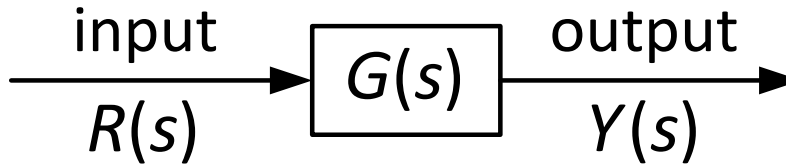


Chapter 5 The Performance of Feedback System

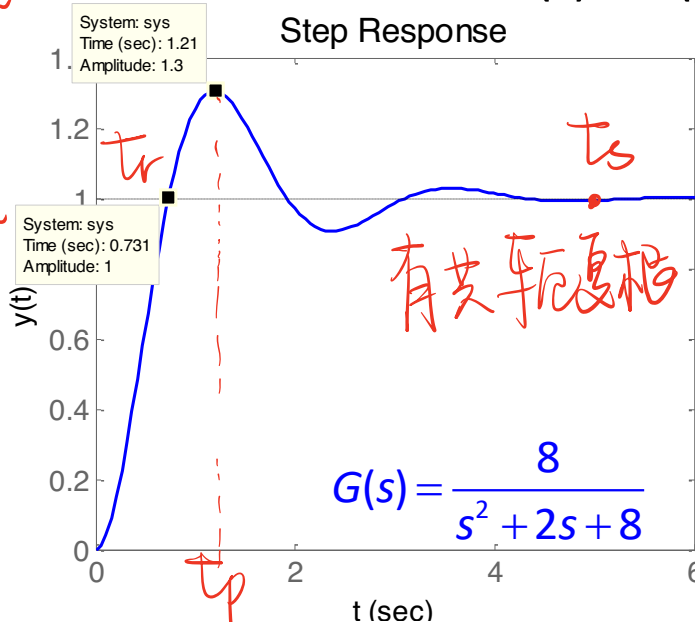
Contents

- ❑ 5.1 Introduction
- ❑ 5.2 Test Input Signals
- ❑ 5.3 Performance of Second-Order Systems
- ❑ 5.4 Effects of a Third Pole and a Zero on the Second-Order System Response
- ❑ 5.5 The s-Plane Root Location and the Transient Response
- ❑ 5.6 The Steady-State Error of Feedback Control Systems
- ❑ 5.7 Summary

5.1 Introduction



$$Y(s) = G(s)R(s)$$



Character:

stability, transient,
steady-state

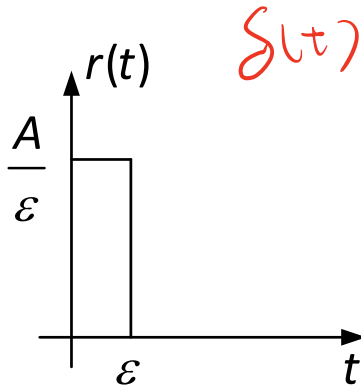
Parameters:

$$t_r, t_p, t_s, P.O., e_{ss}$$

考動圖 14-函数图成

5.2 Test Input Signal

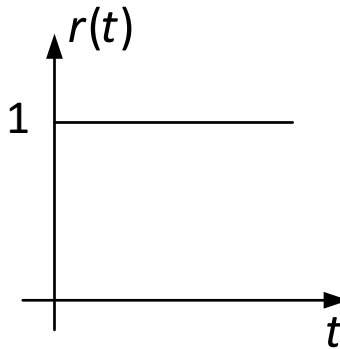
Impulse



$$r(t) = \begin{cases} \frac{A}{\varepsilon} & 0 \leq t \leq \varepsilon \\ 0 & \text{otherwise} \end{cases}$$

$$R(s) = A$$

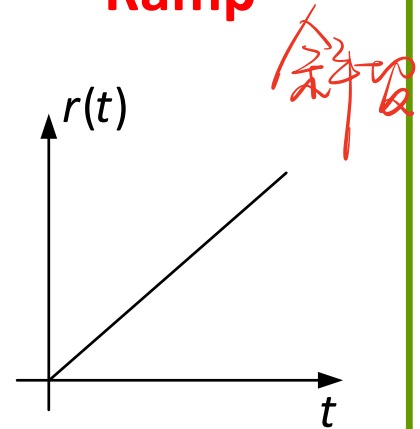
Step



$$r(t) = \begin{cases} 1 & t \geq 0 \\ 0 & t < 0 \end{cases}$$

$$R(s) = \frac{A}{s}$$

Ramp

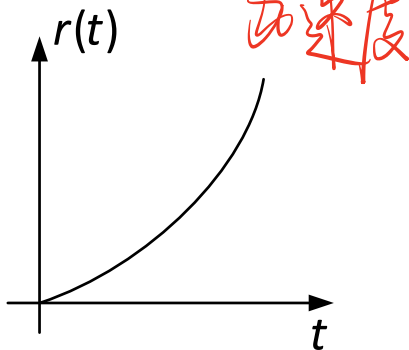


$$r(t) = \begin{cases} At & t \geq 0 \\ 0 & t < 0 \end{cases}$$

$$R(s) = \frac{A}{s^2}$$

5.2 Test Input Signal

Acceleration (Parabolic)

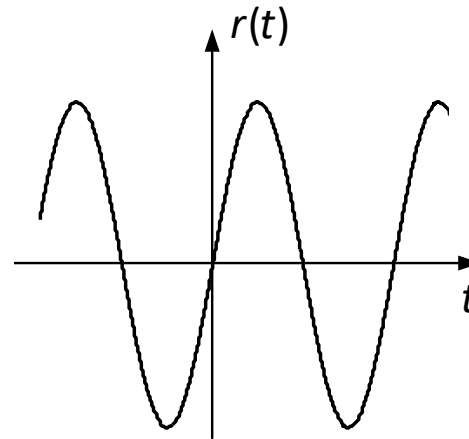


$$r(t) = \begin{cases} At^2 & t \geq 0 \\ 0 & t < 0 \end{cases}$$

$$R(s) = \frac{2A}{s^3}$$

周期
信号

Sine & cosine



$$r(t) = A \sin(\omega t)$$

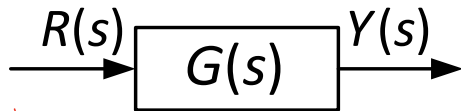
$$R(s) = \frac{A\omega}{s^2 + \omega^2}$$

$$r(t) = A \cos(\omega t)$$

$$R(s) = \frac{As}{s^2 + \omega^2}$$

5.2 Test Input Signal

Example:



系统的增益 $\frac{9}{10}$ 比例决定放大倍数

$$G(s) = \frac{9}{s+10}, R(s) = \frac{1}{s}, y(t) = ?$$

$$Y(s) = G(s) \cdot R(s) = \frac{9}{s+10} \cdot \frac{1}{s}$$

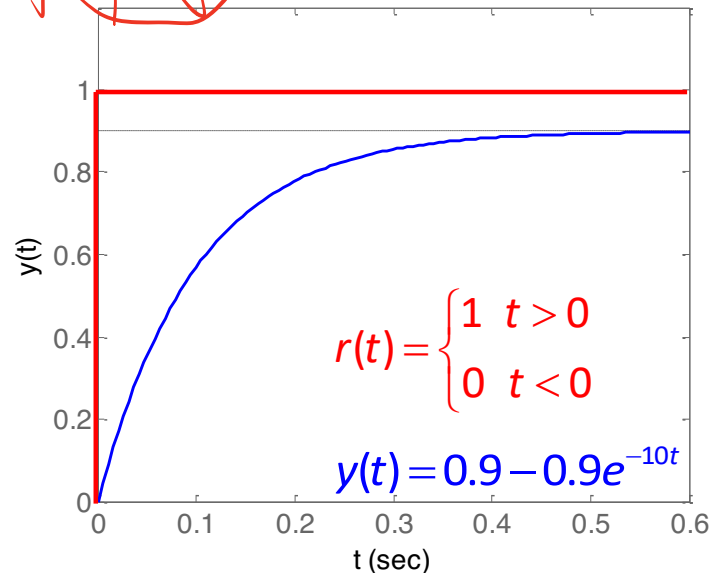
$$= \frac{0.9}{s} - \frac{0.9}{s+10}$$

$$y(t) = 0.9 - 0.9e^{-10t}$$

t_r = 稳态的 0.9 对应的时间

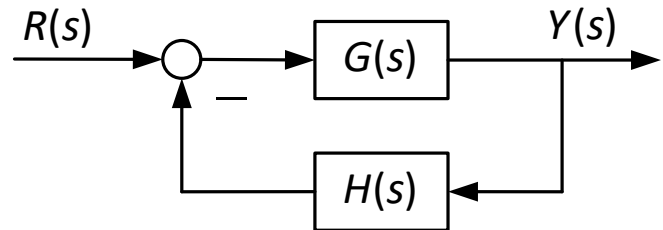
取决于

Step Response



5.3 2nd-order System Performance

$$G(s) = \frac{k}{s(Ts + 1)}, R(s) = \frac{1}{s}, H(s) = 1, y(t) = ?$$



$$G_{\text{closed-loop}}(s) = \frac{G(s)}{1 + G(s)H(s)} = \frac{k / T}{s^2 + (1 / T)s + k / T} = \frac{\omega_n^2}{s^2 + 2\omega_n\zeta s + \omega_n^2}$$

$$\text{Let } \begin{cases} \omega_n^2 = k / T \\ 2\zeta\omega_n = 1 / T \end{cases} \Rightarrow \begin{cases} \omega_n = \sqrt{k / T} \rightarrow \text{natural frequency} \\ \zeta = \frac{1}{2\sqrt{kT}} \rightarrow \text{damping ratio} \end{cases}$$

BIBO

5.3 2nd-order System Performance

$$Y(s) = \frac{\omega_n^2}{s^2 + 2\omega_n\zeta s + \omega_n^2} \cdot R(s) \quad \text{CE: } q(s) = s^2 + 2\omega_n\zeta s + \omega_n^2 = 0$$

$$s_{1,2} = \frac{-2\zeta\omega_n \pm \sqrt{4\zeta^2\omega_n^2 - 4\omega_n^2}}{2} = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1} \quad (\omega_n > 0, \zeta \geq 0)$$

① **overdamped** $\zeta > 1$

② **critical damping** $\zeta = 1$

③ **underdamped** $0 < \zeta < 1$

④ **undamped** $\zeta = 0$

过阻尼

临界阻尼

欠阻尼

无阻尼

5.3 2nd-order System Performance

$$\text{CE: } s^2 + 2\omega_n \zeta s + \omega_n^2 = 0, s_{1,2} = -\zeta\omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$$

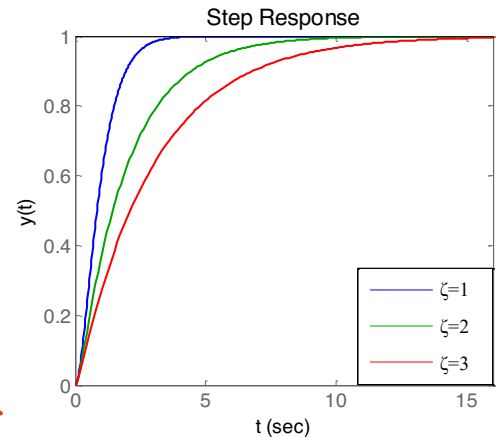
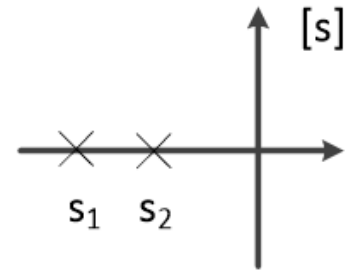
① **overdamped** $\zeta > 1$

s_1, s_2 are negative real roots

$$Y(s) = \frac{\omega_n^2}{s(s-s_1)(s-s_2)}$$

There is **no oscillating** term

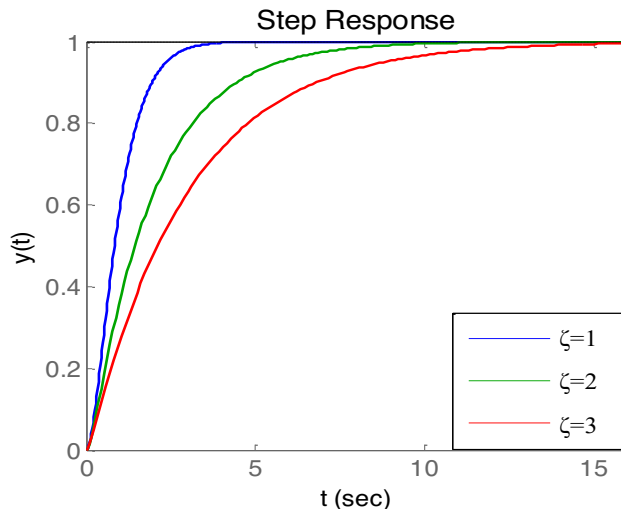
$$y(t) = \frac{\omega_n^2}{s_1 s_2} + \frac{\omega_n^2}{s_1^2 - s_1 s_2} e^{s_1 t} + \frac{\omega_n^2}{s_2^2 - s_1 s_2} e^{s_2 t}$$



