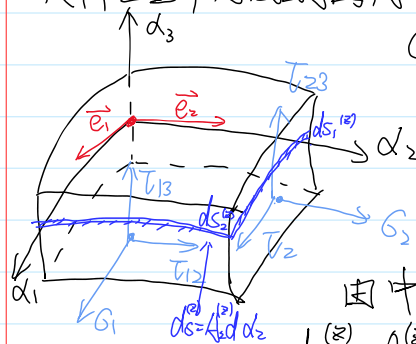


壳体的内力和内矩平衡方程

Friday, November 10, 2023 9:20 AM

1. 壳体内沿 $\alpha_1, \alpha_1 + d\alpha_1, \alpha_2, \alpha_2 + d\alpha_2$ 主坐标线方向
取四个垂面中曲面的面得到一个微元体



σ_1, σ_2 为微元体侧面上的正应力。

而在薄壳理论中, 认为
厚度方向忽略应力, 即有:

$$\sigma_3 = 0$$

由中曲面弧长 $ds_2 = R_2 d\alpha_2$,

$$ds_2^{(2)} = A_2^{(2)} d\alpha_2 = (1 + \frac{z}{R_2}) ds_2$$

此时: 由 $A_2^{(2)} = (1 + \frac{z}{R_2}) A_2$, 则有:

$$N_1 = \int_{-\frac{h}{2}}^{\frac{h}{2}} \sigma^{(2)} dz ds_2^{(2)} \rightarrow \text{认为 } \sigma^{(2)} \text{ 在积分区间内均为 } \sigma, \text{ 则}$$

当我们取单位弧长时, 则 $ds_2 = 1$.

$$\begin{cases} N_1 = \int_{-\frac{h}{2}}^{\frac{h}{2}} \sigma (1 + \frac{z}{R_2}) dz \\ N_2 = \int_{-\frac{h}{2}}^{\frac{h}{2}} \tau_{12} (1 + \frac{z}{R_2}) dz \\ Q_1 = \int_{-\frac{h}{2}}^{\frac{h}{2}} \tau_{13} (1 + \frac{z}{R_2}) dz \end{cases} \quad \text{变为} \quad \begin{cases} N_1 = \int_{-\frac{h}{2}}^{\frac{h}{2}} \sigma (1 + \frac{z}{R_2}) dz \\ S_{12} = \int_{-\frac{h}{2}}^{\frac{h}{2}} \tau_{12} (1 + \frac{z}{R_2}) dz \\ Q_1 = \int_{-\frac{h}{2}}^{\frac{h}{2}} \tau_{13} (1 + \frac{z}{R_2}) dz \end{cases}$$

相应地 \Rightarrow 作用在壳体的力矩为:

$$\begin{cases} M_1 = \int_{-\frac{h}{2}}^{\frac{h}{2}} \sigma z (1 + \frac{z}{R_2}) dz \\ H_{12} = \int_{-\frac{h}{2}}^{\frac{h}{2}} \tau_{12} z (1 + \frac{z}{R_2}) dz \end{cases}$$

因此, 壳体总的内力与内矩可以用如下量描述:

$$\begin{Bmatrix} N_1 \\ N_2 \\ Q_1 \\ Q_2 \\ M_1 \\ M_2 \\ H_{12} \\ H_{21} \end{Bmatrix}$$

※ 需要说明: 即使有剪应力
若有 10 个量, 互等定律, 但由于 $R_1 R_2$
不相等, 故 $S_{12} \neq S_{21}, H_{12} \neq H_{21}$

有关系

$$\textcircled{1} N_1 = \int_{-\frac{h}{2}}^{\frac{h}{2}} \sigma (1 + \frac{z}{R_2}) dz = \sigma_1 h \quad \leftarrow \text{后面一项为 } (\frac{h^2}{2} - \frac{h^2}{2}) = 0$$

$$\textcircled{2} M_1 = \int_{-\frac{h}{2}}^{\frac{h}{2}} \sigma z (1 + \frac{z}{R_2}) dz = \sigma_1 z \Big|_{-\frac{h}{2}}^{\frac{h}{2}} + \sigma_1 \frac{z^2}{2R_2} \Big|_{-\frac{h}{2}}^{\frac{h}{2}} = 0 + \frac{\sigma_1 h^3}{12 R_2} \rightarrow R_2 = \frac{\sigma_1 h^3}{12 M_1}$$

