Scilab Textbook Companion for Fundamentals Of Thermodynamics by B. Claus And R. E. Sonntag¹

Created by
Kush Garg
B.Tech
Civil Engineering
Indian Institute of Technology Roorkee
College Teacher
Not Applicable
Cross-Checked by
TechPassion

August 10, 2013

¹Funded by a grant from the National Mission on Education through ICT, http://spoken-tutorial.org/NMEICT-Intro. This Textbook Companion and Scilab codes written in it can be downloaded from the "Textbook Companion Project" section at the website http://scilab.in

Book Description

Title: Fundamentals Of Thermodynamics

Author: B. Claus And R. E. Sonntag

Publisher: Wiley India Pvt. Ltd., New Delhi

Edition: 7

Year: 2010

ISBN: 978-81-265-2152-4

Scilab numbering policy used in this document and the relation to the above book.

Exa Example (Solved example)

Eqn Equation (Particular equation of the above book)

AP Appendix to Example(Scilab Code that is an Appednix to a particular Example of the above book)

For example, Exa 3.51 means solved example 3.51 of this book. Sec 2.3 means a scilab code whose theory is explained in Section 2.3 of the book.

Contents

Lis	List of Scilab Codes	
2	Control Volumes and Units	9
3	Pure Substance Behaviour	14
4	Energy Transfers	22
5	Energy Equation for a Control Mass	25
6	Energy Equation for a Control Volume	33
7	The Classical Second Law of Thermodynamics	42
8	Entropy for a Control Mass	45
9	Entropy Equation for a Control Volume	53
10	Availibility	61
11	Power and Refrigeration Systems with phase change	64
12	Power and Refrigeration Systems gaseous working fluids	70
13	Ideal Gas Mixtures	79
14	Thermodynamics Property Relations	84
15	Comustion	80

16 Phase and Chemical Equilbrium	94
17 Compressible Flow	97

List of Scilab Codes

Exa 2.1	Weight of a person
Exa 2.2	Average Volume and Density
Exa 2.3	Calculating the required force
Exa 2.4	Calculating atmospheric pressure
Exa 2.5	Pressure inside vessel
Exa 2.6	Calculating Pressure
Exa 2.7	Calculating Balancing Force
Exa 3.1	Determining the phase of water
Exa 3.2	Determining the phase of Ammonia
Exa 3.3	Determining the quality and specific volume 15
Exa 3.4	Percentage of vapor
Exa 3.5	Calculating pressure after heat addition 16
Exa 3.6	Determining the missing property
Exa 3.7	Determining the pressure of water
Exa 3.8	Calculating mass of air
Exa 3.9	Calculating pressure inside tank
Exa 3.10	Mass flow rate
Exa 3.11	Predicting the nature of given state
Exa 3.12	Determining specific using different laws
Exa 3.13	Calculating mass of gas
Exa 4.1	Work done during different processes
Exa 4.3	work produced
Exa 4.4	Calculating work done
Exa 4.7	Heat transfer
Exa 5.1	Calculating height
Exa 5.2	Change in internal energy
Exa 5.3	Analysis of energy transfer
Exa 5.4	Determining the missing properties

Exa 5.5	Calculating heat transfer for the given process	28
Exa 5.6	Calculating work and heat transfer for the process	29
Exa 5.8	Calculating change in enthalpy	29
Exa 5.9	Determining amount of heat transfer	30
Exa 5.10	Calculating rate of increase of internal energy	31
Exa 5.11	Rate of change of temperature	31
Exa 6.1	Calculating mass flow rate	33
Exa 6.2	Work done for adding the fluid	33
Exa 6.3	Rate of flow of water	34
Exa 6.4	Determining quality of steam	34
Exa 6.5	Quality of ammonia leaving expansion valve	35
Exa 6.6	Power output of turbine in kW	35
Exa 6.7	Heat transfer rate in aftercooler	36
Exa 6.8	Required Pump work	37
Exa 6.9	Heat transfer in simple steam power plant	37
Exa 6.10	Analysis of refrigerator	38
Exa 6.11	Determining the final temperature of steam	39
Exa 6.12	Calculating mass flow of steam in tank	40
Exa 6.13	Calculating mass flow of steam in tank	40
Exa 7.1	Rate of fuel consumption	42
Exa 7.2	Coefficient of performance of refrigerator	42
Exa 7.4	Comparison of ideal carnot heat engine with actual heat	
	engine	43
Exa 7.5	Calculating required work	44
Exa 8.1	Coefficient of performance of refrigerator	45
Exa 8.2	Heat transfer in a given process	46
Exa 8.3	Entropy change	46
Exa 8.4	Entropy change with different assumptions	47
Exa 8.5	Entropy change	48
Exa 8.6	Work done by air	49
Exa 8.7	Work and heat transfer	49
Exa 8.8	Calculating increase in entropy	50
Exa 8.9	Entropy generation	51
Exa 8.10	Determining the entropy generated	51
Exa 9.1	Entropy generation	53
Exa 9.2	Exit velocity of steam from nozzle	54
Exa 9.3	Violation of second law	54
Exa 9.4	Calculating required specific work	55

Exa 9.5	Entropy generation	55
Exa 9.6	Work required to fill the tank	56
Exa 9.7	Work required to pump water isentropically	57
Exa 9.8	Velocity in exit flow	57
Exa 9.9	Rate of Entropy Generation	58
Exa 9.10	Turbine efficiency	58
Exa 9.11	Turbine inlet pressure	59
Exa 9.12	Required work input	60
Exa 10.1	Calculating reversible work	61
Exa 10.2	Calculating reversible work	62
Exa 10.3	Calculating reversible work and irreversibility	62
Exa 11.1	To determine the efficiency of Rankine cycle	64
Exa 11.2	To determine the efficiency of Rankine cycle	65
Exa 11.3	To determine the efficiency of a cycle	66
Exa 11.4	Efficiency of Refrigeration cycle	67
Exa 11.5	To determine thermal efficiency of cycle	68
Exa 12.1	Standard brayton cycle	70
Exa 12.2	Standard brayton cycle	71
Exa 12.3	efficiency of the cycle	72
Exa 12.4	Calculation of work in the given cycle	73
Exa 12.5	air standard cycle for jet repulsion	73
Exa 12.6	air standard refrigeration cycle	74
Exa 12.7	the otto cycle	75
Exa 12.8	the diesel cycle	76
Exa 13.3	calculating humidity ratio dew point mass of air mass	
	of vapor	79
Exa 13.4	calculating amount of water vapour condensed on cooling	80
Exa 13.5	calculating heat transfer per kilogram of dry air	80
Exa 13.6	calculating heat transferred in gas vapour mixture	81
Exa 13.7	calculating humidity ratio and relative humidity	82
Exa 14.1	to determine the sublimation pressure of water	84
Exa 14.4	Volume expansivity Isothermal and Adiabatic compress-	
	ibility	84
Exa 14.5	adiabatic steady state processes	85
Exa 14.6	isothermal steady state processes	86
Exa 14.7	percent deviation using specific volume calculated by	
	kays rule and vander waals rule	87
Exa 15.1	theoratical air fuel ratio for combustion of octane	89

Exa 15.6	determining heat transfer per kilomole of fuel entering	
	combustion chamber	89
Exa 15.7	calculating enthalpy of water at given pressure and tem-	
	perature	90
Exa 15.15	calculating reversible electromotive force	92
Exa 15.17	efficiency of generator and plant	92
Exa 16.2	to determine change in gibbs free energy	94
Exa 16.3	calculating equilibrium constant	95
Exa 17.1	to determine isentropic stagnation pressure and temper-	
	ature	97
Exa 17.3	determining the thrust acting on a control surface	97
Exa 17.5	determining velocity of sound in air	98
Exa 17.6	determining mass flow rate through control volume	99
Exa 17.7	determining exit properties in a control volume	100
Exa 17.9	determining exit plane properties in control volume	101

Chapter 2

Control Volumes and Units

Scilab code Exa 2.1 Weight of a person

Scilab code Exa 2.2 Average Volume and Density

```
// example 2
// average volume and density
clear

local Vliq=0.2 // volume of liquid in m^3
dliq=997 // density of liquid in kg/m^3
```

```
7 Vstone=0.12 //volume of stone in m<sup>3</sup>
8 Vsand=0.15 //volume of sand in m<sup>3</sup>
9 Vair=0.53 //vo; ume of air in m<sup>3</sup>
10 mliq=Vliq*dliq //mass of liquid in kg
11 dstone=2750 // density of stone in kg/m<sup>3</sup>
12 dsand=1500 // density of sand in kg/m<sup>3</sup>
13 mstone=Vstone*dstone //volume of stone in m^3
14 msand=Vsand*dsand //volume of sand in m^3
15 Vtot=1 //total volume in m<sup>3</sup>
16 dair=1.1 // density of air in kg/m<sup>3</sup>
17 mair=Vair*dair //mass of air
18 mtot=mair+msand+mliq+mstone //total mass in kg
19 v=Vtot/mtot //specific volume in m<sup>3</sup>/kg
20 d=1/v //overall density in kg/m<sup>3</sup>
21 printf("\n hence, average specific volume is v=\%.6 f
      m^3/kg. \ n", v)
22 printf("\n and overall density is d=\%.0 \text{ f kg/m}^3.\n"
      , d)
```

Scilab code Exa 2.3 Calculating the required force

```
//example 3
//calculating the required force
clear
clc
Dcyl=0.1 //cylinder diameter in m
Drod=0.01 //rod diameter in m
Acyl=%pi*Dcyl^2/4 //cross sectional area of cylinder in m^2
Arod=%pi*Drod^2/4 //cross sectional area of rod in m^2
Pcyl=250000 //inside hydaulic pressure in Pa
Po=101000 //outside atmospheric pressure in kPa
g=9.81 //acc. due to gravity in m/s^2
mp=25 //mass of (rod+piston) in kg
```

Scilab code Exa 2.4 Calculating atmospheric pressure

```
//example 4
//Calculating atmospheric pressure
clear
clc
dm=13534 //density of mercury in kg/m^3
H=0.750 //height difference between two columns in metres
g=9.80665 //acc. due to gravity in m/s^2
Patm=dm*H*g/1000 //atmospheric pressure in kPa
printf("\n hence, atmospheric pressure is Patm = %.2 f kPa. \n",Patm)
```

Scilab code Exa 2.5 Pressure inside vessel

```
//example 5
//pressure inside vessel
clear

clc
dm=13590 //density of mercury in kg/m^3
H=0.24 //height difference between two columns in metres
g=9.80665 //acc. due to gravity in m/s^2
dP=dm*H*g //pressure difference in Pa
Patm=13590*0.750*9.80665 //Atmospheric Pressure in Pa
```

Scilab code Exa 2.6 Calculating Pressure

```
1 //example 6
2 //calculating pressure
3 clear
4 clc
5 dg=750 //density of gaasoline in kg/m<sup>3</sup>
6 dR=1206 // density of R-134a in kg/m<sup>3</sup>
7 H=7.5 //height of storage tank in metres
8 g=9.807 //acc. due to gravity in m/s<sup>2</sup>
9 dP1=dg*g*H/1000 //in kPa
10 Ptop1=101 //atmospheric pressure in kPa
11 P1=dP1+Ptop1
12 disp('hence, pressure at the bottom of storage tank
      if fluid is gasoline is 156.2 kPa')
13 dP2=dR*g*H/1000 //in kPa
14 Ptop2=1000 //top surface pressure in kPa
15 P2=dP2+Ptop2
16 printf("\n hence, pressure at the bottom of storage
      tank if liquid is R-134a is P2 = \%.0 f kPa. \n", P2
     )
```

Scilab code Exa 2.7 Calculating Balancing Force

```
1 //example 62 //calculating balancing force
```

```
3 clear
4 clc
5 Po=100//Outside atmospheric pressure in kPa
6 F1=25 //net force on the smallest piston in kN
7 A1=0.01 //cross sectional area of lower piston in m
8 P1=Po+F1/A1 //fluid pressure in kPa
9 d=900 //density of fluid in kg/m<sup>3</sup>
10 g=9.81 //acc. due to gravity in m/s<sup>2</sup>
11 H=6 //height of second piston in comparison to first
       one in m
12 P2=P1-d*g*H/1000 //pressure at higher elevation on
      piston 2 in kPa
13 A2=0.05 // cross sectional area of higher piston in
     m^3
14 F2=(P2-Po)*A2 //balancing force on second piston in
     kN
15 printf("\n hence, balancing force on second larger
      piston is F2 = \%.1 f N. \n", F2)
```

Chapter 3

Pure Substance Behaviour

Scilab code Exa 3.1 Determining the phase of water

```
//example 1
//determining the phase of water
clear
clc
disp('from the table, we find that at 120C, saturation
    pressure of water is 198.5 kPa.But here we have
    pressure of 500 kPa.hence, water exists as a
    compressed liquid here.')
disp('also at 120C, vf=0.00106 kg/m^3 and vg=0.89186
    kg/m^3.given v=0.5 m^3/kg i.e. vf<v<vg, so we have
    two phase mixture of liquid and vapor.')</pre>
```

Scilab code Exa 3.2 Determining the phase of Ammonia

```
1 //example 2
2 //determining the phase
3 clear
4 clc
```

Scilab code Exa 3.3 Determining the quality and specific volume

```
1 //example 3
2 //determining the quality and specific volume
3 clear
4 clc
5 v1=0.5 //given specific volume in m<sup>3</sup>/kg
6 vf=0.001073 //specific volume when only liquid phase
       is present in m<sup>3</sup>/kg
7 vfg=0.60475 //in m^3/kg
8 disp('For water at a pressure of 300 kPa, the state
      at which v1 is 0.5 m<sup>3</sup>/kg is seen to be in the
      liquid-vapor two-phase region, at which T=133.6 C
      and the quality x is ')
9 x = (v1 - vf) / vfg / quality
10 v2=1 //given specific volume in m<sup>3</sup>/kg
11 disp('By comparing with the values given in the
      table, this state is seen to be in the superheated
       vapor region.temperature will be calculated
      using the method of interplotation.')
T = ((400-300)*(1.0-0.8753))/(1.0315-0.8753)+300
      temperature of the water
```

