



# Astrogeodetic triangulation and geodetic datums

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- General procedure of astrogeodetic triangulation
- Geodetic datum (Ellipsoidal datum)
- Local triangulation-based coordinate systems versus global, GNSS-based coordinate systems

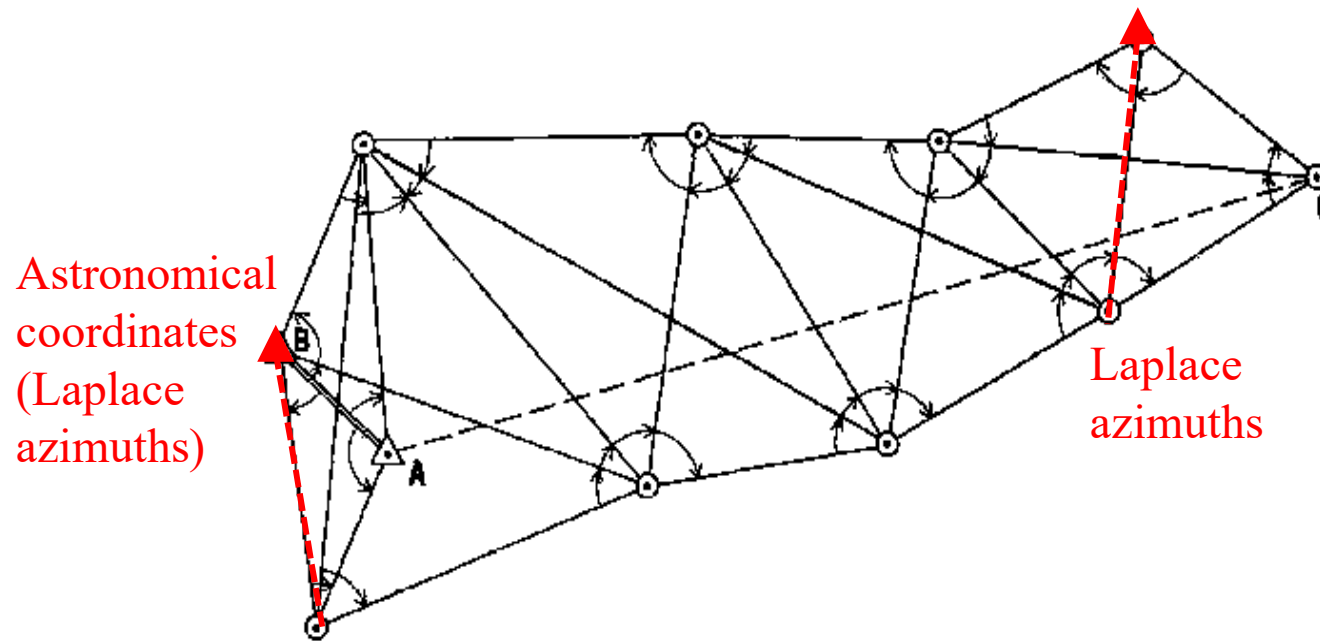


# General procedures

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- Select a reference ellipsoid and define a *datum*
- Design a network of triangles
- Astronomical observations (*a few*)
- Geodetic measurements (angles, distances etc)
- Reduction of ground measurements to the ellipsoid
- Least squares adjustment on the ellipsoid
- Define an official 2D coordinate system
- Re-estimation of new ellipsoidal parameters

# Principle of Triangulation





# Astrogeodetic networks

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- Networks are divided into orders: 1st, 2nd, 3rd
- 1st-order network contains triangle chains
- 2nd-order networks fill in between 1st-order chains
- Triangle chains along meridians/parallels
- Ground points on top of mountains, with towers

