Scilab Textbook Companion for Coulson And Richardson's Chemical Engineering, Volume 2 by J. M. Coulson, J. F. Richardson, J. R. Backhurst And J. H. Harker¹

Created by
Ankit Mishra
B.Tech
Chemical Engineering
IT-BHU, VARANASI
College Teacher
R.S.singh
Cross-Checked by

October 3, 2013

¹Funded by a grant from the National Mission on Education through ICT, http://spoken-tutorial.org/NMEICT-Intro. This Textbook Companion and Scilab codes written in it can be downloaded from the "Textbook Companion Project" section at the website http://scilab.in

Book Description

Title: Coulson And Richardson's Chemical Engineering, Volume 2

Author: J. M. Coulson, J. F. Richardson, J. R. Backhurst And J. H. Harker

Publisher: Elsevier India

Edition: 5

Year: 2006

ISBN: 9788181471444

Scilab numbering policy used in this document and the relation to the above book.

Exa Example (Solved example)

Eqn Equation (Particular equation of the above book)

AP Appendix to Example(Scilab Code that is an Appednix to a particular Example of the above book)

For example, Exa 3.51 means solved example 3.51 of this book. Sec 2.3 means a scilab code whose theory is explained in Section 2.3 of the book.

Contents

List of Scilab Codes

Particulate Solids

Scilab code Exa 1.1 Surface mean diameter

```
1 clear all;
2 clc;
3 printf("\n Example 1.1");
4 //Given size analysis of a powdered material
5 d=[1,101];//diameter of the powdered particles
6 x=[0,1]; //mass fractions of the particles
7 plot2d(d,x,style=2,rect=[0,0,120,1])
8 xtitle ("size analysis of powder", "particle size (um)"
      ", mass fraction(x),
9 d=100*x+1; // from the given plot
10 //calculation of surface mean diameter
11 function [ds] = surface_mean_diameter(x0,x1)
       ds=1/(integrate('1/(100*x+1)', 'x', x0, x1))
12
13
       funcprot(0)
14 endfunction
15 ds=surface_mean_diameter(0,1);//deduced surface mean
       diameter according to def.
16 printf("\n The surface mean diameter is %fum", ds);
```

Scilab code Exa 1.2 Surface and mass distribution curve and surface mean diameter

```
1 clear;
2 clc;
3 printf("\n Example 1.2");
4 //from given differential eq we get these functions
5 // particle number distribution for the size range
      0 - 10 \text{um}
6
8 / n = 0.5 * d^2;
9 //const of integration is 0 since at n=0,d=0
10
11 //particle number distribution for the size range
      10 - 100 \text{um}
12 / n = 83 - (0.33*(10^{\circ}(5))*d^{\circ}(-3))
13 / c2 = 83, since at d=10um, n=50
14
15 //number distribution plot for the powdered material
       of size range 0-100um
16 function[n] = number_distribution(d)
17
       if(d \le 10) then
            n=0.5*d^2;
18
19
       else
20
            n=83-(0.33*(10^{(5)})*d^{(-3)};
21
            end
22
            funcprot(0)
23 endfunction
24 d=0;
25 \text{ while}(d \le 100)
     n=number_distribution(d);
26
       plot(d,n,"+-");
27
       d=d+1;
28
29 end
30 xtitle ("number_distribution_plot", "diameter (um)", "
      number distribution");
31 ps=[0 6.2 9.0 10.0 11.4 12.1 13.6 14.7 16.0 17.5
```

```
19.7 22.7 25.5 31.5 100];
32 function[n1]=difference(i)
33 //ps = [0 6.2 9.0 10.0 11.4 12.1 13.6 14.7 16.0 17.5]
      19.7 \ 22.7 \ 25.5 \ 31.5 \ 10;
34 //according to the given particle sizes particle
      sizes are in um
35
       n1=number_distribution(ps(i+1))-
          number_distribution(ps(i));
       funcprot(0);
36
37 endfunction
38 function[da] = average(i)
       da = (ps(i+1)+ps(i))/2;
39
40
       funcprot(0);
41 endfunction
42 tot_n1d12=0;
43 tot_n1d13=0;
44 i = 1;
45 \text{ for } i=1:14
            tot_n1d12=tot_n1d12+difference(i)*(average(i
46
               ))^2;
            tot_n1d13=tot_n1d13+difference(i)*(average(i
47
               ))^3;
48 end
49 printf("\n tot_n1d12 =%d \n tot_n1d13=%d",tot_n1d12,
      tot_n1d13);
50 function[s]=surface_area(j)
51
       s=(difference(j)*(average(j))^2)/tot_n1d12;
       funcprot(0);
52
53 endfunction
54 \text{ su} = 0;
55 j = 0;
56 xset('window',1);
57
58 plot(0,0,"o-");
59 \text{ for } j=1:14
       su=su+surface_area(j);
60
       plot (ps(j+1), su, "o-");
61
62 end
```

```
63 xtitle("surface area and mass distribution plot","
      diameter (um)", "surface area or mass distribution"
      );
64 //mass distribution plot
65 function[x]=mass_distribution(k)
66
       x=(difference(k)*(average(k))^3)/tot_n1d13;
67
       funcprot(0);
68 endfunction
69 \text{ ma=0};
70 k = 0;
71 plot(0,0,"+-");
72 \quad for \quad k=1:14
73
       ma=ma+mass_distribution(k);
74
       plot (ps(k+1), ma, "+-");
75 end
76 //evaluating surface mean diameter
77 function[d]=surface_mean_diameter(1)
       e=0;
78
79
       for l=1:14
          n=(mass_distribution(1)/average(1));
80
          e=e+n;
81
82
       end
83 d=1/e;
       funcprot(0);
84
85 endfunction
86 printf("\nthe surface mean diameter is: %fum",
      surface_mean_diameter());
```

Scilab code Exa 1.3 variation of mixing index with time

```
5 //for a completely unmixed system
6 so=p*(1-p);
7 //for a completely random mixture :
8 n=100; //Each of the sample removed contains 100
      particles
9 \text{ sr=p*}(1-p)/n;
10 s = [0.025 \ 0.006 \ 0.015 \ 0.018 \ 0.019];
11 time_secs=[30 60 90 120 150];
12 printf("\n degree of mixing is :\n")
13 function[b] = degree_of_mixing()
14 for i=1:5
       b(i) = (so-s(i))/(so-sr);
15
16
       disp(b(i));//b is the degree of mixing
17 end
18
       return b;
19 funcprot(0)
20 endfunction
21 plot2d(time_secs,degree_of_mixing(),style=3)
22 xtitle("degree of mixing curve", "time_secs","
      degree_of_mixing")
23 //plot of sample variance vs time(secs)
24 xset ('window',1)
25 plot2d(time_secs,s,style=2)
26 xtitle ("sample variance curve", "time_secs", "sample
      variance")
27 //from the graph the maxima is at 60 secs
```

Scilab code Exa 1.4 minimum apparent density for seperation

```
1 //minimum size of the particle in the mixture of
        quartz and galena(mm)
2 clear all;
3 clc;
4 printf("\n Example 1.4");
```

```
6 //maximum size of the particle (mm)
7 \quad d_{max} = 0.065;
8 //minimum size of the particle (mm)
9 d_min=0.015;
10 //density of quartz(kg/m<sup>3</sup>)
11 p_quartz=2650;
12 //density of galena (kg/m<sup>3</sup>)
13 p_galena=7500;
14 //minimum density of the particle which will give
      this separation
15 //When stoke's law is applied the required density
      is as given below
16 function[d] = stoke_required_density()
       p=poly([0], 'p');
17
       d=roots((p-7500)-(p-2650)*(d_max/d_min)^2);
18
       funcprot(0);
19
20 endfunction
21 d=stoke_required_density();
22 printf("\n required density is = \%d kg/m<sup>3</sup>",d);
23 //When Newton's law is applied then the required
      density is as given below
24 function[e]=newton_required_density()
25
       r=poly([0], 'r');
       e=roots((r-7500)-(r-2650)*(d_max/d_min));
26
27
       funcprot(0);
28 endfunction
29 e=newton_required_density();
30 printf ("\nrequired density is by newton law =\%d kg/m
      ^{\hat{}}3",e);
```

Scilab code Exa 1.5 efficiency of collection for dust

```
1 clear all;
2 clc;
3 printf("\n Example 1.5");
```

```
4 // efficiency of the collector for different size
     ranges
5 efficiency_1=45; //in percentage for the size range
     of 0-5um
6 efficiency_2=80; //in percentage for the size range
     of 5-10um
  efficiency_3=96; //in percentage for the size range
     greater than 10um
9 //mass percent of the ndust for various size range
10 mass_1=50; //in percentage for the size range of 0-5
11 mass_2=30; //in percetage for the size range of 5-10
12 mass_3=20; //in percentage for the size range
     greater than 10um
13 // on the basis of 100kg dust
14 mass_retained_1=0.45*50; //mass_retained(kg) in the
      size range of 0-5um
15 mass_retained_2=0.80*30; //mass_retained(kg) in the
     size range of 5-10um
16 mass_retained_3=0.96*20; //mass_retained(kg) in the
     size range greater than 10 um
17 overall_efficiency=0.45*50+0.80*30+0.96*20;
18 printf("\n the overall efficiency is =\%f",
     overall_efficiency);
```

Scilab code Exa 1.6 Overall efficiency of collector

```
1 clear all;
2 clc;
3 printf("\n Example 1.6");
4 //To calculate mass flow of the dust emitted
5 mass_1=10;//in percentage in the size range of 0-5um
6 mass_2=15;//in percentage in the size range of 5-10
```

```
um
7 mass_3=35; //in percentage in the size range of 10-20
8 mass_4=20; //in percentage in the size range of 20-40
9 mass_5=10; //in percentage in the size range of 40-80
10 mass_6=10; //in percentage in the size range of
      80 - 160 \text{um}
11 efficiecny_1=20; //in percentage in the size range of
       0-5um
12 efficiency_2=40;//in percentage in the size range of
       5 - 10 \text{um}
13 efficiency_3=80; //in percentage in the size range of
       10 - 20 \text{um}
14 efficiency_4=90; //in percentage in the size range of
       20 - 40 \text{um}
15 efficiency_5=95; //in percentage in the size range of
       40 - 80 \text{um}
16 efficiency_6=100; //in percentage in the size range
      of 80 - 160 \text{um}
17 dust_burden=18; // in g/m^3 at the entrance
18 //taking 1m<sup>3</sup> as the basis of calculation
19 total_mass_retained
      =18*(0.1*0.20+0.15*0.40+0.35*0.80+0.2*0.9+0.1*0.95+0.1*1)
20 printf("\ntotal mass retained = %fg",
      total_mass_retained);
21 total_efficiency=(total_mass_retained/18)*100;
22 printf("\ntotal efficiency is =\%f", total_efficiency)
23 total_mass_emitted=18-total_mass_retained;
24 printf("total mass emitted is: %fg",
      total_mass_emitted);
25 t=18*(0.1*0.80+0.15*0.60+0.35*0.20);
26 printf("\ntotal mass emitted less than 20um is %fg",
      t);
27 e=t*100/total_mass_emitted;
```

```
28 printf("\nThe efficiency of particles emitted is %f"
          ,e);
29 //gas flow is 0.3m^3/sec
30 f=0.3*total_mass_emitted;
31 printf("\nmass flow rate is:%fkg/sec",f);
```

Scilab code Exa 1.7 Estimation of particle size

```
1 clear;
2 clc;
3 printf("\n Example 1.7");
4 Ai = (\%pi/4)*(0.075)^2; //cross sectional area at the
      gas inlet in m<sup>2</sup>
5 do=0.075; //gas outlet diameter in m
6 p=1.3; //gas density in kg/m^3
7 Z=1.2; //height of the seperator in m
8 dt=0.3; //seperator diameter in m
9 v=1.5; //gas entry velocity in m/sec
10 G=(Ai*v*p); //mass flow rate of the gas in kg/sec
11 printf("\n cross sectional area at the gas inlet is
      \% \mathrm{fm}^2", Ai);
12 printf("\ngas outlet diameter is %fm",do);
13 printf("\ngas density is \%fkg/m<sup>3</sup>",p);
14 printf("\nheight of the seperator is %fm",Z);
15 printf("\nseperator diameter is%fm",dt);
16 printf("\nmass flow rate of the gas is %fkg/sec",G);
17 function[u]=terminal_vel()
18
       u=0.2*(Ai)^2*(do)*p*9.8/(%pi*Z*(dt)*G);//
          velocity is in m/sec
19
       funcprot(0);
20 endfunction
21 u=terminal_vel();
22 printf("\nthe terminal velocity of the smallest
      particle retained by the seperator = %fm/sec",u);
23 function[d]=particle_diameter(u)
```

```
24
       u=terminal_vel();
       n=0.018*10^{(-3)}; // viscosity in mNs/m^2
25
       ps=2700;//density of the particle in kg/m^3
26
       d=((u*18*n)/(9.8*(ps-p)))^(0.5);//particle size
27
          in um
28
       funcprot(0);
29 endfunction
30 u=terminal_vel();
31 d=particle_diameter(u);
32 \text{ do=d*10^6};
33 printf("\n particle diameter by the stoke law is
     % fum", do);
```

Particle size reduction and enlargement

Scilab code Exa 2.1 Consumption of energy

```
1 clear;
2 clc;
3 printf("\n Example 2.1");
4 //Computing energy required in particle size
      reduction by Rittinger's law
5 //energy required in crusing is given by E =Kr.fc
      ((1/L2)-(1/L1))
6 //Given: Energy required in crushing particles from
       50mm to 10mm is
                              13.0\,\mathrm{kw/(kg/sec)}.
8 Cr = 13.0*(50/4); //Cr = Kr*fc
10 //Energy required to crush the particles from 75mm
     to 25mm
11 E = Cr*((1/25)-(1/75));
12 printf("\n The energy required in crushing the
      materials from average particle size of 75mm to
      25mm by Rettingers law is %fkj/kg",E)
13
```

```
14 //Computing the energy required for crushing by Kick
      's law
15 //E = (Kk*fc)*ln(L1/L2) by Kick's law
16
17 Ck = (13.0)/log(50/10); //Ck = Kk*fc
18
19 //Energy required to crush the material from 75mm to
       25 \mathrm{mm}
20 \text{ Ek} = \text{Ck} * \log (75/25);
21 printf("\nThe energy required for crushing the
      material from average particle size of by Kicks
      law 75mm to 25mm is \%fkj/kg \n",Ek);
22 printf("\n The size range required is that for
      coarse crushing and Kicks law more closely
      relates the energy required for plastic
      deformation before fracture occurs so the energy
      calculated as that by Kicks law will be taken as
      the more reliable result \n");
```

Scilab code Exa 2.2 Maximum size of the particle

```
1 clear;
2 clc;
3 printf("\n Example 2.2");
4 //Calculating the maximum size of the particle that
        can be fed to the rollers.
5 //Given angle of nip = 31 degree
6 //Given diameter of the crushing rolls = 1m
7 //Distance between the crushing rolls is 12.5mm
8 r1 = 0.5; // size of crushing rolls is in meters
9 b = 0.00625; // Distance between the crushing rolls is
        0.0125mm
10 r2 = (r1 + b)/(cos((%pi/180)*15.5))-0.5;
11 printf("\nThe maximum size of the particles which
        should be fed to the rollers : %d mm",r2*10^3);
```

```
12
13 // Calculating the throughput at 2.0 Hz when the
        actual capacity of the machine is 12%.
14 // Working face of the rolls are 0.4m long
15 // bulk density of the feed is 2500kg/m^3
16 printf("\nThe cross sectional area for flow is %.3 f
        m^2",0.0125*0.4);
17 printf("\nThe volumetric flow rate is %.2 f m^3/sec"
        ,2.0*0.005);
18 printf("\nThe actual throughput is %d kg/sec"
        ,0.010*12*2500/100);
```

Scilab code Exa 2.3 Proposed modifications in ball mill

```
1 clear;
2 clc;
3 printf("\n Example 2.3");
4 //Given diameter of the ball mill is 1.2 meters
5 //Speed of rotation is 0.80Hz
7 // for small particles effective radius is 0.6 meters
8 //critical speed of the rotation
               //acceleration due to gravity is in m
9 g=9.80;
      ^2/\sec .
                //effective radius of rotation is in
10 r=0.6;
     meters.
11 w = sqrt(g/r);
12 printf("\nThe critical speed of the rotation is \%.2 f
       rad/sec",w);
13 f=w/(2*\%pi); //f is the frequency of the rotation
     and is in Hz
14 printf("\nThe critical frequency of the rotation is
     %fHz\n",f);
15 optimum_frequency = 0.6*f;
16 printf ("The optimum frequency of the rotation is \%.2
```

```
f Hz",optimum_frequency);
17 printf("\nGiven frequecy of the rotation is 0.80Hz\n
    ");
18 printf("The frequency of the rotation should be halved\n");
19 printf("Therefore the optimal frequency is half the critical frequency");
```

Motion of particles in a fluid

Scilab code Exa 3.1 terminal velocity

```
1 clear all;
2 clc;
3 printf("\n Example 3.1");
       d = 0.00040; //Diameter of the particle in m
                      //Density of the fluid in kg/m<sup>3</sup>
5
       p1 = 820;
       meu = 0.01; // Viscosity of the fluid in N s/m
       p2 = 7870;
                    //Density of steel in kg/m<sup>3</sup>
       g = 9.81;
                     //Acceleartion due to gravity in m
         / \sec^2
  //Computation of terminal velocity of a spherical
      particle
10 function[x]=galileo_number()
11
12
       x = (2*d^3*(p2-p1)*p1*g)/(3*(meu)^2); //x = (Ro/
          pu^2)*Re^2
13
       funcprot(0);
14 endfunction
15 x = galileo_number();
16 printf("\n The value of (Ro/pu^2)/Re^2 is \%f\n",x);
17
```

Scilab code Exa 3.2 Estimation of galena

```
1 clear;
2 clc;
3 printf("\n Example 3.2");
4 u_{\text{water}} = 5*10^{(-3)}; //The flow velocity of the
     water in m/sec
5 p_{galena} = 7500;
                        //The density of galena is in
     kg/m^3
6 p_limestone = 2700; //The density of limestone is
     in kg/m^3
7 viscosity = 0.001; //The viscosity of water in N
     s/m^2
8
9 //calculating maximum value of reynold's number
      considering 5mm particle size
10 Re_max = (u_water*1000*0.0001)/(viscosity);
11 printf("\n The maximum permissible value of Re is %f
     ", Re_max);
12
13 //maximum particle size of galena which will be
     carried away by water
14 d = sqrt((u_water*(18*viscosity)))/((7500-1000)*9.81)
     );
```

```
15 printf("\nmaximum particle size of galena which will
       be carried away by water is \%.1 \text{ f um}, d*10^{(6)};
16
17 //maximum particle size of limestone which will be
      carried away by water
18 d1 = sqrt((u_water*(18*viscosity)))/((2700-1000))
     *9.81));
19 printf("\nmaximum particle size of limestone which
      will be carried away by water is %.1f um",d1
      *10^(6));
20
21
22 //From the given data 43% galena and 74% limestone
      will be removed .
23 //Given that in the feed there is 20\% galena and 80\%
       limestone
24 //Assuming 100g feed
25 printf("\n nIn the overflow:");
26 printf("\nAmount of galena is \%fg",(20*0.43));
27 printf("\nAmount of limestone is \%fg",(80*0.74));
28 printf("\nconcentration of galena is %.1f per cent"
      ,(20*0.43*100)/(20*0.43+80*0.74));
29 printf("\n\concentration of galena is %fper cent"
      ,(80*0.74*100)/(20*0.43+80*0.74));
30 printf("\nnIn the underflow:")
31 printf("\nconcentration of galena is %.1f percent"
      ,(20*(1-0.43)*100)/(20*(1-0.43)+80*0.26))
32 printf("\nconcentration of limestone is %.1f per
     cent", (80*0.26*100)/(20*0.57+80*0.26))
```

Scilab code Exa 3.3 terminal velocity

```
1 clear;
2 clc;
3 printf("\n Example 3.3");
```

```
4 \min_{\text{area}} =6*10^{(-6)};
                              //minimum area of mica
      plates in m<sup>2</sup>
5 \text{ max\_area} = 6*10^{(-4)};
                              //maximum area of mica
      plates in m<sup>2</sup>
6 p_{oil} = 820;
                              //density of the oil in kg/m
                             //Viscosity is in N s/m<sup>2</sup>
7 \text{ Viscosity} = 0.01;
8 p_mica = 3000;
                             //Density of mica in kg/m<sup>3</sup>
                   smallest particles
10 printf("\n
                                    largest particles");
                    %fm^2
11 printf("\nA:
                                                         \%fm<sup>2</sup>
       ", min_area, max_area);
12 printf("\ndp: %fm
                                                           %fm
      ", sqrt (4*min_area/(%pi)), sqrt (4*max_area/(%pi)));
13 printf ("\ndp 3:\%f*10 (-8)m3
                                                %f*10^{(-5)}m^3
      ", sqrt(4*min_area/(%pi))^(3)*10^(8), sqrt(4*
      max_area/(%pi))^(3)*10^5);
14 printf("\nv:
                   %f*10^9m^3
                                                   %f*10^7m^3
      ",0.285*sqrt(4*min_area/(%pi))^(3)*10^(9),sqrt(4*
      \max_{\text{area}}/(\%\text{pi}))^{(3)}*(10^{7})*0.0285);
15 printf("\nk:
                   \% f
                                                             \%f
      ",0.285,0.0285);
16
17 \text{ x1} = (4*0.285/(\%pi*0.01^2))*(3000-820)
      *(820*2.103*10^(-8)*9.81);
18 \times 2 = (4*0.0285/(\%pi*0.01^2))*(3000-820)
      *(820*2.103*10<sup>(-5)</sup>*9.81);
19 printf("\n(Ro/pu^2)Reo^2 is %d for the smallest
      particles and %d for the largest particles",x1,x2
      );
20 //From table 3.4 Re for smallest particle is 34.9
      and that for the largest particle is 361
```

```
21 u1 = 34.9*0.01/(820*2.76*10^(-3));
22 printf("\nTerminal velocity for the smallest
        particle is %.3 f m/sec",u1);
23 u2 = 361*0.01/(820*2.76*10^(-2));
24 printf("\nTerminal velocity for the largest particle
        is %.3 f m/sec",u2);
25 printf("\n\n Thus it is seen that all the particles
        settle at approximately the same velocity");
```

Scilab code Exa 3.4 Approximate distance travelled

```
1 clear;
2 clc;
3 printf("\n Example 3.4");
4 v_particle = 6; //velocity of the particle in m/sec
                    //veloicity of the water in m/sec
5 v_water = 1.2;
6 v_rel = v_particle - v_water; // relative velocity of
      particles relative to the fluid in m/sec
  Re1 = 6*10^{(-3)}v_rel*1000/(1*10^{(-3)}); //Re1 is the
      reynold's no.
8 printf("\nReynold no. is %d", Re1);
10 //When the particle has been retarded to a velocity
      such that Re=500
11 vdot = (v_rel*500)/Re1;
12 printf("\nParticle velocity is \%.3 \text{ f m/sec} \ ", ydot);
13 c = 0.33/(6*10^{-3})*(1000/2500);
14 f = sqrt((3*6*10^{(-3)}*(2500-1000)*9.81)/1000);
15 function[y]=Fa(t)
      y = (-1/22)*(\log(\cos(0.517*22*t) + 4.8/0.517*\sin(0.517*sin))
16
         (0.517*22*t));
      funcprot(0);
17
18 endfunction
19
20 function[yd]=deriv(t)
```

```
21
       yd = -0.083 + (0.517 * (9.28 * cos (11.37 * t) - sin
           (11.37*t))/(\cos(11.37*t) + 9.28*\sin(11.37*t))
          );
       funcprot(0);
22
23 endfunction
24
25 function[ydd]=double_deriv(t)
       ydd = -0.517*(11.37)^2*(9.28*cos(11.37*t) - sin
26
           (11.37*t))/(\cos(11.37*t) + 9.28*\sin(11.37*t))
       funcprot(0);
27
28 endfunction
29
30
31 \text{ told = 0};
32 while 1
       tnew = told - deriv(told)/double_deriv(told);
33
34
       if (tnew == told) then
            y = Fa(told);
35
36
            d = y;
37
            printf("\nThe distance moved with speed less
                than 0.083 \text{m/sec} is \%.3 \text{fm},d);
38
            t=told;
            printf("\n The time taken by particle to
39
               move this distance is \%.3 fsec",t);
40
            break;
41
       end
42
       told = tnew;
43 end
44
45
46 printf("\nThe distance moved by the particle
      relative to the walls of the plant %.3fm",1.2*t -
       d);
```