Scilab code Exa 3.4 Percentage of vapor

```
//example 4
//percentage of vapor
clear
clc
vliq=0.1 //volume of saturated liquid in m^3
vf=0.000843 //in m^3/kg
vvap=0.9 //volume of saturated vapor R-134a in equilbrium
vg=0.02671 //in m^3/kg
mliq=vliq/vf //mass of liquid in kg
mvap=vvap/vg //mass of vapor in kg
m=mliq+mvap //total mass in kg
x=mvap/m //percentage of vapor on mass basis
disp('hence,% vapor on mass basis is 22.1')
```

Scilab code Exa 3.5 Calculating pressure after heat addition

```
//example 5
//calculating pressure after heat addition
clear
clc
v1=0.14922 //specific volume of sautrated ammonia in m^3/kg
disp('Since the volume does not change during the process, the specific volume remains constant. therefore, ')
v2=v1 //in m^3/kg
disp('Since vg at 40C is less than v2, it is evident that in the final state the Ammonia is superheated vapor.By interplotation, we find that ')
P2=945 //final pressure in kPa
disp('hence, the final pressure is 945 kPa')
```

Scilab code Exa 3.6 Determining the missing property

```
1 //example 6
2 // Determining the missing property
3 clear
4 clc
5 T1=273-53.2 //given temperature in K
6 P1=600 //given pressure in kPa
7 disp('This temperature is higher than the critical
      temperature (critical temp. at P=600 kPa) is
      96.37 K. Hence, v = 0.10788 \text{ m}^3/\text{kg}')
8 T2=100 //given temp. in K
9 v2=0.008 //given specific volume in m<sup>3</sup>/kg
10 vf = 0.001452 //in m^3/kg
11 vg = 0.0312 //in m^3/kg
12 Psat=779.2 //saturation pressure in kPa
13 vfg=vg-vf //in m^3/kg
14 x=(v2-vf)/vfg //quality
15 printf("\n hence, the pressure is Psat = \%.1 f kPa.\
     n", Psat)
16 printf("\n and quality is x = \%.4 f . \n",x)
```

Scilab code Exa 3.7 Determining the pressure of water

```
1 //example 7
2 //determining the pressure of water
3 clear
4 clc
5 vg=0.12736 //specific volume in m^3/kg for water at 200C
6 v=0.4 //specific volume in m^3/kg
7 P1=500 //in kPa
```

Scilab code Exa 3.8 Calculating mass of air

```
//example 8
//calculating mass of air
clear

clc
F=100 //pressure in kPa
V=6*10*4 //volume of room in m^3
R=0.287 //in kN-m/kg-K
T=25 //temperature in Celsius
m=P*V/(R*(T+273.2)) //mass of air contained in room
printf("\n hence, mass of air contained in room is m
= %.3 f kg. \n",m)
```

Scilab code Exa 3.9 Calculating pressure inside tank

```
1 //example 9
2 //calculating pressure inside tank
3 clear
4 clc
5 V=0.5 //volumr of tank in m^3
6 m=10 //mass of ideal gas in kg
7 T=25 //temperature of tank in Celsius
8 M=24 //molecular mass of gas in kg/kmol
9 Ru=8.3145 //universal gas constant in kN-m/kmol-K
```

```
10 R=Ru/M //gas constant for given ideal gas in kN-m/kg
    -K
11 P=m*R*(T+273.2)/V //pressure inside tank
12 printf("\n hence, pressure inside tank is P = %.0f
    kPa. \n",P)
```

Scilab code Exa 3.10 Mass flow rate

```
1 //example 10
2 //mass flow rate
3 clear
4 clc
5 dt=185 //time period in seconds over which there is incrrease in volume
6 dV=0.75 //increase in volume in 0.75 in m^3
7 V=dV/dt //volume flow rate in m^3/s
8 P=105 //pressure inside gas bell kPa
9 T=21 //temperature in celsius
10 R=0.1889 //ideal gas constant in kJ/kg-K
11 m=P*V/(R*(T+273.15)) //mass flow rate of the flow in kg/s
12 printf("\n hence, mass flow rate is m = %.3 f kg/s. \n ",m)
13 printf("\n and volume flow rate is V = %.3 f m^3/s. \n",V)
```

Scilab code Exa 3.11 Predicting the nature of given state

```
1 //example 11
2 //predicting the nature of given state
3 clear
4 clc
```

- 5 disp('For Nitrogn, the critical properties are 126.2 K, 3.39 MPa. Given T=20+273.2 K, P=1.0 MPa. Since, given temperature is more than twice Tc and the reduced pressure is less than 0.3, ideal gas behaviour is a very good assumption.')
- 6 disp('For Carbon Dioxide, the critical properties are $304.1~\mathrm{K}, 7.38~\mathrm{MPa}$. Given $T=20+273.2~\mathrm{K},~\mathrm{P}=1.0~\mathrm{MPa}$ Therefore, reduced properties are $0.96(\mathrm{T/Tc})$ and $0.136~(\mathrm{P/Pc})$. CO2 is a gas with a Z of about 0.95, os the ideal gas is accurate to within about 5% in this case.')
- 7 disp('Given P=1.0MPa, T=20+273.2 K. For Ammonia, at T=293.2 K, Pg=858 kPa. Since, P>Pg, this state is compressible liquid and not a gas.')

Scilab code Exa 3.12 Determining specific using different laws

```
1 // example 12
2 //determining specific using differet laws
3 clear
4 clc
5 T=100 //given temp.in 100 celsius
6 P=3 //given pressure in MPa
7 v1=0.0065 //specific volume in m^3/kg using table
8 printf("\n hence, the specific volume for R-134a
      using R-134a tables is v1 = \%.3 \, f \, m^3/kg. \, n, v1)
9 M=102.3 //molecular mass in kg
10 R=8.3145 //in kJ/K
11 Ru=R/M //in kJ/K-kg
12 v2=Ru*(T+273)/(P*1000) //specific volume assuming R
      -134a to be ideal gas in m<sup>3</sup>/kg
13 printf("\n hence, the specific volume for R-134a
      using R-134a the ideal gas laws is v2 = \%.3 \, f \, m^3/
      kg. \ \ n", v2)
14 Tr=373.2/374.2 //reduced temperature using
```

```
generalized chart

15 Pr=3/4.06 //reduced pressure using generalized chart

16 Z=0.67 //compressibility factor

17 v3=Z*v2 // specific volume using generalized chart
    in m^3/kg

18 printf("\n hence, the specific volume for R-134a
    using the generalized chart is v3 = %.3f m^3/kg.
    \n",v3)
```

Scilab code Exa 3.13 Calculating mass of gas

```
1 // \text{example } 13
2 //calculating mass of gas
3 clear
4 clc
5 Pc=4250 //critical pressure of propane in kPa
6 Tc=369.8 //critical temperature in K
7 T=15 //temperature of propane in celsius
8 Tr=T/Tc //reduced temperature
9 Prsat=0.2 // reduced pressure
10 P=Prsat*Pc //pressure in kPa
11 x=0.1 //given quality
12 \text{ Zf} = 0.035 //\text{from graph}
13 Zg=0.83 //from graph
14 Z=(1-x)*Zf+x*Zg //overall compressibility factor
15 V=0.1 //volume of steel bottle in m<sup>3</sup>
16 R=0.1887 // \text{in } \text{kPa-m}^3/\text{kg-K}
17 m=P*V/(Z*R*(T+273)) //total propane mass in kg
18 printf ("\n hence, the total propane mass is m = \%.3 f
      kg. \ \ n", m)
19 printf("\n and pressure is P = \%.3 f \text{ kPa. } \text{\n",P})
```

Chapter 4

Energy Transfers

Scilab code Exa 4.1 Work done during different processes

```
1 //example 1
2 //work done during different processes
3 clear
4 clc
5 P1=200 //initial pressure inside cylinder in kPa
6 V2=0.1 //in m^3
7 V1=0.04 //initial volume of gas in m<sup>3</sup>
8 W1=P1*(V2-V1) //work done in isobaric process in kJ
9 printf("\n hence, the work done during the isobaric
      process is W1 = \%.3 f \text{ kJ. } \text{n}", W1)
10 W2=P1*V1*log(V2/V1) //work done in isothermal
      process in kJ
11 printf("\n hence, the work done in isothermal process
       is W2 = \%.3 f kJ. \n", W2)
12 P2=P1*(V1/V2)^(1.3) //final pressure according to
      the given process
13 W3 = (P2 * V2 - P1 * V1) / (1 - 1.3)
14 printf("\n hence, the work done during the described
      process is W3 = \%.3 f \text{ kJ. } \text{n", W3}
15 W4=0 //work done in isovolumic process
16 printf("\n hence, the work done in the isovolumic
```

Scilab code Exa 4.3 work produced

```
1 //example 3
2 //work produced
3 clear
4 clc
5 Psat=190.2 //in kPa
6 P1=Psat //saturation pressure in state 1
7 vf=0.001504 //in m^3/kg
8 vfg=0.62184 //in m^3/kg
9 x1=0.25 //quality
10 v1=vf+x1*vfg //specific volume at state 1 in m^3/kg
11 v2=1.41*v1 //specific volume at state 2 in m^3/kg
12 P2=600 //pressure in state 2 in kPa
13 m=0.5 //mass of ammonia in kg
14 W=m*(P1+P2)*(v2-v1)/2 //woork produced by ammonia in kJ
15 disp('hence, work produced by ammonia is 12.71 kJ')
```

Scilab code Exa 4.4 Calculating work done

```
1 //example 4
2 //calculating work done
3 clear
4 clc
5 v1=0.35411 //specific volume at state 1 in m^3/kg
6 v2=v1/2
7 m=0.1 //mass of water in kg
8 P1=1000 //pressure inside cylinder in kPa
9 W=m*P1*(v2-v1) //in kJ
```

10 disp('hence, the work in the overall process is -17.7 kJ')

Scilab code Exa 4.7 Heat transfer

```
1 //example 7
2 //heat transfer
3 clear
4 clc
5 k=1.4 //conductivity of glass pane in W/m-K
6 A=0.5 //total surface area of glass pane
7 dx=0.005 //thickness of glasspane in m
8 dT1=20-12.1 //temperature difference between room
      air and outer glass surface temperature in
      celsius
9 Q=-k*A*dT1/dx //conduction through glass slab in W
10 h=100 //convective heat transfer coefficient in W/m
     ^2-K
11 dT=12.1-(-10) //temperature difference between warm
      room and colder ambient in celsius
12 Q2=h*A*dT //heat transfer in convective layer in W
13 printf("\n hence, the rate of heat transfer in the
      glass and convective layer is Q2 = \%.0 \, f \, kW. \, n,
     Q2)
```

Chapter 5

Energy Equation for a Control Mass

Scilab code Exa 5.1 Calculating height

```
//example 1
//calculating height
clear
clc
m=1100 //mass of car in kg
ke=400 //kinetic energy of car in kJ
V=(2*ke*1000/m)^0.5 //velocity of car in m/s
g=9.807 //acc. due to gravity in m/s^2
H=ke*1000/(m*g) //height to which the car should be lifted so that its potential energy equals its kinetic energy
disp('hence, the car should be raised to a height of 37.1 m to make its potential energy equal to kinetic energy')
```

Scilab code Exa 5.2 Change in internal energy

```
//example 2
//change in internal energy
clear
clc
W=-5090 //work input to paddle wheel in kJ
Q=-1500 //heat transfer from tank in kJ
dU=Q-W //change in internal energy in kJ
disp('hence, change in internal energy is 3590 kJ')
```

Scilab code Exa 5.3 Analysis of energy transfer

```
1 // \text{example } 3
2 //analysis of energy transfer
3 clear
4 clc
5 g=9.806 // acceleration due to gravity in m/s<sup>2</sup>
6 \text{ m=10} //\text{mass of stone in kg}
7 H1=10.2 //initial height of stone above water in
      metres
8 H2=0 //final height in metres
9 dKE1=-m*g*(H2-H1) //change in kinetic energy when
      stone enters state 2 in J
10 dPE1=-1 //change in potential energy when stone
      enters state 2 in J
11 printf("\n hence, when stone is about to enter state
      2, dKE = \%.3 \, f J. \n", dKE1)
12 printf("\n and dPE = \%.3 \, f J. \n", dPE1)
13 dPE2=0 //change in potential energy when stone
      enters state 3 in JQ2=0 //no heat transfer when
      stone enters state 3 in J
14 W2=0 //no work done when stone enters state 3 in J
15 dKE2=-1 //change in kinetic energy when stone enters
       state 3
16 dU2=-dKE2 //change in internal energy when stone
      enters state 3 in J
```

Scilab code Exa 5.4 Determining the missing properties

```
1 //example 4
2 //Determining the missing properties
3 clear
4 clc
5 T1=300 //given temp. in Celsius
6 u1=2780 //given specific internal enrgy in kJ/kg
7 disp ('From steam table, at T=300 \text{ C}, ug=2563.0 \text{ kJ/kg}.
      So, u1>ug, it means the state is in the
      superheated vapor region. So, by interplotation, we
       find P=1648 kPa and v=0.1542 m<sup>3</sup>/kg')
8 P2=2000 //hiven pressure in kPa
9 u2=2000 //given specific intrernal energy in kJ/kg
10 disp('at P=2000 kPa,')
11 uf = 906.4 //in kJ/kg
12 ug=2600.3 //in kJ/kg
13 x2=(u2-906.4)/(ug-uf)
```

```
disp('Also, under the given conditions')
vf=0.001177 //in m^3/kg
vg=0.099627 //in m^3/kg
v2=vf+x2*(vg-vf)//Specific volume for water in m^3/kg
printf("\n hence, specific volume for water is v2 = %.5 f m^3/kg. \n",v2)
printf("\n Therefore, this state is in the two phase region with quality x2=%.4 f. \n",x2)
```

Scilab code Exa 5.5 Calculating heat transfer for the given process

```
1 // example 5
2 //calculating heat transfer for the given process
3 clear
4 clc
5 Vliq=0.05 //volume of saturated liquid in m<sup>3</sup>
6 vf=0.001043 //in m^3/kg
7 Vvap=4.95 //volume of saturated water vapour in m<sup>3</sup>
8 \text{ vg} = 1.6940 //\text{in m}^3/\text{kg}
9 m1liq=Vliq/vf //mass of liquid in kg
10 mlvap=Vvap/vg //mass of vapors in kg
11 ulliq=417.36 //specific internal energy of liquid in
       kJ/kg
12 ulvap=2506.1 //specific internal energy of vapors in
       kJ/kg
13 U1=m1liq*u1liq+m1vap*u1vap //total internal energy
14 m=m1liq+m1vap //total mass in kg
15 V=5 //total volume in m<sup>3</sup>
16 v2=V/m //final specific volume in m<sup>3</sup>/kg
17 disp('by interplotation we find that for steam, if
      vg = 0.09831 \text{ m}^3/\text{kg} then pressure is 2.03 MPa')
18 u2=2600.5 //specific internal energy at final state
      in kJ/kg
```

```
19 U2=m*u2 //internal energy at final state in kJ
20 Q=U2-U1 //heat transfer for the process in kJ
21 printf("\n hence, heat transfer for the process is Q
= %.0 f kJ. \n",Q)
```

Scilab code Exa 5.6 Calculating work and heat transfer for the process

```
1 //example 6
2 //calculating work and heat transfer for the process
3 clear
4 clc
5 V1=0.1 //volume of cylinder in m<sup>3</sup>
6 m=0.5 //mass of steam in kg
7 v1=V1/m //specific volume of steam in m<sup>3</sup>/kg
8 vf=0.001084 //\text{m}^3/\text{kg}
9 vfg=0.4614 //\text{m}^3/\text{kg}
10 x1=(v1-vf)/vfg //quality
11 hf = 604.74 / kJ/kg
12 hfg=2133.8//kJ/kg
13 h2=3066.8 //final specific heat enthalpy in kJ/kg
14 h1=hf+x1*hfg //initial specific enthalpy in kJ/kg
15 Q=m*(h2-h1) //heat transfer for this process in kJ
16 P=400 //pressure inside cylinder in kPa
17 v2=0.6548 // specific enthalpy in m<sup>3</sup>/kg
18 W=m*P*(v2-v1) //work done for the process in kJ
19 printf("\n hence, work done for the process, W = \%.3
      f kJ. \langle n'', W \rangle
20 printf("\n and heat transfer, Q=\%.3 f kJ.\n",Q)
```

Scilab code Exa 5.8 Calculating change in enthalpy

```
1 //example 82 //calculating change in enthalpy
```

```
3 clear
4 clc
5 h1=273.2 //specific heat enthalpy for oxygen at 300
6 h2=1540.2 //specific heat enthalpy for oxygen at
7 T1=300 //initial temperature in K
8 T2=1500 //final temparature in K
9 x=poly([0], 'x');
10 Cp=0.88-0.00001*x+0.54*x^2-0.33*x^3 // expression for
      constant pressure specific heat enthalpy for
     oxygen
11 dh1=h2-h1 //this change in specific heat enthalpy is
      calculated using ideal gas tables
12 dh2=1000*integrate('0.88-0.00001*x+0.54*x^2-0.33*x^3
      ', 'x', T1/1000, T2/1000) //using empirical equation
13 dh3=0.922*(T2-T1) //it is claculated if we assume
      specific heat enthalpy to be constant and uses
     its value at 300K
14 dh4=1.0767*(T2-T1) //it is claculated if we assume
      specific heat enthalpy to be constant and uses
     its value at 900K i.e mean of initial and final
     temperature
15 printf("\n Hence, change in specific heat enthalpy if
      ideal gas tables are used is dh1=\%.1 f kJ/kg. \n"
     , dh1)
16 printf("\n if empirical equations are used, dh2=\%.1f
      kJ/kg. \n", dh2)
17 printf("\n if specific heat is assumed to be
     constant and using its value at T1, dh3=\%.1 f kJ/
     kg. \ n, dh3)
18 printf("\n if specific heat is assumed to be
     constant at its value at (T1+T2)/2, dh4=\%.1 f kJ/
```

Scilab code Exa 5.9 Determining amount of heat transfer

```
1 //example 9
2 //determining amount of heat transfer
3 clear
4 clc
5 P=150 //pressure of nitrogen in cylinder in kPa
6 V=0.1 //initial volume of cylinder in m<sup>3</sup>
7 T1=25 //initial temperature of nitrogen in celsius
8 T2=150 //final tempareture of nitrogen in celsius
9 R=0.2968 //in kJ/kg-K
10 m=P*V/(R*(T1+273)) //mass of nitrogen in kg
11 Cv=0.745 //constant volume specific heat for
      nitrogen in kJ/kg-K
12 W=-20 //work done on nitrogen gas in kJ
13 Q=m*Cv*(T2-T1)+W //heat transfer during the process
     in kJ
14 printf("\n hence, the heat transfer for the above
     process is Q=\%.1 f kJ. \n", Q)
```

Scilab code Exa 5.10 Calculating rate of increase of internal energy

```
//example 10
//calculating rate of increase of internal energy
clear

clc
W=-12.8*20 //power consumed in J/s
Q=-10 //heat transfer rate from battery in J/s
r=Q-W //rate of increase of internal energy
printf("\n hence, the rate of increase of internal energy is r=%.0 f J/s. \n", r)
```

Scilab code Exa 5.11 Rate of change of temperature

```
1 // example 11
2 //rate of change of temperature
3 clear
4 clc
5 Q=1500 //power produced by burning wood in J/s
6 mair=1 //mass of air in kg
7 mwood=5 //mass of soft pine wood in kg
8 miron=25 //mass of cast iron in kg
9 Cvair=0.717 //constant volume specific heat for air
     in kJ/kg
10 Cwood=1.38 //constant volume specific heat for wood
     in kJ/kg
11 Ciron=0.42 //constant volume specific heat for iron
     in kJ/kg
12 dT=75-20 //increase in temperature in Celsius
13 T=(Q/1000)/(mair*Cvair+mwood*Cwood+miron*Ciron) //
     rate of change of temperature in K/s
14 dt = (dT/T)/60 //in minutes
15 printf ("hence, the rate of change of temperature is
     dt=\%.4 f K/s.\n", T)
16 printf(" and time taken to reach a temperature of T=
     \%.0 f min.\n", dt)
```

Chapter 6

Energy Equation for a Control Volume

Scilab code Exa 6.1 Calculating mass flow rate

```
//example 1
//calculating mass flow rate in kg/s
clear
clc
R=0.287 //in kJ/kg-K
T=25 //temperature in celsius
P=150 //pressure in kPa
v=R*(T+273.2)/P //specific volume in m^3/kg
D=0.2 //diameter of pipe in metre
A=%pi*D^2/4 //cross sectional area in m^2
V=0.1 //velocity of air in m/s
m=V*A/v //mass flow rate in kg/s
printf("\n hence, the mass flow rate is m=%.4 f kg/s.\n",m)
```

Scilab code Exa 6.2 Work done for adding the fluid

```
//example 2
//work done for adding the fluid
clear
clc
P=600 //pressure in kPa
m=1 //in kg
v=0.001 //specific volume in m^3/kg
W=P*m*v //necessary work in kJ for adding the fluid
printf(" \n hence, the work involved in this process is W=%.3 f kJ. \n", W)
```

Scilab code Exa 6.3 Rate of flow of water

```
1 //example 3
2 //rate of flow of water
3 clear
4 clc
5 hir=441.89 //in kJ/kg for refrigerant using steam
     table
6 her=249.10 //in kJ/kg for refrigerant using steam
     table
7 hiw=42 //in kJ/kg for water using steam table
8 hew=83.95 //in kJ/kg for water using steam table
9 mr=0.2 //the rate at which refrigerant enters the
     condenser in kg/s
10 mw=mr*(hir-her)/(hew-hiw) //rate of flow of water in
      kg/s
11 printf("\n hence, the rate at which cooling water
     flows thorugh the condenser is mw=\%.3 f kg/s. \n",
      mw)
```

Scilab code Exa 6.4 Determining quality of steam

Scilab code Exa 6.5 Quality of ammonia leaving expansion valve

```
//example 5
//quality of ammonia leaving expansion valve
clear
clc
hi=346.8 //specific heat enthalpy for ammonia at initial state in kJ/kg
he=hi //specific heat enthalpy for ammonia at final state will be equal that at initial state because it is a throttling process
hf=134.4 //at final state in kJ/kg
hfg=1296.4//at final state in kJ/kg
se=(he-hf)/hfg //quality at final state
printf("\n hence, quality of the ammonia leaving the expansion valve is xe=%.4f. \n",xe')
```

Scilab code Exa 6.6 Power output of turbine in kW

```
1 //example 6
2 //power output of turbine in kW
3 clear
4 clc
5 hi=3137 //initial specific heat of enthalpy in kJ/kg
6 he=2675.5 //final specific heat of enthalpy in kJ/kg
7 Vi=50 //initial velocity of steam in m/s
8 Ve=100 //final velocity of steam in m/s
9 Zi=6 //height of inlet conditions in metres
10 Ze=3 //height of exit conditions in metres
11 m=1.5 //mass flow rate of steam in kg/s
12 g=9.8066 //acc. due to gravity in m/s<sup>2</sup>
13 Qcv=-8.5 //heat transfer rate from turbine in kW
14 \text{ Wcv} = \text{Qcv} + \text{m} * (\text{hi} + \text{Vi}^2 / (2*1000) + \text{g} * \text{Zi} / 1000) - \text{m} * (\text{he} + \text{Ve})
      ^2/(2*1000)+g*Ze/1000) //power output of turbine
15 printf("\n hence, the power output of the turbine is
      Wcv=\%.3 f kW. \ n", Wcv)
```

Scilab code Exa 6.7 Heat transfer rate in aftercooler

```
1 //example 7
2 //heat transfer rate in aftercooler
3 clear
4 clc
5 V1=0 //we assume initial velocity to be zero because its given that it enters with a low velocity
6 V2=25 //final velocity with which carbon dioxide exits in m/s
7 h2=401.52 //final specific enthalpy of heat when carbon dioxide exits in kJ/kg
8 h1=198 //initial specific enthalpy of heat in kJ/kg
9 w=h1-h2-V2^2/(2*1000) //in kJ/kg
10 Wc=-50 //power input to the compressor in kW
11 m=Wc/w //mass flow rate of carbon dioxide in kg/s
```

Scilab code Exa 6.8 Required Pump work

```
//example 8
//Required pump work
clear
clc
m=1.5 //mass flow rate of water in kg/s
g=9.807 //acceleration due to gravity in m/s^2
Zin=-15 //depth of water pump in well in metres
Zex=0 //in metres
v=0.001001 //specific volume in m^3/kg
Pex=400+101.3 //exit pressure in kPa
Pin=90 //in kPa
W=m*(g*(Zin-Zex)*0.001-(Pex-Pin)*v) //power input in kW
printf(" \n Hence, the pump requires power input of W=%.0 f W. \n", W*1000)
```

Scilab code Exa 6.9 Heat transfer in simple steam power plant

```
1 //example 9
2 //heat tranfer in simple steam power plant
3 clear
4 clc
```

```
5 h1=3023.5 //specific heat of enthalpy of steam
     leaving boiler in kJ/kg
6 h2=3002.5 //specific heat of enthalpy of steam
     entering turbine in kJ/kg
7 x=0.9 //quality of steam entering condenser
8 hf = 226 //in kJ/kg
9 hfg=2373.1 //in kJ/kg
10 h3=hf+x*hfg //specific heat of enthalpy of steam
     entering condenser in kJ/kg
11 h4=188.5 //specific heat of enthalpy of steam
     entering pump in kJ/kg
12 q12=h2-h1 //heat transfer in line between boiler and
      turbine in kJ/kg
13 w23=h2-h3 // turbine work in kJ/kg
14 q34=h4-h3 //heat transfer in condenser
15 w45=-4 //pump work in kJ/kg
16 h5=h4-w45 //in kJ/kg
17 q51=h1-h5 //heat transfer in boiler in kJ/kg
18 printf("\n hence, heat transfer in line between
      boiler and turbine is q12=\%.1 \text{ f kJ/kg. } \text{n",q12'}
19 printf("\n hence, turbine work is w23=\%.1 f kJ/kg. \n
     ",w23')
20 printf("\n hence, heat transfer in condenser is q34=
     21 printf("\n hence, heat transfer in boiler is q51=\%.0
     f kJ/kg. \ n",q51')
```

Scilab code Exa 6.10 Analysis of refrigerator

```
1 //example 10
2 //analysis of refrigerator
3 clear
4 clc
5 hf4=167.4 //in kJ/kg
6 hfg4=215.6 //in kJ/kg
```

```
7 h3=241.8 //specific heat of enthalpy of R-134a
     entering expansion valve
8 h4=h3 //specific heat of enthalpy of R-134a leaving
     expansion valve
9 h1=387.2 //in kJ/kg
10 h2=435.1 //in kJ/kg
11 x4=(h3-hf4)/hfg4 //quality of R-134a at evaporator
      inlet
12 m=0.1 //mass flow rate in kg/s
13 Qevap=m*(h1-h4) //rate of heat transfer to the
      evaporator
14 Wcomp=-5 //power input to compressor in kW
15 Qcomp=m*(h2-h1)+Wcomp //rate of heat transfer from
      compressor
16 printf("\n hence, the quality at the evaporator
      inlet is x4=\%.3 f. \n", x4')
17 printf("\n hence, the rate of heat transfer to the
      evaporator is Qevap=\%.2 f kW. \n", Qevap')
18 printf("\n hence, rate of heat transfer from the
      compressor is Qcomp=\%.2 f kW. \n", Qcomp')
```

Scilab code Exa 6.11 Determining the final temperature of steam

```
//example 11
//Determining the final temperature of steam
clear

clc
u2=3040.4 //final internal energy in kJ/kg
hi=u2 //in kJ/kg
P2=1.4 //final Pressure in MPa
disp('Since, the final pressure is given as 1.4 MPa, we know two properties at the final state and hence, final state can be determined. The temperature corresponding to a pressure of 1.4 MPa and an internal energy of 3040.4 kJ/kg is
```

```
found to be ')
9 T2=452 //final temperature in Celsius
```