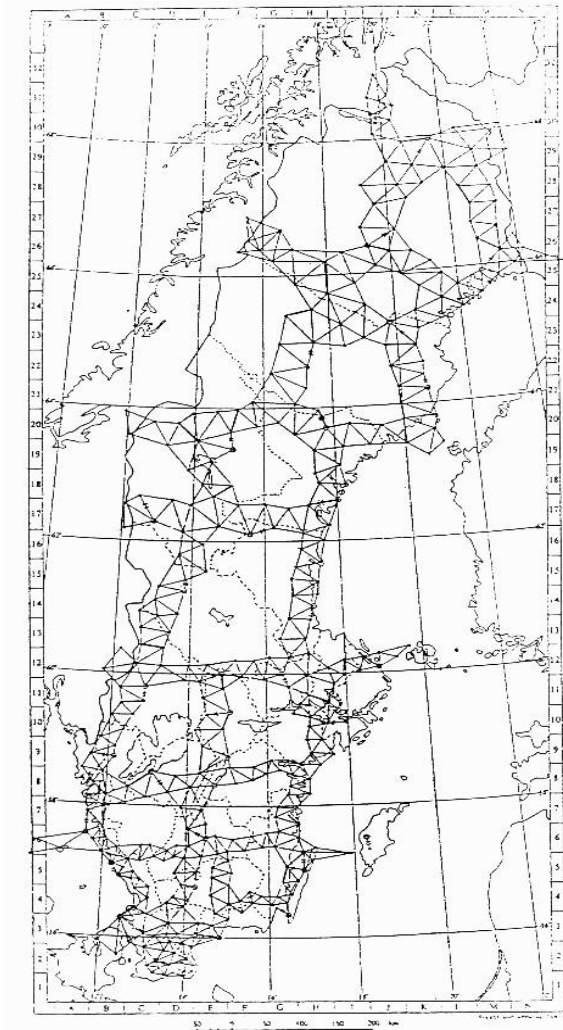


# Astrogeodetic measurements

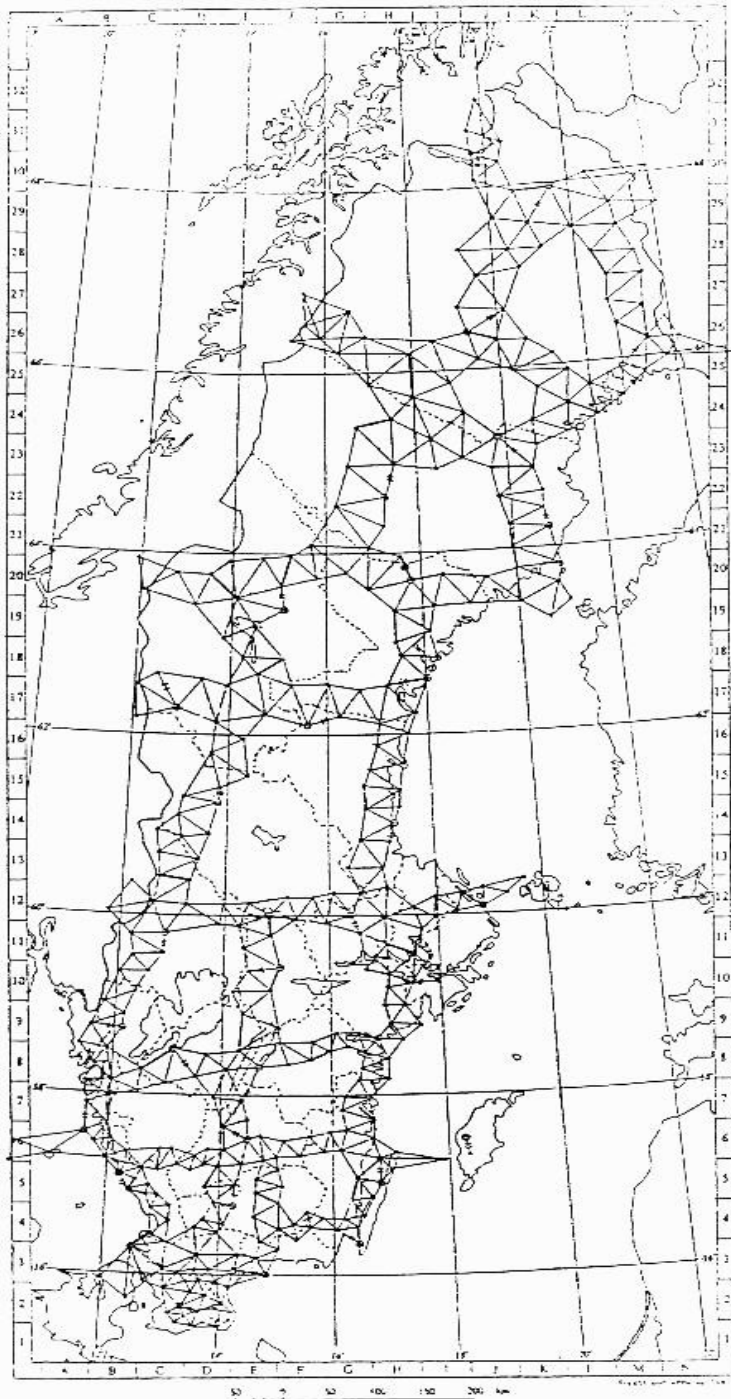
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- Absolute position ( $\Phi, \Lambda$ ) of a few points determined by astronomical observations. ( $0.5'' - 1''$ )
- Astronomical azimuths provide orientation and control of error culmulations in angle measurements
- Only a fewer distances are measured using invar wires due to distance measurement difficulties (in the past) (1:300 000)
- Large number of angles are measured by theodolites ( $0.5'' - 1''$ )

# 1st Swedish national triangulation



- Divided into orders: 1st, 2nd, 3rd
- 1st-order network in triangle chains (sides up to 30 km)
- Chains along meridians/parallels
- 2nd-order networks as fill in between
- Towers on mountain tops



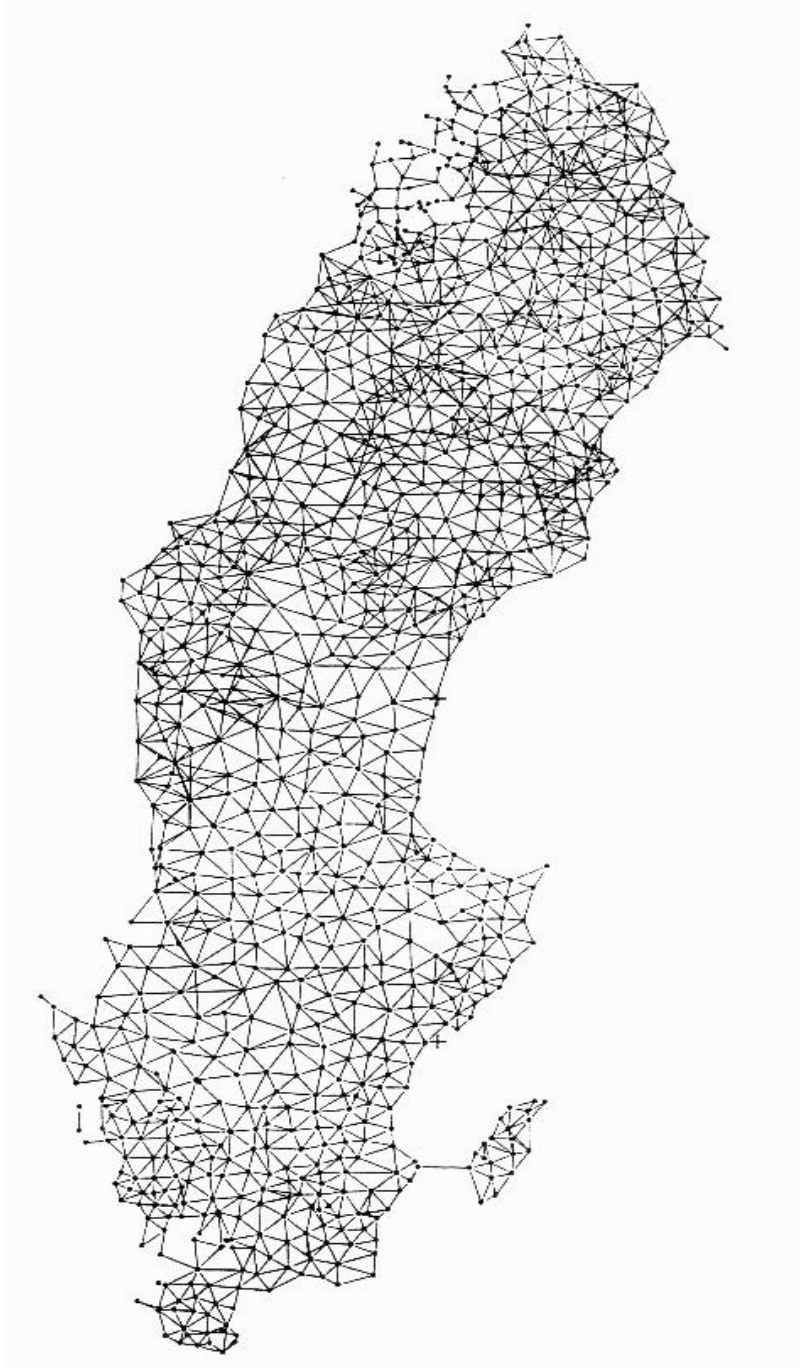
## 2nd Swedish National Triangulation Network (RT38)

- Field work during 1905-1950
- **Triangle chains** (EW, NS) at about 200 km distances
- 366 points with sides of  $\sim 30$  km
- Astronomical coordinates determined at 30 junction points
- 11 baselines measurements by invar wire (accuracy: 1:300 000, **3 ppm**)
- Large number of angle/direction measurements (accuracy:  $\sim 1''$ )
- **Bessel's ellipsoid** was used:  
 $a=6377397.155$ ,  $1/f=299.1528128$
- Gauss-Krüger Projection,  $y+1500\text{km}$ ,  
 $\lambda_0=15.808\ 277\ 777^\circ$
- Coordinate system named as **RT 38**









## The 3rd Swedish National Triangulation Network (RT 90)

- Field work during 1967-1982
- Complete network with 15295 distance measurements using geodimeters
- Including 366 first-order points of RT 38
- Including angles and baselines from RT 38
- 5424 angle (direction) measurements
- Observations are adjusted in ED 87 using Hayford ellipsoid ( $a=63781388\text{m}$ ,  $1/f=297$ )
- Coordinates at 366 common points in ED87 are fitted to coordinates in RT 38
- Final coordinates are referred to a non-geocentric **Bessel's ellipsoid**
- Gauss-Kruger map projection with mid-meridian  $\lambda_0 = 15.808\ 277\ 777^\circ$
- Coordinate system is designated as **RT 90**
- RT 90 = improved coordinates in RT 38

