

Example 3.1(3)

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前两问的解题如下:

例3.1: 如图为一薄壁圆管, 其横截面如图(a), 试讨论三种加载情况
 求: 管内的应力 σ_{θ} 和纵向应变 ϵ_z
 (1) 轴向拉伸 σ_z 保持 $\sigma_z = \sigma_s$
 施加 $T_{z\theta} = \frac{G}{3}$ (沿 θ)
 (2) 先施加 $T_{z\theta} = \frac{G}{3}$ 保持并加载 $\sigma_z = \sigma_s$
 (3) 保持 $\sigma_z = T_{z\theta} = \frac{G}{3}$ 加载

由于 $\sigma_1 = \sigma_2 = T, \sigma_3 = -T$

$$\sigma_1 = \frac{1}{\sqrt{3}} \sqrt{(\sigma_2 + T)^2 + (\sigma_3 - T)^2 + 0}$$

$$= \frac{1}{\sqrt{3}} \sqrt{2\sigma_s^2 + T^2} = \sqrt{\frac{G}{3} \sqrt{3} T}$$

解: (1) 弹性阶段: 由本构关系

$$d\epsilon_{ij} = \frac{1}{2\mu} d\sigma_{ij} + \frac{1-2\nu}{E} \sigma_m \delta_{ij}$$

$$d\epsilon_{ij} = d\epsilon_{\theta\theta} = \frac{1}{2\mu} d\sigma_{\theta\theta} + \frac{1-2\nu}{E} \sigma_m$$

$$\text{其中: } \sigma_m = \frac{1}{3} \sigma_s, \sigma_m = \frac{G}{3}$$

$$\therefore \sigma_{\theta\theta} = \frac{G}{3\mu} + \frac{1-2\nu}{E} \cdot \frac{G}{3} \quad (\text{其中: } \mu = \frac{E}{2(1+\nu)})$$

$$= \frac{2(1+\nu)}{3E} \sigma_s + \frac{1-2\nu}{3E} \sigma_s = \frac{\sigma_s}{E} \rightarrow d\lambda = \frac{3 d\sigma_1}{2 F \sigma_1}$$

(2) 塑性阶段

$$\text{由 } d\epsilon_{ij} = \frac{1}{2\mu} d\sigma_{ij} + \frac{1-2\nu}{E} \sigma_m \delta_{ij} \rightarrow d\lambda = \frac{3 d\sigma_1}{2 F \sigma_1}$$

$$\text{由于塑性: } d\sigma_{ij} = 0, \text{ 另有: } \nu = \frac{1}{2}, \text{ 所以 } 0$$

$$\text{故: } d\epsilon_{ij} = d\epsilon_{\theta\theta}^p = d\lambda \cdot S_{ij}$$

$$\text{其中: } d\lambda \text{ 满足流变关系: } d\lambda = \frac{d\epsilon_{ij}^p}{S_{ij}} = \frac{\sqrt{\frac{3}{2}} d\epsilon^p}{\sqrt{\frac{3}{2}} \sigma_1} = \frac{3 d\sigma_1}{2 F \sigma_1}$$

$$\text{其中: } \frac{d\sigma_1}{d\epsilon_1^p} = F' \quad \text{故: } d\lambda = \frac{3 d\sigma_1}{2 F \sigma_1}$$

$$\text{其中: } \sigma_1 \text{ 由 } \sigma_s \rightarrow \sqrt{\sigma_s^2 + 3T^2} = \sqrt{2} \sigma_s$$

$$\int d\epsilon_1^p = \int d\lambda S_{ij} = \int \frac{3 d\sigma_1}{2 F \sigma_1} S_{ij}$$

此外注意
 $T_{\theta z}, T_{z\theta}$ 均使用正应力计算
 $\rightarrow \sigma_{\theta z}, \sigma_{z\theta}$ 均使用正应力
 (1.4.2.2.2)

