# Scilab Textbook Companion for Stoichiometry And Process Calculations by K. V. Narayanan And B. Lakshmikutty<sup>1</sup>

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# **Book Description**

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Scilab numbering policy used in this document and the relation to the above book.

Exa Example (Solved example)

Eqn Equation (Particular equation of the above book)

**AP** Appendix to Example(Scilab Code that is an Appednix to a particular Example of the above book)

For example, Exa 3.51 means solved example 3.51 of this book. Sec 2.3 means a scilab code whose theory is explained in Section 2.3 of the book.

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## Chapter 2

## Units and Dimensions

#### Scilab code Exa 2.1 Mass flow rate

```
1 //clc()
2 funcprot(0)
3 V1 = 15; //ft^3/min
4 ft = 0.3048; //m
5 min = 60; //secs
6 V = V1*ft^3/min;
7 disp("m^3/s", V, "Volumetric flowrate = ")
8 D = 1000; //kg/m^3
9 M = V * D;
10 disp("kg/s", M, "mass flowrate = ")
```

#### Scilab code Exa 2.2 Poundal to Newton

```
1 //clc()
2 funcprot(0)
3 ft = 0.3048; //m
4 lb = 0.4536; //kg
5 P = ft*lb;
6 disp("N",P,"1 poundal is 1 ft*lb/s^2 = ")
```

#### Scilab code Exa 2.3 Conversion of N per m2

```
1 //clc()
2 funcprot(0)
3 kgf = 9.80665; //N
4 cm = 10^-2; //m
5 P = kgf/cm^2;
6 disp("N/m^2",P,"1 kgf/cm^2 = ")
7 lbf = 32.174; //lb*ft//s^2
8 lb = 0.4535924; //kg
9 ft = 0.3048; //m
10 in = 0.0254; //m
11 P1 = lbf*lb*ft/in^2;
12 disp("N/m^2",P1,"1 lbf/in^2 = ")
```

#### Scilab code Exa 2.4 Thermal conductivity

```
1 //clc()
2 Q1 = 10000; //kJ/hr
3 kJ = 1000; //J
4 hr = 3600; //s
5 Q = Q1*kJ/hr; //J/s
6 disp("J/s",Q,"Q = ")
7 x = 0.1; //m
8 A = 1//m^2
9 T = 800; //K
10 k = x*Q/(A*T);
11 disp("W/(m*K)",k," thermal conductivity = ")
12 J = 1/4.1868; // cal
13 k1 = k*J*hr/1000;
14 disp("kcal/(h*m*C)",k1," thermal conductivity = ")
```

#### Scilab code Exa 2.5 Mass and FPS system

```
1 //clc()
2 F = 300; //N
3 a = 9.81; //m/s^2
4 m = F/a; //kg
5 disp("kg",m,"mass in kg = ")
6 lb = 4.535924/10; //kg
7 m1 = m/lb;
8 disp("lb",m1,"mass in pounds = ")
```

#### Scilab code Exa 2.6 Kinetic energy calculation

```
1 // clc()
2 z = 15; //m
3 PE = 2000; //J
4 g = 9.8067; //m/s^2
5 m = PE/(z*g);
6 disp("kg",m,"mass = ")
7 v = 50; //m/s
8 KE = 1/2*m*(v^2)/1000;
9 disp("kJ",KE,"kinetic energy = ")
```

#### Scilab code Exa 2.7 Force and pressure for piston cylinder

```
1 //clc()

2 g = 9.81; //m/s<sup>2</sup>

3 m = 100 * 0.4536; //kg

4 P = 101325; //N/m<sup>2</sup>
```

```
5 D1 = 4; //inch
6 D = D1 * 2.54 * 10^-2; //m
7 A = 3.1415 * (D^2)/4; //m^2
8 \text{ F1} = P * A; //N
9 	ext{ F2 = m * g; } / N
10 F = F1 + F2;
11 disp("N", F, "Total force acting on the gas = ")
12 P1 = F / A; //N/m^2
13 P2 = P1/100000; //bar
14 \text{ P3} = P1/(6.894757 * 10^3); //psi
15 \operatorname{disp}("N/m^2", P1, "Pressure in N/m^2 = ")
16 disp("bar", P2, "Pressure in bar = ")
17 disp("psi",P3,"Pressure in psi = ")
18 d = 0.4; //m
19 W = F * d;
20 disp("J",W,"Work done = ")
21 \text{ PE} = m * g * d;
22 disp("J", PE, "Change in potential energy = ")
```

#### Scilab code Exa 2.8 units conversion

```
11 C = (6.7 * 10^-4) * (( G * d / ds)^0.8) / ((ds^0.4)
          *(dG^0.2))* kG;
12 disp(C,"Co-efficient = ")
13 // this is the constant for the equation
14 // the equation thus becomes,
15 // kG1 = C * (( G1 * (ds1 + dt1) / ds1)^0.8) / ((ds1^0.4)*(dG1^0.2))
```

#### Scilab code Exa 2.9 units conversion

```
1 // clc ()
2 / \text{Cp} = 7.13 + 0.577 * (10^{-3}) * t + 0.0248 * (10^{-6})
       * t<sup>2</sup>
3 / Cp - Btu/lb-mol F, t - F
4 //Cp1 - kJ/kmol K, t1 - K
5 a = 7.13;
6 b = 0.577 * 10^-3;
7 c = 0.0248 * 10^{-6};
8 / t = 1.8 * t1 - 459.67
9 Cp = 4.1868; //Cp1 (Btu/lb-mol F = 4.1868 * (kJ/kmol)
      K) )
10 //substituting the above, we get,
11 //\text{Cp1} = 28.763 + 4.763 * (10^{-3}) * t1 + 0.3366 *
      (10^{\circ} - 6) * t^{\circ} 2
12 \text{ a1} = 28.763;
13 \ b1 = 4.763 * (10^-3);
14 c1 = 0.3366 * (10^-6);
15 \text{ disp}(a1,"a1 = ")
16 \text{ disp(b1,"b1} = ")
17 \text{ disp}(c1,"c1 = ")
18 // this are the co efficients for the following
      equation;
19 / Cp1 = a1 + b1 * t1 + c1 * (t1)^2
```

## Chapter 3

# Fundamental concepts of stoichiometry

Scilab code Exa 3.1 pounds per minute to kmol per hour

```
1 //clc()
2 m = 1000 * 0.4536; //kg/min
3 M = 30.24; //gm/mol
4 m1 = m * 60 / M;
5 disp("kmol/hr", m1, "molar folw rate = ")
```

Scilab code Exa 3.2 Number of molecules

```
1  // clc()
2  MK = 39.1;
3  MC = 12.0;
4  MO = 16;
5  MK2CO3 = MK * 2 + MC + MO * 3;
6  m = 691;
7  N = m / MK2CO3;
8  A = 6.023 * 10^23;
```

```
9 molecules = N * A;
10 disp("molecules", molecules, "Total no. of molecules =
")
```

#### Scilab code Exa 3.3 Moles of sodium sulphate

```
1 //clc()
2 Na = 23;//gm/mol
3 MNa = 100;//kg
4 N = MNa * 1000 / Na ;//g-atoms
5 NNa2S04 = N / 2;
6 disp("kmol", NNa2S04,"(a) moles of sodium sulphate = ")
7 MNa2S04 = 142.06;
8 m = NNa2S04 * MNa2S04/1000;
9 disp("kg",m,"(b) kilograms of sodium sulphate = ")
```

#### Scilab code Exa 3.4 Pyrites and oxygen moles

```
1 //clc()
2 MFe = 55.85;
3 MO = 16;
4 MS = 32;
5 MFeS2 = MFe + MS * 2;
6 MFe203 = MFe * 2 + MO * 3;
7 MS03 = MS + MO * 3;
8 m1S03 = 100; //kg
9 N1 = m1S03 / (MS03); //kmol
10 NFeS2 = N1 / 2;
11 mFeS2 = NFeS2 * MFeS2;
12 disp("kg", mFeS2," mass of pyrites to obtain 100kg of SO3 =")
13 m2SO3 = 50; //kg
```

```
14 N2 = m2S03 / (MS03); //kmol
15 N02 = N2 * 15/8;
16 m02 = N02 * M0 * 2;
17 disp("kg", m02, "mass of Oxygen consumed to produce 50 kg of SO3 =")
```

#### Scilab code Exa 3.5 Volume of oxygen

```
1 // clc()
2 MKClO3 = 122.55
3 mKClO3 = 100; // kg
4 NKClO3 = mKClO3 / MKClO3;
5 NO2 = 3 * NKClO3 / 2;
6 V1 = 22.4143; //m^3/kmol;
7 V = V1 * NO2;
8 disp("m^3", V, "volume of oxygen produced = ")
```

#### Scilab code Exa 3.6 Reaction of iron and steel

```
1 //clc()
2 mH2 = 100; //kg
3 NH2 = mH2/2.016;
4 NFe = 3 * NH2 / 4;
5 mFe = NFe * 55.85;
6 disp("kg", mFe,"(a) mass of iron required = ")
7 NH20 = NH2;
8 mH20 = NH20 * 18;
9 disp("kg", mH20, "mass of steam required =")
10 V1 = 22.4143; //m^3/kmol;
11 V = V1 * NH2;
12 disp("m^3", V, "Volume of hydrogen = ")
```

#### Scilab code Exa 3.7 Equivalent weight

```
1 // clc()
2 MCaCO3 = 100.08;
3 GE = MCaCO3 / 2;
4 disp("g",GE,"Gram equivalent wt. of CaCO3 =")
```

#### Scilab code Exa 3.8 Specific gravity calculation

```
1 // clc()
2 m1 = 1; //kg (mass in air)
3 m2 = 0.9; //kg (mass in water)
4 m3 = 0.82; //kg (mass in liquid)
5 L1 = m2 - m1; //kg (loss of mass in water)
6 L2 = m3 - m1; //kg (loss of mass in liquid)
7 sp.g = L2 /L1;
8 disp(sp.g, "specific gravity of liquid = ")
```

#### Scilab code Exa 3.9 Specific gravity of mixture

```
1  // clc()
2  m1 = 10; // kg
3  m2 = 5; // kg
4  sp.g1 = 1.17;
5  sp.g2 = 0.83;
6  Dwater = 1000; // kg/m^3
7  DA = Dwater * sp.g1;
8  DB = Dwater * sp.g2;
9  V1 = m1 / DA;
```

```
10  V2 = m2 / DB;
11  V = V1 + V2;
12  Dmix = (m1 + m2) / V;
13  sp.g3 = Dmix / Dwater;
14  disp(sp.g3, "specific gravity of mixture =")
```

#### Scilab code Exa 3.10 Baume scale

```
1 //clc()
2 Tw = 100; //Tw
3 sp.g = Tw/200 + 1;
4 Be = 145 - 145/sp.g;
5 disp("Be", Be," specific gravity on beume scale =")
```

#### Scilab code Exa 3.11 Density using API scale

```
1 // clc ()
2 \text{ API1} = 30; //API
3 sp.g1 = 141.5/(131.5 + API1); // (since, API = 141.5/
       sp.g -131.5
4 Dwater = 999; //kg/m^3;
5 \text{ Doil1} = \text{sp.g1} * \text{Dwater};
6 \text{ V1} = 250; //\text{m}^3
7 \text{ m1} = V1 * Doil1;
8 \text{ API2} = 15; //API
9 sp.g2 = 141.5/(131.5 + API2); // (since, API = 141.5/
       sp.g -131.5
10 Dwater = 999; // \text{kg/m}^3;
11 \text{ Doil2} = \text{sp.g2} * \text{Dwater};
12 V2 = 1000; //m^3
13 \text{ m2} = \text{V2} * \text{Doil2};
14 Dmix = (m1 + m2)/(V1 + V2);
15 \operatorname{disp}("kg/m^3", Dmix, "density of the mixture =")
```

#### Scilab code Exa 3.12 Drying Ammonium sulphate

```
1 //clc()
2 \text{ m1} = 250; //\text{kg}
3 mwater1 = 50; //kg
4 mdrysolid1 = m1 - mwater1;
5 \text{ wfe1} = \text{mwater1} / \text{m1};
6 wr1 = mwater1 / mdrysolid1;
7 wtpercentw1 = mwater1 * 100 / m1;
8 wtpercentd1 = mwater1 * 100 / mdrysolid1;
9 \ a = 90; //\%
10 mwater2 = mwater1 * (1 - a/100);
11 m2 = mdrysolid1 + mwater2;
12 \text{ wfe2} = \text{mwater2} / \text{m2};
13 wr2 = mwater2 / mdrysolid1;
14 wtpercentw2 = mwater2 * 100 / m2;
15 wtpercentd2 = mwater2 * 100 / mdrysolid1;
16 disp(wfe1, "(a) weight fraction of water at entrance =
      ")
17 disp(wfe2, "weight fraction of water at exit = ")
18 disp(wr1,"(b) weight ratio of water at entrance = ")
19 disp(wr2, "weight ratio of water at exit = ")
20 disp(wtpercentw1,"(c) weight percent of moisture on
      wet basis at entrance = ")
21 disp(wtpercentw2," weight percent of moisture on wet
      basis at exit = ")
22 disp(wtpercentd1,"(d)weight percent of moisture on
      dry basis at entrance = ")
23 disp(wtpercentd2, weight percent of moisture on dry
      basis at exit = ")
```

Scilab code Exa 3.13 Percentage of water removed

```
1 //clc()
2 mdrysolid = 100; //kg
3 percentin = 25;
4 mwaterin = mdrysolid * percentin / 100;
5 percentout = 2.5;
6 mwaterout = mdrysolid * percentout / 100;
7 mremoved = mwaterin - mwaterout;
8 percentremoved = mremoved *100 / mwaterin;
9 disp(percentremoved, "percentage of water removed = ")
```

#### Scilab code Exa 3.14 Amount and percentage water removed

```
1 //clc()
2 m = 1; //kg
3 percent1 = 20; //%
4 mwaterin = m * percent1 / 100;
5 mdrysolid = m - mwaterin;
6 percent2 = 2.44; //%
7 mout = mdrysolid / (1 - percent2/100);
8 mwaterout = mout - mdrysolid;
9 mremoved = mwaterin - mwaterout;
10 percentremoved = mremoved * 100 / mwaterin;
11 disp("kg", mremoved, "weight of water removed = ")
12 disp("%", percentremoved, "percentage of water removed = ")
```

#### Scilab code Exa 3.15 NaCl solution

```
1 //clc()
2 mwater = 100; //kg
3 mNaCl = 35.8; //kg
4 msolu = mwater + mNaCl;
```

```
5 mfr = mNaCl / msolu;
6 mpr = mfr * 100;
7 MNaCl = 58.45; //kg/kmol
8 NNaCl = mNaCl / MNaCl;
9 MH2O = 18; //kg/kmol
10 NH2O = mwater / MH2O;
11 Mfr = NNaCl / (NNaCl + NH2O);
12 Mpr = Mfr * 100;
13 N = NNaCl *1000 / mwater;
14 disp(mfr,"(a) mass fraction of NaCl =")
15 disp(mpr," mass percent of NaCl=")
16 disp(Mfr,"(b) mole fraction of NaCl =")
17 disp(Mpr," mole percent of NaCl = ")
18 disp(N,"kmol NaCl per 1000 kg of water =")
```

#### Scilab code Exa 3.16 Molal absolute humidity

```
1 //clc()
2 Y = 0.015; //kg water vapour/kg dry air
3 Mair = 29; //kg/kmol
4 Mwater = 18.016; //kg/kmol
5 Nwater = Y / Mwater; //kmol
6 Nair = 1 / Mair; //kmol
7 Mpr = Nwater *100 / (Nwater + Nair);
8 Mr = Nwater / Nair;
9 disp(Mpr,"(a) mole percent of water vapour = ")
10 disp("kmol water/kmol dry air", Mr,"(b) molal absolute humidity =")
```

#### Scilab code Exa 3.17 K2CO3 solution

```
1 // clc()

2 msolu = 100; //g
```

```
3 \text{ MK2CO3} = 138.20; //g/mol
4 percent1 = 50; //\%
5 mK2CO3 = percent1 *msolu / 100;
6 \text{ NK2CO3} = \text{mK2CO3} / \text{MK2CO3};
7 mwater = msolu - mK2CO3;
8 Nwater = mwater / 18.06;
9 Mpr = NK2C03 * 100 / (NK2C03 + Nwater);
10 \text{ sp.gr} = 1.53;
11 Vsolu = msolu/sp.gr;//mL
12 Vwater = mwater / 1; //mL
13 Vpr = Vwater * 100/ Vsolu;
14 Molality = NK2CO3 / (mwater * 10^-3);
15 Molarity = NK2CO3 / (Vsolu * 10^-3);
16 \text{ Eq.wt} = MK2CO3 / 2;
17 No = mK2CO3/Eq.wt;
18 N = No / (Vsolu * 10^-3);
19 disp("%", Mpr,"(a) Mole present of salt = ")
20 disp("%", Vpr, "(b) Volume percent of water = ")
21 \operatorname{disp}("\operatorname{mol/kg}", \operatorname{Molality}, "(c) \operatorname{Molality} = ")
22 \operatorname{disp}(\operatorname{"mol/L"},\operatorname{Molarity},\operatorname{"(d)}\operatorname{Molarity} = \operatorname{"})
23 disp("N", N, "(e) Normality")
```

#### Scilab code Exa 3.18 Molarity and Molality of Alcohol solution

```
1 //clc()
2 msolu = 100; //kg
3 percent1 = 60; //%
4 Dwater = 998; //kg/m^3
5 Dalco = 798; //kg/m^3
6 Dsolu = 895; //kg/m^3
7 Vsolu = msolu/Dsolu;
8 malco = msolu * percent1 / 100;
9 Valco = malco / Dalco;
10 Vpr = Valco * 100 / Vsolu;
11 Malco = 46.048; //kg/kmol
```

```
12 N = malco/Malco;
13 Molarity = N/(Vsolu );
14 mwater = msolu - malco;
15 Molality = N * 1000 /mwater;
16 disp("%", Vpr,"(a) Volume percent of ethanol in solution = ")
17 disp("mol/L", Molarity,"(b) Molarity = ")
18 disp("mol/(kg of water)", Molality,"(c) Molality = ")
```

#### Scilab code Exa 3.19 CO to phosgene

```
1 //clc()
2 / CO + CL2 = COC12
3 \text{ Np} = 12; // \text{moles}
4 NC12 = 3;//\text{moles}
5 \text{ NCO} = 8; // \text{moles}
6 \text{ N1Cl2} = \text{NCl2} + \text{Np};
7 \text{ N1CO} = \text{NCO} + \text{Np};
8 \text{ pr.ex} = (N1CO - N1Cl2)* 100/N1Cl2;
9 \text{ pr.co} = (N1C12 - NC12) * 100/ N1C12;
10 T = Np + NC12 + NC0;
11 T1 = N1C12 + N1C0;
12 N = T / T1;
13 disp("\%", pr.ex,"(a)) percent excess of CO = ")
14 disp("%", pr.co, "(b) percent conversion = ")
15 disp(N,"(c) Moles of total products per mole of total
        reactants = ")
```

#### Scilab code Exa 3.20 Extent of reaction

```
1 //clc()
2 Nn2 = 2;//moles
3 Nh2 = 7;//moles
```

```
4 Nnh3 = 1;//mole

5 n0 = Nn2 + Nh2 + Nnh3;

6 v = 2 - 1 - 3;

7 //YN2 = (2 - E)/(10 - 2*E)

8 //Yh2 = (7-3*E)/(10 - 2*E)

9 //Ynh3 = (1 + 2*E)/(10 - 2*E)

10 disp("mole fraction of N2 = (2 - E)/(10 - 2*E)")

11 disp("mole fraction of H2 = (7-3*E)/(10 - 2*E)")

12 disp("mole fraction of NH3 = (1 + 2*E)/(10 - 2*E)")
```

#### Scilab code Exa 3.21 ethylene to ethanol

```
1 //clc()
2 \text{ msolu} = 100; //g
3 \text{ MK2CO3} = 138.20; //g/mol
4 percent1 = 50; //\%
5 mK2CO3 = percent1 *msolu / 100;
6 \text{ NK2CO3} = \text{mK2CO3} / \text{MK2CO3};
7 mwater = msolu - mK2CO3;
8 Nwater = mwater / 18.06;
9 \text{ Mpr} = \text{NK2CO3} * 100 / (\text{NK2CO3} + \text{Nwater});
10 \text{ sp.gr} = 1.53;
11 Vsolu = msolu/sp.gr;//mL
12 Vwater = mwater / 1; //mL
13 Vpr = Vwater * 100/ Vsolu;
14 Molality = NK2CO3 / (mwater * 10^-3);
15 Molarity = NK2CO3 / (Vsolu * 10^-3);
16 \text{ Eq.wt} = MK2CO3 / 2;
17 No = mK2CO3/Eq.wt;
18 N = No / (Vsolu * 10^-3);
19 disp("%", Mpr, "(a) Mole preent of salt = ")
20 disp("%", Vpr, "(b) Volume percent of water = ")
21 \operatorname{disp}("\operatorname{mol/kg}", \operatorname{Molality}, "(c) \operatorname{Molality} = ")
22 \operatorname{disp}(\operatorname{"mol/L"},\operatorname{Molarity},\operatorname{"(d)}\operatorname{Molarity} = \operatorname{")}
23 disp("N", N, "(e) Normality")
```

# Chapter 4

### Ideal Gases and Gas Mixtures

#### Scilab code Exa 4.1 gas constant R

```
1 //clc()
2 P1 = 760; //mmHg
3 T1 = 273.15; //K
4 V1 = 22.4143 * 10^-3; //m^3/mol
5 R1 = P1 * V1 / T1;
6 disp("m^3 mmHg / (molK)",R1,"Gas constant R =")
7 P2 = 101325; //N/m^2
8 T2 = 273.15; //K
9 V2 = 22.4143 * 10^-3; //m^3/mol
10 R2 = P2 * V2 / T2; //J/molK
11 R3 = R2 / 4.184; //cal/molK
12 disp("cal/molK",R3,"Gas constant R in MKS system =")
```

#### Scilab code Exa 4.2 Molar volume of air

```
1 //clc()
2 T = 350;//K
3 P = 1;//bar
```

#### Scilab code Exa 4.3 Ideal gas equation

```
1 //clc()
2 P = 10; //bar
3 T = 300; //K
4 V = 150; //L
5 P1 = 1.01325; //bar ( \suffix 1 represents at STD)
6 T1 = 273.15; //K
7 V2 = T1 * P * V /(T * P1); //m^3
8 V1 = 22.4143; //m^3/mol
9 N = V2 / V1; //mol
10 M02 = 32;
11 m = N * M02/1000;
12 disp("kg",m," Mass of oxygen in the cylinder = ")
```

#### Scilab code Exa 4.4 Maximum allowable temperature of tyre

```
1 //clc()
2 P = 195; //kPa
3 T = 273; //K
4 P1 = 250; //kPa
5 T1 = P1 * T / P;
6 disp("K", T1, "Maximum temperature to which tyre may be heated = ")
```

#### Scilab code Exa 4.5 Pressure calculation

```
1  // clc()
2  V = 250; //L
3  T = 300; //K
4  V1 = 1000; //L
5  P1 = 100; //kPa
6  T1 = 310; //K
7  P = T * P1 * V1 /(T1 * V);
8  disp("kPa",P," Original pressure in the cylinder = ")
```

#### Scilab code Exa 4.6 weight composition and density calculation

```
1 //clc()
2 Vper1 = 70; /\% ( 1 = HCl)
3 Vper2 = 20; //\% ( 2 = C12)
4 Vper3 = 10; //\% ( 3 = CCl4)
5 M1 = 36.45;
6 M2 = 70.90;
7 M3 = 153.8;
8 \text{ m1} = \text{Vper1} * \text{M1};
9 \text{ m2} = \text{Vper2} * \text{M2};
10 \text{ m3} = \text{Vper3} * \text{M3};
11 mper1 = m1 * 100/(m1 + m2 + m3);
12 mper2 = m2 * 100/(m1 + m2 + m3);
13 mper3 = m3 * 100/(m1 + m2 + m3);
14 disp(mper1," (a) weight percent of HCl=")
15 disp(mper2, "weight percent of Cl2=")
16 disp(mper3, weight percent of CCl4= ")
17 m = (m1 + m2 + m3)/(Vper1 + Vper2 + Vper3);
18 disp("kg",m,"(b) average molecular weight = ")
19 v = 22.4143; //m^3/kmol
```

```
20 Vtotal = v * (Vper1 + Vper2 + Vper3);
21 D = (m1 + m2 + m3)/Vtotal;
22 disp("kg/m^3",D,"(c) Density at standard conditions =
    ")
```

#### Scilab code Exa 4.7 calculations for natural gas

```
1 // clc ()
2 per1 = 93; //\% ( 1 = methane)
3 per2 = 4.5; //\% (2 = ethane)
4 per3 = 100 - (per1 + per2); //\% ( 3 = N2);
5 T = 300; //K
6 p = 400; //kPa
7 P3 = p * per3 / 100;
8 \text{ v} = 10; //\text{m}^3
9 V2 = per2 * v / 100;
10 \text{ M1} = 16.032;
11 \quad M2 = 30.048;
12 M3 = 28;
13 \text{ N1} = \text{per1};
14 N2 = per2;
15 \text{ N3} = per3;
16 \text{ m1} = \text{M1} * \text{N1};
17 \text{ m2} = M2 * N2;
18 \text{ m3} = M3 * N3;
19 m = m1 + m2 + m3;
20 Vstp = 100 * 22.4143 * 10^{-3}; //m3 at STP
21 D = m /(1000 * Vstp);
22 Pstp = 101.325; //kPa
23 T1 = 273.15; //K
24 V = T * Pstp * Vstp / (T1 * p);
25 D1 = m /(1000 * V);
26 \text{ Mavg} = m / 100;
27 \text{ mper1} = m1 * 100 / (m1 + m2 + m3);
28 \text{ mper2} = m2 * 100 / (m1 + m2 + m3);
```

