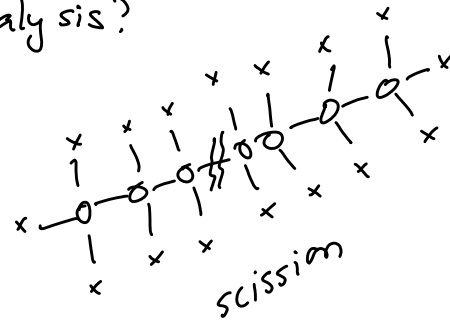
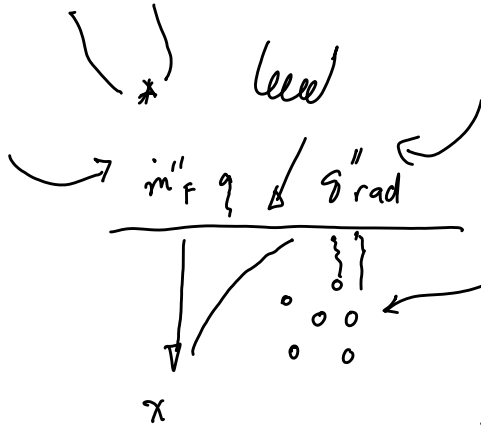


10/29/2010

THIS LECTURE

- * Thank Fraser for cookies!!
- * Thick & Thin Ignition of Solids
- * Examples

Why is valid to model ignition of solids using only heat transfer (conduction) analysis?



ignition requires a series of processes.

$$t_{ign} = t_{pyrolysis} + t_{mix} + t_{react}$$

heat the mat'l to point that fuel vapor escapes [1min] time for flammable mix [1sec] sufficiently energetic source [0.1ms]

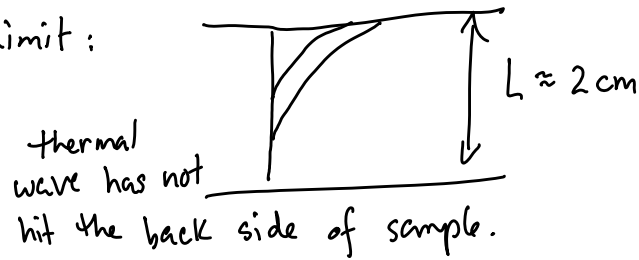
The time for ignition can be reasonably well approximated by the time required for pyrolysis.

Two limiting cases to analyze solid ignition.

Thin Limit & Thick Limit

- Thermally Thin Limit assumes a constant temperature in the solid. We use the Biot # $\frac{hL}{k}$ or some similar parameter to establish if the sample is thin.

- Thermally Thick Limit:



diffusion distance

$$\delta \approx \sqrt{\alpha t}$$

$$\alpha \equiv \frac{k}{\rho c} \quad \text{thermal diffusivity,}$$

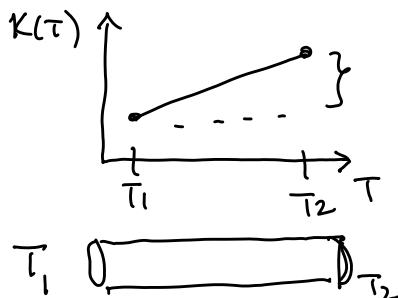
7.5 Calculate time to ignite (piloted) certain samples.

Radiative heat flux q''_{R} is $30 \frac{\text{KW}}{\text{m}^2}$,

The initial sample temperature is 25°C .

Assume samples are thick $\>$ that the convective heat transfer coeff is $15 \frac{\text{W}}{\text{m}^2\text{K}}$. Calculate the critical heat flux.

We are using constant properties. Is this justified & why/when?



$$K = K_0(1 + \alpha T)$$

$$K \frac{d^2 T}{dx^2} = 0 \quad \Leftrightarrow \quad \frac{d}{dx} \left(K \frac{dT}{dx} \right) = 0$$

$K \text{ const} \uparrow$ real eqn is above

$$\frac{\Delta K}{K} \ll 1 \quad \text{then assume const.}$$

The K_{gc} product specified is a calibrated parameter that allows the conduction model to represent experimental observations.

time to ignition

$$\frac{T_s - T_\infty}{\dot{q}''/h} = 1 - \exp(\gamma^2) \operatorname{erfc}(\gamma)$$

$\operatorname{erfc} \equiv$ complementary error function
 $= 1 - \operatorname{erf}()$

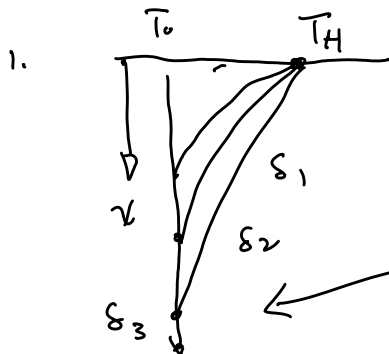
$$\gamma \equiv h \left(\frac{t}{K_{gc}} \right)^{1/2}$$

when $\gamma \ll 1 \quad t_{\text{ign}} \approx \frac{\pi}{4} K_{gc} \left(\frac{T_s - T_\infty}{\dot{q}''} \right)^2$

Thick Fuels

Heat Eon 1.D unsteady....

$$\rho c \frac{\partial T}{\partial t} = K \frac{\partial^2 T}{\partial x^2} \quad \text{subject to BC's \& I.C.}$$



Initial condition $T(x, t=0) = T_0$

Semi- ∞ domain $T(x \rightarrow \infty, t) = T_0$

3 Basics of $x=0$ condition.

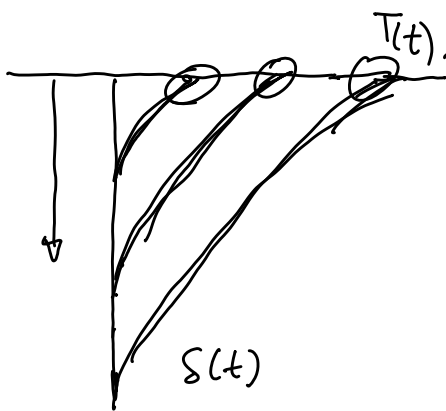
1. $T(x=0, t) = T_H$

solution is by Laplace transform, similarity transform.

$$\frac{x}{\delta(t)} = \eta$$

$$\delta \equiv \sqrt{\alpha t}$$

2. Constant heat flux



$$q_0'' = -K \frac{\partial T}{\partial x} \Big|_{x=0, t}$$

\uparrow const. \uparrow const.

$$q_0'' = +K \frac{T_{\text{surf}} - T_0}{\delta(t)}$$

$$q_0'' = \frac{K (T_{\text{surf}} - T_0)}{\sqrt{\alpha t}}$$

$$\frac{q_0'' \sqrt{\alpha t}}{K} = T_{\text{surf}} - T_0$$

$$T_{\text{surf}}(t) = T_0 + q_0'' \left(\frac{t}{K \rho c} \right)^{1/2}$$

$$\frac{\sqrt{\alpha}}{K} = \frac{1}{\sqrt{K \rho c}}$$