右: 第二阶段: 由 $\sigma_1 = \sigma_s, \sigma_2 = T, \sigma_3 = -T$

$$\begin{cases} S_{\theta\theta} = 0, & G_1 \text{ 由 } G_s \rightarrow F_2 G_s \\ d\sigma_r = d\sigma_{\theta} = 0, \\ S_{rz} = S_{\theta z} = -\frac{G}{3} \\ S_{zz} = \frac{2G}{3} \end{cases}$$

$$S_{r\theta} = \frac{1}{\sqrt{3}} T$$

代换



使用应力表达式求 $d\sigma_1$

$$\text{由 } \sigma_1 = \sqrt{3T_{z\theta}^2 + \sigma_s^2}$$

$$\frac{d\sigma_1}{d\sigma_s} = \frac{3T_{z\theta}}{\sigma_s} \frac{d\sigma_s}{\sigma_s} = \frac{3T_{z\theta}}{\sigma_s} \frac{d\sigma_s}{\sigma_s}$$

$$\text{则等: } \int d\epsilon_1^p = \int \frac{3}{2F} \frac{d\sigma_1}{\sigma_1} S_{ij} = \int \frac{3}{2F} \frac{3T_{z\theta}}{\sigma_s} \frac{d\sigma_s}{\sigma_s} S_{ij} = \frac{G}{F} \int \frac{3T_{z\theta}}{\sigma_s^2} d\sigma_s = \frac{G}{F} \int \frac{3T_{z\theta}}{\sigma_s^2} d\sigma_s$$

$$\text{第二阶段: } \int d\epsilon_{r\theta} = \int \frac{3G}{F} \cdot \frac{3T_{z\theta}}{\sigma_s^2} T_{r\theta} d\sigma_s$$

$$= \frac{3G}{2F} \int \frac{1}{1 + (\frac{G}{\sigma_s})^2} d\sigma_s \rightarrow \frac{G}{\sqrt{3}} d(\frac{\pi}{4})$$

$$\text{由 } \int \frac{1}{1+x^2} dx = \arctan x + C$$

$$d\gamma_{r\theta} = \frac{1}{\mu} dS_{r\theta} + \frac{3}{2F} \frac{d\sigma_1}{\sigma_1} T_{z\theta} \quad (\text{由 } \frac{1}{2})$$

$$\therefore \gamma_{r\theta} = \frac{1}{\mu} \times \frac{G}{\sqrt{3}} + \frac{G}{\sqrt{3}} (1 - \frac{\pi}{4})$$

$$= \frac{G}{2F} \left[\ln \left(\frac{\sigma_s^2 + G^2}{\sigma_s^2} \right) - \ln \left(\frac{\sigma_s^2}{\sigma_s^2} \right) \right]$$

$$= \frac{G}{2F} \ln 2$$

$$\int \frac{1}{1 + (\frac{G}{\sigma_s})^2} d\sigma_s \quad \text{令 } t = \frac{T_{z\theta}}{\sigma_s/\sqrt{3}}$$

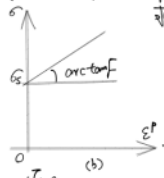
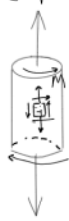
$$\text{由: } \int \frac{1}{1+t^2} dt = \arctan t \quad \text{则 } d\sigma_s = dt \cdot \frac{\sigma_s}{\sqrt{3}}$$

$$= \int \left(1 - \frac{1}{1+t^2} \right) dt \cdot \frac{G}{\sqrt{3}}$$

$$= \left(t - \arctan t \right) \frac{G}{\sqrt{3}}$$

$$= \frac{G}{\sqrt{3}} \left(-\arctan t \right) = \left(-\frac{\pi}{4} \right) \frac{G}{\sqrt{3}}$$

例：② 如图为一薄壁圆管，其材料应力曲线如图(b)，讨论下列三种加载路径求管的轴向应变 ϵ_z 和切向应变 $\gamma_{\theta\phi}$



① 失压加载: $T_{\theta\phi} = \frac{\sigma_s}{\sqrt{3}}$, 保持并加载 $G_z = G_s$

② 失压加载: $T_{\theta\phi} = \frac{\sigma_s}{\sqrt{3}}$ 时 \rightarrow 由 $G_i = \sqrt{3 J_1}$, $\sqrt{\frac{1}{2}[(\sigma_z - \sigma_s)^2 + (\sigma_z + \sigma_s)^2 + (T_{\theta\phi}^2 + T_{\theta\phi}^2 + T_{\theta\phi}^2)]}$

$$G_i = \sqrt{G_z^2 + 3 T_{\theta\phi}^2}$$

(1): 由增量本构关系有:

$$d\epsilon_{ij} = \frac{1}{2\mu} dS_{ij} + \frac{1-2\nu}{E} d\sigma_m \delta_{ij} + d\lambda S_{ij}$$

因此有:

① 弹性阶段: $dS_z = 0 = dG_z = 0$,

故: $d\epsilon_z = 0$,

由剪切胡克定律: $\frac{1}{2}\gamma = \frac{1}{\mu} \tau$, 则: $\gamma = \frac{1}{\mu} \tau = \frac{\sigma_s}{\sqrt{3}} \frac{2(1+\nu)}{E} = \frac{2\sigma_s(1+\nu)}{\sqrt{3}E}$

