

6.11

n-Octane spills on a hot pavement during a summer day. The pavement is at 40°C and heats the octane to this temperature. The wind temperature is at 33°C and the pressure is 1 atm. Use Table 6.1.

$$T_b := 125.6 + 273 \quad T_b = 398.6 \quad T_{inf} := 33 + 273 \quad T_L := 40 + 273 \quad T_L = 313$$

$$x_l := 0.0095 \quad x_u := .032 \quad h_{fg} := 0.305 \cdot 1000$$

$$R_{gas} := 8.314 \quad M_1 := 12 \cdot 8 + 18 \quad M_1 = 114$$

$$c_p := 2.2 \quad c_{pv} := 1.67 \quad \rho_l := 705$$

(a) If the octane interface is really at 40°C then it is simple to find

$$x_{lc} := \exp \left[ \left( \frac{-h_{fg} \cdot M_1}{R_{gas}} \right) \cdot \left( \frac{1}{T_L} - \frac{1}{T_b} \right) \right] \quad x_{lc} = 0.057$$

$$P_{lc} := x_{lc} \cdot 101 \quad \text{Conc} := \frac{P_{lc}}{R_{gas} \cdot T_{inf}} \quad \text{Conc} = 2.252 \times 10^{-3} \quad \frac{\text{kmole}}{\text{m}^3}$$

No spark, too rich

$$y_u := 4 \cdot \left( 1 - \frac{x_u}{x_{lc}} \right) \quad y_u = 1.744$$

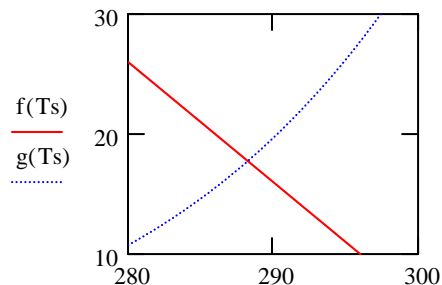
$$y_l := 4 \cdot \left( 1 - \frac{x_l}{x_{lc}} \right) \quad y_l = 3.33$$

But a more accurate solution is required. We assume a heat transfer coefficient

$$h_{inf} := 5$$

$$T_e := T_{inf} \quad h_e := h_{inf} \quad M_{air} := 29 \quad c_g := 1$$

$$f(T_s) := T_e - T_s \quad g(T_s) := \frac{M_1}{M_{air} \cdot c_g} \cdot \exp \left[ -h_{fg} \cdot \frac{M_1}{R_{gas}} \cdot \left( \frac{1}{T_s} - \frac{1}{T_b} \right) \right] \cdot [h_{fg} - c_{pl}(T_L - T_s)]$$



$$f(280) = 26 \quad g(280) = 10.732$$

$$f(300) = 6 \quad g(300) = 34.549$$

$$f(290) = 16 \quad g(290) = 19.663$$

$$f(288) = 18 \quad g(288) = 17.482$$

Figure 6.11

$$\begin{aligned}
 & T_s, T_s & T_{s1} &:= 288 \\
 Y_s &:= \frac{M1}{M_{air}} \cdot \exp \left[ -h_{fg} \cdot \frac{M1}{R_{gas}} \cdot \left( \frac{1}{T_{s1}} - \frac{1}{T_b} \right) \right] & Y_s &= 0.07 & X_s &:= \frac{Y_s \cdot M_{air}}{M1} \\
 x_{lc} &:= \exp \left[ \left( \frac{-h_{fg} \cdot M1}{R_{gas}} \right) \cdot \left( \frac{1}{T_{s1}} - \frac{1}{T_b} \right) \right] & x_{lc} &= 0.018 & X_s &= 0.018 \\
 Plc &:= x_{lc} \cdot 101 & Conc &:= \frac{Plc}{R_{gas} \cdot T_{inf}} & Conc &= 7.062 \times 10^{-4} \frac{\text{kmole}}{\text{m}^3}
 \end{aligned}$$

(b) surface falls in flammable range

$$\begin{aligned}
 y_u &:= 4 \cdot \left( 1 - \frac{x_u}{x_{lc}} \right) & y_u &= -3.196 \\
 y_l &:= 4 \cdot \left( 1 - \frac{x_l}{x_{lc}} \right) & y_l &= 1.864
 \end{aligned}$$

c Assume a linear distribution of fuel vapor over a 4 cm thick boundary layer. Determine the vertical region over which the mixture is flammable?

if the surface is a  $x=0.018$  (1.8%) and this mole fraction decays to zero over the 4 cm thickness of the boundary layer, we are asked to find the height that the mixture goes below 0.0095

$$z := \frac{x_l - x_{lc}}{-x_{lc}} \cdot 4 \qquad z = 1.864 \quad \text{cm}$$

it is no longer flammable above 1.86 cm.