23}{h^2} & \frac{C23}{h^2} & -\frac{C33}{h^2} & \frac{C33}{h^2} \\
 \frac{C14}{h^2} - \frac{C12}{h^2} \left(1 - \frac{x}{h}\right) & -\frac{C14}{h^2} + \frac{C12}{h^2} \left(1 - \frac{x}{h}\right) & \frac{C24}{h^2} - \frac{C22}{h^2} \left(1 - \frac{x}{h}\right) & -\frac{C24}{h^2} + \frac{C22}{h^2} \left(1 - \frac{x}{h}\right) & \frac{C34}{h^2} - \frac{C23}{h^2} \left(1 - \frac{x}{h}\right) & -\frac{C34}{h^2} + \frac{C23}{h^2} \left(1 - \frac{x}{h}\right) \\
 -\frac{C14}{h^2} + \frac{C12}{h^2} \frac{x}{h} & \frac{C14}{h^2} - \frac{C12}{h^2} \frac{x}{h} & -\frac{C24}{h^2} + \frac{C22}{h^2} \frac{x}{h} & \frac{C24}{h^2} - \frac{C22}{h^2} \frac{x}{h} & -\frac{C34}{h^2} + \frac{C23}{h^2} \frac{x}{h} & \frac{C34}{h^2} - \frac{C23}{h^2} \frac{x}{h} \\
 \frac{C15}{h^2} + \frac{C11}{h^2} \left(1 - \frac{x}{h}\right) & -\frac{C15}{h^2} - \frac{C11}{h^2} \left(1 - \frac{x}{h}\right) & \frac{C25}{h^2} + \frac{C12}{h^2} \left(1 - \frac{x}{h}\right) & -\frac{C25}{h^2} - \frac{C12}{h^2} \left(1 - \frac{x}{h}\right) & \frac{C35}{h^2} + \frac{C13}{h^2} \left(1 - \frac{x}{h}\right) & -\frac{C35}{h^2} - \frac{C13}{h^2} \left(1 - \frac{x}{h}\right) \\
 -\frac{C15}{h^2} - \frac{C11}{h^2} \frac{x}{h} & \frac{C15}{h^2} + \frac{C11}{h^2} \frac{x}{h} & -\frac{C25}{h^2} - \frac{C12}{h^2} \frac{x}{h} & \frac{C25}{h^2} + \frac{C12}{h^2} \frac{x}{h} & -\frac{C35}{h^2} - \frac{C13}{h^2} \frac{x}{h} & \frac{C35}{h^2} + \frac{C13}{h^2} \frac{x}{h} \\
 \frac{C16}{h^2} & -\frac{C16}{h^2} & \frac{C26}{h^2} & -\frac{C26}{h^2} & \frac{C36}{h^2} & -\frac{C36}{h^2} \\
 -\frac{C16}{h^2} & \frac{C16}{h^2} & -\frac{C26}{h^2} & \frac{C26}{h^2} & -\frac{C36}{h^2} & \frac{C36}{h^2}
 \end{pmatrix}$$

Integrate the to get 12 x 12 Stiffness Matrix and Force Vector for Straight Beam

```

Jac = 2/h;

xtran[ξ_] = h/2 (ξ + 1);

(* Single point Gauss Integration weighting coefficient *)
w = 2;

(*MatrixForm[Expand[w Kint1[xtran[0]] 1/Jac /.
  {C11→GAKx,C12→0,C13→0,C14→0,C15→0,C16→0,C22→GAKy,C23→0,C24→0,C25→0,C26→0,
   C33→EA,C34→0,C35→0,C36→0,C44→EIxx,C45→0,C46→0,C55→EIyy,C56→0,C66→GJ}]]*)

Ketmp = Expand[w Klint[xtran[0]] 1/Jac];

MatrixForm[Ketmp]
Fetmp = Simplify[Integrate[f[x], {x, 0, h}] + Q];
MatrixForm[Fetmp]

