

Introduction to Feedback

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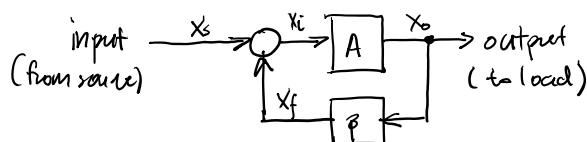
- Desensitize gain
- Reduce Distortion
- Extend BW
- Control I/O impedance
- ↑ Signal to noise ratio.

Recall OPamps has: $BW \sim 10\text{Hz}$
Gain $\sim 1 \times 10^6$

By having a gain of 100, BW would be 100kHz.

- Voltage amplifier: High R_i , Low R_o
- Current amplifier: Low R_i , High R_o .
- Transconductance amplifier: Feedback drives up both R_i , R_o .
- Transimpedance —: low R_i , R_o .

Basic Feedback Configuration



Ideally: $x_o = A x_i$

$$x_f = \beta x_o$$

$$x_i = x_s - x_f$$

$$A_f = \frac{x_o}{x_s}$$

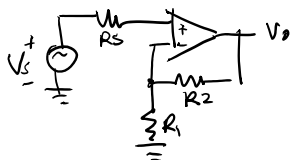
$$A_f = \frac{A}{1 + A\beta}$$

If $A \gg \beta$, then $A_f \approx \frac{1}{\beta}$, so $x_f = \beta x_o = A\beta x_i = A\beta(x_s - x_f)$

$$\Rightarrow x_f = \frac{A\beta x_s}{1 + A\beta} \approx x_s \text{ for } A\beta \gg 1.$$

output follows the input.

Ex. Consider OPAMP with negative feedback (non-inverting)



For open loop gain $A \rightarrow \infty$: Find A_f in terms of R_1 , R_2

$$V_f = V_s, V_n = V_o \left(\frac{R_1}{R_1 + R_2} \right)$$

Ideal negative feedback:

$$V_n = V_p$$

Gain with feedback:

$$A_f = \frac{V_o}{V_s} = \frac{R_1 + R_2}{R_1} = \frac{A}{1 + A\beta} = \frac{1}{\beta} \text{ (since } A \rightarrow \infty \text{)}$$

$$\text{Thus the feedback } \beta = \frac{R_1}{R_1 + R_2}$$

For open loop gain $A = 10^4$, and closed loop gain of $A_f = 100$: Find R_2/R_1

$$A_f = 100 = \frac{A}{1 + A\beta} = \frac{10^4}{1 + 10^4 \beta}$$

$$\text{Since } \beta = \frac{R_1}{R_1 + R_2} \text{ (from before)}$$

$$\text{Then } \beta = \frac{99/10000}{1} = \frac{R_1}{R_1 + R_2}$$

→ The amount of feedback β given as $|1 + A\beta|$

$$= \left| 1 + A \left(\frac{1}{1 + \frac{R_2}{R_1}} \right) \right|, A = 10^4, \frac{R_2}{R_1} = 100.01$$

$$= 20 \log_{10} (100)$$

$$= 40 \text{dB}$$

$$\text{then } R_1 + R_2 \text{ (from } \dots)$$

$$\text{Then } \beta = \frac{99}{10000} = \frac{R_2}{R_1 + R_2}$$

$$\rightarrow \frac{1}{1 + \frac{R_2}{R_1}} = \frac{99}{10000}$$

$$\frac{R_2}{R_1} = \frac{10000}{99} - 1$$

$$= \boxed{100.01}$$

$$= 20 \log_{10}(100) = \boxed{40 \text{ dB}}$$

For open loop gain $A = 7500$ (25% decrease), find A_f

$$A_f = \frac{A}{1 + A\beta}, \quad \beta = \frac{1}{1 + \frac{R_2}{R_1}}, \text{ and } \frac{R_2}{R_1} = 100.01$$

$$A_f = \frac{7500}{1 + 7500 \left(\frac{1}{1 + 100.01} \right)} = \boxed{91.67}$$

We see that we changed base gain by 25%, but the output gain didn't change that much (gain desensitivity)

Properties of negative feedback:

- Gain Desensitivity: can be found by taking $\frac{dA_f}{dA}$:

$$\frac{dA_f}{dA} = \frac{1}{1 + A\beta} - \frac{A\beta}{(1 + A\beta)^2} = \frac{1}{(1 + A\beta)^2}$$

$$dA_f = \left(\frac{1}{1 + A\beta} \right) \left(\frac{A}{1 + A\beta} \right) dA$$

$$\frac{dA_f}{A_f} = \frac{1}{1 + A\beta} \frac{dA}{A}$$

$\frac{1}{1 + A\beta}$ is the desensitivity factor

- Bandwidth Extension

Consider: Low pass single pole amplifier

$$A(s) = A_m \left(\frac{\omega_H}{s + \omega_H} \right) = \frac{A_m}{\left(\frac{s}{\omega_H} + 1 \right)}$$

Applying feedback:

$$A_f(s) = \frac{A_m \left(\frac{\omega_H}{s + \omega_H} \right)}{1 + A_m \left(\frac{\omega_H}{s + \omega_H} \right) \beta}$$

$$= \frac{A_m}{1 + \frac{s}{\omega_H} + A_m \beta}$$

$$= \frac{\left(\frac{A_m}{1 + A_m \beta} \right)}{\left(1 + \frac{s}{\omega_H (1 + A_m \beta)} \right)}$$

A_m reduced by a factor of $1 + A_m \beta$

ω_H increased by a factor of $1 + A_m \beta$

High pass single pole amplifier

$$A(s) = A_m \left(\frac{s}{s + \omega_L} \right)$$

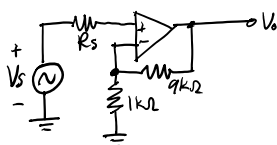
$$A_f(s) = \frac{A_m s}{s(1 + A_m \beta) + \omega_L}$$

$$= \frac{\left(\frac{A_m}{1 + A_m \beta} \right) s}{\left(s + \left(\frac{\omega_L}{1 + A_m \beta} \right) \right)}$$

A_m reduced by a factor of $1 + A_m \beta$

ω_L reduced by a factor of $1 + A_m \beta$

Ex.



$$\text{open loop } A = 1 \times 10^6$$

Low pass single pole amplifier: $\omega_L = 2\pi \cdot 10 \text{ rad/s}$

$$A(s) = A_m \left(\frac{2\pi(10)}{s + 2\pi(10)} \right)$$

$$V_n = \left(\frac{1k}{1k + 9k} \right) \cdot V_o, \quad V_n = V_p = V_s$$

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$$V_n = \left(\frac{1k}{1k+9k} \right) \cdot V_o, \quad V_n = V_p = V_s$$

$$V_o = \left(\frac{1k+9k}{1k} \right) V_s$$

$$A_f = \frac{V_o}{V_s} = 10$$

But also $A_f = \frac{A_{v2}}{1+A_{v2}\beta} \approx \frac{1}{\beta} \Rightarrow \beta \approx 0.10$

$$A_{mf} = \frac{10^6}{1+A_{mf}\beta} = \frac{10^6}{1+(10^6 \cdot 0.1)} = 9.9999$$

$$f_{Hf} = (10)(1+A_{mf}\beta) = (10)(1+10^6 \cdot 0.1) = 1.00001 \text{ MHz}$$

Nonlinear Distortion Reduction:

