Scilab Textbook Companion for Microwave Engineering by D. M. Pozar¹

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Book Description

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Scilab numbering policy used in this document and the relation to the above book.

Exa Example (Solved example)

Eqn Equation (Particular equation of the above book)

AP Appendix to Example(Scilab Code that is an Appednix to a particular Example of the above book)

For example, Exa 3.51 means solved example 3.51 of this book. Sec 2.3 means a scilab code whose theory is explained in Section 2.3 of the book.

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Chapter 2

ELECTROMAGNETIC THEORY

Scilab code Exa 2.1 program to calculate wavelength phase velocity and

```
1 // \text{ example } 2.1, \text{page no.} -24.
2 // program to calculate wavelength, phase velocity
      and wave impedence.
3 f = 3*10^9;
4 mur=3;
5 muo = 4 * \%pi * 10^-7;
6 eipsilao=8.854*10^-12;
7 eipsilar=7;
8 mue=muo*mur;
9 eipsila=eipsilao*eipsilar;
10 Vp=sqrt(1/(mue*eipsila));
11 lamda=Vp/f;
12 eta=sqrt(mue/eipsila);
13 // Result
14 disp(Vp, 'phase velocity in meter per second=')
            // phase velocity.
15 disp(lamda, 'wavelength in meter=') // wavelength.
16 disp(eta, 'wave impedence in ohm=') // wave
      impedence.
```

Scilab code Exa 2.2 program to find out skin depth

```
1 // example: -2.2. page no. -26.
2 // progarm to find out skin depth of aluminium,
     copper, gold and silver at frequency 10GHZ.
3 f = 10 * 10^9;
4 muo=4*%pi*10^-7; // permeability in free space.
5 \text{ omega=2*\%pi*f};
6 sigma_aluminium=3.816*10^7;
7 sigma_copper=5.813*10^7;
8 sigma_gold=4.098*10^7;
9 sigma_silver=6.173*10^7;
10 delta1=sqrt(2/(omega*muo*sigma_aluminium));
11 delta2=sqrt(2/(omega*muo*sigma_copper));
12 delta3=sqrt(2/(omega*muo*sigma_gold));
13 delta4=sqrt(2/(omega*muo*sigma_silver));
14 //result
15 disp(delta1, 'skin depth of aluminium in meter=') //
      skin depth of aluminium.
16 disp(delta2, 'skin depth of copper in meter=')
     skin depth of copper.
17 disp(delta3, 'skin depth of gold in meter=') //skin
     depth of gold.
18 disp(delta4, 'skin depth of silver in meter=') //
     skin depth of silver.
```

Scilab code Exa 2.3 program to find the resulting fields

```
1 // example: -2.3, page no. -31.
2 // program to find the resulting fields by assumibg plane waves on either side of the current sheet and enforcing the boundary conditions.
```

```
3 syms E x E1 E2 H1 H2 z Jo A B c N n d ko y;
4 sym('n*(E2-E1)=0');
                         //boundary condition to be
      satisfied at z=0
5 sym('z*(E2-E1)=0');
6 sym('n*(H2-H1)=Jo');
7 sym('z*(H2-H1)=Jo');
8 E1=A*N*exp(%i*ko*z)*x; // x component of electric
      field (region z<0).
  H1=A*N*exp(%i*ko*z)*(-y); // -y component of
      magnetic field (region z<0).
10 E2=B*N*exp(-\%i*ko*z)*x;
                              // x component of electric
       field (region z>0).
  H2=B*N*exp(-\%i*ko*z)*y;
                              // y component of electric
       field (region z>0).
12 disp(E1, 'for z < 0, E1=')
13 disp(H1, 'for z < 0, H1=')
14 disp(E2, 'for z>0, E2=')
15 disp(H2, 'for z>0, H2=')
16 //from boundary conditions imposed we get:-
17 c = [-1 -1; 1 -1];
18 d = [A; B];
19 c*d==[Jo;0];
20 d = inv(c) * [Jo; 0];
21 //result
22 // A=-Jo/2; B=-Jo/2.
23 disp(d)
```

Scilab code Exa 2.4 program to show decomposition in to RHCP and LHCP

```
1 // example: -2.4, page no. -34.
2 // program to show that a circularly polarized plane
```

```
wave can be decomposed in to RHCP and LHCP.
3 \text{ A=sym}('A');
4 B = sym('B');
5 Eo=sym('Eo');
6 \text{ x=sym}('x');
7 y = sym('y');
8 Ko=sym('Ko');
9 z = sym('z');
10 E=Eo*(x+2*y)*exp(-%i*Ko*z); // given
11 // can be written as:=>E=A*(x-y)*exp(-\%i*Ko*z)+B*(x+
      y)*exp(-\%i*Ko*z), so
12 p=[1 1; -\%i/2 \%i/2];
13 q=[A;B];
14 r=[1;1];
15 p*q==Eo*r;
16 q = inv(p) *Eo*r;
17 //result
18 disp('value of A and B will be=')
19 disp(q)
20 \operatorname{disp}(q(1,1)*(x-y)*\exp(-\%i*Ko*z)+q(2,1)*(x+y)*\exp(-\%i
      *Ko*z), 'E=')
21 //conclusion:-any linearly polarized wave can be
      decomposed in to two circularly polarized waves.
```

Scilab code Exa 2.5 program to compute the poynting vector

```
1 // example: -2.5, page no. -36.
2 // program to compute the poynting vector for the plane wave field.
3 syms E Eo H k s n N x r;
4 E=Eo*exp(-%i*k*r); // electric field.
5 H=(E/N)*n; //N is intrinsic impedence, n is unit vector.
6 H1=conj(H) // conjugate of magnetic field.
7 s=E*H1;
```

```
8 //result
9 disp(s, 'poynting vector is (meter square)=')
10 disp('which shows that power density is flowing in the direction of propagation.')
```

Scilab code Exa 2.6 program to compute propagation constant and other

```
1 // \text{ example:} -2.6, \text{page no.} -46.
2 // program to compute propagation constan, impedence,
     skin depth, reflection and transmission
      coefficient.
3 f=1*10^9;
4 omega=2*\%pi*f;
5 sigma=5.813*10^7; // for copper.
6 mue=4*%pi*10^-7; // permeability in free space.
7 delta=sqrt(2/(mue*sigma*omega)); // skin depth.
8 gama=((1+%i)/delta); //propagation constant.
9 eta=gama/sigma; // impedence
10 etao=377; //intrinsic impedence in free space.
11 tao=((eta-etao)/(eta+etao)); // reflection
      coefficient.
12 t=(2*eta)/(eta+etao); //transmission coefficient.
13 // result
14 disp(delta, 'skin depth in meter=')
15 disp(gama, 'propagation constant=')
16 disp(eta, 'intrinsic impedence in ohm=')
17 disp(tao, 'reflection coefficient=')
18 disp(t, 'transmission coefficient=')
```

Scilab code Exa 2.7 program to plot the reflection coefficients

```
1 // example: -2.7. page no. -50.
```

```
2 // program to plot the reflection coefficients for
      parallel and perpendicular polarized plane waves
      incident from free space on to a dielectric
      region with Er = 2.55, versus incidence angle.
3 \text{ Er} = 2.55;
             // relaitve permittivity of dielectric
     medium.
4 N1=377; // intrinsic impedence
5 N2=N1/sqrt(Er); // intrinsic impedence of
      dielectric medium.
6 xb=asin(sqrt(1/(1+1/2.55))); // brewster angle
      valid only in case of parallel polarization.
7 xt=acos(sqrt(1-(1/Er)^2*sin(xb))); // angle of
      transmission.
8 xi=[0:0.01:%pi/2]; // incidence angle.
9 // for parallel polarization
10 N2=N2*cos(xt);
11 N1 = N1 * \cos(xi);
12 Tpar = (N2 - N1) . / (N2 + N1);
13 w = abs(Tpar);
14 // result
15 subplot (1,2,1)
16 xtitle ("parallel polarization", "xi (incidence angle)"
      "Tpar(reflection coefficient,"),
17 plot2d(xi,w,style=3,rect=[0,0,%pi/2,1])
18 // for perpendicular polarization.
                                           //NOTE:-in
     case of this polarization there is no brewster
      angle.
19 xt = acos(sqrt(1-(1/Er)^2*sin(xi)));
20 n1=377.*cos(xt);
21 n2=(377/sqrt(Er)).*cos(xi);
22 Tper=(n2-n1)./(n1+n2);
23 z = abs(Tper);
24 / result
25 subplot (1,2,2)
26 xtitle ("perpendicular polarization", "xi (inxidence
      angle)", "Tper(reflection coefficient)")
27 plot2d(xi,z,style=2,rect=[0,0,%pi/2,1])
```

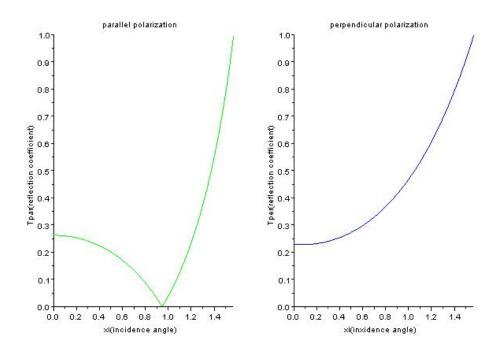


Figure 2.1: program to plot the reflection coefficients

Chapter 3

TRANSMISSION LINE THEORY

Scilab code Exa 3.1 program to determine transmission line parameters

```
1 // \text{example} : -3.1, \text{page no.} -72.
2 // program to determine transmission line parameters
3 syms E H Vo P a b Io mue y z Q pi L eipsila G C R Rs
4 E=(Vo/(P*log(b/a)))*exp(-%i*y*z); // in radial
      direction.
5 H=(Io/(2*pi*P))*exp(-\%i*y*z); // in phi direction.
6 \text{ H=H*conj(H)*P};
7 E=E*conj(E)*P;
8 L=(mue/((Io)^2))*integ(integ(H,P),Q); // surface
      integral in culindrical coordinate system
9 L=limit(L,P,b)-limit(L,P,a); // limits when
     integrated w.r.t rho.
10 L=limit(L,Q,2*pi)-limit(L,Q,0); // limits when
     integrated w.r.t phi.
11 C=(eipsila/(Vo^2))*integ(integ(E,P),Q); // surface
     integral in culindrical coordinate system
12 C=limit(C,P,b)-limit(C,P,a); // limits when
```

```
integrated w.r.t rho.
13 C=limit(C,Q,2*pi)-limit(C,Q,0); // limits when
     integrated w.r.t phi.
14 R=(Rs/(Io^2))*integ(H,Q);
15 R=limit(R,P,b)+limit(R,P,a);
16 R=limit(R,Q,2*pi)-limit(R,Q,0); // limits when
     integrated w.r.t phi.
17 G=((w*eipsila)/(Vo^2))*integ(integ(E,P),Q); //
      surface integral in culindrical coordinate system
18 G=limit(G,P,b)-limit(G,P,a); // limits when
     integrated w.r.t rho.
19 G=limit(G,Q,2*pi)-limit(G,Q,0); // limits when
     integrated w.r.t phi.
20 // result
21 disp(L, 'self-inductance in H/m = ')
22 disp(C, 'capacitance in F/m = ')
23 disp(R, 'resistance in Ohm/m = ')
24 disp(G, 'shunt conductance in S/m = ')
```

