

大挠度薄板的里兹法与中面变形能推导

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一、里兹法:

由薄板变形能:
$$U = \frac{1}{2} \iiint (\sigma_x^2 \epsilon_x^2 + \sigma_y^2 \epsilon_y^2 + \tau_{xy}^2 \gamma_{xy}^2) dx dy dz$$

我们已经在挠度问题基本方程中推出 $\sigma_x^2, \epsilon_x^2, \dots$ 表达式.

则
$$U = \frac{1}{2} \iiint \left\{ \left[\sigma_x - \frac{Ez}{1-\nu^2} \left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2} \right) \right] \cdot \left(\epsilon_x - z \frac{\partial^2 w}{\partial x^2} \right) \right. \\ \left. + \left[\sigma_y - \frac{Ez}{1-\nu^2} \left(\frac{\partial^2 w}{\partial y^2} + \nu \frac{\partial^2 w}{\partial x^2} \right) \right] \cdot \left(\epsilon_y - z \frac{\partial^2 w}{\partial y^2} \right) \right. \\ \left. + \left[\tau_{xy} - \frac{Ez}{1+\nu} \frac{\partial^2 w}{\partial x \partial y} \right] \cdot \left(\gamma_{xy} - 2z \frac{\partial^2 w}{\partial x \partial y} \right) \right\} dx dy dz$$

★ 将变形能 U 分解为薄板力变形能与弯曲变形能之和, 有: $U = U_m + U_b$

$$U_m = \frac{h}{2} \iint_A (\sigma_x \epsilon_x + \sigma_y \epsilon_y + \tau_{xy} \gamma_{xy}) dx dy$$
 ← 对 z 积分, 得 (其中: $\sigma_x, \sigma_y, \dots, \epsilon_x, \dots$ 为常数)

$$U_b = \frac{1}{2} \int_{-h/2}^{h/2} \frac{Ez^2}{1-\nu^2} \left[\left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2} \right) \frac{\partial^2 w}{\partial x^2} \right. \\ \left. + \left(\frac{\partial^2 w}{\partial y^2} + \nu \frac{\partial^2 w}{\partial x^2} \right) \frac{\partial^2 w}{\partial y^2} + 2(1-\nu) \left(\frac{\partial^2 w}{\partial x \partial y} \right)^2 \right] dz$$

$$\int_{-h/2}^{h/2} z^3 dz = \frac{1}{4} \left[\frac{h^3}{8} + \frac{h^3}{8} \right] = \frac{1}{4} \left[\frac{h^3}{4} \right] = \frac{h^3}{16}$$

$$U_b = \frac{D}{2} \iint_A \left[\left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2} \right) \frac{\partial^2 w}{\partial x^2} + \left(\frac{\partial^2 w}{\partial y^2} + \nu \frac{\partial^2 w}{\partial x^2} \right) \frac{\partial^2 w}{\partial y^2} + 2(1-\nu) \left(\frac{\partial^2 w}{\partial x \partial y} \right)^2 \right] dx dy dz$$

$$= \frac{D}{2} \iint_A \left[\left(\frac{\partial^2 w}{\partial x^2} \right)^2 + \left(\frac{\partial^2 w}{\partial y^2} \right)^2 + 2\nu \frac{\partial^2 w}{\partial x^2} \frac{\partial^2 w}{\partial y^2} + 2(1-\nu) \left(\frac{\partial^2 w}{\partial x \partial y} \right)^2 \right] dx dy dz$$
 (2)

利用 $\epsilon_x, \epsilon_y, \gamma_{xy}$ 和 $\sigma_x, \sigma_y, \tau_{xy}$ 的关系: $\begin{cases} \epsilon_x = \frac{1}{E} (\sigma_x - \nu \sigma_y) \\ \epsilon_y = \frac{1}{E} (\sigma_y - \nu \sigma_x) \\ \gamma_{xy} = \frac{\tau_{xy}}{G} = \frac{2(1+\nu)}{E} \tau_{xy} \end{cases}$ 则中面变形能 U_m 成为

$$U_m = \frac{h}{2E} \iint_A [(\sigma_x + \sigma_y) - 2(1+\nu) (\sigma_x \epsilon_y - \tau_{xy}^2)] dx dy$$
 (3) 应力表达式

$$= \frac{h}{2E} \iint_A \left\{ \left[\left(\frac{\partial^2 w}{\partial x^2} \right)^2 + \left(\frac{\partial^2 w}{\partial y^2} \right)^2 + 2\nu \frac{\partial^2 w}{\partial x^2} \frac{\partial^2 w}{\partial y^2} + 2(1-\nu) \left(\frac{\partial^2 w}{\partial x \partial y} \right)^2 \right] \right\} dx dy$$
 (应变表达式)

也可利用: $\sigma_x = \frac{E}{1-\nu^2} (\epsilon_x + \nu \epsilon_y), \sigma_y = \frac{E}{1-\nu^2} (\epsilon_y + \nu \epsilon_x), \tau_{xy} = \frac{E}{2(1+\nu)} \gamma_{xy}$

$$U_m = \frac{Eh}{2(1-\nu^2)} \iint_A \left[\epsilon_x^2 + \epsilon_y^2 + 2\nu \epsilon_x \epsilon_y + \frac{1-\nu}{2} \gamma_{xy}^2 \right] dx dy$$
 (应变表达式)

