



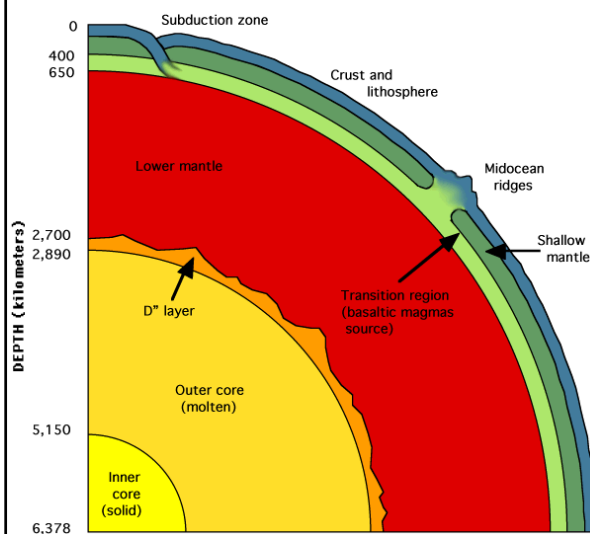
Geodynamics. Geodetic reference systems

- Geodynamics
 - Global tectonic (continental drift)
 - Postglacial land uplift
 - Sea level change,
 - Earth tide, permanent tides, direct vs indirect tides
- Celestial reference systems/frames
 - ICRS, ICRF
- Terrestrial reference systems/frames
 - ITRS, ITRF
- Existing terrestrial reference frames
 - ITRF ??, EUREF 89, WGS 84, SWEREF 99

1



Earth's interior



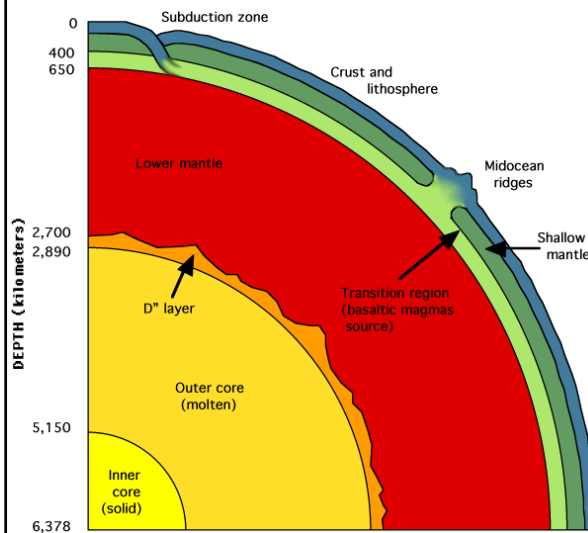
- Crust
- Upper mantle (lithosphere, asthenosphere, rest of upper mantle)
- Lower mantle
- Outer core
- Inner core

The Crust

- Solid materials
- 35km/6km thick
- $\rho = 2.67 \text{ g/cm}^3$
- 15-25° C

2

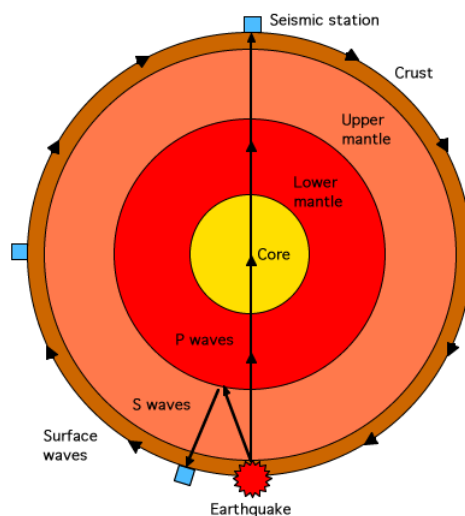
Earth's interior – Upper mantle



- viscoelastic,
- up to 700 km depth,
- $\rho = 3.3\text{-}4.1 \text{ g/cm}^3$
- lithosphere <100 km, asthenosphere <400 km
- Seismic waves change velocity on the boundary surface (Moho surface) between the crust and mantle

3

Surface waves & compression waves

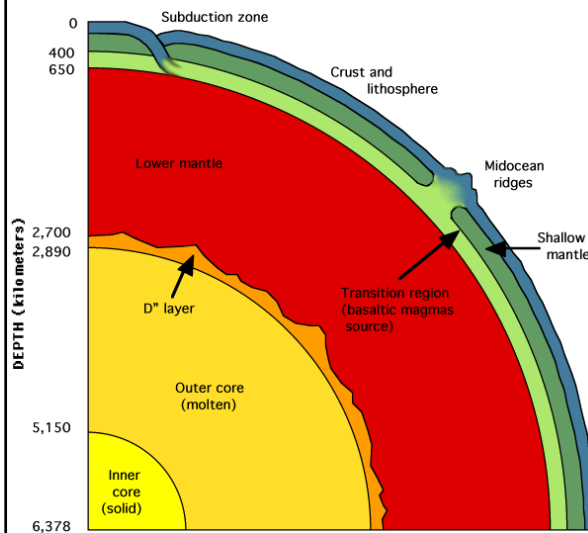


- S-waves (shear waves) travel along the surface at 4-7 km/s
- P-waves (compression) travel through the earth at 6-8 km/s
- P-waves change velocity at the crust-mantle boundary (Moho-surface)
- Seismic measurements are used to monitor earthquakes, atomic bombing tests and studies of the interior mass distribution inside the earth

4



Lower mantle, outer core, inner core

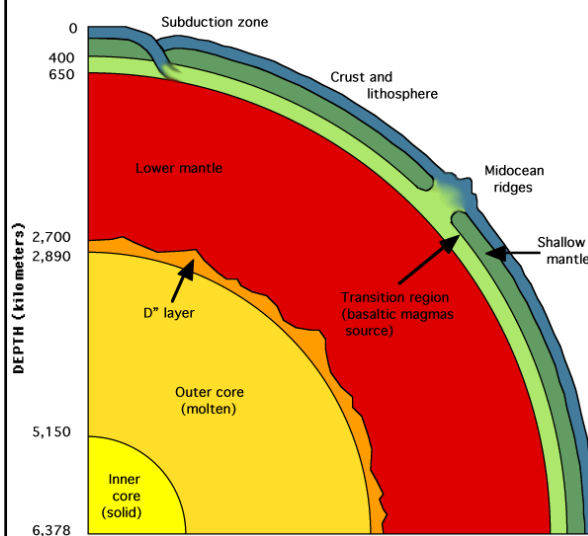


- Viscoelastic
- 700-2890 km
- $\rho = 4.2-5.6 \text{ g/cm}^3$
- Radioactivity in the lower mantle creates heating, 1200-2800° C
- Thermal convection in asthenosphere causes mantle convection
- Molten outer core
- solid inner core
- 2800-4000 ° C
- Thermal convection" inside the outer core creates geomagnetism

5



Mechanism of plate tectonics



- Radioactivity in the lower mantle warms up asthenosphere
- Cooler lithosphere floats above the warmer asthenosphere, meanwhile attracted by the earth's gravitational force
- **Mantle convection:** warmer mantle masses come up at *ocean ridges*, cooler lithosphere sinks at *ocean trenches*
- With mantle convection, the continents or different tectonic plates move in relation to each other.