check Appendix AP 2 for dependency:

```
smith_chart_tao.sci
```

Scilab code Exa 3.2 program to find out load impedence

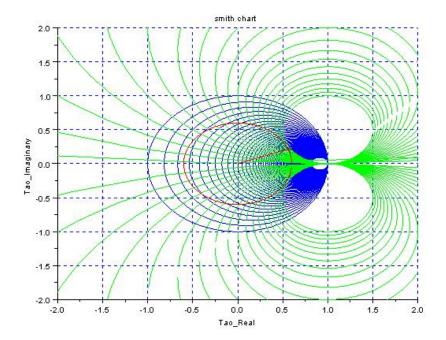


Figure 3.1: program to find out load impedence

11 // when analyse with the help of smith chart.see the angle from x=0 axis i.e Tao_real axis.if it is above this axis take angle anticlockwise and if it is below this axis.take angle clockwise from Tao_real axis below.

```
check Appendix AP 4 for dependency:
reflection_coefficient.sci
check Appendix AP 2 for dependency:
smith_chart_tao.sci
check Appendix AP 5 for dependency:
```

swr.sci

Scilab code Exa 3.3 program to find out return loss in dB and others

```
1 // example: -3.3, page no. -87.
2 // program to find out return loss in dB,SWR and
     reflection coefficient.
3 Z1=80-40*\%i; // load impedence.
4 Zo=50; // characteristic impedence.
5 z=Z1/Zo; // normalized impedence.
6 tao=reflection_coefficient(Z1,Zo);
7 SWR=VSWR(abs(tao));
8 R1=-20*\log 10 (abs(tao));
9 disp(abs(tao), 'reflection coefficient = ')
10 disp(SWR, 'standing wave ratio = ')
11 disp(Rl, 'return loss in dB = ')
12 smith_chart(tao)
13 // when analyse with the help of smith chart.see the
      angle from x=0 axis i.e Tao_real axis.if it is
     above this axis take angle anticlockwise and if
     it is below this axis.take angle clockwise from
     Tao_real axis below.
```

```
check Appendix AP 3 for dependency:
input_impedence.sci
check Appendix AP 4 for dependency:
reflection_coefficient.sci
check Appendix AP 5 for dependency:
swr.sci
```

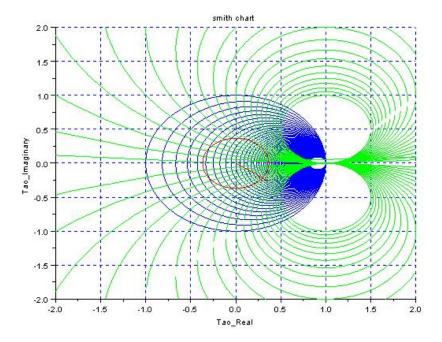


Figure 3.2: program to find out return loss in dB and others

Scilab code Exa 3.4 program to find input impedence and SWR of line

```
// example no.-3.4,page no.-88.
// program to find input impedence and SWR of line.
Co=75; Z1=37.5+75*%i; 1=0.02; eipsilar=2.56; f=3*10^9; c=3*10^8;
b=(2*%pi*f*sqrt(eipsilar))/c; // beta
tao=reflection_coefficient(Z1,Zo);
Zin=input_impedence(tao,b,1,Zo);
// result
disp(Zin, 'input impedence = ')
tao=abs(tao);
s=VSWR(tao);
// result
disp(s, 'SWR of the line = ')
```

Scilab code Exa 3.5 program to find out load admittance and other

```
// example: -3.5, page no. -91.
// program to find out load admittance and input
    admittance of the line
syms lamda;
Zl=100+50*%i;
Zo=50;
le=0.15; //electrical length(l/lamda).
b=(2*%pi);
tao=reflection_coefficient(Zl,Zo);
Zin=input_impedence(tao,b,le,Zo);
Yin=1/Zin;
Yl=1/Zl;
// result
disp(Yin, 'input admittance = ')
disp(Yl, 'load admittance = ')
```

Scilab code Exa 3.6 program to find out characteristic impedence

```
1 / \exp = -3.6, page no. -93.
2 // program to find out characteristic impedence and
      plot the magnitude of reflection coefficient
      versus normalized frequency.
3 Zl=100; // load impedence
4 Zi=50; //impedence of line which is to be matched
5 //as it is a quarter wave transformer so, Zi=(Zo)^2/
      z1;
6 Zo=sqrt(Zi*Z1);
7 disp(Zo, 'characteristic impedence of the matching
      section=')
8 syms f fo x;
9 x=f/fo;
10 x = 0:0.001:4;
11 y = (\%pi/2) * (x);
12 Zin=Zo*(((Z1*cos(y))+(Zo*%i*sin(y)))./((Zo*cos(y))+(Zo*%i*sin(y))).
     Z1*%i.*sin(y))))
13 tao=((Zin-Zo)./(Zin+Zo));
14 tao=abs(real(tao)+imag(tao));
15 plot2d(x,tao,style=6,rect=[0,0,4,1])
16 xtitle ("reflection coefficient versus normalized
      frequency for quarter wave transformer", "f/fo","
      tao (reflection coefficient)")
```

```
check Appendix AP 2 for dependency:
```

smith_chart_tao.sci

Scilab code Exa 3.7 program to determine unknown load impedence

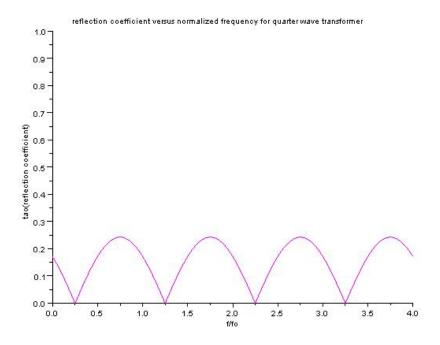


Figure 3.3: program to find out characteristic impedence

```
1 // example: -3.7, page no. -101.
2 // NOTE: - this example is a method for calculating
     unknown load impedence of slotted line section.
      all data are given and preassumed.
3 // program to determine unknown load impedence.
4 Z1=0; Zo=50; // for short circuitting the load.
5 SWR=%inf;
6 // short circuit is removed and replace with unknown
      load.
7 SWR=1.5; lamda=0.04;
8 \quad lmin=4.2-2.72;
9 tao=(1.5-1)/(1.5+1);
10 theta=(\%pi+((4*\%pi)/4)*1.48);
11 tao=abs(tao)*exp(%i*theta);
12 Z1=50*((1+tao)/(1-tao));
13 // result
14 disp(Z1, 'load impedence = ')
15 smith_chart(tao)
16 // when analyse with the help of smith chart.see the
       angle from x=0 axis i.e Tao_real axis.if it is
     above this axis take angle anticlockwise and if
      it is below this axis.take angle clockwise from
      Tao_real axis below.
```

Scilab code Exa 3.8 program to calculate attenuation constant

```
1 // example: -3.8, page no. -108.
2 // program to calculate attenuation constant.
3 syms alpha R Rs L G C eta a b w pi eipsila eipsilac mue eta;
4 // from example 3.1: -alpha=(R*(sqrt(C/L)+G*sqrt(L/C));
5 eta=sqrt(mue/eipsila);
```

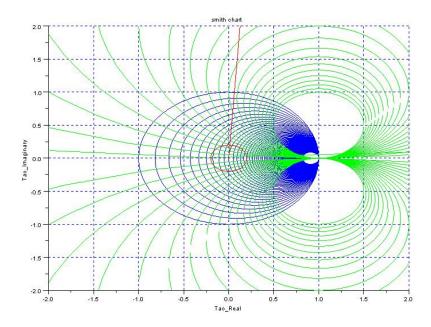


Figure 3.4: program to determine unknown load impedence

```
6 L=(mue/(2*pi))*(log(b/a));
7 C=(2*pi*eipsila)/log(b/a);
8 R=(Rs/(2*pi))*((1/a)+(1/b));
9 G=(2*pi*w*eipsilac)/log(b/a);
10 alpha=(1/2)*(R*sqrt(C/L)+G*sqrt(L/C));
11 disp(alpha, 'attenuation constant = ')
```

Scilab code Exa 3.9 program to find the attenuation constant

```
1 // \text{ example:} -3.9, \text{page no.} -111.
2 // program to find ht eattenuation constant of
      coaxial line.
3 syms E H Vo Zo P a b B z pi Po Q Rs Plc alpha Pld
     Plc w eipsila;
4 //Zo = (eta/(2*pi))*log(b/a);
5 E=(Vo/(P*(log(b)-log(a))))*exp(-%i*B*z);
                                              //B=beta.
6 H=(Vo/(2*pi*P*Zo))*exp(-\%i*B*z);
7 H=conj(H)*P; // for defining E cross H*.
8 Po=(1/2)*integ(integ((E*H),P),Q);
9 Po=limit(Po,P,b)-limit(Po,P,a);
10 Po=limit(Po,Q,2*pi)-limit(Po,Q,0);
11 disp(Po, 'power flowing on the lossless line = ')
12 H=(H*conj(H))/P; // for defining |H|^2;
13 Plc=(Rs/2)*integ(integ(H,z),Q);
14 Plc=limit(Plc,P,b)+limit(Plc,P,a);
15 Plc=limit(Plc,z,1)-limit(Plc,z,0);
16 Plc=limit(Plc,Q,2*pi)-limit(Plc,Q,0);
17 disp(Plc, 'conductor loss = ')
18 E=E*conj(E)*P;
19 Pld=((w*eipsila)/2)*integ(integ(E,P),Q),z);
20 Pld=limit(Pld,P,b)-limit(Pld,P,a);
21 Pld=limit(Pld,z,1)-limit(Pld,z,0);
22 Pld=limit(Pld,Q,2*pi)-limit(Pld,Q,0);
23 disp(Pld, 'dielectric loss = ')
24 alpha=(Pld+Plc)/(2*Po); // attenuation constant.
```

Scilab code Exa 3.10 program to calculate attenuaton

```
// example: -3.10, page no. -114.
// program to calculate attenuaton due to conductor
    loss of a coaxial line using incremental
    inductance rule.
syms Zo eta pi a b Rs l alpha alpha_c alpha_dash
    delta alpha_c_dash sigma w mue;

sd=sqrt(2/(w*mue*sigma))
Zo=(eta*log(b/a))/(2*pi);
alpha_c=(Rs/(4*Zo*pi^2))*(diff(log(b/a),b)-diff(log(b/a),a));
disp(alpha_c, 'attenuation due to conductor loss = ')
alpha_c_dash=alpha_c*(1+((2/pi)*atan((1.4*delta)/sd)));
disp(alpha_c_dash, 'attenuation corrected for surface roughness = ')
```

Chapter 4

TRANSMISSION LINE AND WAVEGUIDES

Scilab code Exa 4.1 program to find the cut off frequency

```
1 // \text{ example:} -4.1, \text{page no.} -148.
2 // program to find the cut off frequency fo the
      first four propagating modes.
3 a=0.02286; b=0.01016; f=10*10^9; k=209.44; sigma
      =5.8*10^7; mue=4*%pi*10^-7;
4 c=3*10^8;
5 m=0; n=1;
6 fc=(c/(\%pi*2))*sqrt(((\%pi*m)/a)^2+((\%pi*n)/b)^2);
7 fc=fc/(10^9);
8 disp(fc, 'cut-off frequency for TE01 mode in GHZ=')
9 m=1; n=0;
10 fc=(c/(\%pi*2))*sqrt(((\%pi*m)/a)^2+((\%pi*n)/b)^2);
11 fc=fc/(10^9);
12 disp(fc, 'cut-off frequency for TE10 mode in GHZ=')
13 m=2; n=0;
14 fc=(c/(\%pi*2))*sqrt(((\%pi*m)/a)^2+((\%pi*n)/b)^2);
15 fc=fc/(10<sup>9</sup>);
16 disp(fc, 'cut-off frequency for TE20 mode in GHZ=')
17 m=1; n=1;
```

```
18 fc=(c/(%pi*2))*sqrt(((%pi*m)/a)^2+((%pi*n)/b)^2);
19 fc=fc/(10^9);
20 disp(fc,'cut-off frequency for TE11 mode in GHZ=')
21 B=sqrt(k^2-(%pi/a)^2) // for TE10 mode
22 Rs=sqrt(((2*%pi*f)*mue)/(2*sigma)); // surface
    resistance.
23 disp(Rs,'surface resistance in ohm=')
24 ac=(Rs/(a^3*b*B*k*377))*((2*b*%pi^2)+(a^3*k^2)) //
    attenuation constant.
25 ac=-20*(-ac)*log10(%e);
26 disp(ac,'attenuation constant in dB/m=')
```