```

$$\begin{pmatrix}
 \frac{C11}{h} & -\frac{C11}{h} & \frac{C12}{h} & -\frac{C12}{h} & \frac{C13}{h} & -\frac{C13}{h} & -\frac{C12}{2} + \frac{C14}{h} & - \\
 -\frac{C11}{h} & \frac{C11}{h} & -\frac{C12}{h} & \frac{C12}{h} & -\frac{C13}{h} & \frac{C13}{h} & \frac{C12}{2} - \frac{C14}{h} & C \\
 \frac{C12}{h} & -\frac{C12}{h} & \frac{C22}{h} & -\frac{C22}{h} & \frac{C23}{h} & -\frac{C23}{h} & -\frac{C22}{2} + \frac{C24}{h} & - \\
 -\frac{C12}{h} & \frac{C12}{h} & -\frac{C22}{h} & \frac{C22}{h} & -\frac{C23}{h} & \frac{C23}{h} & \frac{C22}{2} - \frac{C24}{h} & C \\
 \frac{C13}{h} & -\frac{C13}{h} & \frac{C23}{h} & -\frac{C23}{h} & \frac{C33}{h} & -\frac{C33}{h} & -\frac{C23}{2} + \frac{C34}{h} & - \\
 -\frac{C13}{h} & \frac{C13}{h} & -\frac{C23}{h} & \frac{C23}{h} & -\frac{C33}{h} & \frac{C33}{h} & \frac{C23}{2} - \frac{C34}{h} & C \\
 -\frac{C12}{2} + \frac{C14}{h} & \frac{C12}{2} - \frac{C14}{h} & -\frac{C22}{2} + \frac{C24}{h} & \frac{C22}{2} - \frac{C24}{h} & -\frac{C23}{2} + \frac{C34}{h} & \frac{C23}{2} - \frac{C34}{h} & -C24 + \frac{C44}{h} + \frac{C22}{4}h & -C \\
 -\frac{C12}{2} - \frac{C14}{h} & \frac{C12}{2} + \frac{C14}{h} & -\frac{C22}{2} - \frac{C24}{h} & \frac{C22}{2} + \frac{C24}{h} & -\frac{C23}{2} - \frac{C34}{h} & \frac{C23}{2} + \frac{C34}{h} & -\frac{C44}{h} + \frac{C22}{4}h & C24 \\
 \frac{C11}{2} + \frac{C15}{h} & -\frac{C11}{2} - \frac{C15}{h} & \frac{C12}{2} + \frac{C25}{h} & -\frac{C12}{2} - \frac{C25}{h} & \frac{C13}{2} + \frac{C35}{h} & -\frac{C13}{2} - \frac{C35}{h} & \frac{C14}{2} - \frac{C25}{2} + \frac{C45}{h} - \frac{C12}{4}h & -\frac{C14}{2} - C \\
 \frac{C11}{2} - \frac{C15}{h} & -\frac{C11}{2} + \frac{C15}{h} & \frac{C12}{2} - \frac{C25}{h} & -\frac{C12}{2} + \frac{C25}{h} & \frac{C13}{2} - \frac{C35}{h} & -\frac{C13}{2} + \frac{C35}{h} & \frac{C14}{2} + \frac{C25}{2} - \frac{C45}{h} - \frac{C12}{4}h & -\frac{C14}{2} + C \\
 \frac{C16}{h} & -\frac{C16}{h} & \frac{C26}{h} & -\frac{C26}{h} & \frac{C36}{h} & -\frac{C36}{h} & -\frac{C26}{2} + \frac{C46}{h} & - \\
 -\frac{C16}{h} & \frac{C16}{h} & -\frac{C26}{h} & \frac{C26}{h} & -\frac{C36}{h} & \frac{C36}{h} & \frac{C26}{2} - \frac{C46}{h} & C
 \end{pmatrix}$$

$$\begin{pmatrix}
 Qx1 + \frac{h vx}{2} \\
 Qx2 + \frac{h vx}{2} \\
 Qy1 + \frac{h vy}{2} \\
 Qy2 + \frac{h vy}{2} \\
 P1 + \frac{h pz}{2} \\
 P2 + \frac{h pz}{2} \\
 \frac{h mx}{2} + Mx1 \\
 \frac{h mx}{2} + Mx2 \\
 \frac{h my}{2} + My1 \\
 \frac{h my}{2} + My2 \\
 T1 + \frac{h tz}{2} \\
 T2 + \frac{h tz}{2}
 \end{pmatrix}$$

## 12 x 12 Element Stiffness Matrix for a beam with a Simple Cross-Section:

**MatrixForm**[Ketmp /. {C11 → GAKx, C12 → 0, C13 → 0, C14 → 0, C15 → 0, C16 → 0,  
C22 → GAKy, C23 → 0, C24 → 0, C25 → 0, C26 → 0, C33 → EA, C34 → 0, C35 → 0,  
C36 → 0, C44 → EIdx, C45 → 0, C46 → 0, C55 → EIyy, C56 → 0, C66 → GJ}]