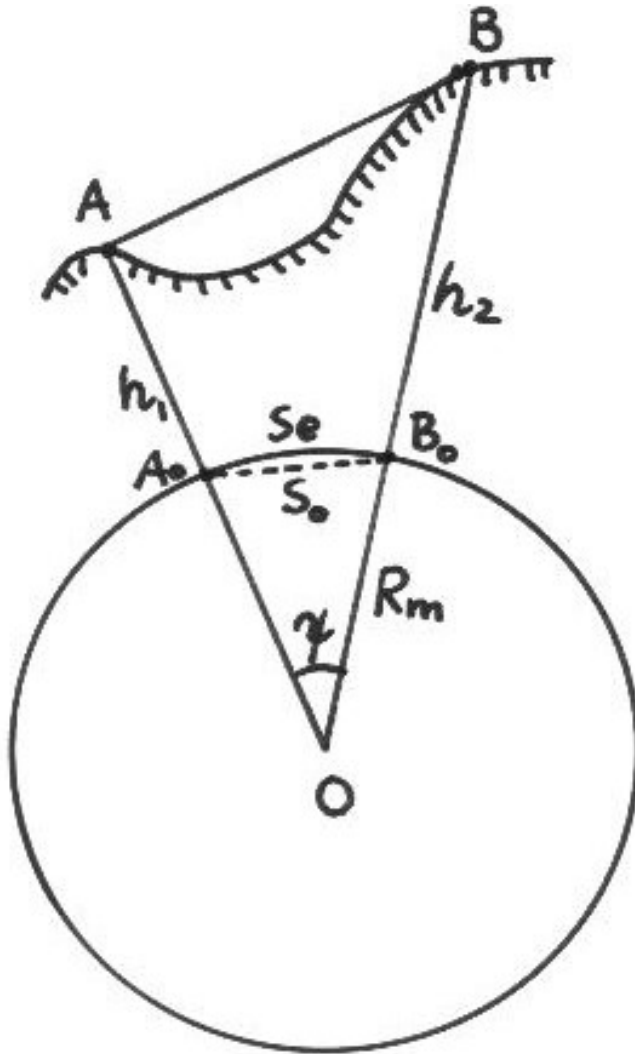


# Reduction of ground measurements down to the reference ellipsoid

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- Reduce slope **distances** on the ground to distances of the geodetic line on the ellipsoid
- Reduce **astronomical coordinates** to obtain geodetic coordinates (*deflection of the vertical is needed*)
- Reduce surface **angles** to angles of geodetic triangles
- Reduce astronomical **zenith distances** to obtain geodetic zenith distances

# Reduction of slope distances



$$s_0 = \sqrt{\frac{s^2 - (h_2 - h_1)^2}{\left(1 + \frac{h_1}{R_m}\right) \left(1 + \frac{h_2}{R_m}\right)}}$$

$$R_m = \frac{a\sqrt{1-e^2}}{W^2} = \frac{a\sqrt{1-e^2}}{1 - e^2 \sin^2 \phi_m}$$

$$s_e = 2R_m \cdot \arcsin \left( \frac{s_0}{2R_m} \right)$$



## Reduction of astronomical coordinates

$$\begin{aligned}\phi &= \Phi - \xi \\ \lambda &= \Lambda - \eta / \cos \phi\end{aligned}$$

$$\alpha_{ab} = A_{ab} - \Delta A_1 - \Delta A_2$$

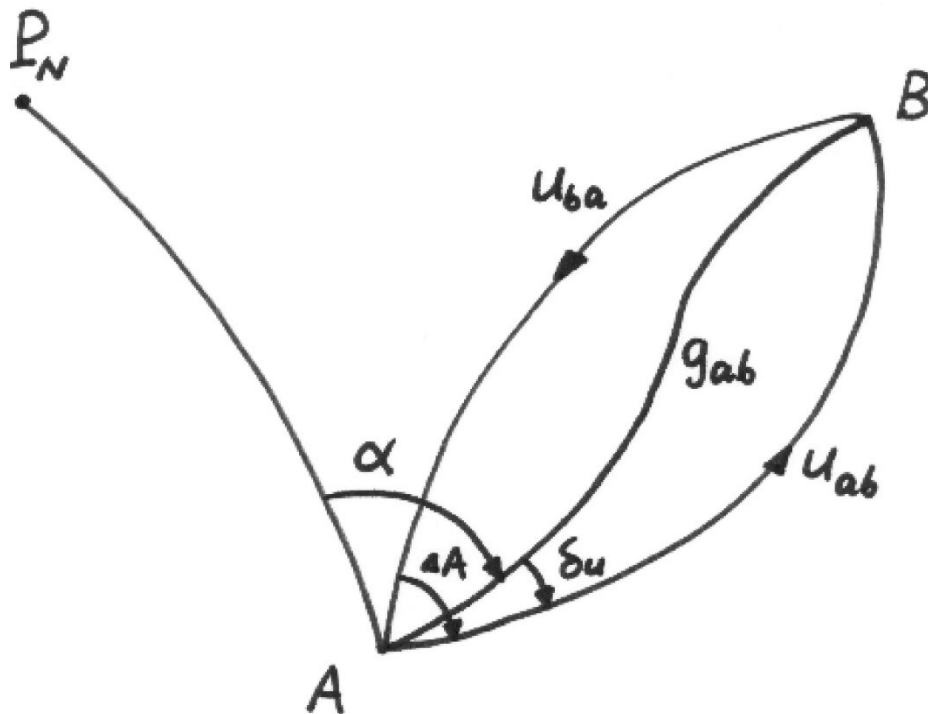
$$\left. \begin{aligned}\Delta A_1 &= \eta \operatorname{tg} \phi = (\Lambda - \lambda) \sin \phi \\ \Delta A_2 &= (\xi \sin \alpha_{ab} - \eta \cos \alpha_{ab}) \cot z_{ab}\end{aligned} \right\}$$

When  $z_{ab} \sim 90^\circ$ , we get the **Laplace condition**:

$$A_{ab} - \alpha_{ab} = (\Lambda - \lambda) \sin \phi$$



## Reduction of ground directions (angles)



- Reduction due to deflection of the vertical  

$$A_{ab} - \alpha_{ab} = (\Lambda - \lambda) \sin \phi$$
- Reduction due to discrepancy between normal section and geodesic  

$$\delta_u \approx \Delta A/3 \approx \frac{e^2 \cdot s^2}{12 N^2} \cos^2 \phi \sin 2\alpha$$
- Reduction due to height of the object above the ellipsoid  

$$\delta_h \approx -\frac{h}{2N} e'^2 \cos^2 \phi \sin 2\alpha$$



# Reduction of astronomical zenith distance

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- Astronomical zenith distances refer to the plumb line (vertical line=gravity vector)
- Geodetic zenith distances refer to the ellipsoidal normal
- Reduction depends on the deflection of the vertical and the azimuth:

$$z_e = z_s + \xi \cos \alpha + \eta \sin \alpha$$



# Least squares adjustment on the reference ellipsoid

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- **Unknown parameters to be determined:** geodetic latitudes and longitudes of unknown triangulation points
- **Observations:** distances, azimuths, angles/directions
- **Observation equation:** an explicit function of the unknown parameters for each observation
- **If an observation equation is non-linear:** the observation equation must be linearized using approximate geodetic latitudes/longitudes