第一阶段: $\epsilon_z = 0$
 $\gamma_{\theta\phi} = \frac{2\sigma_s(1+\nu)}{\sqrt{3}E}$

② 塑性阶段:

$d\epsilon_{ij} = \frac{1}{2\mu} dS_{ij} + \frac{1-2\nu}{E} d\sigma_m \delta_{ij} + d\lambda S_{ij}$ 其中: 使用强化材料本构:

其中: 2方向:

有: $dG_z = \frac{2}{3} d\sigma_s$ 而: $dG_m = \frac{\sigma_s}{3}$

则: $d\epsilon_z = \frac{1+\nu}{E} \cdot \frac{2}{3} d\sigma_s + \frac{\sigma_s}{3} \cdot \frac{1-2\nu}{E} + \frac{3 d\sigma_s}{2F \sigma_s} \cdot \frac{\sigma_s}{3}$

$$\frac{d\sigma_s}{E} = \frac{2(1+\nu)G_s + (1-2\nu)G_s}{3E} + \int \frac{3 d\sigma_s}{2F \sigma_s} \cdot \frac{\sigma_s}{3}$$

其中: $\int \frac{3 d\sigma_s}{2F} \cdot \frac{\sigma_s}{3} = \int \frac{1}{F} \frac{\sigma_s^2}{\sqrt{G_z^2 + 3 T_{\theta\phi}^2}} dG_z$

$$\frac{1}{2} \frac{G_s}{G_s + 3 T_{\theta\phi}^2} = \frac{G_s}{\sqrt{3}} \int \frac{1}{F} \cdot \frac{t}{t^2 + 3} dt = \frac{G_s}{\sqrt{3} F} \int \frac{1}{t^2 + 3} dt$$

因此: 第二阶段:

$\epsilon_z = \frac{G_s}{E} + \sqrt{\frac{G_s}{F}}$

第二阶段中的剪切塑性变形:

由于: $dS_{\theta\phi} = 0$, $dG_m \delta_{ij} = 0$, 只需计算: $d\epsilon_p = d\lambda S_{ij} = \frac{3 d\sigma_s}{2F} \cdot T_{\theta\phi}$

其中: $T_{\theta\phi} = \frac{1}{\sqrt{3}} G_s$, 则: $d\epsilon_p = \frac{3 G_s}{2\sqrt{3} F} \cdot \frac{1}{\sqrt{G_z^2 + 3 T_{\theta\phi}^2}} dG_z$

$$= \frac{1}{2} \int \frac{G_s}{\sqrt{G_z^2 + 3 T_{\theta\phi}^2}} dG_z = \frac{1}{2} \int \frac{1}{\sqrt{1 + 3 T_{\theta\phi}^2 / G_s^2}} dG_z = \frac{1}{2} \int \frac{1}{\sqrt{1 + 3}} dG_z = \frac{1}{2} \sqrt{3} T_{\theta\phi} \ln 2 = 2\sqrt{\frac{G_s}{F}} \ln 2$$

有: $\epsilon_p = \sqrt{\frac{G_s}{F}} = \frac{1}{2}$

因此有: $\epsilon_z = \frac{G_s}{E} + \sqrt{\frac{G_s}{F}} + G_s(1 - \frac{\pi}{4})$

$\gamma_{\theta\phi} = \frac{2 G_s(1+\nu)}{\sqrt{3} E} + 2\sqrt{\frac{G_s}{F}} + \frac{\sqrt{3} G_s}{F} \ln 2$

各阶段积分部分: 注意:

第一个弹性变形部分:

$\int \frac{G_s}{\sqrt{G_z^2 + 3 T_{\theta\phi}^2}} dG_z = \int \frac{1}{\sqrt{1 + 3 T_{\theta\phi}^2 / G_s^2}} dG_z$

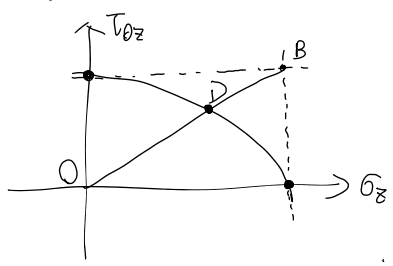
$$= \int \frac{1}{\sqrt{1 + 3}} dG_z = \frac{1}{\sqrt{4}} G_z = \frac{1}{2} G_z$$