$$\begin{pmatrix} \frac{GAKx}{h} & -\frac{GAKx}{h} & 0 & 0 & 0 & 0 & 0 & 0 & \frac{GAKx}{2} & \frac{GAKx}{2} & 0 & 0 \\ -\frac{GAKx}{h} & \frac{GAKx}{h} & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{GAKx}{2} & -\frac{GAKx}{2} & 0 & 0 \\ 0 & 0 & \frac{GAKy}{h} & -\frac{GAKy}{h} & 0 & 0 & -\frac{GAKy}{2} & -\frac{GAKy}{2} & 0 & 0 & 0 & 0 \\ 0 & 0 & -\frac{GAKy}{h} & \frac{GAKy}{h} & 0 & 0 & \frac{GAKy}{2} & \frac{GAKy}{2} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & \frac{EA}{h} & -\frac{EA}{h} & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & -\frac{EA}{h} & \frac{EA}{h} & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -\frac{GAKy}{2} & \frac{GAKy}{2} & 0 & 0 & \frac{EIdx}{h} + \frac{GAKy h}{4} & -\frac{EIdx}{h} + \frac{GAKy h}{4} & 0 & 0 & 0 & 0 \\ 0 & 0 & \frac{GAKy}{2} & -\frac{GAKy}{2} & 0 & 0 & -\frac{EIdx}{h} + \frac{GAKy h}{4} & \frac{EIdx}{h} + \frac{GAKy h}{4} & 0 & 0 & 0 & 0 \\ \frac{GAKx}{2} & -\frac{GAKx}{2} & 0 & 0 & 0 & 0 & 0 & 0 & \frac{EIyy}{h} + \frac{GAKx h}{4} & -\frac{EIyy}{h} + \frac{GAKx h}{4} & 0 & 0 \\ \frac{GAKx}{2} & -\frac{GAKx}{2} & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{EIyy}{h} + \frac{GAKx h}{4} & \frac{EIyy}{h} + \frac{GAKx h}{4} & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \frac{GJ}{h} & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{GJ}{h} \end{pmatrix}$$

## Geometric Stiffness Matrix

Strain Energy for Ritz type formulation:

$$\mathbf{\bar{u}g} = \begin{pmatrix} wx' & 0 & 0 & 0 & 0 & 0 \\ 0 & wy' & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix};$$

$$\mathbf{Pmat} = \begin{pmatrix} P & 0 & 0 & 0 & 0 & 0 \\ 0 & P & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix};$$

$$\mathbf{Kg} = \text{MatrixForm}[P \text{Simplify}[\mathbf{\bar{u}g} \cdot \text{Transpose}[\mathbf{\bar{u}g}]]]$$

$$\begin{pmatrix} P (wx')^2 & 0 & 0 & 0 & 0 & 0 \\ 0 & P (wy')^2 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$

## Strain Energy for Finite Element formulation:

$$\bar{\mathbf{u}}\mathbf{g} = \begin{pmatrix} \mathbf{N1}'[\mathbf{x}] & \mathbf{N2}'[\mathbf{x}] & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \mathbf{N1}'[\mathbf{x}] & \mathbf{N2}'[\mathbf{x}] & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix};$$

```
MatrixForm[Simplify[Transpose[ $\bar{\mathbf{u}}\mathbf{g}$ ].Pmat. $\bar{\mathbf{u}}\mathbf{g}$ ]]
Kgint[ $\mathbf{x}_$ ] = Simplify[Transpose[ $\bar{\mathbf{u}}\mathbf{g}$ ].Pmat. $\bar{\mathbf{u}}\mathbf{g}$ ];
```

$$\begin{pmatrix} \frac{P}{h^2} & -\frac{P}{h^2} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ -\frac{P}{h^2} & \frac{P}{h^2} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \frac{P}{h^2} & -\frac{P}{h^2} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -\frac{P}{h^2} & \frac{P}{h^2} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$

## Generate Geometrix Stiffness Matrix and Integrate

```
Kgtmp = Integrate[Kgint[ $\mathbf{x}$ ], { $\mathbf{x}$ , 0, h}];
MatrixForm[Kgtmp]
```

$$\begin{pmatrix} \frac{P}{h} & -\frac{P}{h} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ -\frac{P}{h} & \frac{P}{h} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \frac{P}{h} & -\frac{P}{h} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -\frac{P}{h} & \frac{P}{h} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$



# Geometric Stiffness Matrix

## Mass Matrix For a Ritz Method Formulation:

$$\mathbf{M} = \begin{bmatrix} m & 0 & 0 & 0 & 0 & -m y_m \\ 0 & m & 0 & 0 & 0 & m x_m \\ 0 & 0 & m & m y_m & -m x_m & 0 \\ 0 & 0 & m y_m & I_{xx} & -I_{xy} & 0 \\ 0 & 0 & -m x_m & -I_{xy} & I_{yy} & 0 \\ -m y_m & m x_m & 0 & 0 & 0 & I_{xx} + I_{yy} \end{bmatrix};$$

$$\mathbf{M} = \begin{bmatrix} M11 & 0 & 0 & 0 & 0 & M16 \\ 0 & M11 & 0 & 0 & 0 & M26 \\ 0 & 0 & M11 & -M16 & -M26 & 0 \\ 0 & 0 & -M16 & M44 & M45 & 0 \\ 0 & 0 & -M26 & M45 & M55 & 0 \\ M16 & M26 & 0 & 0 & 0 & M66 \end{bmatrix};$$