## Observation equation of a distance measurement

$$s_{ij} - \varepsilon_{ij} = s(\phi_i^0 + \delta\phi_i, \lambda_i^0 + \delta\lambda_i, \phi_j^0 + \delta\phi_j, \lambda_j^0 + \delta\lambda_j)$$
$$\approx s_{ij}^0 + \frac{\partial s}{\partial \phi_i} \cdot \delta\phi_i + \frac{\partial s}{\partial \lambda_i} \cdot \delta\lambda_i + \frac{\partial s}{\partial \phi_j} \cdot \delta\phi_j + \frac{\partial s}{\partial \lambda_j} \cdot \delta\lambda_j$$

$$\ell_{ij} - \varepsilon_{ij} = a_i \cdot \delta\phi_i + b_i \cdot \delta\lambda_i + a_j \cdot \delta\phi_j + b_j \cdot \delta\lambda_j$$

$$a_i = -M_i^0 \cos \alpha_{ij}^0$$
$$b_i = N_j^0 \cos \phi_j^0 \sin \alpha_{ji}^0$$
$$a_j = -M_j^0 \cos \alpha_{ji}^0$$
$$b_j = -N_j^0 \cos \phi_j^0 \sin \alpha_{ji}^0$$
$$\ell_{ij} = s_{ij} - s_{ij}^0$$

**For linearization:**

$$\phi_i = \phi_i^0 + \delta\phi_i$$
$$\lambda_i = \lambda_i^0 + \delta\lambda_i$$
$$\phi_j = \phi_j^0 + \delta\phi_j$$
$$\lambda_j = \lambda_j^0 + \delta\lambda_j$$

$$s_{ij}^0 = s(\phi_i^0, \lambda_i^0, \phi_j^0, \lambda_j^0)$$
$$\alpha_{ij}^0 = \alpha(\phi_i^0, \lambda_i^0, \phi_j^0, \lambda_j^0)$$





# Observation equation of an azimuth

$$\alpha_{ij} - \varepsilon_{ij} = \alpha(\phi_i^0 + \delta\phi_i, \lambda_i^0 + \delta\lambda_i, \phi_j^0 + \delta\phi_j, \lambda_j^0 + \delta\lambda_j)$$

$$\approx \alpha_{ij}^0 + \frac{\partial \alpha}{\partial \phi_i} \cdot \delta\phi_i + \frac{\partial \alpha}{\partial \lambda_i} \cdot \delta\lambda_i + \frac{\partial \alpha}{\partial \phi_j} \cdot \delta\phi_j + \frac{\partial \alpha}{\partial \lambda_j} \cdot \delta\lambda_j$$

$$\ell_{ij} - \varepsilon_{ij} = c_i \cdot \delta\phi_i + d_i \cdot \delta\lambda_i + c_j \cdot \delta\phi_j + d_j \cdot \delta\lambda_j$$

$$\left. \begin{aligned} c_i &= M_i^0 \sin \alpha_{ij}^0 / s_{ij}^0 \\ d_i &= N_j^0 \cos \phi_j^0 \cos \alpha_{ji}^0 / s_{ij}^0 \\ c_j &= M_j^0 \sin \alpha_{ji}^0 / s_{ij}^0 \\ d_j &= -N_j^0 \cos \phi_j^0 \cos \alpha_{ji}^0 / s_{ij}^0 \end{aligned} \right\}$$
$$\ell_{ij} = \alpha_{ij} - \alpha_{ij}^0$$



# Least squares adjustment on the reference ellipsoid

Final observation equations for all measurements

$$L - \varepsilon = A X$$

$L$ : (reduced) measurements (azimuths, angles, distances etc)

$\varepsilon$ : residuals (errors)

$X$ : unknowns (coordinate corrections, other parameters)

$A$ : design matrix

Least squares solution:

$$\hat{X} = \left( A^T P A \right)^{-1} A^T P L$$

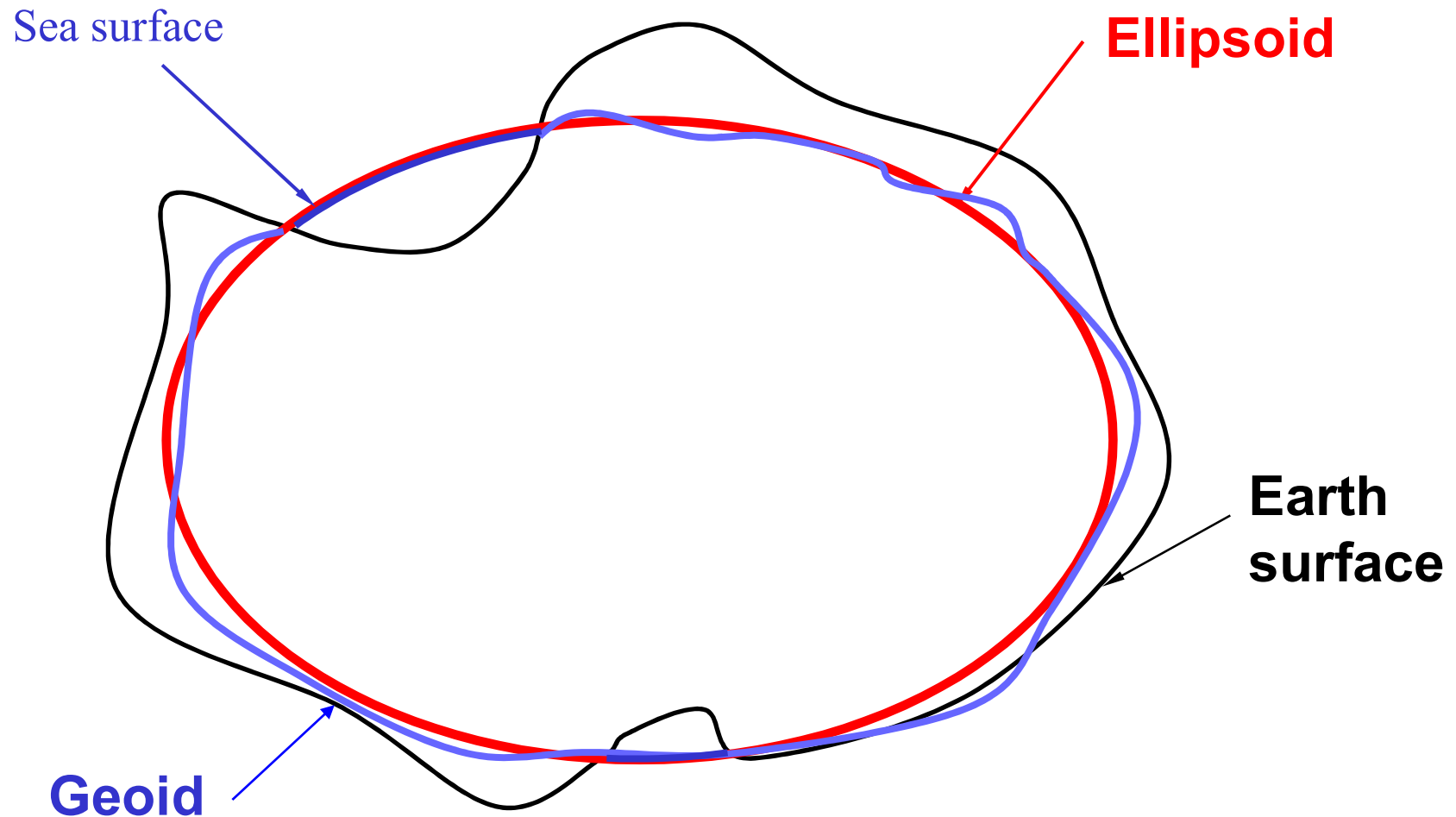


## Geodetic datum (*ellipsoidal datum*)

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- A *geodetic datum* consists of :
  - reference ellipsoid (size, shape and position defined) **and**
  - a set of ground triangulation points whose 2D geodetic coordinates  $(\varphi, \lambda)$  are computed with respect to this reference ellipsoid
- **Assumptions:**
  - The minor axis of ellipsoid is parallel to earth rotation axis;
  - The initial median plane of the ellipsoid is parallel to the *astronomical* Greenwich meridian plane
- The position of the ellipsoid is often/best defined by the geocentric coordinates of the ellipsoidal centre ( $x_0, y_0, z_0$ )

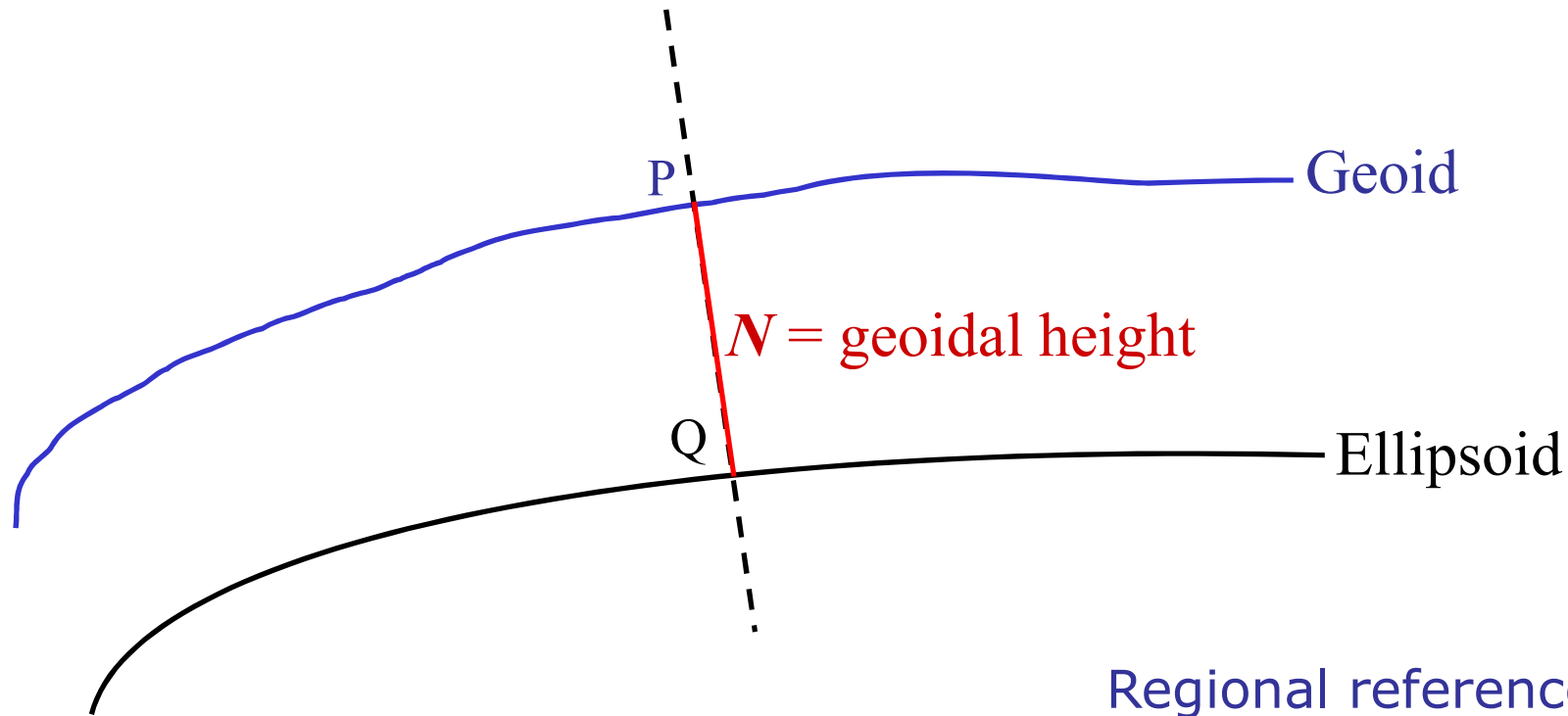
# Fitting ellipsoids to the geoid







# The geoid-ellipsoid separation



Mean Earth Ellipsoid ( $\sigma$ =whole earth)

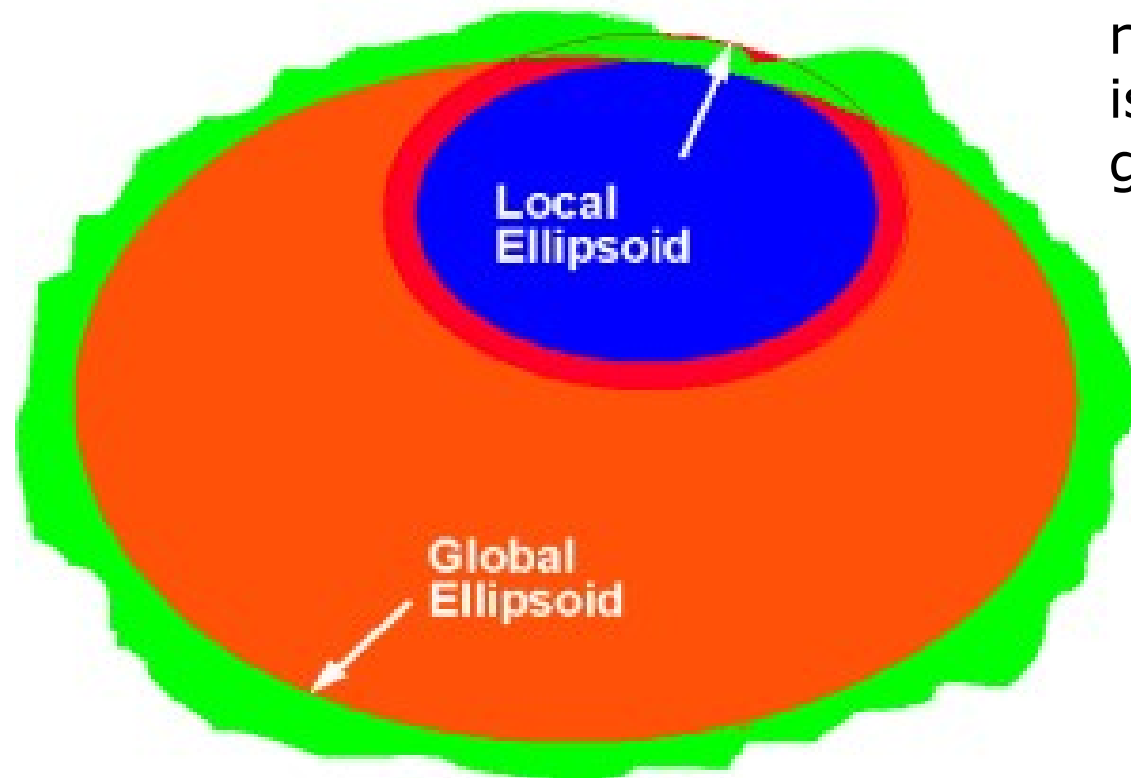
$$\iint_{\sigma} N^2 d\sigma = \text{minimum}$$