#### Scilab code Exa 4.8 Volume of gas from absorption columnn

```
1 //clc()
2 per1 = 20; //\% ( 1 = ammonia)
3 Vstp = 22.4143; //m^3/kmol
4 Pstp = 101.325; //kPa
5 \text{ Tstp} = 273.15; //K
6 \text{ V1} = 100; //\text{m}^3
7 \text{ P1} = 120; //\text{kPa}
8 \text{ T1} = 300; //K
9 P2 = 100; //kPa
10 T2 = 280; //K
11 per2 = 90; //\% (absorbed)
12 N = V1 * P1 * Tstp / (Vstp * Pstp * T1); //kmol
13 Nair = (1 - per1 / 100) * N;
14 \text{ N1} = \text{per1} * \text{N}/100;
15 \text{ Nabs} = \text{per2} * \text{N1} / 100;
16 N2 = N1 - Nabs; // leaving
17 Ntotal = Nair + N2;
18 Vstp1 = Ntotal * Vstp; //\text{m}^3
19 V2 = Vstp1 * Pstp * T2 / (Tstp * P2);
20 disp("m^3", V2," Volume of gas leaving = ")
```

#### Scilab code Exa 4.9 dehumidification

```
1 //clc()
2 V = 100; //m^3
3 Ptotal = 100; //kPa
4 Pwater = 4; //kPa
5 Pair = Ptotal - Pwater;
6 T = 300; //K
7 \text{ T1} = 275; //K
8 Vstp = 22.4143; //\text{m}^3/\text{kmol}
9 Tstp = 273.15; //K
10 Pstp = 101.325; //kPa
11 Pwater1 = 1.8; //kPa
12 Pair1 = Ptotal - Pwater1;
13 V1 = V * Pair * T1 / ( T * Pair1);
14 Nwater = V * Pwater * Tstp/ (Vstp * Pstp * T);
15 Nwater1 = V1 * Pwater1 * Tstp/ (Vstp * Pstp * T1);
16 m = (Nwater - Nwater1) * 18.02;
17 disp("m<sup>3</sup>", V1, "(a) volume of air after
      dehumidification = ")
18 disp("kg", m, "(b) Mass of water vapour removed = ")
```

#### Scilab code Exa 4.10 Absorption column for H2S

```
1 //clc()
2 V = 100; //m^3
3 P = 600; //kPa
4 T = 310; //K
5 per1 = 20; //% ( H2S entering )
6 per2 = 2; //% ( H2S leaving )
7 Pstp = 101.325; //kPa
```

```
8 Tstp = 273.15; //K
9 Vstp = 22.414; //m^3/kmol
10 \text{ Vstp1} = \text{V} * \text{P} * \text{Tstp} / (\text{T} * \text{Pstp})
11 N = Vstp1 / Vstp;
12 \text{ N1} = \text{N} * \text{per1} / 100;
13 N2 = N - N1; // ( 2 = inerts)
14 Nleaving = N2 / (1 - per2 / 100);
15 N1leaving = per2 * Nleaving / 100;
16 mabsorbed = (N1 - N1leaving) * 34.08; //(molecular)
      wt. = 34.08
17 mgiven = 100; //kg/h
18 Vactual = mgiven * V / mabsorbed;
19 Nactual = Nleaving * Vactual / V; // actual moles
      leaving
20 Vstpl = Nactual * Vstp; // volume leaving at STP
21 P2 = 500; //kPa
22 T2 = 290; //K
23 \ V2 = Vstpl * Pstp * T2 / ( P2 * Tstp);
24 Precovery = (N1 - N1leaving)*100 / N1;
25 disp("m^3/h", Vactual,"(a) Volume of gas entering per
      hour")
26 disp("m<sup>3</sup>/h", V2, "(b) Volume of gas leaving per hour")
27 disp("%", Precovery, "(c) Percentage recovery of H2S")
```

#### Scilab code Exa 4.11 Reaction stoichiometry for preparation of ammonia

```
7 \text{ T1} = 350; //K
8 P2 = 5; //bar
9 T2 = 290; //K
10 \ V3 = 3 * V1 * P1 * T2 / (P2 * T1);
11 disp("m^3", V3,"(b) Volume required at 50 bar and 290K
12 m = 1000; // \text{kg} ( ammonia )
13 N = m / 17.03; //kmol
14 N1 = N/2; // ( nitrogen)
15 N2 = N * 3 / 2; // (hydrogen)
16 \text{ P3} = 50; // \text{bar}
17 	ext{ T3} = 600; //K
18 Pstp = 1.01325; //bar
19 Tstp = 273.15; //K
20 Vstp = 22.414; //m^3/kmol
21 V1stp = N1 * Vstp;
22 \text{ V4} = \text{V1stp} * \text{Pstp} * \text{T3} / (\text{P3} * \text{Tstp}); // (\text{nitrogen})
      at 50 bar and 600K)
23 V5 = V4 * 2 ; // ( ammonia at 50 bar and 600K)
24 V6 = V4 * 3; // (hydrogen at 50 bar and 600K)
25 disp("m<sup>3</sup>", V4, "(c) Volume of nitrogen at 50 bar and
      600K")
  disp("m^3", V6,"
                      Volume of hydrogen at 50 bar and
26
      600K")
27 disp("m<sup>3</sup>", V5,"
                         Volume of ammonia at 50 bar and
      600K")
```

Scilab code Exa 4.12 Reaction stoichiometry for preparation of producer gas

```
1 // clc()
2 N = 100; //kmol producer gas
3 P1 = 25; //% ( Carbon monoxide )
4 P2 = 4; //% ( Carbon Dioxide )
5 P3 = 3; //% ( Oxygen )
```

```
6 P4 = 68; //\% ( Nitrogen )
7 N1 = N * P1/100;
8 N2 = N * P2/100;
9 N3 = N * P3/100;
10 N4 = N * P4/100;
11 \text{ NC} = \text{N1} + \text{N2};
12 \text{ m} = \text{NC} * 12;
13 Ngas = N / m; //moles of gas for 1 kg of Carbon
14 Vstp = 22.4143; //\text{m}^3/\text{kmol}
15 \text{ Vstp1} = \text{Vstp} * \text{Ngas};
16 P = 1; // bar
17 T = 290; //k
18 Pstp = 1.01325; //bar
19 Tstp = 273.15; //K
20 V = T * Vstp1 * Pstp / (Tstp * P);
21 disp("m<sup>3</sup>", V, "(a) Volume of gas at 1 bar and 290 K
       per kg Carbon = ")
22 / CO + 1/2 * O2 = CO2
23 Nrequired = N1/2 - N3; //(oxygen required)
24 Nsupplied = Nrequired * 1.2;
25 PO1 = 21; //\% (Oxygen percent in air)
26 Nair = Nsupplied * 100/P01;
27 V1 = 100; //\text{m}^3;
28 \text{ Vair} = \text{V1} * \text{Nair} / \text{N};
29 disp("m^3", Vair,"(b) Volume of air required = ")
30 \text{ NCO2} = \text{N2} + \text{N1};
31 NO2 = Nsupplied - Nrequired;
32 \text{ NN2} = \text{N4} + (\text{Vair} * (1 - \text{PO1}/100));
33 \text{ Ntotal} = \text{NCO2} + \text{NO2} + \text{NN2};
34 \text{ PCO2} = \text{NCO2} * 100 / \text{Ntotal};
35 \text{ PO2} = \text{NO2} * 100 / \text{Ntotal};
36 \text{ PN2} = \text{NN2} * 100 / \text{Ntotal};
37 disp("%", PCO2, "Percent composition of Carbon Dioxide
        = ")
38 disp("%", PO2, "Percent composition of Oxygen = ")
39 disp("%", PN2, "Percent composition of Nitrogen = ")
```

Scilab code Exa 4.13 Reaction stoichiometry for preparation of Chlorine from HCl

```
1 //clc()
2 //4HCl + O2 = 2Cl2 + 2H2O
3 n = 1; //mol (Basis 1 mol of HCl)
4 \text{ NO2} = n / 4;
5 \text{ NO2supp} = 1.5 * \text{NO2};
6 \text{ Nair} = \text{NO2supp} * 100 / 21;
7 V = 100; //m^3
8 \text{ Vair} = V * \text{Nair} / n;
9 disp("m^3", Vair, "(a) Volume of air admitted = ")
10 P1 = 80; //\% ( HCl converted)
11 Ncon = n * P1 / 100;
12 N2 = Ncon/4; // oxygen required
13 \text{ NH2O} = \text{Ncon} / 2;
14 \text{ NCl2} = \text{Ncon} / 2;
15 \text{ nHCl} = n - Ncon;
16 \text{ nO2} = \text{NO2supp} - \text{N2};
17 Nnitro = Nair - NO2supp;
18 Ntotal = nHCl + nO2 + NH2O + NCl2 + Nnitro;
19 V1 = V * Ntotal;
20 \text{ P1} = 1; // \text{bar}
21 \text{ T1} = 290; //K
22 P2 = 1.2; //bar
23 \text{ T2} = 400; //K
24 \ V2 = V1 * P1 * T2 / (P2 * T1);
25 disp("m^3", V2,"(b)) Volume of gas leaving = ")
26 \text{ VC12} = \text{NC12} * \text{V};
27 \text{ Pstp} = 1.01325; //bar
28 \text{ Tstp} = 273; //K
29 Vstp = 22.4143; //m^3/kmol
30 \text{ Vstp1} = \text{Tstp} * \text{P1} * \text{VC12} / (\text{T1} * \text{Pstp});
31 Nstp = Vstp1/Vstp;
```

```
32 \text{ m} = \text{Nstp} * 70.90;
33 disp("kg",m,"(c) Kilograms of Chlorine produced = ")
34 Ntotaldry = nHCl + nO2 + NCl2 + Nnitro; //dry basis
35 p1 = nHCl*100/Ntotaldry;
36 p2 = n02*100/Ntotaldry;
37 p3 = NC12*100/Ntotaldry;
38 p4 = Nnitro*100/Ntotaldry;
39 disp("%",p1,"(d) Percent composition of HCl in exit
      stream = ")
40 disp("%",p2,"
                    Percent composition of Oxygen in
      exit stream = ")
41 disp("%",p3,"
                    Percent composition of Chlorine in
      exit stream = ")
42 disp("%",p4,"
                    Percent composition of nitrogen in
      exit stream = ")
```

Scilab code Exa 4.14 Reaction stoichiometry for dissociation of Carbon Dioxide

```
1 //clc()
2 // CO2 = CO + 1/2 * O2
3 \text{ P1} = 1; // \text{bar}
4 \text{ T1} = 3500; //K
5 P2 = 1; //bar
6 	ext{ T2} = 300; //K
7 V2 = 25; //L
8 V1 = V2 * P2 * T1 / (P1 * T2);
9 disp("L", V1, "(a) Final volume of gas if no
       dissociation occured = ")
10 Pstp = 1.01325; //bar
11 Tstp = 273; //K
12 Vstp = 22.4143; /m^3
13 \text{ N2} = \text{V2} * \text{P2} * \text{Tstp} / (\text{Vstp} * \text{Pstp} * \text{T2});
14 // let x be the fraction dissociated, then after
       dissociation,
```

```
15 // CO2 = (1 - x)mol, CO = xmol, O2 = (0.5*x)mol

16 //total moles = 1 - x + x + 0.5 * x = 1 + 0.5 * x

17 V = 350; //L

18 N1 = V * P1 * Tstp / (Vstp * Pstp * T1);

19 // 1 + 0.5 * x = N1, therefore

20 x = (N1 - 1) / 0.5;

21 p = x*100;

22 disp("%",p,"(b)CO2 converted = ")
```

## Chapter 5

## Properties of Real Gases

Scilab code Exa 5.1 Van der waals equation

```
1 //clc()
2 V = 0.6; //m^3;
3 T = 473; //K
4 N = 1 * 10 ^ 3; //mol
5 R = 8.314; //Pa * m^3/molK
6 P = N * R * T / (V * 10^5);
7 disp("bar",P,"(a) Pressure calculated using ideal gas equation = ")
8 a = 0.4233; //N * m^4 / mol^2
9 b = 3.73 * 10^-5; //m^3/mol
10 P1 = (R*T/(V/N - b)-a/(V/N)^2)/10^5;
11 disp("bar",P1,"(a) Pressure calculated using van der waals equation = ")
```

Scilab code Exa 5.2 Van der waals equation for CO2 gas

```
1 //clc()
2 P = 10^7;//Pa;
```

```
3 T = 500; //K
4 R = 8.314; //Pa * L / mol K
5 V = N * R * T / ( P * 1000);
6 disp("m^3", V, "(a) Volume of CO2 calculated using ideal gas equation = ")
```

Scilab code Exa 5.3 Redlich Kwong equation for gaseous ammonia

```
1 //clc()
2 V = 0.6 * 10^-3; //m^3
3 T = 473; //K
4 Tc = 405.5; //K
5 Pc = 112.8 * 10 ^ 5//Pa
6 R = 8.314;
7 a = 0.4278 * (R^2) * (Tc ^ 2.5)/Pc;
8 b = 0.0867 * R * Tc / Pc;
9 P1 = (R*T/(V - b) - a/((T^0.5)*V*(V + b)))/10^5;
10 disp("bar",P1," Pressure developed by gas = ")
```

Scilab code Exa 5.4 Molar Volume calculation for gaseous ammonia

```
1 //clc()
2 P = 10^6; //Pa
3 T = 373; //K
4 Tc = 405.5; //K
5 Pc = 112.8 * 10 ^ 5//Pa
6 R = 8.314;
7 a = 0.4278 * (R^2) * (Tc ^ 2.5)/Pc;
8 b = 0.0867 * R * Tc / Pc;
9 //P1 = (R*T/(V - b) - a/((T^0.5)*V*(V + b)))/10^5;
10 //10^6 = ((8.314*373)/(V-2.59*10^-5)) - 8.68/((373^0.5)*V*(V+2.59*10^-5))
11 //solving this we get,
```

```
12 V = 3.0 * 10^{-3}; //m^3/mol
13 disp("m^3/mol", V, "molar volume of gas = ")
```

#### Scilab code Exa 5.5 virial equation of state

```
1 //clc()
2 B = -2.19 * 10^-4; //m^3/mol
3 C = -1.73 * 10^-8; //m^6/mol^2
4 P = 10; //bar
5 T = 500; //K
6 // virial equation is given as, Z = PV/RT = 1 + B/V + C/V^2
7 //V = (RT/P)*(1 + B/V + C/V^2)
8 // now by assuming different values for V on RHS and checking for corresponding V on LHS, we have to assume such value of V on RHS by which we get the same value for LHS V
9 //by trial and error we get,
10 V = 3.92 * 10^-3; //m^3
11 disp("m^3", V," Molar volume of methanol = ")
```

#### Scilab code Exa 5.6 Lyderson method for n butane

```
1 //clc()
2 T = 510; //K
3 P = 26.6; //bar
4 Tc = 425.2; //K
5 Pc = 38; //bar
6 Zc = 0.274;
7 R = 8.314;
8 Pr = P / Pc;
9 Tr = T / Tc;
10 disp(Pr, "Pr = ")
```

```
11 disp(Tr, "Tr = ")
12 //From fig. 5.4 and 5.5 from the text book
13 Z = 0.865;
14 D = 0.15;
15 Z1 = Z + D * ( Zc - 0.27);
16 V = R * T * Z1 / (P * 10^5);
17 disp("m^3/mol", V, "Molar volume of n-butane = ")
```

#### Scilab code Exa 5.7 Pitzer correlation for n butane

```
1 //clc()
2 T = 510; //K
3 P = 26.6; //bar
4 Tc = 425.2; //K
5 \text{ Pc} = 38; // \text{bar}
6 w = 0.193;
7 R = 8.314;
8 \text{ Pr} = P / Pc;
9 \text{ Tr} = T / Tc;
10 disp(Pr, "Pr = ")
11 disp(Tr, "Tr = ")
12 //From fig. 5.6 and 5.7 from the text book
13 \ Z0 = 0.855;
14 \ Z1 = 0.042;
15 \ Z = Z0 + w*Z1;
16 \text{ disp}(Z,"Z = ")
17 V = R * T * Z / (P * 10^5);
18 disp("m^3/mol", V, "Molar volume of n-butane = ")
```

#### Scilab code Exa 5.8 Molar volume by different methods

```
1 //clc()
2 P = 6000;//kPa
```

```
3 T = 325; //K
4 \text{ xn2} = 0.4;
5 \text{ xethane} = 0.6;
6 \text{ an2} = 0.1365; //N \text{ m}^4 / \text{ mol}^2
7 bn2 = 3.86 * 10^-5; //m^3/mol
8 aethane = 0.557; //N \text{ m}^4 / \text{mol}^2
9 bethane = 6.51 * 10^-5; //m^3/mol
10 Pcn2 = 3394; //kPa
11 Tcn2 = 126.2; //K
12 Pcethane = 4880; //kPa
13 Tcethane = 305.4; //K
14 R = 8.314;
15 V = R * T / (P*1000);
16 disp("m^3/mol", V, "(a) Molar volume by ideal gas
       equation =")
17 a = (xn2 * (an2^0.5) + xethane * (aethane^0.5))^2;
18 b = (xn2*bn2 + xethane*bethane);
19 //substituting the above values in van der waals
       equation, and solving, we get
20 \text{ V1} = 3.680 * 10^-4; //\text{m}^3/\text{mol}
21 disp("m<sup>3</sup>/mol", V1, "(b) Molar volume by van der waals
       equation =")
22 \text{ Prin2} = P/Pcn2;
23 \text{ Trin2} = T/Tcn2;
24 Priethane = P/Pcethane;
25 Triethane = T/Tcethane;
26 // using compressibilty chart,
27 \text{ Zn2} = 1;
28 Zethane = 0.42;
29 Z = xn2 * Zn2 + xethane * Zethane;
30 \text{ V2} = \text{Z} * \text{R} * \text{T} / \text{P};
31 disp("m<sup>3</sup>/mol", V2, "(c) Molar volume based on
       compressibilty factor =")
32 \text{ Pri1n2} = \text{xn2*P/Pcn2};
33 \text{ Tri1n2} = T/Tcn2;
34 Pri1ethane = xethane*P/Pcethane;
35 Tri1ethane = T/Tcethane;
36 // using compressibilty chart,
```

```
37  Zn21 = 1;
38  Zethane1 = 0.76;
39  Z1 = xn2 * Zn21 + xethane * Zethane1;
40  V3 = Z1 * R * T / P;
41  disp("m^3/mol", V3,"(c) Molar volume based on daltons law =")
42  Tc = xn2 * Tcn2 + xethane * Tcethane;
43  Pc = xn2 * Pcn2 + xethane * Pcethane;
44  Zc = 0.83;
45  V4 = Zc * R * T / P;
46  disp("m^3/mol", V4,"(d) Molar volume by kays method =")
```

#### Scilab code Exa 5.9 Van der waals equation and Kays method

```
1 // clc ()
2 \text{ P1} = 40; //\% \text{ (nitrogen)}
3 \text{ P2} = 60; //\% \text{ (ethane)}
4 T = 325; //K
5 V = 4.5 * 10^-4; //m^3/mol
6 a1 = 0.1365; //N*m^4/mol^2
7 b1 = 3.86 * 10 ^ -5; //m^3/mol
8 \text{ a2} = 0.557; //N*m^4/mol^2
9 b2 = 6.51 * 10 ^ -5; //m^3/mol
10 Pc1 = 3394; //kPa
11 Tc1 = 126.1; //K
12 Pc2 = 4880; //kPa
13 Tc2 = 305.4; //K
14 R = 8.314;
15 Pideal = R * T / (V * 1000); //kPa
16 disp("kPa", Pideal, "(a) Pressure of Gas by the ideal
      gas equation = ")
17 y1 = P1/100;
18 \text{ y2} = P2/100;
19 a = (y1 * (a1^(1/2)) + y2 * (a2^(1/2)))^2;
```

## Chapter 6

## Vapour Pressure

Scilab code Exa 6.1 Quality of steam

```
1 //clc()
2 P = 500; //kPa
3 SV = 0.2813; //m^3/kg
4 Vsaturatedl = 1.093 * 10^-3; //m^3/kg
5 Vsaturatedv = 0.3747; //m^3/kg
6 // let the fraction of vapour be y
7 //(1-y) * Vsaturatedl + y * Vsaturatedv = SV
8 //then we get, (1-y) * (1.093*10^-3) + y * (0.3747) = 0.2813
9 y = (SV - Vsaturatedl)/(Vsaturatedv - Vsaturatedl);
10 P1 = y * 100;
11 P2 = 100 - P1;
12 disp("%",P1," Percentage of Vapour = ")
13 disp("%",P2," Percentage of Liquid = ")
```

Scilab code Exa 6.2 Calculation of vapour pressure

```
1 //clc()
```

```
2 T1 = 363; //K
3 T2 = 373; //K
4 P2s = 101.3; //kPa
5 J = 2275 * 18; //kJ/kmol
6 R = 8.314; //kJ/kmolK
7 //ln (P2s/P1s) = J * (1/T1 - 1/T2) / R
8 P1s = P2s/exp(J * (1/T1 - 1/T2) / R);
9 disp("kPa",P1s," Vapour pressure of water at 363 K = ")
```

### Scilab code Exa 6.3 Clausius Clapeyron equation for acetone

```
1 // clc()
2 P1s = 194.9; //kPa
3 \text{ P2s} = 8.52; //\text{kPa}
4 \text{ T1} = 353; //K
5 T2 = 273; //K
6 \text{ T3} = 300; //K
7 Pair = 101.3; //kPa
8 / \log (P2s/P1s) = J * (1/T1 - 1/T2) / R
9 // let J / R = L
10 L = \log (P2s/P1s)/(1/T1 - 1/T2);
11 P3s = P1s * exp(L * (1/T1 - 1/T3));
12 Ptotal = P3s + Pair; //at saturation vapour pressure
      = partial pressure
13 disp("kPa", Ptotal, "(a) Final pressure of the mixture
      = ")
14 \text{ MP} = P3s * 100 / Ptotal;
15 // mole percent = moles of acetone * 100 / total
      moles
16 //= Partial pressure of acetone * 100 / total
      Pressure
17 disp("%", MP, "(b) Mole percent of acetone in the final
       mixture = ")
```

#### Scilab code Exa 6.4 Antoine equation for n heptane

```
1 //clc()
2 A = 13.8587;
3 B = 2911.32;
4 C = 56.56;
5 T1 = 325; //K
6 // Pressure at normal condition = 101.3kPa
7 P2 = 101.3; //kPa
8 // Antoine equation - lnP = A - B / (T - C)
9 lnP = A - (B / (T - C));
10 P1 = exp(lnP);
11 disp("kPa",P1,"(a) Vapour pressure of n-heptane at 325K = ")
12 T2 = B/(A - log(P2)) + C;
13 disp("K",T2,"(b) Normal boiling point of n-heptane = ")
```

#### Scilab code Exa 6.5 Cox chart

```
1 //clc()
2 T = [273 293 313 323 333 353 373];
3 Ps = [0.61 2.33 7.37 12.34 19.90 47.35 101.3];
4 plot2d('ll',T,Ps,rect=[250,0.1,380,195]);
5 P = get("hdl");
6 xtitle('Construction of cox chart', 'Temperature, K', 'Pressure, kPa');
7 T1 = [273 353]
8 Ps1 = [8.52 194.9]
9 plot2d('ll',T1,Ps1);
```

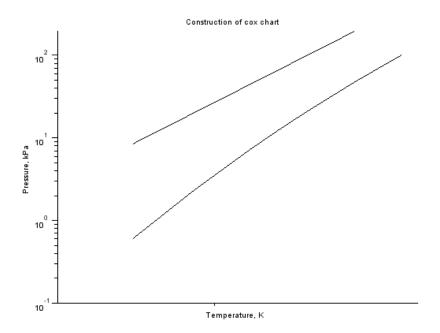


Figure 6.1: Cox chart

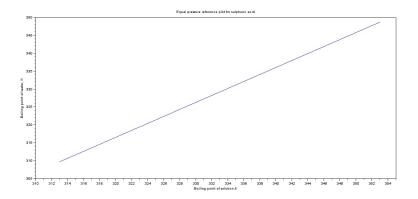


Figure 6.2: Duhring line

### Scilab code Exa 6.6 Duhring line

## Chapter 7

### Solutions and Phase Behaviour

Scilab code Exa 7.1 composition calculation of Liquid and vapour at equilibrium

```
//clc()
Pas = 71.2; //kPa
Pbs = 48.9; //kPa
//P=(Pas-Pbs)*xa+Pbs, xa=mole fraction of n-heptane,
liq. condition, therefore
xa = (P - Pbs)/(Pas - Pbs);
//ya = Pa / P , Vapour condition
ya = Pas * xa / P;
P1 = xa * 100;
P2 = ya * 100;
disp("%",P1," Percentage of hepatne in liquid = ")
disp("%",P2," Percentage of hepatne in vapour = ")
```

Scilab code Exa 7.2 Composition and total pressure calculation

```
1 //clc()
```

```
2 P1 = 100; //kPa ( Vapour pressure of liq A )
3 P2 = 60; //kPa ( Vapour pressure of liq B )
4 T = 320; //K
5 / Pa = xa * P1 = 100 * xa
6 / Pa = xb * P2 = 60 * xb
7 / P = xa * P1 + (1 - xa) * P2
8 // = 100 xa + (1 - xa) * 60
9 // = 60 + 40*xa
10 //ya = Pa / P
11 //0.5 = 100 * xa / (60 + 40 * xa)
12 \text{ xa} = 60 * 0.5 / (100 - 20);
13 \text{ Per1} = xa * 100;
14 disp("%", Per1,"(a) Percentage of A in liquid = ")
15 \text{ Ptotal} = 60 + 40 * xa;
16 disp("kPa", Ptotal, "(b) Total pressure of the vapour =
       ")
```

