

The purpose of this activity is to apply what you have learned in all the previous activities. This document will walk you through the steps to create your own 2D, inviscid panel method. This activity is significantly more computationally involved than the previous ones, so be prepared to see some math.

Panel Methods

By way of introduction: Panel Methods are analytic methods by which we can solve for some of the important airfoil characteristics, such as the lift and moment coefficients. In order to do this, we solve a system of potential flow equations of the standard form $Ax = b$ where A is a square matrix, b is a vector of known values, and x is the vector of unknowns for which we are solving. (The topic of potential flow is covered in the fluid mechanics courses, ME EN 312 and 512, and, of course, in the aerodynamics course, ME EN 515.) A detailed understanding of the physics behind the panel method is not necessary, however, if you are interested in the theory you can look [ME EN 515 Lecture Slides](#) and/or [these lecture slides](#) from a Stanford course (same math, with more explanatory text). All that really needs to be understood is that, as shown in fig. 1, an airfoil is approximated by straight lines that we are calling panels, and based on the geometry of those lines, we can set up a system of equations (the equations will be given to you), to solve for some of the flow characteristics around the airfoil, assuming the fluid is inviscid (no friction), among other assumptions.

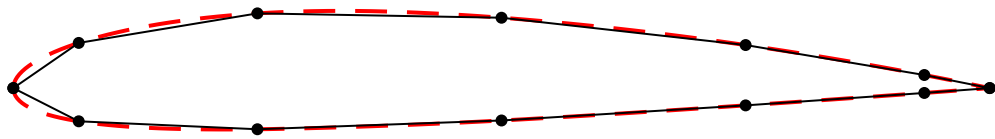


Figure 1: In a panel method, the airfoil is approximated by several “panels.” Shown here is a rough representation of linear panels (straight lines between points) for a NACA 2412 airfoil. In general, many panels are used so that the curvature of the airfoil is well approximated.

There are four major parts to the panel method: 1) characterize the geometry 2) populate the coefficient matrix on the left hand side of the system of equations, 3) populate the right hand side vector of the system of equations, 4) use the solution to the system of equations to obtain the desired flow properties.

Geometry Characterization

We begin with characterizing the geometry since all the following steps depend on the geometry. For the math to work out, you will need to loop through the points/panels from bottom side trailing edge of the airfoil, around the front to the top side trailing edge. Here is an overview of the steps needed to have the geometry values you need:

1. Using your NACA 4-series coordinate function, create the x and z vectors, concatenating them as described in activity 3 such that they begin with the bottom trailing edge point, go toward the front and around until ending at the top side trailing edge point.
2. Calculate each panel length (the distance between consecutive points), and store the results in a 1D array
3. Calculate the midpoint of each panel and store the x and z coordinates either together in a 2D array, or separately in two 1D arrays.
4. Calculate the angle of each panel relative to the $+x$ axis, and store the results in a 1D array. (hint: panel length, center point position, and panel angle can all be done in the same loop.)

5. Calculate the distance between each panel center point, and each panel edge point (the airfoil coordinate points.), and save these in a 2D vector where the rows are associated with each center point, and the columns are associated with each coordinate point. (In other words, there will be one more column there there are rows.)
(hint: you'll need to use a for loop inside of a for loop for this and the next step.)

6. Calculate the angle between each panel and all other panels. Store these in a 2D array.

The equation for the angle between panels is given by:

$$\beta_{i,j} = \begin{cases} \text{atan2} \left[\frac{(x_j - \bar{x}_i)(z_{j+1} - \bar{z}_i) - (z_j - \bar{z}_i)(x_{j+1} - \bar{x}_i)}{(x_j - \bar{x}_i)(x_{j+1} - \bar{x}_i) + (z_j - \bar{z}_i)(z_{j+1} - \bar{z}_i)} \right] & \text{if } i \neq j \\ \pi & \text{otherwise} \end{cases} \quad (1)$$

where x and z are the x and z components of the airfoil coordinates and \bar{x} and \bar{z} are the panel midpoint coordinates. Also note the notation here: for each i th panel, we need the angle between in and every j th panel. This means the array that stores these values should have the same number of rows and columns, where the i th row has the angles between the i th panel and every other panel. atan2 is a Julia function that computes the inverse tangent in the correct quadrant.