阻尼越大，曲线越慢、启动慢

5.3 2nd-order System Performance

$$\frac{Y(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\omega_n\zeta s + \omega_n^2}, \omega_n = 2, \zeta = 1, 2, 3 \quad R(s) = \frac{1}{s}$$



$$\frac{Y(s)}{R(s)} = \frac{4}{s^2 + 4s + 4}$$

$$\frac{Y(s)}{R(s)} = \frac{4}{s^2 + 8s + 4}$$

$$\frac{Y(s)}{R(s)} = \frac{4}{s^2 + 12s + 4}$$

```
>> num=[4]; den=[1 4 4]; step(num,den);hold on;  
>> num=[4]; den=[1 8 4]; step(num,den);hold on;  
>> num=[4]; den=[1 12 4]; step(num,den);hold on;
```

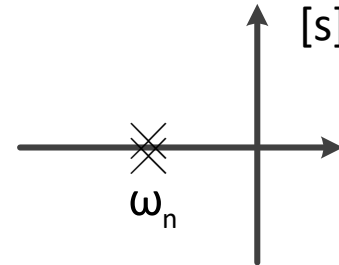
5.3 2nd-order System Performance

② critical damping $\zeta = 1$

s_1, s_2 are repeated real roots, $s_1, s_2 = -\omega_n$.

$$Y(s) = \frac{\omega_n^2}{s(s + \omega_n)^2} = \frac{1}{s} + \frac{-1}{s + \omega_n} + \frac{-\omega_n}{(s + \omega_n)^2}$$

$$y(t) = 1 - e^{-\omega_n t} - \omega_n t e^{-\omega_n t}$$

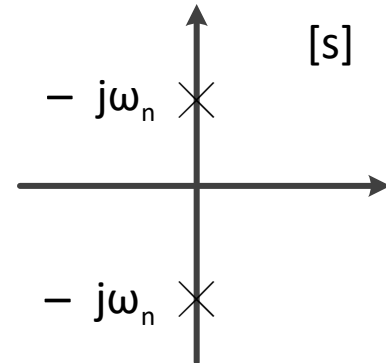


③ undamped $\zeta = 0$

$$s_1, s_2 = \pm j\omega_n$$

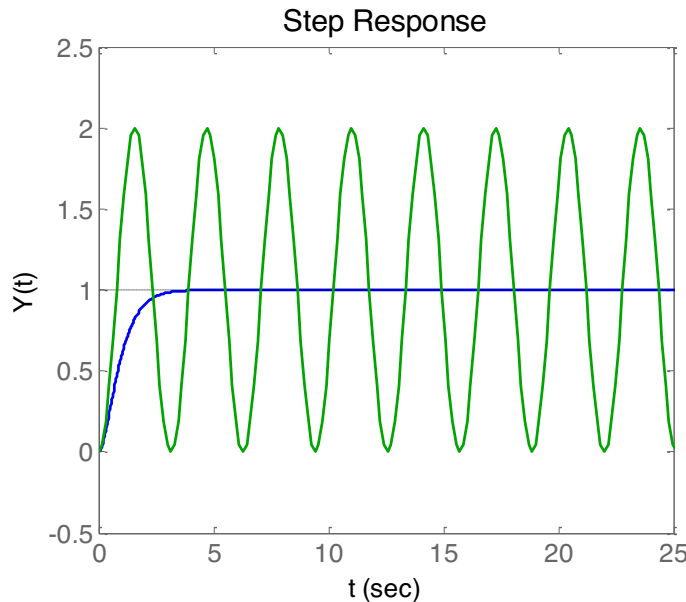
$$Y(s) = \frac{\omega_n^2}{s(s^2 + \omega_n^2)} = \frac{1}{s} - \frac{s}{s^2 + \omega_n^2}$$

$$y(t) = 1 - \cos \omega_n t$$



5.3 2nd-order System Performance

$$\frac{Y(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\omega_n\zeta s + \omega_n^2}, \omega_n = 2, \zeta = 0.1, \text{step response}$$



$$\frac{Y(s)}{R(s)} = \frac{4}{s^2 + 4s + 1}$$

$$\frac{Y(s)}{R(s)} = \frac{4}{s^2 + 4}$$

```
>> num=[4];den=[1 4 4];step(num,den);hold on;  
>> num=[4];den=[1 0 4];step(num,den);hold on;
```

5.3 2nd-order System Performance

④ **underdamped** $0 < \zeta < 1$

s_1, s_2 are complex roots

$$Y(s) = \frac{\omega_n^2}{s(s^2 + 2\zeta\omega_n s + \omega_n^2)}$$

$$y(t) = 1 - \frac{e^{-\sigma t}}{\sqrt{1-\zeta^2}} \sin(\omega_d t + \theta)$$

$\omega_d = \omega_n \sqrt{1-\zeta^2}$: **Damped oscillation frequency**

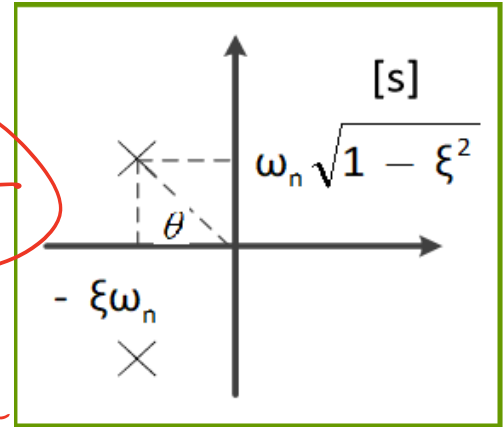
$\sigma = \zeta\omega_n$: **Attenuation coefficient**