Regional reference ellipsoid

( $\sigma_1$  = local area, a country)

$$\iint_{\sigma_1} N^2 d\sigma = \text{minimum}$$

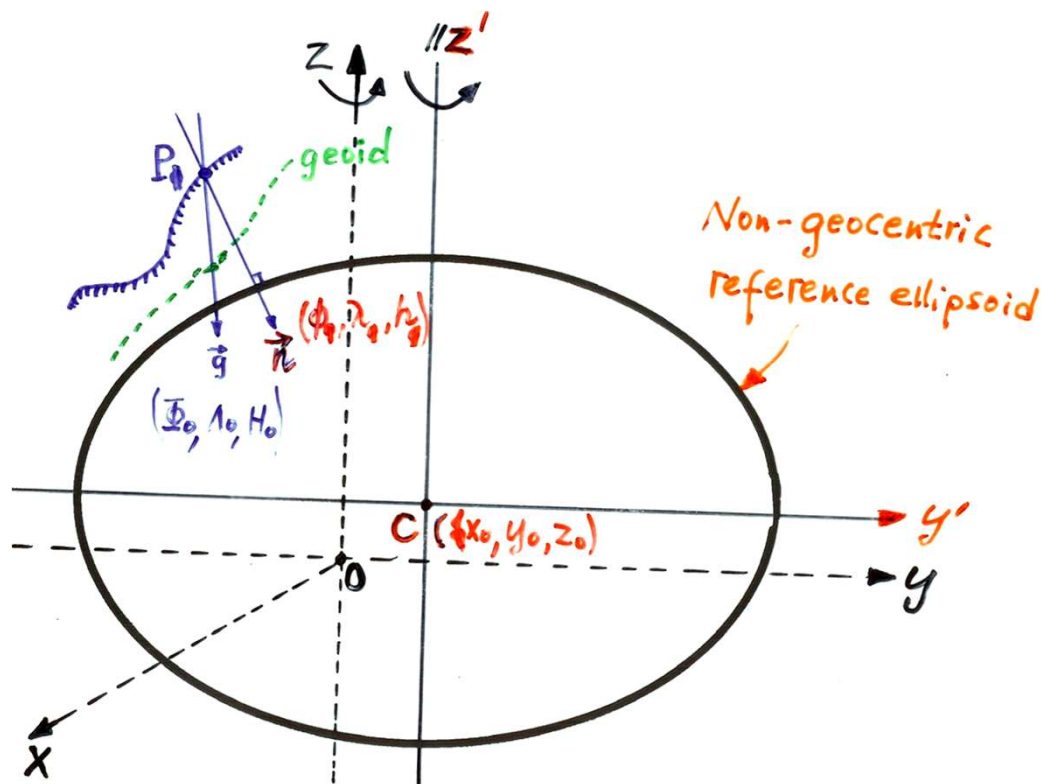
# Local vs global ellipsoids



A locally fitted reference ellipsoid is most often **not** geocentric

A globally fitted reference ellipsoid (*Mean Earth Ellipsoid*) is geocentric

# Positioning of the ellipsoid



O: geocentre

C: centre of the reference ellipsoid

**Assumption:** ellipsoid's minor axis  $z'$  is parallel to the Earth rotation axis  $z$

→ the equator of the ellipsoid is parallel to the Earth's equator

→ position of the ellipsoid in relation to the earth can be defined by the geocentric coordinates  $(x_0, y_0, z_0)$  of the ellipsoidal center  $C$



## 3 (or 2) ways to position the ellipsoid

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- by geocentric coordinate  $(x_0, y_0, z_0)$  of ellipsoidal center  $C$
- by geodetic coordinate  $(\varphi_1, \lambda_1, h_1)$  of the initial point  $P_1$
- by geoid height  $N_1$  and deflection of the vertical  $(\xi_1, \eta_1)$  of  $P_1$





# Geodetic datum parameters

Name	a (m)	1/f	$x_0$ (m)	$y_0$ (m)	$z_0$ (m)
WGS 84	6 378 137	298.257223563	0	0	0
RT 90 (Bessel)	6 377 397.155	299.1528128	414.098	41.338	603.063
Pulkovo 1942 (Krassovski)	6 378 245	298.3	-25.0	141.0	78.5
Adindan 4, Ethiopia (Clarke 1880)	6 378 249.145	293.465	+162	+12	-206



# Coordinate change due to geodetic datum change

If geodetic datum parameters  $(a, f, x_0, y_0, z_0)$  have slight changes  $(\delta a, \delta f, \delta x_0, \delta y_0, \delta z_0)'$ , correspondingly the geodetic coordinates  $(\phi, \lambda, h)$  of a ground point P will have slight changes by  $(\delta \phi, \delta \lambda, \delta h)$

$$\begin{bmatrix} a \cdot \delta \phi \\ a \cos \phi \cdot \delta \lambda \\ dh \end{bmatrix} = \Omega(\phi, \lambda) \cdot \begin{bmatrix} \delta x_0 \\ \delta y_0 \\ \delta z_0 \end{bmatrix} + \Theta(\phi, \lambda) \cdot \begin{bmatrix} \delta a \\ a \cdot \delta f \end{bmatrix}$$

$$\Omega(\phi, \lambda) = \begin{bmatrix} \sin \phi \cos \lambda & \sin \phi \sin \lambda & -\cos \phi \\ \sin \lambda & -\cos \lambda & 0 \\ -\cos \phi \cos \lambda & -\cos \phi \sin \lambda & -\sin \phi \end{bmatrix}, \quad \Theta(\phi, \lambda) = \begin{bmatrix} 0 & \sin 2\phi \\ 0 & 0 \\ -1 & \sin^2 \phi \end{bmatrix}$$