Scilab code Exa 4.2 program to find the cut off frequency

```
1 // \text{example}: -4.2, \text{page no.} -160.
2 //program to find the cut off frequency of two
      propagating modes of a circular waveguide.
3 = 0.005; eipsilar = 2.25; f = 13 * 10^9; c = 3 * 10^8; d = 0.001;
      sigma=6.17*01^7; muo=4*%pi*10^-7;
4 m=1; n=1;
5 p11=1.841; p01=2.405;
6 fc=(p11*c)/(2*%pi*a*sqrt(eipsilar));
7 kc=p11/a;
8 \text{ fc=fc/(10^9)};
9 disp(fc, 'cut-off frequency for TE11 mode in GHZ')
10 m=0; n=1;
11 fc=(p01*c)/(2*%pi*a*sqrt(eipsilar));
12 fc=fc/(10^9);
13 disp(fc, 'cut-off frequency for TE01 mode in GHZ')
14 // so, TE01 can't be propagating mode. only TE11 will
15 k=(2*%pi*f*sqrt(eipsilar))/c;
16 disp(k, 'k in m-1=')
17 B = sqrt(k^2-kc^2);
18 disp(B, 'propagation constant of TE11 mode')
```

```
19 ac=(k^2*d)/(2*B);
20 Rs=sqrt((2*%pi*f*muo)/(2*sigma)); // surface
    resistance.
21 acm=(Rs/(a*k*377*B))*(kc^2+((k^2)/(p11^2-1)));
22 a=ac+acm;
23 a=-20*(-0.547*0.5)*log10(%e);
24 disp(a,'total attenuation factor in dB=')
```

Scilab code Exa 4.3 program to find out the highest usable frequency

```
//example:-4.3,page no.-167.
//program to find out the highest usable frequency.
a=0.000889;b=0.0029464;eipsilar=2.2;c=3*10^8;
// here (b/a)=3.3,so for this kc*a=0.47
kc=0.47/a;
fc=(c*kc)/(2*%pi*sqrt(eipsilar))
fc=fc/(10^9);
fmax=0.95*fc;
disp(fmax, 'maximum usable frequency in GHZ=')
```

Scilab code Exa 4.4 program to calculate and plot propagation constant

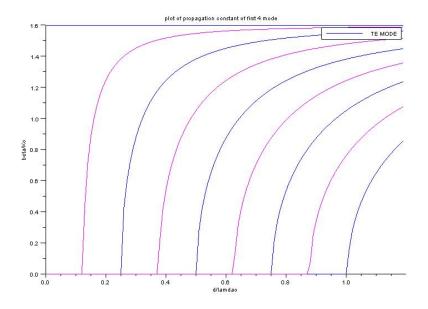


Figure 4.1: program to calculate and plot propagation constant

Scilab code Exa 4.5 program to find width of a copper strip line

```
1 // \text{ example:} -4.5, \text{page no.} -180.
```

```
2 // program to find width of a copper strip line
      conductor.
3 eipsilar=2.20; Zo=50; b=0.0032; d=0.001, f=10^10; t
      =0.00001;
4 c=3*10^8; Rs=0.026; A=4.74;
5 x=(30*\%pi)/(sqrt(eipsilar)*Zo);
6 x = x - 0.441;
7 w=b*x;
8 if ((sqrt(eipsilar)*Zo)<120)</pre>
       disp("width of copper strip line conductor is
          0.00266m")
11 K=(2*%pi*f*sqrt(eipsilar))/c;
12 ad=(K*d)/2;
13 ac = (2.7*(10^-3)*Rs*eipsilar*Zo*A)/(30*%pi*(b-t));
14 \text{ a=ac+ad};
15 \ a=20*a*log10(%e);
16 lamda=c/(sqrt(eipsilar)*f);
17 alamda=lamda*a;
18 disp(K, 'wave number=')
19 disp(ad, 'dielectric aattenuation=')
20 disp(ac, 'conductor attenuation=')
21 disp(a, 'total attenuation constant=')
22 disp(alamda, 'attenuation in dB/lamda=')
```

Scilab code Exa 4.7 program to calculate width and length

```
1 //example: -4.7, page no. -187.
2 //program to calculate the width and length of microstrip line.
3 eipsilae=1.87; // effective dielectric constant.
4 Zo=50; q=%pi/2; c=3*10^8;
5 f=2.5*10^9;
6 ko=(2*%pi*f)/c;
7 d=0.00127;
```

```
8 eipsilar=2.20;
9 // for w/d>2;
10 B=7.985;
11 w=3.081*d*100;
12 disp(w,'width in centi meter=')
13 l=(q*100)/(sqrt(eipsilae)*ko);
14 disp(1,'length of microstrip in centi meter=')
```

Scilab code Exa 4.9 program to calculate the group velocity

```
1 // \text{example}: -4.9, \text{page no.} -197.
2 //program to calculate the group velocity.
3 syms w c v;
4 B = sym('B');
5 \text{ ko=sym('ko')};
6 kc=sym('kc');
7 ko=w/c;
8 B = sqrt(ko^2-kc^2);
9 \text{ v=diff}(B,w);
10 vg=v^{(-1)};
11 vg=(c*B)/ko;
12 vp=w/B;
13 disp(vg, 'group velocity=')
14 disp(vp, 'phase velocity=')
15 disp('conclusion:-since B<ko, we have that vg<c<vp,
      which indicates that the phase velocity of a
      waveguide mode may be greater than the speed of
      light.but the group velocity will be lesser than
      the speed of light.')
```

Chapter 5

MICROWAVE NETWORK ANALYSIS

Scilab code Exa 5.1 program to find equivalent voltages and current

```
// example: -5.1, page no. -209.
//program to find the equivalent voltages and current.
syms a b A Zte V I C1 C2 P;
P=(a*b*A^2)/(4*Zte);
c=(1/2)*V*I;
d=(1/2)*(A^2)*C1*C2;
C1=sqrt((a*b)/2); // on comparision.
C2=sqrt((a*b)/2)*Zte; // on comparision.
c=[C1 C2];
disp(c)
disp(c)
disp(c)
disp(c) TE10 mode.")
```

Scilab code Exa 5.2 program to compute reflection coefficient

```
1 // \text{example} : -5.2, \text{page no.} -212.
2 //program to compute reflection coefficient.
3 = 0.03485; b=0.01580; eipsilao=8.854*10^-12; muo=4*%pi
      *10^-7;
4 f=4.5*10^9;
5 w=2*%pi*f; // angular frequency.
6 //  for z<0 region air filled.
7 eipsilar=2.56; // for z>0 region.
8 ko=w*sqrt(muo*eipsilao);
9 k=ko*sqrt(eipsilar);
10 Ba=sqrt(ko^2-(%pi/a)^2); // propagation constant in
      air region z < 0.
11 Bd=sqrt(k^2-(%pi/a)^2); // propagation constant in
      dielectric region z>0.
12 Zoa=(ko*377)/Ba;
13 Zod = (ko*377)/Bd;
14 tao=(Zod-Zoa)/(Zod+Zoa);
15 disp(tao, 'reflection coefficient')
```

Scilab code Exa 5.3 program to find z parameter of two port network

```
1 //example: -5.3, page no. -220.
2 // program to find the z parameter of the two port network.
3 syms Z11 Z12 Z22 Z21 V1 I1 V2 I2 Za Zb Zc;
4 Z11=Za+Zc; // for I2=0.
5 Z12=(Zc/(Zb+Zc))*(Zb+Zc); // for I1=0.
6 Z21=(Zc/(Za+Zc))*(Za+Zc); // for I2=0.
7 Z22=Zb+Zc; // for I1=0.
8 Z=[Z11 Z12; Z21 Z22]; // z-parameter matrix.
9 disp(Z, 'Z-parameter of two port network = ')
```

Scilab code Exa 5.4 program to find the s parameter of 3 dB attenuator

```
1 // example: -5.4, page no. -221.
2 // program to find the s-parameter of 3-dB
    attenuator circuit.
3 \quad Za=8.56; Zb=8.56, Zc=141.8; Zo=50;
Zc)/(Zo+Zb+Zc))+Za)+Zo); // reflection
    coefficient seen at port 1.
Zc)/(Zo+Za+Zc))+Zb)+Zo); // reflection
    coefficient seen at port 2.
6 S12=(((1/((((Zo+Za)*Zc)/(Zo+Za+Zc))+Zb))*(((Zo+Za)*
    Zc)/(Zo+Za+Zc)))*(Zo/(Zo+Za))); // transmission
    coefficient from port 2 to 1.
7 S21 = (((1/((((Zo+Zb)*Zc)/(Zo+Zb+Zc))+Za))*(((Zo+Zb)*
    Zc)/(Zo+Zb+Zc)))*(Zo/(Zo+Zb))); // transmission
    coefficient from port 1 to 2.
8 S=[S11 S12;S21 S22]; // s-parameter matrix.
9 disp(S, 'S-parameter of 3-db attenuator circuit is ='
    )
```

Scilab code Exa 5.5 program to determine reciprocity and losslessness

```
//example: -5.5, page no. -226.
//program to determine the reciprocity and lossless
    of two port network and find return loss.

syms S Rl tao;
S=[0.1 0.8*%i;0.8*%i 0.2]; // s-parameter matrix.

if (S(1,2)==S(2,1))
disp("the network is reciprocal.")
else
disp("the network is not reciprocal.")
end
if (S(1,1)^2+S(1,2)^2==1)
disp("the network is lossless.")
else
```

Scilab code Exa 5.6 program to find ABCD parameter of two port network

```
1  // example: -5.6, page no. -232.
2  // program to find the ABCD parameter of a two-port network.
3  syms A B C D V1 V2 I1 I2 Z;
4  //A=V1/V2;  // for i2=0;
5  A=1;
6  B=V1/(V1/Z);
7  C=0;
8  D=I1/I1;
9  ABCD=[A B; C D];
10  // result
11 disp(ABCD, 'abcd parameter')
```

Scilab code Exa 5.7 program to find admittance matrix for bridge T

```
7 Ya=1/Za;
8 Y=Ya+Yb;
9 D=((Z2+Z1)^2-Z2^2);
10 // result
11 disp(Y, 'admittance matrix for bridge-T network=')
```

Scilab code Exa 5.8 program to compute power gains

```
1 // example: -5.8, page no. -243.
2 //program to compute power gains.
3 f=10^10; Zs=20; Zl=30; Zo=50;
4 S = [-0.39 + \%i * 0.225 \ 0.009848 + \%i * -0.001736; 2.02 + 0.356 *
     \%i -0.3464 - \%i *0.2;
5 taos=(Zs-Zo)/(Zs+Zo);
6 taol=(Z1-Zo)/(Z1+Zo);
7 taoin=S(1,1)+((S(1,2)*S(2,1)*taol)/(1-S(2,2)*taol));
8 taoout=S(2,2)+((S(1,2)*S(2,1)*taos)/(1-S(1,1)*taos))
9 Ga=(abs(S(2,1)^2)*(1-abs(taos)^2))/((abs(1-S(1,1)*))
     taos)^2)*(1-abs(taoout)^2));
10 Gt = (abs(S(2,1)^2)*(1-abs(taos)^2)*(1-abs(taol)^2))
     /((abs(1-S(2,2)*taol)^2)*abs(1-taos*taoin)^2);
11 G=(abs(S(2,1)^2)*(1-abs(taol)^2))/((abs(1-S(2,2)*
     taol)^2)*(1-abs(taoin)^2));
12 disp(G, 'actual power gain=')
13 disp(Ga, 'the available power gain=')
14 disp(Gt, 'the transducer power gain=')
15 disp(taoin, 'reflection coefficient looking at port
     1 = '
16 disp(taoout, 'reflection coefficient looking at port
17 disp(taos, 'reflection coefficient at the source=')
18 disp(taol, 'reflection coefficient at the load=')
```

Scilab code Exa 5.9 program to derive the expression for taoin

```
// example: -5.9, page no. -248.
// program to derive the expression for taoin.
syms S S11 S22 S12 S21 taol taoin a1 a2 b1 b2 a b;

S=[S11 S12; S21 S22];
b=[b1; b2];
a=[a1; a2];
b=S*a;
disp(b)
//so, S11 will be the reflection coefficient i.e taoin.
taoin=S11+((S21*S12*taol)/(1-S22*taol));
// result
disp(taoin, 'the expression for taoin will be=')
```

Scilab code Exa 5.10 program to find out expression for taoin

```
1  // example: -5.10.page no. -250.
2  //program to find out expression for taoin.
3  syms P1 P2 S11 S22 S12 S21 taol taoin L1 12;
4  P1=S11;  // path one.
5  P2=S21*S12*taol;  //path second.
6  L1=taol*S22;  // loop gain for path 1.
7  L2=L1^2;  // loop gain taking two at a time.(but only one loop wiil exist.i.e=L1.)
8  L2=0;
9  // from mason's gain formula.
10 taoin=(S11*(1-taol*S22)+(S21*taol*S12))/(1-taol*S22);
11  // result
12  disp(taoin)
```

Scilab code Exa 5.11 determine amplitude of forward and backward wave

```
1 // example: -5.11, page no. -264.
2 // program to determine the amplitude of the forward
      and backward travelling TE10 modes and the input
       resistance.
3 syms Io a b x y z h1 e1 J P1 A1p A1m pi Z1 delta b1
     j P Rin;
4 e1=sin(pi*x/a); // in y direction.
5 h1=-\sin(pi*x/a)/Z1; // in z direction.
6 P1=(2/Z1)*integ(integ(sin(pi*x/a)^2,x),y);
7 P1=limit(P1,x,a)-limit(P1,x,0);
8 P1=limit(P1,y,b)-limit(P1,y,0);
9 // taking \sin(2*\text{pi})=0. we get,
10 P1=a*b/Z1;
11 Alp=(-1/P1)*Io*y; // as for x, it will be one at x=a
     /2 and 1 for z at z=0;
12 A1p=limit(A1p,y,b)-limit(A1p,y,0);
13 A1m = (-1/P1)*Io*y; // as for x, it will be one at x=a
     /2 and 1 for z at z=0;
14 A1m=limit(A1m,y,b)-limit(A1m,y,0);
15 P=integ(integ(((A1p^2)/Z1)*sin(pi*x/a)^2,x),y);
16 P=limit(P,x,a)-limit(P,x,0);
17 P=limit(P,y,b)-limit(P,y,0);
18 // taking \sin(2*pi)=0. we get,
19 P=(b*(Io^2)*Z1*pi)/(2*a*pi);
20 Rin=2*P/(Io^2);
21 disp(A1p, amplitude of the forward travelling wave =
22 disp(A1m, 'amplitude of the backward travelling wave
23 disp(Rin, 'input resistance seen by the probe = ')
```

Scilab code Exa 5.12 find excitation coefficient of forward wave TE10

```
1 // \text{ example}: -5.12, \text{page no.} -265.
2 // program to find the excitation coefficient of the
      forward travelling TE10 mode.
3 syms M Pm uo w j a b Io x y z ro pi Z1 h1 A1p P1 no
     ko uo eo;
4 ko=w*sqrt(uo*eo);
5 no=sqrt(uo/eo);
6 h1=sin(pi*x/a)*(-1/Z1); // in x direction.
7 P1=(2/Z1)*integ(integ(sin(pi*x/a)^2,x),y);
8 P1=limit(P1,x,a)-limit(P1,x,0);
9 P1=limit(P1,y,b)-limit(P1,y,0);
10 // taking \sin(2*pi) = 0. we get,
11 P1=a*b/Z1;
12 Pm=Io*pi*(ro^2); // defined at x=a/2, y=b/2 and z=0;
13 M = j*w*uo*Pm;
14 Alp=(1/P1)*(-(1/Z1)*M);
15 disp(A1p, 'the forward wave excitation coefficient
      will be = ')
16 disp("!! NOTE:-replace w=sqrt(uo*eo) and no=sqrt(uo/
      eo), the answer will match!!")
17 disp(" NOTE: - on integrating, x component will
      become one at x=a/2, y component will become one
      at y=b/2 and z component will become one at z=0."
```

Chapter 6

IMPEDENCE MATCHING AND TUNNING

Scilab code Exa 6.1 program to design an L section matching network

```
1 // \text{ example:} -6.1, \text{page no.} -284.
2 // program to design an L section matching network
      to match a series RC load.
3 Z1=200-%i*100; // load impedence.
4 R1=200; X1=-100; f=500*10^6; Zo=100;
5 B1 = (X1 + sqrt(R1/Zo) * sqrt(R1^2 + X1^2 - (R1 * Zo)))/(R1^2 + X1
      ^2);
6 B2=(X1-sqrt(R1/Zo)*sqrt(R1^2+X1^2-(R1*Zo)))/(R1^2+X1
7 C1=(B1/(2*\%pi*f))*10^12;
8 L2=(-1/(B2*2*\%pi*f))*10^9;
9 X1 = (1/B1) + ((X1*Zo)/R1) - (Zo/(B1*R1));
10 X2=(1/B2)+((X1*Zo)/R1)-(Zo/(B2*R1));
11 L1=(X1/(2*%pi*f))*10^9;
12 C2=(-1/(X2*2*\%pi*f))*10^12;
13 disp(L1, 'inductor of first circuit in nH = ')
14 disp(C1, 'capacitor of the first circuit in pF = ')
15 disp(L2, 'inductor of second circuit in nH = ')
16 disp(C2, 'capacitor of the second circuit in pF = ')
```

17 disp("NOTE:-for above specific problem Rl>Zo, positive X implies inductor, negative X implies capacitor, positive B implies capacitor and negative B implies inductor.")

Scilab code Exa 6.5 design quarter wave matching transformer

```
//example:-6.5,page no.-304.
//program to design a single section quarter wave
    matching transformer.

Zl=10; // load impedence.

Zo=50; // characteristic impedence.

fo=3*10^9;swr=1.5; // maximum limit of swr.

Zl=sqrt(Zo*Zl); // characteristic impedence of the
    matching section.

taom=(swr-1)/(swr+1);

frac_bw=2-(4/%pi)*acos((taom/sqrt(1-taom^2))*(2*sqrt
    (Zo*Zl)/abs(Zl-Zo))); // fractional bandwidth.

disp(Zl, 'charecteristic impedence of matching
    section = ')

disp(frac_bw, 'fractional bandwidth = ')
```

Scilab code Exa 6.6 program to evaluate the worst case percent error

```
1 // example: -6.6, page no. -307.
2 // program to evaluate the worst case percent error in computing magnitude of reflection coefficient.
3 Z1=100; Z2=150; Z1=225;
4 tao_1=(Z2-Z1)/(Z2+Z1);
5 tao_2=(Z1-Z2)/(Z1+Z2);
6 tao_exact=(tao_1+tao_2)/(1+tao_1*tao_2); // this results as angle is taken zero.
```

Scilab code Exa 6.7 design three section binomial transformer

```
1 // example: -6.7, page no. -312.
2 // program to design three section binomial
      transformer.
3 \quad Z1=50; Zo=100; N=3; taom=0.05;
4 A = (2^-N) * abs((Z1-Zo)/(Z1+Zo));
5 frac_bw=2-(4/\%pi)*acos(0.5*(taom/A)^2);
6 \text{ for } c=1
     Z1=Zo*((Z1/Zo)^((2^-N)*(c^N)));
8 \text{ disp}(Z1, 'Z1 = ')
9 end
10 for c=3^(1/3)
     Z2=Z1*((Z1/Zo)^((2^-N)*(c^N)));
11
     disp(Z2, `Z2 = `)
12
13 end
14 for c=3^(1/3)
     Z3=Z2*((Z1/Zo)^((2^-N)*(c^N)));
     disp(Z3, 'Z3 = ')
16
17 \text{ end}
```

Scilab code Exa 6.8 design three section chebysev transfomer

```
1 // example: -6.8, page no. -316.
2 // program to design a three section chebysev transformer.
```

```
3 Zl=100; Zo=50; taom=0.05; N=3; A=0.05;
4 thetam=asec(cosh((1/N)*acosh((1/taom)*abs((Zl-Zo)/(Zl+Zo)))))*(180/%pi);
5 x=(cosh((1/N)*acosh((1/taom)*abs((Zl-Zo)/(Zl+Zo)))))
6 tao_o=A*(x^3)/2;
7 tao_l=(3*A*(x^3-x))/2; // from symmetry tao_3=tao_0;
8 Zl=Zo*((1+tao_o)/(1-tao_o));
9 Z2=Zl*((1+tao_l)/(1-tao_l));
10 Z3=Zl*((1-tao_o)/(1+tao_o));
11 disp(Zl,Z2,Z3, 'the characteristic impedences are = ')
```

Scilab code Exa 6.9 design triangular taper and a klopfenstein taper

Chapter 7

MICROWAVE RESONATORS

Scilab code Exa 7.1 program to compare the Q factor

```
1 // example: -7.1, page no. -339.
2 //program to compare the Q of an air filled and
     teflon filled coaxial line resonator.
3 sigma=5.813*10^7; muo=4*\%pi*10^-7; f=5*10^9; eta=377; a
     =1*10^-3; b=4*10^-3;
4 omega=2*\%pi*f; ko=104.7; B=104.7; alpha=0.022;
5 Rs=sqrt((omega*muo)/(2*sigma));
6 alphaca=(Rs/(2*eta*log(b/a)))*((1/a)+(1/b)); //
     attenuation due to conductor loss for air filled
     line.
7 eipsilar=2.08; tandelta=0.0004; // for teflon filled
      line.
8 alphact=((Rs*sqrt(2.08)*0.01)/(2*eta*log(b/a)))*((1/a)
     a)+(1/b)); // attenuation due to conductor loss
     for teflon filled line.
9 alphada=0; // for air filled line.
10 alphadt=ko*(sqrt(eipsilar)/2)*tandelta;
11 Qair=B/(2*alpha);
12 B=B*sqrt(eipsilar);
13 alpha=0.062;
14 Qteflon=B/(2*alpha);
```

Scilab code Exa 7.2 program to compute length and Q of the resonator

```
1 // \text{example} : -7.2, page no. -342.
2 // program to compute the length of the line for
      resonance at 5 GHZ and the Q of the resonator.
3 \text{ W=0.0049; c=3*10^8; f=5*10^9; Zo=50; eipsilar=2.2; ko}
      =104.7; tandelta=0.001;
4 Rs=0.0184; // taken from example 7.1.
5 eipsilae=1.87; // effective permittivity.
6 l=c/(2*f*sqrt(eipsilae)); // resonator length.
7 B=(2*%pi*f*sqrt(eipsilae))/c;
8 alphac=Rs/(Zo*W);
9 alphad=(ko*eipsilar*(eipsilae-1)*tandelta)/(2*sqrt(
      eipsilae)*(eipsilar-1));
10 alpha=alphac+alphad;
11 Q=B/(2*alpha);
12 disp(1, 'length of the line in meter = ')
13 disp(Q, 'Q of the resonator = ')
```