$$\Phi =$$

$$\begin{bmatrix} u1[x] & u2[x] & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & v1[x] & v2[x] & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & w1[x] & w2[x] & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \psi1[x] & \psi2[x] & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \gamma1[x] & \gamma2[x] & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \phi1[x] & \phi2[x] \end{bmatrix};$$

$$\mathbf{Mmat} = \text{Expand}[\text{Simplify}[\text{Transpose}[\Phi] \cdot \mathbf{M} \cdot \Phi]]; \\ \text{MatrixForm}[\mathbf{Mmat}]$$

$$\begin{pmatrix} M11 u1[x]^2 & M11 u1[x] u2[x] & 0 & 0 & 0 \\ M11 u1[x] u2[x] & M11 u2[x]^2 & 0 & 0 & 0 \\ 0 & 0 & M11 v1[x]^2 & M11 v1[x] v2[x] & 0 \\ 0 & 0 & M11 v1[x] v2[x] & M11 v2[x]^2 & 0 \\ 0 & 0 & 0 & 0 & M11 w1[x]^2 & M11 w1[x] w2[x] \\ 0 & 0 & 0 & 0 & M11 w1[x] w2[x] & M11 w2[x]^2 \\ 0 & 0 & 0 & 0 & -M16 w1[x] \psi1[x] & -M16 w1[x] \psi2[x] \\ 0 & 0 & 0 & 0 & -M16 w1[x] \psi2[x] & -M16 w2[x] \psi1[x] \\ 0 & 0 & 0 & 0 & -M26 w1[x] \gamma1[x] & -M26 w1[x] \gamma2[x] \\ 0 & 0 & 0 & 0 & -M26 w1[x] \gamma2[x] & -M26 w2[x] \gamma1[x] \\ M16 u1[x] \phi1[x] & M16 u2[x] \phi1[x] & M26 v1[x] \phi1[x] & M26 v2[x] \phi1[x] & 0 \\ M16 u1[x] \phi2[x] & M16 u2[x] \phi2[x] & M26 v1[x] \phi2[x] & M26 v2[x] \phi2[x] & 0 \end{pmatrix}$$

## Substitute Shape Functions Into Strain/Displacement Matrix and Force Vector

```

Mint[x_] = Mmat /. {u1[x] → N1[x], u2[x] → N2[x], v1[x] → N1[x],
  v2[x] → N2[x], w1[x] → N1[x], w2[x] → N2[x], ψ1[x] → N1[x],
  ψ2[x] → N2[x], γ1[x] → N1[x], γ2[x] → N2[x], φ1[x] → N1[x], φ2[x] → N2[x],
  ψ1[x] → N1[x], ψ2[x] → N2[x], γ1[x] → N1[x], γ2[x] → N2[x]};
MatrixForm[
  Mint[
    x]]

```

$$\begin{pmatrix}
 M11 \left(1 - \frac{x}{h}\right)^2 & \frac{M11 x \left(1 - \frac{x}{h}\right)}{h} & 0 & 0 & 0 & 0 & 0 & 0 \\
 \frac{M11 x \left(1 - \frac{x}{h}\right)}{h} & \frac{M11 x^2}{h^2} & 0 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & M11 \left(1 - \frac{x}{h}\right)^2 & \frac{M11 x \left(1 - \frac{x}{h}\right)}{h} & 0 & 0 & 0 & 0 \\
 0 & 0 & \frac{M11 x \left(1 - \frac{x}{h}\right)}{h} & \frac{M11 x^2}{h^2} & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & M11 \left(1 - \frac{x}{h}\right)^2 & \frac{M11 x \left(1 - \frac{x}{h}\right)}{h} & -M16 \left(1 - \frac{x}{h}\right)^2 & -\frac{M16 x}{h} \\
 0 & 0 & 0 & 0 & \frac{M11 x \left(1 - \frac{x}{h}\right)}{h} & \frac{M11 x^2}{h^2} & -\frac{M16 x \left(1 - \frac{x}{h}\right)}{h} & -\frac{M16}{h} \\
 0 & 0 & 0 & 0 & -M16 \left(1 - \frac{x}{h}\right)^2 & -\frac{M16 x \left(1 - \frac{x}{h}\right)}{h} & M44 \left(1 - \frac{x}{h}\right)^2 & \frac{M44 x}{h} \\
 0 & 0 & 0 & 0 & -\frac{M16 x \left(1 - \frac{x}{h}\right)}{h} & -\frac{M16 x^2}{h^2} & \frac{M44 x \left(1 - \frac{x}{h}\right)}{h} & \frac{M44}{h^2} \\
 0 & 0 & 0 & 0 & -M26 \left(1 - \frac{x}{h}\right)^2 & -\frac{M26 x \left(1 - \frac{x}{h}\right)}{h} & M45 \left(1 - \frac{x}{h}\right)^2 & \frac{M45 x}{h} \\
 0 & 0 & 0 & 0 & -\frac{M26 x \left(1 - \frac{x}{h}\right)}{h} & -\frac{M26 x^2}{h^2} & \frac{M45 x \left(1 - \frac{x}{h}\right)}{h} & \frac{M45}{h^2} \\
 M16 \left(1 - \frac{x}{h}\right)^2 & \frac{M16 x \left(1 - \frac{x}{h}\right)}{h} & M26 \left(1 - \frac{x}{h}\right)^2 & \frac{M26 x \left(1 - \frac{x}{h}\right)}{h} & 0 & 0 & 0 & 0 \\
 \frac{M16 x \left(1 - \frac{x}{h}\right)}{h} & \frac{M16 x^2}{h^2} & \frac{M26 x \left(1 - \frac{x}{h}\right)}{h} & \frac{M26 x^2}{h^2} & 0 & 0 & 0 & 0
 \end{pmatrix}$$