# Coordinate change due to geodetic datum change

$$\begin{bmatrix} a \cdot \delta\phi \\ a \cos \phi \cdot \delta\lambda \\ \delta h \end{bmatrix} = \sum (\phi, \lambda) \cdot \begin{bmatrix} a \cdot \delta\phi_1 \\ a \cos \phi_1 \cdot \delta\lambda_1 \\ \delta h_1 \end{bmatrix} + \Pi(\phi, \lambda) \cdot \begin{bmatrix} \delta a \\ a \cdot \delta f \end{bmatrix}$$

$$\sum_{3 \times 3} (\phi, \lambda) = \Omega(\phi, \lambda) \cdot [\Omega(\phi_1, \lambda_1)]^{-1} =$$

$$= \begin{bmatrix} \cos \phi_1 \cos \phi + \sin \phi_1 \sin \phi \cos(\lambda - \lambda_1) & -\sin \phi \sin(\lambda - \lambda_1) & \sin \phi_1 \cos \phi - \cos \phi_1 \sin \phi \cos(\lambda - \lambda_1) \\ \sin \phi_1 \sin(\lambda - \lambda_1) & \cos(\lambda - \lambda_1) & -\cos \phi_1 \sin(\lambda - \lambda_1) \\ \cos \phi_1 \sin \phi - \sin \phi_1 \cos \phi \cos(\lambda - \lambda_1) & \cos \phi \sin(\lambda - \lambda_1) & \sin \phi_1 \sin \phi + \cos \phi_1 \cos \phi \cos(\lambda - \lambda_1) \end{bmatrix} \quad (2.128)$$

$$\prod_{3 \times 2} (\phi, \lambda) = \Theta(\phi, \lambda) - \Omega(\phi, \lambda) \cdot [\Omega(\phi_1, \lambda_1)]^{-1} \Theta(\phi_1, \lambda_1) = \begin{bmatrix} \sin \phi_1 \cos \phi - \cos \phi_1 \sin \phi \cos(\lambda - \lambda_1) & -\cos \phi_1 \sin(\lambda - \lambda_1) \\ \sin \phi_1 \sin \phi + \cos \phi_1 \cos \phi \cos(\lambda - \lambda_1) & -1 \end{bmatrix}$$

$$\begin{bmatrix} [\sin \phi_1 \cos \phi - \cos \phi_1 \sin \phi \cos(\lambda - \lambda_1)] \sin^2 \phi_1 + 2 \cos \phi (\sin \phi - \sin \phi_1) & -\cos \phi_1 \sin(\lambda - \lambda_1) \sin^2 \phi_1 \\ [\sin \phi_1 \sin \phi + \cos \phi_1 \cos \phi \cos(\lambda - \lambda_1)] \sin^2 \phi_1 + (\sin^2 \phi - 2 \sin \phi_1 \sin \phi) \end{bmatrix} \quad (2.129)$$



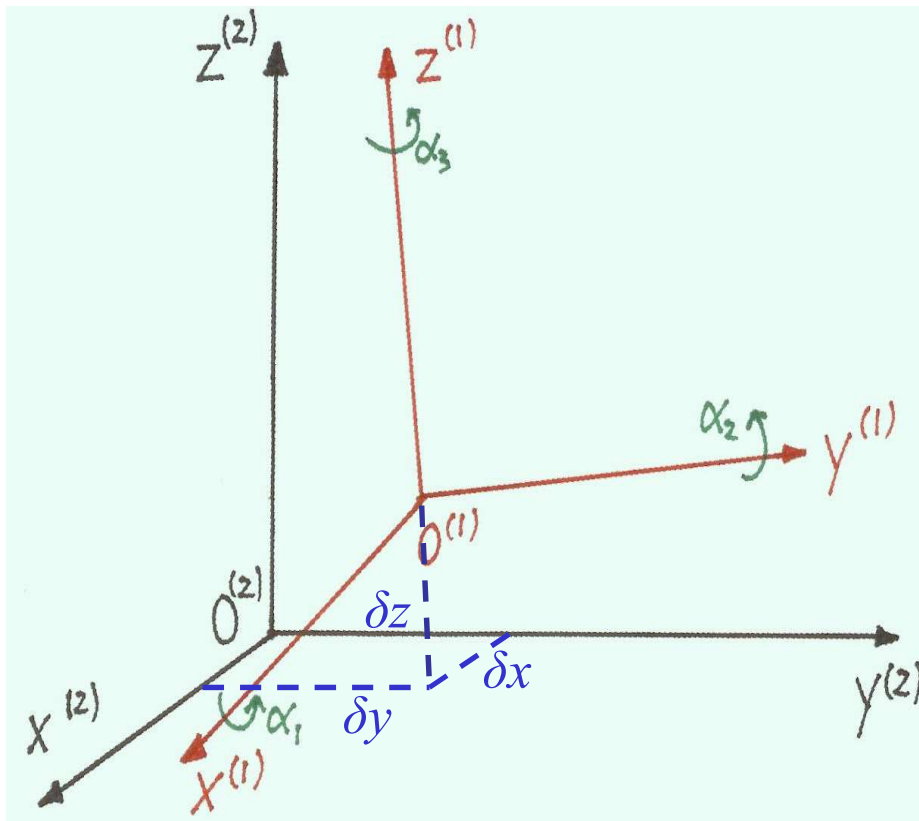
# Local triangulation vs global systems: Reference ellipsoids

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- Theoretically, coordinate system or positions can be uniquely defined using Cartesian coordinates  $(x,y,z)$
- In principle, transformation of two Cartesian coordinate systems are independent of reference ellipsoids
- Reference ellipsoids are needed to define (geographic) geodetic coordinates  $(\varphi,\lambda,h)$
- Local/global systems *often* use different reference ellipsoids
- Reference ellipsoids affect also map projections



# Local triangulation system vs global geocentric systems



- Global system (e.g. GPS) is geocentric while local systems are most often non-geocentric:  $\delta x \neq 0$ ,  $\delta y \neq 0$ ,  $\delta z \neq 0$
- The axes of local and global systems are often not parallel, rather with small angles ( $\alpha_1$ ,  $\alpha_2$ ,  $\alpha_3$ ) between them
- Linear scales can be significantly different due to difficulties of distance measurements in triangulation
- Difference between local and global systems can be modelled by 3 translations, 3 rotations, 1 scale change



# Helmert transformation between 2 Cartesian coordinate systems

$$\begin{bmatrix} X_i^{(2)} \\ Y_i^{(2)} \\ Z_i^{(2)} \end{bmatrix} = \begin{bmatrix} \delta x \\ \delta y \\ \delta z \end{bmatrix} + s \cdot R(\alpha_1, \alpha_2, \alpha_3) \cdot \begin{bmatrix} X_i^{(1)} \\ Y_i^{(1)} \\ Z_i^{(1)} \end{bmatrix}$$