6

Evidences of continental drift



- Bacon (1620): Africa's coasts fit South America
- Wegner (1920's): similar types/ages of vegetations, animal fossils on different continents
- Paleomagnetism (1950'): Rocks in Europa and North America show different magnetic North Poles
- Isostasy hypothesis "needs" a viscoelastic mantle
- Postglacial land uplift supports mantle's *viscoelasticity*
- Ocean bottoms' age increases at ocean ridges

7

Characteristics of global tectonics

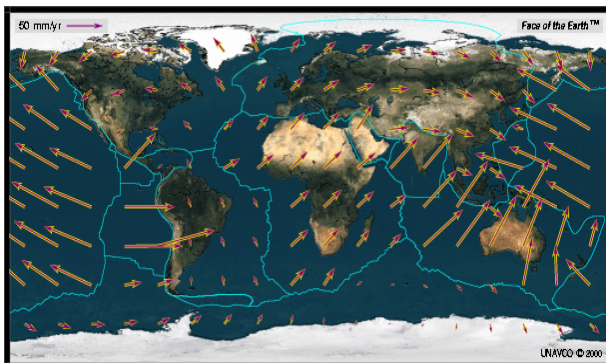


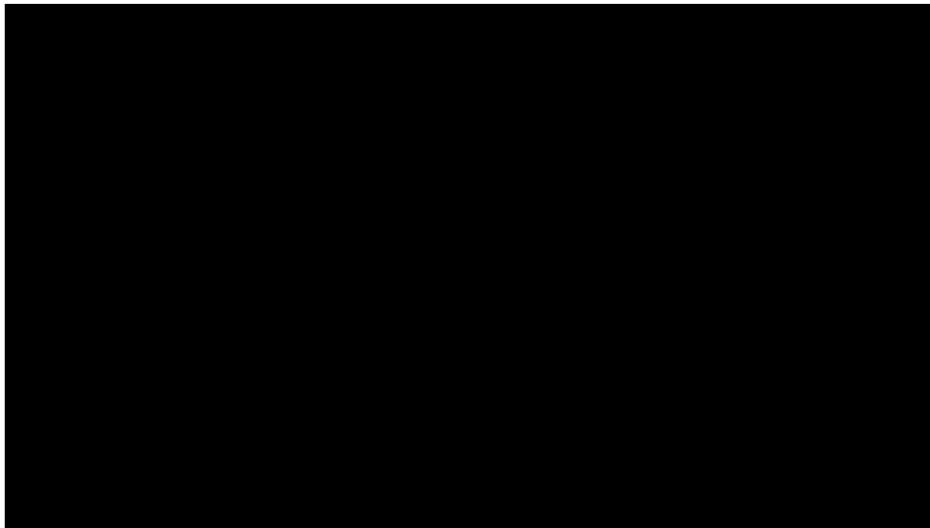
Plate motion model NUVEL-1A NNR

- The lithosphere is divided into several big plates: Euroasia, Pacific, North/South America, Africa, Indian, Antarctica
- **Subduction (convergence)** at ocean trenches: a heavier oceanic plate collides with and sinks below a lighter continental plate. Nazca-plate vs South America
- **Sea floor spreading (divergence)** at ocean ridges: mantle masses come up when two oceanic plates move away from each other. Ex: Mid-atlantic Ridge
- Earthquakes and vulcanos at plate borders. Ex: California, Japan, Southeast Asia, ...

8



Theory of Global Tectonics



9



Implication of Global Tectonics

- Geodetic points on the ground are moving !
- Coordinates of ground points are changing with time:
 - GRS must refer to a specific time epoch: SWEREF 99, ITRF 2000
 - Coordinates must refer to a specific time epoch
 - Velocity vectors must be computed together with position vectors
 - Helmert transformation parameters change with time
- Repeated geodetic measurements give direct determination of global tectonic movement velocity
 - Wegener's prediction comes true !

10

" This must be left to the geodesists.

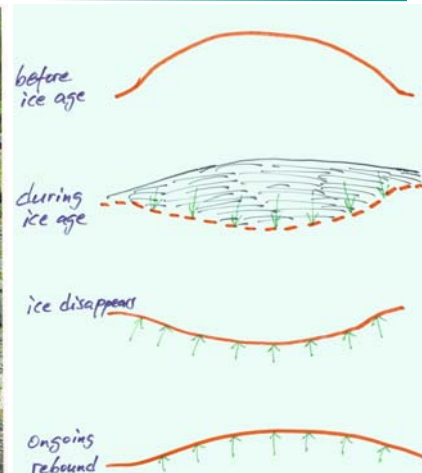
*I have no doubt that in the not too distant future we will be
successful in making a precise measurement of the drift of North
America relative to Europe. "*

Alfred Wegener , 1929

11

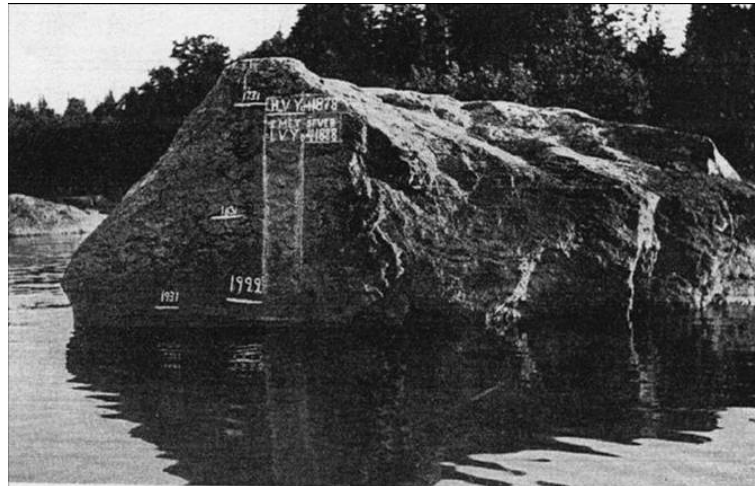


Land uplift - postglacial rebound



12

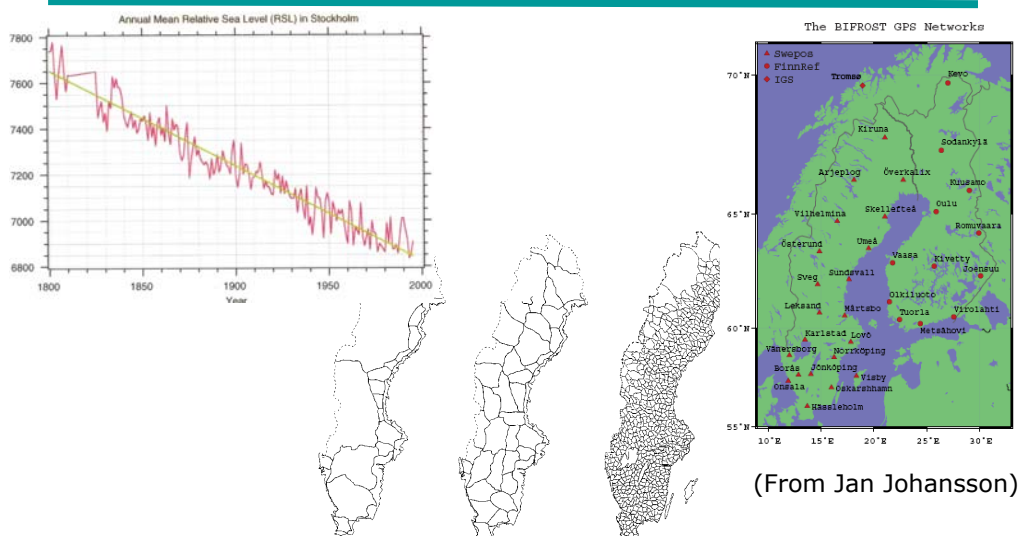
Land uplift or water sinking ???