Scilab code Exa 7.3 Mole fraction calculation for particular component in liquid vapour mixture

```
1 //clc()
2 xa = 0.25;
3 xb = 0.30;
4 xc = 1 - xa - xb;
5 Ptotal = 200; //kPa
6 Pcs = 50; //kPa(Vapour pressure of c)
7 Pc = xc * Pcs; // (partial pressure of c)
8 yc = Pc / Ptotal;
9 yb = 0.5;
10 ya = 1 - yb - yc;
11 per1 = ya * 100;
12 disp("%", per1," Percentage of A in vapour = ")
```

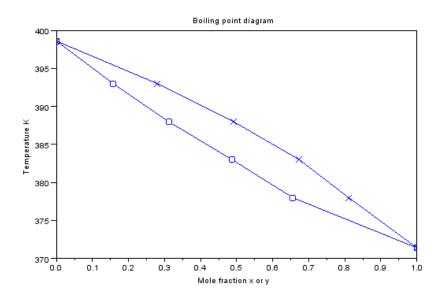


Figure 7.1: Boiling point diagram

Scilab code Exa 7.4 Flash vapourization of benzene toluene mixture

```
1 //clc()
2 P = 101.3; //kPa
3 Pbs = 54.21; //kPa
4 Pas = 136.09; //kPa
5 xf = 0.65;
6 xw = (P - Pbs)/(Pas - Pbs);
7 yd = xw * Pas / P;
8 // f = ( xf - xw ) / ( yd - xw );
9 f = ( xf - xw ) / ( yd - xw );
10 per1 = f * 100;
11 disp("%", per1," mole percent of the feed that is vapourised = ")
```

### Scilab code Exa 7.5.a Boiling point diagram

```
1 // clc ()
2 T = [371.4 378 383 388 393 398.6]
3 \text{ Pas} = [101.3 \ 125.3 \ 140 \ 160 \ 179.9 \ 205.3]
4 Pbs = [44.4 55.6 64.5 74.8 86.6 101.3]
5 Ptotal = 101.3; //kPa
6 \text{ for } i = 1:6
       x(i) = (Ptotal - Pbs(i))/(Pas(i) - Pbs(i));
7
8 end
9 \text{ for } i = 1:6
       y(i) = x(i) * Pas(i) / Ptotal;
10
11 end
12 plot(x,T,'-o');
13 plot(y,T,'-x');
14 xtitle ('Boiling point diagram', 'Mole fraction x or y
      ', 'Temperature K')
```

#### Scilab code Exa 7.5.b Equilibrium Diagram

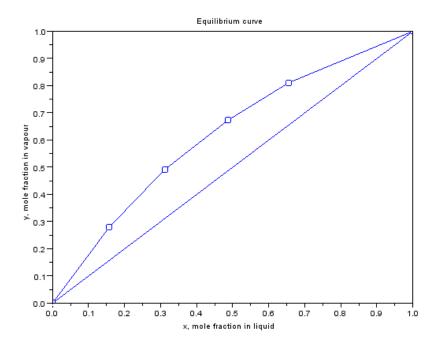


Figure 7.2: Equilibrium Diagram

```
14 plot(x,y,'-o');
15 xtitle('Equilibrium curve','x, mole fraction in liquid','y, mole fraction in vapour');
```

Scilab code Exa 7.6 Bubble point temperature and vapour composition

```
1 //clc()
2 Ps = 100; //kPa
3 A1 = 13.8587; //(1 = n-heptane)
4 A2 = 13.8216; //(2 = n-hexane)
5 B1 = 2911.32;
6 B2 = 2697.55;
7 C1 = 56.51;
8 C2 = 48.78;
9 //lnPs = A - B / (T - C)
10 T1 = B1 / (-log(Ps)+A1) + C1;
11 T2 = B2 / (-log(Ps)+A2) + C2;
12 x2 = 0.25;
```

Scilab code Exa 7.7 Dew point temperature pressure and concentration

```
1 //clc()
2 //lnPas = 14.5463 - 2940.46/(T - 35.93)
3 //lnPbs = 14.2724 - 2945.47 / (T - 49.15)
4 //xa = (P - Pbs)/(Pas - Pbs)
5 //Ya = Pas * (P - Pbs)/(P * (Pas - Pbs))
6 Ya = 0.4;
7 P = 65; //kPa
8 //various temperature value are assumed and tried till LHS = RHS, we get
9 T = 334.15; //K
10 Pas = exp(14.5463 - 2940.46/(T - 35.93));
11 Pbs = exp(14.2724 - 2945.47 / (T - 49.15));
```

#### Scilab code Exa 7.8 Partial pressure of acetaldehyde

```
1 //clc()
2 MW = 44.032;
3 Mwater = 18.016;
4 x = 2; //%
5 Pa = 41.4; //kPa
6 Mfr = (x/MW)/(x/MW + (100-x)/Mwater);
7 //henry's law gives Pa = Ha * xa
8 Ha = Pa / Mfr;
9 Molality = 0.1;
10 Mfr1 = Molality / (1000/Mwater + Molality);
11 Pa1 = Ha * Mfr1;
12 disp("kPa",Pa1," Partial Pressure = ")
```

#### Scilab code Exa 7.9 Raults law application

```
1 // \operatorname{clc}()

2 // 1 - \operatorname{pentane}, 2 - \operatorname{hexane}, 3 - \operatorname{heptane}
```

```
3 \times 1 = 0.6;
4 \times 2 = 0.25;
5 \times 3 = 0.15;
6 \quad A1 = 13.8183;
7 \quad A2 = 13.8216;
8 \quad A3 = 13.8587;
9 B1 = 2477.07;
10 B2 = 2697.55;
11 B3 = 2911.32;
12 C1 = 39.94;
13 \quad C2 = 48.78;
14 \quad C3 = 56.51;
15 //As raoults law is applicable, Ki = yi/xi = Pis/P
16 //yi = xi * Pis/P
17 / \ln P = A - B/(T - C)
18 // Assuming,
19 P = 400; //kPa
20 T = 369.75; //K
21 Pas1 = exp(A1 - B1 / (T - C1));
22 Pas2 = exp(A2 - B2 / (T - C2));
23 Pas3 = exp(A3 - B3 / (T - C3));
24 \text{ Yi} = (x1*Pas1 + x2*Pas2 + x3*Pas3)/P;
25 disp("K",T,"(a)bubble point temperature of the
      mixture = ")
26 \text{ y1} = \text{x1*Pas1/P};
27 \quad y2 = x2*Pas2/P;
28 \text{ y3} = \text{x3*Pas3/P};
29 disp("\%", y1*100,"(b)) composition of n-pentane in
      vapour = ")
30 disp("%", y2*100," composition of n-hexane in vapour =
  disp("%", y3*100, "composition of n-heptane in vapour
31
      = ")
32 \text{ T1} = 300; //K
33 Ps1 = exp(A1 - B1 / (T1 - C1));
34 \text{ Ps2} = \exp(A2 - B2 / (T1 - C2));
35 \text{ Ps3} = \exp(A3 - B3 / (T1 - C3));
36 P1 = x1*Ps1 + x2*Ps2 + x3*Ps3;
```

#### Scilab code Exa 7.10 Dew point temperature and pressure

```
1 // clc ()
2/1 - pentane, 2 - hexane, 3 - heptane
3 \text{ y1} = 0.6;
4 y2 = 0.25;
5 y3 = 0.15;
6 \quad A1 = 13.8183;
7 \quad A2 = 13.8216;
8 \quad A3 = 13.8587;
9 B1 = 2477.07;
10 B2 = 2697.55;
11 B3 = 2911.32;
12 \text{ C1} = 39.94;
13 \quad C2 = 48.78;
14 \quad C3 = 56.51;
15 P = 400; //kPa
16 T = 300; //K
17 //As raoults law is applicable, Ki = yi/xi = Pis/P
18 //xi = yi*P/Pis
19 //\ln P = A - B/(T - C)
20 // Assuming,
21 \text{ T1} = 385.94; //K
22 Pas1 = exp(A1 - B1 / (T1 - C1));
23 Pas2 = \exp(A2 - B2 / (T1 - C2));
24 Pas3 = exp(A3 - B3 / (T1 - C3));
25 disp("K",T,"(a)Dew point temperature of the mixture
      = ")
26 \text{ Ps1} = \exp(A1 - B1 / (T - C1));
27 \text{ Ps2} = \exp(A2 - B2 / (T - C2));
28 \text{ Ps3} = \exp(A3 - B3 / (T - C3));
29 P1 = 1/(y1/Ps1 + y2/Ps2 + y3/Ps3);
30 disp("kPa",P1,"(b)Dew point pressure = ")
```

### Scilab code Exa 7.11 bubble point and dew point

```
1 //clc()
2/1 - methanol, 2 - ethanol, 3 - propanol
3 \times 1 = 0.45;
4 \times 2 = 0.3;
5 \times 3 = 1 - (x1 + x2);
6 P = 101.3; //kPa
7 // by drawing the temperature vs vapour pressure
       graph and interpolation, assuming,
8 T = 344.6; //K
9 \text{ Ps1} = 137.3;
10 \text{ Ps2} = 76.2;
11 \text{ Ps3} = 65.4;
12 \text{ v1} = \text{x1} * \text{Ps1} / \text{P};
13 \text{ y2} = \text{x2} * \text{Ps2} / \text{P};
14 \text{ y3} = \text{x3} * \text{Ps3} / \text{P};
15 disp("K",T,"(a)Bubble point temperature = ")
16 disp("%", y1*100, "Composition of methanol in vapour =
  disp("%", y2*100, "Composition of ethanol in vapour =
17
   disp("%", y3*100, "Composition of propanol in vapour =
19 / again, for xi = 1
20 \text{ T1} = 347.5; //K
21 P1 = 153.28;
22 P2 = 85.25;
23 P3 = 73.31;
24 \text{ xa} = \text{x1} * \text{P} / \text{P1};
25 \text{ xb} = x2 * P / P2;
26 \text{ xc} = \text{x3} * \text{P} / \text{P3};
27 disp("K",T1,"(b))Dew point temperature = ")
28 disp("%", xa*100, "Composition of methanol in liquid =
```

```
")
29 disp("%",xb*100," Composition of ethanol in liquid =
")
30 disp("%",xc*100," Composition of propanol in liquid =
")
```

#### Scilab code Exa 7.12 component calculations

```
1 //clc()
2 \text{ xp} = 0.25;
3 \text{ xnb} = 0.4;
4 \text{ xnp} = 0.35;
5 P = 1447.14; //kPa
6 //assuming temperatures 355.4 K and 366.5 K,
      corresponding Ki values are found from nomograph
      and total Ki value are 0.928 and 1.075 resp, thus
       bubble point temperature lies between, using
      interpolation bubble point temperature is found
      to be,
7 Tb = 361; //K
8 disp("K", Tb, "(a) The buuble point temperature = ")
9 //At 361,
10 \text{ Kip} = 2.12;
11 \text{ Kinb} = 0.85;
12 \text{ Kinp} = 0.37;
13 \text{ xp1} = \text{Kip} * \text{xp};
14 \text{ xnb1} = \text{Kinb} * \text{xnb};
15 \text{ xnp1} = \text{Kinp} * \text{xnp};
16 disp(xp1, "concentration of propane at bubble point =
17 disp(xnb1, "concentration of n-butane at bubble point
18 disp(xnp1, "concentration of n-pentane at bubble
      point = ")
19 //At dew point Yi/Ki = 1, at 377.6K this is 1.1598
```

```
and at 388.8K it is 0.9677, by interpolation dew
      point is found to be
20 \text{ Td} = 387; //K
21 \text{ Kip1} = 2.85;
22 \text{ Kinb1} = 1.25;
23 \text{ Kinp1} = 0.59;
24 \text{ yp1} = \text{xp/Kip1};
25 \text{ ynb1} = \text{xnb/Kinb1};
26 \text{ ynp1} = \text{xnp/Kinp1};
27 disp("K", Td, "(b) The dew point temperature = ")
28 disp(yp1, "concentration of propane at dew point = ")
29 disp(ynb1, "concentration of n-butane at dew point =
30 disp(ynp1, "concentration of n-pentane at dew point =
31 //summation zi / (1 + L/VKi) = 0.45, using trial and
      error, we find
32 T = 374.6; //K
33 L = 0.55;
34 \ V = 0.45;
35 \text{ Kip2} = 2.5;
36 \text{ Kinb2} = 1.08;
37 \text{ Kinp2} = 0.48;
38 t = (xp/(1+L/(V*Kip2)))+(xnb/(1+L/(V*Kinb2))) + (xnp)
      /(1+L/(V*Kinp2));
39 yp2 = (xp/(1+L/(V*Kip2)))/t;
40 ynb2 = (xnb/(1+L/(V*Kinb2)))/t;
41 ynp2 = (xnp/(1+L/(V*Kinp2)))/t;
42 \text{ xp2} = (\text{xp - V * yp2})/L;
43 \text{ xnb2} = (\text{xnb} - \text{V} * \text{ynb2})/\text{L};
44 \text{ xnp2} = (\text{xnp} - \text{V} * \text{ynp2})/\text{L};
45 disp("K",T,"(c)) Temperature of the mixture = ")
46 disp(yp2, "vapour phase concentration of propane = ")
47 disp(ynb2, "vapour phase concentration of n-butane =
48 disp(ynp2, "vapour phase concentration of n-pentane =
49 disp(xp2, "liquid phase concentration of propane = ")
```

```
50 disp(xnb2,"liquid phase concentration of n-butane =
    ")
51 disp(xnp2,"liquid phase concentration of n-pentane =
    ")
```

#### Scilab code Exa 7.13 equilibrium temperature and composition

```
1 //clc()
2 P = 93.30; //kPa
3 T1 = 353; //K
4 T2 = 373; //K
5 Pwater1 = 47.98; //kPa
6 Pwater2 = 101.3; //kPa
7 Pliq1 = 2.67; //kPa
8 Pliq2 = 5.33; //kPa
9 T = T1 + (T2 - T1)*(P - (Pwater1 + Pliq1))/(Pwater2 + Pliq2 - (Pwater1 + Pliq1));
10 disp("K",T,"(a) The equilibrium temperature = ")
11 Pwater = 88.50;
12 y = Pwater * 100 /P;
13 disp("%",y,"(b) Water vapour in vapour mixture = ")
```

#### Scilab code Exa 7.14 Temperature composition diagram

```
1 //clc()
2 //the three phase temperature is first find out,
    which comes to be 342K, the corresponding Ps1 =
    71.18, Ps2 = 30.12
3 T = [342 343 348 353 363 373];
4 Ps2 = [30.12 31.06 37.99 47.32 70.11 101.3];
5 Ps1 = [71.18 72.91 85.31 100.5 135.42 179.14];
```

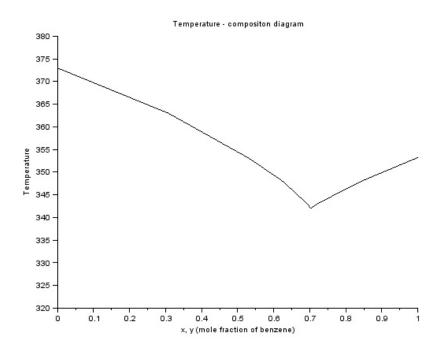


Figure 7.3: Temperature composition diagram

### Scilab code Exa 7.15 Boiling point calculation

```
1 //clc()
2 T = 379.2; //K
3 P = 101.3; //kPa
4 Ps = 70; //kPa
5 Molality = 5;
6 Pws = exp(16.26205 - 3799.887/(T - 46.854));
7 k = P / Pws;
8 Pws1 = Ps / k;
9 T1 = 3799.887 / (16.26205 - log( Pws1)) + 46.854;
10 disp("K",T1," Boiling point of the solution = ")
```

### Chapter 8

# Humidity and Humidity chart

Scilab code Exa 8.1 Nitrogen and ammonia gas mixture

```
1 //clc()
2 T = 280; //K
3 P = 105; //kPa
4 Pas = 13.25; //kPa ( Vpaour pressure of acetone )
5 Pa = Pas; // ( As gas is saturated, partial pressure
      = vapour pressure )
6 Mfr = Pa / P; // (Mole fraction)
7 \text{ Mpr} = \text{Mfr} * 100;
8 disp("%", Mpr,"(a) The mole percent of acetone in the
       mixture = ")
9 Ma = 58.048; // (molecular weight of acetone)
10 Mn = 28; // (molecular weight of nitrogen)
11 N = 1; // mole
12 \text{ Na = Mfr * N;}
13 \text{ Nn} = \text{N} - \text{Na};
14 \text{ ma} = \text{Na} * \text{Ma};
15 \text{ mn} = \text{Nn} * \text{Mn};
16 \text{ mtotal} = \text{ma} + \text{mn};
17 maper = ma *100 / mtotal;
18 mnper = mn *100/ mtotal;
19 disp("%", maper, "(b) Weight percent of acetone = ")
```

```
20 disp("%", mnper, "Weight percent of nitrogen = ")
21 Vstp = 22.4; //m^3/kmol
22 Pstp = 101.3; //kPa
23 Tstp = 273.15; //K
24 V = Vstp * Pstp * T / (Tstp * P);
25 C = ma/V;
26 disp("kg/m^3", C, "(c) Concentration of vapour = ")
```

#### Scilab code Exa 8.2 Benzene vapour air mixture

```
1 //clc()
2 P = 101.3; //kPa
3 Per1 = 10; //%
4 Pa = P * Per1 / 100; // ( a - benzene )
5 Ps = Pa; //( saturation )
6 //lnPs = 13.8858 - 2788.51/(T - 52.36)
7 T = 2788.51 / ( 13.8858 - log(Ps)) + 52.36;
8 disp("K",T," Temperature at which saturation occurs = ")
```

### Scilab code Exa 8.3 Evaporation of acetone using dry air

```
1 // clc()
2 Pdryair = 101.3; //kPa
3 Pacetone = 16.82; //kPa
4 Nratio = Pacetone / (Pdryair - Pacetone);
5 mratio = Nratio * 58.048 / 29; // (Macetone = 58.048, Mair = 29)
6 macetone = 5; //kg (given)
7 mdryair = macetone / mratio;
8 disp("kg", mdryair, "Minimum air required = ")
```

Scilab code Exa 8.4 Humidity for acetone vapour and nitrogen gas mixture

```
1 // clc()
2 Pa = 15; //kPa ( partial pressure of acetone)
3 Ptotal = 101.3; //kPa
4 Mfr = Pa / Ptotal;
5 disp(Mfr, "(a) Mole fraction of acetone = ")
6 Macetone = 58.048;
7 Mnitrogen = 28;
8 mafr = Mfr * Macetone / ( Mfr * Macetone + (1-Mfr)*
      Mnitrogen );
9 disp(mafr,"(b) Weight fraction of acetone = ")
10 \ Y = Mfr / (1 - Mfr);
11 disp("moles of acetone/moles of nitrogen", Y, "(c)
      Molal humidity = ")
12 \text{ Y1} = \text{Y} * \text{Macetone} / \text{Mnitrogen};
13 disp("kg acetone/kg nitrogen", Y1, "(d) Absolute
      humidity = ")
14 Pas = 26.36; //kPa (vapour pressure)
15 Ys = Pas / ( Ptotal - Pas); // saturation humidity
16 disp("moles of acetone/moles of nitrogen", Ys, "(e)
      Saturation humidity = ")
17 Y1s = Ys * Macetone / Mnitrogen;
18 disp("kg acetone/kg nitrogen", Y1s,"(f) Absolute
      saturation humidity = ")
19 V = 100; //\text{m}^3
20 Vstp = 22.4143; //\text{m}^3/\text{kmol}
21 Pstp = 101.3; //kPa
22 Tstp = 273.15; //K
23 T = 295; //K
24 N = V * Ptotal * Tstp / (Vstp * Pstp * T );
25 Nacetone = N * Mfr;
26 macetone = Nacetone * Macetone;
```

```
27 disp("kg", macetone, "(g) Mass of acetone in 100 \mathrm{m}^3 of the total gas = ")
```

### Scilab code Exa 8.5 Percent saturation and relative saturation

```
1 //clc();
2 Pa = 15; //kPa ( Partial pressure )
3 Pas = 26.36; //kPa ( Vapour pressure )
4 RS = Pa * 100 / Pas ;
5 Y = 0.1738;
6 Ys = 0.3517;
7 PS = Y * 100 / Ys;
8 disp("%", RS," Relative humidity = ")
9 disp("%", PS," Percent humidity = ")
```

#### Scilab code Exa 8.6 Analysis of Moist air

```
1 //clc()
2 mwater = 0.0109; //kg
3 \ V = 1; //m^3
4 T = 300; //K
5 P = 101.3; //kPa
6 Vstp = 22.4143; //\text{m}^3/\text{kmol}
7 Pstp = 101.3; //kPa
8 Tstp = 273.15; //K
9 N = V * P * Tstp / (Vstp * Pstp * T);
10 Nwater = mwater / 18.016;
11 Nfr = Nwater / N;
12 Pwater = Nfr * P;
13 disp("kPa", Pwater, "(a) Partial pressure of water
      vapour = ")
14 Ps = \exp(16.26205 - 3799.887/(T - 46.854));
15 \text{ RS} = Pwater * 100 / Ps;
```

```
disp("%",RS,"(b) Relative saturation = ")
Y1 = Pwater *18 / ((P - Pwater)*29);
disp("kg water / kg dry air",Y1,"(c) Absolute
    humidity = ")

Y1s = Ps *18 / ((P - Ps)*29);
PS1 = Y1 * 100 / Y1s;
disp("%",PS1,"(d) Percent saturation = ")
PS = 10; //%
Y1S = Y1 * 100/PS;
//Y1S = Pas/(P - Pas ) * 18 /29
Pas1 = 29 * P * Y1S / (18 + 29*Y1s);
T1 = 3799.887 / (16.26205-log(Pas1)) + 46.854;
disp("K",T1,"(e) Temperature at which 10% saturation occurs = ")
```

# Scilab code Exa 8.7 Heating value calculation for a fuel gas

```
1 // clc()
2 T = 300; //K
3 P = 100; //kPa
4 S = 25000 / kJ/m^3
5 \text{ T1= } 295; //K
6 \text{ P1} = 105; //\text{kPa}
7 \text{ RS} = 50; //\%
8 \text{ Ps} = 3.5; //\text{kPa}
9 Ps1 = 2.6; //kPa
10 Vstp = 22.4143; //\text{m}^3/\text{kmol}
11 Pstp = 101.3; //kPa
12 Tstp = 273.15; //K
13 V = 1; //\text{m}^3
14 N = V * P * Tstp/(Vstp * Pstp * T);
15 Nfuel = N * (P - Ps)/P;
16 Smol = S / Nfuel; //kJ/kmol
17 \text{ N1} = V * P1 * Tstp/(Vstp * Pstp * T1);
18 Pwater = Ps1 * RS /100;
```

# Scilab code Exa 8.8 Analysis of nitrogen benzene mixture

```
1 // clc ()
2 T = 300; //K
3 \text{ T1} = 335; //K
4 P = 150; //kPa
5 //\ln Ps = 13.8858 - 2788.51 / (T - 52.36)
6 \text{ Ps} = \exp(13.8858 - 2788.51 / (T - 52.36));
7 Ps1 = \exp(13.8858 - 2788.51 / (T1 - 52.36));
8 Pa = Ps; // (Vapour pressure at dew point is equal to
      the partial pressure of the vapour)
9 Y = Pa / (P - Pa);
10 \text{ Ys} = \text{Ps1} / (\text{P} - \text{Ps1});
11 PS = Y * 100 / Ys;
12 disp("%", PS, "(a) Percent saturation = ")
13 \text{ Ma} = 78.048;
14 \text{ Mb} = 28;
15 Q = Y * Ma / Mb ;
16 disp("kg benzene/kg nitrogen",Q,"(b)Quantity of
      benzene per kilgram of nitrogen = ")
17 V = 1; //\text{m}^3 ( basis )
18 Vstp = 22.4143; //\text{m}^3/\text{kmol}
19 Pstp = 101.3; //kPa
20 Tstp = 273.15; //K
21 N = V * P * Tstp/(Vstp * Pstp * T1);
22 y = Y / (1 + Y);
23 Nbenzene = N * y;
24 C = Nbenzene * Ma;
25 disp("kg/m<sup>3</sup>",C,"(c)Kilogram of benzene per m<sup>3</sup> of
      nitrogen = ")
```

```
26 P1 = 100; //kPa

27 Pbenzene = y * P1;

28 T1 = 2788.51 / ( 13.8858 - log (Pbenzene)) + 52.36;

29 disp("K",T1,"(d)Dew point = ")

30 Per1 = 60; //%

31 Y2 = Y * (1- Per1/100);

32 //Y2 = Pa / (P - Pa)

33 P = Pa / Y2 + Pa;

34 disp("kPa",P,"(e) Pressure required = ")
```

# Scilab code Exa 8.9 Drying

```
1 // clc ()
2 T = 300; //K
3 \text{ T1} = 285; //K
4 Pwater = 3.56; //kPa
5 Pwater1 = 1.4; //kPa
6 \ V = 1; //m^3 \ (Basis)
7 Vstp = 22.4143; //m^3/kmol
8 N = V / Vstp;
9 Pstp = 101.3; //kPa
10 Y = Pwater / (Pstp - Pwater);
11 Y1 = Pwater1 / (Pstp - Pwater1);
12 Nremoved = Y - Y1;
13 Ndryair = N * 1 / (1 + Y);
14 mremoved = Ndryair * Nremoved * 18.016;
15 disp("kg", mremoved, "(a) amount of water removed = ")
16 Nremaining = Ndryair * Y1;
17 V1 = (Ndryair + Nremaining) * Vstp;
18 disp("m<sup>3</sup>", V1, "(b) Volume of gas at stp after drying
     = ")
```

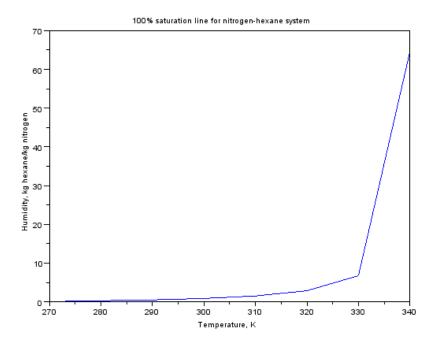


Figure 8.1: Saturation lines for hexane

#### Scilab code Exa 8.10 Saturation lines for hexane

```
1 //clc()
2 P = 100; //kPa
3 T = [273 280 290 300 310 320 330 340];
4 for i =1:8
5     Ps(i) = exp(13.8216 - 2697.55/(T(i)-48.78));
6 end
7 disp((Ps))
8 for j = 1:8
9     Ys(j) = Ps(j) * 86.11 / ((P - Ps(j))*28);
10 end
11 disp(Ys)
12 plot(T,Ys,rect=[273,0,333,10]);
13 xtitle('100% saturation line for nitrogen-hexane system', 'Temperature, K', 'Humidity, kg hexane/kg nitrogen');
```

# Scilab code Exa 8.11 Psychometric chart application

```
1 // clc()
2 Td = 328; //K ( dry bulb )
3 P = 101.3; //kPa
4 PS = 10; //%
5 // referring to the psychometric chart, corresponding to 328 K and 10% saturation
6 Y1 = 0.012; //kg water / kg dry air
7 disp("kg water / kg dry air", Y1,"(a) Absolute humidity = ")
8 //Y1 = Pa * 18 / ( P - Pa ) * 29
9 Pa = Y1 * P * 29 /( 18 + Y1 * 29 );
```

```
10 disp("kPa", Pa, "(b) Partial Pressure of water vapour =
11 //using psychometric chart, saturation humidity at
     328 K is given as
12 Y1s = 0.115; //kg water / kg dry air
13 disp("kg water / kg dry air", Y1s, "(c) The absolute
     humidity at 328K = ")
14 //at saturation partial pressure = vapour pressure
15 Pas = Y1s * P * 29 /( 18 + Y1s * 29 );
16 disp("kPa", Pas, "(d) Vapour Pressure of water vapour =
      ")
17 RS = Pa * 100 / Pas;
18 disp("%", RS, "(e) Percent relative saturation = ")
19 //using psychometric chart, moving horizontally
     keeping humidity constant to 100% saturation, we
     get dew point as,
20 T = 290; //K
21 disp("K",T,"(f)Dew point = ")
```

#### Scilab code Exa 8.12 Humid heat calculation for a sample of air

```
1 //clc()
2 Ca = 1.884; //kJ/kgK
3 Cb = 1.005; //kJ/kgK
4 Y1 = 0.012;
5 //Cs = Cb + Y1 * Ca
6 Cs = Cb + Y1 * Ca;
7 disp("kJ/kgK", Cs, "Humid heat of the sample = ")
8 P = 101.3; //kPa
9 V = 100; //m^3
10 R = 8.314;
11 T = 328; //K
12 T1 = 373; //K
13 N = P * V / (R * T );
14 Pa = 1.921; //kPa
```

```
15  Ndryair = N * (P - Pa)/P;
16  mdryair = Ndryair * 29;
17  Ht = mdryair * Cs * (T1 - T);
18  disp("kJ", Ht, "Heat to be supplied = ")
```

Scilab code Exa 8.14 wet bulb temperature and dry bulb temperature

```
1  //clc()
2  P = 101.3; //kPa
3  MW = 58;
4  T1 = 280.8; //K
5  Ps = 5; //kPa
6  pr = 2; //kJ/kgK ( Psychometric ratio )
7  Hvap = 360; //kJ/kg
8  Tw = T1;
9  Yw1 = Ps * MW / (( P - Ps) * 29);
10  // Tw = Tg - Hvap * ( Yw1 - Y1) / (hG / kY), where hG/kY is the psychmetric ratio pr
11  Y1 = 0;
12  Tg = Tw + Hvap * ( Yw1 - Y1) / pr;
13  disp("K", Tg," The air temperature = ")
```

## Scilab code Exa 8.15 Humidity calculation

```
1 //clc()
2 Td = 353.2; //K
3 Tw = 308; //K
4 Hvap = 2418.5; //kJ/kg
5 pr = 0.950; //kJ/kg
6 Ps = 5.62; //kPa
7 P = 101.3; //kPa
8 Yw1 = (Ps * 18)/ (( P - Ps) * 29);
9 Y1 = Yw1 - pr * ( Td - Tw ) / Hvap;
```

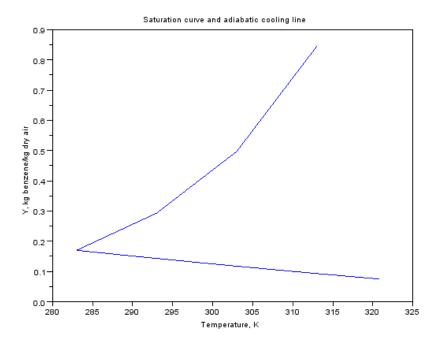


Figure 8.2: SAturation curve and adiabatic cooling line

Scilab code Exa 8.16 SAturation curve and adiabatic cooling line

```
1 //clc()
2 P = 101.3; //kPa
3 T = [283 293 303 313];
4 for i=1:4
```

```
Ps(i) = exp(13.8858 - 2788.51/(T(i)-52.36));
6 end
7 \text{ for } j = 1:4
       Ys(j) = Ps(j) * 78.048 / ((P - Ps(j))*29);
9 end
10 disp(Ps)
11 disp(Ys)
12 plot(T, Ys, rect = [270, 0, 323, 0.9]);
13 //Tas = Tg - L *(Y1as - Y1) / Cs
14 //Cs = Cb + Y1 *Ca = 1.005 + Y1 * 1.2
15 L = 435.4; //kJ/kgK
16 //for different value of Tg and Y1 tried, we have
      the following set of values
17 \text{ Tg} = [283 \ 290.4 \ 300 \ 310.1 \ 320.8];
18 \text{ Y1} = [0.1701150 \ 0.15 \ 0.125 \ 0.1 \ 0.075];
19 plot(Tg, Y1);
20 xtitle ('Saturation curve and adiabatic cooling line'
      , 'Temperature, K', 'Y, kg benzene/kg dry air');
```

#### Scilab code Exa 8.17 Adiabatic drier

```
1 //clc()
2 Tin = 380.7; //K
3 Pin = 101.3; //kPa
4 Tdew = 298; //K
5 mremoved = 2.25; //kg
6 V = 100; //m^3
7 //using humidity chart, humidity of air at dry bulb temperature of 380.7K and dew point = 298K is,
8 Y = 0.02; // kg water /kg dry air
9 disp("kg water /kg dry air", Y,"(a) Humidity of air entering the drier = ")
10 Tstp = 273.15; //K
11 Vstp = 22.4143; //m^3/kmol
12 N = V * Tstp / (Vstp * Tin );
```

```
13 MY = Y * 29 / 18; // molal humidity
14 Ndryair = N / (1 + MY);
15 mdryair = Ndryair *29;
16 mwaterin = mdryair * Y;
17 mwaterout = mwaterin + mremoved;
18 Yout = mwaterout / mdryair;
19 // percent humidity is calculated using the chart,
      and is
20 \text{ PY} = 55; /\%
21 disp("kg water /kg dry air", Yout, "(b) exit air
      humidity = ")
22 disp("%", PY, "Percent humidity = ")
23 //from the humidity chart
24 Twet = 313.2; //K
25 \text{ Td} = 322.2; //K
26 disp("K", Twet,"(c) exit air wet bulb temperature = ")
27 disp("K", Td, "(c) exit air dry bulb temperature = ")
28 MYout = Yout * 29 / 18;
29 Nout = Ndryair * ( 1 + MYout ) / 1;
30 \text{ V1} = \text{Nout} * \text{Vstp} * \text{Td} / \text{Tstp};
31 \operatorname{disp}(\text{"m}^3\text{",V1,"}(d)) Volume of exit air = ")
```

# Scilab code Exa 8.18 Psychometric chart application

```
1 //clc()
2 P = 101.3; //kPa
3 Td = 303; //K
4 Tw = 288; //K
5 //using psychometric chart,
6 Y1 = 0.0045; //kg water/ kg dry air
7 PY = 18; //%
8 Theated = 356.7; //K
9 Cb = 1.005;
10 Ca = 1.884;
11 Cs = Cb + Y1 * Ca;
```

```
12 Q = 1 * Cs * (Theated - Td);
13 disp("kg water/ kg dry air", Y1,"(a) Humidity of the
    initial air = ")
14 disp("%", PY,"(b) Percent humidity = ")
15 disp("K", Theated,"(c) Temperature to which the air is
    heated = ")
16 disp("kJ",Q,"(d) Heat to be suppplied = ")
```

Scilab code Exa 8.19 Psychometric chart application and given wet bulb and dry bulb temperature

```
1 //clc()
2 \text{ Tw} = 313; //K
3 \text{ Td} = 333; //K
4 //Using th psychometric chart,
5 Y = 0.04; //kg water/kg dry air
6 \text{ PS} = 26.5; //\%
7 VS = 1.18; //\text{m}^3/\text{kg} dry air (volume of saturated air
8 VD = 0.94; //\text{m}^3/\text{kg} dry air (volume of dry air)
9 \text{ VH} = \text{VD} + \text{PS} * (\text{VS} - \text{VD})/100;
10 HS = 470; //J / kg dry air (enthalpy of saturated
       air )
11 HD = 60; //J / kg dry air (enthalpy of dry air)
12 \text{ H} = \text{HD} + \text{PS} * (\text{HS} - \text{HD})/100;
13 disp("kg water/ kg dry air", Y, "(a) Absolute Humidity
       of the air = ")
14 disp("%", PS, "(b) Percent humidity = ")
15 disp("m^3/kg dry air", VH, "(c) Humid volume = ")
16 disp("kJ/kg dry air", H, "(d) Enthalpy of wet air = ")
```

# Chapter 9

# Material Balance in Unit Operations

## Scilab code Exa 9.1 Combustion of coal

```
1 //clc()
2 PC1 = 85; //% ( Percent carbon in coal )
3 PA1 = 15; //% ( Percent ash in coal )
4 PA2 = 80; //% ( Percent ash in cinder )
5 PC2 = 20; //% ( Percent carbon in cinder )
6 m = 100; //kg (weight of coal )
7 mash = PA1 * m / 100;
8 w = mash * 100 / PA2; // weight of cinder
9 mcarbon = w - mash;
10 Plost = mcarbon * 100 / ( m - mash );
11 disp("kg", w, "weight of cinder formed = ")
12 disp("%", Plost, "Percent fuel lost = ")
```

Scilab code Exa 9.2 Drying of wood

```
1 //clc()
```

```
2 m = 1;//kg ( mass of completely dry wood )
3 P1 = 40;//% ( percentage moisture in wet wood )
4 P2 = 5;//% ( Percentage moisture in dry wood )
5 mwaterin = P1 * m / ( 100 - P1 );
6 mwaterout = P2 * m / ( 100 - P2 );
7 mevaporated = mwaterin - mwaterout;
8 disp("kg", mevaporated, "mass of water evaporated per kg of dry wood = ")
```

# Scilab code Exa 9.3 Effluent discharge

```
1 //clc()
2 F1 = 6*1000; //L/s
3 B0D1 = 3 * 10^-5; //g/L
4 B0D2 = 5 * 10^-3; //g/L
5 V = 16 * 10^3; //m^3/day
6 v = V * 10^3 / (24 * 3600); //L/s
7 //Let BOD of the effluent be BODeff,
8 B0Deff = (B0D2 * (F1 + v) - B0D1 * F1) / ( v );
9 disp("g/L",B0Deff,"BOD of the effluent of the plant = ")
```

#### Scilab code Exa 9.4 benzene requirement calculation

```
1 // clc()
2 D = 100; //kg of overhead product
3 xfa = 0.956;
4 xdw = 0.074;
5 xdb = 0.741;
6 xda = 0.185;
7 // water balance gives
8 F = D * xdw / (1 - xfa);
9 W = F * xfa - xda * D;
```

```
10 W1 = 100;
11 B = xdb*D;
12 Bused = B * W1 / W;
13 disp("kg", Bused, "Quantity of benzene required = ")
```

# Scilab code Exa 9.5 Fortification of waste acid

```
1 // clc ()
2 //let, W - waste acid, S - Sulfuric acid, N - nitric
        acid, M - mixed acid
3 \text{ xsh2so4} = 0.95;
4 \text{ xsh2o} = 0.5;
5 \text{ wwh} 2 \text{so} 4 = 0.3;
6 \text{ wwhno3} = 0.36;
7 \text{ xwh2o} = 0.34;
8 \text{ xmh} 2 \text{so} 4 = 0.4;
9 \text{ xmhno3} = 0.45;
10 \text{ xmh2o} = 0.15;
11 \quad xnhno3 = 0.8;
12 \text{ xnh2o} = 0.2;
13 M = 1000; //kg
14 // total material balance, W + S + N = 1000;
15 / H2SO4 balance, xwh2so4 * W + xsh2so4 * S = xmh2so4
      *M
16 / \text{HNO3 balance}, xwhno3 * W + xnhno3 * N = xmhno3*M
17 / \text{H2O balance}, xwh2o*W+xnh2o*N + xsh2o*S = xmh2o*M
18 //solving the above equations simultaneously, we get
19 W = 70.22; //kg
20 S = 398.88; //kg
21 N = 530.9; //kg
22 disp("kg", W, "Waste acid = ")
23 disp("kg",S,"Concentrated H2SO4 = ")
24 disp("kg", N, "Concentrated HNO3 = ")
```

# Scilab code Exa 9.6 Triple effect evaporator

```
1 // clc ()
2 \text{ F} = 1000; //\text{kg}
3 Psolute1 = 20; //\%
4 Psolute2 = 80; //\%
5 //taking solute balance
6 L3 = F * Psolute1 / Psolute2;
7 //taking total material balance
8 V = (F - L3) / 3;
9 //for first effect, total balance gives,
10 L1 = F - V;
11 //solute balance gives,
12 Psolute3 = F * Psolute1 / L1;
13 //For second effect, total balance gives,
14 L2 = L1 - V;
15 //solute balnce gives,
16 Psolute4 = L1 * Psolute3 / L2;
17 disp("%", Psolute3, "solute entering second effect = "
18 disp("kg",L1,"Weight entering second effect")
19 disp("%", Psolute4, "solute entering third effect = ")
20 disp("kg",L2,"Weight entering third effect")
```

#### Scilab code Exa 9.7 Crystallization operation

```
1 //clc()
2 F = 100; //kg
3 xf = 0.25;
4 x2 = 7/107;
5 P1 = 10; //%
```

# Scilab code Exa 9.8 Evaporation of Na2CO3

```
1 // clc ()
2 F = 100; //kg
3 \text{ xf} = 0.15;
4 P1 = 80; //\% ( Carbonate recovered )
5 M1 = 106; // (Molecular weight of Na2CO3)
6 M2 = 286; // (Molecular weight of Na2CO3.10H2O)
7 \text{ x1} = \text{M1} / \text{M2}; //(\text{Weight fraction of Na2CO3 in})
      crystals)
8 \text{ Mrecovered} = P1 * F * xf / 100;
9 Wcrystal = Mrecovered / x1;
10 disp("kg", Wcrystal, "(a) quantity of crystals formed =
11 / Na2CO3 balance gives, F*xf = Wcrystal*x1 + W2*x2
12 //W2 weight of mother liquor remaining after
      crystallization
13 / let M = W2 * x2, therefore
14 M = F * xf - Mrecovered;
15 \times 2 = 0.09;
16 W2 = M/x2;
17 W3 = F - Wcrystal - W2; //weight of water evaporated
```

## Scilab code Exa 9.9 Crystallization

```
1 // clc()
2 m = 100; //\text{kg} (of 60% solution)
3 / w - water added to the original solution
4 //w1 - wt. of Na2S2O3.5H2O crystallized
5 / w^2 - wt. of mother liquor obtained
6 //w3 - solution carried away by the crystals
7 \text{ xf} = 0.6;
8 \text{ Mna2s2o3} = 158;
9 \text{ Mna2s2o35h2o} = 248;
10 mcrystals = m * xf * Mna2s2o35h2o / Mna2s2o3;
11 // free water available = m + w - 1 - m crystals
12 //concentration of impurity = 1/(w+4.823)
13 //total balance, 100 - 1 + w = w1 + w2 + w3
14 / w1 + w2 + w3 - w = 99
15 / \text{Na}_{2}S2O3 \text{ balance}, 60 = (w1 + w2 * 1.5/2.5 + w3 *
       1.5/2.5)*158/248
16 / w1 + 0.6 * w2 + 0.6 * w3 = 94.177
17 //each gram crystals carry 0.05 kg solution,
18 / w3 = 0.05 * w1
19 //impurity \% = 0.1
20 / \text{impurity} = \text{w3} / (2.5 * (\text{w}+4.823))
21 //solving above equations, we get
22 \text{ w} = 14.577; //\text{kg}
23 \text{ w1} = 65.08; //\text{kg}
24 \text{ w2} = 45.25; //\text{kg}
25 \text{ w3} = 0.05 * \text{w1};
26 disp("kg",w,"(a)amount of water added = ")
27 disp("kg", w1,"(b) amount of Na2S2O3.5H2O crystals
       added = ")
28 \text{ m1} = \text{w1} * \text{Mna} 2 \text{s} 2 \text{o} 3 / \text{Mna} 2 \text{s} 2 \text{o} 35 \text{h} 2 \text{o} + \text{w3} * 1.5 *
       Mna2s2o3 / (2.5 * Mna2s2o35h2o);
```

```
29 P = m1*100/(m*xf);
30 disp("%",P,"(c)Percentage recovery of Na2S2O3 = ")
```

#### Scilab code Exa 9.10 Extraction

```
1 //clc()
2 m = 100; //kg
3 Pin1 = 40; //\% ( tannin )
4 Pin2 = 5; //\% ( moisture )
5 Pin3 = 23; //\% ( soluble non tannin material )
6 Pin4 = 100 - Pin1 - Pin2 - Pin3; //\% ( insoluble
     lignin )
7 // since, lignin is insoluble, all of it will be
     present in the residue
8 Pout1 = 3; //\%
9 Pout2 = 50; /\%
10 Pout3 = 1; //\%
11 Pout4 = 100 - Pout1 - Pout2 - Pout3;
12 //let W be the mass of residue, then we get
13 W = Pin4 * m / Pout4;
14 Ptannin = W * Pout1 * 100 / (m * Pin1);
15 disp("%", Ptannin," Percent of original tannin
     unextracted = ")
```

#### Scilab code Exa 9.11 Leaching operation

```
1  // clc()
2  F = 100; //kg
3  //F - feed, R - overflow, U - underflow, S - solvent
4  //F + S = U + R ( Total balance )
5  Poil1 = 49; //% ( 1 - feed )
6  Ppulp1 = 40; //%
7  Psalts1 = 3; //%
```

```
8 Pwater = 100 - Poil1 - Ppulp1 - Psalts1;
9 Phexane2 = 25; //\%(2 - underflow)
10 Psalts2 = 2.5; //\%
11 Poil2 = 15; //\%
12 Pwater2 = 7.5; //\%
13 Ppulp2 = 100 - Phexane2 - Poil2 - Pwater2 - Psalts2
14 Poil3 = 25; //\% ( 3 - extract )
15 //taking pulp (inert) balance
16 U = Ppulp1 * F / Ppulp2;
17 //oil balance gives, F * Poil1 = U * Poil2 + R *
     Poil3, from these, we get
18 R = (F * Poil1 - U * Poil2)/Poil3;
19 S = U + R - F;
20 disp("kg",S,"(a) The amount of solvent used for
      extraction = ")
21 Precovered = 95; //\%
22 \text{ mhexane2} = Phexane2 * U / 100;
23 mrecovered = mhexane2 * Precovered / 100;
24 P = mrecovered * 100 / S;
25 disp("%",P,"(b) Percent of hexane used that is
      recovered from the underflow = ")
26 \text{ Poil} = \text{Poil3} * R * 100 / (F * Poil1);
27 disp("%", Poil, "(c) Percent recovery of oil = ")
```

# Scilab code Exa 9.12 Dryer and oven

```
7 //moisture free solid balance for drier, F * ( 1 -
     xf) = S1 * (1 - x1)
8 S1 = F * (1 - xf)/(1 - x1);
9 //total balance for drier, F = S1 + V1
10 \text{ V1} = F - S1;
11 //For oven, S1 * ( 1 - x1 ) = S2 * ( 1 - x2 )
12 S2 = S1 * (1 - x1)/(1 - x2);
13 / Also, S1 = S2 + V2
14 \ V2 = S1 - S2;
15 disp("kg",S1,"(a) Weight of product leaving the drier
16 disp("kg", S2," Weight of product leaving the oven
     = ")
17 P1 = V1 *100/ (F * xf);
18 P2 = V2 *100/ (F * xf);
19 disp("%", P1, "(b) Percentage of original water removed
      in drier = ")
20 disp("%", P2," Percentage of original water removed
      in oven = ")
```

#### Scilab code Exa 9.13 Adiabatic drier

```
1 //clc()
2 //Ss = solid flow rate,
3 Pwaterin = 25; //%
4 Pwaterout = 5; //%
5 X1 = Pwaterin/(100 - Pwaterin); //kg water/kg dry air
6 X2 = Pwaterout/(100 - Pwaterout); //kg water/kg dry air
7 //form humidity chart,
8 Y2 = 0.015; //kg water/kg dry air
9 Y1 = 0.035; //kg water/kg dry air
10 m = 1; //kg of dry air
11 //Ss * X1 + Y2 = Ss * X2 + Y1
12 Ss = (Y1 - Y2) / (X1 - X2);
```

```
13 T = 87.5 + 273.15; //K
14 P = 101.3; //kPa
15 Tstp = 273.15; //K
16 Pstp = 101.3; //kPa
17 Vstp = 22.4143; //\text{m}^3/\text{mol}
18 V = 100; //\text{m}^3
19 N = V * P * Tstp / ( Vstp * Pstp * T);
20 Nr2 = Y2 * 29 / 18; //kmol of water / kmol of dry air
21 \text{ Ndryair} = N * 1 / (1 + Nr2);
22 \text{ mdryair} = \text{Ndryair} * 29;
23 mevaporated = mdryair * ( Y1 - Y2 );
24 disp("kg", mevaporated, "(a) total moisture evaporated
      per 100\text{m}^3 of air entering = ")
25 \text{ Ss1} = \text{mdryair} * \text{Ss};
26 \text{ mproduct} = Ss1 * (1 + X2);
27 disp("kg",mproduct,"(b) mass of finished product per
       100 \text{m}^3 of air entering = ")
```

#### Scilab code Exa 9.14 Extraction of isopropyl alcohol

```
1 // clc ()
2 / F = feed, E = extract, S = solvent, R = Raffinate
3 \text{ xwaterF} = 0.7; // \text{Feed}
4 \text{ xalcoholF} = 0.3;
5 xwaterR = 0.71; // raffinate
6 \text{ xalcoholR} = 0.281;
7 \text{ xethyR} = 0.009;
8 xwaterE = 0.008; //Extract
9 \text{ xalcoholE} = 0.052;
10 \text{ xethyE} = 0.94;
11 //Total balance, R + E = F + S
12 F = 100; //kg
13 / R + E = 100 + S
                                                      (1)
14 //Isopropyl balance, xalcoholR * R + xalcoholE*E =
      xalcoholF * F
```

```
15 / 0.281 *R + 0.052 * E = 30
                                                (2)
16 //Ethylene tetra chloride balance, xethyR * R +
      xethyE * E = S
17 / 0.009 *R + 0.94 *E = S
                                                (3)
18 //Solving equation 1, 2 and 3 simultaneously, we get
19 S = 45.1;
20 E = 47.04;
21 R = 98.06;
22 disp("kg",S,"(a)) Amount of solvent used = ")
23 disp("kg", E,"(b))Amount of extract = ")
24 disp("kg",R," Amount of raffinate = ")
25 mextracted = E * xalcoholE;
26 \text{ P1} = \text{mextracted} * 100 / (F * xalcoholF);
27 disp("%",P1,"(c)Percent of isopropyl alcohol
      extracted = ")
```

#### Scilab code Exa 9.15 Absorption of acetone

```
1 // clc()
2 G1 = 100; //kmol
3 //G1 and G2 be the molar flow rate of the gas at the inlet and the exit of the absorber resp., y1 and y2 mole fraction at entrance and exit resp.,
4 y1 = 0.25; //%
5 y2 = 0.05; //%
6 // air balance gives, G1 * (1-y1) = G2 * (1-y2)
7 G2 = G1 * (1-y1) / (1 - y2);
8 maleaving = G2 * y2;
9 maentering = G1 * y1;
10 Pabsorbed = (maentering - maleaving) * 100 / (maentering);
11 disp("%", Pabsorbed, "Percentage of acetone absorbed = ")
```

# Scilab code Exa 9.16 Absorption of SO3

```
1 //clc()
2 F = 5000; //kg/h
3 \text{ P1} = 50; //\% \text{ (H2O4 in)}
4 \text{ MH2SO4} = 98.016;
5 P1gas = 65; //(nitrogen in gas entering)
6 P2gas = 35; // (SO3)
7 \text{ MN2} = 28;
8 \text{ MSO3} = 80;
9 Mavg = (MN2 * P1gas + MS03 * P2gas)/100; //avg
      molecular wt. of entering gas
10 G = 4500; //kg/h
11 Ng = G / Mavg;
12 \text{ NN2} = \text{Ng} * \text{P1gas} / 100;
13 \text{ NSO3} = \text{Ng} - \text{NN2};
14 P2 = 75; //\% (H2O4 out)
15 /W be the mass of 75% H2SO4, x and y be the moles
      of SO3 and water vapour leaving resp.,
16 Pwater = 25; //kPa
17 Ptotal = 101.3; //kPa
18 //Pwater / Ptotal = y / ( NN2 + x + y )
19 //we get, y = 0.32765 * x + 2.744
20 / \text{Total balance Feed} + G = W + (NN2 * 28 + x * 80 + C)
      y * 18.016
21 / \text{we get}, W + 80*x + 18.016*y = 7727.32
                                                        (2)
\frac{22}{\text{from 1}} and \frac{2}{\text{supple}}, 84.9174*x + W = 7352.68
                                                        (3)
23 //SO3 balance, So3 eneterin with 50\% H2SO4 + SO3 in
      feed gas = SO leaving with 75\%H2SO4 + SO3 leaving
       in exit gas
24 / 5000*0.5*80/98.016 + 34.09*80 = 80* x + 0.75*W*
      80/98.016
                   (4)
25 // from 3 and 4,
26 \times 9.74;
```

```
27 Nabsorbed = NSO3 - x;
28 Pabsorbed = Nabsorbed * 100 / NSO3;
29 disp("%", Pabsorbed, "Percentage of SO3 absorbed = ")
```