Scilab code Exa 7.3 program to find required length and other

```
1 // example: -7.3, page no. -347.
2 // program to find required length, d and Q for l=1
    and l=2 resonator mode.
3 a=0.04755; b=0.02215; eipsilar=2.25; tandelta=0.0004; f
    =5*10^9; c=3*10^8;
4 k=(2*%pi*f*sqrt(eipsilar))/c // wave number.
5 for l=1:1:2
```

```
6 d=(1*%pi)/sqrt((k^2)-((%pi/b)^2)); // m=1 & n=0 mode
    .
7 disp(d, 'd in meter = ')
8 end
9 eta=377/sqrt(eipsilar);
10 Qc1=3380; // l=1.
11 Qc2=3864; // l=2.
12 Qd=2500; // Q due to dielectric loss only.
13 Q1=((1/Qc1)+(1/Qd))^-1; // for l=1.
14 Q2=((1/Qc2)+(1/Qd))^-1; // for l=2.
15 disp(Q1, 'Q1 = ');
16 disp(Q2, 'Q2 = ')
```

Scilab code Exa 7.4 program to find dimension and Q

```
1 // \text{example} : -7.4, \text{page no.} -353.
2 // program to find dimension and Q;
3 f=5*10^9; c=3*10^8; p01=3.832; sigma=5.813*10^7; muo=4*
      %pi *10^-7;
4 eipsilar=2.25;
5 // \text{ mode TE011.} and d=2a.
6 omega=2*\%pi*f;
7 eta=377;
8 lamda=c/f;
9 k=(2*\%pi)/lamda;
10 // f = (c/(2*\%pi))*sqrt((p01/a)^2+(\%pi/(2*a))^2); as d
      =2a given
11 a = sqrt((p01)^2 + (%pi/2)^2)/k;
12 Rs=sqrt((omega*muo)/(2*sigma))
13 Qc=(k*a*eta)/(2*Rs); // for m=l=1, n=0 and d=2a.
14 disp(a, 'a in meter = ')
15 \text{ disp}(Qc, 'Qc = ')
```

Scilab code Exa 7.5 program to find resonant frequency and Q

```
//example: -7.5, page no. -358.
// program to find the resonant frequency and Q for TE01delta mode.
delta=0.001; eipsilar=95; a=0.413; L=0.008255; c=3*10^8;
//tan((B*L)/2)=alpha/beta.
//ko=(2*%pi*f)/c;
alpha=sqrt((2.405/a)^2-(ko)^2);
B=sqrt((eipsilar*(ko)^2)-(2.405/a)^2); // beta
f1=((c*2.405)/(2*%pi*sqrt(eipsilar)*a))*10^-7;
f2=((c*2.405)/(2*%pi*a))*10^-7;
disp(f1, 'f1 in GHZ = ')
disp(f2, 'f2 in GHZ = ')
Q=1/tan(delta);
disp(Q, 'approx. value of Q due to dielectric loss = ')
```

Scilab code Exa 7.6 program to find the mode number and Q

```
1 // example: -7.6, page no. -361.
2 // program to find the mode number and Q of given resonator.
3 fo=94*10^9; d=0.04; c=3*10^8; muo=4*%pi*10^-7; sigma =5.813*10^7;
4 l=(2*d*fo)/c; // mode number.
5 Rs=sqrt((2*%pi*fo*muo)/(2*sigma));
6 Q=(%pi*1*377)/(4*Rs);
7 disp(1, 'mode number = ')
8 disp(Q, 'Q = ')
```

Scilab code Exa 7.7 program to find value of the coupling capacitor

```
1 // example: -7.7, page no. -367.
2 // program to find the value of the coupling
      capacitor required for critical coupling.
3 1=0.02175; Zo=50; eipsilae=1.9; c=3*10^8;
4 fo=c/(2*1*sqrt(eipsilae)); // first resonant
      frequency will occur when the resonator ia about
      l=lamdag/2 in length.
5 lamdag=c/fo;
6 alpha=1/8.7; // in Np/m.
7 Q=%pi/(2*1*alpha);
8 bc=sqrt(%pi/(2*Q));
9 C=bc/(2*%pi*fo*Zo)*10^12;
10 disp(C, 'coupling capacitor in pF = ')
11 C=bc/(2*\%pi*fo*Zo);
12 w1=atan(2*\%pi*fo*C*Zo)*c/(1*sqrt(eipsilae)); //
     from equation tan(B*l) = -bc;
13 w1 = w1 * 10^- - 8;
14 disp(w1, 'frequency in GHZ = ')
```

Scilab code Exa 7.8 derive expression for change in resonant frequency

```
// example: -7.8, page no. -373.
// program to derive an expression for the change in resonant frequency.
syms Ey Hx Hz A Zte n a pi x z d j k t y er eo c wo w b;
Ey=A*sin((pi*x)/a)*sin((pi*z)/d);
Hx=((-j*A)/Zte)*sin((pi*x)/a)*cos((pi*z)/d);
Hz=((j*pi*A)/(k*n*a))*cos((pi*x)/a)*sin((pi*z)/d);
Ey=Ey^2;
//c=(er-1)*eo;
w=c*integ(integ(integ(Ey,z),y),x);
w=limit(w,z,d)-limit(w,z,0);
w=limit(w,y,t)-limit(w,y,0);
w=limit(w,x,a)-limit(w,x,0);
```

```
disp(w)
// as sin(2*pi)=0; then last term of above result
    will be:-

w=(c*A^2*a*t*d)/4;
disp(w,'on taking sin(2*pi)=0 , w becomes = ')
w=((a*b*d*eo)/2)*A^2;
deltaw=(w-wo)/wo;
disp(deltaw,'fractional change in resonant frequency = ')
```

Scilab code Exa 7.9 derive expression for change in resonant frequency

```
1 // example: -7.9, page no. -376.
2 // program to derive an expression for the change in
      resonant frequency.
3 syms Ey Hx Hz A Zte n a pi x z d j eo c wo w b l ro;
4 Ey=A*\sin((pi*x)/a)*\sin((pi*z)/d);
5 Hx=((-j*A)/Zte)*sin((pi*x)/a)*cos((pi*z)/d);
6 Hz=((j*pi*A)/(k*n*a))*cos((pi*x)/a)*sin((pi*z)/d);
7 Ey=A;// at x=a/2,y,z=d/2;
8 Hx = 0; // at x=a/2, y, z=d/2;
9 Hz=0; // at x=a/2, y, z=d/2;
10 //where w is perturbed resonant frequency and wo is
     unperturbed resonant frequency.
11 w = -eo * A^2 * pi * l * ro^2;
12 wo=(a*b*eo*d*A^2)/2;
13 deltaw=(w-wo)/wo;
14 disp(deltaw, 'the perturbation in resonant frequency
     w.r.t wo = ')
```

Chapter 8

POWER DIVIDERS DIRECTIONAL COUPLERS AND HYBRIDS

check Appendix AP 1 for dependency:

parallel_impedence.sce

Scilab code Exa 8.1 program to compute the reflection coefficients

```
// example: -8.1, page no. -392.
// program to compute the reflection coefficients seen looking in to the output port.
// as the power is divided in to 2:1 ratio. and Pin = (1/2)*Vo^2/Zo;
// so,P1=(1/3)*Pin; and P2=(2/3)*Pin ...........(i)
Zo=50;
Z1=3*Zo; // from above condition ...........(i)
Z2=(3/2)*Zo;
Zin=parallel_impedence(Z1,Z2); // input impedence to the junction.
if Zin==Zo
disp("input is matched to the 50 ohm sources")
```

Scilab code Exa 8.2 design equi split wilkinson power divider

```
// example: -8.2, page no. -398.
// program to design an equi-split wilkinson power divider for 50 ohm system impedence.

Zo=50;
Z=sqrt(2)*Zo; // impedence of quarter wave transmission line.
R=2*Zo; // shunt resistor.
disp(R, 'the shunt resistance value should be in ohm = ')
disp(Z, 'the quarter wave transmission line in the divide should have a characteristic impedence in ohm = ')
```

Scilab code Exa 8.3 design bethe hole coupler for x band waveguide

```
1 // example: -8.3, page no. -404.
```

```
2 // program to design bethe-hole coupler for x-band
    wave guide.
3 f=9*10^9; C=20; a=0.02286; b=0.01016; Ko=188.5; B=129; Z10
    =550.9; P10=4.22*10^-7; lamdao=0.0333; uo=4*%pi
    *10^-7; eo=8.854*10^-12; w=2*%pi*f;
4 s=(a/%pi)*asin(lamdao/sqrt(2*(lamdao^2-a^2)))*10^3;
5 // a=10*b; // as C=20db; // take x=a/b; so x=10;
6 ro=(P10/((10*w)*((((2*eo/3)+(4*uo)/(3*Z10^2))*0.944)
    -((4*%pi^2*uo*0.056)/(3*B^2*a^2*Z10^2)))))^(1/3)
    *10^3;
7 disp(s, 'the aperture position in mm = ')
8 disp(ro, 'the aperture size in mm = ')
9 disp("NOTE:-the above shown results completes the design of the betha hole coupler.")
```

Scilab code Exa 8.4 program to design a four hole chebysev coupler

```
1 // \text{example} : -8.4, page no. -410.
    2 // program to design a four hole chebysev coupler in
                                              x-band wave guide using round aperture located
                                         at s=a/4.
    3 a=0.02286; b=0.01016; lamdao=0.0333; ko=188.5; bta=129;
                                        Z10=550.9; P10=4.22*10^-7; f=9*10^9; no=377; N=3;
    4 \text{ s=a/4};
    5 \text{ kf} = ((2*ko)/(3*no*P10))*((sin(%pi*s/a)^2)-(2*(bta^2))
                                        /(ko^2))*((sin(%pi*s/a)^2)+((%pi^2)/((bta^2)*(a)))*((sin(%pi*s/a)^2)+((%pi^2)/((bta^2)*(a)))*((sin(%pi*s/a)^2)+((%pi^2)/((bta^2))*(a)))*((sin(%pi*s/a)^2)+((%pi^2)/((bta^2))*(a)))*((bta^2)*(a)))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a))*((bta^2)*(a
                                          ^2)))*(cos(%pi*s/a)^2)));
    6 \text{ kf} = \text{abs}(\text{kf})
    7 kb = ((2*ko)/(3*no*P10))*((sin(%pi*s/a)^2)+(2*(bta^2))
                                         /(ko^2))*((sin(%pi*s/a)^2)-((%pi^2)/((bta^2)*(a)))*((sin(%pi*s/a)^2))*((%pi^2)/((bta^2)*(a)))*((%pi^2)/((bta^2))*(a))*((%pi^2)/((bta^2))*(a))*((%pi^2)/((bta^2))*(a))*((%pi^2)/((bta^2))*(a))*((%pi^2)/((bta^2))*(a))*((%pi^2)/((bta^2))*(a))*((%pi^2)/((bta^2))*(a))*((%pi^2)/((bta^2))*(a))*((%pi^2)/((bta^2))*(a))*((%pi^2)/((bta^2))*(a))*((%pi^2)/((bta^2))*(a))*((%pi^2)/((bta^2))*(a))*((%pi^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*(a))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2))*((bta^2)/((bta^2)/((bta^2)))*((bta^2)/((bta^2)/((bta^2)/((bta^2)))*((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((bta^2)/((
                                         ^2)))*(cos(%pi*s/a)^2)));
    8 kb=abs(kb)
    9 x = \cosh(a\cosh(100)/3); // x = \sec(thetam).
10 thetam=asec(x)*180/%pi; // so, thetam=70.6 and 109.4
                                         at the band edge.
```

```
11 k=10^(-171.94/20);
12 ro=(((k/2)^(1/3))*x)*1000;
13 r1=(1.5*k*((x^3)-x))^(1/3)*1000;
14 disp(kf,'kf = ')
15 disp(kb,'kb = ')
16 disp(thetam,'thetam in degree = ')
17 disp(ro,'ro in mm = ')
18 disp(r1,'r1 in mm = ')
```