Integrate the to get 12 x 12 Mass Matrix Straight Beam

$$\mathbf{Metmp} = \int_0^h \mathbf{Mint}[\mathbf{x}] \, d\mathbf{x};$$

**MatrixForm**[**Metmp**]

$$\begin{pmatrix} \frac{h M_{11}}{3} & \frac{h M_{11}}{6} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \frac{h M_{16}}{3} & \frac{h M_{16}}{6} \\ \frac{h M_{11}}{6} & \frac{h M_{11}}{3} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \frac{h M_{16}}{6} & \frac{h M_{16}}{3} \\ 0 & 0 & \frac{h M_{11}}{3} & \frac{h M_{11}}{6} & 0 & 0 & 0 & 0 & 0 & 0 & \frac{h M_{26}}{3} & \frac{h M_{26}}{6} \\ 0 & 0 & \frac{h M_{11}}{6} & \frac{h M_{11}}{3} & 0 & 0 & 0 & 0 & 0 & 0 & \frac{h M_{26}}{6} & \frac{h M_{26}}{3} \\ 0 & 0 & 0 & 0 & \frac{h M_{11}}{3} & \frac{h M_{11}}{6} & -\frac{h M_{16}}{3} & -\frac{h M_{16}}{6} & -\frac{h M_{26}}{3} & -\frac{h M_{26}}{6} & 0 & 0 \\ 0 & 0 & 0 & 0 & \frac{h M_{11}}{6} & \frac{h M_{11}}{3} & -\frac{h M_{16}}{6} & -\frac{h M_{16}}{3} & -\frac{h M_{26}}{6} & -\frac{h M_{26}}{3} & 0 & 0 \\ 0 & 0 & 0 & 0 & -\frac{h M_{16}}{3} & -\frac{h M_{16}}{6} & \frac{h M_{44}}{3} & \frac{h M_{44}}{6} & \frac{h M_{45}}{3} & \frac{h M_{45}}{6} & 0 & 0 \\ 0 & 0 & 0 & 0 & -\frac{h M_{16}}{6} & -\frac{h M_{16}}{3} & \frac{h M_{44}}{6} & \frac{h M_{44}}{3} & \frac{h M_{45}}{6} & \frac{h M_{45}}{3} & 0 & 0 \\ 0 & 0 & 0 & 0 & -\frac{h M_{26}}{3} & -\frac{h M_{26}}{6} & \frac{h M_{45}}{3} & \frac{h M_{45}}{6} & \frac{h M_{55}}{3} & \frac{h M_{55}}{6} & 0 & 0 \\ 0 & 0 & 0 & 0 & -\frac{h M_{26}}{6} & -\frac{h M_{26}}{3} & \frac{h M_{45}}{6} & \frac{h M_{45}}{3} & \frac{h M_{55}}{6} & \frac{h M_{55}}{3} & 0 & 0 \\ \frac{h M_{16}}{3} & \frac{h M_{16}}{6} & \frac{h M_{26}}{3} & \frac{h M_{26}}{6} & 0 & 0 & 0 & 0 & 0 & 0 & \frac{h M_{66}}{3} & \frac{h M_{66}}{6} \\ \frac{h M_{16}}{6} & \frac{h M_{16}}{3} & \frac{h M_{26}}{6} & \frac{h M_{26}}{3} & 0 & 0 & 0 & 0 & 0 & 0 & \frac{h M_{66}}{6} & \frac{h M_{66}}{3} \end{pmatrix}$$

## Reorder All Matricies for Easier Global Assembly

Reorder Vector:

**reorder** = {1, 3, 5, 7, 9, 11, 2, 4, 6, 8, 10, 12};

## 12 x 12 RIE Timoshenko Beam Stiffness Matrix:

$$\mathbf{K_e} = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix};$$

$$\mathbf{F_e} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix};$$

`Do[Do[ $\mathbf{K_e}[[i, j]] = \text{Expand}[\mathbf{K_{tmp}}[[\text{reorder}[[i]], \text{reorder}[[j]]]]], \{i, 12\}], \{j, 12\}]$`