Coefficient Matrix

It may be helpful to visualize the entirety of our system of equations in matrix form. It is as follows:

$$\begin{bmatrix} A_{1,1} & A_{1,2} & \cdots & A_{1,N} & A_{1,N+1} \\ A_{2,1} & A_{2,2} & \cdots & A_{2,N} & A_{2,N+1} \\ \vdots & \vdots & & \vdots & \vdots \\ A_{N,1} & A_{N,2} & \cdots & A_{N,N} & A_{N,N+1} \\ A_{N+1,1} & A_{N+1,2} & \cdots & A_{N+1,N} & A_{N+1,N+1} \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \\ \vdots \\ q_N \\ \gamma \end{bmatrix} = \begin{bmatrix} b_1 \\ b_2 \\ \vdots \\ b_N \\ b_{N+1} \end{bmatrix} \quad (2)$$

where A are the elements of the coefficient matrix. The equations 1 through N (where N is the number of panels) have to do with boundary conditions on the airfoil panels and have the same form. The final equation (the $N + 1$ row) has a different form and is associated with a boundary condition at the trailing edge. The q 's and γ are the values for which we are solving, and the b 's are known values we calculate.

Right now we are concerned with calculating the elements of the A matrix. The equation for the A values for i and j from 1 to N is:

$$A_{i,j} = \sin(\theta_i - \theta_j) \ln \left(\frac{r_{i,j+1}}{r_{i,j}} \right) + \cos(\theta_i - \theta_j) \beta_{i,j} \quad (3)$$

where θ are the angles of the panels with respect to the +x axis, r are the distances from the panel centers to the coordinate points, and β are the angles between the panels. For i from 1 to N and $j = N + 1$, the equation is:

$$A_{i,N+1} = \sum_{j=1}^N \left[\cos(\theta_i - \theta_j) \ln \left(\frac{r_{i,j+1}}{r_{i,j}} \right) - \sin(\theta_i - \theta_j) \beta_{i,j} \right] \quad (4)$$

for $i = N + 1$ and j from 1 to N the equation is:

$$A_{N+1,j} = \sum_{k=1 \text{ and } N} \left[\sin(\theta_k - \theta_j) \beta_{k,j} - \cos(\theta_k - \theta_j) \ln \left(\frac{r_{k,j+1}}{r_{k,j}} \right) \right] \quad (5)$$

Note that this sum is only for the first and last panel, not every panel like the previous equations. Finally the equation for $i = j = N + 1$ is:

$$A_{N+1,N+1} = \sum_{k=1 \text{ and } N} \left(\sum_{j=1}^N \left[\cos(\theta_k - \theta_j) \beta_{k,j} + \sin(\theta_k - \theta_j) \ln \left(\frac{r_{k,j+1}}{r_{k,j}} \right) \right] \right) \quad (6)$$

Right Hand Side Vector

Now we need the equations for the b values of the right hand side vector. The equation for i from 1 to N is:

$$b_i = 2\pi V_\infty \sin(\theta_i - \alpha) \quad (7)$$

where V_∞ is the velocity of the air far away from the airfoil, and α is the angle of attack of the airfoil, in other words, the angle of the airfoil relative to the direction of the air velocity. For $i = N + 1$, the equation for b is;

$$b_{N+1} = -2\pi V_\infty [\cos(\theta_1 - \alpha) + \cos(\theta_N - \alpha)] \quad (8)$$

Flow Properties

You can solve the system (let's write it now as $Aq = b$) by using the “\” operator in Julia:

$$q = A \backslash b \quad (9)$$

This is similar to doing a left multiply of the inverse of A to solve for q . (If you haven't seen this before, you will in your linear algebra course.)

$$q = A^{-1}b \quad (10)$$

although the “\” operator doesn't actually invert the matrix (see the [Julia Documentation](#) page, specifically the Base.\ documentation for more details)

Remember the q contains the q and γ values for our system (these are the magnitudes of the potential flows mentioned earlier). We can now use these to find the tangential velocity on each panel and thereby the pressure coefficient distribution around the airfoil. The tangential velocity is calculated by:

$$\begin{aligned} V_{ti} &= V_\infty \cos(\theta_i - \alpha) \\ &+ \frac{1}{2\pi} \sum_{j=1}^N \left(q_j \left[\sin(\theta_i - \theta_j) \beta_{i,j} - \cos(\theta_i - \theta_j) \ln \left(\frac{r_{i,j+1}}{r_{i,j}} \right) \right] \right) \\ &+ \frac{\gamma}{2\pi} \sum_{j=1}^N \left[\cos(\theta_i - \theta_j) \beta_{i,j} + \sin(\theta_i - \theta_j) \ln \left(\frac{r_{i,j+1}}{r_{i,j}} \right) \right] \end{aligned} \quad (11)$$

The coefficient of pressure at the midpoint of each panel can now be calculated by:

$$C_{P_i} = 1 - \left(\frac{V_{ti}}{V_\infty} \right)^2 \quad (12)$$

Example Solutions

The following are intermediate results based on a NACA 2412 airfoil using 10 panels.