## Scilab Textbook Companion for Microwave Devices And Circuits by S. Y. Liao<sup>1</sup>

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# **Book Description**

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Scilab numbering policy used in this document and the relation to the above book.

Exa Example (Solved example)

Eqn Equation (Particular equation of the above book)

**AP** Appendix to Example(Scilab Code that is an Appednix to a particular Example of the above book)

For example, Exa 3.51 means solved example 3.51 of this book. Sec 2.3 means a scilab code whose theory is explained in Section 2.3 of the book.

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## Chapter 2

### Electromagnetic plane waves

Scilab code Exa 2.6.5 Calculation of a Gold Film Coating

```
2/\cosh pter_no.-2, page_no.-69
\frac{3}{\sqrt{\text{Example No.}}} - 2 - 6 - 5
5 clc;
  //(a) Program_to_find_gold_film_surface_resistance
9
10 t=80*(10^(-10));//Film_Thickness
                   //Bulk_conductivity
11 \quad o=4.1*(10^7);
12 p=570*(10^(-10)); //Electron_mean_free_path
13 of = [(3*t*o)/(4*p)]*[0.4228 + log(p/t)]; //the_gold -
      film_conductivity_is_of = [3*t*o/4*p]*[0.4228 + ln(
      p/t)]
14
15 Rs=1/(t*of);//
      the_gold_film_surface_resistance_is_given_by__Rs
      =1/(t*of) in_Ohms_per_square
16 disp(Rs,'
      the_gold_film_surface_resistance_in_Ohms_per_square_is
```

```
<sup>'</sup>);
17
18
19
20
21
   //(b) Program_to_find_the_microwave_attenuation
22
23 Attenuation=40-20*log10(Rs)
                                         //
      Microwave_attenuation
24
  disp(Attenuation, 'Microwave_Attenuation_is_in_db_is
      : ');
26
27
  //(c)Light_transmittance_T
28
29
30 disp('From figure No.2-6-5 of Light transmittance T
      and light attenuation loss L versus wavelength
      with film thickness t as parameter for gold film,
       we find that for given gold film of thickness 80
       angstrom , the LIGHT TRANSMITTANCE T is estimated
       to be 75\%');
31
32
33
  //(d) light_reflection_loss_R
34
35
36 disp('
      From\_the\_same\_figure\_the\_LIGHT\_REFLECTION\_LOSS\_R\_is\_about\_25\%
       <sup>'</sup>);
```

Scilab code Exa 2.6.6 Computation of a Copper Film Coating

```
2 //chapter_no.-1, page_no.-74
```

```
\frac{3}{\sqrt{\text{Example No.}}} - \frac{2-6-6}{6}
4 clc;
  //(a) Program_to_find_copper-film_surface_resistance
7
9 t=60*(10^(-10));//Film_Thickness
                   //Bulk_conductivity
10 o=5.8*(10^7);
11 p=420*(10^(-10)); //Electron_mean_free_path
12 of = [(3*t*o)/(4*p)]*[0.4228 + log(p/t)]; ////
      the_copper-film_conductivity_is_of = [3*t*o/4*p]
      *[0.4228 + ln(p/t)]
13
14
15
16 Rs=1/(t*of);//
      the_copper_film_surface_resistance_is_given_by__Rs
      =1/(t*of) in_Ohms_per_square
17 disp(Rs,'
      the_copper_film_surface_resistance_in_Ohms_per_square_is
      ');
18
19
20 //(b) Program_to_find_the_microwave_attenuation
21
                                       //
22 Attenuation=40-20*log10(Rs)
      Microwave_attenuation
23
24 disp(Attenuation, 'Microwave_Attenuation_in db is:'
      );
25
26
  //(c)Light_transmittance_T
27
28 disp ('From figure No.2-6-11 of Light transmittance T
       and light attenuation loss L versus wavelength
      with film thickness t as parameter for copper
      film, we find that for given copper film of
      thickness 60 angstrom , the LIGHT TRANSMITTANCE T
```

```
is estimated to be 82%');
29
30 //(d)light_reflection_loss_R
31
32 disp('From the same figure the LIGHT REFLECTION LOSS R is about 18%');
```

## Chapter 3

## Electromagnetic plane waves

Scilab code Exa 3.1.1 Line characteristic impedance and phase constant

```
2 / \cosh pter_no. -3, page_no. -84
3 / \text{Example_no.3} - 1 - 1
5 clc;
6
  //(a) Calculate_the_line_Characteristic_Impedance
9
10
11 R=2;
12 L=8*(10^-9);
13 C = .23*(10^-12);
14 f=1*(10^9);
15 G = .5*(10^-3);
16 \ w=2*\%pi*f;
17
18 Z0 = sqrt((R + (\%i*w*L))/(G + (\%i*w*C)));
19 x=real(Z0);
20 y = imag(Z0);
21 o=atand(y,x);
```

```
22 disp(o, 'the_phase_of_ZO_is = ');
23 M = abs(Z0); //magintue_of_Z0
24 disp(M, 'the_magnitude_of_ZO_is = ');
25 disp(ZO, 'the_line_characteristic_impedance is =');
26
27
28
29 //(b) Calculate_the_propagation_constant
30
31 r = sqrt((R + (\%i*w*L))*(G + (\%i*w*C)));
32 x = real(r);
33 y = imag(r);
34 \text{ o=atand}(y,x);
35 disp(o, 'the_phase_of_r_is = ');
36 M=abs(r);//magintue_of_r
37 disp(M, 'the_magnitude_of_r_is =');
38 disp(r, 'the_propagation_constant is =');
```

#### Scilab code Exa 3.2.1 reflection coefficient and transmissioncoefficient

```
1
2
3  //chapter_no.-3, page_no.-89
4  //Example_no.3-2-1
5  clc;
6
7
8  //(a) Calculate_the_reflection_coefficient
9
10
11  Z1=70+(%i*50);
12  Z0=75+(%i*.01);
13  r=(Z1-Z0)/(Z1+Z0);
14  x=real(r);
15  y=imag(r);
```

```
16 o=atand(y,x);
17 disp(o, 'the_phase_of_reflection_coefficient is =');
18 M=abs(r);//magintue_of_r
19 disp(M, 'the_magnitude_of_reflection_coefficient_is =
      ');
20 disp(r, 'the_reflection_coefficient is =');
21
22
23
24
  //(b) Calculate_the_transmission_coefficient
25
26
27
28 T = (2*Z1)/(Z1+Z0);
29 x = real(T);
30 y = imag(T);
31 \text{ o=atand}(y,x);
32 disp(o, 'the_phase_of_transmission_coefficient is =')
33 M=abs(T);//magintue_of_T
34 disp(M, 'the_magnitude_of_transmission_coefficient_is
35 disp(T, 'the_transmission_coefficient is =');
36
37
38
  //(c) Verify_the_relationship_shown_in_Eq (3-2-21)
40
41
42 T2=T^2;
43 x = real(T2);
44 y = imag(T2);
45 \text{ o=atand}(y,x);
46 disp(o, 'the_phase_of_T^2_is =');
47 M = abs(T2); // magintue_of_T^2
48 disp(M, 'the_magnitude_of_T^2_is =');
49 disp(T2, 'T^2 = ');
50
```

```
51 p=(Z1/Z0)*(1-(r^2));
52 x = real(p);
53 y = imag(p);
54 \text{ o=atand(y,x)};
55 disp(o, 'the_phase_of_(Zl/Z0)*(1-(r^2)_is =');
56 M = abs(T2); // magintue_of_(Z1/Z0)*(1-(r^2))
57 disp(M, 'the_magnitude_of_(Z1/Z0)*(1-(r^2)_is =');
58 disp(p,'(Z1/Z0)*(1-(r^2)) = ');
59 disp('since T^2 = (Z1/Z0)*(1-(r^2)) hence
      the_relationship_shown_in_Eq(3-2-21) is verified,
      );
60
61
62
63
64 // (d)
      Verify\_the\_transmission\_coefficient\_equals\_equals\_the\_algebraic\_supplies
      (2-3-18)
65
66
67 y=r+1;
68
69 disp(T, 'T = ');
70 disp(y, r+1 = ');
71 disp('since T = r+1 hence
      the_relationship_shown_in_Eq(2-3-18) is verified,
      );
```

#### Scilab code Exa 3.3.1 Standing Wave Ratio

```
1
2 //chapter_no.-3, page_no.-93
3 //Example_no.3-3-1
4 clc;
5
```

```
//(a) Calculate_the_reflection_coefficient
8
9 Z1=73-(\%i*42.5);
10 Z0=50+(\%i*.01);
11 rl = (Zl - Z0)/(Zl + Z0);
12 x=real(r1);
13 y=imag(r1);
14 o=atand(y,x);
15 disp(o, 'the_phase_of_reflection_coefficient is =');
16
17 M = abs(rl); // magintue_of_r
18 disp(M, 'the_magnitude_of_reflection_coefficient_is =
      <sup>'</sup>);
19 disp(rl, 'the_reflection_coefficient is =');
20
21
22
23 //(b) Calculate_the_standing-wave_ratio
24
25
26 p = (1+M)/(1-M);
27 disp(p, 'the_standing-wave_ratio is =');
```

#### Scilab code Exa 3.4.1 Line Impedance

```
1
2
3 //chapter_no.-3, page_no.-99
4 //Example_no.3-4-1
5
6 clc;
7
8
9 //(a) Calculate_the_input_impedance
```

```
10
11
12 syms x; //x_{is}wavelength
13 Bd=(((2*\%pi)/x)*(x/4));
disp(Bd, 'from_Eq(3-4-26)_the_line_that_is_2.25
      _wavelengths_long_looks like_a_quarter-wave line,
      then Bd= ');
15
16 R0=50; //input_impedance
17 Rl=75; //load_resistance
18 Zin=(R0^2)/R1;
19 disp(Zin, 'From_Eq(3-4-26), the_input_impedance((
      in\_ohms)\_is = ');
20
21
22 //(b)
      Calculate\_the\_magnitude\_of\_the\_instantaneous\_load\_voltage
23
24
25 R0=50; //input_impedance
26 R1=75; //load_resistance
27 rl = (Rl - R0) / (Rl + R0);
28 disp(rl, 'the_reflection_coefficient is =');
29
30
31
32 //(b)
      Calculate\_the\_magnitude\_of\_the\_instantaneous\_load\_voltage
33
34
35 R0=50; //input_impedance
36 R1=75; //load_resistance
37 rl = (Rl - R0) / (Rl + R0);
38 disp(rl, 'the_reflection_coefficient is =');
39
40 V=30; //open-circuit_output_voltage
```

```
41
42 Vl = V * (exp(-1 * \%i * Bd)) * (1 + rl);
43 Vl=abs(V1);
44 disp(V1, 'the_instantaneous_voltage_at_the_load(in V)
      _{i} = ');
45
46
47
48 // (c)
      Calculate\_the\_instantaneous\_power\_delivered\_to\_the\_load
49
50
51 Pl = (Vl^2)/Rl;
52 disp(P1, '
      the_instantaneous_power_delivered_to_the_load(in
      W) is = ');
```

#### Scilab code Exa 3.5.1 Location of Voltage maxima and minima from load

```
//chapter_no.-3, page_no.-104
//Example_no.3-5-1

clc;

Zl=1+ %i*1;//Given normalise load impedance
disp('1. Enter Zl=1+(1*i) on the chart');
disp('read .162lamda on the distance scale by drawing a dashed straight line from the centre of the chart through the load point and inersecting the distance circle');

disp('2. move a distance from the point at .162lamda towards the generator and first stop at the
```

```
voltage maxima on the right hand side real axis
       at .25 lambda');
12 lambda=5; // Given wavelength =5
13 dVmax = (.25 - .162) * lambda;
14 \operatorname{disp}(\operatorname{dVmax}, \operatorname{d1}(\operatorname{Vmax}) \text{ (in cm)=')};
15
16 disp('Similarly, , move a distance from the point of
       .162 lambda towards the generator and first stop
       at the voltage minimum on the left-hand real axis
        at .5 lambda');
17 dVmin = (.5 - .162) * lambda;
18 \operatorname{disp}(\operatorname{dVmin}, \operatorname{dl}(\operatorname{Vmin}) \text{ (in cm)=')};
19
20 disp('4. Make a standing wave circle with the centre
       (1,0) and pass the circle through the point of 1+
       j1. The location intersected by the circle at the
       right portion of the real axis indicates the SWR
       this is p=2.6');
```

#### Scilab code Exa 3.5.2 Impedance with short circuit minima shift

```
1
2 //Example_no.3-5-2
3
4 clc;
5
6 disp('1. When the line is shorted ,the first voltage minimum occurs at the place of the load ');
7
8 disp('2 .When the line is loaded ,the first voltage minimum shifts .15lambda from the load .the distance between successive minimas is half the wavelength');
9
10 disp('3.plot a SWR cirle for p=2');
```

#### Scilab code Exa 3.6.1 Single Stub Matching

```
1
2 / chapter_no. -3, page_no. -108
3 ///Example_no.3-6-1
4 clc;
5
6 R0=50; //characteristic impedance
7 Z1=50/(2+\%i*(2+sqrt(3)));
8 zl=R0/Z1;//normaised load impedance
9 yl=1/zl;//normaised load admittance
10 disp('1. compute the normalised load admittance and
      enter it on the smith chart');
11
12 disp('2 .Draw a SWR circle throuh the point of yl so
      that he circle intersects the unity circle at
     the point yd ');
13 \text{ yd}=1-\%i*2.6;
14 disp(yd, 'yd=');
15
16 disp ('note that there are infinite number of yd.take
      the one that allows the stub to be attached as
```

```
closely as possible the load');
17
18 disp('3. since the charcteristic impedance of the
     stub is different from that of the line , the
      condition for impedance matching at the junction
      requires Y11=Yd + Ys , where Ys is the susceptance
       that the stub will contribute');
     disp('it is clear that the stub and the portion of
19
         the line from the load to the junction are in
        parallel, as seen by the main line extending to
        the generator .the admittance must be converted
         to normalised values for matching on the smith
         chart .the our equation becomes');
20
     disp('y11*Y0= yd*Y0 + ys*y0s');
21
22
23
     Y0=100; // charcteristic impedance of the stub
24
     Y0s = 50;
     ys = (y11 - yd) * (Y0/Y0s);
25
26
27
     disp('4. the distance between the load and the
        stub position can be calculated from the
        distance scale as d=(.302-.215)*lambda');
28
     disp('5. since the stub contributes a susceptance
29
        of j5.20, enter j5.20 on the chart and
        determine the required distance I from the
        short circuited end(z=0,y=infinity), which
        corresponds to the right side of the real axis
        on the chart, by transversing the chart towards
        the generator until the point of j5.20 is
                  Then l = (.5 - .031) lambda = .469 lambda.
        reached.
        When a line is matched at the junction , there
        will be no standing wave in the line from the
        stub to the generator');
30
31
     disp('If an inductive stub is required yd = 1+j
        *.26 and the susceptance will be ys = -j*5.2');
```

```
32
33 disp('7. The position of the stub from the load is d=(.5-(.215-.198))lambda = .483 lambda and the length of the short-circuted stub is l = .031 lambda');
```

#### Scilab code Exa 3.6.2 Double Stub Matching

```
1
2 / chapter_no. -3, page_no. -111
3 / \text{Example_no.3} - 6 - 2
4 clc;
5
6 Z1=100+(\%i*100);
  R0=50; // charcteristic impedance of the stub and the
      line
8
9 z1=Z1/R0;
10 disp('1. compute the normalised load admittance and
      enter it on the smith chart');
11
12 disp('2 .plot a SWR circle and read the normalised
     load admittance 180 degree out of phase with zl
     on the SWR circle: ');
13 vl=1/zl;
14 disp(yl, 'yl=');
15
16 disp('3. Draw the spacing circle of (3/8) lambda by
      rotating the constant-conductance unity circle (g
      =1) through a phase angle of 2Bd=2B(3/8lambda)
      =3/2(\%pi) towards the load .now y11 must be on
      this spacing circle , since yd2 will be on the g=1
       circle (y11 and yd2 are 3/8lambda apart)');
17
18 disp('4. move yl for a distance of .4lambda from
```

```
.458 to .358 along the SWR p circle toward the
      generator and read yd1 on the chart: ');
19
20 \text{ yd1} = .55 - \%i * 1.08;
21 disp('yd1=.55-\%i*1.08')
22 disp('5. there are two possible solutions for y11.
      they can be found by carrying yd1 along the
      constant-conducatnce (g=0.55) circle that
      intersects the spacing circle at two points
              y11=.55-j(.11), y11=.55-j(1.88)');
23
24 \text{ y}11 = .55 - (\%i * .11);
25 \text{ y}112 = .55 - (\%i * 1.88);
26
27 disp('at the junction 1-1 y11=yd1+ys1');
28 \text{ ys1} = \text{y11} - \text{yd1};
29 disp(ys1, 'ys1=');
30 \text{ ys} 12 = \text{y} 112 - \text{y} d1;
31 disp(ys12, 'ys12=');
32
33 disp('7. the length of the stub 1 are found as 11
      = (.25 + .123) lambda = .373 lambda = 11  '= (.25 - .107)
      lambda = .143 lambda');
34
35 disp('8. the 3/8lambda section of the line
      transforms y11 to yd2 and y11 to yd2' along their
       constant standing-wave circles respectively.
      That is yd2=1-(\%i*.61) and yd2'=1+(\%i*2.60)');
36
37 \text{ yd2=1-(\%i*.61)};
38 \text{ yd}22=1+(\%i*2.60);
39
40 disp('9. Then stub 2 must contribute ys2 = (.61*\%i)
      and vs2' = (-2.6*\%i)';
41 disp('10. the length of the stub 1 are found as 12
      =(.25+.087) lambda =.337 lambda =11 '=(.308-.25)
      lambda = .058 lambda');
42 disp('11. It can be seen that normalised impedance yl
```

located inside the hatched area cannot be brought to lie on the locus of y11 or y112 for a possible match by the parallel connection of any short-circuited stub because the spacing circle and g=2 circle are mutually tangent. Thus the area of g=2 circle is called the forbidden region of the normalised load admittance for possible match . ')

## Chapter 4

# microwave waveguides and components

 ${f Scilab\ code\ Exa\ 4.1.1\ TE10}$  in Rectangular Waveguide

```
1
2 //CHAPTER-4
  // EXAMPLE: 4-1-1, page no. -128.
  //(a)program_to_find_the_cut-off_frequency_(fc)
       _of_an_airfilled_rectangular_waveguide_in_TE10_mode
6
8 a=0.07
                          b = 0.035
                   ;
                                                          //wave-
      guide_dimensions_in_metres
9 f=3.5*(10^9);
      // Given_that_guide_is_operating_at_a_frequency_of
        3.5 GHZ
10 c=3*(10^8);
      // \quad c_{-}i\,s_{-}t\,h\,e_{-}s\,p\,e\,e\,d_{-}o\,f_{-}t\,h\,e_{-}l\,i\,g\,h\,t
```

```
11 m=1 ; n=0;
      Given_that_guide_operates_in_the_dominant_mode_TE10
12
13 fc=c/(a*2);
      // since, fc = (c/2) * sqrt(((m/a)^2) + ((n/b)^2)). For
      TE10 mode m=1, n=0, fc=c/2*a
14 disp(fc/(10<sup>9</sup>), 'cut-
      off_frequency_for_TE10_mode_in_GHZ=');
                       //display_fc ,fc_is_divided_by_10
      ^9 to_obtain_frequency_in_GHZ
15
16
17
  // (b) program_to_find_the phase_velocity_of_the
      wave_in_the_guide_at_a_frequency_of_3.5GHZ
19
20 f=3.5*(10^9);
      //Given
      that_guide_is_operating_at_a_frequency_of_3.5.GHZ
21 vg=c/(sqrt(1-((fc/f)^2)));
      // since, phase_velocity=c/(sqrt(1-((fc/f)^2)))
22 disp(vg, '
      phase_velocity_for_a_wave_at_a_frequency_of_3.5
      GHZ_{--}(m/s) = ');
                           //display_the_phase_velocity
23
24
25
26
  // (c) program_to_find_the_guide_wavelength (
27
      lg_of_the_wav__at_a_frequency_of 3.5GHZ
28
29
```

#### Scilab code Exa 4.1.2 TE10 mode in Rectangular Waveguide

```
1
2
3 // \text{chapter no.} -4
4 // Example -4-1-2 , page no. -133
5
  //Program to find the peak value of the electric
      field occuring in the guide.
8
9
10 clc;
11 m=1; n=0;
      given guide transports energy in the TE10 mode.
12 f = 30*(10^9);
                                                   //The
      impressed frequency is 30GHZ
13 uo=(4*(\%pi))*(10^-7); eo=8.85*(10^(-12));
```

```
//scientific values of permeability
       and permittivity in free space
14 a = .02; b = .01;
      dimensions of wave-guide given in metres
15 energyrate=0.5*746;
                                           //given , the
      rate of transport of energy =0.5 hp ,1 horse
      power(1 hp) = 746 watts.
16
17 kc=%pi/a;
                                                       //kc
       is cutoff wave number , kc=sqrt((m*%pi/a)+(n*
      \%pi/b)), For m=1,n=0 => kc=\%pi/a
18 bg = sqrt((((2*\%pi*f)^2)*(uo*eo)) - (kc^2));
                   //bg is the phase constant in radian/
      metre, bg=sqrt((w^2)*(uo*eo))-(kc^2); where w=2*
      %pi*f
19 Zg=((2*\%pi*30*(10^9))*uo)/bg;
                                 //Zg is the
      characteristic wave impedence ,Zg=(w*uo)/bg;
      where w=2*\%pi*f
20
21 syms x z Eoy Hoz
                                               //Defining
      the variables
22
23 \text{ Ex=0};
      //\sin ce, Ex=Eox*cos((m*%pi*x)/a)*sin((n*%pi*y)/b)
      *\exp(-\%i*bg*z)...For m=1 , n=0 => Ex=0
24 Ey = Eoy*sin((\%pi*x)/a)*exp(-\%i*bg*z);
                       // \operatorname{since}, Ey = Eoy*sin((m*%pi*x)/a
      *\cos((n*\%pi*y)/b)*\exp(-\%i*bg*z) (here put m=1,n
25 \text{ Ez=0};
      // For TE mode Ez=0
```

```
26
27 Hx = (Eoy/Zg) * sin((\%pi*x)/a) * exp(-\%i*bg*z);
                       //\sin ce, Hx=Hox*\sin(m*\%pi*x)/a)*\cos
       ((n*\%pi*y)/b)*exp(-\%i*bg*z). put m=1,n=0 and Hox
       =(Eoy/Zg)
28 \text{ Hy} = 0;
       \operatorname{since} \operatorname{Hy} = \operatorname{Hoy} \cdot \operatorname{cos} \left( \left( m \cdot \operatorname{pi} \cdot x \right) / a \right) \cdot \operatorname{sin} \left( \left( n \cdot \operatorname{pi} \cdot y \right) / b \right)
       *\exp(-\%i*bg*z) here (for m=1,n=0) => Hy=0
29 Hz=Hoz*cos((\%pi*x)/a)*exp(-\%i*bg*z);
                              //Hz=Hoz*cos(m*\%pi*x)/a)*cos((n)
       *\%pi*v)/b)*exp(-\%i*bg*z). put m=1,n=0.
30
31 \text{ Hxc=Hx'};
       power formula of poynting involves integrating (
       Ey*cojugate(Hx)) over guide dimension. Thus
       we take conjugate of hx for propagation of wave
       in z direction
32
33 power = (Ey*Hxc);
                                                        //(Taking
       the term (Ey*cojugate(Hx)) from power formula of
       poynting vector
34 power=power/(Eoy^2);
       //normalise power with respect to (Eoy^2) so as
       to definitely integrate remaining terms in x and
       у.
35
36 temp = str2max2sym(power.str1);
37 PowerToIntegrate = max2scistr(temp.str1);
                                                               //
       coverting_type_sym_into_type_string
38
39 I=integrate(PowerToIntegrate, 'x',0,a); //integrate
       X=(E_{y}*cojugate(H_{x})) (which is normalised with
       respect to Eoy^2) with respect
```

```
to x dimension from 0 to a. Thus the result of
     above multiplication (Ey*Hxc)/(Eoy^2)
     = 1333*\sin(2599825*x/16551)^2/519323 is written
     here for definite intergration.
40
41 I = I * b;
     //since definite integral is independent of y.
     Hence dimension in y direction i.e,b can be taken
      out
42
43 I=real(I);
     //since from poyting formula [energyrate = (0.5*)
     real(I))*(Eoy^2)]. So we consider only real
     part of I.
44
45
46 Eoy=sqrt((energyrate*2)/I);
     // since ,energyrate =373= (0.5*(real(I))*(Eoy^2)
47
48 disp((Eoy/1000), 'the peak value of the electric
      field intensity in (KV/m)'); // display peak
     value of electric field. Divide by 1000 to obtain
      the
      electric field intensity in KV/m.
```

#### Scilab code Exa 4.2.1 TE10 Mode in Circular Waveguide

```
5 // (a) program_to_find_the_cut_off_frequency_(fc)
      _of_circular_waveguide_in_TE11_mode
6
7
8 \text{ radius} = 0.05
      //Given . Here radius_is_in_metres.
9 f = 3*(10^9);
      //operating_frequency_is_3_GHZ
10 uo=(4*(\%pi))*(10^-7); eo=8.85*(10^(-12));
      scientific_values_of_permeability_and_permittivity_in_free_space
11 \quad m=1
                              n=1;
                                                       //
      Given_that_a_TE11_mode_is_propagating.
12 X = 1.841;
      //For_TE11_mode_in_circular_waveguide_X= (kc*
      radius) = 1.841
13
14 kc=X/radius;
      //cut-off_wave_number
15 fc=kc/((2*%pi)*(sqrt(uo*eo)));
                                                      //
      since fc=kc/((2*\%pi)*(sqrt(uo*eo)));
16 disp(fc/(10<sup>9</sup>), 'cut-
      off_frequency_for_TE10_mode_in_GHZ=');
                       // display_cut -
      off_frequency_in_GHZ_by_dividing_by_(10^9)
      for_TE10_mode
17
18
19
20
21 // (b) program_to_find_the_guide_wavelength(lg)
```

```
_of_the_wave__at_operating_frequency_of_3GHZ
22
23
24 bg=sqrt((((2*\%pi*3*(10^9))^2)*(uo*eo)) - (kc^2));
           //bg_is_the_phase_constant_in_radian/metre,
      _{\rm bg=sqrt}((w^2)*(uo*eo))-(kc^2)); where w=2*\%pi*f
25 lginmetres=(2*%pi)/bg;
      Guide_wavelength_is_in_meters
  lgincm=100*lginmetres;
      Guide_wavelength_is_in_centimetres
27
  disp(lgincm,'
      Guide_wavelength_for_a_wave_at_a_frequency_of_3.5
      GHZ_{--}(cm) = '); //
      display_Guide_wavelength_for_TE10_mode
28
29
30
31 // (c)
      program_to_find_the_Guide_wavelength_in_the_wave_guide
32 \text{ zg} = (2*\%pi*(3*(10^9))*uo)/bg;
      Zg_is_the_characteristic_wave_impedence, Zg=(w*uo
      )/bg; where w=2*\%pi*f
33 disp(zg, 'wave_impedence_zg_in_the_wave_guide(ohm)=')
          //display_wave_impedence_in_the_wave_guide
```

#### Scilab code Exa 4.2.2 Wave Propagation in Circular Waveguide

```
1
2 //chapter-4
3 //Example-4-2-2 page no.-147
```

```
5 / program_to_find_all_the_TE(n,p)_and_TM(n,p)
      modes_for_which_energy_transmisssion_is_possible.
7 radius = .02;
     //Given. Here_radius_is_in_metres.
8 uo=(4*(\%pi))*(10^-7); eo=8.85*(10^(-12));
      scientific_values_of_permeability_and_permittivity_in_free_space
9 f = (10^10);
     //guide_is_operating_at_the_frequency_of_10GHZ
10 wc = (2*\%pi*f);
     //\sin ce, wc=(2*\%pi*f)
11 kc=wc*sqrt(uo*eo);
      //kc_is_cut-off_wave_number
12 X=kc*radius;
     //the product X=(kc*radius)
      for_a_given_mode_is_constant
13 disp(kc*radius, 'The_value_of_the_product X=(kc*
      radius) is = ');
      display_the_product_X = (kc*a)
14 disp('Any mode having a product (kc*radius) less
      than or equal to 4.18 will propagate the wave
     with a frequency of 10 GHZ . This is (kc*radius)&
      lt = 4.18');
15
16
17 syms i j
      // Defining_the_variables
18
19
20 p=[3.832 1.841 3.054 4.201 5.317 6.416;7.016 5.331
```

```
6.706 8.015 9.282 10.520 ; 10.173 8.536 9.969
      11.346 12.682 13.987] //represent_the_values_of
      X_for_
      different_modes_in_a_form_of_matrix.
      Where_columns_represent
      the \verb|-n-values-of-mode-and-rows-represent\_the \verb|-m-values-of-mode|
21
22 for i=1:1:3
      //value_of_i_traverse_across_the_rows
23 for j=1:1:6
      //value_of_j_traverse_across_the_columns
24 if(X >=p(i,j))
      // check_if_the_value_in(n,p)
      _matrix_is_less_than_or_equal_to_X
25 disp(p(i,j),i,j-1, 'TE mode(n,p)) and corresponding
      value of X=');
      display_TE_mode_for_which_value_in [(n,p)matrix]
     <= X and print
      corresponding_value_of_X
26 \, \text{end}
      //end if
27 end
      //end for
28 end
      //end for
29
30
31 \text{ m} = [2.405 \ 3.832 \ 5.136 \ 6.380 \ 7.588 \ ; \ 5.520 \ 7.106 \ 8.417
```

```
9.761 11.065 ;
                            represent_the_values_of_X_for_different_modes_in_a_form_of_matrix
                             . Where
                            columns\_represent\_the\_n\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_of\_mode\_and\_rows\_represent\_the\_m\_values\_the\_m\_the\_m\_the\_m\_the\_m\_the\_m\_the\_m\_the\_m\_the\_m\_the\_m
32
                    8.645 10.173 11.620 13.015 14.372]
33
34 for i=1:1:3
                            // value_of_i_traverse_across_the_rows_in [(n,p)]
                           matrix].
35 for j=1:1:5
                           //value_of_j_traverse_across_the_columns in [(n,p
                           matrix].
36 if(X >=m(i,j))
                            // check_if_the_value_in(n,p)
                            \_matrix\_is\_less\_than\_or\_equal\_to\_X
37 disp(m(i,j),i,j-1, TM mode(n,p)) and corresponding
                            value of X=');
                            display_TM_mode_for_which_value in [(n,p)matrix]
                           <= X and_print
                            corresponding_value_of_X.
38 end
                           //end if
39 end
                            //end for
40 end
                           //end for
```

#### Scilab code Exa 4.5.1 Directional Coupler

```
1
2
3 //Chapter -4
4 //EXAMPLE: 4-5-1 PAGE NO. 170
6 //(a)
      program_to_find_the_amount_of_the_power_delivered_in_the_load_Zl
8 \text{ PT4=8};
      //Given.
      Transmitted\_power\_to\_Bolometer\_1\_at\_port\_4
9 s = 2;
      //Given.VSWR_of_2.0_is_introduced_on_arm 4
      _by_Bolometer 1
10 r4=(s-1)/(s+1);
                                                   //
      reflection_coefficient_at_port 4(r4)
11 PR4=8/8;
      (r4^2)=PR4/PI4=PR4/(PR4+PT4)=PR4/PR4+8=1/9 =>
        8PR4 = 8
12 \text{ PI4=PT4} + \text{PR4};
                                                    //PI4 =
      power_incident_at_port_4 ;PT4=
      power_transmitted_at_port 4; PR4=
      power_reflected_at_port 4
13 \operatorname{disp}(PI4, 'power_incident_at_the_port_4_is_(mW)=');
14 disp(PR4, 'power_reflected_from_the_port 4_is_(mW) ='
      );
```

```
15
16 disp('Since port 3 is matched and the Bolometer at
      port 3 reads 2mw, then 1 mw must be radiated
      through the holes . Since 20 dB is equivalent to a
       power of 100:1, the power input at port 1 is
      given by=');
17
18 PI2=100*PI4;
      // \operatorname{attenuation} = 20 = 10 * \log (PII/PI4)
19 \operatorname{disp}(PI2, 'power_input_at_port_2_is_given_by_(mW)=');
20
21 PR2 = 100 * PR4;
      // attenuation = 20 = 10 * log (PR2/PR4)
  disp(PR2,'
      power_reflected_from_the_load_at_port_2_is_given_by_
      (mW) = ');
23
24 PT2=PI2-PR2;
      //transmitted power = incident power - reflected
      power
25 disp(PT2, '
      power_dissipated_in_the_load_at_port_2_is_given_by_
      (mW) = ');
26
27
28
29
  //(b) Program_to_find_the_VSWR_on arm 2
30
31
32 \text{ r=sqrt}(PR2/PI2);
      //reflection_coefficient_at_port 2
33 s=(1+r)/(1-r);
      //VSWR ON ARM 2
```

#### Scilab code Exa 4.5.2 Operation Of a Balanced Amplifier

```
2 / \cosh \text{er} - 4
3 / \text{Example } 4-5-2
                     page no. 174
5 //(a) Program_to_find_out_the_input_and_output_VSWRs.
7 s11=0;
      //for_balanced_amplifier s11=0
8 s = (1+s11)/(1-s11);
                                                              //
      Input_VSWR
9 disp(s, 'input vswr=');
10
11 	 s22=0;
      //for_balanced_amplifier s22=0
12 s=(1+s22)/(1-s22);
                                                              //
      output_VSWR
   disp(s, 'output vswr=');
13
14
15
16
  //(b) Program_to_find_out_the_output_power_in_watts
17
18
19 P0 = 200 * 10 * 2;
      //output_power (PO) = [powerinput] * [
      {\tt power\_gain\_of\_each\_GaAs\_chip} \ ] * [ \ n \ ] \qquad , here \ \ n{=}2
20 disp(PO/1000, 'Output_POWER_in_Watts');
```

```
display_power_in_watts_by_dividing_by_1000

21
22
23
24 //(C)Program to find out the linear output power gain in db

25
26 GAIN=10*log10(2);

BECAUSE_TWO_CHIPS_ARE_IN_PARALLEL. Gain=(power gain of each GaAs chip)*log(n),n=2.

27 disp(GAIN, 'Linear_output_power_gain_in_db=');

// display_linear_output_power_gain_in_db
```

# microwave transistors and tunnel diodes

Scilab code Exa 5.1.1 Elements of Hybrid Pi Common Emitter Circuit

```
//CHAPTER NO.-5
//Example No.5-1-1 , Page No.-195
//(a) Program_to_find_the_mutual_inductance_gm.

ic=6*(10^-3); //Collector_Current
vt=26*(10^-3); //vt=26
mV_at_300k_is_the_voltage_equivalent_of_temperature

gm=ic/vt; //the_mutual_inductance_is gm=(ic/vt)
disp(gm,'the_mutual_inductance_is gm(in mho)=');
//(b)
Program_to_find_the_input_inductance_gb_and_resistance_R

hfe=120; //hfe= common-emitter_current_gain_factor
```

```
16 gb=gm/hfe;//input_inductance
17 R=1/gb; //Resistance
18
19 disp(gb, 'input_inductance gb(in mho)=');
20 disp(R, 'input_resistance R (in ohms)=');
21
22 //(c)
      Program_to_find_the_electron_diffusion_coefficient_Dn
23
24 un=1600; //electron_Mobility
25 Dn=un*vt; // Dn=un*kt/q=un*26*(10^--3);
26
  disp(Dn, 'electron_diffusion_coefficient_Dn(in cm2/s)
     = ^{\prime} );
28
29 //(d) Program_to_find_the_diffusion_capacitance_Cbe
30 Wb=(10^-8); //cross_sectional_area
31 Cbe=(gm*(Wb^2))/(2*Dn*(10^-7));
32 \text{ Cbe=Cbe/(10^-12)};
33 disp(Cbe, 'diffusion_capacitance_Cbe(in pF)=');
```