Scilab code Exa 6.12 Calculating mass flow of steam in tank

```
1 // example 12
2 // Calculating mass flow of steam in tank
3 clear
4 clc
5 V1=0.4 //initial volume fo tank in m<sup>3</sup>
6 v1=0.5243 //initial specific volume in m<sup>3</sup>/kg
7 h1=3040.4 //initial specific enthalpy in k\mathrm{J/kg}
8 u1=2548.9 //initial specific internal energy in kJ/
      kg
9 m1=V1/v1 //initial mass of steam in tank in kg
10 V2=0.4 //final volume in m<sup>3</sup>
11 disp('let x=V*(h1-u2)/v2-m1*(h1-u1). If we assume T2
      =300C, then v2=0.1823m^3/kg, u2=2785.2kJ/kg and x
     =+ve. If we assume T2=350C, then v2=0.2003 m<sup>3</sup>/kg,
      u2=2869.1kJ/kg and x=-ve. Hence, actualt T2 must be
       between these two assumed values in order that x
      =0.By interplotation,')
12 T2=342 //final temperature in Celsius
13 v2=0.1974 //final specific volume in m<sup>3</sup>/kg
14 m2=V2/v2 //final mass of the steam in the tank in kg
15 m=m2-m1 //mass of steam that flowsinto the tank
16 printf(" \n Hence, mass of the steam that flows into
      the tank is m=\%.3 f \text{ kg. } n, m)
```

Scilab code Exa 6.13 Calculating mass flow of steam in tank

```
1 //example 132 //Calculating mass flow of steam in tank
```

```
3 clear
4 clc
5 vf1=0.001725 //in m^3/kg
6 vf2=0.0016 //in m^3/kg
7 uf1=368.7 //in kJ/kg
8 uf2=226 //in kJ/kg
9 vg1=0.08313 //in m^3/kg
10 \text{ vfg}2=0.20381
11 ug1=1341 //in kJ/kg
12 ufg2=1099.7 //in kJ/kg
13 Vf=1 //initial volume of liquid in m<sup>3</sup>
14 Vg=1 //initial volume of vapor in m<sup>3</sup>
15 mf1=Vf/vf1 //initial mass of liquid in kg
16 mg1=Vg/vg1 //initial mass of vapor in kg
17 m1=mf1+mg1 //initial mass of liquid in kg
18 he=1461.1 //in kJ/kg
19 V=2 //volume of tank in m<sup>3</sup>
20 disp('m1u1=mf1*uf1+mg1*ug1.If x2 is the quality, then
       m2=V/v2=2/(0.00160+0.20381*x2) and u2=uf2+x2*
      ufg2 = 226.0 + 1099.7 * x2.
21 disp('Also, m2*(he-u2)=m1*he-m1u1.From this equation,
      we will get an equation for x2.')
22 	ext{ x2=((2*1461.1) - (2*226) - (0.00160*634706))}
      /((634706*0.20381)+(2*1099.7)) //quality of
      ammonia
23 v2=0.00160+(0.20381*x2) //final specific volume in m
      ^3/\mathrm{kg}
24 m2=V/v2 //final mass of ammonia in kg
25 m=m1-m2 //mass of ammonia withdrawn
26 printf("\n Hence, mass of ammonia withdrawn is m=\%.1
      f kg. \langle n'', m \rangle
```

Chapter 7

The Classical Second Law of Thermodynamics

Scilab code Exa 7.1 Rate of fuel consumption

```
//example 1
//rate of fuel consumption
clear
clc
W=136*0.7355 //output of automobile engine in kW
neng=0.3 //thermal efficiency of automobile engine
Ph=W/neng //energy output of fuel in kW
Ql=Qh-W //total rate of energy rejected to the ambient
qh=35000 //energy output of fuel in kJ/kg
m=Qh/qh //rate of fuel consumption in kg/s
printf("\n hence, total rate of energy rejected is Ql=%.0f kW.\n",Ql)
printf("\n and rate of fuel consumption is m=%.4f kg/s.\n",m)
```

Scilab code Exa 7.2 Coefficient of performance of refrigerator

```
//example 2
//coefficient of performance of refrigerator
clear
clc
M=400 //heat rejected to kitchen air in W
W=150 //electrical input power in W
Ql=Qh-W //rate of energy taken out to cold space in W
B=Ql/W //coefficient of performance of refrigerator
printf("\n hence, rate of energy taken out of the cold space is Ql=%.3 f W.\n",Ql)
printf("\n and coefficient of performance of the refrigerator is B=%.3 f .\n",B)
```

Scilab code Exa 7.4 Comparison of ideal carnot heat engine with actual heat engine

```
1 //example 4
2 //comparison of ideal carnot heat engine with actual
      heat engine
3 clear
4 clc
5 Qh=1000 //rate of heat transfer to heat engine in kW
6 W=450 //rate of production of work in kW
7 Ql=Qh-W //rate of heat rejected by heat engine in kW
8 nthermal=W/Qh //efficiency from the definition of
     efficiency
9 T1=300 //temperature of surroundings in K
10 Th=550 //temperature of heat source in Celsius
11 ncarnot=1-Tl/(Th+273) // efficiency if heat engine is
      considered to be ideal carnot heat engine
12 W2=ncarnot*Qh //rate of work production if heat
     engine is assumed to be ideal carnot heat engine
```

```
in kW

13 Q12=Qh-W2 //rate of heat rejected by heat engine in
    kW if heat engine is assumed to be ideal carnot
    heat engine

14 printf("\n hence, energy discarded to the ambient
    surroundings is Q12=%.0fkW.\n",Q12)

15 printf("\n and the engine efficiency is ncarnot=%.3f
    .\n",ncarnot)
```

Scilab code Exa 7.5 Calculating required work

```
//example 5
//calculating required work
clear
clc
T1=24+273 //room temperature in Kelvins
Th=35+273 //atmospheric temperature in Kelvins
Q1=4 //rate of heat rejection from room
B=T1/(Th-T1) //coefficient of performance of air conditioner
W=Q1/B //required work in kW
printf("\n hence, the magnitude of required work is W=%.2 f kW.\n", W)
```

Chapter 8

Entropy for a Control Mass

Scilab code Exa 8.1 Coefficient of performance of refrigerator

```
1 // example 1
2 // coefficient of performance of refrigerator
3 clear
4 clc
5 Th=60 //temperature at which heat is rejected from R
     -134a
6 T1=0 //temperature at which heat is absorbed into
     the R-134a
7 s1=1.7262 //specific entropy at 0 Celsius
8 s2=s1 //process of state change from 1-2 is
     isentropic
9 s3=1.2857 //specific entropy at 60 celsius
10 s4=s3 //process of state change from 3-4 is
     isentropic
11 disp('if Pressure is 1400 kPa, then s=1.7360 \text{ kJ/kg-K}
     and if P=1600 \text{ kPa}, then s=1.7135 \text{ kJ/kg-K}. Therefore
12 P2=1400+(1600-1400)*(1.7262-1.736)/(1.7135-1.736)
     pressure after compression in kPa
13 B=(Th+273)/(Th-T1) // coefficient of performance of
      refrigerator
```

Scilab code Exa 8.2 Heat transfer in a given process

```
1 // example 2
2 //heat transfer in a given process
3 clear
4 clc
5 u1=87.94 // specific internal energy of R-12 at state
      1 in kJ/kg
6 u2=276.44 //specific internal energy of R-12 at
      state 2 in kJ/kg
7 s1=0.3357 //specific entropy at state 1 in kJ/kg-K
8 s2=1.2108 //specific entropy at state 2 in kJ/kg-K
9 V=0.001 //volume of saturated liquid in m<sup>3</sup>
10 v1=0.000923 //specific volume in m^3/kg
11 m=V/v1 //mass of saturated liquid in kg
12 T=20 //temperature of liquid in celsius
13 Q12=m*(T+273.15)*(s2-s1) //heat transfer in kJ to
      accomplish the process
14 W12=m*(u1-u2)+Q12 //work required to accomplish the
      process
15 printf("\n hence, work required to accomplish the
      process is W12=\%.1 \, \text{f kJ.} \, \text{n}", W12)
16 printf(" \n and heat transfer is Q12=\%.1 f kJ.\n",Q12
      )
```

Scilab code Exa 8.3 Entropy change

```
1 //example 3
```

```
//entropy change
clear
clc
C=4.184 // specific heat of water in kJ/kg-K
T1=20 //initial temperature of water in celsius
T2=90 //final temperature of water in celsius
dS1=C*log((T2+273.2)/(T1+273.2)) //change in entropy in kJ/kg-K
gdS2=1.1925-0.2966 //in kJ/kg-K using steam tables
printf("\n hence,change in entropy assuming constant specific heat is dS1=%.4f kJ/kg-K.\n",dS1)
printf("\n using steam table is dS2=%.4f kJ/kg-K.\n",dS2)
```

Scilab code Exa 8.4 Entropy change with different assumptions

```
1 //example 4
2 //entropy change with different assumptions
3 clear
4 clc
5 T1=300 //initial temperature in kelvins
6 T2=1500 //final temperature in kelvins
7 P1=200 //initial pressure in kPa
8 P2=150 //final pressure in kPa
9 R=0.2598 // in kJ/kg-K
10 Cp=0.922 // specific heat in kJ/kg-K at constant
     pressure
11 dsT2=8.0649 //in kJ/kg-K
12 dsT1=6.4168 //in kJ/kg-K
13 dS1=dsT2-dsT1-R*log(P2/P1) //entropy change
     calculated using ideal gas tables
14 dS2=integrate('0.88/x-0.0001+0.54*x-0.33*x^2', 'x')
      ,0.3,1.5) -R*log(P2/P1) //entropy change
      calculated using empirical equation
15 dS3=Cp*log(T2/T1)-R*log(P2/P1) //entropy change
```

```
assuming constant specific heat in kJ/kg-K

16 dS4=1.0767*log(T2/T1)+0.0747 //entropy change
    assuming specific heat is constant at its value
    at 990K

17 printf("\n hence, change in entropy using ideal gas
    tables is dS1=%.4f kJ/kg-K.\n",dS1)

18 printf("\n hence, change in entropy using empirical
    equation is dS2=%.4f kJ/kg-K.\n",dS2)

19 printf("\n hence, change in entropy using the value
    of specific heat at 300K is dS3=%.4f kJ/kg-K.\n",
    dS3)

20 printf("\n hence, change in entropy assuming specific
    heat is constant at its value at 900K is dS4=%.4
    f kJ/kg-K.\n",dS4)
```

Scilab code Exa 8.5 Entropy change

```
1 //example 5
2 //entropy change
3 clear
4 clc
5 Cp=1.004 //specific heat at constant pressure in kJ/
     kg-K
6 R=0.287 //gas constant in kJ/kg-K
7 P1=400 //initial pressure in kPa
8 P2=300 //final pressure in kPa
9 T1=300 //initial temperature in K
10 T2=600 //final temperature in K
11 dS1=Cp*log(T2/T1)-R*log(P2/P1) //entropy change
     assuming constant specific heat
12 s1=6.8693 // specific entropy at T1
13 s2=7.5764 //specific entropy at T2
14 dS2=s2-s1-R*log(P2/P1) //entropy change assuming
     variable specific heat
15 printf("\n hence, entropy change assuming constant
```

```
specific heat is dS1=\%.4 \, f \, kJ/kg-K.\n", dS1)

16 printf("\n and assuming variable specific heat is dS2=\%.4 \, f \, kJ/kg-K.\n", dS2)
```

Scilab code Exa 8.6 Work done by air

```
1 //example 6
2 //work done by air
3 clear
4 clc
5 T1=600 //initial temperature of air in K
6 P1=400 //intial pressure of air in kPa
7 P2=150 //final pressure in kPa
8 u1=435.10 //specific internal energy at temperature
     T1 in kJ/kg
  sT1=7.5764 //specific entropy at temperature T1 in
     kJ/kg-K
10 R=0.287 //gas constant in kJ/kg-K
11 ds = 0
12 sT2=ds+sT1+R*log(P2/P1) //specific entropy at
      temperature T2 in kJ/kg-K
13 disp('we know the values of s and P for state 2.So,
     in order to fully determine the state, we will use
      steam table')
14 T2=457 //final temperature in K
15 u2=328.14 //specific internal energy at temperature
     T2 in kJ/kg
16 w=u1-u2 //work done by air in kJ/kg
17 printf("\n hence, work done by air is w=\%.2 \text{ f kJ/kg.} \setminus n
     ",w)
```

Scilab code Exa 8.7 Work and heat transfer

```
1 //example 7
2 //work and heat transfer
3 clear
4 clc
5 P2=500
          //final pressure in cylinder in kPa
6 P1=100 //initial pressure in cylinder in kPa
7 T1=20+273.2 //initial temperature inside cylinder in
       Kelvins
8 n = 1.3
9 T2=(T1)*(P2/P1)^((n-1)/n) //final temperature inside
       cylinder in K
10 R=0.2968 //gas constant in kJ/kg-K
11 w12=R*(T2-T1)/(1-n) //work in kJ/kg
12 Cvo=0.745 //specific heat at constant volume in kJ/
     kg-K
13 q12=Cvo*(T2-T1)+w12 //heat transfer in kJ/kg
14 printf(" \n hence, work done is w12=\%.1 f kJ/kg.\n",
15 printf("\n and heat transfer are q12=\%.1 \text{ f kJ/kg.} \cdot \text{n}",
```

Scilab code Exa 8.8 Calculating increase in entropy

```
//example 3
//calculating increase in entropy
clear
clc
m=1 //mass of saturated water vapour
sfg=6.0480 //in kJ/K
T=25 //temperature of surrounding air in celsius
clear
scheduler
for the strength of the surrounding air in celsius
for the strength of the surrounding air in celsius
for the strength of the surrounding air in celsius
for the strength of the surrounding air in celsius
for the strength of the surrounding air in celsius
for the strength of the surrounding air in celsius
for the strength of the strength of the strength of the surrounding air in celsius
for the strength of the strength
```

```
dSsurroundings=Qtosurroundings/(T+273.15) //in kJ/K
dSnet=dScm+dSsurroundings //net increase in entropy
        in kJ/K
printf(" hence, net increase in entropy of water plus
        surroundings is dSnet=%.4f kJ/K.\n",dSnet)
```

Scilab code Exa 8.9 Entropy generation

```
//example 9
//entropy generation
clear
clc
Qout=1 //value of heat flux generated by 1kW of
    electric power
T=600 //temperature of hot wire surface in K
Sgen=Qout/T //entropy generation in kW/K
printf(" \n hence, entropy generation is Sgen=%.5 f kW /K.\n",Sgen)
```

Scilab code Exa 8.10 Determining the entropy generated

```
//example 10
//Determining the entropy generated
clear
clc
B=4 //COP of air conditioner
W=10 //power input of air conditioner in kW
Qh=B*W //in kW
Ql=Qh-W //in kW
Thigh=323 //in Kelvin
Tlow=263 //in Kelvin
SgenHP=(Qh*1000/Thigh)-(Ql*1000/Tlow) //in W/K
Tl=281 // in K
```

```
13 Th=294 //in K
14 SgenCV1=Q1*1000/Tlow-Q1*1000/Tl //in W/K
15 SgenCV2=Qh*1000/Th-Qh*1000/Thigh //in W/K
16 SgenTOT=SgenCV1+SgenCV2+SgenHP //in W/K
17 printf(" \n Hence, Total entropy generated is SgenTOT
=%.1 f W/K. \n", SgenTOT)
```

Chapter 9

Entropy Equation for a Control Volume

Scilab code Exa 9.1 Entropy generation

```
1 // \text{example } 1
2 //work done by steam
3 clear
4 clc
5 hi=3051.2 //initial specific heat of enthalpy of
     steam in kJ/kg
6 si=7.1228 //initial specific entropy of steam in kJ/
     kg-K
7 Pe=0.15 //final pressure in MPa
8 se=si //specific entropy in final state in kJ/kg-K
9 sf=1.4335 //in kJ/kg-K
10 sfg=5.7897 //in kJ/kg-K
11 vi=50 //velocity with which steam enters turbine in
     m/s
12 ve=200 //velocity with which steam leaves the
     turbine in m/s
13 xe=(se-sf)/sfg //quality of steam in final state
14 hf = 467.1 / in kJ/kg
15 hfg=2226.5 //in kJ/kg
```

Scilab code Exa 9.2 Exit velocity of steam from nozzle

```
1 // example 2
2 //exit velocity of steam from nozzle
3 clear
4 clc
5 hi=3051.2 //initial specific heat of enthalpy in kJ/
6 si=7.1228 //initial specific entropy in kJ/kg-K
7 se=si //final specific entropy
8 Pe=0.3 //final pressure in MPa
9 disp ('from steam table, various properties at final
     state are ')
10 he=2780.2 //final specific heat of enthalpy in kJ/kg
11 Te=159.1 //final temperature in celsius
12 vi=30 //velocity with which steam enters the nozzle
     in m/s
13 ve = ((2*(hi-he)+(vi^2/1000))*1000)^0.5 //final
      velocity of steam with which it exits in m/s
14 printf("\n hence, exit velocity of the steam from the
      nozzle is ve=\%.0 \text{ f m/s.} n", ve)
```

Scilab code Exa 9.3 Violation of second law

```
1 //example 3
```

```
//violation of second law
clear
clc
sdisp('from R-134a tables')
se=1.7148 //specific entropy in final state in kJ/kg
-K
si=1.7395 //initial specific entropy in kJ/kg-K
disp('therefore, se<si, whereas for this process the second law requires that se>=si.The process described involves a violation of the second law and thus would be impossible.')
```

Scilab code Exa 9.4 Calculating required specific work

Scilab code Exa 9.5 Entropy generation

```
1 // example 5
```

```
2 //entropy generation
3 clear
4 clc
5 h1=2865.54 //specific heat of enthalpy at state 1 in
      kJ/kg
6 h2=83.94 //specific heat of enthalpy at state 2 in
     kJ/kg
7 h3=2725.3 //specific heat of enthalpy at state 3 in
     kJ?kg
8 s1=7.3115 //specific entropy at state 1 in kJ/kg-K
9 s2=0.2966 //specific entropy at state 2 in kJ/kg-K
10 s3=6.9918 //specific entropy at state 3in kJ/kg-K
11 m1=2 //mass flow rate at state 1 in kg/s
12 m2=m1*(h1-h3)/(h3-h2) //mass flow rate at state 2 in
      kg/s
13 m3=m1+m2 //mass flow rate at state 3 in kg/s
14 Sgen=m3*s3-m1*s1-m2*s2 //entropy generation in the
      process
15 printf("\n hence, entropy generated in this process
     is Sgen=\%.3 f \text{ kW/K.} \ \text{n", Sgen}
```

Scilab code Exa 9.6 Work required to fill the tank

```
//example 6
//work required to fill the tank
clear

clc
T1=17+273 //initial temperature of tank in Kelvins
ST1=6.83521 //specific entropy in kJ/kg-K
R=0.287 //gas constant in kJ/kg-K
P1=100 //initial pressure in kPa
P2=1000 //final pressure in kPa
ST2=sT1+R*log(P2/P1) //specific entropy at temperature T2 in kJ/kg-K
T2=555.7 //from interplotation
```

```
12 V1=0.04 //volume of tank in m^3
13 V2=V1 //final volume is equal to initial volume
14 m1=P1*V1/(R*T1) //initial mass of air in tank in kg
15 m2=P2*V2/(R*T2) //final mass of air in tank in kg
16 Min=m2-m1 //in kg
17 u1=207.19 //initial specific heat of enthalpy in kJ/kg
18 u2=401.49 //final specific heat of enthalpy in kJ/kg
19 hin=290.43 //in kJ/kg
20 W12=Min*hin+m1*u1-m2*u2 //work required to fill the tank in kJ
21 printf("\n hence, the total amount of work required to fill the tank in kJ
```

Scilab code Exa 9.7 Work required to pump water isentropically

```
//example 7
//work required to pump water isentropically
clear
clc
P1=100 //initial pressure in kPa
P2=5000 //final pressure in kPa
v=0.001004 //specific volume in m^3/kg
w=v*(P2-P1) //work required to pump water isentropically
printf("\n hence, work required to pump water isentropically is w=%.2 f kJ/kg.\n",w)
```

Scilab code Exa 9.8 Velocity in exit flow

```
1 //example 8
2 //Velocity in exit flow
3 clear
```

Scilab code Exa 9.9 Rate of Entropy Generation

```
1 // example 9
2 //Rate of Entropy Generation
3 clear
4 clc
5 disp('From R-410a tables, we get')
6 hi=280.6 //in kJ/kg
7 he=307.8 //in kJ/kg
8 si=1.0272 //in kJ/kg
9 se=1.0140 //in kJ/kg
10 m=0.08 //flow rate of refrigerant in kg/s
11 P=3 //electrical power input in kW
12 Qcv=m*(he-hi)-P //in kW
13 To=30 //in Celsius
14 Sgen=m*(se-si)-Qcv/(To+273.2) //rate of entropy
      generation
15 printf("\n Hence, the rate of entropy generation for
      this process is Sgen=%.5f kW/K. \n", Sgen)
```

Scilab code Exa 9.10 Turbine efficiency

```
1 // example 10
2 //turbine efficiency
3 clear
4 clc
5 hi=3051.2 //initial specific heat of enthalpy in kJ/
6 si=7.1228 //initial specific entropy in kJ/kg-K
7 sf=0.7548 //in kJ/kg-K
8 sfg=7.2536 //in kJ/kg-K
9 ses=si //final specific entropy is same as the
      initial
10 xes=(si-sf)/sfg //quality of steam when it leaves
     the turbine
11 hf = 225.9 //in kJ/kg
12 hfg=2373.1 //in kJ/kg
13 hes=hf+xes*hfg //final specific heat of enthalpy in
     kJ/kg
14 ws=hi-hes //work output of turbine calculated
      ideally in kJ/kg
15 wa=600 //actual work output of turbine in kJ/kg
16 nturbine=wa/ws //efiiciency of turbine
17 printf("\n hence, efficiency of the turbine is
     nturbine=\%.1 f. \ n", nturbine*100)
```

Scilab code Exa 9.11 Turbine inlet pressure

```
1 //example 11
2 //turbine inlet pressure
3 clear
4 clc
5 hi=1757.3 //initial specific heat of enthalpy of air
        in kJ/kg
6 si=8.6905 //initial specific entropy of airin kJ/kg-K
7 he=855.3 //final specific heat of enthalpy of air in kJ/kg
```

```
8 w=hi-he //actual work done by turbine in kJ/kg
9 n=0.85 //efficiency of turbine
10 ws=w/n //ideal work done by turbine in kJ/kg
11 hes=hi-ws //from first law of isentropic process
12 Tes=683.7 //final temperature in kelvins from air tables
13 ses=7.7148 //in kJ/kg-K
14 R=0.287 //gas constant in kJ/kg-K
15 Pi=100/%e^((si-ses)/-R) //turbine inlet pressure in kPa
16 printf("\n hence, turbine inlet pressure is Pi=%.0f kPa.\n",Pi)
```

Scilab code Exa 9.12 Required work input

```
1 // example 12
2 //required work input
3 clear
4 clc
5 Pe=150 //final pressure of air in kPa
6 Pi=100 //initial presure of air in kPa
7 k = 1.4
8 Ti=300 //initial temperature of air in kelvis
9 Tes=Ti*(Pe/Pi)^((k-1)/k) //from second law
10 ws=1.004*(Ti-Tes) //from first law of isentropic
     process
11 n=0.7 // efficiency of automotive supercharger
12 w=ws/n //real work input in kJ/kg
13 Te=Ti-w/1.004 //temperature at supercharger exit in
14 printf("\n hence, required work input is w=\%.1 f kJ/kg
     . \ n", w)
15 printf("\n and exit temperature is Te=\%.1 f K.\n", Te)
```

Chapter 10

Availibility

Scilab code Exa 10.1 Calculating reversible work

```
1 //example 1
2 // Calculating reversible work
3 clear
4 clc
5 //Form the Steam Tables, the inlet and the exit state
      properties are
6 hi=171.95 //initial specific heat of enthalpy in kJ/
7 si=0.5705 //initial specific entropy in kJ/kg-K
8 se=2.1341 //final specific entropy in kJ/kg-K
9 he=765.34 //final specific heat of enthalpy in kJ/kg
     -K
10 m=5 //mass flow rate of feedwater in kg/s
11 q1=900/m //heat added by one of the sources in kJ/kg
12 q2=he-hi-q1 //second heat transfer in kJ/kg
13 To=25+273.3 //Temp. of the surroundings in K
14 T1=100+273.2 //temp. of reservoir of one of the
     source in K
15 T2=200+273.2 //temp. of reservoir of second source
16 wrev=To*(se-si)-(he-hi)+q1*(1-To/T1)+q2*(1-To/T2) //
```

```
reversible work in kJ/kg 17 printf("\n Hence, the irreversibility is i=\%.1f kJ/kg.\n",wrev)
```

Scilab code Exa 10.2 Calculating reversible work

```
1 // example 2
2 // Calculating reversible work
3 clear
4 clc
5 //Form the Steam Tables, the inlet and the exit state
      properties are
6 hi=298.6 //initial specific heat of enthalpy in kJ/
     kg
7 si=6.8631 //initial specific entropy in kJ/kg-K
8 se=7.4664 //final specific entropy in kJ/kg-K
9 he=544.7 //final specific heat of enthalpy in kJ/kg-
10 q=-50 //heat lost to surroundings in kJ/kg
11 w=hi-he+q //work in kJ/kg
12 To=25+273.2 //Temp. of the surroundings in K
13 P1=100 // Pressure of ambient air in kPa
14 P2=1000 //Final pressure of air after compression in
      kPa.
15 R=0.287 // Universal gas constant in kJ/kg-K
16 wrev=To*(se-si-R*\log(P2/P1))-(he-hi)+q*(1-To/To)//
      reversible work for the given change of state in
     kJ/kg
17 i=wrev-w //irreversibility in kJ/kg
18 printf ("\n Hence, the irreversibility is i=\%.1 \text{ f kJ}/
     kg.\n",i)
```

Scilab code Exa 10.3 Calculating reversible work and irreversibility

```
1 //example 3
2 // Calculating reversible work and irreversibility
3 clear
4 clc
5 //Form the Steam Tables at state 1
6 u1=1243.5 //initial specific internal energy in kJ/
     kg
7 s1=4.4819 //initial specific entropy in kJ/kg-K
8 v1=28.895 //initial specific volume in m<sup>3</sup>/kg
9 v2=2*v1 //final specific volume in kg/m<sup>3</sup>
10 u2=u1 //initial specific internal energy in kJ/kg
11 //These two independent properties, v2 and u2, fix
      state 2. The final temp. is calculated by
      interplotation using the data for T2=5C and v2,x
      =0/3928 and u=948.5 kJ/kg. For T2=10C and v2, x
      =0.5433 and u=1317 \text{ kJ/kg}
12 T2=9.1+273.2 // final temp. in K
13 \times 2=0.513 //quality in final state
14 s2=4.644 //final specific entropy in kJ/kg
15 V1=1 //volume of part of A in m<sup>3</sup>
16 m=V1/v1 //mass flow rate in kg/s
17 To=20+273.2 //Room temperature in K
18 Wrev=To*m*(s2-s1) //reversible work in kJ
19 I=Wrev //irreversibility of the process
20 printf ("\n The irreversibility is I=\%.3 \, f \, kJ/kg.\n", I
```

Chapter 11

Power and Refrigeration Systems with phase change

Scilab code Exa 11.1 To determine the efficiency of Rankine cycle

```
1 // Ques 1
2 //To determine the efficiency of Rankine cycle
3 clc
4 clear
5 //1-Inlet state of pump
6 //2 - Exit state of pump
7 P2=2000; //Exit pressure in kPa
8 P1=10; // Inlet pressure in kPa
9 v=0.00101; // specific weight of water in m^3/kg
10 wp=v*(P2-P1); // work done in pipe in kJ/kg
11 h1=191.8; //Enthalpy in kJ/kg from table
12 h2=h1+wp; //enthalpy in kJ/kg
13 //2-Inlet state for boiler
14 //3-Exit state for boiler
15 h3=2799.5; // Enthalpy in kJ/kg
16 //3-Inlet state for turbine
17 //4-Exit state for turbine
18 //s3=s4 (Entropy remain same)
19 s4=6.3409; //kJ/kg
```

Scilab code Exa 11.2 To determine the efficiency of Rankine cycle

```
1 // Ques 2
2 //To determine the efficiency of Rankine cycle
3 clc
4 clear
5 //1-Inlet state of pump
6 //2 - Exit state of pump
7 P2=4000; //Exit pressure in kPa
8 P1=10; // Inlet pressure in kPa
9 v=0.00101; //specific weight of water in m<sup>3</sup>/kg
10 wp=v*(P2-P1);//work done in pipe in kJ/kg
11 h1=191.8; //Enthalpy in kJ/kg from table
12 h2=h1+wp; //enthalpy in kJ/kg
13 //2-Inlet state for boiler
14 //3-Exit state for boiler
15 h3=3213.6; //Enthalpy in kJ/kg from table
16 //3-Inlet state for turbine
17 //4-Exit state for turbine
18 //s3=s4 (Entropy remain same)
19 s4=6.7690; //Entropy in kJ/kg from table
20 sf=0.6493; //Entropy at liquid state in kJ/kg from
21 sfg=7.5009; //Entropy difference for vapor and liquid
```