t_r

$\frac{\pi - \arccos \zeta}{\omega_n \sqrt{1-\zeta^2}}$

$\omega_d t + \theta = k\pi$

$t = \frac{k\pi - \theta}{\omega_d}$



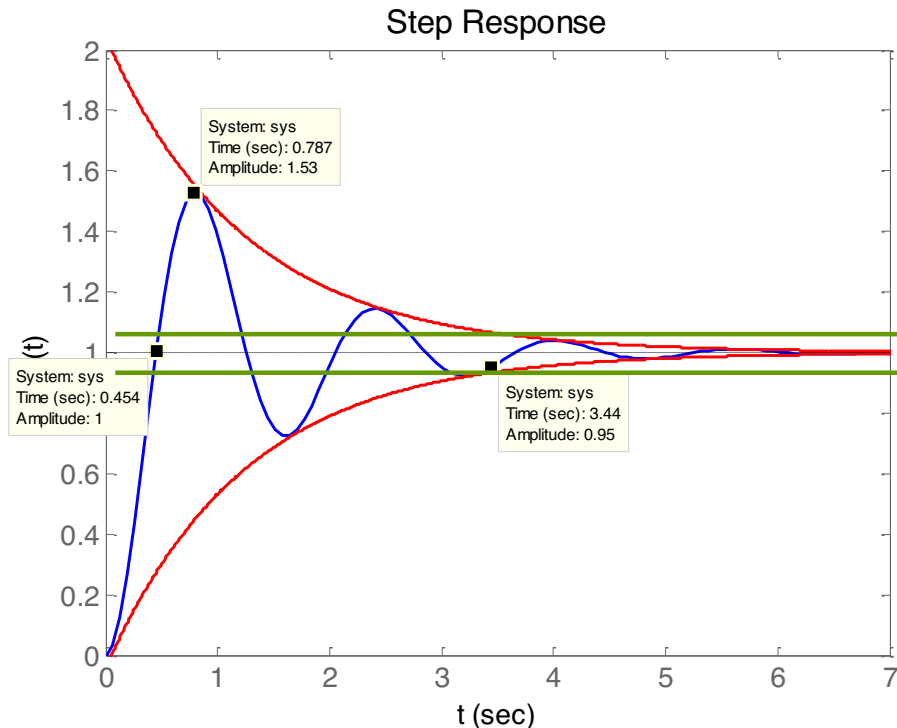
$\sigma^2 + \omega_d^2 = \omega_n^2$

$\theta = \arctan \frac{\sqrt{1-\zeta^2}}{\zeta}$

$= \arccos \zeta$

5.3 2nd-order System Performance

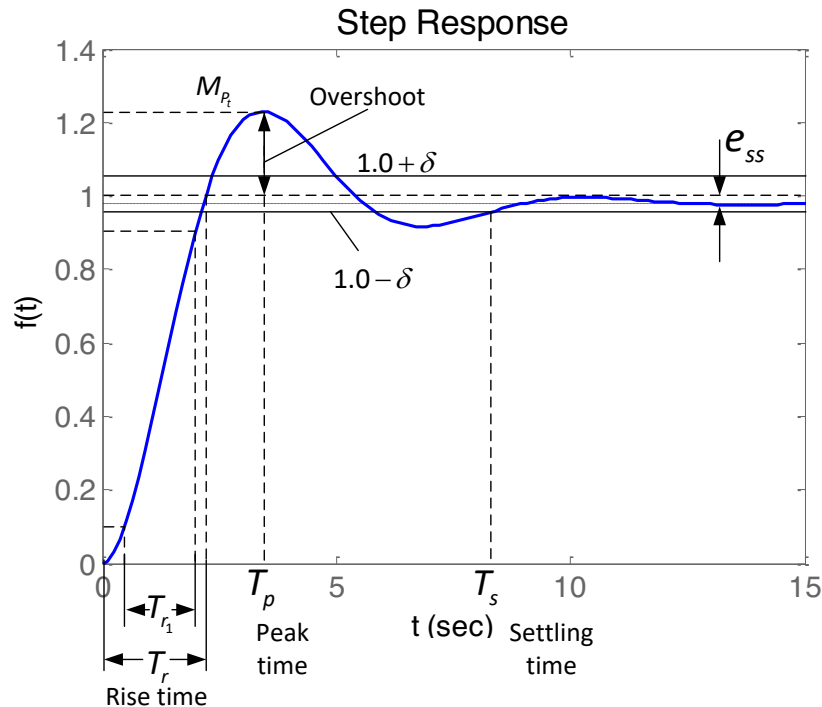
$$\frac{Y(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\omega_n\zeta s + \omega_n^2}, \omega_n = 4, \zeta = 0.2$$



5.3 2nd-order System Performance

The parameters: T_p , $P.O.$, T_r , T_s .

For a 2nd-order system with a unit step input $r(t)=1$:



5.3 2nd-order System Performance

① **T_p (peak time)**: the time it takes to rise from 0 to the peak value of the time response

$$\frac{dy(t)}{dt} = 0$$

$$T_p = \frac{\pi}{\omega_n \sqrt{1-\zeta^2}} = \frac{\pi}{\omega_d}$$

$$M_{pt} = y(T_p) = 1 + e^{\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}}$$

$$y(t) = 1 - \frac{e^{-\sigma t}}{\sqrt{1-\zeta^2}} \sin(\omega_d t + \theta)$$

$$T_p \propto \frac{1}{\omega_n}$$

5.3 2nd-order System Performance

② **P.O. (percentage overshoot)**

$$P.O. = \frac{M_{pt} - fv}{fv} \times 100\%$$

M_{pt} : the peak value of the output response

fv : final value

For the typical second order system (unit step input), $fv=1$

$$P.O. = e^{\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}} \times 100\%$$

$$\zeta \uparrow \Rightarrow P.O. \downarrow$$

5.3 2nd-order System Performance

③ T_r (rising time)

$$y(t) = 1 - \frac{e^{-\sigma t}}{\sqrt{1-\zeta^2}} \sin(\omega_d t + \theta)$$

The time it takes to rise from 0 to 100% of the magnitude of the step input

$$y(T_r) = 1 \Rightarrow \sin(\omega_n \sqrt{1-\zeta^2} T_r + \arccos \zeta) = 0$$

$$\omega_n \sqrt{1-\zeta^2} T_r + \arccos \zeta = k\pi \Rightarrow T_r = \frac{\pi - \arccos \zeta}{\omega_n \sqrt{1-\zeta^2}} \quad T_r \propto \frac{1}{\omega_n}$$

5.3 2nd-order System Performance

④ T_s (settling time):

The time required for the system to settle within a certain percentage of the input amplitude.

$$|y(T_s) - 1| < \Delta, \quad \Delta = 2\% \& 5\%$$

3-4

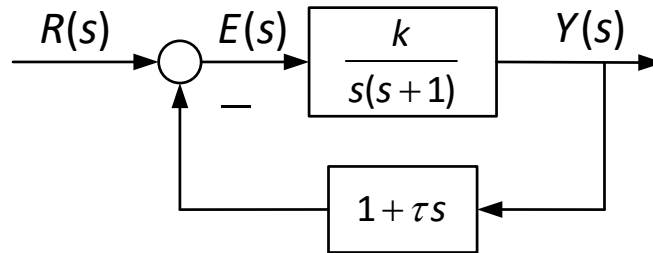
$$T_s = \frac{4}{\zeta \omega_n}, \quad \Delta = 2\%$$

$$T_s = \frac{3}{\zeta \omega_n}, \quad \Delta = 5\%$$

$$T_s \propto \frac{1}{\omega_n}$$

5.3 2nd-order System Performance

Example 1



The response to a unit step input is specified as $P.O.=20\%$, $T_p=1s$.