#### Scilab code Exa 9.17 Continuous distillation column

```
1 //clc()
2 F = 200; //kmol/h
3 //F, D and W be the flow rates of the feed, the
      distillate and residue resp., xf, xd and xw be
      the mole fraction of ethanol in the fee,
      distillate and the residue resp.
4 \text{ xf} = 0.10;
5 \text{ xd} = 0.89;
6 \text{ xw} = 0.003;
7 //total balance gives, F = D + W
8 / D + W = 200
                                 (1)
9 // Alcohol balance gives, F*xf = D*xd + W*xw
10 / 0.89 *D + 0.003 *W = 20
                            (2)
11 // solving 1 and 2
12 D = 21.87; //\text{kmol/h}
13 W = 178.13; //\text{kmol/h}
14 Nawasted = W*xw;
15 mmakeup = Nawasted * 46*24;
16 disp("kg", mmakeup, "The make up alcohol required per
      dav = ")
```

#### Scilab code Exa 9.18 Distillation operation for methanol solution

```
xw be the mole fraction of methanol in the fee,
      distillate and the bottom product resp.
4 \text{ xf} = 0.20;
5 \text{ xd} = 0.97;
6 \text{ xw} = 0.02;
7 //using, F = D + W and F*xf + D*xd + W*xw, we get
8 D = 18.95; //kg/h
9 W = 81.05; //kg/h
10 R = 3.5;
11 / R = L / D
12 //for distillate = 1kg
13 D1 = 1; // kg
14 L = R*D1;
15 //Taking balance around the condenser,
16 G = L + D1;
17 mcondensed = G * D / F;
18 disp("kg",D,"(a)Amount of distillate = ")
19 disp("kg",W," Amount of Bottom Product = ")
20 disp("kg",G,"(b) Amount of vapour condensed per kg of
       distillate = ")
21 disp("kg", mcondensed, "(c) Amount of vapour condensed
      per kg of feed = ")
```

#### Scilab code Exa 9.19 Bypass operation

```
9 // humidity of air leaving dehumidifier is Ys2 and
      humidity of bypassed air is Ys1. these 2 streams
      combine to give humidity of 0.03kg water / kg dry
       air.
10 //therefore, taking balance we get, 1*Ys2 + x * Ys1
      = (1 + x) *Ys
11 x = (1*Ys2 - 1*Ys)/(Ys - Ys1);
12 disp("kg dry air",x,"(a) Mass of dry air bypassed per
       kg of dry air sent through the dehumidifier = ")
13 mcondensed = Ys1 - Ys2;
14 mwetair = mdryair + Ys1;
15 Nwetair = mdryair/29 + Ys1/18.016;
16 Vstp = 22.4143; //\text{m}^3/\text{kmol}
17 Vstp1 = Nwetair * Vstp;
18 T = 320; //K
19 P = 101.3; //kPa
20 \text{ Tstp} = 273.15; //K
21 Pstp = 101.325; //kPa
22 V = Vstp1 * Pstp * T / (P * Tstp);
23 Vgiven = 100; //m^3
24 mcondensed1 = mcondensed * Vgiven / V;
25 disp("kg",mcondensed1,"(b)mass of water vapour
      condensed in the dehumidifier per 100m<sup>3</sup> of air
      sent through it = ")
26 \text{ mfinal} = \text{mdryair} + x;
27 mfinalair = mfinal * Vgiven / V;
28 N = mfinalair / 29;
29 Ysn = Ys * \frac{29}{18}; \frac{kmol water}{kmol dry air}
30 \text{ Ntotal} = \text{N} * (\text{Ysn} + 1);
31 Vfinal = Ntotal * Vstp * Pstp * T / ( Tstp * P );
32 disp("m^3", Vfinal, "(c) Volume of final air obtained
      per 100 cubic metres f air passed through
      dehumidifier = ")
```

Scilab code Exa 9.20 Recycle operation centrifuge plus filter

```
1 //clc()
2 F = 100; //kg/h
3 \text{ xf} = 0.2;
4 \text{ xp} = 0.93;
5 \text{ xr} = 0.5/1.5;
6 xx = 0.65;
7 //R - recycle stream, P - Product stream, W - water
       separeted and removed
8 //component A balance, F * xf = P * xp, that is,
9 P = F * xf / xp;
10 // Total balance, F = P + W, therefore
11 W = F - P;
12 //x be the flow rate of strea entering the filter
13 / total balance, x = P + R
                                    (1)
14 //component A balance , 0.65 * x = 0.5*R/1.5 + 0.93P
         (2)
15 //Solving 1 and 2, we get,
16 R = (xx * P - xp * P)/(xr - xx);
17 disp("kg/h",R,"Flow rate of the recycle stream = ")
```

## Scilab code Exa 9.21 Recycle operation granulator and drier

```
1  //clc()
2  F = 1000; //kg/h
3  xfwater = 0.7;
4  xpwater = 0.2;
5  xrwater = 0.20;
6  xswater = 0.5;
7  y1 = 0.0025;
8  y2 = 0.05;
9  //R - recycle, S - stream entering granulator, P - Product, G1 - air entering the drier, G2 - air leaving the drier,
10  //takin overall, moisture free balance, F * xf = P *
```

```
xp
11 P = F * (1 - xfwater)/(1 - xpwater);
12 // taking material balance at point where recycle
     strea joins the feed,
13 // F = R + S
14 //water balance, F*xfwater = R*xrwater + S*xswater,
     solving this we get,
15 R = (-F*xfwater +F*xswater)/(xrwater - xswater);
16 S = F + R;
17 mleaving = P + R; //solid leaving the drier
18 //dry air entering will there be in air leaving,
      therefore
19 / G1 * (1 - y1) = G2 * (1 - y2)
20 // water balance over the drier gives, S*xswater+G1*
     y1=G2*y2+(P+R)*xpwater
21 //from above 2 equations , we get
22 G1 = ((mleaving*xpwater - S*xswater)/(y1 - y2*(1-y1))
     /(1-y2));
23 disp("kg/h",R,"(a)Amount of solid recycled = ")
24 \text{ mdryair} = G1 * (1 - y1);
25 disp("kg/h",mdryair,"(b) circulation rate of air in
     the drier on dry basis = ")
```

#### Scilab code Exa 9.22 Blowdown operation

```
1  // clc()
2  xf = 500 * 10^-6;
3  xp = 50 * 10^-6;
4  xb = 1600 * 10^-6;
5  //F - Feed water rate, B - blow down rate, S - high pressure steam, P - process stream rate
6  // total balance, F = P + B
7  // Solid balance, F * xf + P * xp = B * xb
8  // eliminating P, we get, F * xf + (F - B)*xp = B * xb
```

# Chapter 10

# Material Balance with Chemical Reaction

# Scilab code Exa 10.1 Combustion of propane

```
1 // clc ()
2 \text{ mair} = 500; //kg
3 \text{ mCO2} = 55; //kg
4 \text{ mCO} = 15; //kg
5 / C3H8 + 5O2 = 3CO2 + 4H20
6 \text{ MCO2} = 44;
7 \text{ MCO} = 28;
8 \text{ NCO2} = \text{mCO2} / \text{MCO2};
9 \text{ NCO} = \text{mCO} / \text{MCO};
10 \text{ Mair} = 29;
11 Nair = mair / Mair;
12 //carbon balance gives,
13 F = (NCO2 + NCO)/3;
14 \text{ MC3H8} = 44.064;
15 \text{ mC3H8} = \text{MC3H8} * \text{F};
16 disp("kg", mC3H8,"(a) mass of propane burnt = ")
17 //one mole of propane requres 5 moles of oxygen for
       combustion
18 \text{ NO2} = F * 5;
```

```
19 Nairt = NO2 * 100 /21; // theoretical air required
20 Pexcess = (Nair - Nairt) * 100 / Nairt;
21 disp("\%", Pexcess,"(b) The percent excess air = ")
\frac{1}{22} //C3H8 + \frac{7}{2} * O2 = 3CO + 4H2O
23 \text{ NH2O} = F * 4;
24 //Taking oxygen balance, unburned oxygen is
        calculated,
\frac{25}{\sqrt{02}} supplied = \frac{02}{\sqrt{02}} present in form of \frac{02}{\sqrt{02}}, \frac{02}{\sqrt{02}} and
       H2O + unburned O2
26 \text{ Nunburnt} = \text{Nair} * 21 / 100 - \text{NCO2} - \text{NCO}/2 - \text{NH}20/2;
27 \text{ NN2} = \text{Nair} * 79 / 100;
28 \text{ Ntotal} = \text{NCO2} + \text{NCO} + \text{NH2O} + \text{NN2} + \text{Nunburnt};
29 \text{ PCO2} = \text{NCO2} * 100 / \text{Ntotal};
30 \text{ PCO} = \text{NCO} *100/ \text{Ntotal};
31 \text{ PH20} = \text{NH20} *100/ \text{Ntotal};
32 \text{ PN2} = \text{NN2} *100/ \text{Ntotal};
33 PO2 = Nunburnt *100 / Ntotal;
34 \operatorname{disp}(\%, PCO2, "(c) Percent composition of \operatorname{CO2} = ")
35 disp("\%", PCO, "Percent composition of CO = ")
36 \text{ disp}("\%", PH2O," Percent composition of H2O = ")
37 disp("%",PN2," Percent composition of N2 =")
38 disp("\%", PO2, "Percent composition of O2 =")
```

#### Scilab code Exa 10.2 Combustion of hydrogen free coke

```
1  // clc()
2  Nflue = 100; //kmol
3  NC02 = 14.84;
4  NC0 = 1.65;
5  N02 = 5.16;
6  NN2 = 78.35;
7  PCF = 85; //PERCENT CARBON IN FEED
8  PIF = 15; //PERCENT INERT IN FEED
9  //F - amount of coke charged, W - mass of coke left,
W = 0.05F
```

```
10 NCflue = NCO2 + NCO;
11 \text{ MC} = 12;
12 \text{ mC} = \text{MC} * \text{NCflue};
13 //carbon balance gives, F * PCF / 100 = W * PCF + mC
14 F = mC / (PCF / 100 - 0.05*PCF / 100);
15 //let A kmol air supplied, taking N2 balance,
16 \text{ Nair} = \text{NN2} * 100/79;
17 NO2supplied = Nair - NN2;
18 Ntheoretical = F * PCF / (100 * MC);
19 Pexcess = ( NO2 supplied - N theoretical ) * 100 / (
      Ntheoretical );
20 disp("%", Pexcess,"(a) Percentage excess air = ")
21 mair = Nair * 29;
22 m = mair / F ; //air supplied per kg of coke charged
23 disp("kg",m,"(b) air supplied per kg of coke charged
      = ")
24 P = 100; //kPa
25 T = 500; //K
26 V = Nflue *22.4143*101.325 * T / (F * P * 273.15);
27 disp("m^3", V, "(c) volume of flue gas per kg of coke =
       ")
28 W = 0.05 * F;
29 mCr = W * PCF/100; // carbon in refuse
30 mir = F * (1-PCF/100); //inert in refuse
31 \text{ mr} = \text{mCr} + \text{mir};
32 C = mCr * 100 / mr;
33 I = mir *100/mr;
34 disp("%",C,"(d)Carbon = ")
35 disp("%",I,"Inert = ")
```

# Scilab code Exa 10.3 Combustion of fuel oil

```
1 //clc()
2 Nflue = 100;//kmol
3 NCO2 = 9;
```

```
4 \text{ NCO} = 2;
5 \text{ NO2} = 3;
6 \text{ NN2} = 86;
7 NCflue = NCO2 + NCO;
8 \text{ MC} = 12;
9 \text{ mC} = \text{MC} * \text{NCflue};
10 //let A kmol air supplied, taking N2 balance,
11 Nair = NN2 * 100/79;
12 NO2supplied = Nair - NN2;
13 // if CO in the flue gas was to be completely
      converted to CO2, then, the moles of oxygen
      present in the flue gas would be 3-1 = 2 \text{kmol}
14 \text{ Noexcess} = \text{NO2} - \text{NCO/2};
15 Pexcess = Noexcess * 100 / ( NO2supplied - Noexcess
      );
16 disp("\%", Pexcess,"(a) Percentage excess air = ")
17 Nwater0 = NO2supplied - NCO2 - NCO/2 - NO2;
18 \text{ NH2} = \text{Nwater0*2};
19 \text{ mH2} = \text{NH2} * 2;
20 \text{ xCF} = 0.7
21 R = mC / mH2;
22 disp(R,"(b) Ratio of carbon to hydrogen in the fuel =
23 //let x be the amount of moisture in the feed, n it
       is given that 70% is carbon, therefore,
24 / 0.7 = 3.32 / (1 + 3.32 + x)
25 \times R / \times CF - 1 - R;
26 \text{ mH} = x * 2.016 / 18.016;
27 \text{ mHtotal} = \text{mH} + \text{mH2};
28 Rtotal = mC / mHtotal;
29 disp(Rtotal,"(c) Ratio of carbon to total hydrogen in
        the fuel = ")
30 \text{ ntotal} = R + 1
31 \text{ PH2} = 1*100/\text{ntotal};
32 \text{ PH20} = x * 100 / \text{ntotal};
33 disp("%",PH2,"(d)percentage of combustible hydrogen
      in the fuel = ")
34 disp("%", PH20," percentage of moisture in the fuel =
```

```
")
35 nH2Ototal = (PH2O + PH2 * 18.016 / 2.016)/100;
36 disp("kg",nH2Ototal,"(e)The mass of moisture in the flue gas per kg of fuel burned = ")
```

# Scilab code Exa 10.4 Combustion of producer gas

```
1 //clc()
2 Nflue = 100; //kmoles
3 \text{ NCO2} = 9.05;
4 \text{ NCO} = 1.34;
5 \text{ NO2} = 9.98;
6 \text{ NN2} = 79.63;
7 \text{ PCO2F} = 9.2; //\% \text{ (Feed.)}
8 PCOF = 21.3; //\%
9 PH2F = 18; /\%
10 PCH4F = 2.5; //\%
11 PN2F = 49; /\%
12 // Taking carbon balance,
13 F = (NCO2 + NCO) / ((PCO2F + PCOF + PCH4F) / 100);
14 // Nitrogen balance gives,
15 Nair = (NN2 - F*PN2F/(100))*100 / 79;
16 R = Nair/F;
17 disp(R,"(a) molar Ratio of air to fuel = ")
18 Oexcess = NO2 - NCO / 2;
19 Pexcess = 0 = x = 100/ (Nair*21/100 - 0 = x = 100);
20 disp("%", Pexcess,"(b) Percent excess of air = ")
21 \text{ NN2F} = F * PN2F / 100;
22 \text{ PN2F} = \text{NN2F} *100/ \text{NN2};
23 disp("%", PN2F, "(c) Percent of nitrogen in the flue
      gas that came from fuel = ")
```

Scilab code Exa 10.5 Combustion of coal

```
1 //clc()
2 Nflue = 100; //kmole
3 \text{ NCO2} = 16.4;
4 \text{ NCO} = 0.4;
5 \text{ NO2} = 2.3;
6 \text{ NN2} = 80.9;
7 PCF = 80.5; //\% ( Feed )
8 \text{ PO} = 5.0; //\%
9 PHF = 4.6; //\%
10 PN = 1.1; //\%
11 Pash = 8.8; //\%
12 // Taking Carbon balance,
13 W = (NCO2 + NCO)*12 / (PCF / 100);
14 \text{ mCO2} = \text{NCO2} * 44;
15 \text{ mCO} = \text{NCO} * 32;
16 \text{ mO2} = \text{NO2} * 28;
17 \text{ mN2} = \text{NN2} * 28.014;
18 \text{ mtotal} = \text{mCO2} + \text{mCO} + \text{mO2} + \text{mN2};
19 Mdryflue = mtotal * 100/ W;
20 disp("kg", Mdryflue,"(a) The weight of dry gaseous
       products formed per 100 kg of coal fired = ")
21 //taking nitrogen balance,
22 \times = (mN2 - W*PN/100)/28.014;
23 Noxygen = x * 21 / 79;
24 Nrequired = W * (PCF /12 + PHF/(2*2.016) - PO/32)
       /100;
25 Pexcess = (Noxygen - Nrequired)*100/Nrequired ;
26 disp("%", Pexcess," (b) Percent excess air supplied for
        combustion = ")
```

Scilab code Exa 10.6 Stoichiometric analysis of combustion of coal

```
1 //clc()
2 mcoal = 100;//kg
3 mC = 63;//kg
```

```
4 \text{ mH} = 12; //\text{kg}
5 \text{ mO} = 16; //\text{kg}
6 mash =9; //kg
7 mfixC = 39; //kg
8 \text{ mH20} = 10; //\text{kg}
9 mCvolatile = mC - mfixC;
10 mHH20 = mH20 *2.016/18.016; // (mass of hydrogen in
      moisture)
11 mHvolatile = mH - mHH20;
12 \text{ mOH2O} = \text{mH2O} - \text{mHH2O};
13 mOvolatile = mO - mOH2O;
14 mtvolatile = mCvolatile + mHvolatile + mOvolatile;
15 PC = mCvolatile * 100 / mtvolatile;
16 PH = mHvolatile * 100 / mtvolatile;
17 PO = mOvolatile * 100 / mtvolatile;
18 disp("%", PC, "(a) percent carbon in volatile matter =
19 disp("%",PH," percent hydrogen in volatile matter
      = ")
20 disp("%",PO," percent oxygen in volatile matter =
21 PCflue = 10.8; //\%
22 Pvflue = 9.0; //\%
23 Pashflue = 80.2; //\%
24 //taking ash balance, Wis the weight of the refuse,
25 W = mash *100 / Pashflue;
26 \text{ mvflue} = \text{Pvflue} * \text{W} / 100;
27 \text{ mCflue} = W * PCflue / 100;
28 Ctflue = mCflue + mvflue * PC / 100; // total carbon
      in flue
29 Htflue = mvflue * PH / 100;
30 Otflue = mvflue * PO / 100;
31 PCflue = Ctflue *100/W;
32 PHflue = Htflue *100/W;
33 POflue = Otflue *100/W;
34 disp("%", PCflue, "(b) percent Carbon in refuse = ")
35 disp("%",PHflue," percent Hydrogen in refuse = ")
36 disp("%", POflue," percent Oxygen in refuse = ")
```

```
37 disp("%", Pashflue," percent Ash in refuse = ")
38 Coalburnt = mcoal - W;
39 NCburnt = (mC - Ctflue)/12;
40 NHburnt = (mH - Htflue)/2.016;
41 NOburnt = (mO - Otflue)/32;
42 PCO2 = 80; // Percentage of carbon burnt
43 \text{ NCO2} = \text{PCO2} * \text{NCburnt} / 100;
44 \text{ NCO} = (1 - PCO2/100) * NCburnt;
45 Vair = 1000; //m^3
46 Nair = Vair / 22.4143;
47 \text{ NN2} = \text{Nair} * 79 / 100;
48 \text{ NO2} = \text{Nair} * 21 / 100;
49 Ocompounds = NCO2 + NCO/2 + NHburnt/2; //Oxygen
       present in CO2, CO and H2O
50 //Oxygen balance gives free oxygen as,
51 Ofree = NO2 + mO/32 - Otflue/32 - Ocompounds;
52 Ntotal = NN2 + Ofree + NCO2 + NCO; //dry basis
53 \text{ PCO21} = \text{NCO2} *100/\text{Ntotal};
54 \text{ PCO1} = \text{NCO} * 100/\text{Ntotal};
55 \text{ PO21} = \text{Ofree} * 100/\text{Ntotal};
56 \text{ PN21} = \text{NN2} * 100/\text{Ntotal};
57 disp("\%", PCO21,"(c) percent CO2 in flue = ")
                      percent CO in flue = ")
58 disp("%", PCO1,"
59 disp("%", PO21,"
                       percent O2 in flue = ")
                      percent N2 in flue = ")
60 \operatorname{disp}("\%", \operatorname{PN21},")
61 NOrequired = mC/12 + mH/(2.016*2) - mO/32;
62 Oexcess = NO2 - NOrequired;
63 Pexcess = Oexcess * 100 / NOrequired;
64 disp("%", Pexcess," (d) Percent excess air supplied = "
      )
65 NH2Oflue = NHburnt;
66 \text{ mH2O} = \text{NH2Oflue} * 18.016;
67 m = mH20 * 100/Ntotal;
68 disp("g water vapour / 100kmol dry flue gas", m, "(e)
      mass of water vapour per 100 moles of dry flue
      gas = ")
```

#### Scilab code Exa 10.7 Orsat analysis

```
1 //clc()
2 Pexcess = 20; //\%
3 PSO3 = 5; //\% ( Percent of sulphur burnt to SO3 )
4 //S + O2 = SO2
5 N = 1; //kmol sulphur
6 Orequired = N; //kmol
7 Osupplied = Orequired * ( 1 + Pexcess/100);
8 Nsupplied = Osupplied * 79/21;
9 \text{ NSO2} = (1-PSO3/100)*N;
10 \text{ NSO3} = \text{PSO3} * \text{N} / 100;
11 Oconsumed = NSO2 + 3/2 * PSO3/100;
12 Oremaining = Osupplied - Oconsumed;
13 Ntotal = NSO2 + NSO3 + Oremaining + Nsupplied;
14 \text{ PSO2} = \text{NSO2} * 100 / \text{Ntotal};
15 \text{ PSO3} = \text{NSO3} * 100 / \text{Ntotal};
16 PO2 = Oremaining * 100 / Ntotal;
17 PN2 = Nsupplied * 100 / Ntotal;
18 disp("%", PSO2, "Percent SO2 in burner gas = ")
19 disp("%", PSO3, "Percent SO3 in burner gas = ")
20 disp("%", PO2, "Percent O2 in burner gas = ")
21 disp("%", PN2, "Percent N2 in burner gas = ")
```

# Scilab code Exa 10.8 Burning of pyrites

```
1 // clc()
2 Nburner = 100; //kmol
3 NSO2b = 9.5; //kmol
4 NO2b = 7; //kmol
5 NN2 = Nburner - NSO2b - NO2b;
6 NOsupplied = NN2 * 21 / 79; //Oxygen supplied
```

```
7 //4 \text{FeS}2 + 1102 = 2 \text{Fe}203 + 8 \text{SO}2
8 / 4 \text{FeS}_2 + 1502 = 2 \text{Fe}_2 + 8 \text{SO}_3
9 \text{ NOtotal} = \text{NO2b} + \text{NSO2b} + \text{NSO2b} * 3 / 8;
10 NOunaccounted = NOsupplied - NOtotal;
11 NSO31 = NOunaccounted * 8 /15;
12 NStotal = NSO2b + NSO31;
13 \text{ mS} = \text{NStotal} * 32.064;
14 Pburnt = 50; //\% ( percentage of pyrites burnt )
15 \text{ mFeS2} = \text{mS} * 100/ Pburnt;
16 disp("kg", mFeS2, "(a) Total pyrites burnt = ")
17 NFeS2 = NStotal / 2;
18 \text{ MFeS2} = 119.975;
19 mFeS21 = MFeS2 * NFeS2;
20 mgangue = mFeS2 - mFeS21;
21 NFe203 = NFeS2 * Pburnt / 100;
22 \text{ MFe} 203 = 159.694;
23 \text{ mFe} 203 = \text{MFe} 203 * \text{NFe} 203;
24 PSO3c = 2.5; //\% ( percentage sulphur as SO3 in
       cinder )
25 \text{ mc} = 100; //\text{kg} \text{ (basis)}
26 \text{ NSO3} = \text{PSO3c} / 32.064;
27 \text{ mSO3} = \text{NSO3} * 80.064;
28 mremaining = mc - mSO3; // (Fe2O3 + gangue)
29 //x be the weight of the cinder
30 x = (mFe203 + mgangue)*100/mremaining;
31 disp("kg",x,"(b)) weight of cinder produced = ")
32 \text{ Slost} = x * NSO3 / 100;
33 PSlost = Slost *100/ NStotal;
34 disp("%", PSlost,"(c) Percent of total S lost in the
       cinder = ")
35 \text{ mSO3c} = \text{mSO3} * x / 100;
36 \text{ NSO3b} = \text{NSO31} - \text{Slost};
37 P = NSO3b * 100 / NStotal;
38 disp("%",P,"(d) Percentage of S charged that is
       present as SO3 in the burner gas = ")
```