Scilab code Exa 11.3 To determine the efficiency of a cycle

```
1 // Ques 3
2 //To determine the efficiency of a cycle
3 clc
4 clear
5 //1-Inlet state of pump
6 //2 - Exit state of pump
7 P2=4000; //Exit pressure in kPa
8 P1=10; // Inlet pressure in kPa
9 v=0.00101; //specific weight of water in m<sup>3</sup>/kg
10 wp=v*(P2-P1); // work done in pipe in kJ/kg
11 h1=191.8; //Enthalpy in kJ/kg from table
12 h2=h1+wp; //enthalpy in kJ/kg
13 //2-Inlet state for boiler
14 //3-Exit state for Boiler
15 h3=3213.6; //Enthalpy in kJ/kg from table
16 //3-Inlet state for high pressure turbine
17 //4-Exit state for high pressure turbine
18 //s3=s4 (Entropy remain same)
19 s4=6.7690; //Entropy in kJ/kg from table
20 sf=1.7766; //Entropy at liquid state in kJ/kg from
      table
21 sfg=5.1193; //Entropy difference for vapor and liquid
       state in kJ/kg from table
22 x4=(s4-sf)/sfg;//x-factor
```

```
23 hf=604.7//Enthalpy of liquid state in kJ/kg
24 hfg=2133.8; //Enthalpy difference in kJ/kg for
      turbine
25 h4=hf+x4*hfg;//Enthalpy in kJ/kg
26 //5-Inlet state for low pressure turbine
27 //6-Exit pressure for low pressure turbine
28 sf=0.6493; //Entropy in liquid state in kJ/kg for
      turbine
29 h5=3273.4; // enthalpy in kJ/kg
30 s5=7.8985; //Entropy in kJ/kg
31 sfg=7.5009; //entropy diff in kJ/kg
32 x6=(s5-sf)/sfg;//x-factor
33 hfg=2392.8; //enthalpy difference for low pressure
      turbine in kj/kg
34 h6=h1+x6*hfg; //entropy in kg/kg
35 wt=(h3-h4)+(h5-h6); // work output in kJ/kg
36 \text{ qh} = (h3-h2)+(h5-h4);
37
38 \text{ nth} = (\text{wt} - \text{wp}) / \text{qh};
39 printf ('Percentage efficiency = \%.1 \,\mathrm{f}', nth*100);
```

Scilab code Exa 11.4 Efficiency of Refrigeration cycle

```
1  //ques4
2  //Efficiency of Refrigeration cycle
3  clc
4  clear
5  //from previous examples
6  h1=191.8; //kJ/kg
7  h5=3213.6; //kg/kg
8  h6=2685.7; //kJ/kg
9  h7=2144.1; //kJ/kg
10  h3=604.7; //kJ/kg
11  //1-Inlet state of pump
12  //2-Exit state of pump
```

```
13 P2=400; //Exit pressure in kPa
14 P1=10; //Inlet pressure in kPa
15 v=0.00101; //specific weight of water in m<sup>3</sup>/kg
16 wp1=v*(P2-P1); //work done for low pressure pump in
      kJ/kg
17 h1=191.8; //Enthalpy in kJ/kg from table
18 h2=h1+wp1; //enthalpy in kJ/kg
19 //5-Inlet state for turbine
20 //6,7-Exit state for turbine
21 y=(h3-h2)/(h6-h2); // extraction fraction
22 wt=(h5-h6)+(1-y)*(h6-h7); // turbine work in kJ/kg
23 //3-Inlet for high pressure pump
24 //4-Exit for high pressure pump
25 P3 = 400; //kPa
26 \text{ P4=4000; } //\text{kPa}
27 v=0.001084; // specific heat for 3-4 process in m<sup>3</sup>/kg
28 wp2=v*(P4-P3);//work done for high pressure pump
29 h4=h3+wp2; //Enthalpy in kJ/kg
30 wnet=wt-(1-y)*wp1-wp2;
31 qh=h5-h4; //Heat output in kJ/kg
32 nth=wnet/qh;
33 printf('Refrigerator Efficiency = \%.1 \, \text{f}', nth*100);
```

Scilab code Exa 11.5 To determine thermal efficiency of cycle

```
1 //ques5
2 //To determine thermal efficiency of cycle
3 clear
4 clc
5 //5-Inlet state for turbine
6 //6-Exit state for turbine
7 //h-Enthalpy at a state
8 //s-Entropy at a state
9 //from steam table
10 h5=3169.1; //kJ/kg
```

```
11 s5=6.7235; //kJ/kg
12 \text{ s6s=s5};
13 sf=0.6493; //Entropy for liquid state in kJ/kg
14 sfg=7.5009; //Entropy difference in kJ/kg
15 hf = 191.8; //kJ/kg
16 hfg=2392.8; //Enthalpy difference in kJ/kg
17 x6s = (s6s - sf)/sfg; //x - factor
18 h6s=hf+x6s*hfg;//kJ/Kg at state 6s
19 nt=0.86; //turbine efficiency given
20 \text{ wt=nt*(h5-h6s)};
21 //1 - Inlet state for pump
\frac{22}{\sqrt{2-Exit}} state for pump
23 np=0.80;//pump efficiency given
24 v=0.001009; // specific heat in m<sup>3</sup>/kg
25 P2=5000; //kPa
26 P1=10; //kPa
27 wp=v*(P2-P1)/np;//Work done in pump in kJ/kg
28 wnet=wt-wp; // net work in kJ/kg
29 //3-Inlet state for boiler
30 //4-Exit state for boiler
31 h3=171.8; //in kJ/kg from table
32 h4=3213.6; //kJ/kg from table
33 \text{ qh}=h4-h3;
34 nth=wnet/qh;
35 printf('Cycle Efficiency = \%.1 \, \text{f}', nth*100);
```

Chapter 12

Power and Refrigeration Systems gaseous working fluids

Scilab code Exa 12.1 Standard brayton cycle

```
1 //ques1
2 //Standard brayton cycle
3 clc
4 clear
5 //1-Inlet for compressor
6 //2-Exit for compressor
7 //T-Temperature at a state
8 //P-Pressure at a state
9 T1=288.2; //K
10 P2=1000; //kPa
11 P1=100; //kPa
12 k=1.4;
13 T2=T1*(P2/P1)^(1-1/k);/K
14 Cp=1.004; // Specific heat at constant pressure in kJ/
15 wc=Cp*(T2-T1); // compressor work in kJ/kg;
16 printf('Temperature T2 = \%.1 f \text{ K/n',T2});
17 printf(' Compressor work = \%.1 \, \text{f kJ/kg } \ \text{n',wc};
18 //3-Turbine Inlet
```

```
19 //4-Turbine Exit
20 P4=P1;
21 P3=P2;
22 T3=1373.2; //K
23 T4=T3*(P4/P3)^(1-1/k);/K
24 \text{ wt} = \text{Cp} * (T3 - T4);
25 \text{ wnet=wt-wc};
26 printf(' Temperature T3 = \%.1 f \text{ K/n',T3});
27 printf (' Temperature T4 = \%.1 f K n', T4);
28 printf(' Turbine work = \%.1 \, \text{f kJ/kg/n',wt});
29 printf(' Net work = \%.1 \, \text{f kJ/kg/n',wt-wc});
30 //2-Also high temperature heat exchanger Inlet
31 //3 - (-do -) Exit
32 qh=Cp*(T3-T2);//Heat of source in kJ/kg
33 //4-high temp heat exchanger inlet
34 //1 - (-do-) Exit
35 ql=Cp*(T4-T1);//Heat of sink in kJ/kg
36 nth=wnet/qh;
37 printf(' Thermal Efficiency of cycle = %.1f percent'
      ,nth*100);
```

Scilab code Exa 12.2 Standard brayton cycle

```
// Calculation mistake in book
// ques2
// Standard brayton cycle
clc
clear
// Calculation mistake in book
//1-Inlet for compressor
//2-Exit for compressor
//T-Temperature at a state
//P-Pressure at a state
//P-Pressure at a state
T1=288.2;//K
P2=1000;//kPa
```

```
13 P1 = 100; //kPa
14 k=1.4;
15 T2s=T1*(P2/P1)^(1-1/k);/K
16 nc=.80; // Compressor Efficiency
17 T2=T1+(T2s-T1)/0.80;
18 Cp=1.004; // Specific heat at constant pressure in kJ/
19 wc=Cp*(T2-T1); // compressor work in kJ/kg;
20 printf ('Temperature T2 = \%.1 \text{ f K/n', T2});
21 printf(' Compressor work = \%.1 \, \text{f kJ/kg } \ \text{n',wc};
22 //3-Turbine Inlet
23 //4-Turbine Exit
24 P4 = P1;
25 P3=P2;
26 \quad T3 = 1373.2; //K
27 \text{ T4s} = \text{T3} * (\text{P4}/\text{P3})^{(1-1/k)}; //\text{K}
28 nt=0.85; //turbine Efficiency
29 \quad T4=T3-(T3-T4s)*0.85;
30 \text{ wt} = \text{Cp} * (T3 - T4);
31 \text{ wnet=wt-wc};
32 printf(' Temperature T3 = \%.1 \text{ f K/n',T3});
33 printf(' Temperature T4 = \%.1 \, f \, K \setminus n', T4);
34 printf (' Turbine work = \%.1 \, \text{f kJ/kg/n', wt});
35 printf(' Net work = \%.1 \, \text{f kJ/kg/n',wt-wc});
36 //2-Also high temperature heat exchanger Inlet
37 //3 - (-do-) Exit
38 qh=Cp*(T3-T2); //Heat of source in kJ/kg
39 //4-high temp heat exchanger inlet
40 //1 - (-do-) Exit
41 ql=Cp*(T4-T1);//Heat of sink in kJ/kg
42 nth=wnet/qh;
43 printf(' Thermal Efficiency of cycle = \%.1f percent'
       ,nth*100);
```

Scilab code Exa 12.3 efficiency of the cycle

```
//ques3
//efficiency of the cycle
clear
wnet=395.2;//kJ/kg from example no 1
//Tx=T4
Tx=710.8;//K from example no 1
T3=1373.2;//K from example no 1
Cp=1.004;//specific heat in kJ/kg
dh=Cp*(T3-Tx);
thewnet/qh;
printf('Thermal efficiency = %.1f percent',nth*100);
```

Scilab code Exa 12.4 Calculation of work in the given cycle

```
1 //ques4
2 //Calculation of work in the given cycle
3 clear
4 clc
5 R=0.287; //gas constant
6 T1=288.2; //compressor temperature K
7 T2=1373.2; //K turbine temperature K
8 //Pe/Pi=c=10, Pi/Pe=1/c from example 12.1
9 c=10;
10 wc=-R*T1*log(c);
11 printf('Isothermal work in compressor = %.1 f kJ/kg \ n',wc);
12 wt=-R*T2*log(1/c);
13 printf(' Isothermal work in turbine = %.1 f kJ/kg\n', wt);
```

Scilab code Exa 12.5 air standard cycle for jet repulsion

```
1 // ques5
2 //air standard cycle for jet repulsion
3 clear
4 clc
5 //1-compressor inlet
6 //2-Compressor exit
7 //P-Pressure at given point
8 //T-Temperature at given point
9 P1=100; //kPa
10 P2=1000; //kPa
11 T1=288.2; //K
12 T2=556.8; //K
13 wc=269.5; //from ex 12.1 work done in compressor in
      kJ/kg
14 //2-Burner inlet
15 //3 - Burner exit
16 P3=1000; //kPa
17 T3=1373.2; //K
18 / \text{wc} = \text{wt}
19 Cp=1.004; // specific enthalpy of heat at constant
      pressure in kJ/kg
20 k = 1.4;
21 \quad T4=T3-wc/Cp;
22 P4=P3*(T4/T3)^(1-1/k);
23 //\text{from } s4=s5 and h4=h5+v2/2 we get
24 T5=710.8//K, from second law
25 v = sqrt(2*Cp*1000*(T4-T5)); //m/s
26 printf ('Velocity of air leaving the nozel = \%.0 f m/s
      ',v);
```

Scilab code Exa 12.6 air standard refrigeration cycle

```
1 //ques6
2 //air standard refrigeration cycle
3 clear
```

```
4 clc
5 //1-compressor inlet
6 //2 - compressor exit
7 P1=100; //kPa
8 P2=500; //kPa
9 k=1.4;
10 rp=P2/P1;
11 cop=(rp^(1-1/k)-1)^-1;
12 printf ('Coefficient of performance = \%.3 \, \text{f} \, \text{n',cop});
13 //3-Expander inlet
14 //4-Expander exit
15 P3=P2;
16 P4=P1;
17 T3=288.23; //K, given and fixed
18 T4=T3/(P3/P4)^(1-1/k);
19 T1=253.2; //K, given
20 Cp=1.004; // Specific heat at cons pressure in kJ/kg
21 ql=Cp*(T1-T4); //heat released in kJ/kg
22 P=1//power required in kW
23 ms=P/q1; //kg/s
24 printf (' Rate at which the air enter the compressor
      = \%.3 \, f \, kg/s \, ,ms);
```

Scilab code Exa 12.7 the otto cycle

```
1 //ques7
2 //the otto cycle
3 clear
4 clc
5 //1-compressor inlet
6 //2-compressor exit
7 P1=100; //kPa
8 T1=288.2; //K
9 R=0.287; //gas constant
10 v1=R*T1/P1; // specific volume at inlet in m^3/kg
```

```
11 rv=10; //compression ratio given
12 k=1.4; //constant
13 T2=T1*rv^(k-1); //K
14 printf ('Temperature at compressor exit, T2 = \%.1 f K
      n', T2);
15 P2=P1*rv^k; //kPa
16 printf (' Pressure at compressor exit, P2 = \%.3 f MPa
      n', P2/1000);
17 v2=v1/rv; //specific heat at exit in m<sup>3</sup>/kg
18 //23-heat addition process
19 / q23 = Cv * (T3 - T2) = 1800 \text{ kJ/kg given}
20 q23=1800; //kJ/kg heat addition, given
21 Cv=0.717; //specific heat at constant volume in kJ/kg
22 T3=T2+q23/Cv; //K
23 printf('\n Initial Temperature during heat additon
      process, T3 = \%.0 f K \setminus n', T3);
24 P3=P2*(T3/T2); //kPa
25 printf ('Initial pressure during heat addition
      process, P3 = \%.3 f MPa \n', P3/1000);
26 r=10; //k=V4/V3=P3/P4
27 T4=T3*(1/r)^(k-1);
28 printf('\n Final temperature during heat addition
      process, T4 = \%.1 f K \setminus n', T4);
29 P4=P3/r^k; //kPa
30 printf(' Final pressure during heat addition process
      P4 = \%.4 f MPa \ n', P4/1000);
31 nth=1-1/r^k; //thermal efficiency
32 printf('\n Thermal efficiency = \%.1f percent \n',nth
      *100);
33 q41=Cv*(T1-T4); //heat for process 4-1 in kJ/kg
34 \text{ wnet} = q23 + q41;
35 mep=wnet/(v1-v2);//effective mean pressure n kPa
36 printf('\n Mean effective pressure = \%.0 \, \text{f kPa } \, \text{n'},
      mep);
```