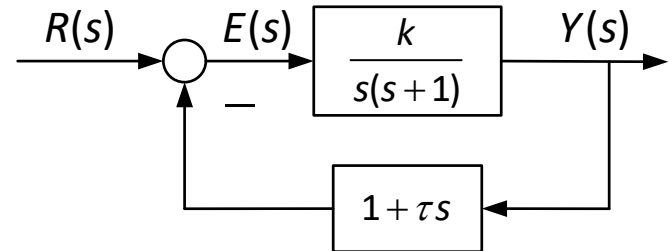
Determine k , τ , T_r , and T_s .

5.3 2nd-order Sys Performance

Example 1

$P.O.=20\%$, $t_p=1s$

k , τ to a unit step input



$$T(s) = \frac{\frac{k}{s(s+1)}}{1 + \frac{k}{s(s+1)}(1+\tau s)} = \frac{k}{s^2 + (1+k\tau)s + k} = \frac{\omega_n^2}{s^2 + 2\omega_n\zeta s + \omega_n^2}$$

$$\text{where } k = \omega_n^2, 1 + k\tau = 2\omega_n\zeta \Rightarrow k = \omega_n^2, \tau = \frac{2\omega_n\zeta - 1}{k}$$

$$P.O. = \frac{M_{pt} - f_v}{f_v} \times 100\% = e^{\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}} \times 100\% = 20\% \Rightarrow \zeta = 0.45$$

$$T_p = \frac{\pi}{\omega_n \sqrt{1-\zeta^2}} = 1s \Rightarrow \omega_n = 3.5 \Rightarrow k = 12.25, \tau = 3.52$$

5.3 2nd-order System Performance

Example 2

Discuss how T and k influence the system performance

$$\frac{Y(s)}{R(s)} = \frac{k/T}{s^2 + (1/T)s + k/T} = \frac{\omega_n^2}{s^2 + 2\omega_n\zeta s + \omega_n^2}, \quad 1/T = 2\omega_n\zeta, k/T = \omega_n^2$$

1) for a given T , $k \uparrow \Leftrightarrow \zeta \downarrow \omega_n \uparrow$

无限 没有超调

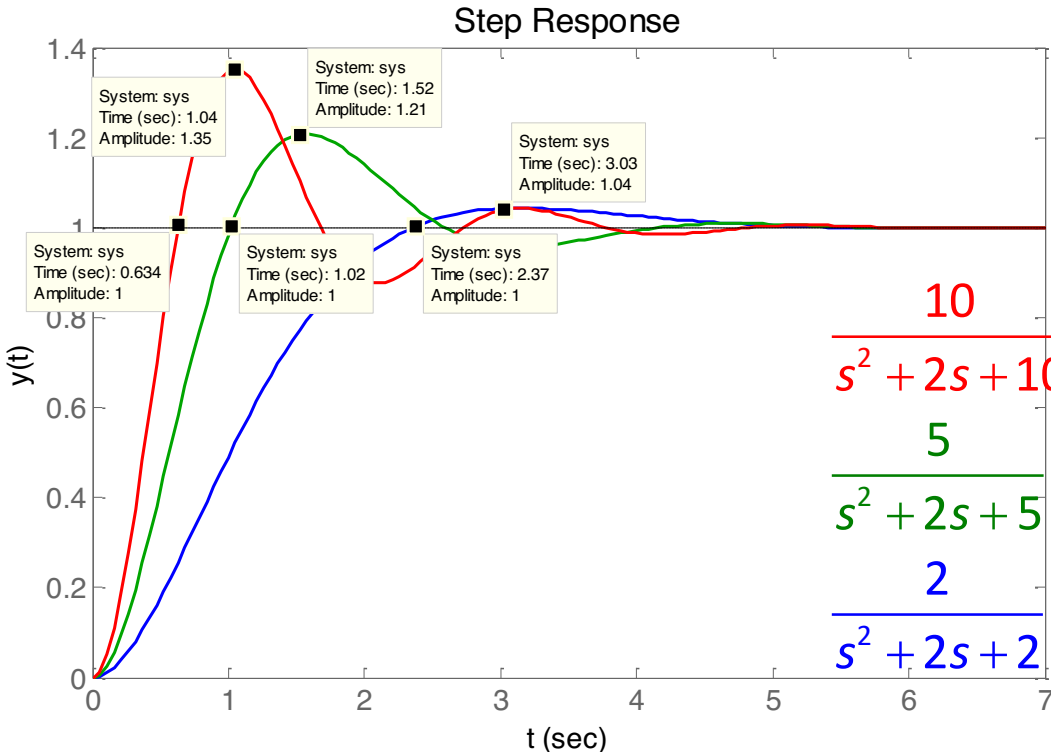
$$P.O. = 100e^{\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}} = e^{\frac{-\pi}{\sqrt{\zeta^2-1}}} \quad \uparrow$$

$$T_s = \frac{3 \sim 4}{\zeta\omega_n} \rightarrow$$

$$T_p = \frac{\pi}{\omega_n\sqrt{1-\zeta^2}} \quad \downarrow$$

$$T_r = \frac{\pi - \arccos\zeta}{\omega_n\sqrt{1-\zeta^2}} \quad \downarrow$$

5.3 2nd-order System Performance



$$\frac{10}{s^2 + 2s + 10}, T = 0.5, k = 5$$
$$\frac{5}{s^2 + 2s + 5}, T = 0.5, k = 2.5$$
$$\frac{2}{s^2 + 2s + 2}, T = 0.5, K = 1$$

```
>> num=[2];den=[1 2 2];step(num,den);hold on;  
>> num=[5];den=[1 2 5];step(num,den);hold on;  
>> num=[10];den=[1 2 10];step(num,den);hold on;
```

The Performance of Feedback System

5.3 2nd-order System Performance

$$\frac{Y(s)}{R(s)} = \frac{k/T}{s^2 + (1/T)s + k/T} = \frac{\omega_n^2}{s^2 + 2\omega_n\zeta s + \omega_n^2}, \quad 1/T = 2\omega_n\zeta, k/T = \omega_n^2$$