Anders Celsius 1765

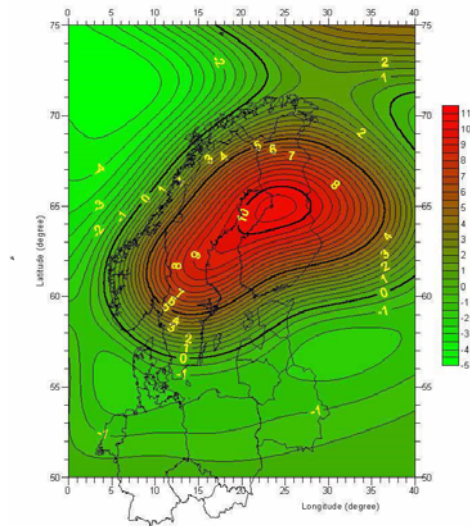
13

Determination of land uplift



14

Geophysical modelling of land uplift

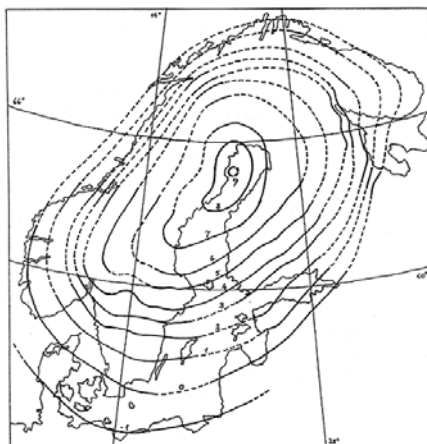


- Input data (ICE + PREM)
 - Ice history
 - Depth of the lithosphere
 - Viscosity of the upper mantle and the lower mantle
 - Gravity inside the earth
 - Density of the earth's interior
 - Seismic velocities
- Prediction:
 - Land uplift

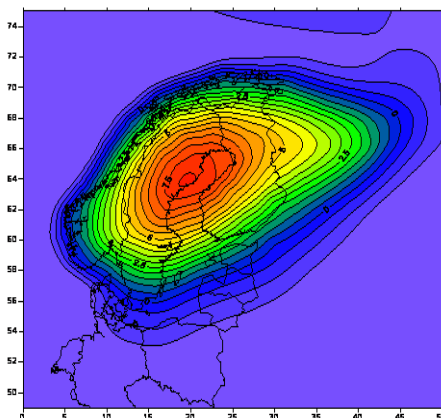
(Software by J Mitrovica, Department of Physics, University of Toronto, 1996)

15

Swedish land uplift model (mm/year)



Martin Ekman (1998)



RH 2000 LU Computed by LMV and based on data from repeated levellings, mareograph, permanent GPS & geophysical model

16



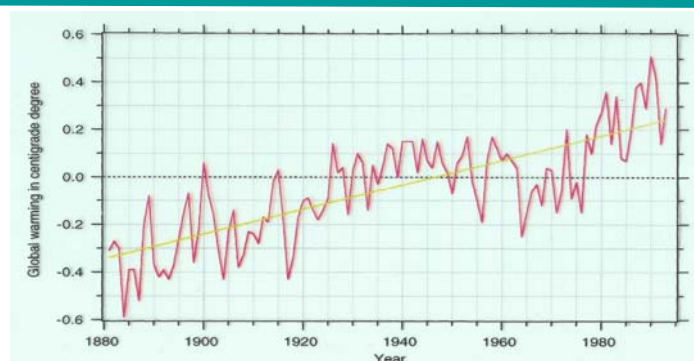
Implication of Land uplift for height determination

- Ground points will rise due to land upgift
- Heights of ground points will change with time
- Geodetic vertical reference systems must refer to a specific time epoch: RH 00, RH 70, RH 2000
- Geodetic heights (elliposidal or levelled) must refer to a specific time epoch
- Geoid model + land uplift: SWEN 08 LR

17



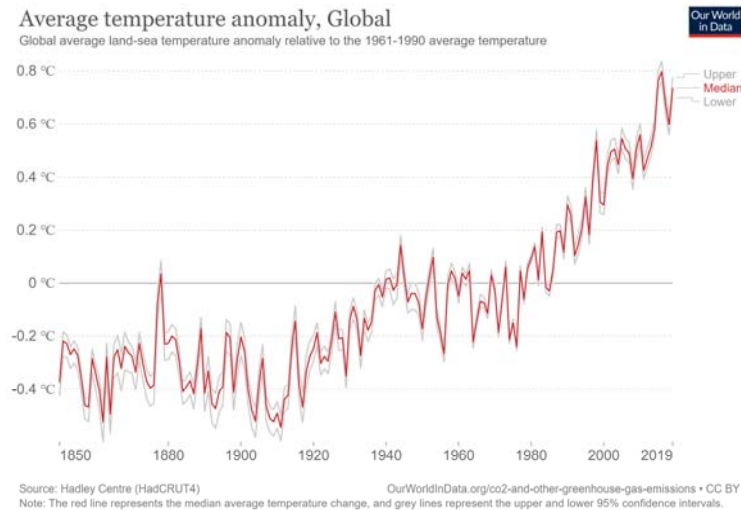
Global warming 1880-1995



- Polar ice to melt, water to expand, sea level to rise
- 1.7 mm/y (1870-2004), 2.7 mm/y (1993-2015)
- Effects of sea level rise and land uplift are mixed up

18

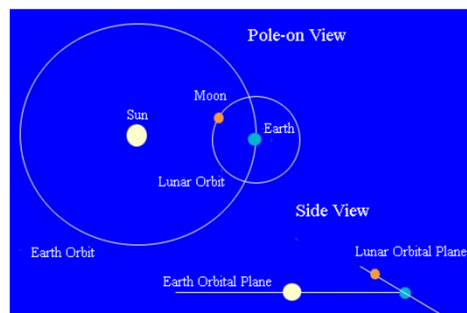
Global warming 1885-2019



19

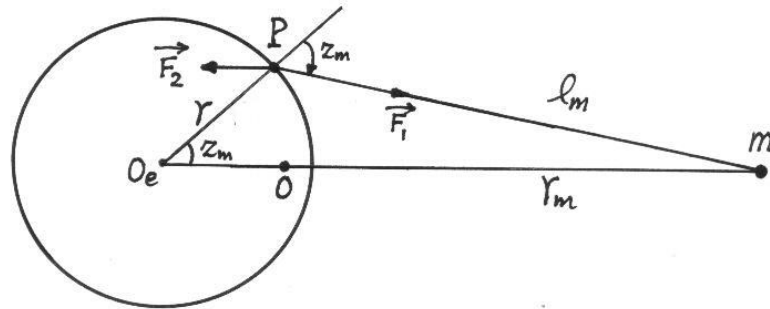
Earth Tide

- Tidal potential T
 - Earth-Moon system.
 - Tidal potential of the Moon
- Equilibrium earth tide
- Love's number, h , κ , l
- Observed earth tide
 - Observed tidal effect on
- **Permanent tidal effect**
 - Direct/indirect effects
 - 3 tidal systems



20

Tidal potential of the Moon



$$T^m = \frac{Gm}{\ell_m} - \left(\frac{Gm}{r_m} + Gm \frac{r}{r_m^2} \cos z_m \right)$$

