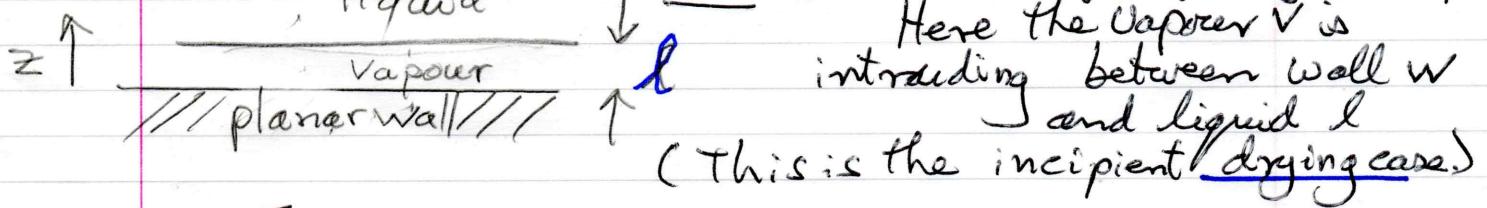


## Relating Local Compressibility $\chi(z)$

### to Contact Angle $\theta$ : Binding Pot.

In a binding pot. treatment we consider the excess grand pot. per unit area  $\omega^{ex}(l)$  as a function of a 'film thickness'  $l$ .



Here the vapour  $v$  is intruding between wall  $w$  and liquid  $l$

(This is the incipient drying case)

The equilibrium thickness  $l_{eq}$  minimizes

$$\omega^{ex}(l) = \gamma_{wv} + \gamma_{lv} + \omega_B(l) + \delta\mu \Delta\rho \quad (1)$$

$\downarrow$  surface tensions

$\delta\mu \equiv \mu - \mu_{co}(T)$  and  $\delta\mu = 0^+$  at coexistence,  
i.e. reservoir is a liquid

$\Delta\rho \equiv \rho_e - \rho_v$  is difference in coexisting densities

$\omega_B(l)$  is the binding potential.

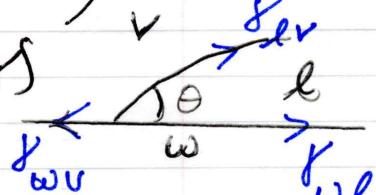
The wall-liquid tension

$$\gamma_{wl} = \omega^{ex}_{-eq}(l_{eq}) ; \delta\mu = 0^+ \quad (2)$$

$$\therefore \gamma_{wl} = \gamma_{wv} + \gamma_{lv} + \omega_B(l_{eq}) ; \delta\mu = 0^+$$

From Young's equation:

$$\frac{\gamma_{wl}}{\gamma_{wv}} = \frac{\gamma_{lv}}{\gamma_{wv}} \cos\theta \quad (3)$$



it follows

$$\omega_B(l_{eq}) = -\gamma_{lv}(\cos\theta + 1) \quad (3)$$

This is a standard result, used in the analysis of surface phase transitions, e.g.

R. Evans et.al. JCP 147, 044701 (2017)

Ref. [1], and refs. therein.

Check: In the approach to drying  $\cos\theta \rightarrow -1$ ,

$$\omega_B(l_{eq}) < 0.$$

For wetting, the liquid intrudes and reservoir is a vapour at  $\delta\mu = 0^-$ . Result corresponding to (3) is  $\omega_B(l_{eq}) = \gamma_{lv}(\cos\theta - 1) < 0$ .

2

(drying)

How  $\cos\theta + 1 \rightarrow 0$  depends on the form of  $\omega_B(l)$ , which depends in turn on the decay of ff and wf potentials.

We can also define a local compressibility via

$$\chi(z) \equiv \left( \frac{\partial p(z)}{\partial \mu} \right)_T$$

where  $p(z)$  is the density profile, and choose to approximate

$$\chi(l_{eq}) \approx -\rho'(z=l_{eq}) \left( \frac{\partial l_{eq}}{\partial \mu} \right)_T \quad (4)$$

[What will be of interest is the product  $\chi(l_{eq})(\cos\theta + 1)$ ]

Consider SR ff with LR wf

for which <sup>critical</sup> drying occurs as  $\epsilon_w \rightarrow 0$  ↳ strength of wall-fluid attraction.