2) for a given $k, T \uparrow \Leftrightarrow \omega_n \downarrow, \zeta \downarrow$

tradeoff

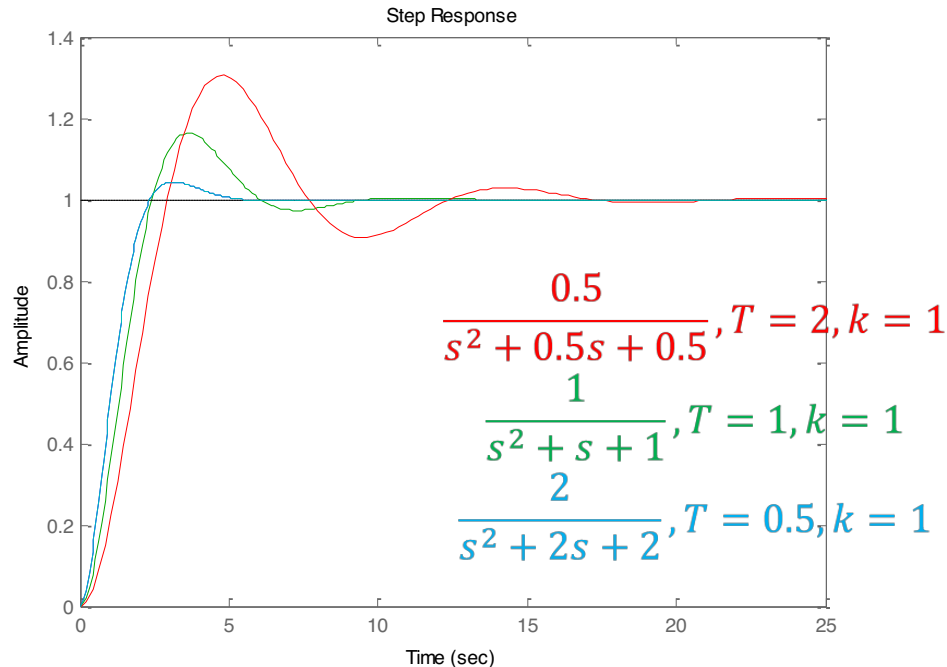
$$P.O. = 100 \cancel{e}^{\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}} = e^{\frac{-\pi}{\sqrt{\zeta^2-1}}} \uparrow$$

$$T_s = \frac{3.5 \sim 4}{\zeta\omega_n} \uparrow$$

$$T_p = \frac{\pi}{\omega_n\sqrt{1-\zeta^2}} \uparrow$$

$$T_r = \frac{\pi - \arccos\zeta}{\omega_n\sqrt{1-\zeta^2}} \uparrow$$

5.3 2nd-order System Performance



```
>> num=[1];den=[1 0.4 1];step(num,den);hold on;  
>> num=[1];den=[1 0.8 1];step(num,den);hold on;  
>> num=[1];den=[1 1.4 1];step(num,den);hold on;  
>> num=[1];den=[1 1.8 1];step(num,den);hold on;
```

5.3 2nd-order System Performance

$$\left. \begin{array}{l} T_r, T_p, T_s \\ P.O. \end{array} \right\} \begin{array}{l} T: \text{consistent} \\ K: \text{contradictory} \end{array}$$

Sometimes, we can not meet all specifications simultaneously, a necessary compromise is needed.

5.4 Effect of a third pole and zero

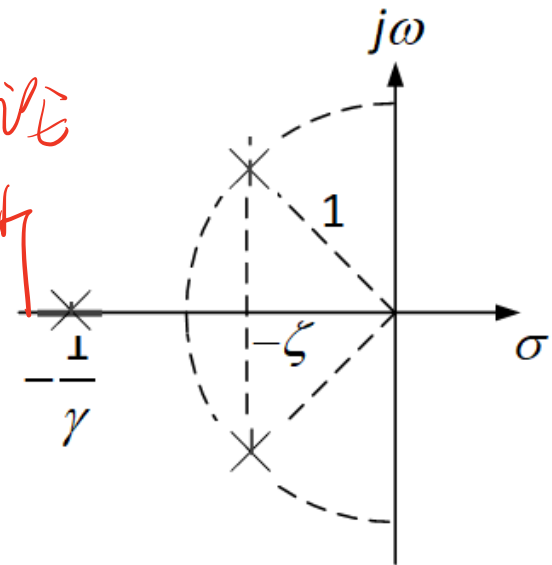
1. A third pole effect

$$T(s) = \frac{Y(s)}{R(s)} = \frac{1}{(s^2 + 2\zeta s + 1)(\gamma s + 1)}, 0 < \zeta < 1, R(s) = \frac{1}{s}, y(t) = ?$$

$$\text{Let } \zeta = 0.5, T(s) = \frac{1}{(s^2 + s + 1)(\gamma s + 1)}$$

γ	$\frac{1}{\gamma}$	P. O.	t_s
2.25	0.444	0	9.63
1.5	0.666	3.9	6.3
0.9	1.111	12.3	8.81
0.4	2.50	18.6	8.67
0.05	20.0	20.5	8.37
0	∞	20.5	8.24

理论
分析



5.4 Effect of a third pole and zero

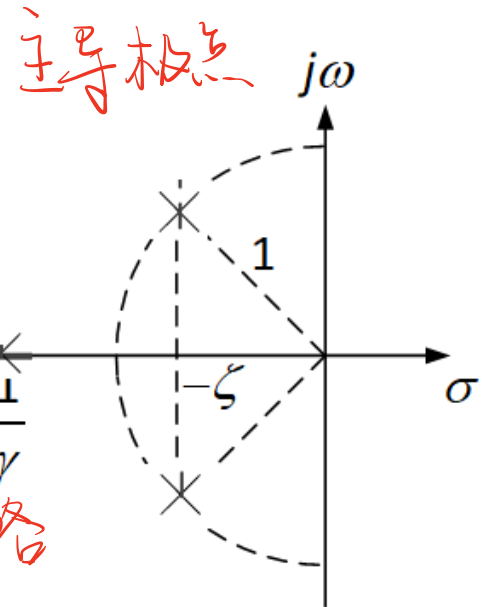
1. A third pole effect

通过实验
确定

It was ascertained experimentally that the response of the third-order system can be approximated by the dominant roots of the second-order system when

$$\left| \frac{1}{\gamma} \right| \geq (10 \text{ or } 5) |\zeta \omega_n|$$

工程

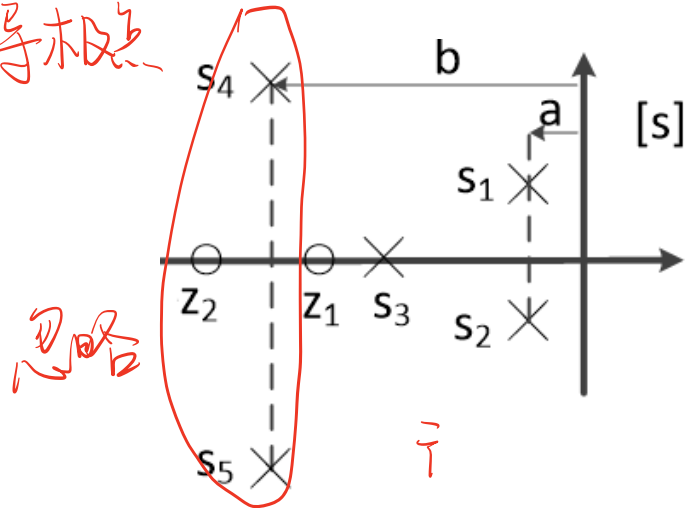
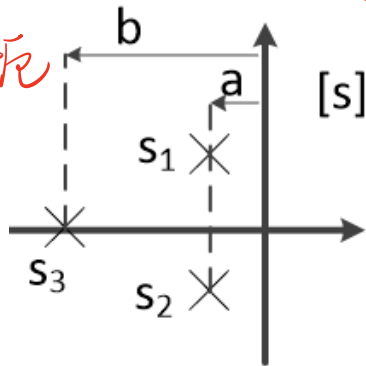


i.e. the real part of the dominant roots is less than one tenth(fifth) of the real part of the third root.