Scilab code Exa 8.5 design 50 ohm branchline quadrature hybrid junc

Scilab code Exa 8.6 determine even and odd mode characteristic impeden

```
11 Zoo=1/(v*Co);

12 disp(Zoe, 'Zoe = ')

13 disp(Zoo, 'zoo = ')
```

Scilab code Exa 8.7 design a 20 db single section coupled line coupler

```
// example: -8.7, page no. -425.
//design a 20 db single section coupled line coupler
    in stripline.

C=10^(-20/20); f=3*10^9; eipsila=2.56; Zo=50; b=0.00158;

Zoe=Zo*sqrt((1+C)/(1-C));

Zoo=Zo*sqrt((1-C)/(1+C));

Zoe=eipsila*Zoe;

Zoo=eipsila*Zoo;

x=0.72; //x=w/b.
y=0.34; // y=s/b.
w=0.72*b*100;
s=0.34*b*100;
disp(w,'conductor width in cm = ')
disp(s,'conductor seperation in cm = ')
```

Scilab code Exa 8.8 design a three section 20 db coupler

```
1 // example: -8.8, page no. -428.
2 // design a three section 20 db coupler with a binomial response.
3 Zo=50; f=3*10^9; N=3;
4 syms C C1 C2 theta;
5 C=10^(-20/20);
6 disp("for a maximally flat response for a three= section coupler doupble derivative of C will be zero.")
7 C1=0.0125; C2=0.125; C3=0.0125;
```

```
8 Zoe1=Zo*sqrt((1+C1)/(1-C1));
9 Zoe3=Zo*sqrt((1+C3)/(1-C3));
10 Zoo1=Zo*sqrt((1-C1)/(1+C1));
11 Zoo3=Zo*sqrt((1-C1)/(1+C1));
12 Zoe2=Zo*sqrt((1+C2)/(1-C2));
13 Zoo2=Zo*sqrt((1+C2)/(1-C2));
14 disp("the even and odd mode characteristic impedences for each section are = ")
15 disp(Zoe1, 'Zoe1 = ')
16 disp(Zoo1, 'Zoo1 = ')
17 disp(Zoe2, 'Zoe2 = ')
18 disp(Zoo2, 'Zoo2 = ')
19 disp(Zoo3, 'Zoo3 = ')
20 disp(Zoo3, 'Zoo3 = ')
```

Scilab code Exa 8.9 design a 3 dB 50 ohm langer coupler

```
//example: -8.9, page no. -434.
// program to design a 3 dB 50 ohm langer coupler
    for operation at 5 GHZ.

f=5*10^9; C=10^(-3/20);

Zo=50;

Zoe=(((4*C)-3+sqrt(9-(8*C^2)))/((2*C)*sqrt((1-C)/(1+C))))*Zo;

Zoo=(((4*C)+3-sqrt(9-(8*C^2)))/((2*C)*sqrt((1+C)/(1-C))))*Zo;

disp(Zoe, 'even mode characteristic impedence of a pair of adjacent coupled lines is = ')

disp(Zoo, 'even mode characteristic impedence of a pair of adjacent coupled lines is = ')
```

Scilab code Exa 8.10 design 180 deg ring hybrid for 50 ohm system imped

```
1 // example: -8.10, page no. -440.
2 // design a 180 deg. ring hybrid for a 50 ohm system impedence.
3 Zo=50;
4 Z=sqrt(2)*Zo;
5 disp(Z,'the characteristic impedence of the ring transmission line in ohm is = ')
```

Scilab code Exa 8.11 calculate even and odd mode characteristic impeden

```
1 // example: -8.11, page no. -444.
2 // calculate the even and odd-mode characteristic impedences for a tapered coupled line 180 deg. hybrid for a 3 db coupling ratio and a 50 ohm characteristic impedence.
3 alpha=0.707; bta=0.707; Zo=50;
4 k=(1-alpha)/(1+alpha);
5 Zoe=Zo/k;
6 Zoo=k*Zo;
7 disp(Zoo, 'Zoo = ')
8 disp(Zoe, 'at (Z=L) the characteristic impedences of the coupled line must be = ')
9 disp('at Z=0,there will be no coupling')
```

Chapter 9

MICROWAVE FILTERS

Scilab code Exa 9.1 program to compute the propagation constant

```
1 // \text{ example:} -9.1, \text{page no.} -462.
2 // program to compute the propagation constant, phase
       velocity and bloch impedence.
3 Co=2.666*10^-12;
4 d=0.01; c=3*10^8;
5 Zo=50; f=3*10^9;
6 p=(Co*Zo*c)/(2*d); // constant of equation given
     below.
7 y=0:0.001:0.96;
8 x=acos(cos(y)-p.*y.*sin(y)); // x=ko*d; and y=beta*d
9 subplot (2,1,1)
10 plot2d(x,y,style=2,rect=[-\%pi,0,\%pi,0.96])
11 plot2d(-x,y,style=2,rect=[-\%pi,0,\%pi,0.96])
12 xtitle("k-beta diagram for first pass band ","beta*d
     ","ko*d")
13 y=3:0.001:4;
14 x=acos(cos(y)-p.*y.*sin(y)); // x=ko*d; and y=beta*d
15 subplot (2,1,2)
16 plot2d(x,y,style=3,rect=[-%pi,3,%pi,4])
```

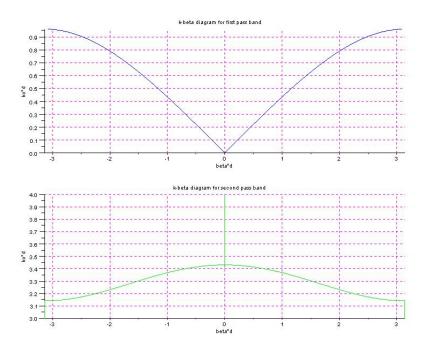


Figure 9.1: program to compute the propagation constant

Scilab code Exa 9.2 program to design a low pass composite filter

```
1 // \text{ example:} -9.2, \text{page no.} -473.
2 // program to design a low pass composite filter
      with cutoff frequency of 2 MHZ.
3 fc=2*10^6; f=2.05*10^6; Ro=75;
4 L=(2*Ro)/(2*\%pi*fc);
5 C=2/(Ro*2*\%pi*fc);
6 for m=sqrt(1-(fc/f)^2)
7 x=m*L/2;
8 y=m*C;
9 z=((1-m^2)/(4*m))*L; // x,y,z are design parameter
10 disp(x,y,z,'design parameter for m=0.2195')
11 end
12 \text{ for } m = 0.6
13 x=m*L/2;
14 y = m * C/2;
15 z=((1-m^2)/(2*m))*L; // x,y,z are design parameter
        assumed.
16 disp(x,y,z,'design parameter for m=0.6')
17 \text{ end}
```

Scilab code Exa 9.3 program to find out number of filter elements

```
1 // example: -9.3, page no. -482.
2 // program to find out number of filter elements
    required.
3 fc=8*10^9;f=11*10^9;
4 w=2*%pi*f;
5 wc=2*%pi*fc;
6 x=abs(w/wc)-1;
```

```
7 disp(x,"from table we see that an attenuation of 20 db at this frequency requires that N>=8 for x = ")
```

Scilab code Exa 9.4 program to design a maximum flat low pass filter

```
1 // example: -9.4, page no. -488.
2 // program to design a maximum flat low pass filter
    with cut off frequency of 2 GHZ.
3 fc=2*10^9;f=3*10^9;
4 w=2*%pi*f;
5 wc=2*%pi*fc;
6 x=abs(w/wc)-1;
7 // from table we can see that N=5 will be sufficient
    .
8 // then prototype element values are:-
9 g1=0.618;g2=1.618;g3=2.000;g4=1.618;g5=0.618;
10 disp(g1, 'g1 = ')
11 disp(g2, 'g2 = ')
12 disp(g3, 'g3 = ')
13 disp(g4, 'g4 = ')
14 disp(g5, 'g5 = ')
```

Scilab code Exa 9.5 program to design a band pass filter

```
1 // example: -9.5, page no. -492.
2 // design a band pass filter having a 0.5 db equal ripple respnse with N=3.
3 N=3; Zo=50; f=1*10^9; delta=1*10^8;
4 L1=1.596; L3=1.5963; C2=1.0967; R1=1.000;
5 L_1=(L1*Zo)/(2*%pi*f*delta);
6 C_1=delta/(2*%pi*f*L1*Zo);
7 L_2=(delta*Zo)/(2*%pi*f*C2);
```

```
8  C_2=C2/(2*%pi*f*delta*Zo);
9  L_3=(L3*Zo)/(2*%pi*f*delta);
10  C_3=delta/(2*%pi*f*L3*Zo);
11  disp(L_1)
12  disp(L_2)
13  disp(C_1)
14  disp(C_2)
15  disp(L_3)
16  disp(C_3)
```

Scilab code Exa 9.6 design a low pass filter using micrstrip lines

```
1 // example: -9.6, page no. -498.
2 // design a low pass filter for fabrication using micrstrip lines.
3 disp("from table, the normalized low pass prototype element values are = ")
4 L1=3.3487; C2=0.7117; L3=3.3487; R1=1.0000; n=1+(1/3.3487); disp(L1)
7 disp(R1)
8 disp(C2)
9 disp(L3)
10 disp(n)
```

Scilab code Exa 9.7 design a stepped impedence low pass filter

```
1 // example: -9.7, page no. -503.
2 // design a stepped-impedence low pass filter having
    a maximally flat response and a cut-off
    frequency of 2.5 GHZ.
3 w=4*10^9; wc=2.5*10^9; Zh=150; Ro=50; Zl=10;
```

```
4 C1=0.517; L2=1.414; C3=1.932; L4=1.932; C5=1.414; L6
       =0.517;
5 // above values are taken from table.
6 // for finding electrical lengths.
7 x1=(C1*Z1/Ro)*(180/\%pi);
8 x2=(L2*Ro/Zh)*(180/\%pi);
9 x3=(C3*Z1/Ro)*(180/\%pi);
10 x4=(L4*Ro/Zh)*(180/\%pi);
11 x5=(C5*Z1/Ro)*(180/\%pi);
12 x6=(L6*Ro/Zh)*(180/\%pi);
13 \operatorname{disp}(x1)
14 \operatorname{disp}(x2)
15 \text{ disp}(x3)
16 \text{ disp}(x4)
17 \text{ disp}(x5)
18 disp(x6)
```

Scilab code Exa 9.8 design a coupled line band pass filter

```
1 // example: -9.8, page no. -516.

2 // design a coupled line band pass filter with N=3.

3 delta=0.1; f=1.8*10^9; fo=2*10^9; Zo=50; fc=1;

4 f=(1/delta)*((f/fo)-(fo/f));

5 x=abs(f/fc)-1; // the value on the horizontal scale.

6 attntn=20; // from above values.

7 disp(attntn, 'attenuation in db = ')
```