`Do[ $\mathbf{F_e}[[i]] = \mathbf{F_{tmp}}[[\text{reorder}[[i]]]], \{i, 12\}]$`

`MatrixForm[ $\mathbf{K_e}$ ]`

`MatrixForm[ $\mathbf{F_e}$ ]`

$$\begin{pmatrix} \frac{C_{11}}{h} & \frac{C_{12}}{h} & \frac{C_{13}}{h} & -\frac{C_{12}}{2} + \frac{C_{14}}{h} & \frac{C_{11}}{2} + \frac{C_{15}}{h} & \frac{C_{16}}{h} & -\frac{C_{11}}{h} \\ \frac{C_{12}}{h} & \frac{C_{22}}{h} & \frac{C_{23}}{h} & -\frac{C_{22}}{2} + \frac{C_{24}}{h} & \frac{C_{12}}{2} + \frac{C_{25}}{h} & \frac{C_{26}}{h} & -\frac{C_{12}}{h} \\ \frac{C_{13}}{h} & \frac{C_{23}}{h} & \frac{C_{33}}{h} & -\frac{C_{23}}{2} + \frac{C_{34}}{h} & \frac{C_{13}}{2} + \frac{C_{35}}{h} & \frac{C_{36}}{h} & -\frac{C_{13}}{h} \\ -\frac{C_{12}}{2} + \frac{C_{14}}{h} & -\frac{C_{22}}{2} + \frac{C_{24}}{h} & -\frac{C_{23}}{2} + \frac{C_{34}}{h} & -C_{24} + \frac{C_{44}}{h} + \frac{C_{22}h}{4} & \frac{C_{14}}{2} - \frac{C_{25}}{2} + \frac{C_{45}}{h} - \frac{C_{12}h}{4} & -\frac{C_{26}}{2} + \frac{C_{46}}{h} & \frac{C_{12}}{2} - \frac{C_{16}}{h} \\ \frac{C_{11}}{2} + \frac{C_{15}}{h} & \frac{C_{12}}{2} + \frac{C_{25}}{h} & \frac{C_{13}}{2} + \frac{C_{35}}{h} & \frac{C_{14}}{2} - \frac{C_{25}}{2} + \frac{C_{45}}{h} - \frac{C_{12}h}{4} & C_{15} + \frac{C_{55}}{h} + \frac{C_{11}h}{4} & \frac{C_{16}}{2} + \frac{C_{56}}{h} & -\frac{C_{11}}{2} - \frac{C_{16}}{h} \\ \frac{C_{16}}{h} & \frac{C_{26}}{h} & \frac{C_{36}}{h} & -\frac{C_{26}}{2} + \frac{C_{46}}{h} & \frac{C_{16}}{2} + \frac{C_{56}}{h} & \frac{C_{66}}{h} & -\frac{C_{16}}{h} \\ -\frac{C_{11}}{h} & -\frac{C_{12}}{h} & -\frac{C_{13}}{h} & \frac{C_{12}}{2} - \frac{C_{14}}{h} & -\frac{C_{11}}{2} - \frac{C_{15}}{h} & -\frac{C_{16}}{h} & \frac{C_{11}}{h} \\ -\frac{C_{12}}{h} & -\frac{C_{22}}{h} & -\frac{C_{23}}{h} & \frac{C_{22}}{2} - \frac{C_{24}}{h} & -\frac{C_{12}}{2} - \frac{C_{25}}{h} & -\frac{C_{26}}{h} & \frac{C_{12}}{h} \\ -\frac{C_{13}}{h} & -\frac{C_{23}}{h} & -\frac{C_{33}}{h} & \frac{C_{23}}{2} - \frac{C_{34}}{h} & -\frac{C_{13}}{2} - \frac{C_{35}}{h} & -\frac{C_{36}}{h} & \frac{C_{13}}{h} \\ -\frac{C_{12}}{2} - \frac{C_{14}}{h} & -\frac{C_{22}}{2} - \frac{C_{24}}{h} & -\frac{C_{23}}{2} - \frac{C_{34}}{h} & -\frac{C_{44}}{h} + \frac{C_{22}h}{4} & -\frac{C_{14}}{2} - \frac{C_{25}}{2} - \frac{C_{45}}{h} - \frac{C_{12}h}{4} & -\frac{C_{26}}{2} - \frac{C_{46}}{h} & \frac{C_{12}}{2} + \frac{C_{16}}{h} \\ \frac{C_{11}}{2} - \frac{C_{15}}{h} & \frac{C_{12}}{2} - \frac{C_{25}}{h} & \frac{C_{13}}{2} - \frac{C_{35}}{h} & \frac{C_{14}}{2} + \frac{C_{25}}{2} - \frac{C_{45}}{h} - \frac{C_{12}h}{4} & -\frac{C_{55}}{h} + \frac{C_{11}h}{4} & \frac{C_{16}}{2} - \frac{C_{56}}{h} & -\frac{C_{11}}{2} + \frac{C_{16}}{h} \\ -\frac{C_{16}}{h} & -\frac{C_{26}}{h} & -\frac{C_{36}}{h} & \frac{C_{26}}{2} - \frac{C_{46}}{h} & -\frac{C_{16}}{2} - \frac{C_{56}}{h} & -\frac{C_{66}}{h} & \frac{C_{16}}{h} \end{pmatrix}$$