21

Equilibrium tides for a rigid earth

Tidal effect on the geoid height for a rigid earth:

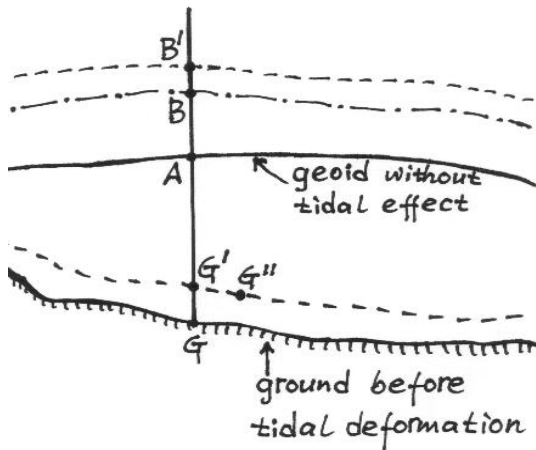
$$\delta N_0 \approx 26.7 \left(\cos 2z_m + \frac{1}{3} \right) + 12.3 \left(\cos 2z_s + \frac{1}{3} \right) \quad (cm)$$

Tidal effect on the gravity magnitude for a rigid earth:

$$\delta g_v \approx - \left(\frac{\partial \{T_2^m + T_2^s\}}{\partial r} \right)_{r=R} = - \frac{4D}{3R} \left(\frac{c}{r_m} \right)^3 (3 \cos^2 z_m - 1) - \frac{4D_s}{3R} \left(\frac{c_s}{r_s} \right)^3 (3 \cos^2 z_s - 1)$$

22

Earth deformation & Love's numbers



$$h = \frac{\overline{GG'}}{\overline{AB}}$$

$$k = \frac{\overline{BB'}}{\overline{AB}}$$

$$\ell = \frac{\overline{G'G''}}{\overline{AB}}$$

$$h \approx 0.62$$

$$k \approx 0.30$$

$$\ell \approx 0.085$$

$$\overline{AB} = \frac{T}{g}, \quad \overline{BB'} = \frac{\delta T}{g}$$

$$k = \frac{\delta T}{T}$$

23

Observed tides for a deformed earth

Observed geoid tide for a deformed earth:

$$\delta N = \overline{G'B'} - \overline{GA} = \overline{AB} + \overline{BB'} - \overline{GG'} = (1 + k - h) \cdot \overline{AB} = (1 + k - h) \cdot \delta N_0$$

Observed gravity tide for a deformed earth:

$$\delta g \approx \left(1 - \frac{3}{2}k + h\right) \cdot \delta g_v$$

24



Non-zero time-average

$$T_2 = D \left[\left(\frac{1}{3} - \sin^2 \phi \right) + 3 \left(\sin^2 \phi - \frac{1}{3} \right) \sin^2 \delta + \cos^2 \phi \cos^2 \delta \cos 2t + \sin 2\phi \sin 2\delta \cos t \right]$$

$$T_2 = D (T_z + T_s + T_t)$$

$$\overline{T_s} = \frac{1}{2\pi} \int_0^{2\pi} D \cdot T_s \, dt = 0$$

$$\overline{T_t} = \frac{1}{2\pi} \int_0^{2\pi} D \cdot T_t \, dt = 0$$

$$\overline{T_z} = \frac{1}{2\pi} \int_0^{2\pi} D \cdot T_z \, d\ell = D \left(\frac{1}{2} \sin^2 \varepsilon - \frac{1}{3} \right) \left(\sin^2 \phi - \frac{1}{3} \right)$$

The time-average of the tidal potential T_2 does not vanish. This causes **permanent tidal effects**, including **permanent deformation** of the solid earth.

25

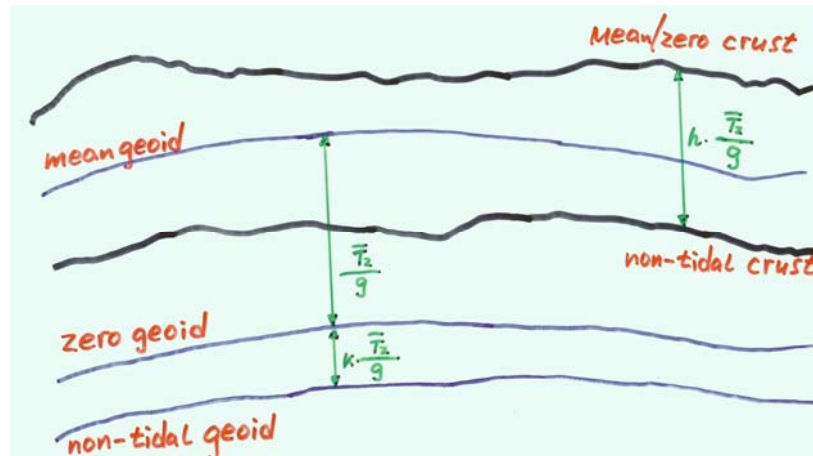


Permanent tide and tidal systems

- 4 parts of tidal effects
 - Direct (extra-terrestrial masses) vs indirect effects (earth's deformation)
 - Periodic vs permanent effects. Periodic effects can be averaged out.
 - Treatment of the permanent tide leads to 3 tidal systems
- Non-tidal model (Tide-free) (GNSS - ITRF)
 - Permanent deformation of the earth is *eliminated* → *earth's form changed*
 - Permanent tidal effects are *eliminated* from the measurements
- Zero tidal model (EVRS 2000)
 - Permanent deformation of the earth is *retained* → *masses outside the geoid*
 - Permanent tidal effects are *eliminated* in the measurements
- Mean tidal model
 - Permanent deformation of the earth is *retained*
 - Permanent tidal effects are *retained* → *included in the normal gravity field ?*

26

Tidal Systems: Non-Tidal, Mean vs Zero Tide



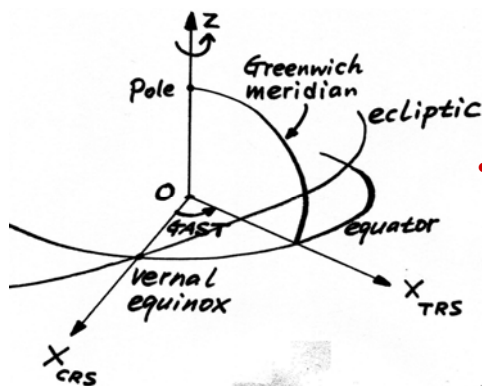
27

Tidal Systems: geoidal differences

Latitude FI	$3 \sin(FI)^2 - 1$	Geoid separation, cm	Geoid separation, cm	Crust separation, cm			
(degree)		Non-tidal - Zero	Zero - Mean	Non-tidal - Mean/zero			
0	-1,000000000	6,80	2,04	4,21	PI/180	0,017453293	D = 26206 cm**2/s**2
5	-0,977211630	6,64	1,99	4,12	YPSILON, deg	23,439291	g= 980 cm/s**2
10	-0,909538931	6,18	1,85	3,83	sin (YPSILON)	0,3977772	D/g 26,741 cm
15	-0,799038106	5,43	1,63	3,37			T0 -6,79805
20	-0,649066665	4,41	1,32	2,74			
25	-0,464181415	3,16	0,95	1,96			
30	-0,250000000	1,70	0,51	1,05			
35	-0,013030215	0,09	0,03	0,05			
40	0,239527733	-1,63	-0,49	-1,01			
45	0,500000000	-3,40	-1,02	-2,11			
50	0,760472267	-5,17	-1,55	-3,21			
55	1,013030215	-6,89	-2,07	-4,27			
60	1,250000000	-8,50	-2,55	-5,27			
65	1,464181415	-9,95	-2,99	-6,17			
70	1,649066665	-11,21	-3,36	-6,95			
75	1,799038106	-12,23	-3,67	-7,58			
80	1,909538931	-12,98	-3,89	-8,05			
85	1,977211630	-13,44	-4,03	-8,33			
90	2,000000000	-13,60	-4,08	-8,43			