第二个塑性变形部分:

$d\epsilon_p = \frac{3 d\sigma_s}{2\sqrt{3} F} \cdot \frac{1}{\sqrt{G_z^2 + 3 T_{\theta\phi}^2}} dG_z$

$$= \frac{3}{2\sqrt{3} F} \int \frac{1}{\sqrt{1 + 3 T_{\theta\phi}^2 / G_s^2}} dG_z = \frac{3}{2\sqrt{3} F} \int \frac{1}{\sqrt{1 + 3}} dG_z = \frac{3}{2\sqrt{3} F} G_z \ln 2 = \frac{3 G_s}{2\sqrt{3} F} \ln 2$$

(3). 加载路径为: ODB 路径时: 有 $G_z: T_{\theta\phi} = \sqrt{3}:1$, 此时: 需要考虑屈服曲面前后的值:



由: $G_i = \sqrt{\frac{1}{2}[(\sigma_z - \sigma_s)^2 + (\sigma_z + \sigma_s)^2 + (T_{\theta\phi}^2 + T_{\theta\phi}^2 + T_{\theta\phi}^2)]}$ 其中使用柱面坐标系:

得: $G_i = \sqrt{G_z^2 + 3 T_{\theta\phi}^2} = G_s$

此时保持 $G_z = \sqrt{3} T_{\theta\phi}$, 有 $\sqrt{6 T_{\theta\phi}^2} = G_s \Rightarrow T_{\theta\phi}^2 = \frac{G_s^2}{6}$

则: $T_{\theta\phi} = \frac{G_s}{\sqrt{6}}, G_z = \frac{G_s}{\sqrt{2}}$

在积分中, 直接代入即可:

由本构方程: $\epsilon_{ij} = \frac{1}{2\mu} S_{ij} + \frac{1-2\nu}{E} \sigma_m \delta_{ij} + \lambda S_{ij}$

其中: 由强化本构关系

此时第一阶段总的变形:

$\epsilon_z = \frac{G_s}{E}$

由本构方程: $\varepsilon_{ij} = \frac{1}{2\mu} S_{ij} + \frac{1-2\nu}{E} \sigma_{ij} \delta_{ij} + \lambda \cdot S_{ij}$

其中: 由强化本构关系: $\lambda = \frac{3 d\sigma_i}{2H\sigma_i} = \frac{3 d\sigma_i}{2F\sigma_i}$

有: ①: 第一阶段(屈服前) 有: $\lambda = 0$

代入: $\varepsilon_{ij} = \frac{1}{2\mu} S_{ij} + \frac{1-2\nu}{E} \sigma_{ij} \delta_{ij}$

即 $d\varepsilon_z = \frac{1}{2\mu} dS_z + \frac{1-2\nu}{E} d\sigma_z$, 其中: $\int dS_z = \frac{2}{3} \sigma_s \times \frac{\sqrt{2}}{2}$

得 $\varepsilon_z = \frac{1}{3\mu} \sigma_s + \frac{1-2\nu}{E} \sigma_s = \frac{2(1+\nu)}{3E} \sigma_s + \frac{1-2\nu}{E} \sigma_s = \frac{\sigma_s}{E} \Rightarrow \sigma_z = \frac{\sqrt{2}}{2} \sigma_s$

此时: $\gamma_{\theta z} = 2 \cdot \left(\frac{1}{2\mu} dS_{\theta z} + \frac{1-2\nu}{E} \cdot 0 \right)$
 $= \frac{2(1+\nu)}{E} \cdot \frac{\sqrt{6}}{3} \sigma_s = \frac{\sqrt{6}(1+\nu)}{3E} \sigma_s$

此时第一阶段的变形为:

$$\varepsilon_z = \frac{\sigma_s}{E} \times \frac{\sqrt{2}}{2}$$

$$\gamma_{\theta z} = \frac{\sqrt{6}(1+\nu)}{3E} \sigma_s$$

②. 塑性阶段:

由本构方程: $d\varepsilon_{ij} = \frac{1}{2\mu} dS_{ij} + \frac{1-2\nu}{E} d\sigma_{ij} + d\lambda \cdot S_{ij}$ 其中 $d\lambda = \frac{3 d\sigma_i}{2F\sigma_i}$

对于 z 方向: 有: $\sigma_z: \frac{\sigma_s}{\sqrt{2}} \rightarrow \sigma_s$

(1). z 方向形变量:

$\tau_{\theta z}: \frac{\sigma_s}{\sqrt{6}} \rightarrow \frac{\sigma_s}{\sqrt{3}}$

其中: $d\sigma_i = \sqrt{\sigma_z^2 + 3\tau_{\theta z}^2}$, 由 $\sigma_z = \sqrt{2}\tau_{\theta z}$

可得: $= \sqrt{2} d\sigma_z$, 而 $\sigma_i = \sqrt{2}\sigma_z$

$\int d\varepsilon_z = \int \left[\frac{1+\nu}{E} d\sigma_z + \frac{1-2\nu}{E} d\sigma_z + \frac{3}{2F} \cdot \frac{E d\sigma_z}{\sigma_z} \cdot \frac{1}{3} \sigma_z \right]$
 $\int d\varepsilon_z = \frac{1+\nu}{E} \times \frac{2}{3} \left(1 - \frac{\sqrt{2}}{2}\right) \sigma_s + \frac{1-2\nu}{E} \cdot \frac{\sigma_s}{3} \left(1 - \frac{\sqrt{2}}{2}\right) + \frac{1}{F} \cdot \left(1 - \frac{\sqrt{2}}{2}\right) \sigma_s$
 $= \frac{\sigma_s}{E} \left(1 - \frac{\sqrt{2}}{2}\right) + \frac{3}{2F} \cdot \frac{1}{2} \ln 2 = \left(1 - \frac{\sqrt{2}}{2}\right) \frac{\sigma_s}{E} + \frac{\sigma_s}{F} \left(1 - \frac{\sqrt{2}}{2}\right)$

注意别漏乘 S_{ij} ,

同理 $\frac{d\sigma_i}{\sigma_i} = \frac{d\tau_{\theta z}}{\tau_{\theta z}}$

(2). θz 方向的夹角改变:

$d\varepsilon_{\theta z} = \frac{1+\nu}{E} d\tau_{\theta z} + \frac{3}{2F} \cdot \frac{d\tau_{\theta z}}{\tau_{\theta z}} \cdot \tau_{\theta z}$

得到第二阶段的形变量表达式:

$\varepsilon_{\theta z} = \int d\varepsilon_{\theta z} = \frac{(1+\nu)}{E} \sigma_s \left(\frac{1}{\sqrt{3}} - \frac{1}{\sqrt{6}} \right) + \frac{3}{2F} \cdot \sigma_s \left(\frac{1}{\sqrt{3}} - \frac{1}{\sqrt{6}} \right)$
 $= \frac{\sqrt{6}(1+\nu)\sigma_s}{3E} (\sqrt{2}-1) + \frac{\sqrt{6}\sigma_s}{3F} (\sqrt{2}-1)$
 $\gamma_{\theta z} = \left(\frac{\sqrt{6}\sigma_s}{3E} + \frac{\sqrt{6}\sigma_s}{2F} \right) (\sqrt{2}-1)$
 $= \sigma_s \left(\frac{\sqrt{6}}{3E} (1+\nu) + \frac{\sqrt{6}}{2F} \right) (\sqrt{2}-1)$
 $\gamma_{\theta z} = \frac{3}{F} \left(\frac{1}{\sqrt{3}} - \frac{1}{\sqrt{6}} \right) = \frac{\sqrt{3}}{F} \left(1 - \frac{\sqrt{2}}{2}\right)$

两式相加: 有:

$\varepsilon_z = \frac{\sigma_s}{E} \times \frac{\sqrt{2}}{2} + \frac{\sigma_s}{E} \left(1 - \frac{\sqrt{2}}{2}\right) + \frac{\sigma_s}{F} \left(1 - \frac{\sqrt{2}}{2}\right)$

$$= \frac{G_s}{E} + \left(1 - \frac{\sqrt{2}}{2}\right) \frac{G_s}{F} \quad \checkmark$$

$$\gamma_{\theta z} = \frac{\cancel{\sqrt{6}}(1+\nu)}{3E} G_s + \frac{\sqrt{6}(1+\nu)}{3E} (\sqrt{2}-1) G_s + \frac{\sqrt{6}}{2F} G_s (\sqrt{2}-1)$$

$$= \frac{2\sqrt{3}(1+\nu)}{3E} G_s + \frac{\sqrt{6} G_s}{2F} (\sqrt{2}-1) \quad \text{由于 } \mu = \frac{2(1+\nu)}{E}$$

$$= \frac{G_s}{\sqrt{3} \mu} + \frac{\sqrt{3}}{F} \left(1 - \frac{1}{\sqrt{2}}\right)$$