# Scilab code Exa 10.9 Production of sulphuric acid

```
1 //clc()
2 Ncgas = 100; //kmol ( basis - SO3 free converter gas
3 \text{ NSO2} = 4.5; //\text{kmol}
4 \text{ NO2} = 7.5; //\text{kmol}
5 \text{ NN2} = 88.0; //\text{kmol}
6 \text{ NOsupplied} = \text{NN2} * 21/79;
7 NOconverter = NO2 + NSO2;
8 NOconsumed = NOsupplied - NOconverter; // (Oxygen
       consumed for SO3)
9 \text{ NSO3c} = \text{NOconsumed} / 1.5;
10 NStotal = NSO3c + NSO2;
11 Nbgas = 100; //kmol ( basis - SO3 free burner gas )
12 NSO21 = 15; //\%
13 NO21 = 5; //\%
14 \text{ NN21} = 80; /\%
15 NOburner = NO21 + NSO21;
16 \text{ NOsupplied1} = \text{NN21} * 21 / 79;
17 NOconsumed1 = NOsupplied1 - NOburner; // (Oxygen
       consumed for SO3)
18 \text{ NSO3b} = \text{NOconsumed1} / 1.5;
19 \text{ NStotal1} = \text{NSO3b} + \text{NSO21};
20 mS = 100; //kg ( basis - sulphur charged )
21 Pburned = 95; //\%
22 mburned = mS * Pburned / 100;
23 Nburned = mburned / 32.064;
24 //let x be the SO3 free burner gas produced, then
       sulphur balance gives,
25 \times = Nburned * Nbgas / NStotal1;
26 \text{ NSO2b} = \text{NSO21} * x / 100;
27 \text{ NO2b} = \text{NO21} * x / 100;
28 \text{ NN2b} = \text{NN21} * x / 100;
```

```
29 \text{ Ntotalb} = \text{NSO2b} + \text{NO2b} + \text{NN2b};
30 \text{ NSO3b1} = \text{NSO3b} * x / 100;
31 //let y be the no. of converter gas produced
32 y = Nburned * Ncgas / NStotal;
33 \text{ NSO2c} = \text{NSO2} * \text{y} / 100;
34 \text{ NO2c} = \text{NO2} * \text{y} / 100;
35 \text{ NN2c} = \text{NN2} * \text{y} / 100;
36 Ntotalc = NSO2c + NO2c + NN2c;
37 \text{ NSO3c1} = \text{NSO3c} * y / 100;
38 \text{ Nairsec} = (NN2c - NN2b) * 100 / 79;
39 P = 100; //kPa
40 T = 300; //K
41 V = Nairsec * 22.414 * 101.3 * T / (P * 273.15);
42 disp("m^3/h", V, "(a) The volume of secondary air at
       100 \, \text{kPa} and 300 \, \text{K} = ")
43 NSabsorbed = 95; //\%
44 \text{ mSO3abs} = \text{NSabsorbed} * \text{NSO3c1} * 80.064 / 100;
45 //let z be the amount of 98% H2SO4, therefore , 100\%
        H2SO4 produced = z + mSO3abs
46 // taking SO3 balance
47 z = (mSO3abs - mSO3abs * 80.064 / 98.08) / (80.064)
       /98.08 - 0.98 * 80.064/98.08);
48 disp("kg",z,"(b) 98\% H2SO4 required per hour = ")
49 \text{ w} = \text{z} + \text{mSO3abs};
50 disp("kg", w, "(c) 100\% H2SO4 produced per hour = ")
```

Scilab code Exa 10.10 Burning of limestone mixed with coke

```
1 // clc()
2 mlime = 5; //kg
3 mcoke = 1; //kg
4 PCaCO31 = 84.5; //%
5 PMgCO31 = 11.5; //%
6 NCaCO31 = PCaCO31 * mlime / (100.09*100);
7 NMgCO31 = PMgCO31 * mlime / (84.312*100);
```

```
8 mInertsl = mlime * ( 100 - PCaCO31 - PMgCO31 ) /
       100;
9 PCc = 76; //\%
10 Pashc = 21; //\%
11 Pwaterc = 3; //\%
12 NCc = mcoke * PCc /(100*12);
13 Nwaterc = mcoke * Pwaterc / ( 100 * 18.016 );
14 \text{ mash} = \text{Pashc} * \text{mcoke} / 100;
15 / \text{CaCO3} + \text{C} + \text{O2} = \text{CaO} + 2\text{CO2}
16 / MgCO3 + C + O2 = MgO + 2CO2
17 PCaCO3conv = 95; //(Percent calcination of CaCO3)
18 PMgCO3conv = 90; //(Percent calcination of MgCO3)
19 NCaO = PCaCO3conv * NCaCO31 / 100;
20 \text{ mCaO} = \text{NCaO} * 56.08;
21 \text{ NMgO} = \text{PMgCO3conv} * \text{NMgCO3l} / 100;
22 \text{ mMgO} = \text{NMgO} * 40.312;
23 \text{ mCaCO3} = (NCaCO31 * (1-PCaCO3conv/100)*100.09);
24 \text{ mMgCO3} = (NMgCO31 * (1-PMgCO3conv/100)*84.312);
25 mtotal = mCaO + mMgO + mCaCO3 + mMgCO3 + mInertsl +
      mash;
26 \text{ PCaO} = \text{mCaO} * 100 / \text{mtotal};
27 disp("%", PCaO, "The weight percent of CaO in the
       product leaving the kiln = ")
```

#### Scilab code Exa 10.11 treating limestone with aqueous H2SO4

```
1 //clc()
2 R = 100; //kg ( basis - residue )
3 MCaSO4 = 136.144;
4 MMgSO4 = 120.376;
5 mCaSO4r = 9; //kg
6 mMgSO4r = 5; //kg
7 mH2SO4r = 1.2; //kg
8 minertr = 0.5; //kg
9 mCO2r = 0.2; //kg
```

```
10 \text{ mH} 20 = 84.10; //kg
11 \text{ NCaSO4} = \text{mCaSO4r} / \text{MCaSO4};
12 \text{ NMgSO4} = \text{mMgSO4r} / \text{MMgSO4};
13 / \text{CaCO3} + \text{H2SO4} = \text{CaSO4} + \text{H2O} + \text{CO2}
14 / MgSO4 + H2SO4 = MgSO4 + H2O + CO2
15 \text{ mCaCO3} = \text{NCaSO4} * 100.08;
16 \text{ mMgCO3} = \text{NMgSO4} * 84.312;
17 mtotallime = minertr + mCaCO3 + mMgCO3;
18 PCaCO3 = mCaCO3 * 100/ mtotallime;
19 PMgCO3 = mMgCO3 *100/ mtotallime;
20 Pinerts = minertr *100/ mtotallime;
21 disp("%", PCaCO3,"(a) Percentage of CaCO3 in limestone
       = ")
22 disp("%", PMgCO3," Percentage of MgCO3 in limestone
       = ")
23 disp("%",Pinerts,"
                             Percentage of inerts in
      limestone = ")
24 \text{ NH}2SO4 = NCaSO4 + NMgSO4;}
25 \text{ mH}2SO4 = NH2SO4 * 98.08;
26 \text{ Pexcess} = \text{mH2SO4r} * 100 / ( \text{mH2SO4});
27 disp("%", Pexcess," (b) The percentage excess of acid
      used = ")
28 \text{ macidt} = \text{mH2SO4} + \text{mH2SO4r};
29 Pacidic = 12; //\%
30 mwaterin = macidt * (100 - Pacidic)/ Pacidic;
31 mwaterr = (NCaSO4 + NMgSO4)*18.016;
32 mwatert = mwaterin + mwaterr;
33 mvaporized = mwatert - mH20;
34 m = mvaporized * 100/mtotallime;//water vaporized
      per 100kg of limestone
35 disp("kg",m,"(c)the mass of water vaporized per 100
      kg 	ext{ of } limestone = ")
36 \text{ mCO2pr} = (NCaSO4 + NMgSO4)*44;
37 \text{ mCO2rel} = \text{mCO2pr} - \text{mCO2r};
38 m1 = mCO2rel * 100 / mtotallime; //CO2 per 100 \,\mathrm{kg} of
      limestone
39 disp("kg",m1,"(d)the mass of CO2 per 100kg of
      limestone = ")
```

#### Scilab code Exa 10.12 Production of TSP

```
1 //clc()
2 macid = 1000; //kg ( basis - dilute phosphoric acid )
3 \text{ Mphacid} = 97.998;
4 P = 1.25; //\% ( dilute % )
5 mphacid = macid * P / 100;
6 Nphacid = mphacid / Mphacid;
7 //1mole of phosphoric acid - 1mole of trisodium
      phosphate
8 NTSP = Nphacid;
9 \text{ MTSP} = 380.166;
10 \text{ mTSP} = \text{NTSP} * \text{MTSP};
11 disp("kg", mTSP, "(a) Maximum weight of TSP obtained =
      ")
12 \text{ NCO2} = \text{NTSP};
13 Pwater = 6.27//kPa
14 //since gas is saturated with water vapour, vapour
      pressure = partial pressure
15 Nwater = NCO2 * Pwater / (100 - Pwater);
16 Ntotal = Nwater + NCO2;
17 P = 100; //kPa
18 T = 310; //K
19 V = Ntotal * 101.3 * T *22.4143 / ( P * 273.15 );
20 disp("m^3", V, "(b)) Volume of CO2 = ")
```

## Scilab code Exa 10.13 Production of sodium phosphate

```
1 //clc()
2 mTSPd = 1000;//kg ( basis - 20% dilute TSP )
3 P = 20;//%
```

```
4 \text{ mTSP} = \text{mTSPd} * P / 100;
5 \text{ NTSP} = \text{mTSP} / 163.974;
6 \text{ msodaashd} = \text{NTSP} * 106;
7 \text{ mphacidd} = \text{NTSP} * 97.998;
8 \text{ mNaOHd} = \text{NTSP} * 40.008;
9 Pphacid = 85; //\% (85% solution phosphoric acid)
10 PNaOH = 50; //\% (50% solution NaOH)
11 //let x be the water in soda ash,
12 //taking water balance,
13 x = (mTSPd - mTSP) - mNaOHd * PNaOH /(100 - PNaOH) -
       mphacidd * (100 - Pphacid) / Pphacid;
14 \mod a sh = msodaashd + x;
15 C = msodaashd *100 / msodaash;
16 disp("%", C, "(a) Concentration of soda ash solution =
17 mphacid = mphacidd * 100 / Pphacid;
18 R = msodaash / mphacid;
19 disp(R,"(b) Weight ratio in which soda ash and
      commercial phosphoric acid are mixed = ")
```

#### Scilab code Exa 10.14 Production of pig iron

```
1 //clc()
2 m = 1000; //kg ( basis - pig iron produced )
3 //let x be the iron ore charged and y be the amount
    of flux added and z be the weight of slag
    produced
4 PFepg = 95; //% ( Fe% in product )
5 PCpg = 4; //%
6 PSipg = 1; //%
7 PFech = 85; //% (Fe% in feed )
8 mcoke = 1000; //kg
9 PCcoke = 90; //%
10 PSicoke = 10; //%
11 PSislag = 60; //%
```

```
12 PSiflux = 5; //\%
13 PCaCO3fx = 90; //\%
14 PMgCO3fx = 5; //\%
15 PCMslag = 40; //\%
16 //iron balance gives,
17 x = PFepg * m *159.694 / (PFech * 111.694);
18 //silicon balance gives,
19 / x*(100 - PFech)*28.086/(100*60.086)+mcoke*Psicoke
      *28.086/(100*60.086)+y*PSiflux
      *28.086/(100*60.086) = 10 + z*Psislag*28.086 / (
      100*60.086
20 / \text{taking} (CaO + MgO) balance
21 //y * ((PCaCO3fx) *56.88/(100*100.88) + (PMgCO3fx)
      *40.312/(100*84.312) = z * PCMslag / 100
22 //solving above 2 equations, we get
23 y = 403.31;
24 disp("kg",y,"the amount of flux required to produce
      1000 \,\mathrm{kg} of pig iron = ")
```

#### Scilab code Exa 10.15 Production of nitric acid

```
12 //Total oxygen used up, O = NNOreac * 5/4 + x*3/2
13 //total oxygen supplied, NOtotal= (O) + NO2s
14 // Nitrogen associated with O2 supplied NN2 = NOtotal
      *79/21 - (2)
15 //comparing 1 and 2,
16 x = 2.1835;
17 //12 moles NO requires 12 moles ammonia, 1 mole N2
      requires 2 mole ammonia
18 Nammonia = x*2 + NNOreac;
19 Oreq = Nammonia * 5 / 4;
20 Osupp = NNOreac * 5/4 + x*3/2 + NO2s;
21 \text{ Pexcess} = (Osupp - Oreq)*100/Oreq;
22 disp("%", Pexcess,"(a) Percentage excess oxygen = ")
23 	ext{ fr = x * 2 / Nammonia;}
24 disp(fr, "Fraction of ammonia taking part in side
      reaction = ")
```

#### Scilab code Exa 10.16 Material balance in nitric acid production

```
1 //clc()
2 m = 100; //kg (basis sodium nitrate reacted)
3 NNaNO3 = m/85;
4 //2NaNO3 + H2SO4 = 2HNO3 + Na2SO4
5 mh2so4 = NNaNO3 * 98.08/2;
6 mhno3 = NNaNO3*63.008;
7 mna2so4 = NNaNO3 * 142.064 /2;
8 Phno3 = 2; //%(percent nitric acid remaining in the cake)
9 mhno3cake = mhno3 * Phno3 / 100;
10 Ph2so4 = 35; //%
11 Pwater = 1.5; //%
12 mtotal = (mna2so4 + mhno3cake)*100/(100 - Ph2so4 - Pwater);
13 mwater = Pwater * mtotal / 100;
14 mh2so4c = Ph2so4 * mtotal / 100;
```

```
15 \text{ Pna2so4} = \text{mna2so4} *100/\text{mtotal};
16 Phno3c = mhno3cake * 100 / mtotal;
17 disp("kg", mna2so4,"(a) Mass of Na2SO4 in the cake = "
18 disp("kg", mhno3, "Mass of HNO3 in the cake = ")
19 disp("kg", mwater, "Mass of water in the cake = ")
20 disp("kg", mh2so4c, "Mass of H2SO4 in the cake = ")
21 disp("\%", Pna2so4," Percentage of Na2SO4 in the cake =
22 disp("%", Phno3c," Percentage of HNO3 in the cake = ")
23 disp("%", Pwater, "Percentage of water in the cake = "
24 disp("%", Ph2so4, "Percentage of H2SO4 in the cake = "
25 \text{ mh}2\text{so}4\text{req} = \text{mh}2\text{so}4 + \text{mh}2\text{so}4\text{c};
26 P = 95; //\% (95% dilute sulphuric acid)
27 w = mh2so4req * 100 / P;
28 \quad disp(mh2so4)
29 disp("kg",w,"(b) Weight of 95% sulphuric acid
      required = ")
30 mnitric = mhno3 - mhno3cake;
31 disp("kg",mnitric,"(c)weight of nitric acid product
      obtained = ")
32 mwaterd = w*(1-P/100)-mwater;
33 disp("kg", mwaterd,"(d)) the water vapour tha tis
      distilled from the nitre cake = ")
```

#### Scilab code Exa 10.17 Electrolysis of brine

```
1 //clc()

2 m = 50; //kg ( basis - mass of brine charged )

3 //let x be the amount of NaCl in the brine

4 Pelect = 50; //% ( electrolyzed )

5 //2NaCl + 2H2O = 2NaOH + Cl2 + H2

6 //amount of NaCl reacted =x*Pelect/(100*58.45)kmol=x
```

```
*Pelect/100 kg (1)
7 //amount of water reacted = x * Pelect * 18.016 / (
      100 * 58.45 ) kg ( 2 )
8 //Gases produced, Cl2 = x * Pelect / (100 * 58.45 *
      2 \text{ }) \text{ kmol} = x * \text{ Pelect } *71/ (100 * 58.45 * 2) \text{ kg}
9 / H2 = x * Pelect / (100 * 58.45 * 2) kmol = x *
      Pelect *2.016/(100 * 58.45 * 2) kg
      (4)
10 Nwater = 0.03; //mol water vapour/mol of gas
11 //water vapour present = Nwater * 2*(C12 + H2)kmol =
       Nwater * 2*(Cl2 + H2)*18.016 kg
      (5)
12 / \text{NaoH} = x * \text{Pelect} * 40.008 / (100 * 58.45) \text{ kg}
                               (6)
13 //water = water in brine - water reacted - water
      present in gas
                       (7)
14 //= (m - Pelect/100) - water reacted (2) - water
      present in the gas (5)
15 // \text{Total weight of solution} = \text{NaCl } (1) + \text{NaOH } (6)
       + Water (7)
16 //since NaOH is 10 percent of the total weight, we
      have NaOH = 0.1 * total weight, from these we get
17 x = 0.1 * 50 / (0.1* 0.3165 + 0.3422);
18 NaOH = x * Pelect * 40.008/ (100 * 58.45);
19 NaCl = x * Pelect / 100;
20 water = 34.5032; //kg
21 Pevap = 50; //NaOh percentage in solution leaving
      evaporator
22 //taking NaOH balance
23 \text{ mevap} = \text{NaOH} * 100 / \text{Pevap};
24 \operatorname{disp}("kg", \operatorname{mevap},"(a) \operatorname{amount} \text{ of } 50\% \operatorname{NaOH} \text{ solution}
      produced = ")
25 Cl2 = x * Pelect *71/ (100 * 58.45 * 2 ); // kg
26 \text{ H2} = x * \text{Pelect} *2.016/ (100 * 58.45 * 2); //kg
```

```
disp("kg",Cl2,"(b)Chlorine produced = ")
disp("kg",H2," Hydrogen produced = ")
Pleav = 1.5;//% NaCl leaving the evaporator
NaClleav = mevap * Pleav / 100;
mcrystal = NaCl - NaClleav;
disp("kg/h",mcrystal,"(c)Amount of NaCl crystallized = ")
mwaterleav = mevap - NaOH - NaClleav;
Mwaterevap = water - mwaterleav;
disp("kg",Mwaterevap,"(d)Weight of water evaporated = ")
```

## Scilab code Exa 10.18 Preparation of Formaldehyde

```
1 //clc()
2 m = 100; //mol (basis reactore exit gas)
3 / CH3OH + O2 = HCOOH + H2O
4 / CH3OH + O2 / 2 = HCHO + H2O
5 \text{ Nn2} = 64.49; //\text{mol}
6 \text{ No2} = 13.88; //\text{mol}
7 \text{ Nh2o} = 5.31; // \text{mol}
8 \text{ Nch3oh} = 11.02; //mol
9 Nhcho = 4.08; //mol
10 Nhcooh = 1.22; //mol
11 //x be the moles of methanol reacted, taking C
      balance, we get,
12 x = Nch3oh + Nhcho + Nhcooh;
13 Pconv = Nhcho * 100 / x ;
14 disp("%", Pconv," (a) Percent conversion of
      formaldehyde = ")
15 Nair = Nn2 * 100 / 79;
16 R = Nair / x;
17 disp(R,"(b) Ratio of air to methanol in the feed = ")
```

Scilab code Exa 10.19 Recycle operation reactor and separator

```
1 //clc()
2 NA = 100; //mol (basi - 100 mol A in the fresh feed
3 Pconv = 95; //\%
4 \text{ NApro} = \text{NA} * (100 - Pconv)/100;
5 / A = 2B + C
6 \text{ NB} = \text{NA} * \text{Pconv} * 2 / 100;
7 \text{ NC} = \text{NA} * \text{Pconv}/100;
8 PAent = 0.5; //\%
9 NAent = NApro * 100 / PAent;
10 PBrec = 1; //\%
11 NBent = NB * 100 / (100 - PBrec);
12 m = (NAent - NApro + NA);
13 conv = ((NAent - NApro + NA) - NAent)*100/(NAent -
       NApro + NA);
14 \operatorname{disp}("\%", \operatorname{conv},"(a) \operatorname{single} \operatorname{pass} \operatorname{converion} = ")
15 Nrecycled = (NAent - NApro) + (NBent - NB);
16 R = Nrecycled/NA;
17 disp(R,"(b)) recycle ratio = ")
```

Scilab code Exa 10.20 Conversion of sugar to glucose and fructose

```
1 //clc()
2 m = 100;//kg ( basis - sucrose solution as fresh feed )
3 //R - recycle reactor exit, let x be the weight fraction of sucrose and y be the weight fracton of inversion sugar in the recycle stream, for combined stream fraction of Glucose + fructose = 0.04
```

```
4 //z be the weight fraction of sucrose in the
     combined stream entering the reactor
5 Psfeed = 25; //\% percent sucrose in fresh feed
6 //sucrose balance gives, 25 + R*x = (100+R)*z
                              (A)
7 //Glucose + fructose balance, R * y = (100 + R)
      *0.04
                             (B)
8 Sucrosecon = 71.7; //\% sucrose consumed
  //sucrose balance around the reactor, (100+R)z
      =0.717*(100+R)z+(100+R)x (C)
10 / \text{From (C)}, x = 0.283 * z
                                                     (D)
11 //Amount converted to Glucose + fructose = 0.717 (
      100 + R) * z
12 // = 0.717 (100 + R) * z * 360.192 / 342.176 kg
13 //Glucose and fructose balance around the reactor,
14 / (100 + R) *0.04 + 0.717(100 + R) *z *360.192/342.176 =
      (100+R)*y
15 //Solving (E), y = 0.04 + 0.7548*z
                                          (F)
16 //Solving, (A), (B), (C) and (F)
17 x = 0.06;
18 y = 0.2;
19 z = 0.212;
20 R = 25;
21 disp("kg",R,"(a) Recycle flow = ")
22 disp("%",y*100,"(b)Combined concentration of Glucose
       and Fructose in the recycle stream = ")
```

## Scilab code Exa 10.21 Purging operation

```
1 //clc()

2 N = 1;//mol ( basis - combined feed )

3 //F - moles of fresh feed

4 Pinert = 0.5;//%
```

```
5 Pconv = 60; //\%
6 P1inert = 2; //\%
7 \text{ NA1} = \text{N} * (1 - \text{Plinert}/100);
8 \text{ NA2} = \text{NA1} * (1 - \text{Pconv} / 100);
9 \text{ NB2} = \text{NA1} - \text{NA2};
10 N1inert = N * P1inert / 100;
11 N2inert = N1inert;
12 //Let R be the moles recycled and P be the moles
      purged
13 / W = R + P
14 W = NA2 + N2inert; //
      (A)
15 PWinert = N2inert * 100/ ( NA2 + N2inert);
16 //component A balance, A fresh feed = A purge stream
       + A recycle stream
17 / F * 0.9 = P * 0.9515 + 0.588
      (B)
18 //inert balance at the point where fresh feed is
      mixed with the recycle,
19 / F*0.005 + R*0.0485 = 1*0.02
      (\mathbf{C})
20 // Solving (A), (B) and (C)
21 F = 0.6552; //mol
22 P = 0.0671; //mol
23 R = 0.3448; //mol
24 disp("mol",R,"(a) moles of recycle stream = ")
25 disp("mol",P,"(b)moles of purge stream = ")
26 \text{ NAconv} = \text{NA1} - \text{NA2};
27 \text{ NAf} = F * (1 - Pinert / 100);
28 \text{ Conv} = \text{NAconv} *100/ \text{NAf};
29 disp("%", Conv, "(c) Overall conversion = ")
```

Scilab code Exa 10.22 Purging operation for production of methanol

```
1 //clc()
```

```
2 N = 100; //moles (Basis - Fresh feed)
3 Pconv = 20; //\%
4 \text{ xco} = 0.33;
5 \text{ xh2} = 0.665;
6 \text{ xch4} = 0.005;
7 / R - recycle stream, P - purge stream
8 //x - mole fraction of CO in recycle stream,
9 \text{ xch4r} = 0.03;
10 / CO = x, H2 = 1 - xch4r - CO = 0.97 - x;
11 //methane balance over the entire system,
12 P = xch4 * N / xch4r;
13 //taking caron balance, 33.5 = M + P (0.03 + x)
14 //Hydrogen balance, 66.5 + 2*0.5 = 2M + P(2*0.03 +
      0.97 - x
15 //substituting P, M + 16.67x = 33.0 and 2M - 16.67x
      = 50.33
16 M = (33.0 + 50.33)/3;
17 x = ((xco + xch4)*N - M) / P - xch4r;
18 //methanol balance, (xco*N+Rx) * Poncv/100 = M
19 R = (M*100 / Pconv - (xco*N))/x;
20 disp("mol",R,"(a)moles of recycle stream = ")
21 disp("mol", P, "(b) moles of purge stream = ")
22 \text{ H2} = 1 - \text{xch4r} - \text{x};
23 disp("\%",xch4r*100,"(c)CH4 in purge stream = ")
24 disp("\%",x*100,"CO in purge stream = ")
25 disp("\%", H2*100," hydrogen in purge stream = ")
26 disp("mol", M, "(d) Methanol produced = ")
```

# Chapter 11

# **Energy Balance Thermophysics**

### Scilab code Exa 11.1 Power calculation

```
1 //clc()
2 m = 75; //kg
3 g = 9.81//m^2/s
4 d = 10; //m
5 t = 2.5*60; //s
6 f = m*g;
7 w = f * d;
8 P = w / t;
9 disp("Nm", w, "The work done = ")
10 disp("W", P, "Power required = ")
```

### Scilab code Exa 11.2 Kinetic energy calculation

```
1 //clc()
2 PE = 1.5*10^3; //J
3 m = 10; //kg
4 g = 9.81; //m/s^2
5 v = 50; //m/s
```

```
6 //PE = mgz
7 z = PE / (m*g);
8 KE = m* (v^2) / 2;
9 disp("m",z," Height of the body from the ground = ")
10 disp("kJ", KE/1000, "Kinetic energy of the body = ")
```

Scilab code Exa 11.3 Work done calculation for a gas confined in a cylinder

```
1 //clc()
2 d = 100 /1000; //m
3 m = 50; //kg
4 P = 1.01325*10^5; //Pa
5 A = %pi * (d^2)/4;
6 Fatm = P * A;
7 Fwt = m * g;
8 Ftotal = Fatm + Fwt;
9 P = Ftotal / A;
10 disp("bar", P/10^5,"(a) Pressure of the gas = ")
11 z = 500/1000; //m
12 w = Ftotal * z;
13 disp("J",w,"(b) Work done by the gas = ")
```

### Scilab code Exa 11.4 Power requirement of the pump

```
1 //clc()
2 Sgr = 0.879;
3 F = 5; //m^3/h
4 D = Sgr * 1000;
5 m = F * D/3600; //kg/s
6 P = 3500; //kPa
7 W = P * m * 1000/ D;
8 disp("W", W," Power requirement for the pump = ")
```

Scilab code Exa 11.5 Specific enthalpy of the fluid in the tank

```
1 //clc()
2 d = 3;//m
3 m = 12500;//kg
4 P = 7000;//kPa
5 U = 5.3*10^6;//kJ
6 Vtank = 4*%pi*((d/2)^3) / 3;
7 Vliq = Vtank / 2;
8 H = U + P * Vliq;
9 disp("kJ/kg", H/m," Specific enthalpy of the fluid in the tank = ")
```