#### Scilab code Exa 5.1.2 I V Characteristics of n p n transistor

```
//CHAPTER NO.-5
//Example No.5-1-2 , Page No.-203

//(a)
Program_to_find_the_impurity_desities_in_the_emitter
, base_and_collector_regions

disp('the impurity densities (in cm-3) are read from
Fig A-1 in the Appendix A as NdE=1*(10^19)[the
impurity density in the n-type emitter region],
```

```
NaB=1.5*(10^17) [the impurity density in the p-
      type base region, NdC=3*(10^14) [the impurity
      density in the n-type collector region]');
8 NdE=1*(10^19);
9 NaB=1.5*(10^17);
10 NdC = 3*(10^14);
11
12 //(b) Program_to_find_the_mobilities_in_the_emitter,
      base and collector_regions
13 disp('the mobilities (in cm2/v*s) are read from fig A
      -2 in the Appendix A as upe=80 mobility in the
      emitter] , unE=105[mobility in the emitter] , upB
      =400[mobility in the base], unC=1600[mobility in
       the collector ]');
14 upE=80;
15 unE=105;
16 \text{ upB} = 400;
17 unC=1600;
18
19 //(c)
      Program_to_find_the_diffusion_lengths_in_the_emitter
      , base and collector_regions
20 disp('the_diffusion_constants_are_computed_to_be');
21 Vt = 26 * (10^-3);
22
23 DpE=upE*Vt;
24 \quad DnE=unE*Vt;
25 \text{ DpB=upB*Vt};
26 \quad DnC=unC*Vt;
27 disp(DpE, 'DpE=');
28 disp(DnE, 'DnE=');
29 disp(DpB, 'DpB=');
30 disp(DnC, 'DnC=');
31
32 //(d) Program_to_compute_the_equilibrium_densities_in
       the emitter, base and_collector_regions
33
34 disp('the_equlibrium_densities_are');
```

```
35 \text{ ni} = 1.5*(10^10);
36
37 \text{ pEo}=(\text{ni}^2)/\text{NdE};
38 \text{ npB}=(\text{ni}^2)/\text{NaB};
39 \text{ pCo}=(\text{ni}^2)/\text{NdC};
40 disp(npB, 'npB=');
41 disp(pEo, pEo=');
42 disp(pCo, 'pCo=');
43
44 //(e) Program_to_compute_the_terminal_currents
45
46 disp('the_terminal_currents_are_computed_as follows.
       From Eq 5-1-39,
      the_electron_current_in_the_emitter_is ');
47 A = 2*(10^-2); // cross - section_area
48 q=1.6*(10^-19);
49 W = (10^-5); //base_width
50 Le=(10^-4); // Diffusion_length_in_emitter
51 Ve=.5; // Emitter_junction_voltage
52 \text{ InE}=-(A*q*DnE*(ni^2)*exp(Ve/Vt))/(NaB*W); //Ine=-(Aq*)
      Dp*(ni^2)*(exp(Ve/Vt)-1))/(Le*Nd);
53 InE = InE / (10^-3);
54 disp(InE, 'the_electron_current_in_the_emitter_is(in
      mA) ');
55
56 disp ('From Eq5-1-42,
      _the_hole_current_in_the_emitter_is ');
57 IpE=(A*q*DpE*(ni^2)*(exp(Ve/Vt)-1))/(Le*NdE); //Ipe=(
      A*q*De*peo*(exp(Ve/Vt)-1))/Le = (A*q*Dp*(ni^2))
      *(\exp(Ve/Vt)-1))/(Le*Nd)
58 \text{ IpE=IpE}/(10^{-6});
59 disp(IpE, 'the_electron_current_in_the_emitter_is(in
      uA)');
60
61
62
63 disp('From Eq-5-1-24,
      the_reverse_saturation_current_in_the_collector_is
```

```
');
64 ICo=-(A*q*DnE*(ni^2)/(NaB*W))-(A*q*DpE*pEo)/Le;
65 ICo=ICo/(10^-12);
66 disp(ICo, 'the_electron_current_in_the_emitter_is(in
     pA)');
67
68
69 disp('From Eq-5-1-40,
      _the_electron_current_which_reaches_the_collector
      is ');
70 InC=-(A*q*DnE*(ni^2)*\exp(Ve/Vt)/(NaB*W));
71 InC=InC/(10^-3);
72 disp(InC, '
      the_electron_current_which_reaches_the_collector_is
      (in mA);
73
74 IE=(-IpE*(10^-6))+(InE*(10^-3));
75 IE=IE/(10^-3);
76 disp(IE, 'the_emitter_current_is (in mA)');
77
78 IC=(-ICo*(10^-12))-(InC*(10^-3));
79 IC=IC/(10^-3);
80 disp(IC, 'the_collector_current_is (in mA)');
81
82 IB=(IpE*(10^-6))-[((InE*(10^-3)))-(InC*(10^-3))]+(
     ICo*(10^-12));
83 IB=IB/(10^-6);
84 disp(IB, 'the_current_in_the_base_terminal_is_(in uA)
85
86 disp('NOTE: The_recombination -
      generation_currents_in_the_spcae -
     charge_regions_are_not_counted;);
```

Scilab code Exa 5.1.3 Silicon Bipolar Transistor

```
1
  //CHAPTER NO. -5
  //Example No.5-1-3, Page No.-206
  //(a) Program_to_find_the_mobilities_un_and_up
    disp('the mobilities (in cm2/v.s ) are read from Fig-
7
      A-2 in Appendix A as un=200 for NdE=5*(10^18) cm
      -3 and up=500 for Na=5*(10^16) cm-3');
8
     un = 200;
     up = 500;
9
10
11
     //(b)
        Program_to_find_the_diffusion_coefficients_Dn_and_Dp
     Vt = 26*(10^-3); //Vt = kt/q
12
     Dn=un*Vt;
13
     Dp=up*Vt;
14
15
     disp(Dn, 'diffusion_coefficient_are_Dn(in cm2/s)=')
16
     disp(Dp, 'and_{-}Dp(in cm2/s)=');
17
18
19 //(c)
      Program_to_find_the_emitter_efficiency_factor_y
20 W = (10^-3); //Base_width
21 Le=(10^-2); //Emitter_Length
22 Na=5*(10^16); // Acceptor_density_in_base_region
23 Nd=5*(10^18);//Donor_density_in_emitter_region
y=1/(1+((Dp*Na*W)/(Dn*Nd*Le)));
25
26 disp(y, 'emitter_efficiency_factor_y=');
27
28
  //(d) Program_to_find_the_transport_factor_B
29
30
31 t=10^-6; //hole_lifetime
32 B=1-(W^2)/(2*Dn*t); //transport_factor
```

```
33
34 disp(B, 'the transport factor B=');
35
36
37 //(e) Program_to_find_the_current_gain_a
38
39 a=B*y;
40
41 disp(a, 'the current_gain a=');
```

#### Scilab code Exa 5.1.4 Power Frequency Limitation

```
1
                //CHAPTER NO. -5
               //Example No.5-1-4, Page No. -211
   4
                                    Program\_to\_determine\_the\_maximum\_allowable\_power\_that\_the\_transistic and the properties of the prope
    6
                              Xc=1; // Reactance
    8
                               ft=4*(10^9); // Transit_cut-off_frequency
                              Em=1.6*(10^5); // maximum_electric_field
    9
10
                              Vx=4*(10^5); // saturation_drift_velocity
11
                              Pm = (((Em * Vx/(2*\%pi)))^2)/(Xc*(ft^2));
12
13
                         disp(Pm, 'the_maximum _allowable_power(in W)
                                            _that_the_transisitor_can_carry_is ');
```

#### Scilab code Exa 5.2.1 Heterojunction Bipolar Transistor

```
1 2 //CHAPTER NO. -5
```

```
3 //Example No.5-2-1 , Page No.-213
5 //(a)
      Program_to_determine_the_latice_match_present_in_percent
     disp('the_latice_match_present_is_within 1%');
6
7
     //(b) Program_to_find_the_conduction -
8
        band\_differential\_between\_Ge\_and\_GeAs
9
     X1=4; //electron_affinity
     X2=4.07; // electron_affinity
10
11
     AE = X1 - X2;
12 disp(AE, 'the_conduction-band differential_is (in eV)
     = ');
13
  //(c) Program_to_find_the_valence-
      band\_differential\_between\_Ge\_and\_GeA
      Eg2=1.43; //energy_gap
15
    Eg1 = .8; //energy_gap
16
17
     Ev = Eg2 - Eg1 - AE
18 disp(Ev, 'the valence-band differential is (in eV) = ')
```

#### Scilab code Exa 5.2.2 n Ge p GaAs n GaAs HBT

```
1
2 //CHAPTER NO.-5
3 //Example No.5-2-2 , Page No.-215
4
5 //(a) Program_to_compute_the_built-in voltage_in_the
    p-GaAs_side
6 Na=6*(10^16); //Acceptor_density_in_p-GaAs_side
7 w02=-26*(10^-3)*log(Na/(1.8*(10^6)));
8 disp(w02, 'the_built-in_voltage(in V) in_the p-
    GaAs_side');
```

```
9
    //(b) Program_to_compute_the_hole_mobility
10
11
    disp('The hole mobility is read from Fig -A-2 in
12
       Appendix A as up=400(cm2/v.s)');
13
    up = 400;
14
    //(c)
15
       Program_to_compute_the_hole_diffusion_constant
    Dp = up * 26 * (10^{-3});
16
17
18
    disp(Dp, 'The_hole_diffusion_constant_is Dp(cm2/s)='
       );
19
20
     //(d) Program_to_compute_the_minority_hole_density
21
         in n-Ge
22
23
     ni=1.5*(10^10);
     Nd=5*(10^18); // Donor_density_in_n-Ge_region
24
25
     pno=(ni^2)/Nd;
      disp(pno, 'the_minority_hole density (cm-3)in_n-
26
         Ge_is = ');
27
        //(e)
28
           Program_to_compute_the_minority_electron_density_in_p
           -GaAs_region
     Na=6*(10^16);
29
    npo=((1.8*10^6)^2)/Na;
30
      disp(npo, 'the_minority_electron_density(in cm-3)
31
         \lim_{p \to G} aAs_{region_is} = ');
32
33
      //(e)
34
         Program_to_compute_the_hole_diffusion_length
      tp=6*(10^-6); //hole_lifetime
35
36
      Lp=sqrt(tp*Dp);
      disp(Lp, 'the_hole_diffusion_length(in cm) is =');
37
```

```
38
      //(e) Program_to_compute_the_emitter-
39
         junction_current
40
      A=2*(10^-2);//cross_section
41
      VE=1; // bias_voltage_at_emitter_junction
42
      q=1.6*(10^-19);
43
      1=VE/(26*(10^-3));
44
      I=(A*q*Dp*pno*(exp(1)-1))/(Lp);
45
      disp(I, 'the_emitter-junction_current(in A) is =');
46
```

# microwave field effect transistors

Scilab code Exa 6.1.1 Pinch Off Voltage Of a Silicon JFET

```
1
2  //chapter_no.-6, page_no.-229
3  //Example_no.6-1-1
4
5  clc;
6  a=.1*(10^-6);//channel_height
7  Nd=8*(10^23);//Electron_Concetration
8  er=11.80;//relative_dielectrin_constant
9  e=8.854*(10^-12)*er;//medium_dielecric_constant
10  q=1.6*(10^-19);//electronic_charge
11  Vp=(q*Nd*(a^2))/(2*e);//pinch-off_voltage
12
13  disp(Vp, 'pinch-off_voltage in(Volts)is');
```

Scilab code Exa 6.1.2 current of a JFET

```
1
\frac{2}{\cosh 2} // chapter_no. -6, page_no. -233
3 / \text{Example_no.} 6-1-2
5 clc;
7 //(a) Calculate_the_pinch-off_Voltage_in_Volts
8 a=.2*(10^-4); // channel_height
9 Nd=1*(10^17); // Electron_Concetration
10 er=11.80; //relative_dielectrin_constant
11 e=8.854*(10^-14)*er;//medium_dielecric_constant
12 q=1.6*(10^-19); // electronic_charge
13 Vp = (q*Nd*(a^2))/(2*e); //pinch-off_voltage
14
15 disp(Vp, 'pinch-off volatge in(Volts) is');
16
17
  //(b) Calculate_the_pinch-off_current
18
19
20 un=800; // electron_mobility
21 L=8*(10^--4); // channel_length
Z=50*(10^-4); // channel_width
23 a=.2*(10^-4); //channel_height
24 Nd=1*(10^17); // Electron_Concetration
25 er=11.80; //relative_dielectrin_constant
26 e=8.854*(10^-14)*er;//medium_dielecric_constant
27 q=1.6*(10^-19); // electronic_charge
28 Ip=(un*(q^2)*(Nd^2)*Z*(a^3))/(L*e);//pinch-
      off_voltage
29 Ip=Ip*1000;
30 disp(Ip, 'pinch-off current in (mA) is');
31
32
33 //(c) Calculate_the_built -in_voltage
34
35 Nd=1*(10^17); // Electron_Concetration
36 Na=1*(10^19); // hole_density
37 \text{ w0} = 26*(10^{-3})*\log((Nd*Na)/((1.5*10^{10})^2));
```

```
38 disp(w0, 'built-in voltage in(volts) is');
39
40
41
42 //(d) Calculate_the_drain_current
43
44 Vd=10; //drain_voltage
45 Vg = -1.5; //gate_voltage
46 Vg=-1*Vg; //we_take_only_magnitude
47 x=((Vd+Vg+w0)/(Vp))^(3/2);
48 x = (2/3) * x;
49 y=((Vg+w0)/(Vp))^{(3/2)};
50 y = (2/3) * y;
51 Id=(Vd/Vp)-x+y;
52 \text{ Id=Ip*Id};
53 disp(Id, 'the_drain_current (mA) is');
54
55
56
57 //(e) Calculate_the_saturation_drain_current_at Vg=0
58
Vg = -1.5; //gate_voltage
60 Vg=-1*Vg; //we_take_only_magnitude
61 x = (Vg + w0) / (Vp);
62 y = ((Vg + w0)/(Vp))^{(3/2)};
63 y = (2/3) * y;
64 Idsat = (1/3) - x + y;
65 Idsat=(Id)*Idsat;
66 disp(Idsat, 'the_saturation_drain_current_(mA) is');
67
68
69 //(f) Calculate_the_cut-off_frequency
70
71 fc=(2*un*q*Nd*(a^2))/(%pi*e*(L^2));
72 disp(fc/(10^9), 'the_cut-off_frequency(Ghz)');
```

#### Scilab code Exa 6.2.1 Pinch Off Voltage Of a MESFET

```
//CAPTION: Pinch-Off_Voltage_Of_a_MESFET
//chapter_no.-6, page_no.-239
//Example_no.6-2-1

clc;
a=.1*(10^-6);//channel_height
Nd=8*(10^23);//Electron_Concetration
er=13.10;//relative_dielectrin_constant
e=8.854*(10^-12)*er;//medium_dielecric_constant
q=1.6*(10^-19);//electronic_charge
Vp=(q*Nd*(a^2))/(2*e);//pinch-off_voltage

disp(Vp,'pinch-off_voltage in(Volts)is');
```

#### Scilab code Exa 6.2.2 Current Voltage Characteristics Of a GaAs MESFET

```
1
2 //chapter_no.-6, page_no.-244
3 //Example_no.6-2-2
4
5 clc;
6
7
8 //(a) Calculate_the_pinch-off_voltage
9
10 a=.1*(10^-6);//channel_height
11 Nd=8*(10^23);//Electron_Concetration
12 er=13.1;//relative_dielectrin_constant
13 e=8.854*(10^-12)*er;//medium_dielecric_constant
```

```
14 q=1.6*(10^-19); // electronic_charge
15 Vp = (q*Nd*(a^2))/(2*e); //pinch-off_voltage
16
17 disp(Vp, 'pinch-off volatge in(Volts) is');
18
19
20
21 //(b) Calculate_the_velocity_ratio
22
23 un=.08; //electron_mobility
24 \text{ vs} = 2*(10^5);
25 L=14*(10^-6);
26 n = (Vp*un)/(vs*L)
27 disp(n, 'the velocity ratio');
28
29
30 //(c) Calculate_the_saturation_drain_current_at Vg=0
31
32 L=14*(10^-6);
33 Z=36*(10^-6);
34 Ipsat = (q*Nd*un*a*Z*Vp)/(3*L);
35 Ipsat=Ipsat*1000;
36 disp(Ipsat, 'the_saturation_drain_current_(mA) is');
37
38
39
40 //(d) Calculate_the_drain_current
41
42 \text{ Vd=5};
43 \text{ Vg=2};
44 u = ((Vd+Vg)/Vp)^(1/2);
45 p=((Vg)/Vp)^(1/2);
46 Id=(3*((u^2)-(p^2))-2*((u^3)-(p^3)))/(1+(n*((u^2)-(p^2))))
      ^2))));
47
48 Id=Id*Ipsat;
49 disp(Id, 'the_drain_current_(mA) is');
```

#### Scilab code Exa 6.2.3 CutOff frequency of a MESFET

```
1
 2
 3 / \cosh \operatorname{pter_no.} -6, \operatorname{page_no.} -247
4 / \text{Example_no.6} - 2 - 3
6 clc;
   //(a) Calculate_the_cut-off_frequency
10 gm = .05;
11 Cgs = .60*(10^-12);
12
13 fco=(gm)/(2*\%pi*Cgs);
14 fco=fco/(10<sup>9</sup>);
15
16 disp(fco, 'the_cut-off_frequency(in Ghz)is');
17
   //(b) Calculate_the_maximum_operating_frequency
18
19
20
21 \text{ Rd} = 450;
22 \text{ Rs} = 2.5;
23 Rg=3;
24 \text{ Ri} = 2.5;
25
26 fmax=(fco/2)*((Rd/(Rs+Rg+Ri))^(1/2));
27
28 disp(fmax, 'the_maximum_operating_frequency(in Ghz) is
       <sup>'</sup>);
```

#### Scilab code Exa 6.3.1 Current of a HEMT

```
1
2  // chapter_no.-6, page_no.-251
3  // Example_no.6-3-1
4  clc;
5
6  // Calculate_the_Drain_Current
7
8  q=1.60*(10^-19);
9  n=5.21*(10^15);
10  W=150*(10^-6);
11  v=2*(10^5);
12
13  Ids=q*n*W*v;
14  Ids=1000*Ids;
15  disp(Ids, 'the_drain_current_is(mA)');
```

#### Scilab code Exa 6.3.2 Sensitivity Of HEMT

```
15
16  //(b)    Calculate_the_sesitivity_of_the_HEMT
17
18    q=1.6*(10^-19);
19    Nd=2*(10^24);
20    wms=.8;
21    Vth=.13;
22    er=4.43;
23    e=er*(8.854*(10^-12));
24    S=-[(2*q*Nd*(wms-AEc-Vth))/(e)]^(1/2);//
        sesitivity_of_the_HEMT
25    S=S/(10^6);
26    disp(S, 'the_sensitivity_of_the_HEMT_(mV/nm)_is=')
27    disp(-1*S, 'd/dv(Vth)(mV/nm) is=');
```

#### Scilab code Exa 6.4.1 Threshold Voltage of an Ideal MOSFET

```
1 / chapter_no.-6, page_no.-260
2 / \text{Example_no.6} - 4 - 1
3 clc;
4
5
6 //(a) Calculate_the_strong_potential_w(inv)
      _for_strong_inversion
8 \text{ kt} = 26*(10^-3);
9 Na=3*(10^17);
10 Ni=1.5*(10^10);
11 wsinv=2*kt*log(Na/Ni);
12 disp(wsinv, 'the_strong_potential_w(inv)
      _for_strong_inversion(volts)');
13
14 //(b) Calculate_the_insulator_Capacitance
15
16 \text{ eir}=4;
```

```
17  ei=8.854*(10^-12)*eir;
18  d=.01*(10^-6);
19  Ci=ei/d;
20  Ci=Ci*(1000);
21  disp(Ci,'the_insulator_Capacitance(mF/m^2)=');
22
23  //(c)  Calculate_the_threshold_voltage
24
25  q=1.6*(10^-19);
26  Na=3*(10^23);
27  er=11.8;
28  e=8.854*er*(10^-12);
29  Vth=wsinv+((2/(Ci*(10^-3)))*((e*q*Na*.437)^(1/2)))
30  disp(Vth,'the_threshold_voltageis () Volts=');
```

#### Scilab code Exa 6.4.2 Characteristics Of a MOSFET

```
1
2 //chapter_no.-6, page_no.-262
3 //Example_no.6-4-2
4 clc;
5
6
7 //(a) Calculate_the_insulation_capacitance
8
9 eir=3.9;
10 ei=8.854*(10^-12)*eir;
11 d=.05*(10^-6);
12 Ci=ei/d;
13 disp(Ci, 'the_insulation_capacitance(in F/m^2)');
14
15 //(b) Calculate_the_saturation_drain_current
16
17 Z=12*(10^-12);
18 Vg=5;
```

```
19 Vth=.10;
20 \text{ vs}=1.70*(10^7);
21 Idsat=Z*Ci*(Vg-Vth)*vs;
22 Idsat=Idsat*10^7;
23 disp(Idsat, 'the_saturation_drain_current(in mA)');
24
25 //(c)
      Calculate\_the\_transconductance\_in\_the\_saturation
      region
26
27
Z = 12 * (10^{-12});
29 \text{ vs}=1.70*(10^7);
30 gmsat=Z*Ci*vs;
31 gmsat=gmsat*10^7;
32 disp(gmsat, 'the_transconductance_in_the_saturation
      region (in_millimhos)');
33
34
35
36 // (d)
      Calculate_the_maximum_operating_frequency_in_the_saturation_region
37
38 \text{ vs}=1.70*(10^7);
39 L=4*(10^-6);
40 fm=vs/(2*\%pi*L);
41 fm=fm/(10^2);
42 \text{ fm=fm/(10^9)};
43 disp(fm, '
      the_maximum_operating_frequency_in_the_saturation_region
      (in GHz)');
```

Scilab code Exa 6.6.1 Power Dissipation of a Three Phase CCD

```
1
2
3  // chapter_no.-6, page_no.-278
4  // Example_no.6-6-1
5  clc;
6
7
8  // Calculate_the_power_dissipation_per_bit
9  n=3;
10  f=10*(10^6);
11  V=10;
12  Qmax=.04*(10^-12);
13  P=n*f*V*Qmax;
14  P=P*(10^6);
15  disp(P, 'the_power_dissipation_per_bit (uW) is=');
```

Scilab code Exa 6.6.2 Design of N Type Three Phase Surface Channel CCD

```
1
2 //chapter_no.-6, page_no.-279
3 //Example_no.6-6-2
4
5 clc;
6
7
8 //(a) Calculate_the_insulator_capacitance
9
10 eir=3.9;
11 ei=8.854*(10^-12)*eir;
12 d=.15*(10^-6);
13 Ci=ei/d;
14 Ci=Ci*(10^5);
15 disp(Ci,'the_insulation_capacitance(in nF/cm^2)');
16
17 //(b) Calculate_the_maximum_stored_charges_per_well
```

```
18
19 Nmax = 2*(10^12);
20 q=1.6*(10^-19);
21 A = .5*(10^-4);
22 Qmax = Nmax * A * q;
23 Qmax = Qmax * (10^12);
24 disp(Qmax, 'the_maximum_stored_charges_per_well(
      picocoulombs)');
25
26 //(c) Calculate_the_required_applied_gate_voltage
27
28 \text{ Nmax} = 2*(10^12);
29 q=1.6*(10^-19);
30 Vg = (Nmax*q)/(Ci*10^-9);
31 disp(Vg, 'the_required_applied_gate_voltage(in_Volts)
      <sup>'</sup>);
32
33
34
35 //(d) Calculate_the_clock_frequency
36
37 P = .67 * (10^-3);
38 n = 3;
39 f=P/(n*Vg*Qmax*(10^-12));
40 f = f/(10^6);
41 disp(f, 'the_clock_frequency(in MHz)');
```

## transferred electron devices

Scilab code Exa 7.2.1 Conductivity of an n Type GaAs Gunn Diode

Scilab code Exa 7.2.2 Charactristics of a GaAs Gunn Diode

```
1
\frac{2}{\cosh 2} / \cosh 2 \sin \theta - 7, page_no.-298
3 / \text{Example_no.} 7 - 2 - 2
4 clc;
5
6 //(a) Calculate_the_electron_drift_velocity
7 q=1.6*(10^-19);
8 f=10*(10^9);//operating\_frequency
9 L=10*(10^-6); // Device_Length
10 vd=f*L;
11 disp(vd, 'the_electron_drift_velocity(in m/sec) is =')
12 vd=vd*100;
13 disp(vd, 'the_electron_drift_velocity(in cm/sec) is ='
      );
14 vd=vd/100;
15
16 //(b) Calculate_the_current_density
17
18 n=2*(10^14)*(10^6);
19 J=q*n*vd;
20 \operatorname{disp}(J, 'the_electron_drift(n A/m^2) is =');
21 J=J/(10^4);
22 disp(J, 'the_electron_drift(n A/cm^2) is =');
23
24
25 //(c)CAPTION:
      Calculate_the_negative_electron_mobility
26
27 E=3200; // applied_field
28 \text{ vd=vd*(100)};
29 un = -1*(vd/E);
30 disp(un, 'negative_electron_mobility(in cm^2/V*sec) is
       = ');
```

#### Scilab code Exa 7.3.1 Criterion of Mode Operation

```
1
\frac{2}{\cosh pter_no.-7}, page_no.-298
3 / \text{Example_no.} 7-2-2
4 clc;
5
6 //(a) Calculate_the_electron_drift_velocity
7 q=1.6*(10^-19);
8 f=10*(10^9);//operating_frequency
9 L=10*(10^-6);//Device_Length
10 vd=f*L;
11 disp(vd, 'the_electron_drift_velocity(in m/sec) is =')
12 \text{ vd} = \text{vd} * 100;
13 disp(vd, 'the_electron_drift_velocity(in cm/sec) is ='
      );
14 vd=vd/100;
15
16 //(b) Calculate_the_current_density
17
18 n=2*(10^14)*(10^6);
19 J=q*n*vd;
20 disp(J, 'the_electron_drift(n A/m^2) is =');
21 J=J/(10^4);
22 disp(J, 'the_electron_drift(n A/cm^2) is =');
23
24
25 //(c)CAPTION:
      Calculate_the_negative_electron_mobility
26
27 E=3200; //applied_field
28 \text{ vd=vd*}(100);
29 un=-1*(vd/E);
30 disp(un, 'negative_electron_mobility(in cm^2/V*sec) is
       = ');
```

#### Scilab code Exa 7.4.1 Output power of an LSA Oscillator

```
2 / \text{chapter_no.} -7, \text{page_no.} -311
3 / \text{Example_no.} 7 - 4 - 1
4
5 clc;
7 // Calculate_the_output_power
8 n=.06; //conversion_efficiency
9 M=3.5; // Multiplication_factor
10 Eth=320*(10^3);//threshold_field
11 L=12*(10^-6);//Device_Length
12 n0=10^21; // Donor_concentration
13 e=1.6*(10^-19);
14 v0=1.5*(10^5); // Average_carrier_velocity
15 A=3*(10^-8); //Area
16 P=n*(M*Eth*L)*(n0*e*v0*A);
17 P=P*1000;
18 disp(P, 'the_output_power(in mW) is =');
```

## Avalanche transit time Devices

Scilab code Exa 8.2.1 CW Output Power Of an IMPATT Diode

```
2 / chapter_no. -8, page_no. -331
3 / \text{Example_no.8} - 2 - 1
5 clc;
7 //(a) Calculate_the_maximum_CW_power
9 n=.15; //efficiency
10 Vomax=100; // maximum_operating_voltage
11 Iomax = 200 * (10^-3); // maximum_operating_current
12 Pdc=Vomax*Iomax;
13 P=n*Pdc;
14 disp(P, 'the_maximum_CW_power(in Watts) is =');
15
16 //(b) Calculate_the_resonant_frequency
17
18 L=6*(10^-6); // drift - region_L ength
19 vd=2*(10^5); // carrier_drift_velocity
20 f = vd/(2*L);
21 f=f/(10^9);
```

```
22 disp(f, 'the_resonant_frequency(in GHz) is =');
```

#### Scilab code Exa 8.3.1 Calculate the avalanche zone velocity

```
1
2 //chapter_no.-8, page_no.-334
3 //Example_no.8-3-1
4
5 clc;
6 J=20*(10^3);//current_density
7 q=1.6*(10^-19);
8 NA=2*(10^15);//Doping_Concentration
9 vs=J/(q*NA);
10 disp(vs, 'avalanche-zone_velocity(in cm/s)is =');
11
12 disp('This means that the avalanch-zone velocity is much larger than the scattering-limited velocity');
```

#### Scilab code Exa 8.4.1 Breakdown voltage Of a BARITT Diode

```
1
2  //chapter_no.-8, page_no.-338
3  //Example_no.8-4-1
4
5  clc;
6
7  //(a)  Calculate_the_break_down_voltage
8  q=1.6*(10^-19);
9  N=2.8*(10^21); // Donor_Concentration
10  L=6*(10^-6); // silicon_length
11  er=11.8; // Relative_dielectric_constant
12  es=8.854*(10^-12)*er;
```

#### Scilab code Exa 8.5.1 UP Converter parametric Amplifier

```
1
2 / chapter_no. -8, page_no. -346
3 / \text{Example_no.8} - 5 - 1
4 clc;
5
6 //(a) Calculate_the_power_gain
7 R=25; //R=f0/fs,
      ratio_of_output_frequency_over_signal_frequency
8 rQ=10; // figure_of_merit
9 x = ((rQ)^2)/R;
10 PG=(R*x)/((1+sqrt(1+x))^2);
11 PG=10*log10(PG);//calculating_in_dB
12 disp(PG, 'Up-converter_power_gain_(in dB) is =');
13
14 //(b) Calculate_the_noise_figure
15
16 Td=350; // Diode_temperature
17 To=300; //ambient_Temperature
```

```
18 F=1+(((2*Td)/To)*((1/rQ)+(1/rQ^2)));
19 F=10*log10(F);//calculating_in_dB
20 disp(F, 'the_noise_figure(in dB) is =');
21
22
23 //(c) Calculate_the_band_width
24
25 r=.4//factor_of_merit_figure
26 BW=2*r*sqrt(R); //R=fo/fs
27 disp(BW, 'the_band_width_is =');
```

# microwave linear beam tubes O type

#### Scilab code Exa 9.2.1 Klystron Amplifier

```
15 f = (3*(10^9));
d=1*(10^-3); // Gap\_spacing\_in\_either\_cavity
17 w = (2 * \%pi * f);
18 Og = (w*d)/v0;
19 disp(Og, 'The_gap_transit_angle_(in radian) is =');
20 disp('The_beam-coupling_coefficient_is');
21 Bi = sin(0g/2)/(0g/2);
22 Bo=Bi;
23 disp(Bi, '');
24 disp('The_dc_transit_angle_(in radian)
      _between_the_cavities_is =');
25 L=4*(10^-2); // Spacing_between_the_two_cavities
26 \quad 00 = (w*L)/v0;
27 disp(00, '');
28 disp('The_maximum_input_voltage_V1_(in Volts)
      -is_{then_given_by} = ');
29 V1max = (2*V0*X)/(Bi*00);
30 disp(V1max,'');
31
32
33
34
35 //(b) Calculate_the_voltage_gain
36
37 R0 = 40 * (10^3);
38 \text{ Rsh} = 30*(10^3); //
      Effective_shunt_impedance_excluding_beam_loading
39
40 Av = ((Bo^2)*00*J1(X)*Rsh)/(R0*X);
41 disp(Av, 'The_voltage_gain_is_found,
      neglecting_the_beam_loading_in_the_output_cavity
      = ');
42
43
44
45
46 //(c) Calculate_the_efficiency_of the _amplifier
47
```

```
48 \quad I0 = 25 * (10^{-3});
49 I2=2*I0*J1(X);
50 V2=Bo*I2*Rsh;
51 efficiency=(Bo*I2*V2)/(2*I0*V0);
52 efficiency=100*efficiency;
53 disp(efficiency, 'the_efficiency_of the _amplifier,
                         neglecting_beam_loading =');
54
55
          //(d) Calculate_the_beam_loading_conductance
56
57
58 G0 = 25*(10^-6);
59 \text{ Og} = (\text{Og} * 180) / \% \text{pi};
60 GB = (GO/2) * ((Bo^2) - (Bo*cos((28.6*\%pi)/180)));
61 disp(GB, 'the_beam_loading_conductance GB (mho) is =')
62
63 RB=1/GB;
64 disp(RB, 'then_the_beam_loading_resistance_RB (rho) is
65 disp('
                         In\_comparasion\_with\_RL\_and\_Rsho\_or\_the\_effective\_shunt\_resistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistance\_thesistanc
                         the_beam_loading_resistance_is_like_an_open_circuit_and_thus_can_l
                              neglected_in_the_preceding_calculations');
```

#### Scilab code Exa 9.3.1 Four Cavity Klystron

```
1
2 //chapter_no.-9, page_no.-385
3 //Example_no.9-3-1
4
5 clc;
6
7 //(a) Calculate_the_dc_electron_velocity
```

```
8 V0=14.5*(10^3);
 9 \text{ v0} = .593*(10^6)*sqrt(V0);
10 disp(v0, 'the_dc_electron_velocity(in m/s) is =');
11
12
13 //(b) Calculate_the_dc_phase_constant
14
15 f = (10*(10^9));
16 Be=(2*\%pi*f)/v0;
17 disp(Be, 'the_dc_phase_constant(in rads/m) is =');
18
19
20
   //(c) Calculate_the_plasma_frequency
21
22
23 po=1*(10^-6); //dc_electron_charge_density
24 \text{wp} = ((1.759*(10^11)*po)/(8.854*(10^-12)))^(1/2);
25 disp(wp, 'the_plasma_frequency(in rad/s)) is = ');
26
27
   //(d) Calculate_the_reduced_plasma_frequency_for_R
      =0.4
29
30 R = 0.4;
31 wq=R*wp;
32 disp(wq, 'the_reduced_plasma_frequency_for_R = 0.4(in)
      rad/s) is =');
33
34
35
36 //(e) Calculate_the_dc_beam_current_density
37
38 \ J0 = po * v0;
39 \operatorname{disp}(J0, 'the_dc_beam_current_density(in A/m2)is = ');
40
41
42
43 //(f)
```

## Calculate\_the\_instantaneous\_beam\_current\_density

```
44
45
46  p=1*(10^-8);
47  v=1*(10^5);//velocity_perturbation
48  J=(p*v0)-(po*v);
49  disp(J, 'the_instantaneous_beam_current_density(in A/m2) is =');
```

#### Scilab code Exa 9.3.2 Operation of a FourCavity Klystron

```
1 //CAPTION: Operation_of_a_Four-Cavity_Klystron
\frac{2}{\cosh pter_no.-9}, page_no.-386
\frac{3}{\sqrt{\text{Example}}}no.9-3-2
5 clc;
7 //(a) Calculate_the_dc_electron_velocity
8 V0=18*(10^3);
9 \text{ v0} = .593*(10^6)*sqrt(V0);
10 disp(v0, 'the_dc_electron_velocity(in m/s) is =');
11
12
13 //(b) Calculate_the_dc_electron_phase_constant
14
15 f = (10*(10^9)); // Operating_frequency
16 \ w = 2 * \%pi * f
17 Be=w/v0;
18 disp(Be, 'the_dc_electron_phase_constant(in rads/m) is
       = ^{\prime} );
19
20
21
22 //(c) Calculate_the_plasma_frequency
23
```

```
24 po=1*(10^-8); //dc_electron_beam_current_density
25 \text{wp} = ((1.759*(10^11)*po)/(8.854*(10^-12)))^(1/2);
26 disp(wp, 'the_plasma_frequency(in rad/s) is =');
27
28
29
  //(d) Calculate_the_reduced_plasma_frequency_for_R
      =0.5
30
31 R=0.5;
32 \text{ wq} = R * wp;
33 disp(wq, 'the_reduced_plasma_frequency_for_R = 0.5(in
      rad/s) is =');
34
35
36
37 //(e) Calculate_the_reduced_plasma_phase_constant
38
39 Bq=wq/v0;
40 disp(Bq, 'the_reduced_plasma_phase_constant(in rad/m)
      is = ');
41
42
43
44
45
  //(f)
      Calculate_the_transit_time_across_the_input_gap
46
47 d=1*(10^-2); //gap_distance
48 \text{ t=d/v0};
49 t=t*(10^9);
50 disp(t, 'the_transit_time_across_the_input_gap(in ns)
      is = ');
51
52
53
54
55 // (g)
      Calculate_the_electron_velocity_leaving_the_input_gap
```

#### Scilab code Exa 9.3.3 Characteristics of Two Cavity Klystron

```
1 // CAPTION: Characteristics_of_Two-Cavity_Klystron
\frac{2}{\cosh pter_no.-9}, page_no.-388
3 / \text{Example_no.9} - 3 - 3
4 clc;
5
6 //(a) Calculate_the_plasma_frequency
7 po=1*(10^-6); //dc_electron_beam_current_density
8 wp = ((1.759*(10^11)*po)/(8.854*(10^-12)))^(1/2);
9 disp(wp, 'the_plasma_frequency(in rad/s) is =');
10
11
12 //(b) Calculate_the_reduced_plasma_frequency_for_R
      =0.5
13
14 R = 0.5;
15 f = (8*(10^9));
16 \ w=2*\%pi*f;
17 wq=R*wp;
18 disp(wq, 'the_reduced_plasma_frequency_for_R = 0.5(in)
      rad/s) is =');
19
20 //(c)
      Calculate_the_induced_current_in_the_output_cavity
```

```
21
22 V0 = 20 * (10^3);
23 IO=2; //beam_current
24 V1=10; // \operatorname{Signal_voltage}
25 Bo=1; // Beam_coupling_coefficient
26 I2=(I0*w*(Bo^2)*V1)/(2*V0*wq);
27 disp(I2, 'the_induced_current_in_the_output_cavity(in
       Ampere) is = ');
28
29
30
31
32 / (d)
      Calculate_the_induced_voltage_in_the_output_cavity
33
34 Rshl=30*(10^3);//
      total_shunt_resistance_including_load
35 \ V2 = I2 * Rshl;
36 \quad V2 = V2 / 1000;
37 disp(V2, 'the_induced_voltage_in_the_output_cavity(in
       KV) is = ');
38
39
   //(e) Calculate_the_output_power_delivered_to
      the_load
41
42
43 Rsh=10*(10^3);//shunt_resistance_of the_cavity
44 Rshl=30*(10^3);//
      total\_shunt\_resistance\_including\_load
45 Pout = (I2^2) * Rshl;
46 Pout=Pout/1000;
47 disp(Pout, 'the_output_power_delivered_to the_load(in
       KW) is = ');
48
49
50
```

```
//(f) Calculate_the_power_gain
//(f) Calculate_the_power_gain

powergain=(((I0*w)^2)*(Bo^4)*Rsh*Rshl)/(4*((V0*wq)^2));

powergain=10*log10(powergain);//powergain_in_dB
disp(powergain, 'the_power_gain is =');

//(g) Calculate_the_electronic_efficiency

//(g) calculate_the_electr
```