Then  $\omega_B(l) = a e^{-l/\xi_b} + b l^{-2}$  ↳ bulk corr. length of Vj intruding phase (5)

$$a > 0 \text{ and } b = -\Delta \rho \epsilon_w \xi_b^3 \sigma^{3/2} < 0 \quad (6)$$

see [1].  $\sigma = L_J$  diameter ↳ well-depth.

Requiring  $\left. \frac{\partial \omega}{\partial l} \right|_{l_{eq}} = 0$

yields  $\frac{a e^{-l_{eq}/\xi_b}}{\xi_b} = -2b l_{eq}^{-3}, \delta \mu = 0^+$  (7)

and Eq (30) of Ref [1] which was tested in [1], for small  $\epsilon_w$ , using SFT.

The local compressibility is easily calculated:

$$\left( \frac{\partial l_{eq}}{\partial \mu} \right)_T = -\Delta \rho \left( \frac{a e^{-l_{eq}/\xi_b}}{\xi_b^2} + \frac{6b}{l_{eq}^4} \right)^{-1} = -6\rho \frac{a e^{-l_{eq}/\xi_b}}{\xi_b^2} \frac{3ae^{-l_{eq}/\xi_b}-4\xi_b-1}{5\xi_b^4}, \delta \mu = 0^+ \quad (8)$$

augments Eq (32) of [1]. To obtain the contact angle  $\theta$  we use (3).

Substituting (7) into (5) we find

$$\begin{aligned} \omega_B(l_{eq}) &= a e^{-l_{eq}/\xi_b} - \frac{a l_{eq}}{2 \xi_b^2} e^{-l_{eq}/\xi_b} \\ &= a e^{-l_{eq}/\xi_b} \left[ 1 - \frac{l_{eq}}{2 \xi_b} \right] \end{aligned} \quad (9)$$

**Check:** In the approach to (critical) drying  $\epsilon_w \rightarrow 0$ , 2nd term in (9)  $\gg$  1st and  $\omega_B(l_{eq}) < 0$ .

Using Eq (30) of [1] (see next pg.)

$$\omega_B(l_{eq}) \approx a \epsilon_w \left( \frac{l_{eq}}{\xi_b} \right)^{-3} \left( \frac{-1}{2} \right) \left( \frac{l_{eq}}{\xi_b} \right)$$

2

(drying)

How  $\cos\theta + 1 \rightarrow 0$  depends on the form of  $\omega_B(l)$ , which depends in turn on the decay of ff and wt potentials.

We can also define a local compressibility via

$$\chi(z) = \left( \frac{\partial \rho(z)}{\partial \mu} \right)_T$$

where  $\rho(z)$  is the density profile, and choose to approximate

$$\chi(l_{eq}) \approx -\rho'(z=l_{eq}) \left( \frac{\partial l_{eq}}{\partial \mu} \right)_T \quad (4)$$

[What will be of interest is the product  $\chi(l_{eq})(\cos\theta + 1)$ ]

Consider SR ff with LR wf

for which <sup>critical</sup> drying occurs as  $\epsilon_w \rightarrow 0$  ↳ strength of wall-fluid attraction.

Then  $\omega_B(l) = a e^{-l/\xi_b} + b l^{-2}$  <sup>bulk</sup> <sub>corr length of V<sub>j</sub> intruding phase</sub> (5)

$$a > 0 \text{ and } b = -\Delta \rho \epsilon_w \xi_b^3 \sigma^3/2 < 0 \quad (6)$$

see [1].  $\sigma = L_J$  diameter ↳ well-depth.