$$\begin{aligned} \rightarrow \sigma_1^{(2)} = \sigma_1 (1 + \frac{z}{R_2}) &= \frac{N_1}{h} + \frac{12 M_1}{h^3} z \quad \textcircled{1} \\ \text{同理有 } \sigma_2^{(2)} = \sigma_2 (1 + \frac{z}{R_2}) &= \frac{N_2}{h} + \frac{12 M_2}{h^3} z \quad \textcircled{2} \end{aligned}$$

$$\text{而: } N_2 = \int_{-\frac{h}{2}}^{\frac{h}{2}} \tau_{12} (1 + \frac{z}{R_2}) dz = \tau_{12} h$$

$$H_{12} = \int_{-\frac{h}{2}}^{\frac{h}{2}} \tau_{12} z (1 + \frac{z}{R_2}) dz = \tau_{12} \frac{h^3}{12 R_2}$$

$$\text{得 } \tau_{12}^{(2)} = \tau_{12} (1 + \frac{z}{R_2}) = \frac{N_{12}}{h} + \frac{12 H_{12}}{h^3} z \quad \textcircled{3}$$

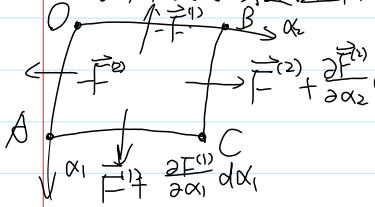
$$\text{同理 } \tau_{21}^{(2)} = \tau_{21} (1 + \frac{z}{R_1}) = \frac{N_{21}}{h} + \frac{12 H_{21}}{h^3} z \quad \textcircled{4}$$

薄膜

弯曲应力、

当壳体微元四条边上作用 F, M, Q 且表面力有 q_1, q_2, q_3 时

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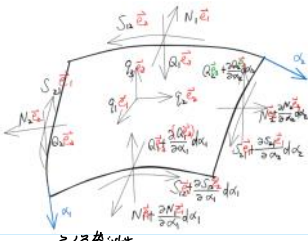


其中, F 由正应力, 剪力, 弯矩共同构成, 故有:

边缘外力为:

$$\vec{F}^{(1)} = -(N_1 \vec{e}_1 + S_{12} \vec{e}_2 + Q_1 \vec{e}_3) A_2 d\alpha_2$$

$$\vec{F}^{(2)} = -(N_2 \vec{e}_1 + S_{21} \vec{e}_2 + Q_2 \vec{e}_3) A_1 d\alpha_1$$



注意!!!

整体偏导, 而非展开偏导 (因是向量, 考虑 $\vec{e}_1, \vec{e}_2, \vec{e}_3$ 非

$\alpha_1, \alpha_2, \alpha_3$ 导数)

由于 $A, d\alpha_1$ 等列平衡方程为:

$$(\vec{F}^{(1)} + \frac{\partial \vec{F}^{(1)}}{\partial \alpha_1} d\alpha_1) - \vec{F}^{(1)} + (\vec{F}^{(2)} + \frac{\partial \vec{F}^{(2)}}{\partial \alpha_2} d\alpha_2) - \vec{F}^{(2)} + \vec{q} A_1 A_2 d\alpha_1 d\alpha_2 = \vec{0}$$

$$\Rightarrow \text{有: } \frac{\partial \vec{F}^{(1)}}{\partial \alpha_1} d\alpha_1 + \frac{\partial \vec{F}^{(2)}}{\partial \alpha_2} d\alpha_2 + \vec{q} A_1 A_2 d\alpha_1 d\alpha_2 = \vec{0} \quad \text{平衡方程}$$

$$\frac{\partial}{\partial \alpha_1} [(N_1 \vec{e}_1 + S_{12} \vec{e}_2 + Q_1 \vec{e}_3) A_2 d\alpha_2] + \frac{\partial}{\partial \alpha_2} [(S_{21} \vec{e}_1 + N_2 \vec{e}_2 + Q_2 \vec{e}_3) A_1 d\alpha_1] + \vec{q} A_1 A_2 d\alpha_1 d\alpha_2 = \vec{0}$$