Scilab code Exa 9.9 design a bandpass filter

```
4 Zon=4*Zo/(%pi*gn*delta);
5 Z_on=(%pi*Zo*delta)/(4*gn);
6 disp(Zon, 'the cahracteristic impedence of a bandpass filter is = ')
7 disp(Z_on, 'for a bandpass filter using short circuited stub resonators, the corresponding result is = ')
```

Scilab code Exa 9.10 design a bandpass filter using capacitive coupled

```
1 // \text{ example}: -9.10, \text{page no.} -524.
2 // design a bandpass filter using capacitive coupled
       resonators, with a 0.5 db equal passband
      haracteristic.
3 fo=2*10^9; delta=0.1; Zo=50; f=2.2*10^9; g1=1.5963; g2
      =1.0967; g3=1.5963; g4=1;
4 f = (1/delta)*((f/fo)-(fo/f));
5 \text{ x=abs(f/fc)-1}; // the value on the horizontal scale.
6 x0=sqrt((\%pi*delta)/(2*g1))/Zo; // x0=ZoJ1;
7 x1 = ((\%pi*delta)/(2*sqrt(g1*g2)))/Zo; // x0=ZoJn;
8 B0=x0/(1-(Zo*x0)^2)
9 B1=x1/(1-(Zo*x1)^2)
10 theta0=(\%pi-0.5*(\frac{1}{2}atan(2*Zo*B0)+\frac{1}{2}atan(2*Zo*B1)))*(180/
      %pi);
11 C0=(B0/(2*\%pi*fo))*10^12;
12 disp(theta0, 'thetao in degree = ')
13 disp(CO, 'the coupling capacitor value in PF = ')
```

Chapter 10

THEORY AND DESIGN OF FERRIMAGNETIC COMPONENTS

Scilab code Exa 10.1 calculate and plot phase and attenuation constants

```
1 // example: -10.1; page no. -547.
2 // problem to calculate and plot the phase and
      attenuation constants for RHCP & LHCP plane wave.
3 M=1800; // M=4*pi*Ms;
4 deltaH=75; eo=8.854*10^-12; muo=4*\%pi*10^-7; c=3*10^8;
5 Ho=3570; er=14; tandelta=0.001;
6 fo=(2.8*10^9)/Ho; // IN GHZ.
7 wo = 2 * \%pi * fo;
8 fm = (2.8*10^9)/M; // IN GHZ.
9 wm = 2 * \%pi * fm;
10 mue=muo*(1+(wo*wm)/(wo^2-wm^2));
11 e=eo*er*(1-%i*tandelta);
12 f = 0:1000000:20*10^9;
13 w = 2 * \%pi.*f;
14 k=muo*((w.*wm)/(wo^2-w^2));
15 gama=%i*w*sqrt(e.*(mue-k));
16 alpha=abs(real(gama));
```

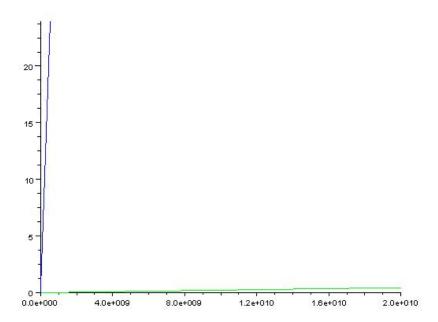


Figure 10.1: calculate and plot phase and attenuation constants

```
17 bta=abs(imag(gama));

18 plot2d(f,gama,style=3,rect=[0,0,20*10^9,24])

19 plot2d(f,bta,style=2,rect=[0,0,20*10^9,24])
```

Scilab code Exa 10.2 program to design an e plane resonance isolator

```
5 f=10*10^9; alpha_=12.4; // from graph 10.13.
6 L=revatt/alpha_;
7 alpha_1=27/L;
8 disp(L,'for total reverse attenuation of 20 db, the length of the slab in cm must be = ')
9 disp(alpha_1,'for total reverse attenuation to be at least 27 db, alpha_ in db/cm be > ')
```

Scilab code Exa 10.3 program to design a resonance isolator

```
1 // \text{example} : -10.3. \text{ page no.} -560.
2 // program to design a resonance isolator using the
      H-plane ferrite slab geometry in x-band.
3 f=10*10^9; delta_sbys=0.01; forpims=1700; deltaH=200;
4 revatt=30; ko=(2*\%pi*f)/(3*10^8);
5 Ho=f/(2.8*10^9);
6 // for x-band waveguide, a=2.286 cm.
7 a=2.286;
8 \text{ kc} = (\%\text{pi} * 100)/\text{a};
9 betao=sqrt(ko^2-kc^2);
10 x=(1/\%pi)*atan(kc/betao); // x=c/a.
11 L=revatt/2;
12 disp(L, 'the slab length required for 30db total
      reverse attenuation in cm = ')
13 disp(kc, 'cut-off wave number in m-1 = ')
14 disp(betao, 'propagation constant = ')
```

Scilab code Exa 10.5 design a two slab remanent phase shifter

```
1 //example:10.5, page no.-567.
2 // program to design a two slab remanent phase shifter.
```

Chapter 11

ACTIVE MICROWAVE CIRCUITS

Scilab code Exa 11.1 determine equivalent noise temperature of amplifie

```
// example:-11.1, page no.-589.
// program to determine the equivalent noise
    temperature of the amplifier.

T1=290; P1=-62; G=100; B=10^9; k=1.38*10^-23;

T2=77; P2=-64.7; Ts=450;
Y=P1-P2; // Y-factor in db.
Y=10^0.27;
Te=(T1-Y*T2)/(Y-1);
Po=G*k*B*(Ts+Te);
Po=10*log10(Po/0.001); /// converting in to dBm.
disp(Te, 'the equivalent noise temperature in kelwin = ')
disp(Po, 'the total noise power out of the amplifier in dBm will be = ')
```

Scilab code Exa 11.2 find the dynamic range of the amplifier

```
// example: -11.2, page no. -591.
// program to find the dynamic range of the amplifier.
G=20; F=3.5; // in db.
k=1.38*10^-23; To=290; B=2*10^9;
// output noise power => No=G*F*k*To*B.so in dbm it will be-
No=20+3.5+10*log10((k*To*B)/0.001);
R=10-No;
disp(DR, 'the dynamic range in dB = ')
```

Scilab code Exa 11.3 program to calculate the noise figure

```
// example: -11.3, page no. -593.
// program to calculate the noise figure ig anteena is replaced by amplifier.
L=10^0.2; T=300; To=290; Te=150;
Fl=1+(L-1)*(T/To);
Fld=10*log10(Fl); // converting in to dBm.
Fa=1+(Te/To)
Fad=10*log10(Fa); // converting in to dBm.
Fcas=Fl+L*(Fa-1);
Fcasd=10*log10(Fcas); // converting in to dBm.
disp(Fcasd, 'the noise figure of the cascade in dB = ')
disp(Fad, 'the noise figure of the amplifier in dB = ')
disp(Fld, 'the noise figure of the line in dB = ')
```

Scilab code Exa 11.4 calculate the impedence of the diode

```
1 //example: -11.4, page no. -596.
2 //program to calculate the impedence of the diode.
```

Scilab code Exa 11.5 determine the stability of the transistor

```
1 // \text{example}: -11.5, \text{page no.} -617.
2 //program to determine the stability of the
      transistor by calculating k and |delta|.
3 s11=0.894*expm(%i*(-60.6)*%pi/180);
4 s21=3.122*expm(%i*(123.6)*%pi/180);
5 	ext{ s12=0.02*expm}(\%i*(62.4)*\%pi/180);
6 s22=0.781*expm(%i*(-27.6)*%pi/180);
7 delta=(s11*s22)-(s12*s21);
8 [mag_delta,theta_delta]=polar(delta);
9 k = (1 + (abs(delta)^2) - (abs(s11)^2) - (abs(s22)^2))/(2*
      abs(s12*s21));
10 Cl = conj(s22 - delta * conj(s11)) / (abs(s22)^2 - abs(delta))
      ^2);
11 [mag_Cl,theta_Cl]=polar(Cl);
12 Rl = abs(s12*s21)/(abs(s22)^2 - abs(delta)^2);
13 Cs=conj(s11-delta*conj(s22))/(abs(s11)^2-abs(delta)
      ^2);
14 [mag_Cs, theta_Cs] = polar(Cs);
15 Rs=abs(s12*s21)/(abs(s11)^2-abs(delta)^2);
16 disp([mag_Cl,theta_Cl])
17 disp([mag_Cs,theta_Cs])
18 disp(R1)
19 disp(Rs)
20 disp("NOTE:-theta is in radian")
```

Scilab code Exa 11.6 design an amplifier for maximum gain

```
1 // \text{ example:} 11.6, \text{page no.} -620.
2 // program to design an amplifier for maximum gain
      at 4 GHZ using single stub matching section.
3 s11=0.72*expm(%i*(-116)*%pi/180);
4 s22=0.73*expm(%i*(-54)*%pi/180);
5 	ext{ s12=0.03*expm}(\%i*(57)*\%pi/180);
6 s21=2.6*expm(%i*(76)*%pi/180);
7 delta=(s11*s22)-(s12*s21)
8 k=(1+(abs(delta)^2)-(abs(s11)^2)-(abs(s22)^2))/(2*
      abs(s12*s21))
9 B1=1-(abs(delta)^2)+(abs(s11)^2)-(abs(s22)^2);
10 B2=1-(abs(delta)^2)-(abs(s11)^2)+(abs(s22)^2);
11 C1=s11-delta*conj(s22);
12 C2=s22-delta*conj(s11);
13 taos=(B1-sqrt(B1^2-4*abs(C1)^2))/(2*C1);
14 [mag_taos,theta_taos]=polar(taos);
15 taol=(B2-sqrt(B2^2-4*abs(C2)^2))/(2*C2);
16 [mag_taol,theta_taol]=polar(taol);
17 Gs=1/(1-abs(taos)^2);
18 Gs = 10 * log 10 (Gs);
19 Go = abs(s21)^2;
20 Go=10*log10(Go);
21 Gl = (1 - abs(taol)^2)/(abs(1 - s22*taol)^2);
22 \text{ Gl} = 10 * \frac{\log 10}{(Gl)};
23 Gtmax=Gs+Go+G1;
24 \text{ disp}(Gs, 'Gs = ')
25 \text{ disp}(Go, 'Go = ')
26 \text{ disp}(Gl, 'Gl = ')
27 disp(Gtmax, 'the over all transducer gain in dB will
      be = ')
28 Gs=1/(1-abs(taos)^2);
29 Gs=10*log10(Gs);
```

Scilab code Exa 11.7 design an amplifier to have a gain of 11 dB

```
1 // \text{ example:} -11.7, \text{page no.} -625.
2 // program to design an amplifier to have a gain of
      11 dB at 4 GHZ.
3 s11=0.75*expm(%i*(-120)*%pi/180);
4 s21=2.5*expm(%i*(80)*%pi/180);
5 s12=0;
6 s22=0.6*expm(%i*(-70)*%pi/180);
7 Gsmax=1/(1-abs(s11)^2);
8 Gsmax=10*log10(Gsmax);
9 Glmax=1/(1-abs(s22)^2);
10 Glmax=10*log10(Glmax);
11 Go=abs(s21)^2;
12 Go=10*log10(Go);
13 Gtumax = Gsmax + Glmax + Go;
14 disp (Gsmax, 'the maximum matching section gain in dB
15 disp(Glmax, 'the maximum matching section gain in dB
16 disp(Go, 'the gain of the mismatched transistor in dB
17 disp(Gtumax, 'the maximum unilateral transducer gain
      in dB = '
```