Requiring  $\left. \frac{\partial \omega}{\partial l} \right|_{l_{eq}} = 0$

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The local compressibility is easily calculated:  $\left( \frac{\partial l_{eq}}{\partial \mu} \right)_T = -\Delta \rho \left( \frac{a e^{-l_{eq}/\xi_b}}{\xi_b^2} + \frac{6b}{l_{eq}^2} \right)^{-1} = -\Delta \rho \frac{a e^{-l_{eq}/\xi_b}}{\xi_b^2} \frac{3a e^{-l_{eq}/\xi_b} - 4\xi_b - 1}{3\xi_b l_{eq}}, \delta \mu = 0^+$  (8)

augments Eq (32) of [1]. To obtain the contact angle  $\theta$  we use (3).

Substituting (7) into (5) we find

$$\begin{aligned} \omega_B(l_{eq}) &= a e^{-l_{eq}/\xi_b} - \frac{a l_{eq}}{2 \xi_b^2} e^{-l_{eq}/\xi_b} \\ &= a e^{-l_{eq}/\xi_b} \left[ 1 - \frac{l_{eq}}{2 \xi_b} \right] \end{aligned} \quad (9)$$

**Check:** In the approach to (critical) drying  $\epsilon_w \rightarrow 0$ , 2nd term in (9) >> 1st and  $\omega_B(l_{eq}) < 0$ .

Using Eq (30) of [1] (see next pg.)

$$\omega_B(l_{eq}) \approx a \epsilon_w \left( \frac{l_{eq}}{\xi_b} \right)^{-3} \left( \frac{-1}{2} \right) \left( \frac{l_{eq}}{\xi_b} \right)$$

$$-\frac{\partial \theta}{\partial \xi} = \ln \xi_w - 3 \ln \left( \frac{\partial \theta}{\partial \xi} \right) + \text{const.} \quad (30) \text{ of } [1]$$

It follows that

$$\omega_B (\frac{\partial \theta}{\partial \xi}) \approx -\frac{\alpha}{2} \xi_w \left( \frac{\partial \theta}{\partial \xi} \right)^{-2} \approx -\frac{\alpha}{2} \xi_w (-\ln \xi_w)^{-2}$$

so from (3)

$$(\cos \theta + 1) \gamma_{ev} \approx \frac{\alpha}{2} \xi_w (-\ln \xi_w)^{-2}, \quad \xi_w \rightarrow 0$$

This has correct dimensions and is (36) of [1].

We attempt to combine (8) and (9)

$$\begin{aligned} \omega_B (\frac{\partial \theta}{\partial \xi}) \cdot \frac{(\partial \theta)}{\partial \mu} &= \cancel{\alpha e^{-\frac{\partial \theta}{\partial \xi}} \left[ 1 - \frac{\partial \theta}{\partial \xi} / 2 \xi_b \right]} \cdot \cancel{\left( -\frac{4 \rho}{\xi_b} \right) \left[ \frac{-\partial \theta}{\partial \xi} \right]} \\ &\quad \left( \frac{1}{\xi_b} - \frac{3}{\partial \theta} \right)^{-1} \\ &= -\Delta p \xi_b \left[ 1 - \frac{\partial \theta}{\partial \xi} / 2 \xi_b \right] / \left( \frac{1}{\xi_b} - \frac{3}{\partial \theta} \right) \\ &= -\Delta p \left[ 1 - \frac{\partial \theta}{\partial \xi} / 2 \xi_b \right] \xi_b^2 / \left( 1 - 3 \xi_b / \partial \theta \right) \end{aligned}$$

{ Has correct dimensions }

$\xrightarrow{?}$  dominates near drying (16)

Check: in approach to drying  $\xi_w \rightarrow 0$ , this product must vary as l.h.s.

$$\xi_w (-\ln \xi_w)^{-2} \cdot \xi_w^{-1} (-\ln \xi_w)^3 = (-\ln \xi_w) \quad \checkmark$$

but r.h.s.  $\sim \frac{\partial \theta}{\partial \xi} \sim \frac{\partial \theta}{\partial \xi} \sim (-\ln \xi_w) \therefore \text{OK.}$