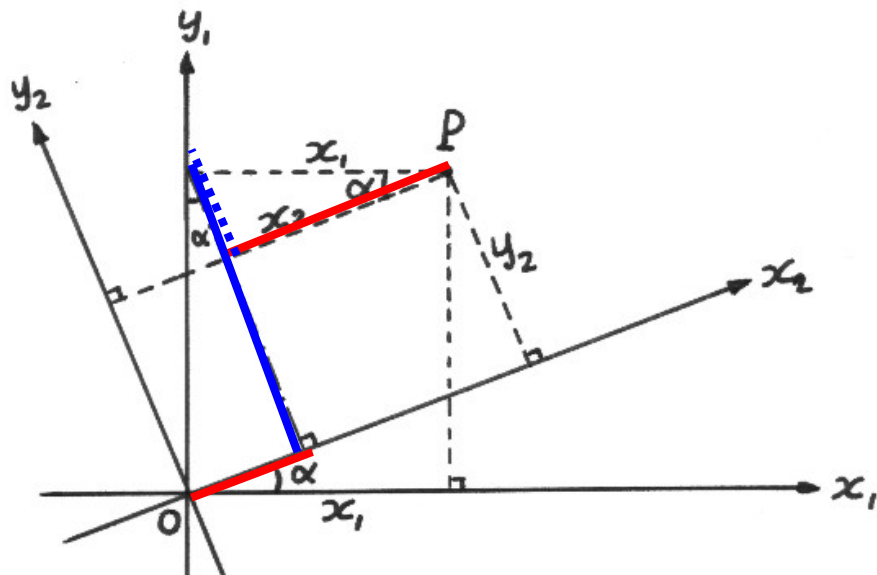
$$s = 1 + \delta s$$

$$R_{3 \times 3} = R(\alpha_1, \alpha_2, \alpha_3) = R_3(\alpha_3) \cdot R_2(\alpha_2) \cdot R_1(\alpha_1)$$

$$= \begin{bmatrix} \cos \alpha_2 \cos \alpha_3 & \cos \alpha_1 \sin \alpha_3 + \sin \alpha_1 \sin \alpha_2 \cos \alpha_3 & \sin \alpha_1 \sin \alpha_3 - \cos \alpha_1 \sin \alpha_2 \cos \alpha_3 \\ -\cos \alpha_2 \sin \alpha_3 & \cos \alpha_1 \cos \alpha_3 - \sin \alpha_1 \sin \alpha_2 \sin \alpha_3 & \sin \alpha_1 \cos \alpha_3 + \cos \alpha_1 \sin \alpha_2 \sin \alpha_3 \\ \sin \alpha_2 & -\sin \alpha_1 \cos \alpha_2 & \cos \alpha_1 \cos \alpha_2 \end{bmatrix}$$



# Rotation Matrices



$$R = R_1(\alpha) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \alpha & \sin \alpha \\ 0 & -\sin \alpha & \cos \alpha \end{bmatrix}$$

$$R = R_2(\alpha) = \begin{bmatrix} \cos \alpha & 0 & -\sin \alpha \\ 0 & 1 & 0 \\ \sin \alpha & 0 & \cos \alpha \end{bmatrix}$$

$$\begin{bmatrix} x_2 \\ y_2 \\ z_2 \end{bmatrix} = R \begin{bmatrix} x_1 \\ y_1 \\ z_1 \end{bmatrix}$$

$$R = R_3(\alpha) = \begin{bmatrix} \cos \alpha & \sin \alpha & 0 \\ -\sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



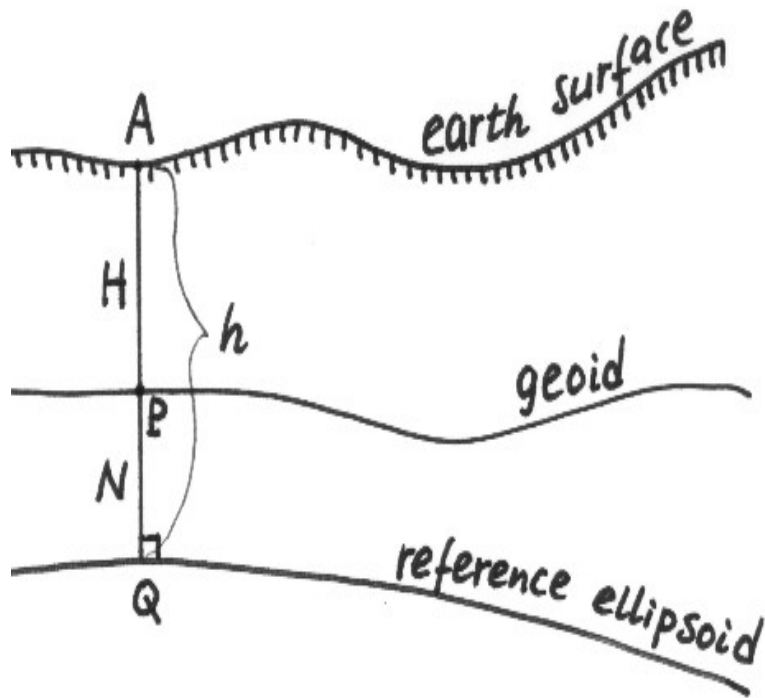
# Helmert transformation parameters



From System 1:	<b>SWEREF 99</b> (GPS-based)
To System 2:	<b>RT 90</b> (Swedish triangulation)
$\delta x$ (metre):	- 414.0979
$\delta y$ (metre):	- 41.3381
$\delta z$ (metre):	- 603.0627
$\delta s$ (ppm):	+ 0.000 000 000 0
$\alpha_1$ (arcsecond):	- 0.855 043 431 4
$\alpha_2$ (arcsecond):	+ 2.141 346 518 5
$\alpha_3$ (arcsecond):	- 7.022 720 951 6



# Local triangulation system Vs global coordinate systems



**$2 + 1 \neq 3!$**

- Triangulation gives us basically 2D coordinates ( $\phi, \lambda$ )
- GNSS provides ellipsoidal heights  $h$
- Height above MSL ( $H$ ) from precise levelling refers to the geoid
- $h$  and  $H$  are different by definition and related to each other by:  
$$h = H + N$$
- $h$ ,  $N$  must refer to the same ellipsoid
- $N$  depends on gravity field of the earth
- Triangulation + levelling is not equivalent to 3D positioning using e.g. GNSS



# Steps from SWEREF 99 to RT 90

- $(\varphi, \lambda, h)_{\text{SWEREF 99}} \rightarrow (x, y, z)_{\text{SWEREF 99}}$  ← GRS 80 ellipsoid
- $(x, y, z)_{\text{SWEREF 99}} \rightarrow (x, y, z)_{\text{RT 90}}$  ← Helmert model (7 parameters)
- $(x, y, z)_{\text{RT 90}} \rightarrow (\varphi, \lambda, h)_{\text{RT 90}}$  ← Bessel's ellipsoid
- $(\varphi, \lambda)_{\text{RT 90}} \rightarrow (X, Y)_{\text{UTM / RT 90}}$  ← Bessel's ellipsoid
- $(h)_{\text{SWEREF 99}} \rightarrow (H)$  ← Geoid model, GRS 80 ellipsoid



# Steps from RT90 to SWEREF 99TM

- $(x, y)_{\text{RT 90}} \rightarrow (\varphi, \lambda)_{\text{RT 90}} \leftarrow \text{Bessel's ellipsoid}$
- $(\varphi, \lambda, h=0/H)_{\text{RT 90}} \rightarrow (x, y, z)_{\text{RT 90}} \leftarrow \text{Bessel's ellipsoid}$
- $(x, y, z)_{\text{RT 90}} \rightarrow (x, y, z)_{\text{SWEREF 99}} \leftarrow \text{Helmert model (7 parameters)}$
- $(x, y, z)_{\text{SWEREF 99}} \rightarrow (\varphi, \lambda, h)_{\text{SWEREF 99}} \leftarrow \text{GRS 80 ellipsoid}$
- $(\varphi, \lambda)_{\text{SWEREF 99}} \rightarrow (x, y)_{\text{SWEREF 99TM}} \leftarrow \text{GRS 80 ellipsoid}$