## Scilab code Exa 9.3.4 Output Power of Four Cavity Klystron

```
1 // CAPTION: Output_Power_of_Four-Cavity_Klystron
        \frac{2}{\cosh \theta} = \frac{1}{\cosh \theta} - \frac{1}{\cosh \theta} = \frac{1}{\cosh \theta} - \frac{1}{\cosh \theta} = \frac{1}{\cosh \theta} - \frac{1}{\cosh \theta} = \frac{1}
        3 / \text{Example_no.9} - 3 - 4
       4
        5 clc;
        7 //(a) Calculate_the_plasma_frequency
        8 po=5*(10^-5); //dc_electron_beam_current_density
        9 wp = ((1.759*(10^11)*po)/(8.854*(10^-12)))^(1/2);
 10 disp(wp, 'the_plasma_frequency(in rad/s) is =');
11
 12
13 //(b) Calculate_the_reduced_plasma_frequency_for_R
                                                                    =0.6
14
15 R = 0.6;
16 f = (4*(10^9));
```

```
17 w=2*\%pi*f;
18 \text{ wq} = R * wp;
19 disp(wq, 'the_reduced_plasma_frequency_for_R = 0.6(in)
      rad/s) is =');
20
21 //(c)
      Calculate_the_induced_current_in_the_output_cavity
22
23
24 Rsh=10*(10^3);//shunt_resistance_of the_cavity
   Rshl = 5*(10^3); //
      total_shunt_resistance_including_load
26 \quad V0 = 10 * (10^3);
27 I0=0.7; //beam_current
28 V1=2; // Signal_voltage
29 Bo=1; // Beam_coupling_coefficient
30 I4 = (((I0*w)^3)*(Bo^6)*V1*(Rsh^2))/(8*((V0*wq)^3));
31 disp(I4, 'the_induced_current_in_the_output_cavity(in
       Ampere) is = ');
32
33
34
35
36
  //(d)
      Calculate_the_induced_voltage_in_the_output_cavity
37
38
39
40 V4 = I4 * Rshl;
41 V4 = V4 / 1000;
42 disp(V4, 'the_induced_voltage_in_the_output_cavity(in
       KV) is = ');
43
44
45 //(e) Calculate_the_output_power_delivered_to
      the_load
```

```
46
47 Pout=(I4^2)*Rsh1;
48 Pout=Pout/1000;
49 disp(Pout, 'the_output_power_delivered_to the_load(in KW) is =');
```

## Scilab code Exa 9.4.1 Reflex Klystron

```
1 // CAPTION: Reflex_Klystron
2 / \cosh \operatorname{pter_no.} -9, \operatorname{page_no.} -399
3 / \text{Example_no.9} - 4 - 1
5 clc;
7 //(a) Calculate_the_value_of_the_repeller_voltage
8 V0 = 600;
9 n=2; //mode=2
10 fr=9*(10<sup>9</sup>);
11 w=2*%pi*fr;
12 L=1*(10^-3);
13 em=1.759*(10^11); //em=e/m
14 x=((em)*(((2*\%pi*n)-(\%pi/2))^2))/(8*(w^2)*(L^2));/x
      =V0/(V0+Vr)^2
15 y=V0/x;//y=(V0+Vr)^2
16 z=sqrt(y);//z=V0+Vr
17 Vr=z-V0;
18 disp(Vr, 'the_value_of_the_repeller_voltage(volts) is
      = ');
19
20
21
22
23
24 //(b)
```

Calculate\_the\_direct\_current\_necessary\_to\_give\_a\_microwave\_gap\_volume

```
25
26 disp('Assume_that_Bo=1');
27 disp('V2 = I2*Rsh = 2*I0*J1(X)*Rsh');
28 disp('the_direct_current_I0_is_I0 = V2/ 2*J1(X)*Rsh'
      );
29 V2=200;
30 \text{ Rsh} = 15*(10^3);
31 X = 1.841
32 J1(X) = .582;
33 I0 = V2/(2*J1(X)*Rsh);
34 \quad I0 = I0 * 1000;
35 disp(I0,'
      the_direct_current_necessary_to_give_a_microwave_gap_voltage_of_20
      (mA) is = ');
36
37
38
39 //(c) Calculate_the_electronic_efficiency
40
41 disp('From Eq(9-4-11), Eq(9-4-12) and Eq(9-4-20),
      the_electronic_efficiency_is');
42
43 efficiency=(2*X*J1(X))/((2*\%pi*n)-(\%pi/2));
44 efficiency=efficiency*100;
45 disp(efficiency, 'the_electronic_efficiency(in %) is =
      <sup>'</sup>);
```

## Scilab code Exa 9.5.1 Operation of Travelling WAVE TUBE

```
1 // CAPTION: Operation_of_Travelling -WAVE_TUBE(TWT)
2 //chapter_no.-9, page_no.-416
3 //Example_no.9-5-1
4
5 clc;
```

```
7 //(a) Calculate_the_gain_parameter
9 I0=30*(10^-3);//Beam_current
10 V0=3*(10^3);//Beam_voltage
11 Z0=10; //characteristic_impedance_of_the_helix
12 C = (((I0*Z0)/(4*V0))^(1/3));
13 disp(C, 'From Eq(9-5-56)) the gain parameter is =');
14
15
16 //(b) Calculate_the_output_power_gain_in_dB
17
18 N=50; // Crcular_length
19 Ap = -9.54 + (47.3 * N * C);
20 disp(Ap, 'the_output_power_gain_(in_dB) is =');
21
22
23
24 //(c) Calculate_the_four_propagation_constants
25
26 f = 10 * (10^9);
27 \quad V0 = 3*(10^3);
28 \text{ w} = 2*(\%\text{pi})*f;
v0 = .593*(10^6)*sqrt(V0);
30 Be=w/v0;
31
32 \text{ r1} = (-1*\text{Be}*\text{C}*(\text{sqrt}(3)/2)) + \%i*\text{Be}*(1+(C/2));
33 disp(r1, 'the_first_propagtaion_constant_is =');
34
35 r2=(Be*C*(sqrt(3)/2))+%i*Be*(1+(C/2));
36 disp(r2, 'the_second_propagtaion_constant_is =');
37 \text{ r3=\%i*Be*(1-C)};
38 disp(r3, 'the_third_propagtaion_constant is =');
39
40 r4=-1*\%i*Be*(1-((C^3)/4));
41 disp(r4, 'the_fourth_propagtaion_constant is =');
```

#### Scilab code Exa 9.7.1 Gridded Travelling Wave Tube

```
2 / \cosh \operatorname{pter_no.} -9, \operatorname{page_no.} -427
3 / \text{Example_no.9} - 7 - 1
4 clc;
6
7 //(a)
      Calculate\_the\_number\_of\_electrons\_returned\_per\_second
8 Ir=.85; //returned_current
9 q=1.6*(10^-19);//electronic_charge
10 Nr = Ir/q;
11 disp(Nr, 'the_number_of_electrons_returned_(
      per_second) is =');
12
13
14
15
16
17 //(b)
      Calculate_the_Energy_associated_with_these_returning_electrons_in_
18
19
20 V=11*(10^3);//overdepression_collector_voltage
21 t = 20*(10^-3);
22 \ W = V * Nr * t;
23 disp(W,'
      the_Energy_associated_with_these_returning_electrons_in_20ms
      (in eV) is =');
24
25
```

```
26
  //(c) Calculate_the_Power_for_returning_electrons
27
28
29
30 \text{ P=V*Ir};
31 P=P/1000;
32 disp(P, 'the_Power_for_returning_electrons (in KW) is =
      <sup>'</sup>);
33
34
35 //(d)
      Calculate\_the\_Heat\_associated\_with\_the\_returning\_electrons
36
37 t = 20*(10^-3);
38 \text{ H}=.238*P*1000*t;
39 disp(H,'
      the\_Heat\_associated\_with\_the\_returning\_electrons (
      in calories) is =');
40
41
42 //(e) Calculate_the_temperature
43
44 mass=250*(10^-3);
45 specificheat = .108;
46 T=H/(mass*specificheat);
47 disp(T, 'the_temperature(in degree Celsius) is =');
48
49 // (f)
      Calculate_whether_the_output_iron_pole_piece_is_melted
50
51
52 disp('the_output_iron_pole_piece_is_melted');
```

## Chapter 10

# Microwave crossed field tubes M type

### Scilab code Exa 10.1.1 Conventional Magnetron

```
1 //CAPTION: Conventional_Magnetron
\frac{2}{\cosh pter_no.-10}, page_no.-448
3 / \text{Example_no.} 10 - 1 - 1
5 clc;
7 //(a) Calculate_the_cyclotron_angular_frequency
9 em=1.759*(10^11); //em=e/m=charge_is_to_mass_ratio
10 B0=.336; // Magnetic_flux_density
11 wc = (em) * B0;
12 disp(wc, 'The_cyclotron_angular_frequency(in rad) is =
      ');
13
14
15
  //(b) Calculate_the_cutoff_voltage_for_a_fixed_B0
17
18
```

```
19 a=5*(10^-2); // radius_of_cathode_cylinder
20 b=10*(10^-2); // radius_of_vane_edge_to_centre
21 Voc = (em*(B0^2)*(b^2)*((1-((a/b)^2))^2))/8;
22 \text{ Voc=Voc}/(10^5);
23 disp(Voc, 'the_cutoff_voltage_for_a_fixed_B0(in KV) is
       = ');
24
25
26
27 //(c)
      Calculate_the_cutoff_magnetic_flux_density_for_a_fixed_V0
28
29
30 V0=26*(10^3); // Anode_voltage
31 Boc=(((8*V0)/em)^(1/2))/(b*(1-((a/b)^2)));
32 \, \text{Boc} = \text{Boc} * 1000;
33 disp(Boc,'
      the_cutoff_magnetic_flux_density_for_a_fixed_V0(
      in mWb/m^2) is =');
```

#### Scilab code Exa 10.1.1.A Pulsed Magnetron

```
// CAPTION: Pulsed_Magnetron
//chapter_no.-10, page_no.-452
//Example_no.10-1-1A

clc;
//(a) Calculate_the_angular_resonant_frequency

f=9*(10^9);//Operating_frequency
wr=2*%pi*f;
disp(wr,'the_angular_resonant_frequency(in rad)is =');
```

```
12
13
  //(b) Calculate_the_unloaded_quality_factor
14
15
16
17 C=2.5*(10^-12); // vane_capacitance
18 Gr=2*(10^-4); // Resonator_capacitance
19 Qun=wr*C/Gr;
20 disp(Qun, 'the_unloaded_quality_factor');
21
22
23
24
25 //(c) Calculate_the_loaded_quality_factor
26
27
28 C=2.5*(10^-12); // vane_capacitance
29 Gr=2*(10^-4); // Resonator_capacitance
30 G1=2.5*(10^-5); //loaded_capacitance
31 Ql=wr*C/(Gl+Gr);
32 disp(Q1, 'the_loaded_quality_factor');
33
34
35
36 //(d) Calculate_the_external_quality_factor
37
38
39 C=2.5*(10^-12);//vane_capacitance
40 Gl=2.5*(10^-5);//loaded_capacitance
41 Qex=wr*C/Gl;
42 disp(Qex, 'the_external_quality_factor');
43
44
45 //(e) Calculate_the_circuit_efficiency
47 n = (1/(1+(Qex/Qun)));
48 n=n*100;
49 disp(n, 'the\_circuit\_efficiency(in \%) is=');
```

## Scilab code Exa 10.1.2 Linear Magnetron

```
1 //CAPTION: Linear_Magnetron
\frac{2}{\cosh pter_no.-10}, page_no.-457
3 / \text{Example_no.} 10 - 1 - 2
5 clc;
6
8 //(a) Calculate_the_Hall_cutoff_voltage_for_fixed_Bo
9 em=1.759*(10^11); //em=e/m
10 Bo = . 01; // Magnetic_flux_density
11 d=5*(10^-2); // Distance_between_cathode_and_anode
12 Voc = (1/2) * (em) * (Bo^2) * (d^2);
13 Voc = Voc / 1000;
14 disp(Voc, 'the_Hall_cutoff_voltage_for_fixed_Bo(in KV
      ) is = ');
15
16
17
18
19 //(b)
      Calculate_the_Hall_cutoff_magnetic_field_density_for_fixed_Vo
```