Scilab code Exa 3.5 maximum size of crystals

```
1 clear;
2 clc;
3 printf("\n Example 3.5");
4 //rate of dissolution of salt
5 function[x]=dissolution(d)
      x = (3*10^{(-6)}) - (2*10^{(-4)}*3.406*10^{(5)}*d^2);
      funcprot(0)
8 endfunction
10 //rate of falling of the particle in stokes law
      region
11 function[y]=rate_h(d)
       y = 3.406*d^2(2)/(-3*10^(-6)-68.1*d^2); //y is in
12
       funcprot(0);
13
14 endfunction
15
16 printf("\n By trial and error the solution for d is
      0.88 \text{ mm}");
17 printf("\n The rate of dissolution is \%f",
     dissolution (8.8*10*(-4));
18 printf("\n The rate of falling of the particle is %f
      m/sec", rate_h(8.8*10^(-4)));
```

Flow of fluids through granular beds and packed columns

Scilab code Exa 4.1 pressure calculation

```
1 clear;
2 clc;
3 printf("\n Example 4.1");
4 // Calculating modified reynold's no.
                           //it is in m^2/m^3
5 a = 800;
6 Product_rate = 0.5;
                       //it is in g/sec
7 Reflux_ratio = 8;
8 Vapour_rate = 4.5; //it is in g/sec
9 G = (4.5*10^{(-3)})/((\%pi/4)*(0.1^2));// units are in
     kg/m^2.sec
10 meu = 0.02*10^{(-3)};
                                      //units are in Ns/
     m^2
11 e = 0.72;
12
13 Re1 = G/(800*0.28*0.02*10^{-3});
14 printf("\n The modified reynolds no. is %d", Re1);
15
16 x = 4.17/\text{Re}1 + 0.29; //x = R1/(pu1^2)
17 printf("\n The value of R1/(pu1^2) is %f",x);
```

Sedimentation

Scilab code Exa 5.1 Minimum area of thickener

```
1 clear;
2 clc;
3 printf("\n Example 5.1");
4 //Basis 1 kg of solids
5 feed_rate_solid = 1.33; //Mass rate of feed of
      solids in kg/sec
6 U = 1.5;
                             //Mass rate of solids in
     the underflow in kg/sec
7 Y = [5.0 ; 4.2; 3.7 ; 3.1; 2.5];
8 printf("\n concentration(Y) (kg water/kg solids):\n"
     );
9 printf("\%.1 f\n",Y);
10 printf("\n water to overflow (Y-U) (kg water/kg
      solids):\n");
11 O = Y - 1.5; //Amount of water to overflow in kg
      water/kg solids
12 printf("\n %.1 f\n",0);
13 Uc = [2.00*10^{(-4)};1.20*10^{(-4)};0.94*10^{(-4)}]
      ;0.70*10^{(-4)};0.50*10^{(-4)};
14 printf("\n sedimentation rate uc (m/sec):\n");
15 printf("\%f \n",Uc);
```

Scilab code Exa 5.2 Sedimentation velocity and solids flux

```
1 clear;
2 clc;
3 printf("\n Example 5.2");
4 // Area of the tank required to give an underflow
      concentration of 1200kg/m<sup>3</sup> for a feed rate of 2
     m^3/min
6 //Initial height of slurry in the tank
7 H =
      [900;800;700;600;500;400;300;260;250;220;200;180];
8 uc =
      [13.4;10.76;8.6;6.6;4.9;3.2;1.8;1.21;1.11;0.80;0.60;0.40];
9 i = 1;
10 while i<13
       c(i) = 200*900/H(i);
11
12
       x(i)=1000*(1/c(i)-1/1200);
```

```
13
        sed(i) = c(i)*uc(i)/(1000*60);
        y(i) = uc(i)*10^(-3)/((1/c(i)-1/1200)*60);
14
15
        z(i) = 1/y(i);
16
        i=i+1;
17 \text{ end}
18 printf("\nH(mm)");
19 printf("\n\%d",H);
20 printf("\n c(\kg/m^3):\n");
21 printf("%d\n",c);
22 printf ("Sedimentation flux (kg.s/m<sup>2</sup>):\n");
23 printf("\%.4 f\n",x);
24 printf("uc/(1/c-1/1200) \setminus nkg.sec/m^2: \setminus n");
25 printf("\%.4 f\n",y);
26 printf("1000*(1/c-1/cu)\nm^3/kg*10^3\n");
27 printf("\%.3 f \n",x);
28 printf("\ln (1/c-1/1200)/uc \ln m^2.kg/sec \ln");
29 printf("\%.1 f\n",z);
30 \text{ m1} = \text{max}
      ([18.7;20.1;21.3;22.7;23.8;26.0;27.8;30.3;30.0;29.2;27.8;25.0])
31 printf("\n nthe maximum value of (1/c-1/1200)/uc is
      \%.1 \text{ f m}^2 * \text{kg/s}, \text{m1};
32 A = 2*200*30.3/60;
33 printf("\n The area required is A = Qc[(1/c-1/cu)/uc]
      ]\max = \%dm^2, A)
```

Scilab code Exa 5.3 Rate of deposition and maximum flux

```
1 clear;
2 clc;
3 printf("\t Example 5.3 ");
4 //Assumption: Resistance force F on an isolated
        sphere is given by Stoke's law:F = 3*%pi(meu)d*u
5
6 C = poly([0], 'C');
```

```
7 \text{ x=roots}(-4.8*C+(1-C));
8 printf("\n concentration is:\%.3 f",x);
10 //terminal falling velocity u can be calculated by
      force balance
11 / u = d^2*g/(18*meu)*(ps-p)
12 function[u] = terminal_velocity()
       d = 10^{(-4)};
                        //diameter is in meters
13
       g = 9.81;
                         //acceleration due to gravity is
14
          in m/\sec^2
       meu = 10^{(-3)}; // viscosity is in N.s/m<sup>2</sup>
15
       ps = 2600;
                        //density is in kg/m<sup>3</sup>
16
17
       p = 1000;
                         //density is in kg/m<sup>3</sup>
18
       u = (d^2)*g*(ps-p)/(18*meu);
19
       funcprot(0);
20
21 endfunction
22
23
24 function[si]=si_max()
25
       u=terminal_velocity()
       printf("\n The terminal falling velocity is %.5f
26
           m/sec",u);
        si=u*x*(1-x)^(4.8);
27
       funcprot(0);
28
29 endfunction
30 si = si_max();
31 printf("\nThe maximum value is \%f*10^{(-4)} m<sup>3</sup>/m<sup>2</sup>sec
      ",si*10^4)
```

Fluidisation

Scilab code Exa 6.1 minimum fluidising velocity

```
1 clear;
2 clc;
3 printf("\n Example 6.1");
4 // Calculating minimum fluidisation velocity
6 // Calculating Galileo number
7 function[Ga] = Galileo_number()
       d = 3*10^{(-3)}; //particle size is in meters
                         //density of liquid is in kg/m<sup>3</sup>
       p = 1100;
9
                         //density of spherical particles
10
       ps = 4200;
           is in kg/m<sup>3</sup>
                       //acceleration due to gravity is
11
       g = 9.81;
           in m/sec^2
12
       u = 3*10^{(-3)}; //viscosity is in Ns/m<sup>2</sup>
       Ga = d^3*p*(ps-p)*g/u^2;
13
14
       funcprot(0);
15 endfunction
16 Ga = Galileo_number();
17 printf("\nGalileo number = \%f*10^5", Ga*10^(-5));
18
19 // Calculating Re mf
```

```
20 Remf = 25.7*(sqrt(1+5.53*10^(-5)*(1.003*10^5))-1);
21 printf("\nValue of Remf is %d",Remf);
22
23 umf = Remf*(3*10^(-3))/(3*10^(-3)*1100);
24 printf("\nminimum fluidisation velocity is %.1f mm/sec",umf*1000);
```

Scilab code Exa 6.2 fluidisation and transport of particles

```
1 clear;
2 clc;
3 printf("\n Example 6.2");
4 // Calculating voidage by considering eight closely
      packed spheres of diameter d in a cube of size 2d
5 printf("\n (a)");
6 function[e]=voidage()
       d = 1*10^{(-4)};
                        //diameter is in meters
       meu = 3*10^(-3); //viscosity is in Ns/m<sup>2</sup>
8
                          //density is in kg/m<sup>3</sup>
9
       ps = 2600;
       p = 900;
                          //density is in kg/m<sup>3</sup>
10
11
       e = [8*d^{(3)}-8*(\%pi/6)*d^{(3)}]/(8*d^{(3)});
12
       funcprot(0);
13 endfunction
14 e = voidage();
15 printf("\nvoidage = \%.2 \, \text{f}",e);
16
17 // Calculating minimum fluidisation mass flow rate
18
19 function[Gmf]=min_fluidis_vel()
20
       e = voidage();
                        //diameter is in meters
21
       d = 1*10^{(-4)};
       meu = 3*10^(-3); // viscosity is in Ns/m^2
22
                          //density is in kg/m<sup>3</sup>
23
       ps = 2600;
24
       p = 900;
                          //density is in kg/m<sup>3</sup>
25
       g = 9.81;
                          //acceleration due to gravity
```

```
is in m/sec^2
26
       Gmf = 0.0055*(e)^{(3)}/(1-e)*(d^{2})*p*(ps-p)*g/meu;
27
       funcprot(0);
28 endfunction
29 Gmf = min_fluidis_vel();
30 printf("\nminimum fluidisation velocity is %.3 f kg/m
      ^2 \sec ", Gmf);
31
32
33 printf("\n (b)");
34 function[u]=terminal_velocity()
35
       e = voidage();
36
       d = 1*10^{(-4)};
                         //diameter is in meters
       meu = 3*10^(-3); //viscosity is in Ns/m<sup>2</sup>
37
                          //density is in kg/m<sup>3</sup>
       ps = 2600;
38
       p = 900;
                          //density is in kg/m<sup>3</sup>
39
       g = 9.81;
                           //acceleration due to gravity
40
          is in m/sec^2
       u = d^{(2)}*g*(ps-p)/(18*meu);
41
42
       funcprot(0);
43 endfunction
44 printf("\nterminal velocity is %.4fm/sec",
      terminal_velocity());
45
46 //Reynolds no for this Terminal velocity is
47 Re = (10^{(-4)}*0.0031*900)/(3*10^{(-3)});
48 printf("\nReynlds no =%.3f", Re);
49 printf("\nThe required mass flow rate is \%.2 f kg/m^2
      sec",terminal_velocity()*900);
```

Scilab code Exa 6.3 Voidage of the bed

```
1 // to calculate voidage of the bed
2 clear;
3 clc;
```

```
4 printf("\n Example 6.3");
5 function[Ga] = Galileo_number()
       d = 4*10^{(-3)}; // particle size is in meters
                          //density of water is in kg/m<sup>3</sup>
7
       p = 1000;
                         //density of glass is in kg/m<sup>3</sup>
8
       ps = 2500;
       g = 9.81;
                         //acceleration due to gravity is
           in m/\sec^2
       u = 1*10^{(-3)};
                         //viscosity is in Ns/m<sup>2</sup>
10
       Ga = d^3*p*(ps-p)*g/u^2;
11
12
       funcprot(0);
13 endfunction
14 printf ("\nGalileo number = \%.2 \text{ f}*10^5", Galileo_number
      ()*10^{(-5)};
15
16 function [Re] = Reynolds_no()
       Ga = Galileo_number();
17
       Re = (2.33*Ga^(0.018)-1.53*Ga^(-0.016))^(13.3);
18
19
       funcprot(0);
20 endfunction
21 printf("\n The Reynolds no is %d", Reynolds_no());
22 \text{ v} = \text{Reynolds\_no()}*(1*10^(-3))/(0.004*1000);
23 printf("\nvelocity = \%.2 \text{ f m/sec}",v);
24
25 n = poly([0], 'n');
z = roots((4.8-n)-0.043*(Galileo_number())^(0.57)*(n)
      -2.4));
27 printf("\nvalue of n is \%.2 f",z);
28
29 //voidage at a velocity is 0.25m/sec
30 e = 0.1;
31 while 1
       enew = e -((0.25/0.45)-e^{(2.42)})/(-2.42*e^{1.42});
32
       if (enew == e) then
33
            printf("\nVoidage is %.3f",e);
34
35
            break:
36
       end
37
       e=enew;
38 end
```

Scilab code Exa 6.4 slope of adsorption isotherm

```
1 clear;
2 clc;
3 printf("\n Example 6.4");
4 t = 250:250:2000; //time is in secs
5 y =
      [0.00223; 0.00601; 0.00857; 0.0106; 0.0121; 0.0129; 0.0134; 0.0137];
6
7 i = 1;
8 \text{ yo} = 0.01442;
9 while i<9
10
       z(i) = y(i)/yo;
       y(i)=1-z(i);
11
       x(i) = log(y(i));
12
13
       i=i+1;
14 end
15 xtitle("slope of adsorption isotherm", "Time(sec)","
      \log (1 - (y/yo))")
16 plot(t,x,"o-")
17 printf("\nFrom the graph the value of slope is \%f"
      ,-0.00167);
                           //units are in kmol/sec
18 Gm = 0.679*10^{(-6)};
19 W = 4.66;
                           //units are in gram
20 b = poly([0], 'b');
21 \text{ s} = \text{roots}(-0.00167*4.66*b+0.679*10^(-6));
22 printf("\n b = \%.4 \text{ f kmol/kg}",s*10^3);
```

Scilab code Exa 6.5 Coefficient of heat transfer between gas and the particles

```
1 clear;
2 clc;
3 printf("\n Example 6.5");
4 gas_flow_rate =0.2;
                                 //units are in kg/m<sup>2</sup>
5 c = 0.88;
                                  //specific heat capacity
      of air is kj/kg K
6 viscosity = 0.015*10^{(-3)}; //viscosity is in Ns/m^2
7 d = 0.25*10^{(-3)};
                                 //particle size is in
      meters
                                 //thermal conductivity is
8 k = 0.03;
      in W/m K
                                  //e is voidage
9 e = 0.57;
10
11 T = [339.5; 337.7; 335.0; 333.6; 333.3; 333.2]; //
      temperature is in kelvins
12 \text{ deltaT} = T - 333.2;
13 h = [0; 0.64; 1.27; 1.91; 2.54; 3.81];
14 xtitle ("temperature rise as a function of bed height
      ", "height above bed support (mm)", "deltaT (K)");
15 plot(h, deltaT, 'o-');
16
17 // Area under the curve gives the value of the heat
      teansfer integral =8.82mm K
18
19 \quad q = 0.2*0.88*(339.5-332.2);
20 printf("\n heat transferred = \%.2 \,\text{f kw/m}^2 of bed
      cross sectional area",q);
21
22 //Assuming 1m<sup>3</sup> volume
                           //Volume of particles is in m<sup>3</sup>
23 \text{ Vp} = (1-0.57);
24 printf("\n Volume of particles is \%.2 \text{ f m}^3", Vp)
                        //Volume of 1 particle in m<sup>3</sup>
25 \text{ v1} = (\%\text{pi/6})*\text{d}^3;
26 printf("\n Volume of 1 particle is \%.2 f*10^(-12) m<sup>3</sup>
      ", v1*10^(12));
27 printf("\n number of particles is \%.2 \, f*10^{(10)}", Vp/
      v1*10^{(-10)};
28
29 x = poly([0], 'x');
```

```
30 h = roots(1100 - x*(1.03*10^4)*(8.82*10^(-3)));
31 printf("\n heat transfer coefficient = %.1 f W/m^2",h
      );
32
33 //Nu = 0.11Re^(1.28)
34 Re = (0.2*0.25*10^(-3))/(0.015*10^(-3));
35 h1 = 0.11*(Re)^(1.28)*k/d;
36 printf("\n h = %.1 f W/m^2 K",h1);
```

Scilab code Exa 6.6 Volumetric fraction of the bed carrying out evaporation

```
1 clear;
2 clc;
3 printf("\n Example 6.6");
                                                //specific
4 \text{ cp} = 0.85;
      heat capacity of the air
5 h = [0 0.625 1.25 1.875 2.5 3.75];
                               //height in mm
6 T=[339.5 337.7 335.0 333.6 333.3 333.2];//
      temperature in K
7 \text{ deltaT} = T - 333.2;
      temperature difference in kelvins
8 plot(h,deltaT,"o-");
9 xtitle ("deltaT as a function of bed height", "Height
      above bed support z(mm)", "Temperature difference
      deltaT (K)");
10 //From the plot area under the curve is 6.31 K mm
11 sp = (6/(0.25*10^{-3}))*(0.5);
                                      //sp is surface area
       per unit volume in m<sup>2</sup>/m<sup>3</sup>
12 G = 0.2;
                                       //in kg/m^2 sec
                                       //Cp is in J/kg K
13 \text{ Cp} = 850;
14 \text{ h1} = poly([0], 'h1');
15 \text{ s} = \text{roots}(0.2*850*6.3-h1*1.2*10^(4)*6.31*10^(-3));
16 printf(" \n Coefficient for heat transfer between
```

```
the gas and the particles= \%.1 \,\mathrm{fW/m^2} K",s);
17
18 printf("\n Let the evaporation rate be 0.1 kg/sec at
       a temp difference = 50 \text{ degK}");
19 \text{ mdot} = 0.1;
                           //evaporation rate is 0.1 kg/sec
20 Latent_heat = 2.6*10^(6);
21 printf("\n The heat flow = \%.1\,f*10^5\ W', mdot*
      Latent_heat *10^(-5);
22 A = (2.6*10^5)/(14.1*50);
23 printf("\n the effective area of the bed A = \%d \text{ m}^2"
       ,A);
24 printf("\n The surface area of the bed = \%d m<sup>2</sup>"
       ,0.1*1.2*10^4);
25 printf("\n hence the fraction of the bed = \%.2 \,\mathrm{f}"
      ,369/1200);
```

Chapter 7

Liquid filtration

Scilab code Exa 7.1 volume of filtrate collected per cycle

```
1 clear;
2 clc;
3 printf("\n Example 7.1");
4 //In the leaf filter filtration is at const pressure
       from the start
5 //V^2 + 2ALV/v = 2(-deltaP)A^2t/(ruv)
7 //In the filter press, a volume V1 of filtrate is
      obtained under const rate conditions in time t1,
      and filtration is then carried out at constant
      pressure.
8 //V1^2 + 2ALV1/v = 2(-deltaP)A^2t1/(ruv)
9 //and (V^2 V1^2) + 2AL/ (V V1) = 2(P)A
      ^2/ r (t t1)
10
11 //for the leaf filter
12 t2 = 300;
                      //t2 is in secs
13 V2 = 2.5*10^(-4); //V2 is in m<sup>3</sup>
14 t3 = 600;  //t3 is in secs
15 V3 = 4*10^(-4);  //V3 is in m^3
16 A = 0.05;
                        //A is in m^2
```

```
17 deltaP = -7.13*10^{(4)}; //it is in N/m<sup>2</sup>
18 //putting these values in above eq
19
20 a = [2*7.13*10^{(4)}*0.05^{(2)}*300 -2*0.05*2.5*10^{(-4)}
      ;2*7.13*10^{(4)}*0.05^{(2)}*600 -2*0.05*4*10^{(-4)};
21 b = [(2.5*10^{(-4)})^2; (4*10^{(-4)})^2];
22 x = inv(a)*b;
23 y = [1/x(1);x(2)];
24 printf ("\n L/ =\%f*10^(-3) and r = \%f*10^(11)"
       ,y(2)*10^3,y(1)*10^(-11));
25
26 //for the filter press
27 \text{ V1} = poly([0], 'V1');
28 \text{ s} = \text{roots}(V1^2 + (2.16*y(2)*V1) - (4*10^(5)*2.16^2)/y
      (1)*180);
29 printf("\n the value of V1 = \% \text{fm}^3",s(2));
30
31 //For a constant pressure period (t - t1) = 900 \text{ secs}
32 // Calculting the total volume of filtrate
33 \ V = poly([0], 'V');
34 d = roots((V^2-3.33*10^(-4))+(1.512*10^(-2)*(V
      -1.825*10^{(-2)} -5.235*10^{(-6)}*900);
35 printf("\n The value of V = \%.3 \, \text{f m}^3", d(2));
36
37 f = (4*10^{(5)}*(2.16)^{(2)}/(7.13*10^{(11)}*(6.15*10^{(-2)})
      + 2.16*3.5*10^(-3)));
38 printf("\n The final rate of filtration is %.2f
      *10^{(-5)} \text{ m}^3/\text{sec}, f*10^(5));
39
40 // Assuming viscosity of the filtrate is the same
      as that of the wash-water
41 \text{ rw}_400 = (0.25)*f;
42 printf("\n Rate of washing at 400 kN/m2 = \%.1 f
      *10^{(-6)} \text{ m}^3/\text{sec}, rw_400*10^(6));
43
44 \text{ rw}_275 = \text{rw}_400*(275/400);
45 printf("\n Rate of washing at 275 kN/m<sup>2</sup> = \%.1 f
      *10^{(-6)} m<sup>3</sup>/sec", rw_275*10<sup>6</sup>;
```

```
46 printf("\n Thus the amount of wash-water passing in 600s = \%.3 \text{ f m}^3", 600*rw_275);
```

Scilab code Exa 7.2 Effect on optimium thickness of the cake

```
1 clear;
2 clc;
3 printf("\n Example 7.2");
4 //The slurry contains 100kg whiting/m<sup>3</sup> of water
5 printf("\n Volume of 100 kg whiting = \%f m^3"
       ,100/3000);
6 printf("\n Volume of cake = \%f m^3",0.0333/0.6);
7 printf("\n Volume of liquid in cake = \%f m^3"
      ,0.05556*0.4);
8 printf("\n Volume of filtrate = \%.3 \, \text{f m}^3", (1-0.0222)
9 printf("\n volume of cake/volume of filtrate v = \%f"
      ,0.0556/0.978);
10 A = 10^{(-4)};
                                     //area in sq meters
11 deltaP = -1.65*10^{(5)};
                                     //P is in pascals
12 \ 1 = 0.01;
                                     //length is in meters
13 vol_flow_rate = 2*10^(-8);
                                              //Volume flow
      rate is in m<sup>3</sup>/sec
14 u = 10^{(-3)};
                                     //vicosity is in Ns/m<sup>2</sup>
15
16 r = poly([0], 'r');
17 \text{ r1} = \frac{\text{roots}((10^4)*(2*10^(-8)*r)-1.65*10^(5)}{(10^(-5))}
18 printf("\n r = \%.2 \text{ f} *10^{(13)} / \text{m}^2", r1*10^(-13));
19
20 function [Lopt] = optimum()
        Lopt = 1.161*10^{(-3)}*(900)^{(0.5)}; //t = 900
21
           secs
22
        funcprot(0);
23 endfunction
```

Scilab code Exa 7.3 Time taken to produce 1 m3 of filtrate and pressure in this time

```
1 clear;
2 clc;
3 printf("\n Example 7.3");
                      //volume in m<sup>3</sup>
4 V = 0.094;
5 deltaP = -3530; //P is in kN/m^2
7 / At t = 1105 secs
  V1 = 0.166;
                       //V is in m<sup>3</sup>
    deltaP1 = -5890; //P is in kN/m^2
9
10
11 a = [2.21*10^{(6)} -0.094; 6.51*10^{(6)} -0.166];
12 b = [0.0088; 0.0276];
13 x = inv(a)*b;
14 y = [x(2); x(1)];
15 printf("\n LA/v = %f A^2/r v = \%f*10^(-7)", y
      (1), y(2)*10^7);
16 printf("\n For the full size plant:");
17 printf ("\n LA/v = %f A^2/r v = %f*10^(-7)", 10*y
      (1), y(2)*10^8;
18
```