Scilab code Exa 11.6 internal energy and enthalpy change calculation

```
1 //clc()
2 P = 101.3; //kPa
3 SVl = 1.04 * 10^-3; //m^3/kmol
4 SVg = 1.675; //m^3/kmol
5 Q = 1030; //kJ
6 W = P * 10^3 * (SVg - SVl)/1000;
7 U = Q - W;
8 H = U + P * 10^3 * (SVg - SVl)/1000;
9 disp("kJ/kmol", U, "Change in internal energy = ")
10 disp("kJ/kmol", H, "Change in enthalpy = ")
```

Scilab code Exa 11.7 change in internal energy

```
1 //clc()
```

```
//work is done on the system, hence, W is negative
W = - 2 * 745.7; //J/s
//heat is transferres to the surrounding, hence,
heat transferred is negative,
Q = -3000; //kJ/h
U = Q*1000/3600 - W;
disp("J/s",U,"Change in internal energy = ")
```

#### Scilab code Exa 11.8 reaction of iron with HCl

```
1 //clc()
2 //Fe(s) + 2HCl(aq) = FeCl2(aq) + H2(g)
3 MFe = 55.847;
4 m = 1; //kg
5 Nfe = m * 10^3/MFe;
6 Nh2 = Nfe; //(since 1 mole of Fe produces 1 mole of H2)
7 T = 300; //K
8 R = 8.314;
9 //the change in volume is equal to the volume occupied by hydrogen produced
10 PV = Nh2 * R * T;
11 W = PV;
12 disp("kJ",W,"Work done = ")
```

#### Scilab code Exa 11.9 Thermic fluid

```
1 // clc()
2 //Cp =1.436 + 2.18*10^-3*T;
3 m = 1000/3600; //kg/s
4 T1 = 380; //K
5 T2 = 550; //K
6 x = integrate('1.436 + 2.18*10^-3*T', 'T', T1, T2);
```

```
7 Q = m*x;
8 disp("kW",Q,"Heat load on the heater = ")
```

#### Scilab code Exa 11.10 Heat capacity

```
1 //clc()
2 / Cp = 26.54 + 42.454*10^{-3} * T - 14.298 * 10^{-6} * T
       ^2:
3 \text{ T1} = 300; //K
4 T2 = 1000; //K
5 m = 1; //kg
6 N = m/44; //kmol
7 x = integrate('26.54 + 42.454*10^{-3} * T - 14.298 *
      10^{-6} * T^{2}, T^{7}, T1, T2);
8 \quad Q = N*x;
9 \operatorname{disp}("kJ", Q, "(a) \operatorname{Heat} required = ")
10 //for temperature in t degree celsius
11 / Cp = 26.54 + 42.454*10^{-3} * (t + 273.15) - 14.298
      * 10^{-6} * (t + 273.15)^{2}
12 / Cp = 37.068 + 34.643 * 10^{-3}t - 14.298 * 10^{-6} * t
       ^2 (kJ/kmolC)
  //\text{Cp} = 8.854 + 8.274*10^{-3}*t -3.415*10^{-6}*t^{2} ( Kcal
      /kmolC)
14 //For degree Fehreneit scale, replacet by ( t1 - 32)
      /18, we get
15 / Cp = 8.7058 + 4.6642 * 10^{-3} * t1 - 1.0540 * 10^{-6}
      * t1^2 (Btu/lbmolF)
```

Scilab code Exa 11.11 Enthalpy change when chlorine gas is heated

```
1 //clc()
```

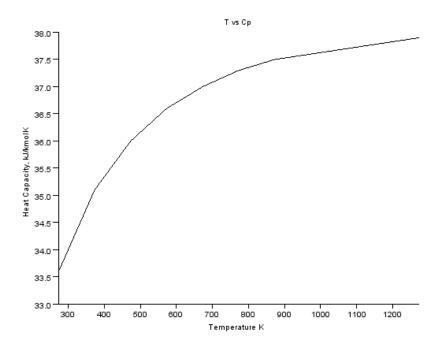


Figure 11.1: Enthalpy change when chlorine gas is heated

#### Scilab code Exa 11.12 Molal heat capacity

```
1 // clc ()
2 / Cp = 26.586 + 7.582 * 10 -3 * T - 1.12 * 10 -6 *
      T^2
3 \text{ T1} = 500; //K
4 \text{ T2} = 1000; //K
5 x = integrate('26.586 + 7.582 * 10^{-3} * T - 1.12 *
      10^{-6} * T^{2}, T^{7}, T1, T2);
6 \text{ Cpm} = 1 *x / (T2 - T1);
7 disp("kJ/kmolK", Cpm, "(a) Mean molal heat capacity = "
      )
8 V = 500; //m^3;
9 N = V / 22.4143;
10 Q = N * Cpm * (T2 - T1);
11 \operatorname{disp}("kJ/h", Q, "(b)) Heat to be supplied = ")
12 T3 = 1500; //K
13 \ Q1 = Cpm * (T3 - T1);
14 y = integrate('26.586 + 7.582 * 10 -3 * T - 1.12 *
      10^{\circ}-6 * T^{\circ}2', T', T1, T3);
15 Q2 = y;
16 disp(Q2)
```

```
17 Perror = (Q2 - Q1) * 100 / Q2;
18 disp("%", Perror,"(c) Percent error = ")
```

### Scilab code Exa 11.13 Enthalpy change of a gas

```
1 //clc()
2 T1 = 1500; //K
3 Tr = 273; //K
4 T2 = 400; //K
5 Cpm1 = 50; //kJ/kmol
6 Cpm2 = 35; //kJ/mol
7 H = Cpm1 * ( T1 - Tr ) - Cpm2 * ( T2 - Tr );
8 disp("kJ/kmol", H," Enthalpy change = ")
```

#### Scilab code Exa 11.14 Combustion of solid waste

```
1 //clc()
2 / CO, 26.586 + 7.582*10^{-3}T - 1.12*10^{-6}T^{2}
3 / (CO2, 26.540 + 42.454*10^{-3}T - 14.298*10^{-6}T^{2}
4 //O2, 25.74 + 12.987*10^{-3}T - 3.864*10^{-6}T^{2}
5 / N2, 27.03 + 5.815*10^{-3}T - 0.289*10^{-6}T^{2}
6 //Cpmix = summation ( yi*Cpi ) = summation(yi*ai +
      yi*bi*T + yi*ci*T^2
7 \text{ xco2} = 0.09;
8 \text{ xco} = 0.02;
9 \times 02 = 0.07;
10 \text{ xn2} = 0.82;
11 T1 = 600; //K
12 T2 = 375; //K
13 sumai = xco * 26.586 + xco2 * 26.540 + xo2 * 25.74 +
      xn2*27.03;
14 sumbi = xco * 7.582*10^{-3} + xco2*2.454*10^{-3}+xo2
      *12.987*10^{-3} + xn2*5.815*10^{-3};
```

# Scilab code Exa 11.15 Heat capacity calculation for Na2SO4 10H2O

```
1  // clc()
2  Hna = 26.04; // J/g-atomK
3  Hs = 22.6; // J/g-atomK
4  Ho = 16.8; // J/g-atomK
5  Hh = 9.6; // J/g-atomK
6  Hna2so410h2o = 2*Hna + Hs + 14*Ho + 20*Hh;
7  Hexp = 592.2; // J/molK
8  Deviation = (Hexp - Hna2so410h2o)*100/Hexp;
9  disp("%", Deviation," Deviation in heat capacity = ")
```

# Scilab code Exa 11.16 Heat of vaporization calculation

## Scilab code Exa 11.17 Heat requirement

```
1 //clc()
2 \text{ T1} = 250; //K
3 T = 273.15; //K
4 \text{ T2} = 400; //K
5 Cice = 2.037; //kJ/kgK
6 	ext{ T3} = 373.15; //K
7 Cliq = 75.726; //kJ/kmolK
8 / \text{Cp} = 30.475 + 9.652*10^{-3} + 1.189*10^{-6} + T^{2}
9 Hfusion = 6012; //kJ/kmol
10 Hvap = 40608; //kJ/kmol
11 //1 - Heat for raising the temperature of ice, H1
12 \text{ H1} = \text{Cice} * (T - T1);
13 / 2 - Latent heat of fusion of ice, Hf
14 Hf = Hfusion / 18.016; //kJ
15 //3 - Sensible heat of raising the temperature of
      water, H2
16 \text{ H2} = \text{Cliq} * (T3 - T)/18.016;
17 //4 - Latent heat of vaporization of water, Hv
```

# Scilab code Exa 11.18 Equilibrium temperature of mixture

```
1 // clc ()
2 / Cp = 0.16 + 4.78 * (10^{-3}) * T (organic liquid)
3 / \text{Cp} = 0.7935 + 1.298 * (10^-4) * T ( CCL4 )
4 Tb = 349.9; //K
5 \text{ Hv} = 195; //kJ/kg
6 \text{ Cp} = 0.4693; //kJ/kgK
7 //Let T be the final temperature
8 //integration (T - 650)(0.16 + 4.78 * (10^-3) * T) dt
     = integration (295 - T) (0.7935 + 1.298 * (10^-4) *
      T) dt
  // the above equation yields, 2.4549*(10^-3)*T^2 +
      0.9535*T - 1353.51 = 0, from this we get
10 T = 573.3; //K
11 //since this temperature is above boiling point of
      CCl4,
12 //heat balance is, integration (T - 650)(0.16 + 4.78)
      * (10^{-3}) * T) dt = integration (295 - 349.9)
      (0.7935 + 1.298 * (10^{-4}) * T) dt + Hv +
      integration (349.9 - T)*0.4693*dT
13 //solving above equation, we get,
14 \text{ T1} = 540.1; //K
15 disp("K", T1, equilibrium temperature of the mixture
     = ")
```

# Scilab code Exa 11.19 Estimation of mean heat of vaporisation

```
1 //clc()
2 T1 = 363; //K
3 T2 = 373; //K
4 P1s = 70.11; //kPa
5 P2s = 101.3; //kPa
6 R = 8.314; //kJ/kmolK
7 // ln(P2s / P1s) = Hv / R * (1/T1 - 1/T2);
8 Hv = (log(P2s/P1s)*R)/(1/T1 - 1/T2);
9 Hv1 = Hv / (18);
10 disp("kJ/kg", Hv1, "Mean heat of vaporization = ")
```

#### Scilab code Exa 11.20 Heat of vaporization of methyl chloride

```
1  //clc()
2  T = 273.15 - 30; //K
3  //lnPs = 14.2410 - 2137.72 / (T-26.72)
4  //dlnPs/dT = Hv / RT2
5  Hv = 2137.72 * R * T^2 / ( T - 26.72 )^2;
6  disp("kJ/kmol", Hv, "Heat of vaporization = ")
```

### Scilab code Exa 11.21 Watson equation

```
1 //clc()
2 Hv1 = 2256; //kJ/kg
3 T1 = 373; //K
4 T2 = 473; //K
5 Tc = 647; //K
```

```
6 Tr1 = T1 / Tc;
7 Tr2 = T2 / Tc;
8 //Hv2 / Hv1 = ((1-Tr2)/(1-Tr1))^0.38
9 Hv2 = Hv1*(((1-Tr2)/(1-Tr1))^0.38);
10 disp("kJ/kg",Hv2,"Latent heat of vaporization of water at 473K = ")
```

# Scilab code Exa 11.22 Kistyakowsky equation

```
1 //clc()
2 / Cp = a + b*T
3 \text{ T1} = 293.15; //K
4 Cp1 = 131.05; //J/molK
5 T2 = 323; //K
6 Cp2 = 138.04; //J/molK
7 / a + 293*b = 131.05
8 / a + 323*b = 138.04
9 b = (Cp1 - Cp2)/(T1 - T2);
10 \ a = Cp1 - b * T1;
11 / Cp = 62.781 + 0.233*T
12 // \text{Hvb} / \text{Tb} = 36.63 + 8.31 \ln \text{Tb}
13 Tb = 273.15 + 80.1; //K
14 Hvb = (36.63 + 8.31*log(Tb)) * Tb;
15 m = 100; //kg
16 H = m*(10^3) * (integrate('62.781 + 0.233*T', 'T', T1,
      Tb))/78.048 + m*(10^3)*Hvb/78.048;
17 disp("J",H,"Heat required = ")
```

#### Scilab code Exa 11.23 Quality of steam

```
1 //clc()
2 P = 10;//kPa
3 T1 = 323.15;//K
```

```
4 T2 = 373.15; //K
5 T = 358.15; //K
6 H1 = 2592.6; //kJ/kg
7 H2 = 2687.5; //kJ/kg
8 //H by interpolation,
9 H = H1 + ((H2 - H1)/(T2 - T1))*(T - T1);
10 H1 = 697.061; //kJ/kg
11 Hg = 2762; //kJ/kg
12 //H = x*H1 + (1 - x) * Hg
13 x = (H - Hg)/(H1 - Hg);
14 Pmois = x*100;
15 Psteam = (1 - x)*100;
16 disp("%", Pmois," Percentage of moisture = ")
17 disp("%", Psteam," Percentage of dry saturated steam = ")
```

#### Scilab code Exa 11.24 Heat calculation

```
1 // clc ()
2 P = 3500; //kPa
3 T = 673.15; //K
4 \text{ SV} = 0.08453; //\text{m}^3/\text{kg}
5 Vcondensed = 1/2;
6 \text{ m} = 100; //\text{kg}
7 V = m * SV / (m/2);
8 //m*(Vl+Vg)*Vcondensed = m * SV
9 //But VI is negligible,
10 Vg = m * SV / (m * Vcondensed);
11 //using steam table
12 \text{ T1} = 459.5; //K
13 P1 = 1158; //kPa
14 //internal energy of superheated steam from steam
       table
15 I = 2928.4; //kJ/kg
16 \text{ U1} = \text{m} * \text{I};
```

```
17  Ul = 790; //kJ/kg
18  Ug = 2585.9; //kJ/kg
19  U2 = m*Vcondensed*Ul + m*(1-Vcondensed)*Ug;
20  Q = U2 - U1;
21  disp("kJ",Q,"The amount of heat removed fromt he system = ")
```

# Scilab code Exa 11.25 Enthalpy balance for evaporation process

```
1 //clc()
2 m = 1000; //kg/h (basis mass of 10\% NaOH solution)
3 Pfeed = 10; //\%
4 Ppro = 50; // (Percentage NaOH in product)
5 //Taking NaOH balance, P being the weight of the
      product
6 P = Pfeed * m / Ppro;
7 /W be the weight of water evaporized
8 W = m - P;
9 / \text{step1} - \text{cooling } 1000 \,\text{kg/h} \text{ of } 10\% \text{ solution from } 305 \,\text{K}
       to 298K
10 T1 = 305; //K
11 T2 = 298; //K
12 Cliq = 3.67; //kJ/kgK
13 \text{ H1} = m*Cliq * (T2 - T1);
14 //step2 - separation into pure components
15 Hsolution = -42.85; //kJ/mol
16 \text{ H2} = -\text{Pfeed} * m *1000 * \text{Hsolution} / (40*100);
17 //step3 - W kg water is converted to water vapour
18 Hvap = 2442.5; //kJ/kg
19 H3 = W * Hvap;
20 //step4 - water vapour at 298K is heated to 373.15K
21 Cvap = 1.884; //kJ/kgK
22 \text{ T3} = 373.15; //K
23 \text{ H4} = \text{W} * \text{Cvap} * (\text{T3} - \text{T2});
24 //step5 - formation of 200kg of 50% NaOH solution at
```

```
298K
25  Hsolu = -25.89; //kJ/mol
26  H5 = Pfeed * m *1000 *Hsolu/ (40*100);
27  //step6 - Heating the solution from 298K to 380K
28  Csolu = 3.34; //kJ/kg
29  T4 = 380; //K
30  H6 = P * Csolu * (T4 - T2);
31  Htotal = H1 + H2 + H3 + H4 + H5 + H6;
32  disp("kJ", Htotal, "The enthalpy change accompanying the complete process = ")
```

Scilab code Exa 11.26 Mean heat capacity of ethanol water solution

```
1 //clc()
2 Nwater = 0.8; // moles
3 Nethanol = 0.2; // moles
4 T = 323; //K
5 Cwater = 4.18*10^3; //J/kgK
6 Cethanol = 2.58*10^3; //J/kgK
7 Hmixing1 = -758; //J/mol ( at 298K )
8 Hmixing2 = -415; //J/mol ( at 323K )
9 \text{ T1} = 298; //K
10 T2 = 523; //K
11 / \text{step1} - 0.8 \text{ mol of water is cooled from } 323 \text{ K to}
       298K
12 \text{ H1} = \text{Nwater} * 18 * \text{Cwater} * ( \text{T1} - \text{T} ) / 1000;
13 //step2 - 0.2 mol ethanol cooled from 323K to 298K
14 \text{ H2} = \text{Nethanol} * 46 * \text{Cethanol} * (T1 - T)/1000;
15 / \text{step } 3 - 0.8 \text{ mol water and } 0.2 \text{ mol ethanol are}
       mixed together,
16 \text{ H3} = \text{Hmixing1};
17 //step4 solution is heated to 323K, H4 = Cpm * (T -
       T1)
18 / \text{Hmixing2} = \text{H1} + \text{H2} + \text{H3} + \text{H4}
19 \text{ H4} = \text{Hmixing2} - \text{H1} - \text{H2} - \text{H3};
```

```
20 Cpm = H4 / ( T - T1 );
21 disp("J/molK", Cpm, "The mean heat capacity of a 20 percent solution = ")
```

# Scilab code Exa 11.27 Evaporation of NaOH solution

### Scilab code Exa 11.28 Heat transfer to air

```
1 //clc()
2 U2 = 0.35*10^3; //kJ
3 U1 = 0.25*10^3; //kJ
4 //since the tank is rigid the volume does not change during heating, Under constant volume, the change in the internal energy is equal to the heat supplied
5 Q = U2 - U1;
6 disp("kJ",Q,"Heat transferred to the air = ")
```

### Scilab code Exa 11.29 change in internal energy

```
1 //clc()
2 W = -2.25*745.7; //W ( work done on the system and 1
          hp = 745.7W)
3 Q = -3400; //kJ/h ( Heat transferred to the
          surrounding )
4 U = Q*1000/3600 - W;
5 disp("J/s",U," Rise in the Internal energy of the
          system = ")
```

# Scilab code Exa 11.30 Heat liberation in oxidation of iron fillings

```
1 //clc()
2 //2Fe + 3/2O2 = Fe2O3
3 Hliberated = 831.08; //kJ
4 Q = -Hliberated*1000;
5 disp("J",Q,"Q = ")
6 //P(V) = (n)RT
7 //W = P(V) = (n)RT
8 n = -1.5;
9 R = 8.314;
10 T = 298; //K
11 W = (n) * R * T;
12 disp("J",W,"W = ")
13 U = Q - W;
14 disp("J",U,"U = ")
```

Scilab code Exa 11.31 Saturated steam and saturated water

```
1 // clc()
2 \text{ Vgas} = 0.09; //\text{m}^3
3 \text{ Vliq} = 0.01; //\text{m}^3
4 SVliq = 1.061*10^{-3}; //m^3/kg
5 SVvap = 0.8857; //m^3/kg
6 mvap = Vgas / SVvap;
7 mliq = Vliq / SVliq;
8 U1 = 504.5; //kJ/kg
9 Ug = 2529.5; //kJ/kg
10 U1 = U1 * mliq + Ug * mvap;
11 SVtotal = (Vgas + Vliq)/(mvap + mliq);
12 //using steam table, these value of specific volume
       corresponds to pressure of 148.6 bar and internal
       energy of 2464.6 \,\mathrm{kJ/kg}
13 U = 2464; //kJ/kg
14 Utotal = U * (mvap + mliq);
15 // Utotal - U1 = Q - W, but W = o, hence,
16 Q = Utotal - U1;
17 disp("kJ",Q,"Heat to be added = ")
```

Scilab code Exa 11.32 constant volume and constant pressure process

```
1 //clc()
2 m = 10; //kg(air)
3 N = m / 29; //kmol
4 P1 = 100; //kPa
5 T1 = 300; //K
6 R = 8.314;
7 V1 = N * R * T1 / P1;
8 V2 = V1;
9 T2 = 600; //K
10 Cv = 20.785; //kJ/kmolK
11 Cp = 29.099; //kJ/kmolK
12 U = N * Cv * (T2 - T1);
13 Q = U;
```

```
14 \quad W = Q - U;
15 H = U + N * R * (T2 - T1);
16 disp("kJ",U,"(a) Change in internal energy at
      constant volume = ")
17 disp("kJ",Q,"heat supplied at constant volume = ")
18 disp("kJ", W, "Work done at constant volume = ")
19 disp("kJ", H, "Change in Enthalpy at constant volume =
       ")
20 P2 = P1;
21 \text{ H2} = \text{N} * \text{Cp} * (\text{T2} - \text{T1});
22 Q2 = H2;
23 U2 = H2 - N * R * (T2 - T1);
24 \text{ W2} = \text{Q2} - \text{U2};
25 disp("kJ",U2,"(b)Change in internal energy at
      constant Pressure = ")
  disp("kJ",Q2,"heat supplied at constant Pressure = "
27 disp("kJ", W2, "Work done at constant Pressure = ")
28 disp("kJ", H2, "Change in Enthalpy at constant
      Pressure = ")
```

## Scilab code Exa 11.33 series of operations

```
1 //clc()
2 Cp = 29.3; //kJ/kmol
3 R = 8.314;
4 Cv = Cp - R;
5 T1 = 300; //K
6 P1 = 1; //bar
7 P2 = 2; //bar
8 //step1 - Volume remains constant, therefore the work done is zero and heat supplied is Cv, Also T2/T1 = P2/P1
9 T2 = P2 * T1 / P1;
10 Q1 = Cv * (T2 - T1);
```

```
11 W1 = 0;
12 disp("kJ", W1, "Work done at constant volume = ")
13 disp("kJ",Q1,"Heat supplied at constant volume = ")
14 //step2 - Process is abdiabatic
15 \quad Q2 = 0;
16 r = 1.4;
17 T3 = T2 * (( P1 / P2 )^((r - 1)/r));
18 \text{ W2} = \text{Cv} * (\text{T2} - \text{T3});
19 disp(T3)
20 disp("kJ", W2, "Work done in adiabatic process = ")
21 disp("kJ",Q2,"Heat supplied in adiabatic process = "
22 //step3 - process is isobaric
23 \ Q3 = Cp * (T1 - T3);
24 \text{ U3} = \text{Cv} * (\text{T1} - \text{T3});
25 \text{ W3} = \text{Q3} - \text{U3};
26 disp("kJ", W3, "Work done at constant pressure = ")
27 disp("kJ",Q3,"Heat supplied at constant pressure = "
      )
```

Scilab code Exa 11.34 change in internal energy and enthalpy and heat supplied and work done

```
1  // clc()
2  P1 = 5; // bar
3  P2 = 4; // bar
4  T1 = 600; //K
5  V = 0.1; //m^3
6  T2 = 400; //K
7  T = 298; //K
8  Cp = 30; // J/molK
9  // step1 - isothermal condition
10  U1 = 0;
11  H1 = 0;
12  P = 1; // bar
```

```
13 R = 8.314;
14 W1 = R*T1*log(P1/P2);
15 \ Q1 = W1;
16 disp("kJ/kmol", U1, "(a) Change in the internal energy
      in isothermal condition = ")
17 disp("kJ/kmol", H1, "Change in the enthalpy energy in
      isothermal condition = ")
18 disp("kJ/kmol", W1, "Work done in isothermal condition
       = ")
  disp("kJ/kmol",Q1,"Heat supplied in isothermal
      condition = ")
20 N = P * (1.01325 * 10^5) * V / (R * T);
21 \text{ Cv} = \text{Cp} - \text{R};
22 	 U2 = Cv * (T2 - T)*N;
23 \text{ H2} = \text{Cp} * (\text{T2} - \text{T}) * \text{N};
24 \text{ W2} = 0;
25 Q2 = U2 + W2;
26 disp("kJ/kmol", U2, "(b) Change in the internal energy
      at constant volume condition = ")
  disp("kJ/kmol", H2, "Change in the enthalpy energy at
      constant volume condition = ")
  disp("kJ/kmol", W2, "Work done at constant volume
      condition = ")
29 disp("kJ/kmol",Q2,"Heat supplied at constant volume
      condition = ")
```

## Scilab code Exa 11.35 Heat removed in condenser

```
1 //clc()
2 m = 1; //kg
3 u2 = 0.5; //m/s
4 u1 = 60; //m/s
5 H = -3000; //kJ/kg
6 //KE = (u^2)/2
7 KE = ((u2 ^ 2) - (u1^2))/2000;
```

```
8  g = 9.81; //m/s^2
9  Z1 = 7.5; //m
10  Z2 = 2; //m
11  //PE = g * (Z)
12  PE = g * (Z2 - Z1)/1000;
13  W = 800; //kJ/kg
14  Q = H + PE + KE + W;
15  disp("kJ/kg",Q,"Heat removed from the fluid = ")
```

## Scilab code Exa 11.36 Throttling process

```
1 //clc()
2 PE = 0;
3 W = 0;
4 Q = 0;
5 //(H) + (u^2)/2 = 0
6 //according to the realtion u1 * v1 = u2 * v2
7 //(u^2)/2 is negligible, change in enthalpy is 0
8 T1 = 623;/K
9 P1 = 6000;//kPa
10 H1 = 3045.8;//kJ/kg (Enthalpy of the steam using steam table )
11 P2 = 1000;//kPa
12 T2 = 570;//K (value of temperature corresponding to the enthalpy and pressure using the steam table )
13 disp("K",T2," Temperature of superheated steam = ")
```