$$\begin{pmatrix} Qx1 + \frac{h vx}{2} \\ Qy1 + \frac{h vy}{2} \\ P1 + \frac{h pz}{2} \\ \frac{h mx}{2} + Mx1 \\ \frac{h my}{2} + My1 \\ T1 + \frac{h tz}{2} \\ Qx2 + \frac{h vx}{2} \\ Qy2 + \frac{h vy}{2} \\ P2 + \frac{h pz}{2} \\ \frac{h mx}{2} + Mx2 \\ \frac{h my}{2} + My2 \\ T2 + \frac{h tz}{2} \end{pmatrix}$$

## 12 x 12 RIE Timoshenko Beam Geometric Stiffness Matrix:

$$\mathbf{Keg} = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix};$$

```
Do[Do[Keg[[i, j]] = Expand[Kgtmp[[reorder[[i]], reorder[[j]]]]], {i, 12}], {j, 12}]
MatrixForm[Keg]
```

$$\begin{pmatrix} \frac{P}{h} & 0 & 0 & 0 & 0 & 0 & -\frac{P}{h} & 0 & 0 & 0 & 0 & 0 \\ 0 & \frac{P}{h} & 0 & 0 & 0 & 0 & 0 & -\frac{P}{h} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ -\frac{P}{h} & 0 & 0 & 0 & 0 & 0 & \frac{P}{h} & 0 & 0 & 0 & 0 & 0 \\ 0 & -\frac{P}{h} & 0 & 0 & 0 & 0 & 0 & \frac{P}{h} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$

## 12 x 12 Timoshenko Beam Mass Matrix:

$$\mathbf{Me} = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix};$$

**Do[Do[Me[[i, j]] = Expand[Metmp[[reorder[[i]], reorder[[j]]]], {i, 12}], {j, 12}]**  
**MatrixForm[Me]**

$$\begin{pmatrix} \frac{h M11}{3} & 0 & 0 & 0 & 0 & \frac{h M16}{3} & \frac{h M11}{6} & 0 & 0 & 0 & 0 & \frac{h M16}{6} \\ 0 & \frac{h M11}{3} & 0 & 0 & 0 & \frac{h M26}{3} & 0 & \frac{h M11}{6} & 0 & 0 & 0 & \frac{h M26}{6} \\ 0 & 0 & \frac{h M11}{3} & -\frac{h M16}{3} & -\frac{h M26}{3} & 0 & 0 & 0 & \frac{h M11}{6} & -\frac{h M16}{6} & -\frac{h M26}{6} & 0 \\ 0 & 0 & -\frac{h M16}{3} & \frac{h M44}{3} & \frac{h M45}{3} & 0 & 0 & 0 & -\frac{h M16}{6} & \frac{h M44}{6} & \frac{h M45}{6} & 0 \\ 0 & 0 & -\frac{h M26}{3} & \frac{h M45}{3} & \frac{h M55}{3} & 0 & 0 & 0 & -\frac{h M26}{6} & \frac{h M45}{6} & \frac{h M55}{6} & 0 \\ \frac{h M16}{3} & \frac{h M26}{3} & 0 & 0 & 0 & \frac{h M66}{3} & \frac{h M16}{6} & \frac{h M26}{6} & 0 & 0 & 0 & \frac{h M66}{6} \\ \frac{h M11}{6} & 0 & 0 & 0 & 0 & \frac{h M16}{6} & \frac{h M11}{3} & 0 & 0 & 0 & 0 & \frac{h M16}{3} \\ 0 & \frac{h M11}{6} & 0 & 0 & 0 & \frac{h M26}{6} & 0 & \frac{h M11}{3} & 0 & 0 & 0 & \frac{h M26}{3} \\ 0 & 0 & \frac{h M11}{6} & -\frac{h M16}{6} & -\frac{h M26}{6} & 0 & 0 & 0 & \frac{h M11}{3} & -\frac{h M16}{3} & -\frac{h M26}{3} & 0 \\ 0 & 0 & -\frac{h M16}{6} & \frac{h M44}{6} & \frac{h M45}{6} & 0 & 0 & 0 & -\frac{h M16}{3} & \frac{h M44}{3} & \frac{h M45}{3} & 0 \\ 0 & 0 & -\frac{h M26}{6} & \frac{h M45}{6} & \frac{h M55}{6} & 0 & 0 & 0 & -\frac{h M26}{3} & \frac{h M45}{3} & \frac{h M55}{3} & 0 \\ \frac{h M16}{6} & \frac{h M26}{6} & 0 & 0 & 0 & \frac{h M66}{6} & \frac{h M16}{3} & \frac{h M26}{3} & 0 & 0 & 0 & \frac{h M66}{3} \end{pmatrix}$$