Scilab code Exa 7.4 Speed of rotation for maximum throughput

```
1 clear;
2 clc;
3 printf("\n Example 7.4");
4 a = [2*84300*0.02^{(2)}*60]
      -2*0.02*0.0003;2*84300*0.02^(2)*120
      -2*0.02*0.00044];
5 b = [0.0003^2; 0.00044^2];
6 x = inv(a)*b;
7 y = [x(2); 1/x(1)];
8 printf("\n L/v = \%f
                           ruv = \%f*10^{(10)}, y(1), y
      (2)*10^{(-10)};
9 printf("\n Area of filtering surface = \%f m^2", 4*(
      %pi));
10 printf("\n Bulk volume of cake deposited =\%.3 f m\^3/
      revolution",4*(%pi)*0.005);
11
12 V = sqrt(1*10^{-6})*143^{2};
13 printf("\n V = \%.3 \, \text{f m}^3", V);
14
15 t =poly([0],'t');
16 	 t1 = roots(0.141^2 + 2*2.19*10^{-3})
      *0.141-2*84300*(4*(%pi))^(2)*t/(3.48*10^10));
17 printf("\n t = \%f secs",t1);
18 printf("\n time for 1 revolution =\%.1 f secs", t1/0.4)
```

Scilab code Exa 7.5 Optimum filtration time for maximum throughput

```
1 clear;
2 clc;
3 printf("\n Example 7.5");
                                  //V is in m<sup>3</sup>
4 V1 = 0.00025;
5 t = 300;
                                  //t is in secs
6 = [7.14*10^{-6}] 2.86*10^{-4}; 11.42*10^{-6}
      2.86*10^(-4)];
  b = [1.2*10^{(6)}; 1*10^{(6)}];
8 x = inv(a)*b;
10 //for the plate and frame filter
11 B1 = x(1)/(2*2.2^2*413*10^3);
12 B2 = x(2)/(2.2*413*1000);
13
14 printf("\nr v = %d\n",x(1));
15 printf("\n r l = \%d", x(2));
16 printf("\n B1= \%f B2= \%f", B1, B2);
17 printf("\n the filtration time for maximum
      throughput is:");
18 \ t1 = 21.6*10^3;
19 t0 = t1 + B2*(t1/B1)^(0.5);
20 printf("\n t = \%f secs",t0);
21 V = (t1/B1)^{(0.5)};
22 printf("\n V= \%f m^3",V);
23 printf("\nMean rate of filtration is: \%.2 \text{ f }*10^-6 \text{ m}
      ^3/s",(V/(t1+t0))/10^-6);
```

Scilab code Exa 7.6 Thickness of cake produced

```
1 clear;
2 clc;
3 printf("\n Example 7.6");
                     //in m^2
4 A=0.6*0.6*%pi;
5 rate=1.25*10^-4; // in m^3/s
6
7 v_w = 0.2/(3*10^3);
8 \text{ v_f} = 10^{-3} - \text{v_w};
10 v=v_w/v_f;
11 v_rate=rate*v;
12 \quad w = 360 * 0.2;
13
14 t=v_rate*w/A;
15 printf("\nThickness of cake produced is: %.1f mm",t
      /10^-4);
16 \text{ K} = poly([0], 'K');
17 K1 = roots((1.25*10^{-4})*360)^2-K*(6.5*10^{4})
      *(0.36*(%pi))^(2)*72));
18 printf("\n The value of K is \%.2 f*10^{(-10)}", K1
      *10^(10));
19
20 // Filter press
21 //Using a filter press with n frames of thickness b
     m the total time, for one complete cycle of the
      press = (tf+120n+240), where tf is the time during
      which filtration is occurring
22 //overall rate of filtration = Vf/(tf + 120n + 240)
23
24 // Vf = 0.3^{(2)}*n*b/0.143
25 / tf = 2.064*10^5 b^2
26
```

```
27 b = poly([0], 'b');
28 b1 = roots(b^2 - 0.0458*b - 0.001162);
29 printf("\n The thickness is \%.4 \,\mathrm{f} m", b1(1));
30
31 function[n]=number_of_plates()
32
33
       n = (0.030 + 25.8*b1(1)^2)/(0.629*b1(1)-0.015);
       funcprot(0);
34
35 endfunction
36 n = number_of_plates();
37 printf("\n The minimum number of plates required is
     %d", ceil(n));
38
39 d = poly([0], 'd');
40 	ext{ d1 = roots(ceil(n)*(0.629*d-0.015)-0.030-25.8*d^2);}
41 printf("\n The sizes of frames which will give
      exactly the required rate of filtration when six
      are used are \%f mm", d1*10^3);
42 printf("\n\n\n\n Thus any frame thickness between 47
      and 99 mm will be satisfactory. In practice, 50 mm
       (2 in) frames would probably be used.")
```

Scilab code Exa 7.7 Increase in the overall throughput of the press

```
1 clear;
2 clc;
3 printf("\n Example 7.7");
  //Case 1
5
                     //dV/dt = A^2(-deltaP)/vru(V + AL/v)
6
                        ) = a/V + b
7
                     //For constant rate filtration:
8
                     //Vo/to = a/Vo + b
9
                     //Vo^2 + bVo = ato
10
                     //For constant pressure filtration
```

```
//0.5(V^2 - Vo^2) + b(V-Vo) = a(t-to)
11
12
                      //to = 600s, t - to = 3600s, Vo = V/4
                      //V^2/16 + bV/4 = 600a
13
                      //o.5(V^2 - V^2/16) + b(V-V/4) = 3600a
14
15
                      //3600a = (15/32)V^2 + 3/4(bV) =
                         3/8(V^2) + 3/2(bV)
                     //b = V/8
16
                    // a = (V^2/16 + V^2/32)/600 =
17
                        (3/19200)V^2
                     // Total cycle time = 900 + 4200 =
18
                       5100 \sec s
19
                     //Filtration rate = V/5100 =
                       0.000196V
20
  //Case 2
21
                    //V1/t1 = a/(V1 +b/4)=Vo/to=a/(Vo+b)
22
                    //0.5*(49/64V^2 - V1^2)+b/4(7/8V-V1)
23
                       =a(t-t1)
                    //V/2400 = (3/19200)V^2/(V1+V/32)
24
25
                    //t1 = (to/Vo)V1
     t1 = 600/(1/4)*(11/32);
26
     printf(" \mid n t1 = \% dsecs", t1);
27
28
     //Substituting gives
29
     deltaT = (19200/3)*(784-121+34)/2048;
     printf("\n t -t1 = \%d \sec s", deltaT);
30
     Cycle_time = 180+900+t1+deltaT;
31
     printf("\n cycle time = %d secs", Cycle_time);
32
     Increase = (0.000214 - 0.000196)/(0.000196)*100;
33
     printf("\n Increase in filtration rate is %.1f per
34
         cent", Increase);
```

Chapter 8

Membrane Separation Processes

Scilab code Exa 8.2 Area of membrane and average flux

```
1 clear;
2 clc;
3 printf("\n Example 8.2");
5 //From the gel polarisation model:
              //J = (1/A) (dV/dt) = hD ln (Cg/Cf)
7
              //\mathrm{Cf} = \mathrm{Co}(\mathrm{Vo/V})
      //where Co and Vo are the initial concentration
         and volume, respectively and Cf and V are the
         values at subsequent times
9
     //Combining these eq gives
             //dV/dt = A(hDln(Cg/Co)-hDln(Vo/V))
10
11 \quad V = [10 \quad 5 \quad 3 \quad 2 \quad 1];
12 y = [9.90 \ 13.64 \ 18.92 \ 27.30 \ 112.40];
13 plot(V,y)
14 xtitle("Area under the curve is 184.4", "Volume(m<sup>3</sup>)"
      " (J - hDln (Vo/V))^(-1)")
15
16
```

```
17 //(b)
18 Jo = 0.04*log(250/20);
19 printf("\n Jo = %.3 f m/h", Jo);
20 Jf = 0.04*log(250/200);
21 printf("\n Jf = %f m/h", Jf);
22 Jav = Jf + 0.27*(0.101-0.008);
23 printf("\n Jav = %f m/h", Jav);
24 //For the removal of 9m^3 filtrate in 4 hours
25 Area = (9/4)/Jav;
26 printf("\n Area = %fm^2", Area);
```

Scilab code Exa 8.3 Minimum number of membrane modules required

```
1 clear;
2 clc;
3 printf("\n Example 8.3");
4 //It is assumed that Q0 is the volumetric flowrate
      of feed
5 // Q2 the volumetric flowrate of concentrate
6 //C0 the solute concentration in the feed
7 // C2 the solute concentration in the concentrate
8 // F the volumetric flowrate of membrane permeate
9 // A the required membrane area.
10 // It is also assumed that there is no loss of
      solute through the membrane.
11 \text{ Cl} = 3;
12 while 1
13
       Clnew = Cl - (0.04 - 0.02 * log (30/Cl)) / (Cl^(-1)/50);
       if Clnew == Cl then
14
15
           break;
16
       end
17
       Cl = Clnew;
18 end
       printf("\n Cl = \%d \text{ kg/m}^3",Cl);
19
20 printf("\n below this concentration the membrane
```

```
flux is 0.04 \text{ m/h}");
21
22 //This does not pose a constraint for the single
      stage as the concentration of solute C2 will be
      that of the final concentrate, 20 kg/m3.
23 //Conservation of solute gives:QoCo = Q2C2
\frac{24}{A} fluid balance gives : Qo = F + Q2
25 //Combining these eq and substituting Known values:
26 A = (2.438/0.02)/\log(30/20);
27 printf("\n A = \%d m^2", A);
28 //The tubular membranes to be used are available as
      30 \text{ m}^2 \text{ modules}.
29
  printf("\n the no of required modules are %d", A/30)
30
31
  //Part(b)
32
33 //Conservation of solute gives = QoCo = Q1C1 = Q2C2
34 //A fluid balance on stage 2 gives Q1 = Q2 + F2
35 //A fluid balance on stage 2 gives Q1 = Q2 + F2
36 //Substituting given values in above eqns
37 / 2.5 = 1.25/C1 + 0.02 A1ln (30/C1)
38 function[A1] = a(C1)
       A1 = (2.5-1.25/C1)/(0.02*\log(30/C1));
39
40
       funcprot(0);
41 endfunction
42 function [A2] = b(C1)
       A2 = (1.25/C1 - 0.0625)/0.00811
43
44
       funcprot(0);
45 endfunction
46
47 printf("\n The procedure is to use trial and error
      to estimate the value of C1 that gives the
      optimum values of A1 and A2");
  printf("\n If C1 = 5 \text{kg/m}^3 then A1 = \% \text{d m}^2 and A2 =
       \%d \text{ m}^2",a(5),b(5));
49 printf("\n an arrangement of 3 modules 1 module
      is required.");
```

- 50 printf("\n\n\n If C1 = 4 kg/m^3 then A1 = %dm^2 and A2 = %dm^2",a(4),b(4));
- 52 printf("\n\n\n If $C1 = 4.5 \text{ kg/m}^3 \text{ then } A1 = \%dm^2 \text{ and } A2 = \%d m^2 \text{",a(4.5),b(4.5)};$
- 53 printf("\n an arrangement of 2 modules 1 module which meets the requirement");
- 54 $printf("\n\n This arrangement requires the minimum number of modules.");$

Chapter 9

Centrifugal Separations

Scilab code Exa 9.1 Value of capacity factor

```
1 clear;
2 clc;
3 printf("\n Example 9.1");
4 d_particle = 5;
                               //particle size is in um
5 p = 1000;
                             //density of water in kg/m<sup>3</sup>
6 \text{ ps} = 2800;
                             //density of solids in kg/m
7 viscosity = 10^{(-3)}; //viscosity is in Ns/m^2
8 uo = ((d_particle*10^(-6))^2)*(ps-p)*9.81/(18*
      viscosity);
9 printf("\n Terminal falling velocity of particles of
       diameter = \%.2 \text{ f m/sec}", uo *10^5);
10 Q = 0.25;
                             //volumetric flow rate is in
      m^3/\sec c
11 printf("\n E = \%.2 \text{ f}*10^{(4)} \text{ m}^2",(Q/uo)*10^(-4));
12
13 printf("\n For coal-in-oil mixture");
14 \text{ uo1} = 0.04/(Q/uo);
15 printf("\n uo = \%.2 \text{ f}*10^--6 \text{ m/sec}", uo1*10^6);
16
17 d = sqrt((18*0.01*uo1)/((1300-850)*9.81));
```

```
18 printf("\n d = \%d um",(d/3)*10^6);
```

Scilab code Exa 9.3 TIme taken to produce filtrate

```
1 clear;
2 clc;
3 printf("\n Example 9.3");
4 //In the filter press
5 // V^2 + 2(AL/v)V = 2(-deltaP)A^2*t/(ruv)
                        //1 is in meters
7 1 = 0.025;
                        //L is in meters
8 L = 0.003;
9 \text{ deltaP} = 350;
                       //it is in N/m^2
10 t = 3600;
                        //t is in secs
11
12 // x = v/ru
13 x = poly([0], 'x');
14 \times 1 = roots(0.025^2 + 2*0.003*0.025 - 2*3.5*10^(5))
      *3600*x);
15 printf("\n the value of ru/v = \%.2 \text{ f}*10^12", (1/x1)
      *10^(-12));
16
17 //In the centrifuge
18 R = 0.15;
                            //R is in meters
                            //H is in meters
19 H = 0.20;
20 \quad V = 0.00225;
                            //V is in m^3
21 r = poly([0], 'r');
22 r1 = roots(\%pi*(R^2 - r^2)*H-V);
23 printf("\n Value of ro = \%f mm", r1(1)/2);
24 printf("\n angular frequency = \%.1 \, \text{frad/s}",(r1(1)
      /2*10<sup>3</sup>)*2*(%pi));
25
26 / (R^2 - r^2) (1+2L/R) + 2r^2 ln (r/R) = 2vtpw^2/ru (R^2 - ro)
27 t = poly([0], 't');
```

Chapter 10

Leaching

Scilab code Exa 10.1 Time required for solute to dissolve

```
1 clear
2 clc;
3 printf("\n Example 10.1");
4 //For the pilot scale vessel
                                //in kg/m^3
    c = (2.5*75)/100;
                                //in kg/m^3
    cs = 2.5;
    V = 1.0;
                                //V is in m^3
8
    t = 10;
                                //t is in secs
    //1.875 = 2.5(1 - e^{(-kA/b*100)})
10
    // x = kA/b
11
    x = -\log(1-1.875/2.5)/10;
12
13
14
    //For the full scale vessel
15
    c = (500*28/100)/100;
    printf("\n C = \%fkg/m<sup>3</sup>",c);
16
17
    cs = 2.5;
                                 // cs is in kg/m<sup>3</sup>
18
    V = 100;
                                 //V is in m^3
    t = -\log(1-1.4/2.5)*(100/0.139); //t is in secs
19
20
    printf(" \mid n \mid t = %d \mid secs", t);
```

Scilab code Exa 10.2 Rate of feed of neutral water to the thickeners

```
1 clear;
2 clc;
3 printf("\n Example 10.2");
5 // If x1, x2, x3 are the solute: solvent ratios in
      thickeners 1, 2, and 3, respectively, the
      quantities of CaCO3. NaOH, and water in each of
      the streams can be calculated for every 100 kg of
       calcium carbonate
  //Since the final underflow must contain only 1 per
      cent of NaOH
8 \quad function[f] = F(x)
       f(1) = (300 * x(3)) / 100 - 0.01;
10
       f(2)=300*(x(2)-x(3))/x(4) - x(3);
                                                    //Wf =
          x(4)
       f(3)=300*(x(1)-x(3))/x(4) - x(2);
11
       f(4) = (80-300*x(3))/(600+x(4))-x(1);
12
       funcprot(0);
13
14 endfunction
15 //An initial guess
16 \times = [0.1 \ 0.1 \ 0.1 \ 0.1];
17 y = fsolve(x,F);
18 printf("\n x1 = \%f
                       x2 = \%f \quad x3 = \%f \quad Wf = \%f", y (1), y
      (2), y(3), y(4));
19
20 printf("\n Thus the amount of water required for
      washing 100 kg CaCO3 is %f kg", y(4));
21 printf("\n The solution fed to reactor contains 0.25
       kg/s Na2CO3. This is equivalent to 0.236 kg/s
      CaCO3, and hence the actual water required is \%.2 f
       kg/sec", y(4)*0.236/100);
```

Scilab code Exa 10.3 Required number of thickners

```
1 clear;
2 clc;
3 printf("\n Example 10.3");
5 //part 1
6 //Solvent in underflow from final washing thickener
      = 50 \text{ kg/s}.
7 //The solvent in the overflow will be the same as
      that supplied for washing (200 kg/s).
  //Solvent discharged in overflow/Solvent discharged
      in underflow= for the washing thickeners.
9 //Liquid product from plant contains 54.9 kg of salt
       in 195 kg of solvent.
10 //This ratio will be the same in the underflow from
      the first thickener.
11 printf("\n the material fed to the washing
      thickeners consists of 100 kg TiO2, 50 kg solvent
       and %d kg salt", 50*(54.9/195));
12
13 / m = n+1
14 \text{ m} = \log(421)/\log(4);
15 printf("\n The required number of thickeners for
      washing are %f",m);
16
17 // Part 2
18 //From an inspection of the data, it is seen that Wh
       = 0.30 + 0.2 \text{Xh}.
19 //Thus: Sh = WhXh = 0.30Xh + 0.2X2h = 5Wh^2
                                                     1.5\mathrm{Wh}
20 //Considering the passage of unit quantity of TiO2
      through the plant, then:
21 \text{ Ln} = 0; \text{ wn} = 2; \text{ Xn} = 0;
22 //since 200 kg/s of pure solvent is used.
```

```
23 \text{ Sn} = 0.001;
24 \text{ Wn} = 0.3007;
25 \text{ So} = 0.55;
26 \text{ Wo} = 1.00;
27 / X1 = (Ln+1 + S0)
                             Sn)/(wn+1 + W0)
                                                  Wn)
28 \times 1 = (0+0.55-0.001)/(2+1-0.3007);
29 printf("\n concentration in the first thickener is
      %f", X1);
30
31 \quad W1 = 0.30 + 0.2 * 0.203;
32 printf("\n W1 = \%f", W1);
33 \text{ S1} = (0.3406*0.203);
34 printf("\n S1 = \%f", S1);
35 \text{ X2} = (0.0691 - 0.001)/(1.7 + 0.3406);
36 printf ("\n X2 = \%f", X2);
37 \text{ W2} = (0.30+0.2*0.0334);
38 printf ("\n W2 = \%f", W2);
39 \times 3 = (0.01025 - 0.001) / (1.7 + 0.3067);
40 printf("\n X3 = \%f", X3);
41 printf("\n W3 = 0.30089");
42 printf("\n S3 = \%f",0.0013);
43 printf("\n W4 = \%f and S4 = \%f",0.30003,0.000045);
44 printf("\n Thus S4 is less than Sn and therefore 4
      thickeners are required.");
```

Scilab code Exa 10.4 Number of ideal stages required

```
1 clear;
2 clc;
3 printf("\n Example 10.4");
4 //Since the seeds contain 20 per cent of oil
5 xAo=0.2;
6 xBo=0.8;
7 printf("\n xAo = %.1f and xBo = %.1f",xAo,xBo);
8 //The final solution contains 50 per cent oil
```

```
9 yA1=0.5;
10 yS1=0.5;
11 printf ("\n yA1 = \%.1 f and yS1 = \%.1 f", yA1, yS1);
12 //The solvent which is used for extraction is pure
     and hence
13 ySn1=1:
14 //1 kg of insoluble solid in the washed product is
      associated with 0.5 kg of solution and 0.025 kg
      oil.
15 \text{ xAn} = 0.0167;
16 \text{ xBn} = 0.6667;
17 \text{ xSn} = 0.3166;
18
19 //The mass fraction of insoluble material in the
      underflow is constant and equal to 0.667. The
      composition of the underflow is therefore
      represented, on the diagram Figure 10.22, by a
      straight line parallel to the hypotenuse of the
      triangle with an intercept of 0.333 on the two
     main axes.
20
21 //The difference point is now found by drawing in
      the two lines connecting x0 and y1 and xn and yn
      +1.
22
23 //The graphical construction described in the text
      is then used and it is seen from Figure 10.22
      that xn lies in between x4 and x5.
24 printf("\n Thus 5 thickeners are adequate and for
      the required degree of extraction");
```

Scilab code Exa 10.5 Number of theoretical stages required

```
1 clear;
2 clc;
```

```
3 printf("\n Example 10.5");
5 //On the basis of 100 kg untreated solids
6 //In the underflow feed:
7 //0.35 kg oil is associated with each kg of
      exhausted livers.
8 printf("\n mass of livers fed=%d kg containg %d kg
      oil",100/(1+0.35),100-74);
9 \text{ xA} = 0.26;
10 printf ("\n xA = \%.2 f", xA);
11 xs = 0;
12 //In the overflow feed, pure ether is used
13 \text{ ys} = 1.0;
14 \text{ xs} = 0;
15 / \text{Recovery} = 90 \text{ per cent}
16 printf("\n
                                      Exhausted livers
                         Ether");
            Oil
17 printf("\n Underflow feed
                                            %d
                                    -",74,26);
18 printf("\n Overflow feed
                                     %d",50);
19 printf("\n Underflow product
                                   e(say)",74,2.6);
                      %d
20 printf("\n Overflow product
                                    50-e", 23.4);
                       \%d
21 printf("\n In the underflow product:");
22 printf("\n the ratio(oil/exhausted livers) = \%.3 f kg
      / \text{kg}", 2.6/74);
23 printf("\n Ratio(ether/exhausted livers) = \%.3 f kg/
      kg",0.306);
24 printf("\n e = \%.1 \, \text{f kg}",0.306*74);
25 //In the overflow product:
26 printf("\n The mass of ether = \%.1 \,\mathrm{f} kg",50-22.6);
27 printf("\n yA = \%.2 f", 23.4/(23.4+27.4));
28 printf("\n ys = %.2f",1-23.4/(23.4+27.4));
29 printf("\n ");
```

Chapter 11

Distillation

Scilab code Exa 11.1 Mole fraction calculation

```
1 //Example 11.1
3 clear all;
4 clc;
6 printf("\tExample 11.1\n");
8 p0_A=106; //Vapour pressure of n-heptane in kN/m<sup>2</sup>
9 p0_B=73.7; //Vapour pressure of toluene in kN/m^2
10 P=101.3; //\text{Total pressure in kN/m}^2
11
12 xA = (P-p0_B)/(p0_A-p0_B);
13
14 yA = pO_A * xA/P;
15
16 printf("\nMole fraction in liquid phase is : %.3f",
17 printf("\nMole fraction in vapour phase is : \%.3 \text{ f} \ \text{n}"
      , yA);
18
19 / End
```

Scilab code Exa 11.2 Saturated Pressure calculation

```
1 //Example 11.2
3 clear all;
4 clc;
6 printf("\tExample 11.2\n");
               //Critical pressure in kN/m<sup>2</sup>
8 \text{ Pc} = 4700;
9 Tc=508.1; // critical temperature in K
10 p1=100.666; //in kN/m^2
11 T1=329.026; //in K
12 \quad T = 350.874;
                //in K
13
14 Tr1=T1/Tc;
15 \text{ Pr1=p1/Pc};
16 printf("\nTr1 = \%f\nPr1 = \%f\n", Tr1, Pr1);
17
18 c5 = -35 + (36/Tr1) + (42 * log(Tr1)) - (Tr1^6);
19 c2=((0.315*c5)-log(Pr1))/((0.0838*c5)-log(Tr1));
20 c1=0.0838*(3.758-c2);
21 printf ("\nc5 = \%.4 f\\nc2 = \%.4 f\\nc1 = \%.4 f\\n",c5,c2
       ,c1);
22
23 k9 = -35 * c1;
24 \text{ k10} = -36 * c1;
25 \text{ k11} = (42 * c1) + c2;
26 \text{ k12=-c1};
27
28 printf("\nk9 = \%.3 f \nk10 = \%.3 f \nk11 = \%.4 f", k9,
      k10,k11);
29 printf("\nk12 = \%.5 f\n", k12);
30
```

```
31 Tr=T/Tc;

32 Pr=exp(k9-(k10/Tr)+(k11*log(Tr))+(k12*Tr^6));

33 p0=Pc*Pr;

34 printf("\nPr = %f \n\nP0 = %.2 f kN/m^2\n",Pr,p0);

35 

36 //End
```

Scilab code Exa 11.3 Vapour phase composition of a mixture

```
1 //Exaple
              11.3
3 clear all;
4 clc;
6 printf("\tExample 11.3\n");
8 k1_B=6.90565;
9 k2_B=1211.033;
10 k3_B=220.79;
11
12 k1_T=6.95334;
13 k2_T = 1343.943;
14 \text{ k3}_{T} = 219.377;
15
16 t=338-273; //in Degree celsius
             //in kN/m^2
17 P=101.3;
18 xB=0.5;
19 xT = 0.5;
20
21 function [p0] = antoine (k1, k2, k3, T)
       p0=10^(k1-(k2/(T+k3)));
22
23
       funcprot(0)
24 endfunction
25
26 p0_B=antoine(k1_B,k2_B,k3_B,t)*101.325/760;
```