Translate  $\gamma$  to contact angle using (3):

$$\begin{aligned} -\gamma_{ev} (\cos \theta + 1) \left( \frac{\partial \theta}{\partial \mu} \right)_T &= -\frac{\Delta p}{\xi_b} \left[ 1 - \frac{\partial \theta}{\partial \xi} / 2 \xi_b \right] / \left( 1 - 3 \xi_b / \partial \theta \right) \\ &= -\xi_b^2 \Delta p \left[ 1 - \frac{\partial \theta}{\partial \xi} \right] \left[ 1 + \frac{3 \xi_b}{\partial \theta} + \frac{9 \xi_b^2}{\partial \theta^2} + \dots \right] \end{aligned}$$

(Assuming  $3 \xi_b / \partial \theta \ll 1$ )

$$= -\xi_b^2 \Delta p \left[ \frac{-\partial \theta}{2 \xi_b} + 1 + \frac{3 \xi_b}{\partial \theta} - \frac{3}{2} + \frac{9 \xi_b^2}{\partial \theta^2} - \frac{9 \xi_b}{2 \partial \theta} \right]$$

$$\therefore \gamma_{ev} (\cos \theta + 1) \left( \frac{\partial \theta}{\partial \mu} \right)_T = \xi_b^2 \Delta p \left[ -\frac{\partial \theta}{2 \xi_b} - \frac{1}{2} - \frac{3}{2} \frac{\xi_b}{\partial \theta} + O\left(\frac{\xi_b}{\partial \theta}\right) \right]$$

{ Has correct sign near drying:  $(\frac{\partial \theta}{\partial \mu})_T \sim 0$  } (11)

We now use (4) to introduce  $\chi(\xi_b)$ :

$\boxed{?} = A$

$$\gamma_{ev}(\cos\theta+1)\chi(l_{eq}) = -\rho'(l_{eq})\xi_b^2 \Delta p [A] \quad (12)$$

Recall in Bet K:  $\chi_b = (\frac{\partial p}{\partial \mu})_T = \rho_b^{-2} \chi_c$   
 where  $\xi_b$  refers to  $\xi_v$  for drying  
 usual isothermal compressibility

Eq. (12) suggests we reconsider the formula for the ev surface tension given in Perry et.al. (2016)

Here we have

$$\gamma_{ev} = f_2 (\Delta p)^2 \quad (13)$$

(Their (85))

- Notation This follows from a square-gradient SFT. Perry:  $\sigma \equiv \gamma_{ev}$  = liquid-vapor tension in the SFT
- $f_2$  is the coeff. of the sq. gradient term and is assumed to be constant.

If we choose to focus on the bulk liquid

compressibility (bulk corr. length):  $\xi_l^2 = f_2 / \phi''(p_e)$ .

And  $\chi_b^l = [\phi''(p_e)]^{-1}$ , refers to liquid.

Here  $\phi(p)$  is the bulk free energy density.

correlation length:  $\xi_l^2 = f_2 \chi_b^l$  see also B.Q. Lu et.al (1985) below.

It follows that from (13):  $\gamma_{ev} = \xi_l^2 / \chi_b^l \cdot (\Delta p)^2$

where we choose to focus on the bulk liquid compressibility.

Now substitute into (12):

$$(\cos\theta+1) \xi_l^2 \frac{\chi(l_{eq})}{\chi_b^l} \frac{(\Delta p)^2}{3(\xi_l + \xi_v)} = -\rho'(l_{eq}) \xi_b^2 \Delta p [A]$$

Recall: in the case of drying:  $\xi_b = \xi_v$ : the vapor is intruding.

$$\therefore (\cos\theta+1) \frac{\chi(l_{eq})}{\chi_b^l} = -\frac{\rho'(l_{eq})}{\Delta p} 3(\xi_l + \xi_v) \left(\frac{\xi_v}{\xi_l}\right)^2 [A] \quad (15)$$

[Check: dimensionality]

We might suppose:  $\rho'(\text{deg}) \approx \Delta\rho/w$   
 measure of width  $w$  of 'interface'

Then (15) reduces to:

$$\begin{aligned} (\cos\theta + 1) \frac{\chi(\text{deg})}{\chi_b^l} &= -\frac{3}{w} (\xi_e + \xi_v) \left( \frac{\xi_v}{\xi_e} \right)^2 [A] \\ &= -\frac{3}{w} \xi_e \left( 1 + \frac{\xi_v}{\xi_e} \right) \left( \frac{\xi_v}{\xi_e} \right)^2 \left[ -\frac{\text{deg}}{2\xi_e} - \frac{1}{2} \frac{3}{2} \frac{\xi_v}{\xi_e} \right] \\ &\quad + H.O. \end{aligned} \quad (16)$$

is tve. ✓  
Estimated:  $\xi_v/\xi_e \sim 0.42$  at  $T/T_c = 0.7$

$$\begin{aligned} (\cos\theta + 1) \frac{\chi(\text{deg})}{\chi_b^l} &= +3 (1.42) 0.42^2 \frac{\text{deg}/w}{2 \times 1.42} \\ &= 0.89 \frac{\text{deg}}{w} \quad \text{at leading order} \end{aligned} \quad (17)$$

+ B.Q. Lee, R. Evans and M.M. Telo da Gama  
 Molec. Phys. 55, 1819, (1985)

See Figs. 3 & 4.  
 Note: These refer to bulk correlation lengths from a square gradient theory. More sophisticated approaches will yield different ratios.

+ The same paper indicates (Fig. 10) that the width of the free v. interface is  $\approx 2.5 \frac{\text{deg}}{w}$  for  $T/T_c = 0.7$ .

### Remarks:

- The analysis presented is for large contact angle  $\theta > \pi/2$  and should be 'exact' in the limit of critical drying:  $(\cos\theta + 1) \rightarrow 0$ , when ff is SR and wf is LR. This case is the easiest to analyse since we know critical drying occurs as  $\omega \rightarrow 0$ .
- How general might the conclusion be? We should consider other bonding potentials that lead to other types of drying or wetting transitions. In particular we need to understand a 1st order wetting transition. What does the product  $(1 - \cos\theta)\chi(\text{deg})$  look like in this situation?
- How far can one trust a formula such as (17)

when one is not very close to drying, i.e. when  $\cos\theta$  is substantial and  $\cos\theta \approx -1$ . In these circumstances  $l_{eq}$  is small,  $\approx \sigma_{LJ}$ , the fluid-fluid diameter.

The work of Many Coe suggests that binding potential predictions work down to surprisingly small length scales, so there is hope that these might provide insight outside the critical drying regime.

iv) Eq (17) has an interesting structure. On l.h.s.  $\cos\theta = (\delta_{wv} - \delta_{vw})/\delta_v$  is clearly determined by macroscopic quantities. On r.h.s.  $\chi^l$  is clearly the (macroscopic) bulk K "compressibility".  $\kappa(l_{eq})$  is a local quantity. On the r.h.s. we have interfacial quantities pertaining to a near-drying situation or simulation. Obviously, within SFT one could calculate  $\kappa(l_{eq})$ . And  $l_{eq}$  is defined via the Gibbs adsorption:  $\Gamma = \int dz (\kappa(z) - \rho_b) = -\delta p_{eq}$ , for drying.

The r.h.s. is a mixture of macroscopic (integrated) quantities  $\Gamma$  and a local measure  $w$ .

v) Clearly one might test (16) or (17) within SFT or simulation, especially away from critical drying. What might one learn?

Bobs (25/10/22).

N.B. a) I should check out paper by J.R. Henderson where I think he showed how to generate a flat density profile at a wall, perfectly.

b) When we consider the binding potential  $w_B(l)$  I am reminded of the work K (simulation) by J.R. Forington. We should look at this.