## 12 x 12 Timoshenko Beam Rotation Matrix Testing

```
KetmpRot = Ke /. {C11 → GAKx, C12 → 0, C13 → 0, C14 → 0, C15 → 0, C16 → 0,
  C22 → GAKy, C23 → 0, C24 → 0, C25 → 0, C26 → 0, C33 → EA, C34 → 0, C35 → 0,
  C36 → 0, C44 → EIdx, C45 → 0, C46 → 0, C55 → EIyy, C56 → 0, C66 → GJ};
```

```
P1 = {0, 0, 0};
```

```
P2 = {0, 0, 1};
```

```
nuVec = {0, 1, 0};
```

```
zVec = (P2 - P1) / Norm[P2 - P1]
```

```
yVec = Cross[zVec, nuVec] / Norm[Cross[zVec, nuVec]]
```

```
xVec = Cross[yVec, zVec] / Norm[Cross[yVec, zVec]]
```

```
Lambda = Transpose[{xVec, yVec, zVec}]
```

```
MatrixForm[Lambda]
```

```

      0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0
rot = 0 0 0 0 0 0 0 0 0 0 0 0;
      0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0
      0 0 0 0 0 0 0 0 0 0 0 0
```

```
rot[[1 ;; 3, 1 ;; 3]] = Lambda;
```

```
rot[[4 ;; 6, 4 ;; 6]] = Lambda;
```

```
rot[[7 ;; 9, 7 ;; 9]] = Lambda;
```

```
rot[[10 ;; 12, 10 ;; 12]] = Lambda;
```

```
MatrixForm[rot]
```

```
MatrixForm[Transpose[rot].KetmpRot.rot]
```

```
{0, 0, 1}
```

```
{-1, 0, 0}
```

```
{0, 1, 0}
```

```
{{0, -1, 0}, {1, 0, 0}, {0, 0, 1}}
```

```

( 0 -1 0 )
( 1  0 0 )
( 0  0 1 )
```

$$\begin{pmatrix} 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & -1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

$$\begin{pmatrix} \frac{GAKy}{h} & 0 & 0 & 0 & \frac{GAKy}{2} & 0 & -\frac{GAKy}{h} & 0 & 0 & 0 & \frac{GAKy}{2} \\ 0 & \frac{GAKx}{h} & 0 & -\frac{GAKx}{2} & 0 & 0 & 0 & -\frac{GAKx}{h} & 0 & -\frac{GAKx}{2} & 0 \\ 0 & 0 & \frac{EA}{h} & 0 & 0 & 0 & 0 & 0 & -\frac{EA}{h} & 0 & 0 \\ 0 & -\frac{GAKx}{2} & 0 & \frac{EIyy}{h} + \frac{GAKx h}{4} & 0 & 0 & 0 & \frac{GAKx}{2} & 0 & -\frac{EIyy}{h} + \frac{GAKx h}{4} & 0 \\ \frac{GAKy}{2} & 0 & 0 & 0 & \frac{EIxx}{h} + \frac{GAKy h}{4} & 0 & -\frac{GAKy}{2} & 0 & 0 & 0 & -\frac{EIxx}{h} + \frac{GAKy h}{4} \\ 0 & 0 & 0 & 0 & 0 & \frac{GJ}{h} & 0 & 0 & 0 & 0 & 0 \\ -\frac{GAKy}{h} & 0 & 0 & 0 & -\frac{GAKy}{2} & 0 & \frac{GAKy}{h} & 0 & 0 & 0 & -\frac{GAKy}{2} \\ 0 & -\frac{GAKx}{h} & 0 & \frac{GAKx}{2} & 0 & 0 & 0 & \frac{GAKx}{h} & 0 & \frac{GAKx}{2} & 0 \\ 0 & 0 & -\frac{EA}{h} & 0 & 0 & 0 & 0 & 0 & \frac{EA}{h} & 0 & 0 \\ 0 & -\frac{GAKx}{2} & 0 & -\frac{EIyy}{h} + \frac{GAKx h}{4} & 0 & 0 & 0 & \frac{GAKx}{2} & 0 & \frac{EIyy}{h} + \frac{GAKx h}{4} & 0 \\ \frac{GAKy}{2} & 0 & 0 & 0 & -\frac{EIxx}{h} + \frac{GAKy h}{4} & 0 & -\frac{GAKy}{2} & 0 & 0 & 0 & \frac{EIxx}{h} + \frac{GAKy h}{4} \\ 0 & 0 & 0 & 0 & 0 & -\frac{GJ}{h} & 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$