Scilab code Exa 11.4 Boiling point of equimolar mixture

```
1 //Example 11.4
2
3 clear all;
4 clc;
6 printf("\tExample 11.4\n");
8 function[p0] = antoine(k1,k2,k3,T)
9
       p0=10^{(k1-(k2/(T+k3-273)))};
10
       funcprot(0)
11 endfunction
12
13 k1_B=6.90565;
14 k2_B=1211.033;
15 k3_B=220.79;
16
17 k1_T=6.95334;
```

```
18 \text{ k2}_T = 1343.943;
19 k3_T=219.377;
20
21 \times B = 0.5;
22 xT = 0.5;
23
24 printf("\n \t T(K)");
25 T = [373 353 363 365 365.1];
26 disp(T);
27
28 i = 1;
29
30 while i<6
31
        p0_B(i) = antoine(k1_B, k2_B, k3_B, T(i))
           *101.325/760;
32
       p0_T(i) = antoine(k1_T, k2_T, k3_T, T(i))
           *101.325/760;
       pB(i)=xB*p0_B(i);
33
       pT(i)=xT*p0_T(i);
34
35
       p(i)=pB(i)+pT(i);
36
        i=i+1;
37 \text{ end}
38 printf("\n\t p0 B")
39 disp(p0_B);
40 printf("\n\t p0 T");
41 disp(p0_T);
42 printf("\n\tpB");
43 disp(pB);
44 printf("\n\tpT");
45 disp(pT);
46 printf("\n\tpB+pT");
47 disp(p);
48
49 //since total pressure at 365.1 K is nearly same as
      101.3 kPa
50 printf("\nBoiling temperature is %f K",T(5));
51
52 //End
```

Scilab code Exa 11.5 Dew point of a equimolar mixture

```
1 //Example 11.5
3 clear all;
4 clc;
6 printf("\tExample 11.5\n");
8 function[p0] = antoine(k1, k2, k3, T)
       p0=10^{(k1-(k2/(T+k3-273)))};
       funcprot(0)
10
11 endfunction
12
13 k1_B=6.90565;
14 \text{ k2}_B = 1211.033;
15 k3_B=220.79;
16
17 k1_T=6.95334;
18 \text{ k2}_T = 1343.943;
19 k3_T=219.377;
20
21 //Since total pressure is 101.3 kPa, pB=pT
22 pB = 50.65;
23 pT = 50.65;
24
25 printf("\n\tT(K)");
26 T=[373.2 371.2 371.7 371.9 372];
27 disp(T);
28
29 i = 1;
30
31 while i<6
32
       p0_B(i) = antoine(k1_B, k2_B, k3_B, T(i))
```

```
*101.325/760;
33
       p0_T(i) = antoine(k1_T, k2_T, k3_T, T(i))
           *101.325/760;
       xB(i)=pB/p0_B(i);
34
35
       xT(i)=pT/p0_T(i);
36
       x(i)=xB(i)+xT(i);
37
       i=i+1;
38 end
39
40 printf("\n\t p0 B")
41 disp(p0_B);
42 printf("\n\t p0 T");
43 disp(p0_T);
44 printf("\n\txB");
45 disp(xB);
46 printf("\n \txT");
47 disp(xT);
48 printf("\n \t x = xB+xT");
49 \text{ disp}(x);
50
  //Since last value is closer to 1, 372 K is the
51
      required dew point
52 printf("\nDew point can be taken as \%f K", T(5));
53
54 / End
```

Scilab code Exa 11.6 Composition of vapour and liquid

```
1 //Example 11.6
2
3 clear all;
4 clc;
5 printf("\tExample 11.6\n");
7
```

Scilab code Exa 11.7 Number of theoretical plates needed

```
1 clear all;
2 clc;
3 printf('Example 11.7'); //Example 11.7
4 // Find Number of theoretical plates needed and the
      position of entry for the feed
                              //Feed [kmol]
6 F = 100;
8 function[f]=Feed(x)
       f(1)=x(1)+x(2)-100;
                                                    //Overall
           mass Balance
10
       f(2) = 0.9 \times x(1) + .1 \times x(2) - (100 \times .4);
                                                   //A
           balance on MVC, benzene
11
       funcprot(0)
12 endfunction
13 x = [50 50];
14 product = fsolve(x, Feed);
15
```

```
16 //Using notation of figure 11.13
17 Ln = 3*product(1);
18 \text{ Vn} = \text{Ln} + \text{product}(1);
19
20 //Reflux to the plate
21 \text{ Lm} = \text{Ln} + \text{F};
22 \text{ Vm} = \text{Lm} - \text{product}(2);
23
24 // Equilibrium Composition
25 \text{ xt} = .79;
                  yt = .9;
26 //From Top eqm line
27 yt1 = (Ln/Vn)*xt + (product(1)/Vn);
28 \text{ xt1} = .644;
                       //Thus from Eqm curve for yt1
29 //From Top eqm line
30 yt2 = (Ln/Vn)*xt1 + (product(1)/Vn);
                        //Thus from Eqm curve for yt2
31 \text{ xt2} = .492;
32 //From Top eqm line
33 yt3 = (Ln/Vn)*xt2 + (product(1)/Vn);
                        //Thus from Eqm curve for yt3
34 \text{ xt3} = .382;
35 //From II Eqm Line
36 \text{ yt4} = (Lm/Vm)*xt3 - (product(2)/Vm)*.1;
37 \text{ xt4} = .2982;
                          //Thus from Eqm curve for yt4
38 //From II Eqm Line
39 yt5 = (Lm/Vm)*xt4 - (product(2)/Vm)*.1;
40 \text{ xt5} = .208;
                        //Thus from Eqm curve for yt5
41 //From II Eqm Line
42 \text{ yt6} = (Lm/Vm)*xt5 - (product(2)/Vm)*.1;
                        //Thus from Eqm curve for yt6
43 \text{ xt6} = .120;
44 //From II Eqm Line
45 \text{ yt7} = (\text{Lm/Vm})*xt6 - (\text{product}(2)/\text{Vm})*.1;
46 \text{ xt7} = .048;
                        //Thus from Eqm curve for yt7
47
48 //Equilibrium Data
49 y=[0 yt7 yt6 yt5 yt4 yt3 yt2 yt1 yt];
50 x = [0 xt7 xt6 xt5 xt4 xt3 xt2 xt1 xt];
51 //Top Equilibrium Line equation 11.35
52 \text{ x1} = linspace(0,.79,100);
53 \text{ y1} = (\text{Ln/Vn})*x1 + (\text{product}(1)/\text{Vn});
```

```
54 //Equilibrium Line equation 11.37
55 \text{ x2} = linspace(0.048, .44, 100);
56 \text{ y2} = (\text{Lm/Vm})*x2 - (\text{product}(2)/\text{Vm})*.1;
57 clf();
58 plot(x,y,x1,y1,x2,y2);
59 xtitle("Lewis-Sorel Method", "Mole fraction of C6H6
      in Liquid (x)", "Mole Fraction C6H6 in Vapor (y)"
      );
60 legend ("Equilirium Plot", "Top Eqm Line", "Bottom
      Eqm Line");
61 printf("\n As the least point on equilibrium Line
      xt-7 correspond to reboiler, and there will be
      seven plates");
62
63
64 / END
```

Scilab code Exa 11.8 The Mc Cabe Thiele method

```
1 clear all;
2 clc;
3 printf('Example 11.8'); //Example 11.8
4 // Find Number of theoretical plates needed and the
      position of entry for the feed by mccabe thiele
      method
6 F = 100;
                              //Feed [kmol]
8 function[f]=Feed(x)
                                                    //Overall
       f(1) = x(1) + x(2) - 100;
           mass Balance
       f(2) = 0.9 \times x(1) + .1 \times x(2) - (100 \times .4);
10
                                                    //A
           balance on MVC, benzene
       funcprot(0)
11
12 endfunction
```

```
13 \times = [50 50];
14 product = fsolve(x, Feed);
15
16 //Using notation of figure 11.13
17 Ln = 3*product(1);
18 \text{ Vn} = \text{Ln} + \text{product}(1);
19
20 //Reflux to the plate
21 \text{ Lm} = \text{Ln} + \text{F};
22 \text{ Vm} = \text{Lm} - \text{product}(2);
23
24 // Equilibrium Data
25 \text{ y} = [0 .127 .252 .379 .498 .594 .708 .818 .9 1];
26 \text{ x} = [0 .048 .12 .208 .298 .382 .492 .644 .79 1];
27 // Diagnol Line
28 \text{ y3} = [0 1];
29 \times 3 = [0 \ 1];
30 //Top Equilibrium Line equation 11.35
31 \times 1 = linspace(0,.985,100);
32 y1 = (Ln/Vn)*x1 + (product(1)/Vn);
33 //Equilibrium Line equation 11.37
34 	ext{ x2} = linspace(0.048, .44, 100);
35 \text{ y2} = (\text{Lm/Vm})*x2 - (\text{product}(2)/\text{Vm})*.1;
36 clf();
37 //Setting initial point A x = .985 at top eqm line
38 \text{ xm} = [.985 .965 .965 .92 .92 .825 .825 .655 .655 .44]
        .44 .255 .255 .125 .125 .048];
39 \text{ ym} = [.985 .985 .965 .965 .92 .92 .825 .825 .655]
       .655 .44 .44 .255 .255 .125 .125];
40 \text{ xp} = [.985 .965 .92 .825 .655 .44 .255 .125 .048];
41 \text{ yp} = [.985 .965 .92 .825 .655 .44 .255 .125 .048];
42 plot(x,y,x3,y3,x1,y1,x2,y2,xm,ym);
43 xtitle("Mccabe Thiele Method", "Mole fraction of
      C6H6 in Liwuid (x)", "Mole Fraction C6H6 in Vapor
        (y)");
44 legend ("Equilirium Plot", "Diagnol Line", "Top Eqm
      Line", "Bottom Eqm Line", 5);
45 xset ('window',1);
```

Scilab code Exa 11.9 Number of plates required at total reflux

```
1 //Example 11.9
3 clear all;
4 clc;
6 printf("\tExample 11.9\n");
8 \text{ xA_d=0.9};
9 xA_s=0.1;
10 xB_d=1-xA_d;
11 xB_s=1-xA_s;
12
13 a=2.4;
14 \text{ xd=0.9};
15 \text{ xf} = 0.4;
16 \text{ xw} = 0.1;
17
18 n = (log(xA_d*xB_s/(xB_d*xA_s))/log(a))-1;
19 printf("\nNo. of theoretical plates in column is:
      %d",n);
20
```

```
21  Rm = ((xd/xf) - (a*((1-xd)/(1-xf))))/(a-1);
22  printf("\nMinimum reflux ratio is %.2 f\n", Rm);
23  24  yf = 0.61;
25  printf("\nUsing Graphical construction with yf = 0.61\n");
26  Rmin = (xd-yf)/(yf-xf);
27  printf("Minimum reflux ratio is %.2 f\n", Rmin);
28  29  // End
```

Scilab code Exa 11.10 Heat required

```
1 //Example 11.10
3 clear;
4 clc;
6 printf("\tExample 11.10\n");
  //From material balance
9
           D+W=1
           0.995D+0.1W=1*3
10
11
12 A = [1 1; 0.995 0.1];
13 B = [1;3];
14 \text{ Rm} = (1952-1547)/(1547-295);
15 printf ("\n Rm = \%. 3 f", Rm);
16 \text{ NA} = 1.08*405;
17 printf("\n Since the actual reflux is 8 pre cent
      above the minimum NA = 1.08*NmA = \%.3 f", NA);
18 N = 5/0.6;
19 printf("\n Number of plates to be required are \%.3 f
      ",5/0.6);
20
```

Scilab code Exa 11.11 Number of theoretical stages required

```
1 //Example 11.11
3 clear all;
4 clc;
6 printf("\tExample 11.11\n");
8 //
          F is feed
9 //
         D is distillate
10 //
         W is waste
11 //
        S is sidestream
12
13 F = 100;
14 S = 10;
15
16 //Mass fractions of CCl4 in various streams
17 xf = 0.5;
18 \text{ xd} = 0.95;
19 xw = 0.05;
20 \text{ xs} = 0.8;
21
22 //
        D + W = 100 - 10
0.95D + 0.00W = 50-8
24 \quad A = [1, 1; 0.95, 0.05];
25 B = [90; 42];
26 x = inv(A) *B;
```

```
27 printf("\nD = \%.1 f \ W = \%.1 f\n", x(1), x(2));
28
29 disp("From the enthalpy data and the reflux ratio,
     the upper pole point M is located as shown in
     Figure.");
30
31 disp("Points F and S are located, such that FS/FF =
      10.");
32
33 disp("MF is Joined and extended to cut NSA at O,
     the immediate pole point.");
34 disp("The number of stages required is then obtained
      from the figure and");
35 printf("13 theoretical stages are required");
36
37 / End
```

Scilab code Exa 11.12 Amount of distillate

```
1 clear;
2 clc;
3 printf("\n Example 11.12");
4 R = [0.85 1.0 1.5 2.0 3.0 4.0];
                                             //Reflux ratio
5 \text{ xd} = 0.75;
                                             //top
      concentration of alcohol
6 \text{ xs} = [0.55 \ 0.50 \ 0.37 \ 0.20 \ 0.075 \ 0.05]; //From the
      graph fig.11.35 page -596
7 \text{ Db}(1) = 0;
                                     Fί
9 printf("\n
                  \mathbf{R}
                                                           XS
                       ");
                 Db
10 i=1;
11 while i<=6
12
        Fi(i) = xd/(R(i) + 1);
13
        if i>1 then
```

```
14
       Db(i) = 100*(xs(1)-xs(i))/(xd-xs(i));
15
       end
      printf ("\n %.2 f
                                              \%.2~\mathrm{f}
                               \%.3 f
                                                          %
16
         .1 f", R(i), Fi(i), xs(i), Db(i));
17
       i=i+1;
18 end
19 plot(R, Db);
20 xtitle("", "Reflux ratio(R)", "Product Db (kmol)");
21 printf("\n The area under the Db vs R curve is given
       by 96 kmol");
22 \text{ Hav} = 4000;
                            //average latent heat in kJ/
      kmol
23 \ Qr = 96*Hav/1000;
24 printf("\n Heat to be supplied to provide the reflux
      , Qr is approximately %.1f MJ", Qr);
  printf("\n Heat to be supplied to provide the reflux
       per kmol of product is then \%.2 f MJ", 380/71.4);
26 printf("\n Total heat = \%.2 f MJ/kmol product"
      ,5.32+4.0);
```

Scilab code Exa 11.13 Heat required and average composition

```
1 //Example 11.13
2
3 clear all;
4 clc;
5
6 printf("\tExample 11.13\n");
7
8 xs=[0.55;0.5;0.425;0.31;0.225;0.105];
9 xd=[0.78;0.775;0.77;0.76;0.75;0.74];
10 differ=xd-xs;
11 for i=1:6
12 reci(i)=1/(xd(i)-xs(i));
13 end
```

```
14
15 m=[xs xd differ reci];
                             xd \qquad (xd-xs) \qquad 1/(xd-xs) \setminus n
16 printf("\n
                    xs
      ");
17 disp(m);
18 plot(xs,reci);
19 xtitle('Graphical integration', 'xs', '1/xd-xs)');
20
21 // Area under the curve is calculated and is found to
       be 1.1
22
23 //\log div = S1/S2 = area under the curve
24 logdiv=1.1;
25 \text{ S1} = 100;
                       //Assume
26 div=exp(logdiv);
27 S2=S1/div;
28 \text{ Db} = S1 - S2;
                      //Product obtained
29 amt=xs(1)*S1-(xs(6)*S2);
30 avg=amt/Db;
31
32 printf("\nAverage composition is \%.2 \text{ f kmol} \n", avg);
33
                     //latent heat
34 L = 4000;
35 R=2.1;
36
37 h=R*L;
38 printf("Heat required to produce reflux per kmol:
      %d kJ n", h);
39
40 //End
```

Scilab code Exa 11.14 Ideal plates required

```
1 clear;
2 clc;
```

```
//per cent of ortho top
3 \text{ xdo} = 0.98;
      product
                               //per cent of ortho bottom
4 \text{ xwo} = 0.125;
      product
6 function[f]=product(x)
       f(1) = 100 - x(1) - x(2); //x(1) is D and x
          (2) is W
       f(2) = 60 - x(1)*xdo - x(2)*xwo;
       funcprot(0);
10 endfunction
11 x = [0,0];
12 y = fsolve(x, product)
13 printf("\n D = \%.2 \text{ f kmol & W = } \%.2 \text{ f kmol}", y(1), y(2))
14
15 printf("\n Let us assume that the distillate
      contains 0.6 mole per cent meta and 1.4 mole per
      cent para");
16 printf("\n Component
                                 Feed
                              Distillate
                       "):
      Bottoms
17 printf("\n
                          (kmol) (mole per cent) (
      kmol) (mole per cent) (kmol) (mole per cent
18 printf ("\n Ortho %.3 f %.2 f
                                                      %.2 f
                                     \%.2 \text{ f}
                                                     \%.2 f
            \%.2 f
              ",60,60,y(1)*0.98,98,y(2)*0.125,12.5);
19 printf("\n Meta %.3 f
                                   \%.2 {\rm f}
                         \%.2 {\rm f}
                                     %.2 f
                           \%.2 \text{ f}
      ,4,4,y(1)*0.006,0.6,y(2)*0.083,8.3);
20 printf("\n Para %.3 f
                                                          %
               %.2 f
                                          %.2 f
                                                        \%.2
      . 2 f
               ", 36, 36, y(1) *0.014, 1.4, y(2) *0.792, 79.2);
21
22 ao = 1.7;
                           //relative volatility of ortho
       relative to para
```

```
//relative volatility of meta
23 \text{ am} = 1.16;
       relative to para
                                //relative volatility of para
24 \text{ ap } = 1;
      w.r.t. to itself
25 \text{ xso} = 0.125;
26 \text{ xsm} = 0.083;
27 \text{ xsp} = 0.792;
28 \text{ xwo} = 0.125;
29 \text{ xwp} = 0.083;
30 \text{ xwm} = 0.792;
31 yso = ao*xso/(ao*xso+ap*xsp+am*xsm);
32 \text{ ysm} = \text{am}*\text{xsm}/(\text{ao}*\text{xso}+\text{ap}*\text{xsp}+\text{am}*\text{xsm});
33 ysp = ap*xsp/(ao*xso+ap*xsp+am*xsm);
34 //Equations of operating lines
35 //Above the feed point
36 \text{ Ln} = 5*y(1);
                                //Liquid downflow
37 \text{ Vn} = 6*y(1);
                              //Vapour up
38 //Assuming the feed is liquid at its boiling point
39 F = 100;
                            //feed
                           //liquid downflow
40 \text{ Lm} = \text{Ln+F};
                           //Vapour up
41 Vm = Lm - y(2);
42 \text{ x1o} = \text{poly}([0], 'x1o');
43 \times 11 = roots(yso - (Lm/Vm)*x1o + (y(2)/Vm)*xwo);
44 x1p = poly([0], 'x1p');
45 \text{ x} 12 = \text{roots}(ysp - (Lm/Vm)*x1p + (y(2)/Vm)*xwp);
46 \text{ x1m} = \text{poly}([0], 'x1m');
47 	ext{ x13} = roots(ysm - (Lm/Vm)*x1m + (y(2)/Vm)*xwm);
48 	 x1 = [x11 	 x13 	 x12];
49 \text{ ax1} = [ao*x11 am*x13 ap*x12];
50 \text{ y1} = [ax1(1)/(ax1(1)+ax1(2)+ax1(3)) ax1(2)/(ax1(1)+ax1(2))]
       ax1(2)+ax1(3)) ax1(3)/(ax1(1)+ax1(2)+ax1(3))];
51 \times 20 = poly([0], 'x2o');
52 \times 21 = roots(y1(1) - (Lm/Vm)*x2o + (y(2)/Vm)*xwo);
53 \text{ x2p} = poly([0], 'x2p');
54 \times 22 = roots(y1(3) - (Lm/Vm)*x2p + (y(2)/Vm)*xwp);
55 \text{ x2m} = \text{poly}([0], 'x2m');
56 	ext{ x23 = } 	ext{roots}(y1(2) - (Lm/Vm)*x2m + (y(2)/Vm)*xwm);
57 \times 2 = [x21 \times 23 \times 22];
```

```
58 printf("\n
                           plate compositions below the
      feed plate");
59 printf("\n Component
                                           xs
                                               x1
      axs
                            ys
                                                           x2");
                      ax1
                                          y1
60 printf("\n
                                                %.3 f
                     O
                                   %.3 f
                                                %.3 f
                  %.3 f
                                                                %
                   \%.3 f
                                  \%.3 f", xso, ao*xso, yso, x1(1)
      . 3 f
       ,ax1(1),y1(1),x2(1));
                                                %.3 f
61 printf("\n
                     \mathbf{m}
                                   %.3 f
                                                \%.3 f
                  \%.3 f
                                                                \%
      . 3 f
                   \%.3 f
                                  \%.3 f", xsm, am*xsm, ysm, x1(2)
       ,ax1(2),y1(2),x2(2));
62 printf("\n
                                                %.3 f
                     р
                                                %.3 f
                  %.3 f
                                   %.3 f
                                                                %
                   %.3 f
                                  \%.3 f", xsp, ap*xsp, ysp, x1(3)
      . 3 f
       ,ax1(3),y1(3),x2(3));
63 printf("\n
                                                %.3 f
                                                \%.3 f
                                                                %
                  \%.3 f
                                   \%.3 f
      .3 f
                   %.3 f
                                  \%.3 f", xso+xsm+xsp, ao*xso+
      am*xsm+ap*xsp, yso+ysm+ysp, x1(1)+x1(2)+x1(3), ax1
      (1) + ax1(2) + ax1(3), y1(1) + y1(2) + y1(3), x2(1) + x2(2) +
      x2(3));
64
65 \text{ ax2} = [ao*x2(1) am*x2(2) ap*x2(3)];
66 	 y2 = [ax2(1)/(ax2(1)+ax2(2)+ax2(3)) ax2(2)/(ax2(1)+ax2(2))]
      ax2(2)+ax2(3)) ax2(3)/(ax2(1)+ax2(2)+ax2(3))];
67 \times 30 = poly([0], 'x3o');
68 \times 31 = roots(yso - (Lm/Vm)*x3o + (y(2)/Vm)*xwo);
69 \text{ x3p} = poly([0], 'x3p');
70 x32 = roots(ysp - (Lm/Vm)*x3p + (y(2)/Vm)*xwp);
71 \text{ x3m} = poly([0], 'x3m');
72 x33 = roots(ysm - (Lm/Vm)*x3m + (y(2)/Vm)*xwm);
73 \times 3 = [x31 \times 33 \times 32];
74
75 \text{ ax3} = [ao*x3(1) am*x3(2) ap*x3(3)];
76 	 y3 = [ax3(1)/(ax3(1)+ax3(2)+ax3(3)) ax3(2)/(ax3(1)+ax3(2))
      ax3(2)+ax3(3)) ax3(3)/(ax3(1)+ax3(2)+ax3(3))];
```

```
77 \text{ x4o} = poly([0], 'x4o');
78 	 x41 = roots(yso - (Lm/Vm)*x4o + (y(2)/Vm)*xwo);
 79 x4p = poly([0], 'x4p');
80 x42 = roots(ysp - (Lm/Vm)*x4p + (y(2)/Vm)*xwp);
81 x4m = poly([0], 'x4m');
82 	ext{ x43} = roots(ysm - (Lm/Vm)*x4m + (y(2)/Vm)*xwm);}
83 \times 4 = [x41 \times 43 \times 42];
84
85 \text{ ax4} = [ao*x4(1) am*x4(2) ap*x4(3)];
86 	 y4 = [ax4(1)/(ax4(1)+ax4(2)+ax4(3)) ax4(2)/(ax4(1)+ax4(2))]
       ax4(2)+ax4(3)) ax4(3)/(ax4(1)+ax4(2)+ax4(3))];
87 \times 50 = poly([0], 'x50');
88 x51 = roots(yso - (Lm/Vm)*x5o + (y(2)/Vm)*xwo);
89 x5p = poly([0], 'x5p');
90 	ext{ x52} = \frac{\text{roots}(ysp - (Lm/Vm)*x5p + (y(2)/Vm)*xwp)};
91 \times 5m = poly([0], 'x5m');
92 \times 53 = roots(ysm - (Lm/Vm)*x5m + (y(2)/Vm)*xwm);
93 	 x5 = [x51 	 x53 	 x52];
94
95 \text{ ax5} = [ao*x5(1) am*x5(2) ap*x5(3)];
96 	 y5 = [ax5(1)/(ax5(1)+ax5(2)+ax5(3)) ax5(2)/(ax5(1)+ax5(2))
       ax5(2)+ax5(3)) ax5(3)/(ax5(1)+ax5(2)+ax5(3))];
97 \times 60 = poly([0], 'x60');
98 \times 61 = roots(yso - (Lm/Vm)*x6o + (y(2)/Vm)*xwo);
99 x6p = poly([0], 'x6p');
100 x62 = roots(ysp - (Lm/Vm)*x6p + (y(2)/Vm)*xwp);
101 \times 6m = poly([0], 'x6m');
102 \times 63 = roots(ysm - (Lm/Vm)*x6m + (y(2)/Vm)*xwm);
103 \times 6 = [x61 \times 63 \times 62];
104
105 \text{ ax6} = [ao*x6(1) am*x6(2) ap*x6(3)];
106 \text{ y6} = [ax6(1)/(ax6(1)+ax6(2)+ax6(3)) ax6(2)/(ax6(1)+ax6(2)+ax6(3))]
       ax6(2)+ax6(3)) ax6(3)/(ax6(1)+ax6(2)+ax6(3))];
107 \times 70 = poly([0], 'x70');
108 \times 71 = roots(yso - (Lm/Vm)*x7o + (y(2)/Vm)*xwo);
109 \text{ x7p} = poly([0], 'x7p');
110 x72 = roots(ysp - (Lm/Vm)*x7p + (y(2)/Vm)*xwp);
111 x7m = poly([0], 'x7m');
```

```
112 x73 = roots(ysm - (Lm/Vm)*x7m + (y(2)/Vm)*xwm);
113 \times 7 = [x71 \times 73 \times 72];
114 printf("\n Component
                                             ax2
                                                ax3
                       y3
                                           x4
                                                             ax4");
115 printf ("\n
                      O
                                                   %.3 f
                                     %.3 f
                                                  %.3 f
                   \%.3 f
                                                                  %
        . 3 f
                     \%.3 f
                                   \%.3 f", ax2(1), y2(1), x3(1),
        ax3(1), y3(1), x4(1), ax4(1));
                                                   %.3 f
116 printf("\n
                    \%.3 f
                                     %.3 f
                                                  %.3 f
        .3 f
                     %.3 f
                                   \%.3 \text{ f}", xsm, am*xsm, ysm, x1(2)
        ,ax1(2),y1(2),x2(2));
                                                   %.3 f
117 printf("\n
                      р
                                                  %.3 f
                    %.3 f
                                     %.3 f
                     %.3 f
        .3 f
                                   \%.3 f", xsp, ap*xsp, ysp, x1(3)
        ,ax1(3),y1(3),x2(3));
118
119 printf("\n Component
                                             y4
       x5
                                                 y5
                             ax5
                       x6
                                           ax6
                                                              y6");
120 printf ("\n
                                                   %.3 f
                       O
                                     %.3 f
                                                  %.3 f
                    %.3 f
                                                                  %
        . 3 f
                     \%.3 f
                                   \%.3 f", y4(1), x5(1), ax5(1),
       y5(1), x6(1), ax6(1), y6(1));
121 printf("\n
                                                   %.3 f
                      \mathbf{m}
                                     %.3 f
                                                  %.3 f
                    \%.3 f
                     %.3 f
                                   \%.3 f", y4(2), x5(2), ax5(2),
        . 3 f
       y5(2),x6(2),ax6(2),y6(2));
122 printf ("\n
                                                   %.3 f
                      р
                   %.3 f
                                    %.3 f
                                                  %.3 f
                     %.3 f
                                   \%.3 f", y4(3), x5(3), ax5(3),
        . 3 f
       y5(3), x6(3), ax6(3), y6(3));
123
124
125 \text{ ax7} = [ao*x7(1) am*x7(2) ap*x7(3)];
126 	 y7 = [ax7(1)/(ax7(1)+ax7(2)+ax7(3)) ax7(2)/(ax7(1)+ax7(2)+ax7(3))]
        ax7(2)+ax7(3)) ax7(3)/(ax7(1)+ax7(2)+ax7(3))];
```

```
127 \times 80 = poly([0], 'x80');
128 x81 = roots(yso - (Ln/Vn)*x8o + (y(2)/Vn)*xwo);
129 x8p = poly([0], 'x8p');
130 x82 = roots(ysp - (Ln/Vn)*x8p + (y(2)/Vn)*xwp);
131 x8m = poly([0], 'x8m');
132 x83 = roots(ysm - (Ln/Vn)*x8m + (y(2)/Vn)*xwm);
133 \times 8 = [x81 \times 83 \times 82];
134
135 \text{ ax8} = [ao*x8(1) am*x8(2) ap*x8(3)];
136 \text{ y8} = [ax8(1)/(ax8(1)+ax8(2)+ax8(3)) ax8(2)/(ax8(1)+ax8(3))]
       ax8(2)+ax8(3)) ax8(3)/(ax8(1)+ax8(2)+ax8(3))];
137 \times 90 = poly([0], 'x90');
138 x91 = roots(yso - (Ln/Vn)*x9o + (y(2)/Vn)*xwo);
139 x9p = poly([0], 'x9p');
140 x92 = roots(ysp - (Ln/Vn)*x9p + (y(2)/Vn)*xwp);
141 \times 9m = poly([0], 'x9m');
142 x93 = roots(ysm - (Ln/Vn)*x9m + (y(2)/Vn)*xwm);
143 \times 9 = [x91 \times 93 \times 92];
144
145 printf ("\n Component
                                           x7
       ax7
                            y7
                                               x8
                                                           x9");
                       ax8
                                           v8
                                                 %.3 f
146 printf ("\n
                      О
                                   %.3 f
                                                %.3 f
                   \%.3 f
                    %.3 f
                                  \%.3 f", x7(1), ax7(1), y7(1),
       . 3 f
       x8(1), ax8(1), y8(1), x9(1));
                                                 %.3 f
147 printf("\n
                     \mathbf{m}
                   %.3 f
                                   %.3 f
                                                %.3 f
       .3 f
                    %.3 f
                                  \%.3 f", x7(2), ax7(2), y7(2),
       x8(2),ax8(2),y8(2),x9(2));
                                                 %.3 f
148 printf ("\n
                     р
                   \%.3 f
                                   %.3 f
                                                %.3 f
       .3 f
                    %.3 f
                                  \%.3 f", x7(3), ax7(3), y7(3),
       x8(3), ax8(3), y8(3), x9(3));
149
150 printf("\n Component
                                           x7
       ax7
                            у7
                                               x8
                                                           x9");
                       ax8
                                           y8
```

```
%.3 f
151 printf("\n
                   %.3 f
                                    %.3 f
                                                  %.3 f
                                   \%.3 f", y4(1), x5(1), ax5(1),
        .3 f
                     \%.3 f
       y5(1),x6(1),ax6(1),y6(1));
152 printf ("\n
                                                  %.3 f
                     \mathbf{m}
                                                  %.3 f
                   %.3 f
                     %.3 f
                                   \%.3 f", y4(2), x5(2), ax5(2),
       .3 f
       y5(2),x6(2),ax6(2),y6(2));
153 printf ("\n
                                                  %.3 f
                     р
                   %.3 f
                                    %.3 f
                                                  %.3 f
                                                                  %
                                   \%.3 f", y4(3), x5(3), ax5(3),
       .3 f
                     \%.3 f
       y5(3),x6(3),ax6(3),y6(3));
```