## Scilab code Exa 10.1.2.a Linear Magnetron

```
1 //CAPTION: Linear_Magnetron
2 / chapter_no. -10, page_no. -459
\frac{3}{\sqrt{\text{Example_no.}10-1-2a}}
5 clc;
7 //(a)
      Calculate_the_electron_velocity_at_the_hub_surface
8
9 em=1.759*(10^11); //em=e/m
10 Bo = . 015; // Magnetic_flux_density
11 d=5*(10^-2); // Distance_between_cathode_and_anode
12 h=2.77*(10^-2); //hub_thickness
13 V=em*Bo*h;
14 disp(V, 'the_electron_velocity_at_the_hub_surface(in
     m/s) is =');
15
16
17
18
19
  //(b) Calculate_the_phase_velocity_for_synchronism
20
```

### Scilab code Exa 10.1.5 Inverted Coaxial Magnetron

```
1 // CAPTION: Inverted_Coaxial_Magnetron
\frac{2}{\cosh 2} // chapter_no. -10, page_no. -465
3 / \text{Example_no.} 10 - 1 - 5
4
5 clc;
6
   //(a) Calculate_the_cutoff_voltage_for_fixed_Bo
9 em=1.759*(10^11); //em=e/m
10 Bo = . 01; // Magnetic_flux_density
11 a=3*(10^-2); // anode_radius
12 b=4*(10^-2);//Cathode_radius
13 Voc=(1/8)*(em)*(Bo^2)*(a^2)*((1-((b/a)^2))^2);
14 Voc = Voc / 1000;
15 disp(Voc, 'the_cutoff_voltage_for_fixed_Bo(in KV) is =
      <sup>'</sup>);
16
17
18
```

### Scilab code Exa 10.1.6 Frequency Agile Magnetron

```
1 //CAPTION: Frequency-Agile_Magnetron
\frac{2}{\cosh pter_no.-10}, page_no.-467
\frac{3}{\sqrt{\text{Example}}}no.\frac{10-1-6}{2}
5 clc;
7 //(a) Calculate_the_agile_excursion
8 t = .2*(10^-6); //pulse_duration
9 N=14; // pulse_rate_on_target
10 AC=N/t; // agile_Excursion
11 AC=AC/(10^6); //in MHz
12 disp(AC, 'the_agile_excursion(in MHz) is =');
13
14
15
  //(b) Calculate_the_pulse-to-
16
      pulse_frequency_separation
17
18
19 fp=1/t;
```

```
20 fp=fp/(10^6);//in MHz
21 disp(fp, 'the_pulse-to-pulse_frequency_separation(in
      MHz) is = ');
22
23
24
  //(c) Calculate_the_signal_frequency
26
27 \quad DC = .001 // Duty_cycle
28 f = (DC/t);
29 f=f/(10^3); //in KHz
30 disp(f, 'the_signal_frequency(in KHz) is =');
31
32
33
34 //(d) Calculate_the_time_for_N_pulses
35
36 \text{ Time=N/f};
37 disp(Time, 'the_time_for_14_pulses_per_second_(in ms)
      is = ');
38
39
40
41
42 //(e) Calculate_the_agile_rate
43
44 Agilerate=1/(2*Time*10^-3);
45
46 disp(Agilerate, 'the_agile_rate(in Hz) is =');
```

#### Scilab code Exa 10.2.1 Crossed Field Amplifier

```
1 //CAPTION: Crossed-Field_Amplifier
2 //chapter_no.-10, page_no.-473
3 //Example_no.10-2-1
```

```
4
5 clc;
7 //(a) Calculate_the_induced_RF_power
9 Vao=2*(10^3); //Anode_dc_voltage
10 Iao=1.5; // Anode_dc_current
11 ne=.20; // Electronic_efficiency
12 Pgen=Vao*Iao*ne;
13 disp(Pgen, 'the_induced_RF_power(in W) is =');
14
15
16
17
  //(b) Calculate_the_total_RF_output_power
18
19
20
21 Pin=80; //RF_input_power
22 Pout=Pin+(Pgen);
23 disp(Pout, 'the_total_RF_output_power(in W) is =');
24
25
26 //(c) Calculate_the_power_gain
27
28 g=Pout/Pin;
29 g=10*log10(g);//in_decibels
30 disp(g, 'the_power_gain(in dB) is =');
```

## Scilab code Exa 10.3.1 Amplitron characteristics

```
1 //CAPTION: Amplitron_characteristics
2 //chapter_no.-10, page_no.-478
3 //Example_no.10-3-1
4
5 clc;
```

```
//(a) Calculate_the_dc_electron -beam_velocity
9 V0=15*(10^3);//Anode_voltage
10 v0 = .593*(10^6)*sqrt(V0);
11 disp(v0, 'the_dc_electron-beam_velocity_(in m/s) is =
      <sup>'</sup>);
12
13
14
   //(b) Calculate_the_electron -beam_phase_constant
15
16
17
18 f = 8*(10^9);
19 w = 2 * \%pi * f;
20 Be=w/v0;
21 disp(Be, 'the_electron - beam_phase_constant(in rad/m)
      is = ');
22
23
24
25
26
27 //(c) Calculate_the_cyclotron_angular_frequency
28
29 em=1.759*(10^11); //em=e/m
30 Bo=.2; // Magnetic_flux_density
31 wc = (em *Bo);
32 disp(wc, 'the_cyclotron_angular_frequency(in rad/s) is
        = ');
33
34
35 //(d) Calculate_the_cyclotron_phase_constant
36
37 Bm=wc/v0;
38 disp(Bm, 'the_cyclotron_phase_constant(in rad/m) is =
      <sup>'</sup>);
39
```

```
40 //(e) Calculate_the_gain_parameter
41
42 Z0=50; //characteristic_impedance
43 I0=3; // Anode_current
44 C=((I0*Z0)/(4*V0))^(1/3);
45 disp(C, 'the_gain_parameter is =');
```

#### Scilab code Exa 10.4.1 Carcinotron Characteristics

```
1 //CAPTION: Carcinotron_Characteristics
\frac{2}{\cosh pter_no.-10}, page_no.-483
\frac{3}{\sqrt{\text{Example_no.}10-4-1}}
5 clc;
  //(a) Calculate_the_dc_electron_velocity
9 V0=20*(10^3);//Anode_voltage
10 v0 = .593 * (10^6) * sqrt(V0);
11 disp(v0, 'the_dc_electron_velocity_(in m/s) is =');
12
13
14
15
   //(b) Calculate_the_electron -beam_phase_constant
16
17
18 f=4*(10^9); // operating_frequency
19 w = 2 * \%pi * f;
20 Be=w/v0;
21 disp(Be, 'the_electron -beam_phase_constant(in rad/m)
      is = ');
22
23
24
25
```

```
26 //(c) Calculate_the_delta_differentials
27
28
29 b=.5; //b_factor
30 disp('The_Delta_differentials_are : s1=');
31 s1=(\%i)*((b-sqrt((b^2)+4))/2);
32 disp(s1, 's1=');
33 s2=(\%i)*((b+sqrt((b^2)+4))/2);
34 disp(s2, 'And s2=');
35
36
37
38 //(d) Calculate_the_propagation_constants
39
40 D=.8; //D_factor
41 disp('the_propagation_constants are ');
42 r1=((\%i)*(Be+b))+(b*D*s1);
43 disp(r1, ' r1=');
44 r2=((\%i)*(Be+b))+(b*D*s2);
45 disp(r2, 'r2=');
46
47
48
49 //(e) Calculate_the_oscillation_condition
50
51 disp('the_oscillation_occurs_at_ DN=1.25 for n=1 ');
52 N=1.25/D;
53 disp(N, 'then N=');
54
55 l = (2*\%pi*N)/Be;
56 l=1*100; //in_cm
57 disp(1, 'and l= 2*pi*N/Be(in cm) = ')
```

## Chapter 11

## Strip lines

Scilab code Exa 11.1.1 Characteristic Impedance of Microstrip line

Scilab code Exa 11.2.1 Characteristics of a Parallel Strip Line

```
1 //CAPTION: Characteristics_of_a_Parallel_Strip_Line
  \frac{2}{\cosh 2} // chapter_no.-11, page_no.-505
  3 / \text{Example_no.} 11 - 2 - 1
  5 clc;
  7 //(a) Calculate the required width of the conducting
                         strip
  8 erd=6; // relative_dielectric_constant
  9 d=4*(10^-3); //thickness
10 Z0=50; // characteristic_impedance
11
12 w = (377*(d))/((sqrt(erd))*Z0);
13 disp(w, 'the_required_width_of_the_conducting_strip(
                     in metres) is =');
14
15 //(b) Calculate_the_strip_line_capacitance
16
17 ed=8.854*(10^-12)*erd;
18 d=4*(10^-3); //thickness
19 C = (ed*w)/d;
20 C=C*(10^12);
21 disp(C, 'the_strip_line_capacitance(in pF/m) is =');
22
23
24
25
26 //(c) Calculate_the_strip_line_inductance
27
28 \text{ uc}=4*\%\text{pi}*(10^-7);
29 d=4*(10^-3); //thickness
30 C = (uc*d)/w;
31 C=C*(10^6);
32 disp(C, 'the_strip_line_inductance(in uH/m) is =');
33
34 / (d)
                      Calculate\_the\_phase\_velocity\_of\_the\_wave\_in\_the\_parallel\_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_lin_strip\_l
```

Scilab code Exa 11.3.1 Characteristic Impedance of a Coplanar Stripline

```
1
2 //chapter_no.-11, page_no.-507
3 //Example_no.11-3-1
4
5 clc;
6
7 Pavg=250*(10^-3);//
    average_power_flowing_in_the_positive_z_direction
8 Io=100*(10^-3);//total_peak_current
9 Z0=(2*Pavg)/(Io^2);
10 disp(Z0,'
    the_characteristic_impedance_of_the_coplanar_strip_line
    (in ohms) is =');
```

Scilab code Exa 11.4.1 Characteristic Impedance of a Shielded Strip Line

```
1
2  //chapter_no.-11, page_no.-508
3  //Example_no.11-4-1
4
5
6  clc;
7
```

```
9 //(a) Calculate_the_K_factor
10
11 er=2.56//relative_dielectric_constant
12 w=25; // strip_width
13 t=14; // strip_thickness
14 d=70; //shield_depth
15 K=1/(1-(t/d));
16 disp(K, 'the_K_factor is =');
17
18 //(b) Calculate_the_fringe_capacitance
19
20 Cf = ((8.854*er)*((2*K*log(K+1))-((K-1)*log((K^2)-1)))
      )/%pi;
21 disp(Cf, 'the_fringe_capacitance(in pF/m) is =');
22
23
24 //(c)
      Calculate\_the\_characteristic\_impedance\_of\_the\_line
25
26 Z0=94.15/((((w/d)*K)+(Cf/(8.854*er)))*(sqrt(er)));
27 disp(ZO, 'the_characteristic_impedance_of_the_line(in
       ohms) is = ');
```

## Chapter 12

# Monolithic Microwave Integrated Circuits

Scilab code Exa 12.4.1 Resistance of a planar resistor

```
1
2 //chapter_no.-12, page_no.-534
3 //Example_no.12-4-1
4
5 clc;
6 l=10*(10^-3);;//resistance_film_length
7 ps=2.44*(10^-8);//sheet_resistivity_of_gold_film
8 w=10*(10^-3);//resistive_film_width
9 t=.1*(10^-6);//resistive_film_thickness
10 R=(1*ps)/(w*t);
11 disp(R,'the_planar_resistance(in ohm/square)is =');
```

Scilab code Exa 12.4.2 Planar Circular Spiral inductor

```
1 2 //chapter_no.-12, page_no.-536
```

```
3 //Example_no.12-4-2
4
5 clc;
6 n=5;//number_of_turns
7 w=50;//film_width
8 s=100;//separation
9 d0=2.5*n*(w+s);
10 L=.03125*(n^2)*d0;
11 disp(L,'the_inductance(in (nH/mil)is =');
```

### Scilab code Exa 12.4.3 Planar Capacitor

```
1
2 //chapter_no.-12, page_no.-537
3 //Example_no.12-4-3
4
5 clc;
6
7 N=8; // number_of_fingers
8 er=13.1; // relative_dielectric_constant
9 h=.254; // substarte_height
10 1=.00254; // finger_length
11 w=.051; // finger_base_width
12 A1=.089; // contribution_of_interior_finger_for_h> w
14 C=((er+1)*1*((A1*(N-3))+A2))/w;
15 disp(C, 'the_Capacitance(in (pF/cm) is =');
```