Scilab code Exa 11.8 calculate maximum error in Gt and design amplifier

```
1 // example:-11.8, page no.-629.
2 // program to maximum error in Gt and design an amplifier having a 2 dB noise figure with the maximum gain that is compatible with the noise figure.
```

```
3 s11=0.6*expm(%i*(-60)*%pi/180);
4 s21=1.9*expm(%i*(81)*%pi/180);
5 s12=0.05*expm(%i*(26)*%pi/180);
6 s22=0.5*expm(%i*(-60)*%pi/180);
7 Fmin=1.6; F=1.58; Zo=50;
8 Fmin1=10<sup>0</sup>.16
9 tao_opt=0.62*expm(%i*(100)*%pi/180);
10 atan(imag(tao_opt)/real(tao_opt))
11 Rn = 20;
12 U=abs(s12*s21*s11*s22)/((1-abs(s11)^2)*(1-abs(s22))
       ^2));
13 x=1/(1+U)^2;
14 y=1/(1-U)^2;
15 \operatorname{disp}(\mathrm{"x}<(\operatorname{Gt}/\operatorname{Gtu})<\mathrm{y"})
16 N=(((F-Fmin1)*Zo)/(4*Rn))*abs(1+tao_opt)^2
17 Cf = tao_opt/(N+1);
18 [mag_Cf, theta_Cf] = polar(Cf);
19 Rf=sqrt(N*(N+1-abs(tao_opt)^2))/(N+1);
20 \text{ disp}(N, 'N = ')
21 disp([mag_Cf,theta_Cf],'center of the 2 db noise
       figure circle = ')
22 disp(Rf, 'the radius of the 2 dB noise figure circle
      = ')
23 Gl=1/(1-abs(s22)^2);
24 \text{ Gl} = 10 * \log 10 \text{ (Gl)};
25 \text{ Go} = abs(s21)^2;
26 \text{ Go} = 10 * \frac{10}{9} (\text{Go});
27 Gs=1.7; // all Gl, Go, Gtu are in dB.
28 Gtu=Gs+Go+G1;
29 disp(Gtu, 'the over all transducer gain in db will be
       = ')
```

Scilab code Exa 11.9 design a load matching network

```
1 // \text{ example:} -11.9, \text{page no.} -635.
```

```
2 // program to design a load matching network for a
     50 ohm load impedence.
3 Zo=50;f=6*10^9;taoin=1.25*expm(%i*(40)*%pi/180);
4 Zin=((1+taoin)/(1-taoin))*Zo;
5 Zl=-Zin;
6 disp(Zl, 'the load impedence = ')
```

Scilab code Exa 11.10 program to design a transistor oscillator

```
1 // \text{example} : 11.10, page no. -637.
2 // program to design a transistor oscillator at 4
     GHZ using a GaAs FET in common gate configuration
3 \text{ s11=2.18*expm}(\%i*(-35)*\%pi/180);
4 s21=2.75*expm(%i*(96)*%pi/180);
5 	ext{ s12=1.26*expm}(\%i*(18)*\%pi/180);
6 s22=0.52*expm(%i*(155)*%pi/180);// all are s
      parameter that are applicable for transistor in
     common gate configuration with aseries inductor.
7 delta=s12*s21-s11*s22;
8 Ct=conj(s22-delta*conj(s11));
9 Rt=abs((s12*s21)/(abs(s22)^2-abs(delta)^2))
10 taot=0.59*expm(%i*(-104)*%pi/180);
11 taoin=s11+(s12*s21*taot)/(1-s22*taot);
12 [mag_taoin,theta_taoin]=polar(taoin)
13 Zin=((1+taoin)/(1-taoin))*Zo;
14 Z1 = -(real(Zin)/3) - (\%i * imag(Zin));
15 disp([mag_taoin,theta_taoin])
16 disp(Z1, 'the load impedence will be = ')
```

Scilab code Exa 11.11 obtain the greatest ratio of off to on attenuation

```
1 // \text{example} : -11.11, \text{page no.} -642.
```

```
2 // program to obtain the greatest ratio of off to
     on attenuation.
3 Cj=0.1*10^-12; Rr=1; Rf=5; Li=0.4*10^-9; f=5*10^9; Zo=50;
4 w = 2 * \%pi * f;
5 Zr=Rr+\%i*((w*Li)-(1/(w*Cj)));
6 Zf = Rf + (\%i*w*Li);
7 // for series circuit.
8 ILon=-20*log10(abs((2*Zo)/(2*Zo+Zf)));
9 ILoff=-20*log10(abs((2*Zo)/(2*Zo+Zr)));
10 // for shunt circuit.
11 ILon1=-20*log10(abs((2*Zr)/(2*Zr+Zo)));
12 ILoff1 = -20*log10(abs((2*Zf)/(2*Zf+Zo)));
13 disp(ILon, 'for series circuit = ')
14 disp(ILoff, 'for series circuit = ')
15 disp(ILon1, 'for shunt circuit = ')
16 disp(ILoff1, 'for shunt circuit = ')
```

Chapter 12

INTRODUCTION TO MICROWAVE SYSTEMS

Scilab code Exa 12.1 compute directivity radiation intensity and others

```
1 // \text{ example}: -12.1, \text{page no.} -668.
2 //program to compute directivity, radiation intensity
      ,F, the effective area.
3\, syms Etheta Hphi ko no Io 1\, r pi theta C\, phi lamda;
4 Etheta=((\%i*ko*no*Io*1)/(4*pi*r))*sin(theta)*exp(-\%i
      *ko*r);
5 Hphi = ((\%i*ko*Io*1)/(4*pi*r))*sin(theta)*exp(-\%i*ko*r)
      );
6 F=(r^2)*(Etheta*conj(Hphi));
7 Prad=C*integ(integ(sin(theta)^3, theta), phi);
8 Prad=limit(Prad, theta, pi)-limit(Prad, theta, 0);
9 Prad=limit(Prad,phi,2*pi)-limit(Prad,phi,0); // take
       \cos (pi) = -1;
10 Prad=8*pi*C/3;
11 D=4*pi*C/Prad;
12 Ac = ((lamda^2)*D)/(4*pi);
13 disp(F, 'the radiation intensity is given by = ')
14 disp(D, 'directivity is given by = ')
15 disp(Ac, 'the effective area of the dipole = ')
```

Scilab code Exa 12.2 program to find the reactive power in dbm

```
1 // example: -12.2, page no. -674.
2 // program to find the reactive power in dbm.
3 Pt=120; f=6*10^9;
4 Gt=10^4.2; Gr=10^3.1;
5 lamda=0.05; R=3.59*10^7;
6 Pr=(Pt*Gt*Gr*(lamda^2))/((4*%pi*R)^2);
7 Pr=10*log10(Pr/0.001);
8 disp(Pr, 'received power in dBm will be = ')
```

Scilab code Exa 12.3 calculate the input and output SNR

```
1 // example: -12.3, page no. -677.
2 // program to calculate the input and output SNR.
3 f=4*10^9; B=1*10^6; Grf=10^2; Gif=10^3; Lt=10^0.15; Lm
      =10^0.6; To =290;
4 Fm=10^0.7; Tm=(Fm-1)*To; Tp=300; Tb=200; eta=0.9;
5 Frf=10^0.3; Fif=10^0.11; k=1.38*10^-23;
6 Trf = (Frf - 1) * To;
7 Tif = (Fif - 1) * To;
8 Trec=Trf+(Tm/Grf)+((Tif*Lm)/Grf);
9 Ttl=(Lt-1)*Tp;
10 Ta=eta*Tb+(1-eta)*Tp;
11 Ni=k*B*Ta;
12 Ni=10*log10(Ni/0.001); // converting in to dBm.
13 si=-80; // in dBm.
14 SNRi=si-Ni; // input SNR.
15 Tsys=Ta+Ttl+Lt*Trec;
16 SNRo=\sin -10*\log 10((k*B*Tsys)/0.001);
17 disp(SNRi, 'input SNR in dB = ')
18 disp(SNRo, 'output SNR in dB = ')
```

Scilab code Exa 12.4 program to find the maximum range of radar

Scilab code Exa 12.5 program to find the J by S ratio

```
1 //example: -12.5, page no. -702.
2 // program to find the J/S ratio.
3 Gr=10^3.5; Pj=1000; R=3000; Br=1*10^6; Bj=20*10^6;
4 Gj=10; lamda=0.03; Pt=10^5; sigma=4; Rj=10000;
5 x=(Pj/Pt)*((4*%pi*(R^2)*Gj)/(sigma*Gr))*(Br/Bj); // x=J/S
6 x=10*log10(x);
7 Grsl=10^(3.5-2); // radar anteena gain in its sidelobe region.
8 x1=(Pj/Pt)*(((R^4)*Gj*Grsl)/((Gr^2)*(Rj^2)))*(Br/Bj);
9 x1=10*log10(x1);
10 disp(x, 'THE J/S ration for the SSJ case in dB is = ')
11 disp(x1, 'THE J/S ratio for the SOJ case in dB is = ')
```

Scilab code Exa 12.6 calculate power density of 20 m from anteena

```
1 // example: -12.6, page no. -704.
2 // program to calculate the power density of 20 m from the anteena.
3 G=10^4; Pin=5; R=20;
4 S=(Pin*G)/(4*%pi*(R^2))*0.1;
5 disp(S, 'the power density in the main beam of the anteena at a distance of 20 m in mw/cm^2 = ')
```

Appendix

Scilab code AP 1 equivalent of two resistances in parallel

```
//function example: -5.4, page no. -221.
function[Z]=parallel_impedence(Z1, Z2)
Z=(Z1*Z2)/(Z1+Z2);
endfunction
```

Scilab code AP 2 smith chart for finding load impedence when reflection coefficient is given.

```
1 // function for smith chart for finding load
      impedence when reflection coefficient is given.
2 function[]=smith_chart(tao)
3 \text{ theta=0:0.1:2*\%pi;}
4 \quad for \quad r = 0:0.1:10
5 x=(1/(1+r))*cos(theta)+(r/(1+r));
6 y=(1/(1+r))*sin(theta);
7 plot2d(x,y,style=2,rect=[-2,-2,2,2])
8 end
9 for X = -2:0.1:2
     if X == 0
10
11
       X = 0.01;
12
     end
13 x=1+(1/X)*cos(theta);
14 y=(1/X)*sin(theta)+(1/X);
15 plot2d(x,y,style=3,rect=[-2,-2,2,2])
16 xgrid(2)
17 xtitle ("smith chart", "Tao_Real", "Tao_Imaginary")
```

```
18 end
19 x = abs(tao) * cos(theta);
20 y=abs(tao)*sin(theta);
21 \text{ plot2d}(x,y,style=5,rect=[-2,-2,2,2])
22 theta=-\%pi/2:0.1:\%pi/2;
23 x = abs(tao) * cos(theta);
24 [r angle]=polar(tao);
25 tao=[r angle]
26 \ y=x*tan(tao(1,2));
27 \text{ plot2d}(x,y,style=5,rect=[-2,-2,2,2])
28 endfunction
          Scilab code AP 3 function for input impedence
  1 // function for input impedence.
  2 function [Zin] = input_impedence(tao,b,1,Zo)
                  Zin=Zo*((1+(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1)))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*b*1))/(1-(tao*exp(-2*\%i*
                             *b*1))))
  4 endfunction
          Scilab code AP 4 function for reflection coefficient
  1 "Tao_Real", "Tao_Imaginary" "Tao_Real", "Tao_Imaginary"
                     // function for reflection coefficient.
  2 function[tao] = reflection_coefficient(Z1,Zo)
                   tao = (Z1 - Zo)/(Z1 + Zo);
  4 endfunction
          Scilab code AP 5 function to find SWR
  1 // function to find SWR,
  2 function[SWR] = VSWR(tao)
                  SWR = (1 + tao) / (1 - tao)
  4 endfunction
```