28

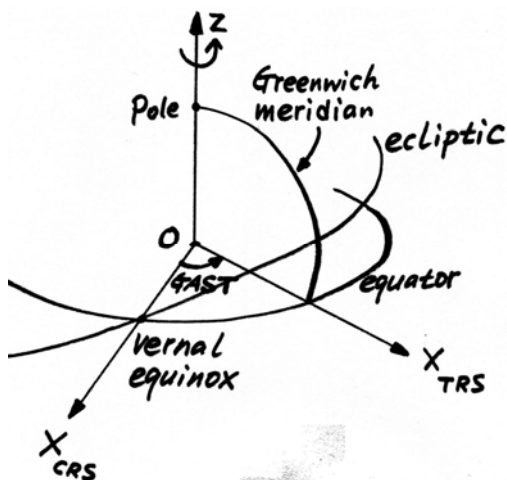
Reference system vs reference frame



- Definition of the origin and the orientation of the 3 coordinate axes, together with related assumptions, is called a **reference system**
- A network of ground points or celestial bodies, at which the coordinates and velocities in a certain reference system have been explicitly specified, is called a **reference frame** which is an realization of the (theoretical) reference system

29

International Celestial Reference System (ICRS)



- Origin at the barycentre (practically at geocentre)
- Z-axis toward the *mean celestial North Pole* at **J2000.0**
- X-axis toward the *mean equinox* at J2000.0
- Y-axis follows to form a right-handed system

30



IERS

- IERS, **International Earth Rotation Service**, was established in 1987 by IAU and IUGG to replace
 - International Polar Motion Service (IPMS)
 - Bureau International de l'Heure (BIH)
- Renamed in 2003 as **International Earth Rotation and Reference Systems Service**

31



International Celestial Reference Frame (ICRF)

- First realization of ICRS, **ICRF1**, is made by IAU in 1997 based on VLBI measurements of 212 defining radio sources
- Two extensions of ICRF1 are made by IERS in 1999 and 2004
- Second realization of ICRS, **ICRF2**, is made in 2009
 - VLBI measurements of 3414 radio sources
 - 295 defining radio sources

32



International Celestial Reference Frame (ICRF2)

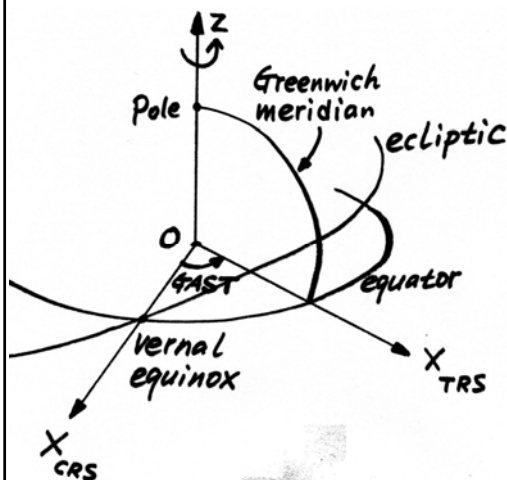
Coordinates of 295 ICRF2 defining sources

ICRF Designation (1)	IERS Des. (2)	Right Ascension J2000.0			Declination J2000.0			Uncertainty	
		h	m	s	°	'	"	R.A. s	Dec. "
ICRF J000435.6-473619	0002-478	00	04	35.65550384	-47	36	19.6037899	0.00001359	0.0002139
ICRF J001031.0+105829	0007+106	00	10	31.00590186	10	58	29.5043827	0.00000491	0.0000930
ICRF J001101.2-261233	0008-264	00	11	01.24673846	-26	12	33.3770171	0.00000660	0.0000936
ICRF J001331.1+405137	0010+405	00	13	31.13020334	40	51	37.1441040	0.00000482	0.0000683
ICRF J001611.0-001512	0013-005	00	16	11.08855479	-00	15	12.4453413	0.00000435	0.0001005
ICRF J001945.7+732730	0016+731	00	19	45.78641940	73	27	30.0174396	0.00000989	0.0000424
ICRF J002232.4+060804	0019+058	00	22	32.44120914	06	08	04.2690807	0.00000439	0.0000956
ICRF J003824.8+413706	0035+413	00	38	24.84359231	41	37	06.0003032	0.00000499	0.0000613
ICRF J005041.3-092905	0048-097	00	50	41.31738756	-09	29	05.2102688	0.00000278	0.0000428
ICRF J005109.5-422633	0048-427	00	51	09.50182012	-42	26	33.2932480	0.00000932	0.0001177
ICRF J010245.7+582411	0059+581	01	02	45.76238248	58	24	11.1366009	0.00000523	0.0000414
ICRF J010645.1-403419	0104-408	01	06	45.10796851	-40	34	19.9602291	0.00000376	0.0000455
ICRF J010915.4-604948	0107-610	01	09	15.47520598	-60	49	48.4599686	0.00001744	0.0001750
ICRF J011205.8+224438	0109+224	01	12	05.82471754	22	44	38.7863909	0.00000379	0.0000653
ICRF J011327.0+494824	0110+495	01	13	27.00680344	49	48	24.0431742	0.00000597	0.0000727
ICRF J011857.2-214130	0116-219	01	18	57.26216666	-21	41	30.1399986	0.00000683	0.0001138
ICRF J012141.5+114950	0119+115	01	21	41.59504339	11	49	50.4131012	0.00000279	0.0000429
ICRF J013305.7-520003	0131-522	01	33	05.76255607	-52	00	03.9457209	0.00001218	0.0001605

33



International Terrestrial Reference System (ITRS)



- Origin at the earth's centre of masses including the oceans and the atmosphere
- Z-axis toward the **CIO** (IRP - IERS Reference Pole)
- X-axis along intersection of the equator and the Greenwich Meridian
- Y-axis inside the equator to form a right-handed system

34



International Terrestrial Reference Frame

- ITRF is realization of ITRS
- ITRF networks consists of stations all over the world, measured by 4 space geodetic methods
 - 1) Very Long Baseline Interferometry (VLBI)
 - 2) Satellite Laser Ranging (SLR)
 - 3) GNSS
 - 4) Doppler Orbitography Integrated by Satellites (DORIS)
- Final products include:
 - Position **coordinates** and **velocities** for a reference epoch
 - **Transformation parameters** and their time derivatives
 - Consistent estimates of 5 **EOP**

35



Earth Orientation Parameters (EOP)

- 2 Polar coordinates with respect to CIO : x_p, y_p
- 2 Nutation parameters :
 - nutation in obliquity ($\Delta\epsilon$)
 - nutation in longitude ($\Delta\Psi$)
- 1 time parameter
 - UTC-UT1 (provide UT1 when UTC is known)
- EOPs are estimated and distributed by IERS
- EOPs relate (X, Y, Z) defined in ICRF to (x, y, z) defined in ITRF