代入应变公式, 即:
$$\begin{cases} \epsilon_x = \frac{\partial u}{\partial x} + \frac{1}{2} \left(\frac{\partial w}{\partial x} \right)^2, \epsilon_y = \frac{\partial v}{\partial y} + \frac{1}{2} \left(\frac{\partial w}{\partial y} \right)^2 \\ \gamma_{xy} = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} + \frac{\partial w}{\partial x} \frac{\partial w}{\partial y} \end{cases}$$

故:

$$U_m = \frac{Eh}{2(1-\nu^2)} \iint_A \left\{ \left[\left(\frac{\partial u}{\partial x} \right)^2 + \frac{1}{4} \left(\frac{\partial w}{\partial x} \right)^4 + \frac{\partial u}{\partial x} \left(\frac{\partial w}{\partial x} \right)^2 \right] + \left[\left(\frac{\partial v}{\partial y} \right)^2 + \frac{1}{4} \left(\frac{\partial w}{\partial y} \right)^4 + \frac{\partial v}{\partial y} \left(\frac{\partial w}{\partial y} \right)^2 \right] \right. \\ \left. + 2\nu \left(\frac{\partial u}{\partial x} + \frac{1}{2} \left(\frac{\partial w}{\partial x} \right)^2 \right) \left(\frac{\partial v}{\partial y} + \frac{1}{2} \left(\frac{\partial w}{\partial y} \right)^2 \right) + \frac{1-\nu}{2} \left[\left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} + \frac{\partial w}{\partial x} \frac{\partial w}{\partial y} \right)^2 \right] \right\} dx dy$$

$$\begin{aligned}
 & + \frac{1-\nu}{2} \left\{ \left(\frac{\partial u}{\partial y} \right)^2 + \left(\frac{\partial v}{\partial x} \right)^2 + \left(\frac{\partial w}{\partial x} \frac{\partial w}{\partial y} \right)^2 + 2 \left[\frac{\partial u}{\partial y} \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \frac{\partial w}{\partial x} \frac{\partial w}{\partial y} + \frac{\partial v}{\partial x} \frac{\partial w}{\partial x} \frac{\partial w}{\partial y} \right] \right\} \\
 & = \frac{Eh}{2(1-\nu^2)} \iint \left\{ \left[\left(\frac{\partial u}{\partial x} \right)^2 + \frac{\partial u}{\partial x} \frac{\partial w}{\partial x} \right] + \left(\frac{\partial v}{\partial y} \right)^2 + \frac{\partial v}{\partial y} \left(\frac{\partial w}{\partial y} \right) \right] + \frac{1}{4} \left[\left(\frac{\partial w}{\partial x} \right)^2 + \left(\frac{\partial w}{\partial y} \right)^2 \right] \right. \\
 & \quad \left. + 2\nu \left[\frac{\partial u}{\partial x} \frac{\partial v}{\partial y} + \frac{1}{2} \left(\frac{\partial w}{\partial x} \right)^2 \frac{\partial v}{\partial y} + \left(\frac{\partial w}{\partial y} \right)^2 \frac{\partial u}{\partial x} \right] \right. \\
 & \quad \left. + \frac{1-\nu}{2} \left\{ \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right)^2 + 2 \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) \frac{\partial w}{\partial x} \frac{\partial w}{\partial y} \right\} \right\} dx dy
 \end{aligned}$$

此时：作用于平板上的横向载荷 $q(x,y)$ ，外力功为：↓

$$W = \iint q(x,y) w \, dx dy$$

故薄板大挠度有：总势能

$$\Pi = U_m + U_b - W$$

$$\begin{aligned}
 & \frac{1-\nu}{2} \left(\frac{\partial w}{\partial x} \right)^2 \left(\frac{\partial w}{\partial y} \right)^2 + \frac{2\nu}{4} \left(\frac{\partial w}{\partial x} \right)^2 \left(\frac{\partial w}{\partial y} \right)^2 \\
 & = \frac{1}{2} \left(\frac{\partial w}{\partial x} \right)^2 \left(\frac{\partial w}{\partial y} \right)^2, \text{ 和上面合并}
 \end{aligned}$$

在使用里兹法做近似解时，首先假设挠度函数 w 为

$$w = a_1 \varphi_1(x,y) + a_2 \varphi_2(x,y) + \dots + a_n \varphi_n(x,y) = \sum_{i=1}^n a_i \varphi_i(x,y)$$

对满足的协调方程：

$$\frac{1}{E} \nabla^4 F = \left(\frac{\partial^2 w}{\partial x \partial y} \right)^2 + \frac{\partial^2 w}{\partial x^2} \frac{\partial^2 w}{\partial y^2}, \text{ 积分该式}$$

将 w 代入可得 $F(x,y)$ 表达式，并令：

$$\frac{\partial \Pi}{\partial a_1} = \frac{\partial \Pi}{\partial a_2} = \dots = \frac{\partial \Pi}{\partial a_n} = 0, \text{ 即可解出参数并确定 } w,$$