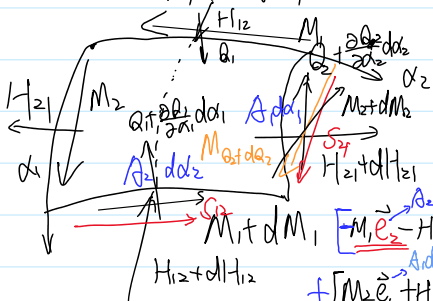
$$\begin{aligned} & \left[\frac{\partial(N_1 A_2)}{\partial \alpha_1} \vec{e}_1 + N_1 A_2 \frac{\partial \vec{e}_1}{\partial \alpha_1} + \frac{\partial(S_{12} A_2)}{\partial \alpha_1} \vec{e}_2 + S_{12} A_2 \frac{\partial \vec{e}_2}{\partial \alpha_1} + \frac{\partial(Q_1 A_2)}{\partial \alpha_1} \vec{e}_3 + Q_1 A_2 \frac{\partial \vec{e}_3}{\partial \alpha_1} \right] \\ & + \left[\frac{\partial(S_{21} A_1)}{\partial \alpha_2} \vec{e}_1 + S_{21} A_1 \frac{\partial \vec{e}_1}{\partial \alpha_2} + \frac{\partial(N_2 A_1)}{\partial \alpha_2} \vec{e}_2 + N_2 A_1 \frac{\partial \vec{e}_2}{\partial \alpha_2} + \frac{\partial(Q_2 A_1)}{\partial \alpha_2} \vec{e}_3 + Q_2 A_1 \frac{\partial \vec{e}_3}{\partial \alpha_2} \right] \end{aligned}$$

$$\begin{aligned} \frac{\partial \vec{e}_1}{\partial \alpha_1} &= -\frac{1}{A_2} \frac{\partial A_1}{\partial \alpha_2} \vec{e}_2 - \frac{A_1}{R_1} \vec{e}_3 & \frac{\partial \vec{e}_1}{\partial \alpha_2} &= \frac{1}{A_1} \frac{\partial A_2}{\partial \alpha_1} \vec{e}_1 \\ \frac{\partial \vec{e}_2}{\partial \alpha_1} &= \frac{1}{A_2} \frac{\partial A_1}{\partial \alpha_2} \vec{e}_1 & \frac{\partial \vec{e}_2}{\partial \alpha_2} &= -\frac{1}{A_1} \frac{\partial A_2}{\partial \alpha_1} \vec{e}_1 - \frac{A_2}{R_2} \vec{e}_3 \\ \frac{\partial \vec{e}_3}{\partial \alpha_1} &= \frac{A_1}{R_1} \vec{e}_1 & \frac{\partial \vec{e}_3}{\partial \alpha_2} &= \frac{A_2}{R_2} \vec{e}_2 \end{aligned}$$

$$\begin{aligned} \vec{e}_1: & \frac{\partial(N_1 A_2)}{\partial \alpha_1} + S_{12} \frac{\partial A_1}{\partial \alpha_2} + \frac{Q_1 A_1 A_2}{R_1} + \frac{\partial(S_{12} A_2)}{\partial \alpha_1} - N_2 \frac{\partial A_2}{\partial \alpha_1} + A_1 A_2 q_1 = 0 \\ \vec{e}_2: & -N_1 \frac{\partial A_1}{\partial \alpha_2} + \frac{\partial(S_{12} A_2)}{\partial \alpha_1} + S_{21} \frac{\partial A_2}{\partial \alpha_1} + \frac{\partial(N_2 A_1)}{\partial \alpha_2} + \frac{Q_2 A_1 A_2}{R_2} + A_1 A_2 q_2 = 0 \\ \vec{e}_3: & -N_1 \frac{A_1 A_2}{R_1} + \frac{\partial(Q_1 A_2)}{\partial \alpha_1} - N_2 \frac{A_1 A_2}{R_2} + \frac{\partial(Q_2 A_1)}{\partial \alpha_2} + A_1 A_2 q_3 = 0 \end{aligned}$$

而内矩的平衡条件如下:

平衡方程的矢量式:



首先: q 对于任一轴的力矩近似为

$$q A_1 A_2 d\alpha_1 d\alpha_2 \approx \frac{1}{2} A_1 d\alpha_1 + \frac{1}{2} A_2 d\alpha_2$$

\Rightarrow 为 $d\alpha$ 高阶微量 \rightarrow 可略, 内力矩考虑 Q, S 则:

弯矩矩和内力矩矩和为 0, 外力矩考虑 M 则:

$$\begin{aligned} & [M_1 \vec{e}_1 + H_{12} \vec{e}_2 + \frac{\partial H_{12} \vec{e}_2}{\partial \alpha_1} d\alpha_1] A_2 d\alpha_2 - (Q_1 \vec{e}_3 + \dots) A_1 d\alpha_1 A_2 d\alpha_2 + (S_{12} \vec{e}_3 + \dots) A_1 A_2 d\alpha_1 d\alpha_2 \\ & + [M_2 \vec{e}_1 + H_{12} \vec{e}_1 - \frac{\partial M_2 \vec{e}_1}{\partial \alpha_2} d\alpha_2] A_1 d\alpha_1 - (Q_2 \vec{e}_3 + \dots) A_1 d\alpha_1 A_2 d\alpha_2 - (S_{21} \vec{e}_3 + \dots) A_1 A_2 d\alpha_1 d\alpha_2 = 0 \end{aligned}$$

$$\left[H_{12} + dH_{12} + \left[M_2 \vec{e}_1 + H_{12} \vec{e}_1 - \left(M_2 \vec{e}_1 + \frac{\partial M_2}{\partial \alpha_2} d\alpha_2 \right) \left(H_{12} \vec{e}_1 + \frac{\partial H_{12}}{\partial \alpha_1} d\alpha_1 \right) + (Q_2 \vec{e}_1 + \dots) A_1 d\alpha_1 d\alpha_2 - (S_{21} \vec{e}_3 + \dots) A_1 A_2 d\alpha_1 d\alpha_2 \right] \right] = 0$$

此时,略去 $d\alpha$ 的高阶小量,得到:

$$\left[\frac{\partial(A_1 H_{12} \vec{e}_1)}{\partial \alpha_2} + \frac{\partial(A_2 M_1 \vec{e}_2)}{\partial \alpha_1} - Q_1 A_1 A_2 \vec{e}_2 + S_2 A_1 A_2 \vec{e}_3 \right] + \left[-\frac{\partial(A_1 M_2 \vec{e}_2)}{\partial \alpha_2} - \frac{\partial(A_2 H_{12} \vec{e}_1)}{\partial \alpha_1} + Q_2 A_1 A_2 \vec{e}_1 - S_1 A_1 A_2 \vec{e}_3 \right] = 0$$

(注意乘积的边长!)

代入微分公式(4个,略)有:

$$\vec{e}_2: \frac{\partial(A_1 H_{12})}{\partial \alpha_2} + \frac{\partial(A_2 M_1)}{\partial \alpha_1} + H_{12} \frac{\partial A_1}{\partial \alpha_2} - M_2 \frac{\partial A_2}{\partial \alpha_1} - Q_1 A_1 A_2 = 0 \quad \text{化简有:}$$

★ 板内平衡方程

$$\textcircled{1} \quad \frac{\partial(A_2 M_1)}{\partial \alpha_1} + \frac{\partial(A_1 H_{12})}{\partial \alpha_2} - M_2 \frac{\partial A_2}{\partial \alpha_1} + H_{12} \frac{\partial A_1}{\partial \alpha_2} - Q_1 A_1 A_2 = 0$$

$$\vec{e}_1: -H_{21} \frac{\partial A_2}{\partial \alpha_1} + M_1 \frac{\partial A_1}{\partial \alpha_2} - \frac{\partial(A_1 M_2)}{\partial \alpha_2} - \frac{\partial(A_2 H_{12})}{\partial \alpha_1} + Q_2 A_1 A_2 = 0, \text{得:}$$

$$\textcircled{2} \quad \frac{\partial(A_2 M_2)}{\partial \alpha_2} + \frac{\partial(A_1 H_{12})}{\partial \alpha_1} - M_1 \frac{\partial A_1}{\partial \alpha_2} + H_{21} \frac{\partial A_2}{\partial \alpha_1} - Q_2 A_1 A_2 = 0$$

$$\vec{e}_3: -\frac{A_1 A_2}{R_2} H_{21} + S_{12} A_1 A_2 + H_{12} \frac{A_2 A_1}{R_1} - S_{21} A_1 A_2 = 0$$

$$\textcircled{3} \quad \frac{H_{12}}{R_1} - \frac{H_{21}}{R_2} = S_{21} - S_{12}$$

由等式(切应力互等)
 $\tau_{12} = \tau_{21}$
 自然满足