36



Transformation from ICRF to ITRF

$$\begin{bmatrix} x \\ y \\ z \end{bmatrix} = R_p(x_p, y_p) \cdot R_3(GAST) \cdot N(\varepsilon_0, \Delta\varepsilon, \Delta\psi) \cdot P(z, \vartheta, \xi) \cdot \begin{bmatrix} X \\ Y \\ Z \end{bmatrix}$$

$$P(z, \vartheta, \xi) = R_3(-z) \cdot R_2(\vartheta) \cdot R_3(-\xi)$$

$$= \begin{bmatrix} +\cos z \cos \vartheta \cos \xi - \sin z \sin \xi & -\cos z \cos \vartheta \sin \xi - \sin z \cos \xi & -\cos z \sin \vartheta \\ +\sin z \cos \vartheta \cos \xi + \cos z \sin \xi & -\sin z \cos \vartheta \sin \xi + \cos z \cos \xi & -\sin z \sin \vartheta \\ +\sin \vartheta \cos \xi & -\sin \vartheta \sin \xi & +\cos \vartheta \end{bmatrix}$$

$$N_{3 \times 3}(\varepsilon_0, \Delta\varepsilon, \Delta\psi) = R_1(-\varepsilon) \cdot R_3(-\Delta\psi) \cdot R_1(\varepsilon_0) \quad (\varepsilon = \varepsilon_0 + \Delta\varepsilon)$$

$$= \begin{bmatrix} \cos \Delta\psi & -\sin \Delta\psi \cos \varepsilon_0 & -\sin \Delta\psi \sin \varepsilon_0 \\ \sin \Delta\psi \cos \varepsilon & +\cos \Delta\psi \cos \varepsilon \cos \varepsilon_0 + \sin \varepsilon \sin \varepsilon_0 & +\cos \Delta\psi \cos \varepsilon \sin \varepsilon_0 - \sin \varepsilon \cos \varepsilon_0 \\ \sin \Delta\psi \sin \varepsilon & +\cos \Delta\psi \sin \varepsilon \cos \varepsilon_0 - \cos \varepsilon \sin \varepsilon_0 & +\cos \Delta\psi \sin \varepsilon \sin \varepsilon_0 + \cos \varepsilon \cos \varepsilon_0 \end{bmatrix}$$

37



Computation of *GAST*

$$\varepsilon_0 = 23^0 26' 21.448'' - 46.8150'' \cdot T - 0.00059'' \cdot T^2 + 0.001813'' \cdot T^3$$

$$\left. \begin{aligned} \xi &= 2306.2181 \cdot T + 0.30188 \cdot T^2 + 0.017998 \cdot T^3 \\ z &= 2306.2181 \cdot T + 1.09468 \cdot T^2 + 0.018203 \cdot T^3 \\ \vartheta &= 2004.3109 \cdot T - 0.42665 \cdot T^2 - 0.041833 \cdot T^3 \end{aligned} \right\} \quad (\text{unit: arcsecond})$$

$$T = \frac{JD(t) - J2000.0}{36525} = \frac{JD(t) - 2\,451\,545.0}{36525}$$

$$GAST = (GMST)_0 + 1.002\,737\,909\,35 \cdot UT1 + \Delta\psi \cos \varepsilon_0$$

$$(GMST)_0 = 24\,110.54841^s + 8\,640\,184.812866^s T_0 + 0.093\,104^s T_0^2 - 6.2^s \cdot 10^{-6} T_0^3$$

$$T_0 = \frac{JD_{UT=0} - 2\,451\,545.0}{36525}$$

38



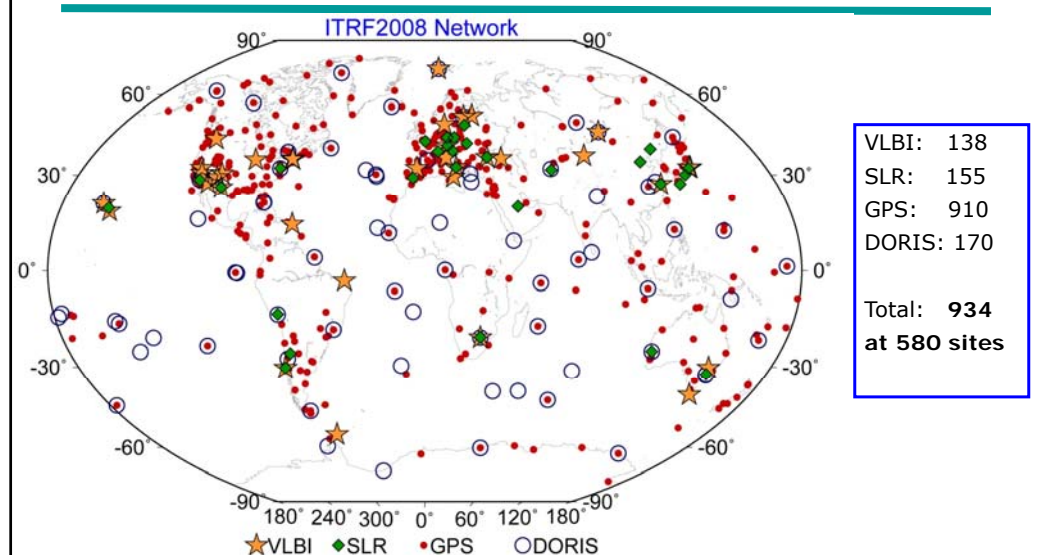
List of ITRF solutions

• ITRF88	• 1988.0 reference epoch
• ITRF89	• 1988.0
• ITRF92	• 1988.0
• ITRF93	• 1988.0
• ITRF94	• 1997.0
• ITRF96	• 1997.0
• ITRF97	• 1997.0
• ITRF2000	• 1997.0
• ITRF2005	• 2000.0
• ITRF2008	• 2005.0
• ITRF2014	• 2010.0

39



Global Network of ITRF 2008



40



ITRF 2008

- Computations in 3 steps
 - 1) Each type (VLBI,SLR,GPS,DORIS) is processed separately to produce weekly (daily VLBI) time series of positions and EOP
 - 2) Above results are combined to estimate position coordinates for epoch 2005.0, velocity and daily EOP
 - 3) Combination with local survey at co-locating stations
- ITRF 2008 results:
 - Origin and scale are defined by SLR data
 - Orientation is defined by average of VLBI and SLR data
 - Scale accuracy: **1 ppb, 0.05 ppb/year** (VLBI-SLR agreement)
 - Origin accuracy: at the level of or better than **1 cm**

41



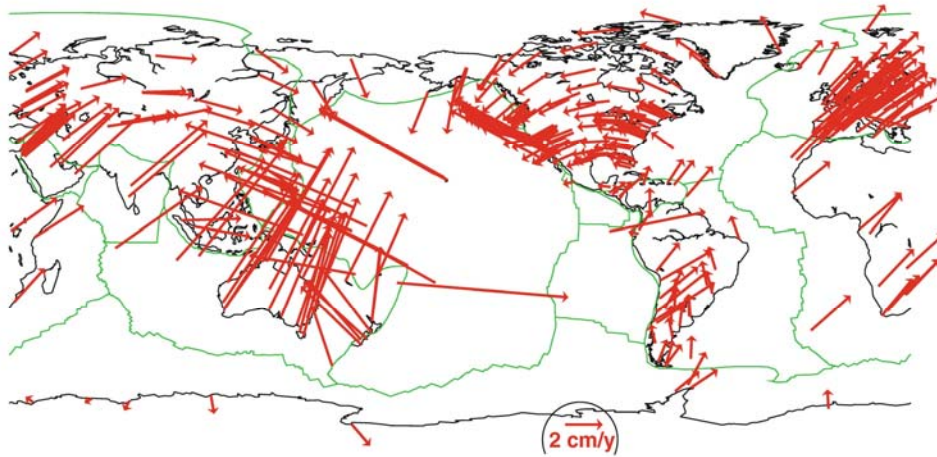
Station coordinates/velocities of ITRF 2008