Scilab code Exa 11.15 Minimum reflux ratio

```
1 clear all;
2 clc;
3 printf("\n Example 11.15");
5 printf("\n Dew point calculation");
6 \text{ xd1} = 0.975;
                                 //n-C4 light distillate
                                //C5 heavy key distillate
7 \text{ xd2} = 0.025;
8 \text{ Td} = 344;
                                //temperature in kelvins
9 \text{ K1} = 1.05;
                               //Eqillibrium constant
       calculation for n-C4 at 344 K
                               //Equillibrium constant
10 \text{ K2} = 0.41;
       calculation for C5 at 344K
11 //By a dew point calculation
12 / \operatorname{sum}(xd) = \operatorname{sum}(xd/K)
                                                       Td = 344
13 printf("\n Component
                                  xd
      K");
14 printf("\n
                                                       K
      xd/K");
15 printf("\nn-C4
                                  %.3 f
                                                      %.2 f
      \%.3 \, f", xd1, K1, xd1/K1);
```

```
16 printf("\n C5
                                   %.3 f
                                                      %.2 f
      \%.3 \text{ f}", xd2, K2, xd2/K2);
17 printf("\n
                                   %.1 f
      \%.3 f", xd1+xd2, (xd1/K1)+(xd2/K2));
18
19 \text{ K11} = 1.04;
20 \text{ K21} = 0.405;
21 // Calculation for xd at 343 K
22 x = poly([0], 'x');
23 x1 = roots(x/K11 + (1-x)/K21);
24 printf("\n
      Td = 343 \text{ K}");
25 printf("\n
             xd/K");
      K
26 printf("\n
      \%.3 \text{ f}
            \%.3 \, \mathrm{f} ", K11, x1/K11);
27 printf("\n
      \%.3 f
             \%.3 \, f", K21, (1-x1)/K21);
28 printf("\n
      \%.3 f", x1/K11+(1-x1)/K21);
29 printf("\n At 343 K
                                   K1 = 1.04 K2 = 0.405
         from fig.11.39");
30
31 printf("\n\n Estimation of still temperature Ts");
32 / \operatorname{sum}(xw) = \operatorname{sum}(K*xw)
33 \text{ K31} = 3.05;
                               //equillibrium const at 419 K
                               //equillibrium const at 419 K
34 \text{ K32} = 1.6;
                               //equillibrium const at 419 K
35 \text{ K33} = 0.87;
                               //equillibrium const at 419 K
36 \text{ K34} = 0.49;
                               //mass fraction of n-C4
37 \times 1 = 0.017;
38 \times 2 = 0.367;
                               //mass fraction of C5
                               //mass fraction of C6
39 \times 3 = 0.283;
40 \times 40 = 0.333;
                               //mass fraction of C7
```

```
41
42 printf("\n At Ts = 416 K equillibrium constants are
      from fig.11.39");
43 printf("\n n-C4
                                 C5
                                             C6
                                                           C7")
                                 %.2 f
                                             %.2 f
44 printf ("\n %.2 f
                                                         \%.2 f"
      ,K31,K32,K33,K34);
45 printf("\n
                   at Ts = 416 \text{ K}");
46 printf ("\n n-C4
                                             C6
                                                           C7")
                                 C5
                                              %.3 f
47 printf ("\n %.3 f
                                 %.3 f
                                                         %.3 f"
      ,xw1*K31,xw2*K32,xw3*K33,xw4*K34);
48 printf ("\n Sum of Kxw = \%d", xw1*K31+xw2*K32+xw3*K33+
      xw4*K34);
49 printf("\n Hence the still temperature Ts = 416 \text{ K}");
50 printf("\n\n Calculation of feed condition");
51 printf("\n Component
                                             Tb = 377K
                                хf
               Tb = 376 \text{ K}");
52 printf("\n
                                           K
                                                     Kxf
                     Kxf ");
              K
53 \text{ xf1} = 0.40;
54 \text{ xf2} = 0.23;
55 \text{ xf3} = 0.17;
56 \text{ xf4} = 0.20;
                               //equillibrium constants at
57 \text{ Kb1} = 1.80;
      377 \text{ K for } n-C4
  Kb2 = 0.81;
                               //equillibrium constants at
      377 K for C5
  Kb3 = 0.39;
                               //equillibrium constants at
      377 K for C6
60 \text{ Kb4} = 0.19;
                               //equillibrium constants at
      377 K for C7
61 \text{ Kb11} = 1.78;
                               //equillibrium constants at
      377 K for n-C4
  Kb21 = 0.79;
                               //equillibrium constants at
      377 K for C5
63 \text{ Kb31} = 0.38;
                               //equillibrium constants at
      377 K for C6
```

```
//equillibrium constants at
64 \text{ Kb41} = 0.185;
       377 K for C7
                                                      \%.3 f
65 printf ("\n n-C4
                                \%.2 {\rm f}
                                           %.2 f
               \%.3 \, f", xf1, Kb1, xf1*Kb1, Kb11, xf1*Kb11);
66 printf("\n C5
                                %.2 f
                                           %.2 f
                                                      %.3 f
               \%.3 f", xf2, Kb2, xf2*Kb2, Kb21, xf2*Kb21);
      \%.2 f
67 printf("\n C6
                                \%.2 {\rm f}
                                           \%.2 f
                                                      %.3 f
               \%.3 f", xf3, Kb3, xf3*Kb3, Kb31, xf3*Kb31);
      %.2 f
68 printf("\n C7
                                %.2 f
                                           %.2 f
               \%.3 \, f", xf4, Kb4, xf4*Kb4, Kb41, xf4*Kb41);
69 printf("\n
                                                      \%.3 f
                     \%.3 f", xf1*Kb1+xf2*Kb2+xf3*Kb3+xf4*Kb4
       ,xf1*Kb11+xf2*Kb21+xf3*Kb31+xf4*Kb41);
70
71 // Calculation of pinch temperatures
72 printf ("\n\n The upper pinch temperature, \n Tn = %d K
      ",343+0.33*(416-343));
73 printf("\n The lower pinch temperature, Tm = \%d K"
       ,343+0.67*(416-343));
74
75 // Calculation of approximate minimum reflux ratio.
76 printf("\langle n \rangle n \rangle");
77 printf("\n Component
                                   Tn = 367 \text{ K}
                                                      Tm = 391 \text{ K}
                   axfh");
           xfh
78 printf("\n
                                       a
                                                           a
                            ");
                                      %.2 f
79 printf("\n n-C4
                                                           %.2 f
                         ",2.38,2.00);
80 printf ("\n C5
                                                           %.2 f
                         ",1.00,1.00);
81 printf ("\n C6
                                                           %.3 f
                                      %.3 f
            \%.2 f
                      \%.3 \,\mathrm{f}", 0.455, 0.464, 0.17, 0.077);
                                                           %.3 f
82 printf ("\n C7
                                      \%.3 f
            %.2 f
                      \%.3 \, f", 0.220, 0.254, 0.20, 0.044);
83 printf("\n
      \%.3 f", 0.077+0.044);
84 \text{ rf} = xf1/xf2;
```

```
85 printf("\n rf = \%.3f",rf);
 86 \text{ xn4} = \text{rf}/[(1+\text{rf})*(1+0.121)];
 87 printf("\n xn4 = \%.3 \, \text{f}", xn4);
 88 \times n5 = xn4/rf;
 89 printf("\n xn5 = \%.3 f", xn5);
 90 Rm = [1/(2.38-1)]*(0.975/0.563)-2.38*(0.025/0.325);
 91 printf ("\n Rm = \%.2 \,\mathrm{f}", Rm);
 92
 93 //The streams in the column
 94 D = 40;
95 Ln = D*Rm;
96 \text{ Vn} = \text{Ln+D};
97 F = 100;
98 \text{ Lm} = \text{Ln} + \text{F};
99 W = 60;
100 \text{ Vm} = \text{Lm} - \text{W};
101 Ratio = Lm/W;
102 printf("\n Ln = \%.1 \text{ f kmol}", 44.8);
103 printf("\n Vn = \%.1 \text{ f kmol}",84.8);
104 printf("\n Lm = \%.1 \, \text{f kmol}",144.8);
105 printf("\n Vn = %.1 f kmol",84.4);
106 printf("\n Lm/W = \%.2 \, f", Ratio);
107 //Check on minimum reflux ratio
108 / xn = xd/(a-1)Rm
109 xn = xd1/[(2.38-1)*Rm];
110 printf("\n For n-C4.....xn = \%.3 f",xn);
111 \quad xn1 = 1-xn;
112 printf("\n For n-C5...xn = \%.3 \, f", xn1);
113 printf("\n Temperature check for upper pinch gives
        sum of K*xn = ");
114 \text{ sumKxn} = 1.62*xn + 0.68*xn1;
115 printf ("%.3f", sumKxn);
```

Scilab code Exa 11.16 Minimum reflux ratio

```
1 //Example 11.16
3 clear all;
4 clc;
6 printf("\tExample 11.16\n");
8 // Mole fractions
9 \text{ xf} = [0.40 \ 0.35 \ 0.25];
10 xd = [0.534 \ 0.453 \ 0.013];
11 xw = [0 \ 0.04 \ 0.96];
12
13 //Amount of feed, product, bottom in kmol
14 F = [40 35 25];
15 D = [40 34 1];
16 \quad W = [0 \quad 1 \quad 24];
17
18 //roots of equation
19 theta=[1.15 1.17];
20
21 //relative volatility
22 alpha=[2.7 2.22 1];
23
24 //Underwoods 1st equation for q=1
25 \text{ sums} = [0 \ 0];
26 \text{ for } i=1:2
27
        for j=1:3
             sums(i)=sums(i)+(alpha(j)*xf(j)/(alpha(j)-
28
                theta(i));
29
        end
30 end
31 printf("\nFrom Underwoods 1st eq\n");
32 printf ("The value of 1-q at theta = 1.15 and 1.17
      are");
33 disp(sums);
34
35 //Underwoods 2nd equation for minimum reflux ratio
36 \text{ sum} 2 = 0;
```

```
37  for l=1:3
38     sum2=sum2+(alpha(1)*xd(1)/(alpha(1)-theta(2)));
39  end
40
41  Rm=sum2-1;
42  printf("\nMinimum Reflux ratio is %.3 f\n",Rm);
43
44  //End
```

Scilab code Exa 11.17 Number of theoretical plates required

```
1 //Example 11.17 Fenske's Equation
3 clear all;
4 clc;
6 printf("\tExample 11.17\n");
8 //From previous question data
9 \text{ xA_d=0.453};
10 xB_d=0.013;
11
12 xA_s = 0.04;
13 xB_s = 0.96;
14
15 alpha_av=2.22;
16
17 //By Fenske Equation for no. of plates
18
19 n=((log(xA_d*xB_s/(xA_s*xB_d)))/log(alpha_av))-1;
20
21 printf("\nMinimum no. of plates are \%f or \%d\n",n,n)
22
23 / End
```

Scilab code Exa 11.18 Xhange in n with R

```
1 //Example 11.18
3 clear all;
4 clc;
6 printf("\tExample 11.18\n");
8 R = [1 2 5 10];
9 \text{ Rm} = 0.83;
10
11 nm=8.5-1;
12
13 //X are points on X-axis of graph
14 for i=1:4
        X(i) = (R(i) - Rm) / (R(i) + 1);
16 \text{ end}
17
18 // Values at Y-axis for corresponding values of X-
      axis in graph are given by
19 Y = [0.55 \ 0.32 \ 0.15 \ 0.08];
20
21 //where Y=(n+1)-(nm+1)/(n+2)
22
23
24 for i=1:4
25
       n=poly([0], 'x');
       N(i) = roots(((n+1) - (nm+1)) - (Y(i)*(n+2)));
26
27 end
28
29 printf("\nThe values of R and n are\n");
30 \text{ for } i=1:4
       printf("\n\t\%d \t %.2 f", R(i), N(i));
31
```

```
32 end
33
34 printf("\n\nThe change in R and n can be seen as above\n");
35
36 //End
```

Scilab code Exa 11.19 Optimum reflux ratio

```
1 clear all;
2 clc;
3 printf("\n Example 11.19");
4 //Data from fig. 11.42
5 a = [0 \ 0.02 \ 0.04 \ 0.06 \ 0.08 \ 0.1 \ 0.2 \ 0.4 \ 0.6 \ 0.8 \ 1.0];
6 b = [0.75 \ 0.62 \ 0.60 \ 0.57 \ 0.55 \ 0.52 \ 0.45 \ 0.30 \ 0.18
      0.09 0];
7 / a = (R-Rm)/(R+1)
8 / b = [(n+1)-(nm+1)]/(n+2)
9 R = [0.92 1.08 1.25 1.75 2.5 3.5 5.0 7.0 9.0];
10 \text{ n} = [28.6 \ 22.8 \ 16.9 \ 13.5 \ 11.7 \ 10.5 \ 9.8 \ 9.2 \ 8.95];
11 plot(n,R);
12 xtitle("Plot of R vs n", "n", "R");
13 printf("\n Derivative calculated from the graph");
14 d = [110.0 34.9 9.8 3.8 1.7 0.6 0.4 0.2 0.05];
15 i=1;
16 while i <=9
      s = R(i)+1 - (n(i)+7.72)/d(i);
17
18
      if s <=0.0001 then
19
           Ropt = R(i);
           printf ("\n Ropt = \%.2 f", Ropt);
20
21
           break;
22
      end
23
      i=i+1;
25 printf("\n R is approximately %.1f percent of the
```

Scilab code Exa 11.20 Plate efficiency for the given data

```
1 //Example 11.20
3 clear all;
4 clc;
6 printf("\tExample 11.20\n");
8 //Mole fraction
9 xf = [0.2 \ 0.3 \ 0.2 \ 0.3];
10
11 // Viscosity at mean tower temp. in mNs/m<sup>2</sup>
12 uL=[0.048 0.112 0.145 0.188];
13
14 // Viscosity of water in mNs/m<sup>2</sup>
15 \text{ uw} = 1;
16
17 sums=0;
18 \text{ for } i=1:4
        sums=sums+(xf(i)*uL(i)/uw);
19
20 end
21
22 // Efficiency by DRICKAMER and BRADFORD
23 E=0.17-(0.616*log10(sums));
24
25 printf("\nEfficiency is \%.2 \, f",E);
26
27 //End
```

Chapter 12

Absorption of gases

Scilab code Exa 12.1 Overall liquid film coefficient

```
1 clear;
2 clc;
3 printf("\n Example 12.1");
4 //Overall liquid transfer coefficient KLa = 0.003
      kmol/s.m^3(kmol/m^3)
6 //(1/KLa) = (1/kLa) + (1/HkGa)
7 // let (KLa)=x
8 x = 0.003;
9 overall = 1/x;
11 //For the absorption of a moderately soluble gas it
      is reasonable to assume that the liquid and gas
      phase resistances are of the same order
      ofmagnitude, assuming them to be equal.
12 // (1/KLa) = (1/kLa) + (1/HkGa)
13 / let 1/kLa = 1/HkGa = y
14 y = (1/(2*x));
15 z = (1/y);
                         //z is in kmol/s m<sup>3</sup>(kmol/m
16 printf("\n For S02:");
```

```
17 printf("\n kGa = \%f kmol/s m<sup>3</sup>(kN/m<sup>2</sup>)",z/50);
18 printf("\n For NH3:");
                              //diffusivity at 273K for
19 d_S02 = 0.103;
     SO2 in cm^2/sec
20 d_NH3 = 0.170;
                              //diffusivity at 273K for
     NH3 in cm^2/sec
21 printf("\n
                  kGa = \%f \ kmol/s \ m^3(kN/m^2)",(z/50)*(
      d_NH3/d_SO2)^0.56;
22 printf("\n For a very soluble gas such as NH3, kGa =
      KGa.");
23 printf("\n
                 For NH3 the liquid-film resistance will
       be small, and:");
24 printf("\n
                        kGa = KGa = \%fkmol/s m^3(kN/m^2)"
      (z/50)*(d_NH3/d_SO2)^0.56);
```