5.4 Effect of a third pole and zero

2. Dominant poles 主导极点

一定指共轭的复根



● For a stable higher-order system, the poles would be the dominant poles when the location of the close-loop is

① The closest poles to the imaginary axis are the conjugate complex poles

② Other poles are far away from Im axis and $b \geq 5a$

● The transient response can be determined by dominant poles.

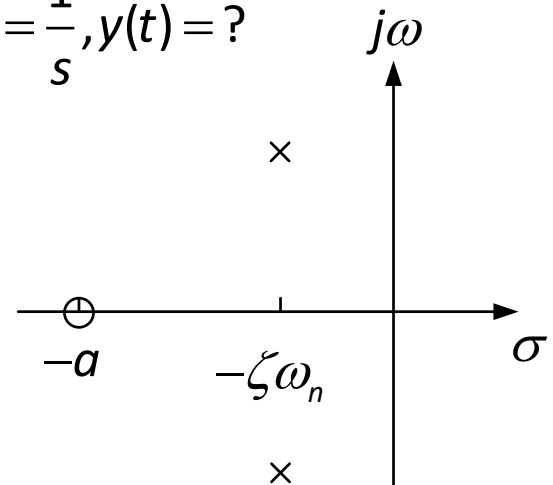
5.4 Effect of a third pole and zero

3. Effects of a zero

$$T(s) = \frac{(\omega_n^2 / a)(s + a)}{(s^2 + 2\zeta\omega_n s + \omega_n^2)}, 0 < \zeta < 1, R(s) = \frac{1}{s}, y(t) = ?$$

$\frac{a}{\zeta\omega_n}$	P.O.	t_s	t_p
5	23.1	8	3
2	39.7	7.6	2.2
1	89.9	10.1	1.8
0.5	210.0	10.3	1.5

$\frac{a}{\zeta\omega_n} \uparrow \Rightarrow P.O. \downarrow, t_s \downarrow, t_p \uparrow$
 超调时间



相当于增加了系统的阻尼

Avoid selecting zeros near the imaginary axis or the dominant poles.

5.5 s-plane root location & the transient response

Closed-loop TF:

$$\frac{Y(s)}{R(s)} = \frac{\sum P_k \Delta_k}{\Delta} = \frac{G(s)}{1+G(s)} = \frac{\text{zeros}}{\text{poles}}$$

$$\text{CE: } \Delta = 0 \Rightarrow 1 + G(s) = 0$$

$$R(s) = \frac{1}{s} \Rightarrow Y(s) = \frac{\text{zeros}}{\text{poles}} \cdot R(s)$$

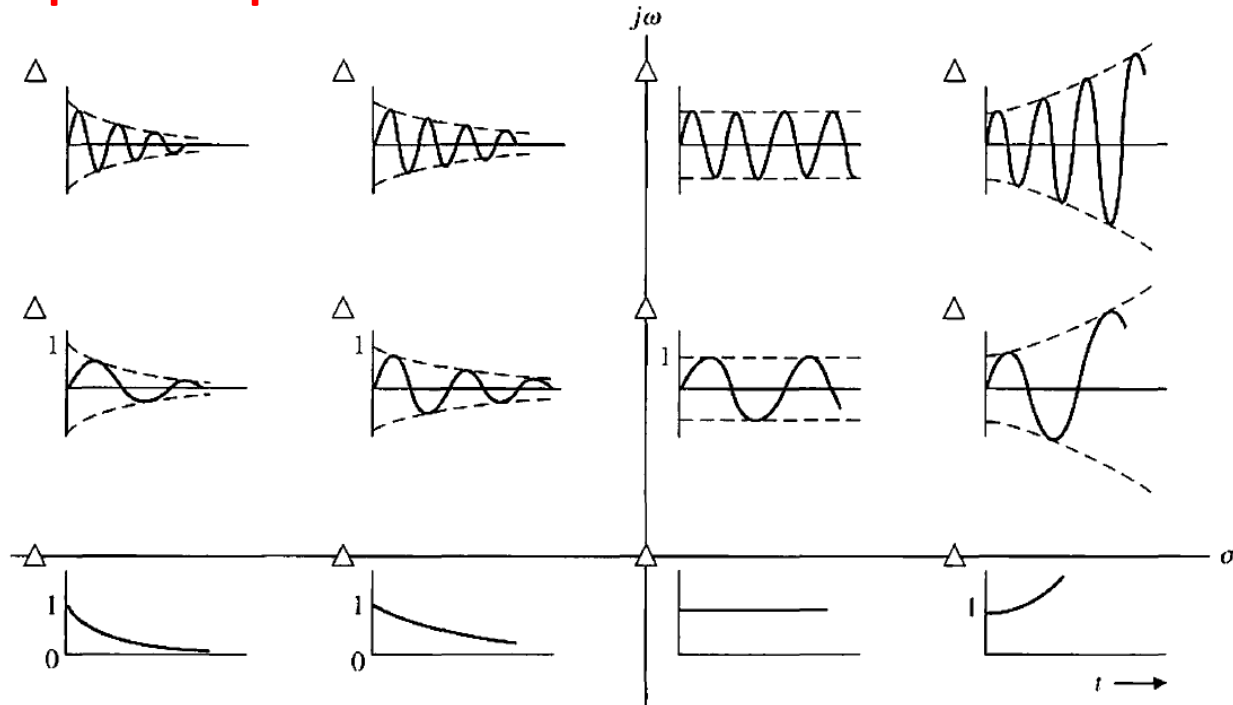
Under none repeated roots assumptions:

$$Y(s) = \frac{1}{s} + \sum_{i=1}^M \frac{A_i}{s + \sigma_i} + \sum_{k=1}^N \frac{B_k s + C_k}{s^2 + 2\alpha_k s + (\alpha_k^2 + \omega_k^2)}$$

$$y(t) = 1 + \sum_{i=1}^M A_i e^{-\sigma_i t} + \sum_{k=1}^N D_k e^{-\alpha_k t} \sin(\omega_k t + \theta_k)$$