10	VELX	7205	A	1	05:001:00000	m/y	2	-0.154701843128797E-01	0.47543E-04
11	VELY	7205	A	1	05:001:00000	m/y	2	-0.121094247184766E-02	0.62981E-04
12	VELZ	7205	A	1	05:001:00000	m/y	2	0.408529863128065E-02	0.69402E-04
13	STAX	7204	A	1	05:001:00000	m	2	0.882879772507557E+06	0.13845E-02
14	STAY	7204	A	1	05:001:00000	m	2	-0.492448231271830E+07	0.35634E-02
15	STAZ	7204	A	1	05:001:00000	m	2	0.394413070534473E+07	0.27791E-02
16	VELX	7204	A	1	05:001:00000	m/y	2	-0.143669405946909E-01	0.81983E-04
17	VELY	7204	A	1	05:001:00000	m/y	2	-0.102511002663171E-02	0.20579E-03
18	VELZ	7204	A	1	05:001:00000	m/y	2	0.274104971026836E-02	0.17380E-03
19	STAX	7216	A	1	05:001:00000	m	2	-0.132421109976204E+07	0.97620E-03
20	STAY	7216	A	1	05:001:00000	m	2	-0.533202313706689E+07	0.15257E-02
21	STAZ	7216	A	1	05:001:00000	m	2	0.323211831880121E+07	0.11575E-02
22	VELX	7216	A	1	05:001:00000	m/y	2	-0.126619959048342E-01	0.51526E-04
23	VELY	7216	A	1	05:001:00000	m/y	2	0.339720116768070E-03	0.84921E-04
24	VELZ	7216	A	1	05:001:00000	m/y	2	-0.467559096977887E-02	0.69110E-04
25	STAX	7213	A	1	05:001:00000	m	2	0.337060591485963E+07	0.65329E-03
26	STAY	7213	A	1	05:001:00000	m	2	0.711917602784800E+06	0.54467E-03
27	STAZ	7213	A	1	05:001:00000	m	2	0.534983082091565E+07	0.69138E-03
28	VELX	7213	A	1	05:001:00000	m/y	2	-0.142016652825457E-01	0.54415E-04
29	VELY	7213	A	1	05:001:00000	m/y	2	0.145280633229021E-01	0.36261E-04
30	VELZ	7213	A	1	05:001:00000	m/y	2	0.103568368182873E-01	0.76909E-04
31	STAX	7203	A	1	05:001:00000	m	2	0.403394735308593E+07	0.30487E-02
32	STAY	7203	A	1	05:001:00000	m	2	0.486990645775994E+06	0.11888E-02
33	STAZ	7203	A	1	05:001:00000	m	2	0.490043088922310E+07	0.34356E-02
34	VELX	7203	A	1	05:001:00000	m/y	2	-0.137947899098904E-01	0.23546E-03

42



Horizontal velocity from ITRF 2008

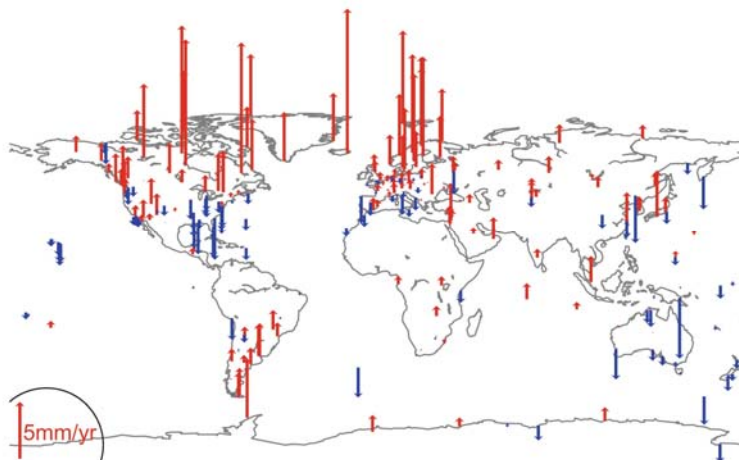


406 stations have formal errors $< 0.2\text{mm/year}$

43



Vertical velocity from ITRF 2008



278 stations have formal errors $< 0.2\text{mm/year}$

44



Transformation between different ITRF

$$\begin{bmatrix} X \\ Y \\ Z \end{bmatrix}_{ITRF_{yy}} = \begin{bmatrix} X \\ Y \\ Z \end{bmatrix}_{ITRF\ 2000} + \begin{bmatrix} T_1 \\ T_2 \\ T_3 \end{bmatrix} + \begin{bmatrix} \delta & -\omega_Z & \omega_Y \\ \omega_Z & \delta & -\omega_X \\ -\omega_Y & \omega_X & \delta \end{bmatrix} \begin{bmatrix} X \\ Y \\ Z \end{bmatrix}_{ITRF\ 2000}$$

$$T_1(t) = T_1(t_0) + \left(\frac{dT_1}{dt}\right) \cdot (t - t_0)$$

45



Remarks on ITRF

- With ITRF, a internationally common reference system has been established for positioning, navigation and space applications
- ITRF-related work demonstrated geodesy's contribution to basic sciences as well as current problems related to global change
- Achievable accuracy of latest ITRF: **1cm, 1ppb**
- It is desirable for all the countries to go over to ITRF-based or ITRF-connected GRS.

46



Reference systems of GNSS (=ITRS)

- GPS
 - WGS 84, defined in 1987 using TRANSIT observations. **1-2 m**
 - WGS 84 (G730) defined in 1994, WGS 84 (G873) defined in 1996, agrees with **ITRF94** at **10cm** level
 - WGS 84 (G1150), defined in 2002, agrees with **ITRF2005** up to **1cm**
- GLONASS
 - PZ-90, defined in 1990 using 26 ground stations
 - Agrees with ITRF at **meter level** (from a joint campaign in 1999)
- Galileo
 - GTRF agrees with ITRF within **1.5cm**

47



Navy Navigation Satellite System (NNSS)

- Developed for US strategic nuclear submarines (Polaris) in 1960's
- 6 polar satellites at 600km
- 4 ground monitoring stations defining **World Geodetic System 1972**
- Doppler effects of satellite signals are measured by ground receivers
- 10 metres accuracy achieved with dual frequency receivers
- Also called TRANSIT or Doppler system



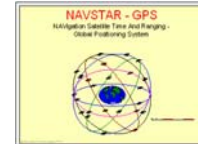
Swedish west coast was probably the best place for Polaris submarines to launch missile attacks toward Moscow ?