Scilab code Exa 12.2 Mass transfer coefficient

```
1 clear;
2 clc;
3 printf("\n Example 12.2");
4 G = 2;
                                             //air flow rate
      in kg/m<sup>2</sup>.sec
5 \text{ Re} = 5160;
                                             //Re stands for
      Reynolds number
                                            //friction factor
6 f = 0.02;
      = R/pu^2
7 	 d_S02 = 0.116*10^{(-4)};
                                            //diffusion
      coefficient in m<sup>2</sup>/sec
8 v = 1.8*10^{(-5)};
                                                   // viscosity
      in mNs/m^2
                                            //density is in kg
9 p = 1.154;
      /\mathrm{m}^3
10
  //(hd/u) (Pm/P) (u/p/d_SO2) 0.56 = BRe(-0.17) = jd
11
12
```

```
13 function[x]=a1()
        x = (v/(p*d_S02))^(0.56);
14
15
        funcprot(0);
16 endfunction
17
18 / jd = f = R/pu^2
19 function[y]=a2()
20
        y = f/a1();
21
        funcprot(0);
22 endfunction
23 //G = pu
    u = (G/p);
                                            //u is in m/sec
24
25
26 \quad function[x1] = a3()
        x1 = a2()*u;
27
28
        funcprot(0);
29 endfunction
30
31 function[d]=d1()
        d = Re*v/(G);
32
        funcprot(0);
33
34 endfunction
35
36 printf("\n d = \%f mm",d1());
37 R = 8314;
                              //R is in m<sup>3</sup> (N/m<sup>2</sup>)/K kmol
38 T = 298;
                              //T is in Kelvins
39 function [kG] = kG1()
40
        kG = a3()/(R*T);
        funcprot(0);
41
42 endfunction
43
44 printf("\n kG = \%.2 \text{ f}*10^{(-8)} \text{ kmol/m}^2 \text{sec} (N/m}^2)", kG1
       ()*10^{(8)};
45 printf("\n kG = \%.2 \text{ f}*10^{(-4)} \text{kg } \text{SO}2/\text{m}^2 \text{sec}(\text{kN/m}^2)",
       kG1()*10<sup>(7)</sup>*64);
```

Scilab code Exa 12.3 Overall transfer units required

```
1 clear;
2 clc;
3 printf("\n Example 12.3");
4 //as the system are dilute mole fractions are
      approximately equal to mole ratios.
5 //At the bottom of the tower
6 \text{ y1} = 0.015;
                            //mole fraction
                            //Gas flow rate is in kg/m<sup>2</sup>
7 G = 1;
      sec
8 //At the top of the tower
9 	 y2 = 0.00015;
                           //mole fraction
10 x2 = 0;
11 L = 1.6;
                           //liquid flow rate is in kg/m
      ^{\hat{}}2.\sec c
                           //liquid flow rate is in kmol/m
12 \text{ Lm} = 1.6/18;
      ^{\hat{}}2.\,\mathrm{sec}
13 \text{ Gm} = 1.0/29;
                           //gas flow rate is in kmol/m<sup>2</sup>.
      sec
14 \times 1 = poly([0], 'x1');
15 x11 = roots(Gm*(y1-y2)-Lm*(x1));
16 printf("\n x1 = \%f", x11);
17 function[ye1]=henry_law(x)
18
        ye1 = 1.75*x;
19
        funcprot(0);
20 endfunction
21 bottom_driving_force = y1 - henry_law(x11);
22
    function[lm] = log_mean()
         lm = (bottom_driving_force-y2)/log(
23
            bottom_driving_force/y2);
24
         funcprot(0);
25
    endfunction
26 \quad NoG = (y1-y2)/log_mean();
```

```
27 NoL = NoG*1.75*(Gm/Lm);
28 printf("\n NoL =\%.2 f", NoL);
```

Scilab code Exa 12.4 Height of transfer units and number of transfer units

```
1 clear;
2 clc;
3 printf("\n Example 12.4");
4 \text{ Gm} = 0.015;
5 \text{ KGa} = 0.04;
6 \text{ top} = 0.0003;
7 \text{ Y1} = 0.03;
8 \text{ Ye} = 0.026;
9 \text{ bottom} = (Y1-Ye);
10 log_mean_driving_force = (bottom-top)/log(bottom/top
      );
11 Z = poly([0], 'Z');
12 Z1 = roots(Gm*(Y1-top)-KGa*log_mean_driving_force*Z)
13 printf("\n
                     Z = \%.2 \,\text{fm}", Z1);
14 \text{ HoG} = \text{Gm/KGa};
15 printf("\n Height of transfer unit HoG = \%.3 \, fm", HoG
      );
16 printf("\n Number of transfer units NoG = \%f", ceil
       (7.79/0.375));
```

Scilab code Exa 12.5 Height of the tower

```
1 clear;
2 clc;
3 printf("\n Example 12.5");
4 y1 = 0.10;
5 Y1 = 0.10/(1-0.10);
```

```
6 y2 = 0.001;
7 \ Y2 = y2;
8 mass_flowrate_gas = 0.95; //mass flow rate in
      kg/m<sup>2</sup>.sec
9 mass_percent_air = (0.9*29/(0.1*17+0.9*29))*100;
10 mass_flowrate_air = (mass_percent_air*
      mass_flowrate_gas); //in kg/m^2.sec
11 Gm = (mass_flowrate_air/29);
12 \text{ Lm} = 0.65/18;
                            //Lm is in kmol/m<sup>2</sup>.sec
13 //A mass balance between a plane in the tower where
      the compositions are X and Y and the top of the
      tower gives:
14
15 / Y = 1.173X + 0.001
16 \quad X = 0:0.001:0.159;
17 \quad Y = 1.173 * X + 0.001;
18 plot(X,Y);
20 x = [0.021 \ 0.031 \ 0.042 \ 0.053 \ 0.079 \ 0.106 \ 0.159];
21
22 \text{ PG} = [12 \ 18.2 \ 24.9 \ 31.7 \ 50.0 \ 69.6 \ 114.0];
23 i = 1;
24 while i<8
       Y1(i) = PG(i)/(760-PG(i));
25
26
       i=i+1;
27 end
28 plot(x, Y1);
29 //xlabel("Area under the curve is 3.82m", "kmolNH3/
      kmolH2O", "kmolNH3/kmol air");
30 xtitle ("Operating and equilibrium lines", "kmol NH3/
      kmol H2O", "kmol NH3/kmol air");
31 //If the equilibrium line is assumed to be straight,
       then:
               Y1) = KGaZdeltaPlm
32 / \text{Gm}(Y2)
33
34 //Top driving force
35 \text{ deltaY2} = 0.022;
36 //Bottom driving force
```

```
37 deltaY1 = 0.001;

38 deltaY1m = 0.0068;

39 Z = (0.0307*0.11)/(0.001*0.688);

40 printf("The height of the tower is %.2f meters",Z);
```

Scilab code Exa 12.6 specific steam consumption

```
1 clear;
2 clc;
3 printf("\n Example 12.6");
4 printf("\n Number of theoretical plates = %d"
      ,(30*0.3));
6 //At the bottom of the tower:
7 // Flowrate of steam = Gm (kmol/m^22s)
8 // Mole ratio of pentane in steam = Y1, and
9 //Mole ratio of pentane in oil = X1
10 X1 = 0.001;
11
12 //At the top of the tower:
13 //exit steam composition = Y2
14 //inlet oil composition = X2
15 \quad X2 = 0.06;
16 //flowrate of oil = Lm (kmol/m^2.sec)
17
18 //The minimum steam consumption occurs when the exit
      steam stream is in equilibrium with the inlet
      oil, that is when:
19 //The equilibrium relation for the system may be
     taken as Ye = 3.0X, where Ye and X are expressed
     in mole ratios of pentane in the gas and liquid
     phases respectively.
20 \text{ Ye2} = X2*3;
21 //Lmin(X2
             X1) = Gmin(Y2)
                                Y1)
22 //If Y1 = 0, that is the inlet steam is pentane-free
```

```
. then:
23 \text{ ratio_min} = (X2 - X1)/Ye2;
24
25
26 //The operating line may be fixed by trial and error
       as it passes through the point (0.001, 0), and 9
       theoretical plates are required for the
      separation. Thus it is a matter of selecting the
      operating line which, with 9 steps, will give X2
      = 0.001 when X1 = 0.06. This is tedious but
      possible, and the problem may be better solved
      analytically since the equilibrium line is
      straight.
27
28 / let x = 1/A
29 //for a stripping operation
30 LHS = (X2-X1)/(X2);
31 printf("\n LHS = \%f", LHS);
32 x = poly([0], 'x');
33 x1 = roots((x^10-x)-LHS*(x^(10)-1));
34 printf("\n 1/A = \%.2 f", x1(9));
35 / A = Lm/mGm
36 printf ("\n Gm/Lm = \%.3 f", x1(9)/3);
37 printf ("\n Actual/minimum Gm/Lm = \%.2 f", 0.457/0.328)
38
39 // If (actual Gm/Lm) / (min Gm/Lm) = 2
40 printf("\n Actual Gm/Lm = \%.3 \, \text{f}", .328*2);
41 	 x2 = 3*(0.656);
42 printf("\n 1/A = mGm/Lm = \%.3 f", 3*0.656);
43
44 //y = (1.968)^{(N+1)}
45 y = poly([0], 'y');
46 \text{ y1} = \text{roots}(0.983*(y-1)-(y-1.968));
47 N = \log(y1)/\log(1.968) -1;
48 printf("\n The actual number of plates are : %.1f",
      ceil(N/0.3));
```

Chapter 13

Liquid liquid extraction

Scilab code Exa 13.1 Composition of final raffinate

```
1 clear all;
2 clc;
3 printf("\n Example 13.1");
4 printf("\n
                   (a) Countercurrent operation");
5 //(a) Countercurrent operation
                                        //Solvent flow rate
6 S = 1.6*10^{(-4)};
      in m^3/\sec
  mass_flowrate = (S*800);
                                        //mass flow rate is
      in kg/sec
  //Considering the solution, 400 \text{cm} 3/\text{s} = 4
       ^3/sec containing, say, a m^3/sec A and (5)
                                                             10
         4
                 a) m3/sec B.
10 //Thus mass flow rate of A = 1200a \text{ kg/sec}
11 //and mass flow rate of B = (4*10^{\circ}(-4)-a)*1000 =
      (0.4-1000\,\mathrm{a})\,\mathrm{kg/sec}
                                          (0.4+200a) kg/sec
12 //a total of:
13 C = poly([0], 'C');
14 \text{ C1} = \text{roots}(0.1*(0.4+200*C)-1200*C);
15 printf ("\n Concentration of the solution is \%.2 f
      *10^{(-5)} m<sup>3</sup>/sec", C1*10<sup>5</sup>;
```

```
16 printf("\n mass flow rate of A = \%.3 f \text{ kg/sec}",1200*
      C1);
17 printf("\n mass flow rate of B = \%.3 f kg/sec"
       ,0.4+200*C1);
18 printf ("\n Ratio of A/B in the feed, Xf = \%.3 f \text{ kg/kg}
      ",0.041/0.366);
19
20 X = [0.05 0.10 0.15];
21 \quad Y = [0.069 \quad 0.159 \quad 0.258];
22 plot(X,Y);
23 xtitle("Equilibrium curve", "kg A/kg B", "kg A/kg S");
24 //From The curve:
25 \text{ slope} = 0.366/0.128;
26 printf("\n Slope of the equilibrium line is \%.2 \,\mathrm{f}",
      slope);
27
28 //Since pure solvent is added, Yn+1 = Y4 = 0 and a
      line of slope 2.86 is drawn in such that stepping
       off from Xf = 0.112 \text{ kg/kg} to Y4 = 0 \text{ gives}
      exactly three stages. When Y4 = 0, Xn = X3 =
      0.057 \text{ kg/kg}
29 printf("\n The composition of final raffinate is
      0.057 \, \text{kg A/kg B}");
30
31 printf("\n\n
                           (b) Multiple contact");
32 printf("\n Stage 1");
33 printf("\n In this case \%.4 \,\mathrm{f} kg/sec", 0.128/3);
34 //and from the equilibrium curve, the extract
      contains 0.18 \text{ A/kg S} and (0.18)
                                             0.0427) =
      0.0077 \text{ kg/s A}.
35 printf("\n Thus raffinate from stage 1 contains %.4f
       kg/sec Aand %.3 f kg/sec B", (0.041-0.0077), 0.366)
36 \times 1 = 0.0333/0.366;
37 printf("\n X1 = \%.3 \, \text{f} \, \text{kg/kg}",0.0333/0.366);
38
39 printf("\n Stage 2");
40 //the extract contains 0.14 kg A/kg S
```

Scilab code Exa 13.3 Overall transfer coefficient

```
1 clear all;
2 clc;
3 printf("\n Example 13.3");
4 //From the equilibrium relationship
5 \text{ CB1} = (0.0247*0.685);
6 printf("\n CB1* = \%.4 \text{ f kmol/m}^3", CB1);
7 \text{ CB2} = (0.0247*0.690);
8 printf("\n CB2* = \%.4 \text{ f kmol/m}^3", CB2);
10 //Thus the driving force at the bottom:
11 deltaC1 = (0.0169 - 0.0040);
12 printf("\n deltaC1 = \%.4 \text{ f kmol/m}^3", deltaC1);
13 //Driving force at the top
14 \text{ deltaC2} = (0.0170 - 0.0115);
15 printf("\n deltaC2 = \%.4 \text{ f kmol/m}^3", deltaC2);
16 function[x] = log_mean_driving_force()
        x = (deltaC1 - deltaC2)/log((deltaC1)/deltaC2);
17
```

```
18     funcprot(0);
19     endfunction
20     printf("\n log mean driving force is given by
          deltaClm = %.4 f kmol/m^3",log_mean_driving_force
          ());
21     KBa = (4.125*10^(-8))/(log_mean_driving_force()
          *0.0063);
22     printf("\n KBa = %.1 f*10^(-4) kmol/sec m^3(kmol/m^3)
          ",KBa*10^4);
23     HoB = (1.27*10^(-3))/KBa;
24     printf("\n HoB = %.2 f meters",HoB);
```

Scilab code Exa 13.4 Surface mean droplet size

```
1 clear all;
2 clc;
3 printf("\n Example 13.4");
4 diameter = [2 3 4 5 6];
5 \text{ number} = [30 \ 120 \ 200 \ 80 \ 20];
7 function[x] = Sum_d1cube()
       sum = 0;
9
        i = 1;
10
       while (i \le 5)
            sum = sum + number(i)*(diameter(i))^3;
11
12
            i = i+1;
13
       end
14
       x = sum;
15
       funcprot(0);
16 endfunction
17
18 function[y]=sum_d1square()
       sum1 = 0;
19
20
       j=1;
21
       while (j \le 5)
```

```
22
            sum1 = sum1 + number(j)*(diameter(j))^2;
23
            j = j+1;
24
       end
25
       y = sum1;
26
       funcprot(0);
27 endfunction
28
29 function[z] = ds()
       z = Sum_d1cube()/sum_d1square();
30
       funcprot(0);
31
32 endfunction
33 printf("\n Mean droplet size = \%.2 \text{ f mm}", ds());
```

Scilab code Exa 13.5 Number of overall transfer units in raffinate phase

```
1 clear all;
2 clc:
3 printf("\n Example 13.5");
4 \text{ CSA} = (\%\text{pi}/4)*(0.075)^2;
                                               //cross
      sectional area is in m<sup>2</sup>
5 V = (0.0044*3);
                                               //volume of
      packing is in m<sup>3</sup>
6 C = 0.01;
                                               //concentration
       is in kg/kg
7 printf("\n mass of acid transferred to the ether %.4
      f kg/m^2.sec or \%f kg/sec, 0.05*(0.01-0)
       ,0.005*0.0044);
8 printf("\n Acid in the aqueous feed = \%.2 \,\mathrm{f} \,\mathrm{kg/m}^3.
      sec",0.25*0.04);
9 printf("\n Acid in the raffinate = \%.3 \, f \, kg/m^2.sec"
      ,0.01-0.005);
10 printf("\n Concentration of acid in the raffinate =
      \%.2 \text{ f kg/kg}", 0.005/0.25);
11 printf("\n At the top of the column");
12 \text{ CR2} = 0.040;
                                   //Concentration is in kg/
```

```
kg
13 CR22 = 0.040*0.3; //Concentration is in kg/
14 \text{ deltaC2} = (0.012-0.010);
15 printf("\n deltaC2 = \%.3 f \text{ kg/kg}", deltaC2);
16 printf("\n At the bottom of the column");
17 \text{ CR1} = 0.20;
                               //Concentration is in kg/
      kg
                               //Concentration is in kg/
18 \text{ CR11} = 0.020*0.3
      kg
19 \text{ deltaC1} = 0.006 - 0;
                               //Concentration is in kg/
20 printf("\n deltaC1 = \%.3 f \text{ kg/kg}", deltaC1);
21 deltaCRlm = (0.006-0.002)/log(0.006/0.002);
22 printf("\n Logarithmic driving force is : %.4f kg/kg
      ", deltaCRlm);
23 \text{ KRa} = 0.000022/(0.01333*deltaCRlm);}
24 printf("\n KRa = \%.3 f kg/m^3.sec(kg/kg)", KRa);
25 printf("\n Height of an overall transfer unit = \%.2 f
      m", 0.25/KRa);
26 printf("\n The number of overall transfer units = \%
      .2 f ",3/0.54);
```

Chapter 14

Evaporation

Scilab code Exa 14.1 Heat surface required

```
1 clear;
2 clc;
3 printf("\n Example 14.1");
4 //Assuming that the steam is dry and saturated at
      205 kN/m2, then from the Steam Tables in the
      Appendix, the steam temperature = 394 K at which
      the total enthalpy = 2530 \text{ kJ/kg}.
6\ //At\ 13.5\ kN/m2, water boils at 325\ K and, in the
      absence of data on the boiling point elevation,
      this will be taken as the temperature of
      evaporation, assuming an aqueous solution. The
      total enthalpy of steam at 325 K is 2594 kJ/kg.
8 //Thus the feed, containing 10 per cent solids, has
      to be heated from 294 to 325 K at which
      temperature the evaporation takes place.
10 printf("\n mass of dry solids = \%.1 \, \text{f kg/sec}"
      ,(7*10/100));
11 x = poly([0], 'x');
```

```
12 \times 1 = roots(0.7*100-50*(0.7+x));
13 printf("\n x = \%.1 f kg/sec", x1);
14 printf("\n Water to be evaporated = \%.1 \, \text{f kg/sec}"
      ,(7-0.7)-0.7);
15 printf("\n Summarising");
16 printf("\n Stream
                                 Solids
                                                 Liquid
               Total
                       ");
17 printf("\n
                                                 (kg/s)
                                 (kg/s)
               (kg/s) ");
                                     %.1 f
                                                      %.1 f
18 printf("\n Feed
                  \%.1 \text{ f} ", x1,7-x1,x1+7-x1);
19 printf("\n Product
                                                      %.1 f
                 \%.1 f", x1, x1, x1+x1);
                                                      %.1 f
20 printf ("\n Evaporation
                 \%.1 \; f ",7-x1-x1,7-2*x1);
21 //Using a datum of 273K
22 \text{ q_entering} = (7*3.76)*(294-273);
23 printf("\n Heat entering with the feed = \%.1 \,\mathrm{f} kW",
      q_entering);
24 \text{ q_leaving} = (1.4*3.14)*(325-273);
25 printf("\n Heat leaving with the product = \%.1 \, \text{f kW}",
      q_leaving);
26 printf("\n Heat leaving with the evaporated water =
      %d kW",5.6*2594);
27 printf("\n Heat transferred from the steam = %d kW"
      ,14526+228.6-552.7);
28 printf("\n The enthalpy of the condensed steam
      leaving at 352.7 \text{ K} = \%.1 \text{ f kJ/kg}"
      ,4.18*(352.7-273));
29 printf("\n The heat transferred from 1 kg steam = \%
      .1 f kJ/kg",2530-333.2);
30 printf("\n Steam required = \%.2 \,\mathrm{f} kg/s"
      ,14202/2196.8);
31
32 //s the preheating of the solution and the sub-
      cooling of the condensate represent but a small
      proportion of the heat load, the temperature
      driving force may be taken as the difference
```

```
between the temperatures of the condensing steam
and the evaporating water, or:
33 printf("\n deltaT = %d deg K ",394-325);
34 printf("\n Heat transfer area ,A = %.1 f m^2"
,14202/(3*69));
```

Scilab code Exa 14.2A Forward feed

```
1 clear;
2 clc;
3 printf("\n Example 14.2a");
4 //Temperature of dry saturated steam at 205 \text{ kN/m2} =
      394 K.
5 //At a pressure of 13 kN/m2 (0.13 bar), the boiling
      point of water is 325 K, so that the
      total temperature difference &T = (394)
                                                    325) =
      69 deg K.
6
8 // First Approximation.
10 //Assuming that: U1*deltaT1 = U2*deltaT2 = U3*
      deltaT3
11 //then substituting the values of U1, U2 and U3 and
     \&T = 69 \text{ deg K gives}:
12 printf("\n deltaT1 = \%f deg K",13);
13 printf("\n deltaT2 = \%f deg K",20);
14 printf("\n deltaT2 = %f degK",36);
15
16 //Since the feed is cold, it will be necessary to
      have a greater value of T1 than given by this
      analysis. It will be assumed that T1 = 18 \deg K,
      T2 = 17 \text{ deg K}, T3 = 34 \text{ deg K}.
17
18 //For steam to 1: T0 = 394 \text{ K} and 0 = 2200 \text{ kJ/kg}
```

```
19 //For steam to 2: T1 = 376 \text{ K} and T = 2249 \text{ kJ/kg}
20 //For steam to 3: T2 = 359 K and
                                           2 = 2293 \text{ kJ/kg}
                        T3 = 325 \text{ K} \text{ and}
                                          3 = 2377 \text{ kJ/kg}
21 //
22
23 //Assuming that the condensate leaves at the steam
      temperature, then heat balances across each
       effect may be made as follows:
24
25
   //Effect 1 :
  //2200 D0 = 4
                       4.18(376
                                      294) + 2249 D1
26
27
28 // Effect 2:
29 / 2249 D1 + (4)
                        D1) 4.18(376
                                            359) = 2293 D2
30
31 // Effect 3:
32 / 2293 D2 + (4)
                         D1
                                D2)4.18(359
                                                    325) =
      2377 D3
33
34 printf("\n
                           Solids
                                                 liquor
                    Total ");
35 printf("\n
                                                 (kg/s)
                           (kg/s)
                    (kg/s) ");
36 printf("\nFeed
                           %.1 f
                                                  %.1 f
                      \%.1 \, \text{f} ",0.4,3.6,4.0);
                                                  %.1 f
37 printf("\nProduct
                           %.1 f
                      \%.1 \, \text{f} ",0.4,0.4,0.8);
                                                  %.1 f
38 printf("\nEvaporation
                      \%.1 f
                             ", 3.6-0.4, 4.0-0.8);
39
40 / D1 + D2 + D3 = 3.2 \text{ kg/s}
41 D = [2177.94 - 2293 0; -4.18*(359-325)]
      2293-4.18*(359-325) -2377;1 1 1];
42 \text{ C} = [-4*4.18*(376-359); -4*4.18*(359-325); 3.2];
43 D1 = inv(D)*C;
44 printf("\n ans = \%.3 f \text{ kg/s}",D1);
45
46 D0 = (4*4.18*(376-294)+2249*D1(1))/2200;
47 \text{ A1} = D0*2200/(3.1*18);
```

```
48 printf("\n A1 = \%.1 \text{ f m}^2", A1);
49 \quad A2 = D1(1)*2249/(2*17);
50 printf("\n A2 = \%.1 \, \text{f m}^2", A2);
51 \quad A3 = D1(2)*2293/(1.1*34);
52 printf("\n A3 = \%.1 \text{ f m}^2", A3);
53 printf("\n These three calculated areas are
      approximately equal, so that the temperature
      differences assumed may be taken as nearly
      correct");
54
55 // let, deltaT1 = x
56 // deltaT2 = y
57 // deltaT3 = z
58 X = [3.1 -2.0 0; 0 2.0 -1.1; 1 1];
59 A = [0;0;69];
60 T = inv(X) *A;
61 printf("\n deltaT1 = %d deg K",T(1));
62 printf("\n deltaT2 = %d deg K",T(2));
63 printf("\n deltaT3 = \%d deg K", T(3));
64
65 //ghting the temperature differences to allow for
      the fact that the feed enters at ambient
      temperature gives:
66 // deltaT1 = 18 deg Kdelta T2 = 18 degK delta T3 = 33
       deg K
67 Steam_temp = 394;
68 	ext{ T1 = Steam\_temp-18;}
69 printf("\n T1 = \%d K", T1);
70 	ext{ T2} = 	ext{T1} - 	ext{18};
71 printf ("\n T2 = \%d K", T2);
72 \quad T3 = T2 - 33;
73 printf("\n T3 = \%d K", T3);
74
75 //The total evaporation (D1 + D2 + D3) is obtained
      from a material balance:
76 printf ("\n
                          Solids
                                               liquor
                    Total ");
77 printf("\n
                                               (kg/s)
                          (kg/s)
```

```
(kg/s) ");
78 printf("\nFeed
                          %.1 f
                                               %.1 f
                     \%.1 f ",0.4,3.6,4.0);
79 printf("\nProduct
                          %.1 f
                                               %.1 f
                     \%.1 f ",0.4,0.4,0.8);
80 printf ("\nEvaporation
                                                %.1 f
                            ",3.6-0.4,4.0-0.8);
                     \%.1 {\rm f}
81
82 //Assuming, as an approximation, equal evaporation
      in each effect, or D1 = D2 = D3 = 1.07 \text{ kg/s}, then
       the latent heat of flash vaporisation in the
      second effect is given by:
83 q = 4.18*(4-1.07)*(376-358);
84 printf("\n latent heat of flash vaporisation in the
      second effect is = \%.1 \, \text{f kW}, q);
85 printf("\n latent heat of flash vaporisation in the
      third effect is:= \%.1 \text{ f kW} ",4.18*(4-2*1.07)
      *(358-325));
86 printf("\n At 394 K, the latent heat = 2200 \text{ kJ/kg}");
87 printf("\n At 325 K, the latent heat = 2377 \text{ kJ/kg}");
88 printf("\n Mean value, = 2289 \text{ kJ/kg}");
89
90 printf("\n Values of T1, T2T3 are now chosen by trial
      and error to give equal values of A in each
      effect, as follows");
91 printf("\n deltaT1
                                  deltaT2
                                              A2
      deltaT3
                    A3");
92 printf("\n (deg K)
                          (m^2)
                                  (deg K)
                                              (m^2)
                                                      (deg K
             m^2");
93 printf("\n
                          64.2
                                     18
                                               61.4
                                                         33
                 18
               66.9 ");
94 printf("\n
                 19
                          60.5
                                     17
                                               65.0
                                                         33
               66.9");
95 printf("\n
                 18
                         64.2
                                  17.5
                                              63.1
                                                        33.5
             65.9");
                                                        34
96 printf("\n
                         64.2
                                  17
                                              65.0
                 18
               64.9");
97
```

```
98 printf("\n Steam consumption = %.2 f kg/s",3580/2289);
99 printf("\n Economy = %.1 f kg/kg",3.2/1.56);
```