## Scilab code Exa 11.37 water pumping and energy balances

```
1 //clc()
2 g = 9.81;//m/s<sup>2</sup>
3 z = 55;
```

```
4 PE = g * z;
5 \text{ KE} = 0;
6 	ext{ T2} = 288; //K
7 f = 1.5*10^-2; //m^3/min
8 D = 1000; //kg/m^3
9 m = f * D;
10 Qsupp = 500; //kJ/min
11 Qlost = 400; //kJ/min
12 Qnet = (Qsupp - Qlost) * D / m;
13 W = 2*745.7; /W
14 Ws = -W * 0.6 / (m/60);
15 H = Qnet - Ws - PE - KE;
16 \text{ Cp} = 4200;
17 T1 = H / Cp;
18 T = T1 + T2;
19 disp("K",T,"The temperature of exit water = ")
```

#### Scilab code Exa 11.38 Energy balance on rotary drier

```
1 //clc()
2 m = 1000; //kg/h (dried product)
3 // S be the amount of dry solid in the product
      stream
4 Pmoisture1 = 4; //\%
5 Pmoisture2 = 0.2; //\%
6 S = m * (1 - P/1000);
7 X1 = Pmoisture1/(100 - Pmoisture1);
8 X2 = Pmoisture2/(100 - Pmoisture2);
9 //let G be the weight of dry air in the air stream
10 Y1 = 0.01; //kg water/kg dry solid
11 Cp = 1.507;
12 \text{ Cw} = 4.2;
13 T1 = 298; //K
14 T = 273; //K
15 T2 = 333; //K
```

```
16 \text{ Tg1} = 363; //K
17 \text{ Tg2} = 305; //K
18 \text{ Hs1} = (Cp + X1 * Cw) * (T1 - T);
19 Hs2 = (Cp + X2 * Cw) * (T2 - T);
20 / \text{Hg} = \text{Cs} (\text{Tg} - \text{To}) + \text{Y*L}
21 / Cs = 1.005 + 1.884 * Y
22 L = 2502.3; //kJ/kg dry air
23 \text{ Hg1} = (1.005 + 1.884 * Y1)*(Tg1 - T) + Y1 * L;
24 Q = -40000; //kJ/h
25 / \text{Calculating for T2}, \text{Hg2} = 32.16 + 2562.59*Y
\frac{26}{\text{change in enthalpy}} = Q
27 / H1 = S * Hs1 + G * HG1 = 37814.22 + 117.17G
28 / H2 = 100728.14 + G* (32.16 + 2561.59*Y)
\frac{29}{\text{change in enthalpy}} = Q
30 / 62913.92 + G * (-85.01 + 2561.59*Y) + 40000 = 0
31 / 102913.92 + G * (-85.01 + 2561.59*Y) = 0
                   (1)
32 //moisture balance, S*X1 + G*Y1 = S*X2 + G*Y2
33 / G*(Y-0.01) = 39.62
34 //solving simultaneously (1) and (2),
35 Gdry = 3443; //kg/h
36 G = Gdry*(1 + Y1);
37 disp("kg/h",G,"Air requirement = ")
```

### Scilab code Exa 11.39 Energy balance on the fractionator

```
1 //clc()
2 m = 1000; //kg/h ( feed solution )
3 //F - mass of feed distilled, W - mass of the bottom
        product, D - mass of the distillate, xf, xd and
        xw - weight fraction of actone in feed,
        distillate and residue resp.
4 //total balance, F = D + W
5 //Acetone balance, F*xf = D*xd + w*xw
```

```
6 F = 1000;
7 \text{ xf} = 0.10;
8 \text{ xd} = 0.9;
9 \times w = 0.01;
10 //substituting in above equations,
11 D = F * (xf - xw) / (xd - xw);
12 \quad W = F - D;
13 R = 8;
14 L = R * D;
15 //material balance around the condenser, G vapour
      reaching the condenser
16 G = L + D;
17 Td = 332; //K
18 T2 = 300; //K
19 Tw = 370; //K
20 \text{ Tf} = 340; //K
21 Lacetone1 = 620; //kJ/kg
22 Lwater1 = 2500; //kJ/kg
23 Ld = xd * Lacetone1 + (1 - xd) * Lwater1;
24 Cpacetone = 2.2; //kJ/kgK
25 Cpwater = 4.2; //kJ/kgK
26 Cp = xd * Cpacetone + (1-xd)*Cpwater;
27 H = Ld + Cp * (Td - T2);
28 Cpc = 4.2; //kJ/kg
29 Tc = 30; //K ( change in temperature allowable for
      cooling water )
30 m = G * H / (Cpc * Tc);
31 disp("kg/h",m,"(a)The circulation rate of cooling
      water = ")
32 \ Qc = G * H;
33 \text{ Hd} = 0;
34 Hw = (xw * Cpacetone + (1-xw)*Cpwater)*(Tw - T2);
35 Hf = (xf * Cpacetone + (1-xf)*Cpwater)*(Tf - T2);
36 \text{ Qb} = D * Hd + W * Hw + Qc - F * Hf;
37 Hcondensation = 2730; //kJ/kg
38 msteam = Qb/Hcondensation;
39 \operatorname{disp}("kg/h", msteam,"(b)) Amount of steam supplied = ")
```

## Chapter 12

# Energy Balance Thermochemistry

#### Scilab code Exa 12.1 Heat liberated calculation

```
1 //clc()
2 N = 100; //mol gas mixture burned
3 /(CO(g) + 1/2 O2(g) = CO2 -
                                                           Hr1 =
       -282.91 \, kJ/mol
4 / H2(g) + 1/2 O2(g) = H2O -
                                                           Hr2 =
       -241.83 \, kJ/mol
5 \text{ Hr1} = -282.91; //kJ/mol
6 \text{ Hr2} = -241.83; //kJ/mol
7 \text{ Nco1} = 20;
8 \text{ Nh21} = 30;
9 \text{ Nn21} = 50;
10 Htotal = Nco1*Hr1 + Nh21*Hr2;
11 disp("kJ",-Htotal,"the amount of heat liberated on
      the complete combustion of 100 mol of the gas
      mixture = ")
12 \text{ Ncoreac} = \text{Nco1} * 0.9;
13 \text{ Nh2reac} = \text{Nh21} * 0.8;
14 Htotal1 = Ncoreac*Hr1 + Nh2reac*Hr2;
15 disp("kJ",-Htotal1," the amount of heat liberated if
```

```
only 90\% of CO and 80\% of H2 react of 100\,\mathrm{mol} of the gas mixture = ")
```

#### Scilab code Exa 12.2 Heat of formation of methane

```
1 //clc()
                                        Hf = ?
2 / C(s) + 2H2(g) = CH4(g)
3 \text{ Hc} = -393.51; //kJ/mol
4 \text{ Hh2} = -285.84; //kJ/mol
5 \text{ Hch4} = -890.4; //kJ/mol
6 //heat of reaction can be calculated from the heat
     of combustion data using following equation, the
     heat of reaction is the sum of the heat of
     combustion of all the reactants in the desired
     reaction minus the sum of the heat of combustion
     of all the products of the desired reaction. Here
      the reactants are one mole of Carbon and two
     moles hydrogen, and the product is one mole of
     methane, there heat of reaction is
7 \text{ Hf} = 1 * \text{Hc} + 2 * \text{Hh2} - 1 * \text{Hch4};
8 disp("kJ", Hf, "Heat of formation of methane = ")
```

#### Scilab code Exa 12.3 Net heating value of coal

```
1 // clc()
2 m = 1; //kg of coal burned
3 xc = 0.7;
4 xh2 = 0.055;
5 xn2 = 0.015;
6 xs = 0.03;
7 xo = 0.13;
8 xash = 0.07;
9 Hvap = 2370; //kJ/kg
```

Scilab code Exa 12.4 Heat of reaction for esterification of ethyl alcohol

Scilab code Exa 12.5 Vapour phase hydration of ethylene to ethanol

```
 \begin{array}{lll} 1 & //\operatorname{clc}\left(\right) \\ 2 & //\operatorname{C2H4}(g) + \operatorname{H2O}(g) = \operatorname{C2H5OH}(g) \\ 3 & //\operatorname{2CO2}(g) + \operatorname{3H2O}(1) = \operatorname{C2H5OH}(1) + \operatorname{3O2}(g) \\ & & \operatorname{1366.91\,kJ} \quad (A) \\ 4 & \operatorname{Hc2h4} = -1410.99; //\operatorname{kJ/mol} \\ 5 & \operatorname{Hvap} = 44.04; //\operatorname{kJ/mol} \\ 6 & \operatorname{Hc2h5oh} = 42.37; //\operatorname{kJ/mol} \\ \end{array}
```

```
7 / C2H4(g) + 3H2O(1) = C2H5OH(1) + 3O2(g)
                                                        H =
      -1410.99 \,\mathrm{kJ} (B)
8 / H2O(1) = H2O(g)
                                                        H =
      44.04 \,\mathrm{kJ}
                 (\mathbf{C})
  //C2H5OH(1) = C2H5OH(g)
                                                        H =
      42.37\,\mathrm{kJ}
                 (D)
10 /A + B + D - C gives the required reaction
11 Ha = 1366.91; //kJ
12 Hb = -1410.99; //kJ
13 Hc = 44.04; //kJ
14 Hd = 42.37; //kJ
15 Hreac = Ha + Hb + Hd - Hc;
16 disp("kJ", Hreac, "The standard heat of reaction = ")
```

Scilab code Exa 12.6 Standard heat of formation of acetylene

```
1 // clc()
2 / C2H5(g) + 5/2O2(g) = 2CO2(g) + H2O(1)
      H1 = -1299.6 \,\mathrm{kJ}
3 / C(s) + O2(g) = CO2(g)
      H2 = -393.51 \,\mathrm{kJ}
                              (B)
4 / H2(g) + 1/2O2(g) = H2O(1)
      H3 = -285.84 \,\mathrm{kJ}
                              (\mathbf{C})
5 / 2C(s) + H2(g) = C2H2(g)
      H = ?
6 \text{ H1} = -1299.6; //kJ
7 \text{ H2} = -393.51; //kJ
8 \text{ H3} = -285.84; //kJ
9 \text{ Hreac} = 2 * H2 + H3 - H1;
10 disp("kJ", Hreac, "Heat of formation of acetylene = ")
```

Scilab code Exa 12.7 Standard heat of roasting of iron pyrites

```
1 //clc()
2 m = 100; //kg of pyrites charged
3 \text{ xfes2in} = 0.8;
4 \text{ xganguein} = 0.2;
5 \text{ xfes2out} = 0.05;
6 //let x be the FeS2 in the feed, then, Fe2O3 = (80 - 6)
       (x)*159.69 / (119.98*2) and gangue = 20, total =
      73.24 + 0.3345, be FeS2 is only 5 % in the
      product, hence
7 \times = 0.05 \times 73.24 / (1 - 0.05 \times 0.3345);
8 mfes2reacted = m*xfes2in - x;
9 / 4 \text{FeS}2 + 1102 = 2 \text{Fe}203 + 8 \text{SO}2
10 Hfes2 = -178.02; //kJ/mol
11 Hfe2o3 = -822.71; //kJ/mol
12 Hso2 = -296.9; //kJ/mol
13 Hreac = 2 * Hfe2o3 + 8 * Hso2 - 4 * Hfes2;
14 N = mfes2reacted *1000/ 119.98;
15 H = Hreac * N / 4;
16 H1 = H/m; // (heat of reaction per kg of coal burnt)
17 disp("kJ", H1, "Heat of reaction per 1 kg of coal
      burned = ")
```

Scilab code Exa 12.8 Standard heat of formation of liquid methanol

Scilab code Exa 12.9 Gross heating value and Net heating value calculation

```
1 //clc()
2 N = 100; //mol fuel gas
3 \text{ Nco} = 21;
4 \text{ Nh2} = 15.6;
5 \text{ Nco2} = 9.0;
6 \text{ Nch4} = 2;
7 \text{ Nc2h4} = 0.4;
8 \text{ Nn2} = 52;
9 Hco = 282.99; //kJ/mol ( heat of combustion )
10 Hh2 = 285.84; //kJ/mol ( heat of combustion )
11 Hch4 = 890.4; //kJ/mol (heat of combustion)
12 Hc2h4 = 1410.99; //kJ/mol ( heat of combustion )
13 Hvap = 44.04; //kJ/mol
14 	ext{ H} = 	ext{Nco} * 	ext{Hco} + 	ext{Nh2} * 	ext{Hh2} + 	ext{Nch4*Hch4} + 	ext{Nc2h4*Hc2h4};
      //kJ
15 V = N * 22.4143/1000;
16 H1 = H / V; //kJ/m^3
17 //on combustion, 1 mol hydrogen gives 1 mol of water
      , 1 mol of methane gives 2 mol of water and 1 mol
       of ethylene gives 2 moles of water
18 Nwater = Nh2 + 2 * Nch4 + 2 * Nc2h4;
19 Hvap1 = Hvap * Nwater;
20 Hnet = H1 - Hvap1;
21 disp("kJ", Hnet, "Net heating value of the fuel = ")
```

Scilab code Exa 12.10 Standard heat of reaction calculation

```
3 Hfco2 = -393.51; //kJ
4 Hfh2o = - 241.826; //kJ
5 Hfc5h12 = -146.4; //kJ
6 Hvap = 43.967; //kJ/mol
7 H1 = 6*Hfh2o +5*Hfco2 - Hfc5h12;
8 H2 = 6 * (-Hvap);
9 Hreac = H1 + H2;
10 disp("kJ", Hreac, "Standard heat of reaction = ")
```

#### Scilab code Exa 12.11 Constant pressure heat of combustion

```
1 //clc()
2 m = 1; //kg \text{ of oil burned}
3 \text{ mc} = 0.9; //kg
4 \text{ mh2} = 0.1; //kg
5 Mc = mc / 12; //kmol
6 / C(s) + O2(g) = CO2(g)
7 \text{ Nh2} = \text{mh2} / 2.016; //kmol}
8 //change in the no. of gaseous components
      accompanying the combustion of 1 mole of hydrogen
       in liquid state is -1/2 mol, therefore for Nh2
      mol
9 R = 8.314;
10 T = 298; //K
11 x = Nh2 * R * T / (-2);
12 Qv = -43000; //kJ/kg
13 Qp = Qv + x;
14 disp("kJ/kg",Qp,"the constant pressure heat of
      combustion = ")
```

Scilab code Exa 12.12 Heat of reaction for ammonia synthesis

```
1 //clc()
```

```
2 //1 - N2, 2 - H2, 3 - NH3
3 \text{ a1} = 27.31;
4 a2 = 29.09;
5 \quad a3 = 25.48;
6 b1 = 5.2335*10^{-3};
7 b2 = -8.374*10^{-4};
8 b3 = 36.89 * 10^{-3};
9 c1 = -4.1868 * 10^-9;
10 c2 = 2.0139*10^-6;
11 c3 = -6.305*10^-6;
12 \text{ H1} = -46191; //J
13 T1 = 298; //K
14 / 1/2 \text{ N2} + 3/2 \text{ H2} = \text{NH3}
                                                    H = -46.191 \,\text{kJ}
15 / \text{Ht} = \text{H} + \text{a*T} + \text{b*T}^2 / 2 + \text{c*T}^3 / 3
16 / at 298
17 a = a3 - a1 / 2 - 3 * a2 / 2;
18 b = b3 - b1 / 2 - 3 * b2 / 2;
19 c = c3 - c1 / 2 - 3 * c2 / 2;
20 H = H1 -a * T1 - b * (T1^2) / 2 - c * (T1^3) / 3;
21 T2 = 700; //K
22 \text{ H2} = \text{H} + \text{a} * \text{T2} + \text{b} * (\text{T2}^2) / 2 + \text{c} * (\text{T2}^3) / 3;
23 disp(H);
24 disp("kJ", H2, "Heat of reaction at 700K =")
```

Scilab code Exa 12.13 Standard heat of reaction of methanol synthesis

```
10^4 * T^-2
8 //for reactants,
9 H1 = integrate('28.068 + 4.631 * 10^{-3} * T - 2.5773
      *10^4 * T^-2', T', T2, T1) + 2 * integrate('27.012)
       + 3.509 * 10^{-3} * T + 6.9006 * 10^{4} * T^{-2}, 'T',
      T2,T1);
10 //for product,
11 H2 = integrate ('18.382 + 101.564 * 10^{-3} * T -
      28.683 * 10^{-6} * T^{2}, T^{7}, T1, T2);
12 //H298 = Hproducts - Hreactants;
13 / CO + 2H2 = CH3OH
                                      Ha1 = -238.64 \, kJ
14 \text{ Ha1} = -238.64; //kJ
15 / CH3OH(1) = CH3OH(g)
                                      Hvap = 37.98 kJ
16 Hvap = 37.98; //kJ
17 / (CO(g) + 2H2(g) = CH3OH(g)  Ha2 = -200.66 kJ
18 Ha2 = Ha1 + Hvap; //kJ
19 Hco = -110.6; //kJ/mol
20 \text{ H298} = \text{Ha2} - (\text{Hco});
21 \text{ Htotal} = \text{H}1/1000 + \text{H}298 + \text{H}2/1000;}
22 disp("kJ/mol", Htotal, "The heat of reaction at 773K =
       ")
```

#### Scilab code Exa 12.14 Combustion of CO

```
1 //clc()
2 Nco = 1; //mol CO reacted
3 //CO + 1/2 O2 = CO2
4 No2 = Nco / 2;
5 Pexcess = 100;
6 Nosupp = No2 * ( 1 + Pexcess / 100 ); //oxygen supplied
7 Nn2 = Nosupp * 79 / 21;
8 Nco2 = Nco;
9 Noremain = Nosupp - No2;
10 T1 = 298; //K
```

```
11 T2 = 400; //K
12 Hr1 = -282.99; //kJ
13 T3 = 600; //K
14 SHco = 29.1; //J/molK
15 SHo2 = 29.7; //J/molK
16 SHn2 = 29.10; //J/molK
17 SHco2 = 41.45; //J/molK
18 H1 = (Nosupp * SHo2 + Nn2 * SHn2 + Nco * SHco) * (T1 - T2); // enthalpy of cooling of reactants from 298 to 400 K
19 H2 = (Nco2 * SHco2 + Nn2 * SHn2 + Noremain * SHo2) * (T3 - T1); // enthalpy of heating the products from 298K to 600K
20 H = H1/1000 + Hr1 + H2/1000;
21 disp("kJ", H, "Heat change at 600K = ")
```

#### Scilab code Exa 12.15 Heat added or removed calculation

```
1 //clc()
2 / (CO(g) + H2O(g) = CO2(g) + H2(g)
                                                         H298 =
      -41.190
3 \text{ T1} = 298; //K
4 Pconv = 75; //\%
5 \text{ T2} = 800; //\text{K}
6 \text{ H298} = -41.190; //kJ
7 Hco = 30.35; //J/molK
8 Hco2 = 45.64; //J/molK
9 Hwater = 36; //J/molK
10 Hh2 = 29.3; //J/molK
11 Nco = 1; // \text{mol}
12 Nh2o = 1; // \text{mol}
13 Ncofinal = Nco * (1 - Pconv/100);
14 Nwaterf = Ncofinal;
15 Nco2final = Nco - Ncofinal;
16 Nh2final = Nco2final;
```

## Scilab code Exa 12.16 CO2 O2 and N2 passed through a bed of C

```
1 // clc ()
2 / (CO2(g) + C(s)) = 2CO(g)
                                              H1298 = 170
      kJ/mol
3 / O2(g) + 2C(s) = 2CO(g)
                                              H2298 =
      -221.2 \,\mathrm{kJ/mol}
4 T2 = 1298; //K
5 \text{ T1} = 298; //K
6 Hc = 0.02; //kJ/molK
7 Ho = 0.03; //kJ/molK
8 Hco = 0.03; //kJ/molK
9 Hco2 = 0.05; //kJ/molK
10 //let the flue gas contain x mol CO2 per mole of
      oxygen, product contains 2(1+x)mol CO. Nitrogen
      in reactant and product remain the same
11 //enthalpy of cooling xmol CO2, 1 mol O2 and 2 +
      xmol carbon from 1298 to 298K is given as, H1 = (
      Hco2 * x + Ho * 1 + Hc * (2 + x)) * (298 - 1298)
12 / H1 = (-70x - 70) kJ
13 //enthalpy of heating the product, H2 = 2 * (1 + x)
     * Hco * (1298 - 298)
14 / H2 = 60 + 60x kJ
15 //Hr = 170x - 221.2
16 / Htotal = 0 = H1 + H2 + Hr
```

## Scilab code Exa 12.17 Partial oxidation of natural gas

```
1 // clc()
 2 N = 100; //mol flue gas
 3 //Carbon balance,
 4 //x is the feed of methane, w is water in flue ga, y
         is the oxygen supplied
 5 \text{ xco2} = 0.019;
 6 \text{ xch2o} = 0.117;
 7 \text{ xo2} = 0.038;
 8 \text{ xch4} = 0.826;
9 \text{ xc} = \text{xco2} + \text{xch2o} + \text{xch4};
10 Nc = xc * N;
11 \text{ Nch4i} = \text{Nc};
12 //Hydrogen balance,
13 \text{ xh2} = \text{xch2o} + \text{xch4*2};
14 w = 2 * (Nch4i) - xh2*N;
15 //oxygen balance
16 \text{ No2s} = (xco2 + xch2o/2 + xo2)*N + w/2;
17 y = No2s;
18 \text{ T1} = 298; //K
19 T2 = 573; //K
20 \text{ T3} = 673; //K
21 //oxygen cooled from 573K and methane from 673 to
        298K
22 Ho573 = 30.5; //J/molK
23 Hch4673 = 45.9; //J/molK
24 \text{ H1} = y * \text{Ho}573 * (\text{T1} - \text{T2}) + \text{Nch4i} * \text{Hch4673} * (\text{T1} - \text{T2}) + \text{Nch4i} * \text{Hch4673} * (\text{T1} - \text{T2})
         T3);
25 / CH4 + O2 = CH2O + H2O
                                               Hr1 = -282.926 \, kJ
26 / CH4 + 2O2 = CO2 + 2H2O
                                              Hr2 = -802.372 \,\text{kJ}
```

```
27 \text{ Hr1} = -282.926; //kJ
28 \text{ Hr2} = -802.372; //kJ
29 H2 = xch2o*N*Hr1 + xco2*N*Hr2;
30 \text{ T4} = 873; //K
31 Ho = 31.9
32 \text{ Hch4} = 51.4;
33 \text{ Hco2} = 46.3;
34 \text{ Hch2o} = 47.1;
35 \text{ Hh2o} = 36.3;
36 \text{ H3} = ((xco2 * Hco2 + xo2 * Ho + xch4 * Hch4 + Hch2o*)
       xch2o)*N + w * Hh2o)*(T4 - T1);
37 \text{ Htotal} = \text{H}1/1000 + \text{H}2 + \text{H}3/1000;}
38 \text{ Nch2o} = \text{xch2o} * \text{N};
39 mch2o = Nch2o * 30.016/1000; //kg
40 //for 1000 kg of formaldehyde produced,
41 H = Htotal * 1000 / mch2o;
42 disp("kJ", H, "The amount of heat to be removed per
       1000 \,\mathrm{kg} of formaldehyde produced = ")
```

#### Scilab code Exa 12.18 Maximum allowable conversion calculation

## Scilab code Exa 12.19 Theoretical flame temperature calculation

```
1 // clc ()
   2 \text{ Nco} = 1; //\text{mol CO}
   3 // CO + 1/2 O2 = CO2
   4 \ 02r = 1; //mol
   5 \text{ N2r} = 3.76; //\text{mol}
   6 \text{ COr} = 1; //\text{mol}
   7 	ext{ O2p = 0.5; //mol}
   8 \text{ N2p} = 3.76; //\text{mol}
   9 \text{ CO2p} = 1; //\text{mol}
10 Hco = 29.23; //J/molK
11 Ho2 = 34.83; //J/molK
12 Hn2 = 33.03; //J/molK
13 Hco2 = 53.59; //J/molK
14 Hcomb1 = -282.99; //kJ/mol
15 \text{ T1} = 298; //K
16 	ext{ T2} = 373; //K
17 \text{ H1} = (02r * Ho2 + N2r * Hn2 + C0r * Hco) * (T1 - T2)
          //For product at temp T, H2 = (O2p * Ho2 + N2p * Hn2)
                              + CO2p * Hco2) * (T - T1)
19 //For adiabatic condition, -(H1 + Hcomb1) = H2
20 T = -(H1 + Hcomb1 * 1000) / (O2p * Ho2 + N2p * Hn2 + Hn
                               CO2p * Hco2) + T1;
```

Scilab code Exa 12.20 Temperature of products on burning of hydrogen gas

```
1 //clc()
2 N = 1; //kmol hydrogen burned
3 \text{ No} = \text{N}/2;
4 \text{ Nosupplied} = 2 * \text{No};
5 Nair = Nosupplied * 100 / 21;
6 Nn2 = Nair - Nosupplied;
7 / \text{Reactants}, H2 = 1 \text{kmol}, Air = 4.762 \text{kmol}
   //Product, Water vapour = 1kmol, Oxygen = 0.5kmol,
       N2 = 3.762 \,\mathrm{kmol}
9 / (Cp(water) = 30.475 + (9.652*10^{-3})*T + 1.189 *
       10^{-6} * T^{2}
10 / \text{Cp(nitrogen)} = 27.034 + 5.815 * 10^{-3} *T - 0.2889
       * 10^{-6} * T^{2}
   //\text{Cp}(\text{oxygen}) = 25.611 + 13.260 * 10^{-3} * T - 4.2077
       * 10^{-6} * T^{2}
12 / H2 = integration (298 to T of (1 * Cp(water) + 0.5)
       * \operatorname{Cp}(\operatorname{oxygen}) + 3.762 * \operatorname{Cp}(\operatorname{nitrogen}))
  // \text{therefore}, H2 = 140.34 * T + 31.222 * <math>10^{-3} * T^{2}
       -4.928 * 10^{\circ} - 6 * T^{\circ} 2 - 44463.54 \text{ kJ}
14 \text{ H298} = -241.826 * 10^3; //kJ
15 / H2 = -H1 - H298
16 / H1 = 0
17 //therefore using equation H2, the value of T is
       obtained to be
18 T = 1609.8; //K
19 disp("K",T," Temperature of the reaction products = "
```