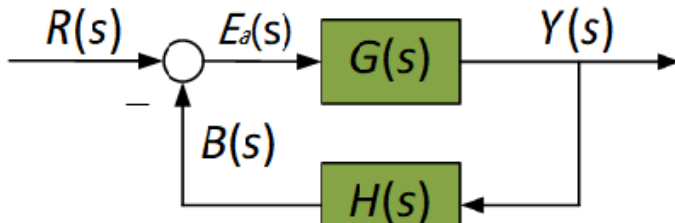
5.5 s-plane root location & the transient response

The impulse response for various root locations:



稳态误差

5.6 the Steady-state Error



$$E(s) = R(s) - Y(s)$$

$$E(s) = R(s) - Y(s) = R(s) - T(s)R(s)$$

$$= \left(1 - \frac{G(s)}{1 + G(s)H(s)}\right)R(s)$$

$$= \frac{1 + G(s)H(s) - G(s)}{1 + G(s)H(s)}R(s)$$

$$\begin{aligned} E_a(s) &= R(s) - B(s) \\ &= R(s) - H(s)Y(s) \\ &= \frac{1}{1 + G(s)H(s)}R(s) \end{aligned}$$

$$E(s) = \frac{1}{1 + G(s)H(s)}R(s) = E_a(s)$$

两种形式
相同

$$H(s) = 1$$

$$e_{ss} = e(\infty) = \lim_{t \rightarrow \infty} e(t) = \lim_{s \rightarrow 0} sE(s) = \lim_{s \rightarrow 0} s \frac{1}{1 + G(s)}R(s)$$

5.6 the Steady-state Error

$$e_{ss} = e(\infty) = \lim_{t \rightarrow \infty} e(t) = \lim_{s \rightarrow 0} sE(s) = \lim_{s \rightarrow 0} s \frac{1}{1 + G(s)} R(s)$$

The general open-loop transfer function is

$$G(s) = \frac{K \prod_{j=1}^M (s + z_j)}{s^N \prod_{i=1}^Q (s + p_i)}$$

$N=0$	$N=1$	$N=2$
Type 0	Type I	Type II

N: The type number of the system

Three steady-state error constants:

① position error constant

$$K_p = \lim_{s \rightarrow 0} G(s)$$

位置误差系数

② velocity error constant

$$K_v = \lim_{s \rightarrow 0} sG(s)$$

速度

③ acceleration error constant

$$K_a = \lim_{s \rightarrow 0} s^2 G(s)$$

加速度

5.6 the Steady-state Error

① For step input, $R(s) = \frac{A}{s}$

$$e_{ss} = e(\infty) = \lim_{t \rightarrow \infty} e(t) = \lim_{s \rightarrow 0} sE(s) = \lim_{s \rightarrow 0} s \frac{1}{1+G(s)} R(s)$$

$$= \lim_{s \rightarrow 0} s \frac{1}{1+G(s)} \frac{A}{s} = \frac{A}{1 + \lim_{s \rightarrow 0} G(s)}$$

$$= \frac{A}{1 + K_p} \quad (\text{type 0})$$

$$= \frac{A}{1 + \infty} = 0 \quad (\text{type I})$$

$$= \frac{A}{1 + \infty} = 0 \quad (\text{type II})$$

5.6 the Steady-state Error

② For ramp input, $R(s) = \frac{A}{s^2}$

$$e_{ss} = e(\infty) = \lim_{t \rightarrow \infty} e(t) = \lim_{s \rightarrow 0} sE(s) = \lim_{s \rightarrow 0} s \frac{1}{1 + G(s)} R(s)$$

$$= \lim_{s \rightarrow 0} s \frac{1}{1 + G(s)} \frac{A}{s^2} = \lim_{s \rightarrow 0} \frac{A}{s + sG(s)} = \frac{A}{\lim_{s \rightarrow 0} sG(s)}$$

$$= \frac{A}{0} = \infty \quad (\text{type 0})$$

$$= \frac{A}{K_v} \quad (\text{type I})$$

$$= \frac{A}{\infty} = 0 \quad (\text{type II})$$

5.5 the Steady-state Error

③ For acceleration input, $R(s) = \frac{A}{s^3}$

$$e_{ss} = e(\infty) = \lim_{t \rightarrow \infty} e(t) = \lim_{s \rightarrow 0} sE(s) = \lim_{s \rightarrow 0} s \frac{1}{1 + G(s)} R(s)$$

$$= \lim_{s \rightarrow 0} s \frac{1}{1 + G(s)} \frac{A}{s^3} = \frac{A}{\lim_{s \rightarrow 0} s^2 G(s)}$$

$$= \frac{A}{0} = \infty \quad (\text{type 0})$$

$$= \frac{A}{0} = \infty \quad (\text{type I})$$

$$= \frac{A}{K_a} \quad (\text{type II})$$

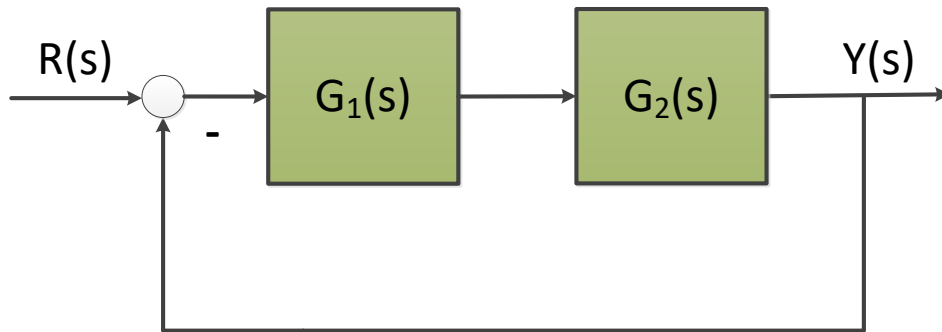
5.6 the Steady-state Error

The value of e_{ss} depends on the type of $R(s)$ and $G(s)$

	Type 0	Type 1	Type 2
Step input	$\frac{A}{1 + K_p}$	0	0
Ramp input	∞	$\frac{A}{K_v}$	0
Acceleration input	∞	∞	$\frac{A}{K_a}$

设置系统

Example(5.6)



$$G_1(s) = k_1 + \frac{k_2}{s}$$

$$G_2(s) = \frac{k}{\tau s + 1}$$

Determine e_{ss}

5.7 Summary

Concept

- Test input signals: step, ramp, parabolic, impulse
- Performance of the second-order system with unity step input
rise time, peak time, settling time, percent overshoot
- Dominant poles, effects of the zero 降阶
- The relationship between the s-plane root location and the transient response
- The steady-state error
 K_p, k_a, k_v

Technique

- Calculate $T_r, T_p, T_s, P.O.$ 百分比调整量
- Calculate steady-state error

End