Scilab code Exa 14.2B Backward feed

```
1 clear;
2 clc;
3 printf("\n Example 14.2b");
4 \text{ deltaT1} = 20;
                                //temperature is in deg K
                                //temperature is in deg K
5 \text{ deltaT2} = 24;
6 \text{ deltaT3} = 25;
                                //temperature is in deg K
7 \text{ To} = 394;
                                //temperature is in deg K
8 T1 = 374;
                                //temperature is in deg K
9 T2 = 350;
                                //temperature is in deg K
                                //temperature is in deg K
10 \quad T3 = 325;
11 \quad latent_heat0 = 2200;
                                //latent heat in kJ/kg
12 latent_heat1 = 2254;
                                //latent heat in kJ/kg
13 latent_heat2 = 2314;
                                //latent heat in kJ/kg
14 latent_heat3 = 2377;
                                //latent heat in kJ/kg
15
16 // Effect 3:
17 //
                   2314 D2 = 4 4.18(325)
                                                   294) +
      2377 D3
18
19 // Effect 2:
20 //
                   2254 \text{ D1} = (4 \text{ D3}) 4.18(350)
                                                        325)
      + 2314 D2
21
22 // Effect 1:
23 //
                   2200 D0 = (4)
                                 D3 D2) 4.18(374
          350) + 2254 D1
24
25 / (D1 + D2 + D3) = 3.2 \text{ kg/s}
26
```

```
27  D = [0 2314 -2377;2254 -2314 4.18*(350-325);1 1 1];
28  C = [4*4.18*(325-294);4*4.18*(350-325);3.2];
29  D1 = inv(D)*C;
30  printf("\n D1 = %.3 f kg/s",D(1));
31  printf("\n D2 = %.3 f kg/s",D(2));
32  printf("\n D3 = %.3 f kg/s",D(3));
33  A1 = 1.387*latent_heat0/(2.5*20);
34  A2 = 1.261*latent_heat1/(2*24);
35  A3 = 1.086*latent_heat2/(1.6*25);
36  printf("\n A1 = %.1 f m^2",A1);
37  printf("\n A2 = %.1 f m^2",A2);
38  printf("\n A3 = %.1 f m^2",A3);
```

Scilab code Exa 14.3 Efficiency of the compressor

```
1 clear;
2 clc;
3 printf('\n Example 14.3");
4 \text{ He} = 2690;
                      //He is the enthalpy of entrained
      steam in kJ/kg
5 H4 = ((1*2780) + (1.6*2690))/2.60;
7 // Again assuming isentropic compression from 101.3
      to 135 \text{ kN/m2}, then:
8 \text{ H3} = 2640;
                    //in kJ/kg (from the chart)
9 n = (1.0+1.6)*(2725-2640)/[1.0*(2780-2375)];
10 printf ("\n
               = \%.2 \text{ f } ", \text{n};
11 printf("\n This value is low, since in good design
      overall efficiencies approach 0.75
                                              0.80.
      Obviously the higher the efficiency the greater
      the entrainment ratio or the higher the saving in
       live steam");
12 \text{ Pe} = 101.3;
                      //pressure of entrained vapour in
      kN/m^2
13 discharge P = 135; // discharge pressure in kN/m^2
```

```
14 printf("\n the required flow of live steam = 0.5 kg/kg entrained vapour.");
15 printf("\n In this case the ratio is (1.0/1.6) = 0.63 \text{ kg/kg}");
```

Scilab code Exa 14.4 Quantity of additional stream required

```
1 clear;
2 clc;
3 printf("\n Example 14.4");
4 // Making a mass balance, there are two inlet streams
5 //the additional steam, say Gx kg/s
6 //the sea water feed, say Gy kg/s.
8 //The two outlet streams are
9 // distilled water product, 0.125 kg/s
10 //the concentrated sea water, 0.5 Gy kg/s
12 / \text{Thus}: (Gx + Gy) = (0.125 + 0.5 Gy) \text{ or } (Gx + 0.5 Gy)
      ) = 0.125
13
14 //At 650 \text{ kN/m2}, the total enthalpy of the steam =
      2761 \text{ kJ/kg}.
15
16 //Thus the energy in this stream = 2761Gx kW
17 //sea water enters at 344 K
18 / \text{enthalpy of feed} = [Gy]
                                 4.18(344
                                                273) =
      296.8Gy kW
19 printf ("\n The enthalpy of the product is 439*0.125
      = 54.9 \text{ kW}");
20
21 //Making a balance
22 / (E + 2761Gx + 296.8Gy) = (211.3Gy + 54.9)
23 / (E + 2761Gx + 85.5Gy) = 54.9
```

```
24 //where E is the power supplied to the compressor
25 / (E + 2590Gx) = 33.5
26
27 //For a single-stage isentropic compression
28 //the work done in compressing a volume V1 of gas at
       pressure P1 to a volume V2 at pressure P2 is
      given by
29 P1 = 101.3;
                            //pressure is in kN/m<sup>2</sup>
                           //pressure is in kN/m<sup>2</sup>
30 P2 = 120;
31 dsteam_P1 = (18/22.4)*(273/374.1); //density of
      steam at 101.3 \text{ kN/m}^2 and 374.1 \text{ K}
32 / V1 = 0.5 Gy/dsteam_P1 = 0.853 Gy m^3/sec
33 E = poly([0], 'E');
34 E1 = roots(0.5*E-(P1*0.853)/(1.3-1)*[(P2/P1)
      (0.3/1.3)-1]);
35 printf("\n E = \%.1 \text{ f kW/(kg/sec)}", E1);
36
37 printf("\n As the compressor is 50 per cent
      efficient then E = \%.1 f \text{ kW/(kg/sec)}", E1/0.5);
38 / E = 46*0.5*Gy = 23.0Gy kW
39 Gx = poly([0], 'Gx');
40 \text{ Gx1} = \frac{\text{roots}}{2761*\text{Gx}} - 54.9 - 4.72*(33.5-2590*\text{Gx}));
41 printf ("\n Gx = \%.3 \, \text{f kg/sec}", Gx1);
```

Scilab code Exa 14.5 Capacity and economy of the system

```
9 P2 = 101.3;
                         //pressure of entrained steam
10 H1 = 2970; //The enthalpy of the live steam at 650 kN
      /m2 and (435 + 100) in kJ/kg
11 H2 = 2605; //the enthalpy after isentropic expansion
      from 650 to 101.3 kN/m2, using an
      enthalpy entropy chart, in kJ/kg
12 \times 2 = 0.97;
                       //dryness fraction
13
14 printf("\n The enthalpy of the steam after actual
      expansion to 101.3 \text{ kN/m}^2 \text{ is } \% \text{d kJ/kg}, e1*(H1 -
      H2));
15 LatentHeat = 2258;
                             //latent heat at 101.3 kN/m
16 //dryness after expansion but before entrainment x21
       is given by:
                   = (1)
                              e1)(H1
17 / (x 2 1 x2)
                                           H2)
18 \times 21 = poly([0], 'x21');
19 x22 = roots((x21-x2)*LatentHeat-(1-e1)*(H1-H2));
20 printf("\n dryness after expansion but before
      entrainment x21 is = \%.3 f", x22);
21
22 //If x23 is the dryness after expansion and
      entrainment, then:
23 / (x 2 3 x 2) = (1
                             e3)(H1
                                         H2)
24 \times 23 = poly([0], 'x23');
25 	ext{ x24 = } \frac{\text{roots}((x23-x2)*LatentHeat} - (1-e3)*(H1-H2));
26 printf("\n the dryness after expansion and
      entrainment is \%.2 f", x24);
27
28 P3 = 205;
                           //discharge pressure in kN/m<sup>2</sup>
29 //Assuming that the steam at the discharge pressure
      P3 = 205 \text{ kN/m2} is also saturated
30 \times 3 = 1;
31 H3 = 2675; //enthalpy of the mixture at the start of
      compression in the diffuser section at 101.3 kN/
      m2
32
33 //Again assuming the entrained steam is also
```

```
saturated, the enthalpy of the mixture after
      isentropic compression in the diffuser from 101.3
      to 205 \text{ kN/m2} is H4
                      //in kJ/kg
34 \text{ H4} = 2810;
35 m = {[(H1-H2)/(H4-H3)]*e1*e2*e3-1}; //m = m2/m1
36 printf ("n m2/m1 = \%.2 f kg vapour entrained/kg kive
      stream",m);
37 printf("\n Thus with a flow of 0.14 kg/s live steam,
       the vapour entrained at 101.3 kN/m2 is %.2 f kg/
      sec ",0.14*m);
38 printf('\n Total saturated steam = \%.2 \, f \, kg/sec at
      205 \text{ kN/m}^2, 0.14+0.14*\text{m};
  printf ("\n The economy of the steam = \%.2 \,\mathrm{f}
      ", 0.214/0.14);
40 printf ("\n The capacity in terms of throughput of
      solution Gf = \%.3 f \text{ kg/sec}^{"}, 0.214 + 0.025);
```

Scilab code Exa 14.6 Method to drive the compressor

```
1 clear;
2 clc;
3 printf("\n Example 14.6");
4 //(a) Diesel engine
5 printf("\n (a) Diesel engine");
6
7 printf("\n For 1 kg evaporation, ammonia circulated = 2.28 kg");
8 printf("\n Work done in compressing the ammonia = %d MJ/kg",150*2.28);
9 printf("\n For an output of 1 MJ, the engine consumes 0.4 kg fuel.");
10 printf("\n fuel consumption = %.3 f kg/kg water evaporated",0.4*0.342);
11 printf("\n cost = %.5 f euro/kg water evaporated ",0.02*0.137);
```

```
12
13 printf("\n (b) Turbine");
14
15 printf("\n The work required is 0.342 MJ/kg
      evaporation");
16 //Therefore with an efficiency of 70 per cent:
17 printf("\n energy required from steam = \%.3 \, f \, MJ/kg"
      ,0.342*100/70);
18 printf("\n Enthalpy of steam saturated at 700 kN/m2
      = 2764 \text{ kJ/kg.}");
19 printf("\n Enthalpy of steam saturated at 101.3 kN/
      m2 = 2676 \text{ kJ/kg}");
20 printf("\n thus : energy from steam = \%d kg/kg"
      ,2764-2676);
21 printf ("\n steam required = \%.2 \,\mathrm{f} kg/kg evaporation"
      ,0.489/0.088);
22 printf("\n Cost = \%.4 f euro/kg water evaporated"
      ,0.01*5.56/10);
23 printf("\n Hence the Diesel engine would be used for
       driving the compressor");
```

Scilab code Exa 14.7 Optimum boiling time

```
10 Qb = (2*40*40)*(7*10^{(-5)})*[((7*10^{(-5)}*2.81*10^4)
      +0.2) ^0.5-0.2^0.5];
11 printf("\n The heat transferred during boiling is %
      .2 f*10^7 kJ", Qb);
12 printf("\n the water vaporated = \%.2 \text{ f} * 10^4 \text{ kg}"
      ,(4.67*10^{(7)}/2300)*10^{(-4)};
13 printf("\n Rate of evaporation during boiling = \%.3 f
       kg/secs", (2.03*10^4)/(2.81*10^4));
14 printf("\n Mean rate of evaporation during the cycle
       = \%.3 \, f \, kg/secs, 2.03*10^(4)/[(2.8*10^4)
      +(15*10^3)]);
15 printf("\n cost = \%.1 f euro/cycle", ((2.81*10^(4)*18)
      /1000)+600);
16
17
18 printf("\n (b) Minimum cost");
19 t_bopt1 = (600/0.018) + [2*(7*10^(-5)*0.2*600*0.018)]
      ^0.5]/(7*10^(-5)*0.018);
20 printf("\n The boiling time to give minimum cost is
     \%.1 f ksecs", t_bopt1*10^(-3));
21 \quad Qb1 = [(2*40*40)/(7*10^{(-5)})]*[(7*10^{(-5)}*5.28*10^{4}
      + 0.2)^0.5-0.2^0.5;
22 printf("\n The heat transferred during one boiling
      period is \%.2 f*10^7 kJ, Qb1*10^(-7))
23 printf("\n The water evaporated = \%.2 \, f*10^4 \, kg",Qb1
      /2300);
24 printf("\n Rate of evaporation = \%.3 \, \text{f kg/secs}"
      ,(3.03/5.28));
25 printf("\n Mean rate of evaporation during the cycle
       = \%.2 \, \text{f kg/secs}", (3.03*10^4)/[(5.28*10^4)]
      +(15*10^3)]);
26 printf("\n cost of one cyce = \%.1 f euro", 5.28*10^(4)
      *0.018+600):
```

Chapter 15

Crystallisation

Scilab code Exa 15.1 Supersaturation ratio

```
1 clear;
2 clc;
3 printf("\n Example 15.1");
4 printf("\n For concentrations in kg sucrose/kg water
                               //\operatorname{concentration} is in kg/kg
5 c = 2.45;
6 printf("\n c = \%.2 \, \text{f kg/kg}",c);
7 c1 = 2.04;
                               //concentration is in kg/kg
8 printf("\n c1 = \%.2 \, \text{f kg/kg}", c1);
9 S = c/c1;
10 printf("\n S = \%.2 \, \text{f}",S);
11
12 printf("\n\n For concentrations in kg sucrose/kg
      water:")
13 co = c/(c+1);
                               //concentration is in kg/kg
       solution
14 printf("\n co = \%.3 f \text{ kg/kg solution}",co);
15 co1 = c1/(c1 + 1); //concentration is in kg/kg
       solution
16 printf("\n co1 = \%.3 f kg/kg solution", co1);
17 S = co/co1;
```

Scilab code Exa 15.2 Increase in solubility

```
1 clear;
2 clc;
3 printf("\n Example 15.2");
4 printf("\n For barium sulphate");
6 function[x] = increase_barium(d)
       y = \exp((2*233*0.13)/(2*8314*298*4500*d));
8
       x = y-1;
       funcprot(0);
10 endfunction
11 i=1;
12 d = [0.5 0.05 0.005];
13 while(i<=3)
       printf("\n Increase in solubility for barium
14
          sulphate fpr particle size %f um = %f per
          cent", d(i)*2, (increase_barium(d(i)*10^{(-6)})
          *100));
15
       i = i+1;
16 \text{ end}
17
18 printf("\n For Sucrose");
19 function[a] = increase_sucrose(d1)
       b = \exp((2*342*0.01)/(1*8314*298*1590*d1));
20
21
       a = b-1;
22
       funcprot(0);
23 endfunction
24 j = 1;
25 while (j<=3)
       printf("\n Increase in solubility for barium
26
          sulphate fpr particle size %f um = %f per
          cent",d(j)*2,(increase_sucrose(d(j)*10^(-6))
```

Scilab code Exa 15.3 Theoretical yield

```
1 clear;
2 clc;
3 printf("\n Example 15.3");
4 R = 322/142;
5 //The initial concentration
6 c1 = 1000/5000;
                                   //Concentration is in
      kg Na2SO4/kg water
7 printf("\n The initial concentration c1 = \%.1 f \text{ kg}
      Na2SO4/kg water",c1);
8 //The solubility
9 c2 = 9/100;
                                   //solubility is in Kg
     Na2SO4/kg water
10 printf("\n The solubility c2 = \%.2 f \text{ Kg Na} 2SO4/\text{kg}
      water",c2);
11 printf("\n Initial mass of water, w1 = 5000 kg and
      the water lost by evaporation E = \%f kg/kg"
      ,2/100);
12 printf("\n yield y = \%d kg Na2SO4.10H2O", (5000*2.27)
      *[0.2-0.09*(1-0.02)]/[1-0.09*(2.27-1)]);
```

Scilab code Exa 15.4 Yield of Sodium acetate

```
1 clear;
2 clc;
3 printf("\n Example 15.4");
4 //Given data:
5 //Heat of crystallisation, q = 144 kJ/kg trihydrate
```

```
6 //Heat capacity of the solution, Cp = 3.5 \text{ kJ/kg deg}
7 //Latent heat of water at 1.33 kN/m2,
                                               = 2.46 \text{ MJ}/
      kg
8 //Boiling point of water at 1.33 \text{ kN/m2} = 290.7 \text{ K}
9 //Solubility of sodium acetate at 290.7 K, c2 =
      0.539 \text{ kg/kg water}
10
11 //Equilibrium liquor temperature
12 T = 290.7 + 11.5;
13 printf("\n Equilibrium liquor temperature is\%.1 f K",
      T);
14
15 // Initial concentration
16 c1 = 40/(100-40);
17 printf("\n Initial concentration c1 = \% .3 f kg/kg
      water", c1);
18
19 //Final concentration
20 c2 = 0.539;
21 printf("\n Final concentration, c2 = \%.3 f \text{ kg/kg} water
      ",c2);
22
23 //Ratio of molecular masses
24 printf("\n Ratio of molecular masses, R = \%.2 f"
      ,136/82);
25
26 E = \{144*1.66*(0.667-0.539)+3.5*(353-302.2)\}
      *(1+0.667)*[1-0.539*(1.66-1)
      ] /{2460*[1-0.539*(1.66-1)]-(144*1.66*0.539)};
27 printf("\n\n E = \%.3 f kg/kg water originally
      present", E);
28 printf("\n yeild y = \%.3 \, \text{f kg/sec}", (0.56*(100-40)
      /100) *1.66*[0.667-0.539*(1-0.153)
      ]/[1-0.539*(1.66-1)]);
```

Scilab code Exa 15.5 Length of crystalliser

```
1 clear;
2 clc;
3 //The molecular mass of hydrate/molecular mass of
      anhydrate
    R = 380/164;
5 printf("\n The molecular mass of hydrate/molecular
      mass of anhydrate, R = \%.2 \, f", R);
6 //It will be assumed that the evaporation is
      negligible and that E = 0.
7 c1 = 0.23;
8 printf("\n The initial concentration, c1 = \%.2 f \text{ kg/}
      kg solution or \%.2 f \text{ kg/kg water}, c1, c1/(1-c1));
9 c2 = 15.5;
10 printf ("\n The final concentration, c2 = \%.1 f \text{ kg/kg}
      water or 0.155 \text{ kg/kg water}, c2);
11 \quad w1 = 0.77;
12 printf("\n In 1 kg of the initial feed solution,
      there is 0.23 kg salt and 0.77 kg water and hence
       w1 = \%.2 f kg", w1);
13 y = 2.32*0.77*[0.30-0.155*(1-0)]/[1-0.155*(2.32-1)];
14 printf("\n yeild y = \%.2 f kg",y);
15 printf("\n In order to produce 0.063 kg/s of
      crystals, the required feed is: \%.3 f kg/sec"
      ,1*0.063/0.33);
16 q = 0.193*3.2*(313-298);
17 printf("\n The heat required to cool the solution %
      .1 f kW",q);
18 \ q1 = 0.063*146.5;
19 printf("\n Heat of crystallisation = \%.1 \text{ f kW}",q1);
20 printf("\n total heat loss = \%.1 \, \text{f kW}",q+q1);
21 printf("\n Assuming counter current flow");
22 \text{ deltaT1} = (313-293);
```

```
printf("\n deltaT1 = %d deg K",deltaT1);
deltaT2 = 298 - 288;
printf("\n deltaT2 = %d deg K",deltaT2);
deltaTlm = (deltaT1-deltaT2)/log(deltaT1/deltaT2);
printf("\n The logarithmic mean temperature is %.1f deg K",deltaTlm)

A = (q+q1)/(0.14*14.4);
printf("\n The heat transfer area required, A= Q/U

deltaTm = %.1f m^2",A);
printf("\n Length of heat exchanger required = %.1f",A)

printf("\n\n\n\n In practice 3 lengths, each of 3 m length would be specified.");
```

Scilab code Exa 15.6 Crystal production rate

```
1 clear;
2 clc;
3 printf("\n Example 15.6");
4 \text{ down\_time} = (4/0.00017);
5 printf("\n Draw down time = %d secs", down_time);
6 printf("\n\n
                                (a)");
7 printf("\n from a mass balance the total mass of
      solids is :")
8 cs = (6*0.6*2660*10^13)*(10^(-8)*23530)^4;
9 printf("\n cs = \%d kg/m<sup>3</sup>",cs);
10 printf("\n\n
                                  (b)");
11 printf("\n The production rate = \%.3 \, f \, kg/sec",cs
      *0.00017);
12
13 printf("\n The crystal population decreases
      exponentially with size ")
```

Scilab code Exa 15.7 Vapour pressure

Scilab code Exa 15.8 Mass sublimation rates

```
1 clear;
2 clc;
3 printf("\n Example 15.8");
```

```
4 printf("\n Vaporisation stage :");
5 Pt = 101.5;
6 Ps = 1.44;
7 Sv = 0.56*(138/29)*(1.44/(101.5-1.44));
8 printf("\n Sv = %.3 f kg/sec",Sv);
9
10 printf("\n\n COndensation stage: ")
11 Ptc = 100;
12 Psc = 0.0023;
13 S = 0.56*(138/29)*(0.0023/(100-0.0023));
14 printf("\n S = %f kg/sec",S);
```

Chapter 16

Drying

Scilab code Exa 16.1 Time taken to dry the solids

```
1 clear;
2 clc;
3 printf("\n Example 16.1");
4 //For the first drying operation
5 \text{ w1} = 0.25;
                                 //in kg/kg
6 \quad w = 0.10;
                                 //in kg/kg
7 \text{ wc} = 0.15;
                                 //in kg/kg
8 \text{ we} = 0.05;
                                 //in kg/kg
                                 //in kg/kg
9 	 f1 = w1 - we;
                                 //in kg/kg
10 fc = wc - we;
                                 //in kg/kg
11 f = w - we;
12
13 / x = mA
14 function[x]=TotalDryingTime(t)
15
       x = (1/t)*[(f1-fc)/fc + log(fc/f)];
16
       funcprot(0);
17 endfunction
18 printf("\n mA = %.3 f kg/sec", TotalDryingTime(15)
      );
19
20 //For the second drying operation
```

```
//in kg/kg
21 \text{ w} 12 = 0.30;
22 	 w2 = 0.08;
                                      //in kg/kg
23 \text{ wc2} = 0.15;
                                      //in kg/kg
                                      //in kg/kg
24 \text{ we2} = 0.05;
25 	 f12 = w12 - we2;
                                      //in kg/kg
26 \text{ fc2} = \text{wc2} - \text{we2};
                                      //in kg/kg
27 	 f2 = w2 - we2;
                                      //in kg/kg
28
29 t1=(1/TotalDryingTime(15))*[(0.25-0.10)/0.10 + log
      (0.10/0.03);
30 printf("\n The total drying time is then %.1f ksec
      or \%.2 f hr ",t1,t1*1000/3600);
```