Scilab code Exa 12.8 the diesel cycle

```
1 // ques7
2 //the diesel cycle
3 clear
4 clc
5 //1-compressor inlet
6 //2-compressor exit
7 P1=100; //kPa
8 T1=288.2; //K
9 R=0.287; //gas constant
10 v1=R*T1/P1; //specific volume at inlet in m<sup>3</sup>/kg
11 rv=20; //compression ratio given
12 k=1.4; //constant
13 T2=T1*rv^(k-1); //K
14 printf('Temperature at compressor exit, T2 = \%.1 f K
      n',T2);
15 P2=P1*rv^k; //kPa
16 printf (' Pressure at compressor exit, P2 = \%.3 f MPa
      n', P2/1000);
17 v2=v1/rv;//specific heat at exit in m^3/kg
18 //23-heat addition process
19 / q23 = Cv*(T3-T2) = 1800 \text{ kJ/kg given}
20 q23=1800; //kJ/kg heat addition, given
21 \text{ Cv} = .717;
22 Cp=1.004; //specific heat at constant pressure in kJ/
      kg
23 T3=T2+q23/Cp; //K
24 printf('\n Initial Temperature during heat addition
      process, T3 = \%.0 f K \setminus n', T3);
25 r=T3/T2; //T3/T2=V3/V2=r
26 v3 = r * v2;
27 T4=T3/(v1/v3)^(k-1);
28 printf ('Final temperature during heat addition
      process, T4 = \%.0 f K \setminus n', T4);
29 q41=Cv*(T1-T4); //heat for process 4-1 in kJ/kg
30 \text{ wnet} = q23 + q41;
31 mep=wnet/(v1-v2); // effective mean pressure in kPa
```

```
32 qh=1800; // heat transfer in kJ/kg
33 nth=wnet/qh; // thermal efficiency
34
35 printf('\n Thermal efficiency = %.1f percent \n',nth
     *100);
36 printf('\n Mean effective pressure = %.0f kPa \n',
     mep);
```

Ideal Gas Mixtures

Scilab code Exa 13.3 calculating humidity ratio dew point mass of air mass of vapor

```
1 //ques3
2 //calculating humidity ratio, dew point, mass of air,
      mass of vapor
3 clear
4 clc
5 r=0.70; //relative humidity
6 Pg=5.628;//saturation pressure in kPa
7 Pv=r*Pg;//vapour pressure in kPa
8 P=100; // net pressure kPa
9 Pa=P-Pv; // Partial pressure of air
10 w=0.622*Pv/Pa;//humidity ratio formula
11 V=100; //volume in m<sup>3</sup>
12 Ra=0.287; //gas constant for water vapour
13 T=308.2; // Temperature in K
14 ma=Pa*V/(Ra*T); //mass in kg
15 mv=w*ma; //mass of vapour
16 printf('Mass of vapour = \%.2 \, f \, Kg', mv);
```

Scilab code Exa 13.4 calculating amount of water vapour condensed on cooling

```
1 //ques4
2 //calculating amount of water vapour condensed on
      cooling
3 clear
4 clc
5 //from example 3
6 w1=0.0255; //w1=w, humidity ratio at initial
      temperature
7 ma=108.6; //mass of air in kg
8 P=100; //kPa net pressure
9 //at 5 C mixture is saturated so Pv2=Pg2
10 Pg2=0.8721;
11 Pv2=Pg2;
12 \text{ w}2=0.622*Pv2/(P-Pg2);
13 mc = ma * (w1 - w2);
14 printf('Mass of vapour condense = \%.3 \, \text{f kg } \ \text{n',mc});
```

Scilab code Exa 13.5 calculating heat transfer per kilogram of dry air

```
//ques5
//calculating heat transfer per kilogram of dry air
clear
clc
//1-inlet state
//2-Exit state
r1=0.80;//realtive humidity at state 1
Pg1=4.246;//saturation pressure of vapour in kPa
P1=105;//net pressure at state 1 in kPa
P2=100;//net pressure at state 2 in kPa
Pv1=r1*Pg1;//partial pressure of vapour in kPa
v1=0.622*Pv1/(P1-Pv1);//humidity ratio at state 1
r2=0.95;//relative humidity at state 2
```

```
14 Pg2=1.7051; // saturation pressure of vapour in kPa
15 Pv2=r2*Pg2; // partial pressure of vapour in kPa
16 w2=0.622*Pv2/(P2-Pv2); // humidity ratio at state 2
17 T1=30; //C
18 T2=15; //C
19 Cp=1.004; // specific heat of water vapour in kJ/kg
20 hv2=2528.9; // enthalpy of vapourisation of vapour in kJ/kg
21 hv1=2556.3; // enthalpy of vapourisation of vapour in kJ/kg
22 h12=62.99; // enthalpy of
23 q=Cp*(T2-T1)+w2*hv2-w1*hv1+h12*(w1-w2); //kJ/kg
24 printf('Heat transferred per unit mass = %.2 f kJ/kg of dry air',q);
```

Scilab code Exa 13.6 calculating heat transferred in gas vapour mixture

```
1 //ques6
2 //calculating heat transferred in gas vapour mixture
3 clear
4 clc
5 //n-Nitrogen
6 //v-water vapour
7 Pn2=1995; // Pressure of nitrogen in kPa
8 V=0.5; //Volume in m<sup>3</sup>
9 Rn2=0.2968; //Gas constant for nitrogen in kJ/kg.K
10 Rv=0.4615; //gas constant for vapour
11 T1=323.2; // Temperature in K
12 T2=283.2; // Temperature in K
13 Pv1=5; // Pressure of water vapour in kPa at state 1
14 Pv2=1.2276; // Pressure of water vapour in kPa at
      state 2
15 mn2=Pn2*V/(Rn2*T1);//mass of nitrogen
16 mv1=Pv1*V/(Rv*T1);//mass of vapour in kg
17 mv2=Pv2*V/(Rv*T2); //mass of vapour in kg
```

```
18 ml2=mv1-mv2; // mass of liquid condensed n kg
19 uv1=2443.1; // specific internal energy of vapour in
        kJ/kg at state 1
20 uv2=2389.2; // specific internal energy of vapour in
        kJ/kg at state 2
21 ul2=42.0; // specific internal energy of liquid water
        in kJ/kg
22 Cv=0.745; // specific heat at constant volume in kJ/kg
        .K
23 Q=mn2*Cv*(T2-T1)+mv2*uv2+ml2*ul2-mv1*uv1;
24 printf('Heat transferred = %.1 f kJ ',Q);
```

Scilab code Exa 13.7 calculating humidity ratio and relative humidity

```
1 // ques7
2 //calculating humidity ratio and relative humidity
3 clear
4 clc
5 //1-Inlet state
6 / 2 - Exit state
7 P=100; //net pressure n kPa
8 //it is steady state adiabatic process
9 //water vapour leaving is saturated so Pv2=Pg2
10 Pg2=2.339; //saturation pressure of vapour in kPa
11 Pv2=Pg2; // partial pressure of vapour
12 \text{ w}2=0.622*\text{Pv}2/(P-\text{Pg}2);
13 Cpa=1.004; // specific heat n kJ/kg/K
14 T2=20; // final temp in C
15 T1=30; // initial temp in C
16 Hfg2=2454.1; //specific heat difference at state 2 in
       kJ/kg
17 hv1=2556.3; //enthalpy of water vapour at state 1 in
     kJ/kg
18 h12=83.96; //enthalpy of liquid water in kJ/kg
19 w1 = (Cpa*(T2-T1)+w2*Hfg2)/(hv1-hl2);
```

```
20  printf('Relative humidity = %.4 f \n',w1);
21  //also w1=0.622*Pv1/(100-Pv2)
22  Pv1=100*w1/(0.622+w1);
23  Pg1=4.246;//saturation pressure at state 1 in kPa
24  r=Pv1/Pg1;//humidity ratio
25  printf(' Humidity ratio = %.3 f ',r);
```

Thermodynamics Property Relations

Scilab code Exa 14.1 to determine the sublimation pressure of water

```
//ques1
//to determine the sublimation pressure of water
clear
clc
//from table in appendix B.1.5
T1=213.2;//K, Temperature at state 1
P2=0.0129;//kPa, pressure at state 2
T2=233.2;//K, Temperature at state 2
hig=2838.9;//kJ/kg, enthalpy of sublimation
R=.46152;//Gas constant
//using relation log(P2/P1)=(hig/R)*(1/T1-1/T2)
P1=P2*exp(-hig/R*(1/T1-1/T2));
printf('Sublimation Pressure = %.5f kPa \n',P1);
```

Scilab code Exa 14.4 Volume expansivity Isothermal and Adiabatic compressibility

```
1 // ques4
2 //Volume expansivity, Isothermal and Adiabatic
      compressibility
3 clear
4 clc
5 //known data
6 ap=5*10^-5; //K^-1 Volume expansivity
7 bt=8.6*10^-12; //\text{m}^2/\text{N}, Isothermal compressibility
8 v=0.000114; //m^3/kg, specific volume
9 P2=100*10^6; //pressure at state 2 in kPa
10 P1=100; //pressure at state 1 in kPa
11 w=-v*bt*(P2^2-P1^2)/2; //work done in J/kg
12 / q = T*ds \text{ and } ds = -v*ap*(P2-P1)
13 //so q=-T*v*ap*(P2-P1)
14 T=288.2; //Temperature in K
15 q=-T*v*ap*(P2-P1); //heat in J/kg
16 du=q-w; //change in internal energy in J/kg
17 printf ('Change in internal energy = \%.1 \,\mathrm{f} J/kg', du);
```

Scilab code Exa 14.5 adiabatic steady state processes

```
1 //ques5
2 //adiabatic steady state processes
3 clear
4 clc
5 //from table A.2
6 P1=20; // pressure at state 1 in MPa
7 P2=2; // pressure at state 2 in MPa
8 T1=203.2; // Temperature at state 1 in K
9 Pr1=P1/3.39; // Reduced pressure at state 1
10 Pr2=P2/3.39; // Reduced pressure at state 2
11 Tr1=T1/126.2; // Reduced temperature
12 // from compressibility chart h1*-h1=2.1*R*Tc
13 // from zero pressure specific heat data h1*-h2*=Cp*(T1a-T2a)
```

Scilab code Exa 14.6 isothermal steady state processes

```
1 //ques6
2 //isothermal steady state processes
3 clear
4 clc
5 //from table A.2
6 P1=8;//pressure at state 1 in MPa
7 P2=0.5; //pressure at state 2 in MPa
8 T1=150; // Temperature at state 1 in K
9 Pr1=P1/3.39; // Reduced pressure at state 1
10 Pr2=P2/3.39; //Reduced pressure at state 2
11 Tr1=T1/126.2; //Reduced temperature
12 T2=125; //temperature at state 2
13 //from compressibility chart h1*-h1=2.1*R*Tc
14 //from zero pressure specific heat data h1*-h2*=Cp*(
     T1a-T2a)
15 / h2*-h2=0.5*R*Tc
16 // this gives dh=h1-h2=-2.1*R*Tc+Cp*(T1a-T2a)+0.15*R*
     Tc
17 R=0.2968; //gas constant for given substance
18 Tc=126.2; //K, Constant temperature
```

Scilab code Exa 14.7 percent deviation using specific volume calculated by kays rule and vander waals rule

```
1 // ques7
2 //percent deviation using specific volume calculated
      by kays rule and vander waals rule
3 clear
4 clc
5 //a-denotes C02
6 //b-denotes CH4
7 T=310.94; // Temperature of mixture K
8 P=86.19; // Pressure of mixture in MPa
9 //Tc- critical Temperature
10 //Pc-critical pressure
11 Tca=304.1; //K
12 Tcb=190.4; //K
13 Pca=7.38; //MPa
14 Pcb=4.60; //MPa
15 Ra=0.1889; // gas constant for a in kJ/kg.K
16 Rb=0.5183; //gas constant for b in kJ/kg.K
17 xa=0.8; //fraction of CO2
18 xb=0.2; //fraction of CH4
```

```
19 Rm=xa*Ra+xb*Rb; //mean gas constant in kJ/kg.K
20 Ma=44.01; //molecular mass of a
21 Mb=16.043; // molecular mass of b
22 //1.Kay's rule
23 ya=xa/Ma/(xa/Ma+xb/Mb); //mole\ fraction\ of\ a
24 yb=xb/Mb/(xa/Ma+xb/Mb);//mole fraction of b
25 Tcm=ya*Tca+yb*Tcb;//mean critical temp in K
26 Pcm=ya*Pca+yb*Tcb;//mean critical pressure n MPa
27 //therefore pseudo reduced property of mixture
28 \text{ Trm}=T/Tcm;
29 Prm=P/Pcm;
30 Zm=0.7; // Compressibility from generalised
      compressibility chart
31 vc=Zm*Rm*T/P/1000;//specific volume calculated in m
      ^3/\mathrm{kg}
  ve=0.0006757; //experimental specific volume in m<sup>3</sup>/
      kg
33 pd1=(ve-vc)/ve*100;//percent deviation
34 printf ('Percentage deviation in specific volume
      using Kays rule = \%.1f percent \n', pd1);
35
36 //2. using vander waals equation
37 //values of vander waals constant
38 Aa=27*Ra^2*Tca^2/(64*Pca*1000);
39 Ba=Ra*Tca/(8*Pca*1000);
40 Ab=27*Rb^2*Tcb^2/(64*Pcb*1000);
41 Bb=Rb*Tcb/(8*Pcb*1000);
42 //mean vander waals constant
43 Am = (xa*sqrt(Aa)+xb*sqrt(Ab))^2;
44 Bm = (xa*Ba+xb*Bb);
45 //using vander waals equation we get cubic equation
46 //solving we get
47 vc=0.0006326; //calculated specific volume in m<sup>3</sup>/kg
48 \text{ pd2} = (\text{ve-vc})/\text{ve} * 100;
49 printf (' Percentage deviation in specific volume
      using vander waals eqn = \%.1 f percent \n', pd2);
```

