

10/22/2010

THIS LECTURE

- Review of liquid evaporation
 - Example Problems
- (HW due on Weds)

Review

liquid

① assume T_{liq} specified
then $P_{vap, surf}$ specified
 $\{ X_{vap, surf} = \frac{P_{vap}}{P_{TOTAL}}$

$X_L < X_{vap, surf} < X_u$

② assume $h, h_m, T_\infty, Y_{vap, \infty}$
then under some conditions
shallow, insulated, well mixed
 $q'' = h(T_\infty - T_{surf}) = h_m(Y_{surf} - Y_\infty)$

$X = \frac{P_{vap}}{P_{TOTAL}} = \exp \left[-\frac{h_{fg} W}{R} \left(\frac{1}{T_{surf}} - \frac{1}{T_b} \right) \right]$

$Y_i = \frac{n_i W_i}{\sum n_j W_j} = \frac{x_i W_i}{\bar{W}_{mix}}$

3 eqns w/ 3 unknowns
 $T_{surf}, Y_{surf}, X_{surf}$

problem 6.5. CALCULATE VAPOR PRESS. OF LIQUIDS
AT 0°C . USE CC { TABLE G.1

a) n-octane b) methanol c) acetone

→ $C_m H_n O_s H_p$ } CALCULATE W_i molecular weight

	n-octane	
T_b	398 K	
h_{fg}	0.3 kJ/g	

eqn 6.18.
$$\frac{P}{P_{atm}} = \exp \left[\frac{h_{fg} W}{\bar{R}} \left(\frac{1}{T} - \frac{1}{T_b} \right) \right]$$

Problems 6.5 & 6.6 are similar.

Problem 6.13

a) compute the flashpoint temperature given

$$T_b = 40 + 273 \text{ K} \quad P_{TOT} = 101 \text{ kPa}, \quad c_{p,l} = 2, \quad \rho_l = 1330 \text{ kg/m}^3$$

$$X_L = 0.12 \dots$$

The procedure is to invert the C-C eqn for

$$T_{surf} \text{ in terms of } X = \frac{P_{vap}}{P_{TOT}}.$$

$$T = \left(\frac{1}{T_b} - \frac{\bar{R} \cdot \ln(X_L)}{h_{fg} W_i} \right)^{-1} \quad T = 266 \text{ K}$$

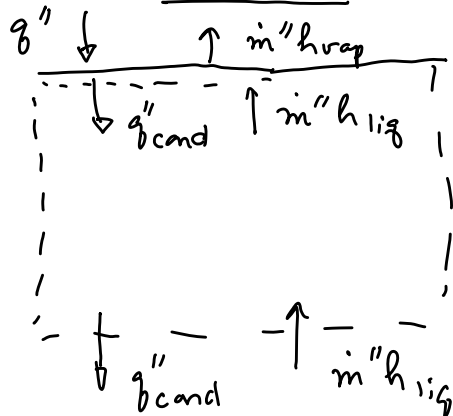
b) $T_{\infty} = 28^{\circ}\text{C}$, $Y_{\infty} = 0$, $h = 10 \frac{\text{W}}{\text{m}^2\text{K}}$, $h_m = \frac{h}{C_p}$

\uparrow mass transfer coeff
 \nwarrow okay to use air C_p .

liq

Assume deep pool.

What does deep pool mean?



$$q''_{\text{cond, top}} + m'' h_{\text{liq, bot}} = q''_{\text{cond, bot}} + m'' h_{\text{liq, top}}$$

if $q''_{\text{cond, bottom}} = 0$

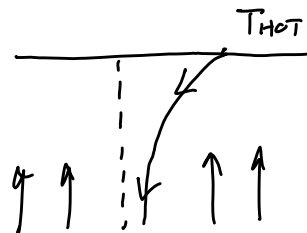
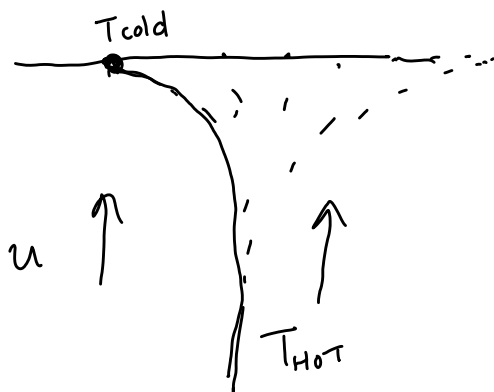
then

$$q''_{\text{cond, top}} = m'' C_p (T_{\text{surf}} - T_{\text{bottom}})$$

surface balance

$$q'' = \underbrace{m'' (h_{\text{vap}} - h_{\text{liq}})}_{\text{phase change process}} + \underbrace{q''_{\text{cond}}}_{\text{heat transfer into liquid}}$$

\uparrow
 in shallow pool we set this equal to zero.



$$\begin{aligned} \dot{q}''_{\text{external}} &= \dot{m}'' h_{fg} + \dot{m}'' c_p (T_{\text{surf}} - T_{\text{bottom}}) \\ &= \dot{m}'' \left[h_{fg} + \underbrace{c_p (T_{\text{surf}} - T_{\text{bottom}})}_{\text{correct for deep pools.}} \right] \end{aligned} \quad \text{eqn 6.34}$$

$$h(T_{\infty} - T_{surf}) = \underset{\uparrow}{\dot{m}''} [$$

Formally

energy eqn
applies in the
liquid.

$$\underbrace{\rho u c_p \frac{dT}{dx}}_{\text{convection}} = \underbrace{K \frac{d^2 T}{dx^2}}_{\text{conduction}}$$

$\overset{\text{top}}{\underset{\downarrow}{\overset{\uparrow}{n}}} \quad \text{We don't know } g_n = m''$

$$\begin{aligned} \dot{m}'' q_p (T_{\text{top}} - T_{\text{bottom}}) &= K \left. \frac{dT}{dx} \right|_{\text{top}} - K \left. \frac{dT}{dx} \right|_{\text{bottom}} \\ &= q_{\text{cond, top}} - \cancel{q_{\text{cond, bottom}}} \\ &= 0 \end{aligned}$$

solution is available

$$m''_{cp} f = K \frac{df}{dx}$$

$$\ln f = \int \frac{\ddot{m}}{K} C_p dx$$

you get an exponential function.

$$\exp\left(\frac{\rho u c_p x}{k}\right) = \exp\left(\frac{u x}{\alpha}\right) \quad \begin{array}{l} \text{characteristic} \\ \text{length.} \\ \alpha/u \end{array}$$

* For a deep pool, the depth $H \gg \alpha/u$.