Scilab code Exa 16.2 Time taken to dry the solids

```
1 clear;
2 clc;
3 printf("\n Example 16.2");
4 E = [1 0.64 0.49 0.38 0.295 0.22 0.14];
5 J = [0 0.1 0.2 0.3 0.5 0.6 0.7];
6 plot(J,E,rect=[0,1,0,1]);
7 xtitle ("Plot for drying data", "J = kt/L^2", "E");
8
9 //For the 10 mm strips
10 \text{ mi} = (0.28 - 0.07);
                               //Initial free moisture
      content in kg/kg
11 mf = (0.13-0.07);
                               //Final free moisture
     content in kg/kg
12 / at
13 t = 25;
                               //time is in ksecs
14 E = (0.06/0.21);
15 //at E = 0.286 ,J = 0.52 from the plot of given data
      and J = kt/L^2
16 k = poly([0], 'k');
17 k1 = roots(0.52 - (k*t)/(10/2)^2);
```

Scilab code Exa 16.3 Mass flow rate of dry air

```
1 clear;
2 clc;
3 printf("\n example 16.3");
4 //(a) Air
5 //G kg/s dry air enter with 0.006G kg/s water vapour
       and hence the heat content of this stream=
  //[(1.00G) + (0.006G)]
                            2.01) ] (385
                                          273) = 113.35
     G kW
8 //(b) Wet solid
9 //0.125 \text{ kg/s} enter containing 0.40 \text{ kg water/kg} wet
      solid, assuming the moisture is expressed on a
      wet basis.
10 flowWater = (0.125*0.40);
                                              //in kg/sec
                                              //in kg/sec
11 flowDrySolid = (0.125-0.050);
12 //Hence heat content of this stream
13 q = [(0.050*4.18)+(0.075*0.88)]*(295-273);
14 printf ("\n The heat content of this stream = \%.2 f kW
     ",q);
```

```
15
16 //Heat out
17 //(a) Air
18 //Heat in exit air = [(1.00 \text{ G}) + (0.006 \text{ G})]
                                                       2.01)
      ](310
                 273) = 37.45G \text{ kW}.
19 \text{ fd} = 0.075;
                                 //mass flow rate of dry
      solids in kg/sec
20 \quad w = 0.05*0.075/(1+0.05);
                                //water in the dried
      solids leaving in kg/secs
21 \text{ we} = (0.050 - \text{w});
                                 //The water evaporated
      into gas stream in kg/secs
22
23 //Assuming evaporation takes place at 295 K, then:
24 \text{ qout} = 0.0464*[2.01*(310-295)+2449+4.18*(295-273)];
25 printf ("\n Heat in the water vapour = \%.1 \,\mathrm{f} kW", gout)
26
   //the total heat in this stream = (119.30 + 37.45G)
      kW.
   //(b) Dried solids
28
29
30
      //The dried solids contain 0.0036 kg/s water and
31
                                  t of this stream is:
          hence heat conten
      q1 = [(0.075*0.88) + (0.0036*4.18) / (305-273)];
32
33
      printf("\n The dried solids contain 0.0036 kg/s
          water and hence heat content of this stream is
          : \%.2 f kW, q1);
34
35
36 //(c) Losses
37 //These amount to 20 kJ/kg dry air or 20m kW.
38 //Heat Balance
39 G = poly([0], 'G');
40 \text{ G1} = \text{roots}(113.35*G + 6.05 - 119.30 - 37.45*G - 2.59)
       -20*G);
41 printf("\n G = \%.2 \, \text{f kg/secs}", G1);
42 printf("\n Water in the outlet stream %.4 f kg/secs"
```

```
,0.006*2.07+0.0464);
43 printf("\n The humidity H = %.4 f kg/kg dry air"
,0.0588/2.07);
```

Scilab code Exa 16.4 Approximate drying time

```
1 clear;
2 clc;
3 printf("\n Example 16.4");
4 //In 100 kg of feed
6
      //mass of water =
      mw = 100*30/100;
                                          //mass of water
          in kg
      //mass of dry solids =
      md = 100-30;
                                          //mass of dry
         solids
10
11 // and:
12 //For b kg water in the dried solids: 100b/(b + 70)
     = 15.5
13 b = poly([0], 'b');
14 \ b1 = roots(100*b - 15.5*(b+70));
15 printf("\n water in the product ,b = \%.1 \, \text{f kg}",b1);
16
17
      //Initial water content
      w1 = 30/70;
                               //Intial moisture content
18
         in kg/kg dry solids
19
      //Final moisture content
      w2 = (12.8/70);
                              //Final moisture content
20
         in kg/kg dry solids
21
      //water to be removed
      w3 = (30-12.8);
                              //water to be removed in
22
         kg
23
```

Scilab code Exa 16.5 Proposed diameter and length

```
1 clear;
2 clc;
3 printf("\n Example 16.5");
4 //Inlet air temperature
5 \text{ Tair} = 400;
                           //Inlet air temperature in
      kelvins
                            //Humidity is in kg/kg dry
6 H = 0.01;
      air
7 //*therefore wet bulb temperature =
                           //Inlet wet-bulb temperature
8 Twetbulb = 312;
9 \text{ NTU} = 1.5;
                             //Number of transfer units
10
11 //Then for adiabatic drying the outlet air
      temperature, To is given by
12 To = poly([0], 'To');
13 To1 = roots(exp(1.5)*(To-312)-(400-312));
14 printf("\n For adiabatic drying the outlet air
      temperature = \%.1 f K", To1);
15
```

```
16 //Solids outlet temperature will be taken to be
     maximum allowable, 325K
17 //From the steam tables in the Appendix, the latent
     heat of vaporisation of water at 312 K is 2410 kJ/
     kg. Again from steam tables, the specific heat
      capacity of water vapour = 1.88 kJ/kg K and that
      of the solids will be taken as 2.18 kJ/kg K.
18
19 //For a mass flow of solids of 0.35 kg/s and inlet
     and outlet moisture contents of 0.15 and 0.005 kg
      /kg dry solids respectively, the mass of water
      evaporated = 0.35(0.15)
                              0.005) = 0.0508 kg/s.
20
  //For unit mass of solids , the heat duty includes:
          //Heat to the solids
22
          qsolids = 2.18*(325-300);
                                            //heat to
23
             solids in kJ/kg
          //Heat to raise the moisture to the dew point
24
          qdew = (0.15*4.187*(312-300)); //in kJ/kg
25
26
          //Heat of vaporisation
27
          qvap = 2410*(0.15-0.005);
                                            //in kJ/kg
          //Heat to raise remaining moisture to solids
28
             outlet temperature
          qremaining = (0.05*4.187)*(325-312);
29
          //Heat to raise evaporated moisture to the
30
             air outlet temp.
31
          qevapo = (0.15-0.005)*1.88*(331.5-312);
32
          qtotal = qsolids + qdew + qvap + qremaining +
              qevapo;
          printf("\n Total heat = \%.1 \, \text{f kJ/kg} or \%d \, \text{kW}",
33
             qtotal,qtotal*0.35);
34
  //The humid heat of entering air is 1.03 kJ/kg K
35
          //G1 (1 + H1) = Q/Cp1(T1)
36
                                       T2)
          //where: G1 (kg/s) is the mass flowrate of
37
             inlet air,
          //H1 (kg/kg) is the humidity of inlet air,
38
          //Q (kW) is the heat duty,
39
```

```
//Cp1 (kJ/kg K) is the humid heat of inlet
40
              air
          //and: T1 and T2 (K) are the inlet and outlet
41
               air temperatures
                                          respectively.
42
          G1 = poly([0], 'G1');
          G = roots(G1*(1+0.01)-146/(1.03*(400-331.5)))
43
44
          printf("\n Mass flow rate of inlet air = \%.2 f
              kg/secs", G);
          printf("\n Mass flow rate of dry air ,Ga = \%
45
             .2 f kg/secs, G/1.01);
          printf("\n the humidity of the outlet air H2
46
             = \%.4 \, \text{f} \, \text{kg/kg}, 0.01+0.0508/2.05);
47
48 //At a dry bulb temperature of 331.5 K, with a
      humidity of 0.0347 kg/kg, the wet-bulb
      temperature of the outlet air, from Figure 13.4 in
       Volume 1, is 312 K, the same as the inlet, which
       is the case for adiabatic drying.
49
50 //The dryer diameter is then found from the
      allowable mass velocity of the air and the
      entering air flow and for a mass velocity of 0.95
       kg/m<sup>2</sup>.secs, the cross sectional area of the
      drver is
51 printf("\n The cross sectional area of the dryer is
     \%.2 \text{ f m}^2", 2.07/0.95);
52 printf("\n The equivalent diameter of the dryer = \%
      .2 f m, [(4*2.18)/%pi]^0.5);
53
   //With a constant drying temperature of 312 K:
54
           //at the inlet
55
           deltaT1 = 400-312;
                                           //inlet
56
              temperature is in deg K
            //at the outlet
57
           deltaT2 = 331.5-312;
                                           //outlet
58
               temperature is in deg K
           Tlogmean = (deltaT1 - deltaT2)/log(deltaT1/
59
```

```
deltaT2);
60
            printf("\n Logarithmic mean temperature
               difference = \%.1 f \deg K, Tlogmean);
   //The length of the dryer, L is then: L = Q/(0.0625)
       DG^{(0.67)}*Tm
       //where D (m) is the diameter
62
       //and G(kg/m^2.secs) is the air mass velocity.
63
       L = 146/[0.0625*(\%pi)*1.67*(0.95)^{(0.67)}*45.5];
64
       printf("\n The length of the dryer = \%.1 \, \text{f m}",L);
65
       printf("\n Length/diameter ratio = %d "
66
           ,10.1/1.67);
```

Scilab code Exa 16.6 Specified diameter of the bed

```
1 clear;
2 clc;
3 printf("\n Example 16.6");
4 H = 0.036;
                              //Humidity is in kg/kg at
      811 K
5 //Taking R as 90 per cent and P as 101.3 kN/m2, then
      , for assumed values of Tb of 321, 333 and 344 K
6
        //Pw = 13,20 and 32 \text{ kN/m2}, respectively
        //G = 27.8, 12.9 and 6.02 kg/s, respectively.
9 / for Tb = 321, 333 and 344 K,
10 //G = 7.16, 7.8 and 7.54 kg/s respectively.
11 Tb = [321 \ 333 \ 344];
12 \text{ G1} = [27.8 \ 12.9 \ 6.02];
                                      //Temperature is in
       kelvins
13 G = [7.16 7.8 7.54];
                                      //flow rate in kg/
      secs
14 plot2d(Tb,G,style=3);
15 plot2d(Tb,G1,style=2);
16 xtitle ("Temperature vs Flow rate", "Temperature Tb(K)
      ", "Flow rate G(kg/secs)");
```

```
17
18
19 // Plotting G against Tb for each equation on the
      same axis, then
                                         //Gas flow rate is
20 \text{ Go} = 8.3;
       in kg/secs
                                         //temperature is
21 Tb = 340;
      in Kelvins
22 \text{ uf} = 0.61;
                                         //velocity is in m
      /secs
23
24 D = sqrt(340*(8.3+(1.58*1.26))/(278*0.61));
25 printf("\nD = %.2 f m",D);
```

Chapter 17

Adsorption

Scilab code Exa 17.1 Comparison of estimates with the geometric surfaces

```
1 //Example 17.1
2 clear;
3 clc;
4 printf("\n Example 17.1");
  //For 1 m3 of pellet with a voidage
                                            , then
           //Number of particles = (1)
                                                ) / (
                                                     /6)(15
                   10^
                         9 ) ^3
            //Surface area per unit volume = (1
                 (15)
                        10
                           9)2/(/6)(15
                                               10^
            //= 6(1)
                                   10^{\circ}(9) m^{2}/m^{3}
                           )/(15
            //1 m<sup>3</sup> of pellet contains 2290(1-
               solid and hence:
10
            specific_surface = 6/(15*10^{-9})*2290);
11
           printf("\n Specific surface = \%.3 f*10^5 m^2/
              kg ",specific_surface*10^(-5));
   //(a) Using the BET isotherm
12
13
           //y = (P/Po)/V *10^{(-6)}
14
           y = [1500 \ 2660 \ 3576 \ 4283 \ 4613 \ 4615];
15
           //y1 = (P/Po)/V *(1-(P/Po))
16
```

```
17
            y1 = [1666 3333 5109 7138 9226 11358];
             //x = P/Po
18
            x = [0.1 \ 0.2 \ 0.3 \ 0.4 \ 0.5 \ 0.6];
19
20
            plot2d(x,y,style = 2);
            xtitle("","P/Po","(P/Po)/(V *10^{(-6)}) or (P/Po)/(V *10^{(-6)})
21
                Po) / (V * (1-(P/Po))");
22
            plot2d(x,y1,style=3);
             legend ("Langmuir isotherm", "(BET) isotherm")
23
                ;
24
           //intercept, 1/VB = 300, and slope, (B)
25
                                                              1)
              /VB = 13,902
26
           B = (13902/300) + 1;
           printf("\n B = \%.2 f ",B);
27
           V = 1/(300*47.34);
28
           //Total surface area
29
           S = [(70.4*10^{(-6)}*808*6.2*10^{(26)}]
30
               *0.162*10^(-18))]/28;
           printf("\n Total surface area = \%.3 \, \text{f} *10^5 \, \text{m}
31
               ^2/\text{kg}, S*10^(-5));
32
33
   //(b) Using the Langmuir form of the isotherm
34
           // Slope 1/V = 13,902
35
           V = 1/13902;
36
           printf ("\n V = \%.1 \text{ f}*10^{(-6)}\text{m}^3/\text{kg}", V*10^6);
37
38
           //which agrees with the value of the BET
               isotherm
       //It may be noted that areas calculated from the
39
          isotherm are some 20 per cent greater than the
           geometric surface, probably due to the
          existence of some internal surface within the
          particles
```

Scilab code Exa 17.2 Applicability of various equilibrium theories

```
1 //Example 17.2
2 clear;
3 clc;
4 printf("\n Example 17.2");
5 //(a)
6
    //For n = 1,
     //(P/P0)/V = (P/P0)V1 + 1/B2V1
7
     //where V is the gas phase volume equivalent to
8
        the amount adsorbed
     //x = (P/Po)
9
10
       x = [0.05 \ 0.10 \ 0.15 \ 0.20 \ 0.25 \ 0.30 \ 0.35 \ 0.40];
11
     //y = (P/Po)/V \text{ in } kg/m^3
12
       y = [0.76 \ 1.35 \ 1.85 \ 2.27 \ 2.66 \ 2.94 \ 3.21 \ 3.42];
     //y1 = (P/Po)/(V*(1-P/Po)) in kg/m<sup>3</sup>
13
       y1 = [0.80 \ 1.50 \ 2.18 \ 2.88 \ 3.55 \ 4.20 \ 4.94 \ 5.73];
14
15
       plot(x,y,"o-");
       plot(x,y1,"+-");
16
       xtitle("","(P/Po)","(P/Po)/V or (P/Po)/(V*(1-P/Po))
17
          Po))");
       legend("B.E.T.", "Langmuir");
18
19
20
     //The data, which are plotted as (P /P 0)/V
        against P/P0 may be seen to conform to a
        straight line only at low values of P/P0,
                       g that more than one layer of
        suggestin
        molecules isadsorbed.
21
     Slope = 12.56;
22
     V1 = 1/12.56;
     //The surface area occupied by this absorbed
23
        volume
     S = V1*6.02*10^(26)*0.162*10^(-18)/24;
24
     printf("\n S = \%d m<sup>2</sup>/kg",S);
25
26
27
28 //(b)
     //P/P0/V*(1)
                       P/P0 = 1/V1*B2+(B2 1)/(V1*B2)*(P
29
         /P 0)
     //y2 = (P/Po)
30
```

Scilab code Exa 17.3 Length of the bed

```
1 //Example 17.3
2 clear;
3 clc;
4 printf("\n Example 17.3");
5 //For case (a):
     //\mathrm{Cs} = 10\mathrm{C} which represents a linear isotherm.
     //All concentrations move at the same velocity. If
        z0=0 at t=0 for a ll concentrations, the
        adsorption wave propagates as a step change
            from the inlet to the outlet concentration.
     //f (Cs ) = 10
8
     //u = 1 \ 10^{(4)}/[(4)*(0.15^{(2)}*)] \text{ m/s}
9
     //where is the intergranular voidage = 0.4
10
     e = 0.4;
11
     m = e/(1-e);
12
13
     printf("\n = \%f",m);
14
     t = 3600;
                              //time is in secs
15
     z = [(4*10^{(-4)})/(\%pi*(0.15^2)*0.4)]
        ]*[3600/(1+10*(0.6/0.4))];
     printf("\n z = \%.2 \text{ f m}",z);
16
17
18
19 //It may be noted that, when the adsorption wave
      begins to emerge from the bed, the bed is
```

```
saturated in equilibrium with the inlet
      concentration.
20 //Hence: uA tCO = zA[CO + (1)]
21
22 //For case (b):
23 //Cs = 3C0.3 which represents a favourable isotherm.
24 //As C increases, f(C) decreases and points of
      higher concentrations are predicted to move a
      greater distance in a given time than lower
      concentrations. It is not possible for points of
      higher concentrations to overtake lower
      concentrations, and if z0=0 for all
      concentrations, the adsorption wave will propagate
       as a step change similar to case a.
25
26 //Hence: z = ut/[1+(1/m)(Cs/Co)]
                                //in kmol/m<sup>3</sup>
     Co = 0.003;
27
28
     z = [(4*10^{(-4)}*5/((\%pi)*0.4*0.15^2))]
        ]*[3600/(1+(0.6/0.4)*(3/Co^0.7))];
     printf("\n z = \%.2 \text{ f m}",z);
29
30
31 //For case (c):
32 //Cs = (10^{\circ}(4))*(C^{\circ}2) which represents an
      unfavourable isotherm.
33 // f(C) = 2* 10^4 * C.
34 //As C increases, f (C) increases such that, in a
      given time, z for lower concentrations is greater
       than for higher concentrations. Following the
      progress of the breakpoint concentration, C =
      0.003 \text{ kmol/m}^3, then:
35 / f(0.003) = 60
     z1 = [4*10^{(-4)}/(\%pi*0.15^{(2)}*0.4)
36
        ]*[3600/(1+(0.60/0.40)*60)];
     printf("\n For case (c)");
37
     printf("\n z = \%.2 \text{ f m}", z1);
38
39
40
41 //At breakpoint, the bed is far from saturated and:
```

```
42 saturation = 100*[(4*10^(-4)*3600)/(%pi*(0.15^(2)
*0.4))]/[0.55*(1+(0.6/0.4)*(9/0.03))];
43 printf("\n saturation = %.1 f per cent", saturation);
```

Scilab code Exa 17.5 Moving bed adsorption design

```
1 clear;
2 clc;
3 printf("\n Example 17.5");
4 // let x = [f(C)] mean
    x = (8.4*10^{(-2)}*1266)/(2.67*10^{(-3)}*1.186);
7
    //e is porosity
      e = 0.47;
      m = e/(1-e);
9
      printf("\n = \%.2 f",m);
10
11
12 //The velocity uc with which the adsorption wave
      moves through the column may be obtained from
      equation 17.79
    uc = 6.2*10^{-}(-6);
13
                                       //density is in kg/m
    density = 1266;
14
        ^3
    Gs = uc*(1-e)*density;
15
    printf ("\n Gs = \%.2 \text{ f}*10^{(-3)} \text{ kg/m}^2.\text{sec}", Gs*10^3);
16
17
18
   //From overall balance:
19
     //We have given eq: Gs1(0.084-0)=0.129(0.00267)
20
     //On solving above eq :
21
     Gs1 = poly([0], 'Gs1');
22
     Gs2 = roots(Gs1*(0.084-0)-0.129*(0.00267));
23
24
     printf ("\n Gs1 = \%.2 \text{ f}*10^{(-3)} \text{ kg/m}^2.\text{sec}", Gs2
        *1000);
```

```
25
26 // Part (b)
    //time ta for the adsorption zone to move its own
27
       length za is given by:
28
    za = 0.185;
29
    ta = (za/uc)/3600;
    printf("\n ta = %.1 f hrs",ta);
30
31
32
    //The time taken for a point at a distance z into
       the zone to emerge is given by:
    //t = (z1/za)ta
33
    yr = [0.0001 \ 0.0002 \ 0.0006 \ 0.0010 \ 0.0014 \ 0.0018
34
       0.0022 0.0024];
    yre = [0.00005 0.0001 0.00032 0.00062 0.00100
35
       0.00133 0.00204 0.00230];
36 I = 0;
37 \quad I1 = 0;
38 i = 1;
39 printf("\nI= \%.1 f", I);
40 while i <=8
        y(i)=1/(yr(i)-yre(i));
41
        if i>1 then
42
            I = I + (yr(i)-yr(i-1))*(y(i)+y(i-1))/2;
43
            printf("\n I=\%.1 \, \text{f}",I);
44
45
        end
46
        i=i+1;
47 end
48 \text{ z_za} = [0 \ 0.137 \ 0.362 \ 0.473 \ 0.560 \ 0.674 \ 0.852]
      1.000];
49 t = (z_za)*ta;
50 \quad j = 1;
51 while j<=8
52
        printf("\ntime = \%.1 f h",t(j));
53
        j = j + 1;
54 end
```

Chapter 18

Ion Exchange

Scilab code Exa 18.1 Prediction of time t against xs values

```
1 clear;
2 clc;
3 printf("\n Example 18.1");
                //in kg/kg
4 Cse=0.132;
5 \text{ Cs} = [0.091 \ 0.097 \ 0.105 \ 0.113 \ 0.125 \ 0.128 \ 0.132];
6 C = Cs/Cse;
7 C1 = 1-C;
8 C2 = 1-C^2;
9 t = [2 4 10 20 40 60 120];
10 // xset ('window', 1);
11 //
12 plot(t,C1,t,C2);
13 xtitle('1-(Cs/Cs* vs t(min)',"1-(Cs/Cs*)", 't(min)');
14 legend("1-(C_S/C_S*)","1-(C_S/C_S*)^2");
15
16 //From the plot ^2Dr/ri^2 = 0.043
17 //For a pellet of twice the radius, that is r = 2ri
18 Slope = -0.043/4;
19 printf("\n Slope = \%.3 \, f", Slope);
20
21 //Thus, when the radius = 2ri
```

```
22 function[x] = equation1(t)
       x = 1-(6/(\%pi)^2)*exp(-Slope*t);
23
24
       funcprot(0);
25 endfunction
26
               \exp\left(
27 //CS/CS*=[1]
                          D R / tri^2) ]^0.5
28 // DR/ri^2 = 0.04
29 //For a pellet twice the size
30
31 function[x1] = equation2(t)
       x1 = [1-exp(-0.01*t)]^0.5;
32
33
       funcprot(0);
34 endfunction
35
36 printf("\n t(min)
                                                       ");
                                      Cs(kg/kg)
37 printf("\n
                              equation (i)
      equation (ii)
                     ");
38 t = [4 20 60];
                                  //t is in min
39 i = 1;
40 while i<=3
41 printf ("\n %f
                                  %f
           ",t(i),Cse*equation1(t(i)),Cse*equation2(
      t(i)));
42 i = i + 1;
43 end
```

Scilab code Exa 18.2 Concentration of HNO3 in solution

```
//HNO3 (Molecular weight = 63 kg/kmol)
//Concentration = p per cent
//Concentration = (10p/63)(1030/1000) = 0.163p kg/m3
//In the solution: xNa+ = 0.242/(0.242 + 0.163p)
//For univalent ion exchange
//yNa+/(1 yNa+) = KNa+H + [xNa+/(1 xNa+)]
// yNa = 0.1;
K_NaH = 2/1.3;
p = poly([0], 'p');
p1 = roots((0.1/0.9)*[0.163*p*(0.242+0.163*p)]);
printf("\n p = %d percent",p1(1));
```