Comustion

Scilab code Exa 15.1 theoratical air fuel ratio for combustion of octane

```
//ques1
//theoratical air-fuel ratio for combustion of octane
clear
clc
rm=(12.5+47.0)/1;//air fuel ratio on mole basis
rma=rm*28.97/114.2;//air fuel ratio on mass basis;
printf('Theoratical air fuel ratio on mass basis = % .1 f kg air/kg fuel \n',rma);
```

Scilab code Exa 15.6 determining heat transfer per kilomole of fuel entering combustion chamber

```
1 //ques6
2 //determining heat transfer per kilomole of fuel
        entering combustion chamber
3 clear
4 clc
```

```
5 //1-CH4
6 //2-CO2
7 //3-H2O
8 //hf-standard enthalpy of given substance
9 hf1=-74.873; //kJ
10 hf2=-393.522; //kJ
11 hf3=-285.830; //kJ
12 Qcv=hf2+2*hf3-hf1; //kJ
13 printf('Heat transfer per kilomole of fuel entering combustion chamber = %.3 f kJ ',Qcv);
```

Scilab code Exa 15.7 calculating enthalpy of water at given pressure and temperature

```
1 //ques7
2 //calculating enthalpy of water at given pressure
     and temperature
3 clear
4 clc
5 //1. Assuming steam to be an ideal gas with value of
     Cp
6 T1=298.15; // Initial temperature in K
7 T2=573.15; //final temperature in K
8 T=(T1+T2)/2; //average temperature in K
9 Cp=1.79+0.107*T/1000+0.586*(T/1000)^2-.20*(T/1000)
     ^3; // specific heat at constant pressure in kj/kg.
     K
10 M=18.015; //mass in kg
11 dh=M*Cp*(T2-T1);//enthalpy change in kJ/kmol
12 ho = -241.826; //enthalpy at standard temperature and
      pressure in kJ/mol
13 htp1=ho+dh/1000; //enthalpy at given temp and
     pressure in kJ/kmol
14 printf('1. Enthalpy of water at given pressure and
     temperature using value of Cp = \%.3 f kJ/kmol n',
```

```
htp1);
15
16 //2. Assuming steam to be an ideal gas with value
      for dh
17 dh=9359; //enthalpy change from table A.9 in kJ/mol
18 htp2=ho+dh/1000; //enthalpy at given temp and
      pressure in kJ/kmol
19 printf (' 2. Enthalpy of water at given pressure and
      temperature assuming value od dh = \%.3 \,\mathrm{f} \,\mathrm{kJ/kmol} \,
      n', htp2);
20
21 //3. Using steam table
22 dh=M*(2977.5-2547.2);//enthalpy change for gases in
      kJ/mol
23 \text{ htp3g=dh/1000+ho};
24 \text{ dh=M*}(2977.5-104.9); //enthalpy change for liquid in
      kJ/mol
25 hl=-285.830; // standard enthalpy for liquid in kJ/
26 htp3l=hl+dh/1000; //enthalpy at given temp and
      pressure in kJ/kmol
27 printf(' 3.(i) enthalpy at given temp and pressure
      in kJ/kmol in terms of liquid = \%.3 f kJ/kmol \ n',
      htp31);
28 printf(' 3.(ii) enthalpy at given temp and pressure
      in kJ/kmol in terms of liquid = \%.3 f kJ/kmol \n',
      htp3g);
29 //4. using generalised charts
30 / htp = ho - (h2*-h2) + (h2*-h1*) + (h1*-h1);
\frac{1}{h^2} + h^2 = Z * R * Tc
32 / h2*-h1*=9539 kJ/mol, from part 2
33 //h1*-h1=0 , as ideal gas
34 \quad Z=0.21; //from \quad chart
35 R=8.3145; //gas constant in SI units
36 Tc=647.3; // critical temperature in K
37 htp4=ho+9539/1000-Z*R*Tc/1000;//enthalpy at given
      temp and pressure in kJ/kmol
38 printf(' 4. enthalpy at given temp and pressure in
```

```
kJ/kmol using compressibility chart = \%.3 \, f \, kJ/kmol \, \ n', htp4);
```

Scilab code Exa 15.15 calculating reversible electromotive force

```
1 //ques15
2 //calculatng reversible electromotive force
3 clear
4 clc
5 / 1 - H2O
6 //2 - H2
7 //3 - O2
8 //hf-standard enthalpy
9 //sf-standard entropy
10 hf1=-285.830; //kJ
11 hf2=0; //kJ
12 hf3=0; //kJ
13 sf1=69.950; //kJ/K
14 sf2=130.678; //kJ/K
15 sf3=205.148; //kJ/K
16 dH=2*hf1-2*hf2-hf3;//change in enthalpy in kJ
17 dS=2*sf1-2*sf2-sf3;//change in entropy in <math>kJ/K
18 T=298.15; //temperature in K
19 dG=dH-T*dS/1000; //change in gibbs free energy in kJ
20 E=-dG*1000/(96485*4); //emf in V
21 printf('Reversible electromotive Force = \%.3 \, \mathrm{f} \, \mathrm{V}',E);
```

Scilab code Exa 15.17 efficiency of generator and plant

```
1 //ques17
2 //efficiency of generator and plant
3 clear
4 clc
```

Phase and Chemical Equilbrium

Scilab code Exa 16.2 to determine change in gibbs free energy

```
1 // ques 2
2 //to determine change in gibbs free energy
3 clear
4 clc
5 //1-H2
6 / 2 - O2
7 / 3 - H2O
9 / at T = 298 K
10 T1=298; //K
11 Hf1=0; //Enthalpy of formation of H2 at 298 K
12 Hf2=0; //Enthalpy of formation of O2 at 298 K
13 Hf3=-241.826; //enthalpy of formation of H2O at 298 K
      in kJ
14 dH=2*Hf1+Hf2-2*Hf3; // Change in enthalpy in kJ
15 Sf1=130.678; //Entropy of H2 at 298 K n J/K
16 Sf2=205.148; // Entropy of O2 at 298 K in J/K
17 Sf3=188.834; //entropy of H2O at 298 K in J/K
18 dS=2*Sf1+Sf2-2*Sf3; // Change in entropy in J/K
```

```
19 dG1=dH-T1*dS/1000; //change n gibbs free energy in kJ
20 printf ('Change in gibbs free energy at \%.0 \, \text{f K} = \%.3
      f kJ \setminus n', T1, dG1);
21
22 / at T = 2000 K
23 T2 = 2000; //K
24 Hf1=52.942-0; //Enthalpy of formation of H2 at 2000 K
25 Hf2=59.176-0; // Enthalpy of formation of O2 at 2000 K
26 Hf3=-241.826+72.788; //enthalpy of formation of H2O
      at 2000 K in kJ
27 dH=2*Hf1+Hf2-2*Hf3;//Change in enthalpy in kJ
28 Sf1=188.419; //Entropy of H2 at 2000 K n J/K
29 Sf2=268.748; //Entropy of O2 at 2000 K in J/K
30 Sf3=264.769; // entropy of H2O at 2000 K in J/K
31 dS=2*Sf1+Sf2-2*Sf3; //Change in entropy in J/K
32 dG2=dH-T2*dS/1000; //change n gibbs free energy in kJ
33 printf(' Change in gibbs free energy at \%.0\,\mathrm{f} K = \%
      .3 f kJ ',T2,dG2);
```

Scilab code Exa 16.3 calculating equilibrium constant

```
,K1);   
13 printf(' Equilibrium constant at \%.0\,f K=\%.3\,f \n', T2,K2);
```

Compressible Flow

Scilab code Exa 17.1 to determine isentropic stagnation pressure and temperature

```
//ques1
//to determine isentropic stagnation pressure and temperature
clear
clc
T=300;//Temperature of air in K
P=150;//Pressure of air in kPa
v=200;//velocity of air flow n m/s
Cp=1.004;//specific heat at constant pressure in kJ/kg
To=v^2/(2000*Cp)+T;//stagnation temperature in K
k=1.4;//constant
Po=P*(To/T)^(k/(k-1));//stagnation pressure in kPa
printf('Stagnation Temperature = %.1f K \n',To);
printf('Stagnation Pressure = %.1f kPa \n',Po);
```

Scilab code Exa 17.3 determining the thrust acting on a control surface

```
1 //ques3
2 //determining the thrust acting on a control surface
3 clear
4 clc
5 //i - i n l e t
6 / e - exit
7 //using momentum equation on control surface in x
       direction
8 me=20.4; //mass exiting in kg
9 mi=20; //mass entering in kg
10 ve=450; // \text{exit} velocity in m/s
11 vi=100; //exit velocity in m/s
12 Pi=95; // Pressure at inlet in kPa
13 Pe=125; // Pressure at exit in kPa
14 Po=100; //surrounding pressure in kPa
15 Ai=0.2; // inlet area in m<sup>2</sup>
16 Ae=0.1; // \text{exit} area in m<sup>2</sup>
17 Rx = (\text{me} * \text{ve} - \text{mi} * \text{vi}) / 1000 - (\text{Pi} - \text{Po}) * \text{Ai} + (\text{Pe} - \text{Po}) * \text{Ae}; / / \text{thrust}
        in x direction in kN
18 printf('Thrust acting in x direction = \%.2 f kN', Rx);
```

Scilab code Exa 17.5 determining velocity of sound in air

```
1 //ques5
2 //determining velocity of sound in air
3 clear
4 clc
5 k=1.4;//constant
6 R=0.287;//gas constant
7 //at 300K
8 T1=300;//K
9 c1=sqrt(k*R*T1*1000);
10 printf('Speed of sound at %.0 f K = %.1 f m/s \n',T1, c1);
11 T2=1000;//K
```

```
12 c2=sqrt(k*R*T2*1000);  
13 printf(' Speed of sound at \%.0\,\mathrm{f~K}=\%.1\,\mathrm{f~m/s~n'}, T2, c2);
```

Scilab code Exa 17.6 determining mass flow rate through control volume

```
1 //ques6
2 //determining mass flow rate through control volume
3 clear
4 clc
5 \text{ k=1.4;}//\text{constant}
6 R=0.287; //gas constant
7 To=360; //stagnation Temperature in K
8 T=To*0.8333; // Temperature of air in K, 0.8333
      stagnation ratio from table
9 v = sqrt(k*R*T*1000); // velocity in m/s
10 P=528; //stagnation pressure in kPa
11 d=P/(R*T); //stagnation density in kg/m<sup>3</sup>
12 A=500*10^-6; //area in m^2
13 ms=d*A*v; //mass flow rate in kg/s
14 printf ('Mass flow rate at the throat section = \%.4 \,\mathrm{f}
      kg/s \setminus n', ms);
15 //e-exit state
16 Te=To*0.9381; // exit temperature in K, ratio from
17 ce=sqrt(k*R*Te*1000); //exit velocity of sound in m/s
18 Me=0.573; //Mach number
19 ve=Me*ce;
20 Pe=800; //exit pressure in kPa
21 \text{ de=Pe/R/Te};
22 \text{ mse=de*A*ve};
23 printf (' Mass flow rate at the exit section = \%.4 \, \mathrm{f}
      kg/s \setminus n', mse);
```

Scilab code Exa 17.7 determining exit properties in a control volume

```
1 //ques7
2 //determining exit properties in a control volume
3 clear
4 clc
5 Po=1000; //stagnation pressure in kPa
6 To=360; //stagnation temperature in K
8 //when diverging section acting as nozzle
9 Pe1=0.0939*Po;//exit pressure of air in kPa
10 Te1=0.5089*To; //exit temperature in K
11 k=1.4; //constant
12 R=0.287; //gas constant for air
13 ce=sqrt(k*R*Te1*1000); //velocity of sound in exit
      section in m/s
14 Me=2.197; //mach number from table
15 ve1=Me*ce; // velocity of air at exit section in m/s
16 disp(" When diverging section act as a nozzle :-");
17 printf ('Exit pressure = \%.1 \, \text{f kPa } \, \text{n',Pe1});
18 printf ('Exit Temperature = \%.1 \, \text{f K } \text{n'}, \text{Te1});
19 printf ('Exit velocity = \%.1 \, \text{f m/s } \setminus \text{n',ve1});
20
21 //when diverging section act as diffuser
22 \text{ Me} = 0.308;
23 Pe2=0.0936*Po;//exit pressure of air in kPa
24 Te2=0.9812*To; // \text{exit} temperature in K
25 ce=sqrt(k*R*Te2*1000); //velocity of sound in exit
      section in m/s
26 \text{ ve2=Me*ce};
27 disp(" When diverging section act as a diffuser :-")
28 printf ('Exit pressure = \%.1 \,\mathrm{f} kPa \n', Pe2);
29 printf('Exit Temperature = \%.1 \, \text{f K } \text{n',Te2});
```

```
30 printf('Exit velocity = \%.1 \, \text{f m/s } \setminus \text{n',ve2});
```

Scilab code Exa 17.9 determining exit plane properties in control volume

```
1 //ques9
2 //determining exit plane properties in control
      volume
3 clear
4 clc
5 / x-inlet
6 //y - exit
7 Mx=1.5; //mach number for inlet
8 My=0.7011; //mach number for exit
9 Px=272.4; //inlet pressure in kPa
10 Tx=248.3; //inlet temperature in K
11 Pox=1000; //stagnation pressure for inlet
12 Py=2.4583*Px;//Exit Pressure in kPa
13 Ty=1.320*Tx; //Exit temperature in K
14 Poy=0.9298*Pox; //Exit pressure in kPa
15
16 printf('Exit pressure = \%.1 \, \text{f kPa } \, \text{n',Py});
17 printf(' Exit temperature = \%.1 f K \setminus n', Ty);
18 printf(' Exit stagnation pressure = \%.1 \, \text{f kPa } \setminus \text{n',Poy}
      );
```