48



World Geodetic System 1984 (WGS 84)

- GPS = a new satellite navigation system to replace TRANSIT
 - Space segment: 24 satellites in 3 orbits, 55° inclination, 22000km altitude
 - Control segment: 6 Air Force OCS monitoring stations
 - User segment: GPS receivers
- WGS 84 \approx Conventional TRS
 - Origin at the earth's centre of masses including atmosphere/oceans
 - Z-axis toward CIO, as defined by the IERS Reference Pole (IRP)
 - X-axis along intersections of the equator and Greenwich Meridian
- Realization of WGS 84
 - 6 OCS stations determined by NNSS (TRANSIT) in 1987
 - Parameters: $a = 6378137\text{m}$, $GM = 3.986005 \cdot 10^{14}$, C_{20} , ω , $1/f = 298.257223563$
 - Estimated accuracy: ≈ 1 metre
- TRANSIT-derived WGS 84 is less precise than GPS measurements !



49



Ellipsoids of WGS 84 and GRS 80

Parameters	Values of WGS 84	Values of GRS 80
<i>Defining parameters</i>		
Semi-major axis a	6 378 137 m	6 378 137 m
Gravitational constant GM	$0.398\,600\,5 \cdot 10^{14} \text{ m}^3 \text{ s}^{-2}$	$0.398\,600\,5 \cdot 10^{14} \text{ m}^3 \text{ s}^{-2}$
Normalized dynamic factor C_{20}	$-0.4\,84\,166\,85 \cdot 10^{-2}$	
Non-normalized factor $J_2 (= -\sqrt{5}C_{20})$		$0.108\,263 \cdot 10^{-2}$
Angular velocity ω	$0.729\,211\,5 \cdot 10^{-5} \text{ rad s}^{-1}$	$0.729\,211\,5 \cdot 10^{-5} \text{ rad s}^{-1}$
<i>Derived Parameters</i>		
Semi-minor axis b	6 356 752.314 2 m	6 356 752.314 1 m
Flattening ($1/f$)	298.257 223 563	1/298.257 222 101
First eccentricity (e^2)	0.006 694 380 004	0.006 694 380 023

50



WGS 84 (G703, G873)

- Same system definition – ITRS
- Realization of WGS 84 (G873)
 - 6 OCS, 13 NIMA, 18 IGS are surveyed by GPS in 1996
 - Coordinates of 12 IGS fiducial stations in ITRF 94 are held fixed
 - Coordinates of all other stations are computed in ITRF94
 - New parameters:
 - $a = 6378137$ m, $1/f = 298.257223563$, $GM = 3.986004418 \times 10^{14}$, ω
 - orbits defined by EGM96
 - Final coordinates consistent with ITRF within 10 cm

51



NIMA and Air Force OCS Tracking Stations

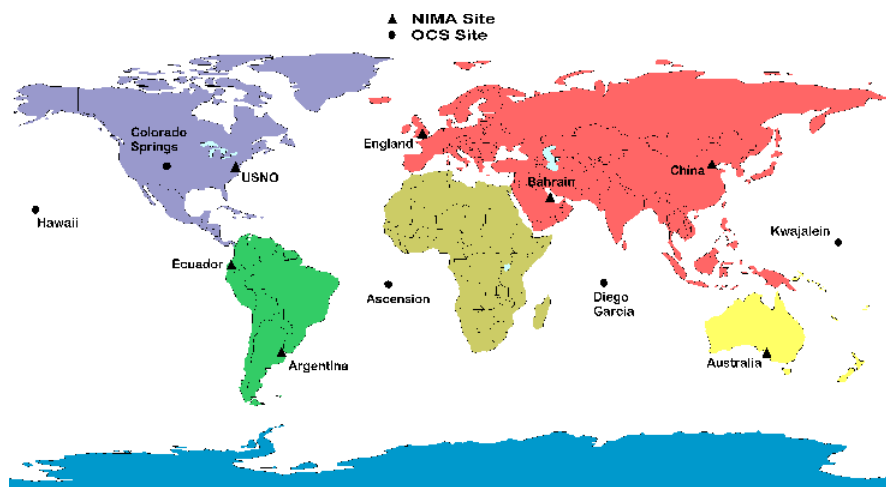


Figure 1. Continuum of WGS84-ITRF94

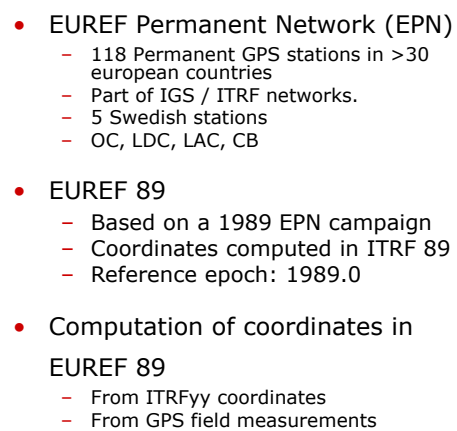
52

□ OCS/NIMA
 * IGS EDUCIAL
 * IGS ADDITIONAL
 x NIMA ADDITIONAL

2



EUropean REference Frame EUREF 89



27



Computation of Coordinates in EUREF 89

- From coordinates in ITRFyy
 - Compute ITRFyy coordinates at epoch 1989.0
 - Transform into EUREF 89 coordinates
 - Compute velocity in EUREF 89
- From GPS measurements made at epoch t_c
 - Carry out field measurements at epoch t_c (epoch of middle measurements)
 - Transform ITRFyy coordinates of fiducial stations referred to epoch t_0 into coordinates referred to central measurement epoch t_c
 - Process GPS measurements to obtain ITRFyy coordinates referred to epoch t_c
 - Convert into EUREF 89 coordinates at epoch t_c
 - Convert into EUREF 89 coordinates at epoch 89.0

55



Swedish 3D reference systems



- SWEPOS - 21 permanent GPS stations (25 since March 2000)
 - Realization of Swedish 3D reference systems
 - Monitoring GNSS system integrity
 - Support network-RTK – VRS(Virtual Reference Station) (70km, 1-2cm (H), 2-3cm (V))
- SWEREF 93
 - 4 Swedish GPS stations in EUREF 89 campaign
 - 23 GPS stations in DOSE campaign, computed in ITRF 91 at epoch 1993.6
 - 11 DOSE points (5 Swedish) are fitted to EUREF coordinates
 - The final set of coordinates is named **SWEREF 93**

56



3D reference system SWEREF 99



- Based on a Nordic GPS campaign in 1999, with 49 stations incl. 25 SWEPOS stations
- Coordinates computed in ITRF97 for 1999.5
- Transformed to EUREF89 for 1989.0
- Adopted in 2000 as a realisation of ETRS 89
- Introduced in 2001 as Swedish national reference frame **SWEREF 99**
- Tectonic epoch: 1989.0
- Height epoch: 1999.5 (GPS campaign)
- Ellipsoid: GRS 1980

57



Transform SWEREF 99 to RT 90/RH 2000

$$\begin{bmatrix} X \\ Y \\ Z \end{bmatrix}_{RT\ 90} = \begin{bmatrix} \delta x \\ \delta y \\ \delta z \end{bmatrix} + (1 + \delta s) \cdot R(\alpha_1, \alpha_2, \alpha_3) \cdot \begin{bmatrix} X \\ Y \\ Z \end{bmatrix}_{SWEREF\ 99}$$



$$\begin{aligned} \delta x &= -414.0979 \text{ metres} \\ \delta y &= -41.3381 \text{ metres} \\ \delta z &= -603.0627 \text{ metres} \\ \delta s &= +0.000\ 000\ 000\ 0 \cdot 10^{-6} \\ \alpha_1 &= -0.855\ 043\ 431\ 4'' \\ \alpha_2 &= +2.141\ 346\ 518\ 5'' \\ \alpha_3 &= -7.022\ 720\ 951\ 6'' \end{aligned}$$

58